REGIONE EMILIA ROMAGNA

PROVINCIA DI BOLOGNA

COMUNE DI SALA BOLOGNESE

COMUNE DI CALDERARA

COMUNE DI SAN GIOVANNI IN PERSICETO

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Opera	Progetto di realizzazione di un Impianto agrivoltaico integrato con un sistema di accumulo e opere connesse nei Comuni di Sala Bolognese (BO), Calderara di Reno (BO) e San Giovanni in Persiceto (BO) denominato "Pratello"		
Oggetto	Codice elaborato: PRASS0R01-00		
	Titolo elaborato: Relazione geologico-sismica		

00	13/12/2024	Emissione per progetto definitivo	Dott. Geol. Giulia Gardosi Dott. Geol. Maurizio Zamboni	Ing. Sara Simone	Ing. Fabio Domenico Amico
Rev.	Data	Oggetto della revisione	Elaborazione	Verifica	Approvazione

Comune di Sala Bolognese (BO)

Sala Bolognese - Località: Capoluogo

Oggetto: Studio geologico*) relativo alla realizzazione di un campo agrivoltaico nel comune di Sala Bolognese e di opere connesse (progetto denominato "Pratello").

- Relazione geologica-

- Modellazione geofisica -

dicembre 2024

-------- Indice:

-------- **Tavole:**

- corografia: _____ C.T.R. 1:25.000
- carta geologica: _____ C.T.R. 1:10.000

Tav.1 - inquadramento generale: _____ C.T.R. 1:10.000
Tav.2 - ubicazione indagini: _____ 1: 10.000
Tav.3a - sezioni stratigrafiche interpretative: _____ 1: 200
Tav.3b - sezioni stratigrafiche interpretative: _____ 1: 200
Tav.3c - sezioni stratigrafiche interpretative: _____ 1: 200

-------- **Allegati:**

- **Prove penetrometriche** –

Cptm: - diagrammi di resistenza; - tabelle valori di resistenza;
- valutazioni litologiche; - parametri geotecnici;

Cptu: - diagrammi di resistenza; - valutazioni litologiche;
- parametri geotecnici;

- **Sismica** - report indagini sismiche;
- parametri sismici;

- **report verifica liquefazione**

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1. Premessa

Su incarico della committenza, è stato svolto il presente studio geologico, di modellazione geofisica a corredo del progetto per la realizzazione di un campo agrivoltaico nel comune di Sala Bolognese e di opere connesse (progetto denominato "Pratello").

Al fine di verificare l'idoneità geologica e geomorfologia del sito è stato eseguito un primo sopralluogo sull'area, i cui risultati, unitamente alle conoscenze desunte dalla bibliografia ed a dati in possesso dello scrivente relativi all'area in esame, hanno permesso di definire una prima conoscenza dell'area. Inoltre è stata condotta una iniziale campagna di indagini geognostiche e geofisiche, al fine di definire la caratterizzazione litostratigrafia, geofisica del terreno.

Scopo dello studio è dunque fornire l'inquadramento geologico, idrologico, idrogeologico nonché sismico necessario per effettuare le necessarie valutazioni di compatibilità dell'opera in progetto con le peculiarità dei luoghi. Per quanto riguarda l'aspetto sismico il presente studio fa riferimento alla classificazione sismica dei Comuni, definita nell'allegato 1- punto 3, dell'O.P.C.M. 3274 del 20/03/2003, nel quale il comune di Sala Bolognese è classificato di zona sismica 3.

2. Quadro normativo di riferimento adottato

- R.D. n. 3267 del 30 dicembre 1923 "*Riordinamento e riforma della legislazione in materia di boschi e di terreni montani*";
- R.D. n. 1126 del 16 maggio 1926 "*Approvazione del regolamento per l'applicazione del regio decreto 30 dicembre 1923, n. 326, concernente il riordinamento e la riforma della legislazione in materia di boschi e di terreni montani*";
- R.D. n. 1775 del 11 dicembre 1933 "*Approvazione del testo unico delle disposizioni di legge sulle acque e sugli impianti elettrici*";
- Legge n. 64 del 2 febbraio 1974 "*Provvedimenti per le costruzioni con particolari prescrizioni per le zone sismiche*";
- AGI – Associazione Geotecnica Italiana, giugno 1977 "*Raccomandazioni sulla programmazione ed esecuzione delle indagini geotecniche*";
- D.Min.LL.PP. 11 marzo 1988 "*Norme tecniche riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione e il collaudo delle opere di sostegno delle terre e delle opere di fondazione*";
- Circ. LL.PP. n. 30483 del 24/09/1988 "*Istruzioni riguardanti le indagini sui terreni e sulle rocce, la stabilità dei pendii naturali e delle scarpate, i criteri generali e le prescrizioni per la progettazione, l'esecuzione ed il collaudo delle opere di sostegno delle terre e delle opere di*

fondazione";

- Legge n. 36 del 5 gennaio 1994 "*Disposizioni in materia di risorse idriche*";
- EN 1997 (2002) – Eurocode 7 "*Geotechnical Design*";
- EN 1998 (2003) – Eurocode 8 "*Design of structures for earthquake resistance*"
- Ordinanza n.3274 della Presidenza del Consiglio dei Ministri del 20 marzo 2003 "*Primi elementi in materia di criteri generali per la classificazione sismica del territorio nazionale e di normative tecniche per le costruzioni in zona sismica*" e successivi aggiornamenti:
    - Ordinanza n.3316 della Presidenza del Consiglio dei Ministri del 2 ottobre 2003;
    - Ordinanza n.3431 della Presidenza del Consiglio dei Ministri del 3 maggio 2005;
- D.Min.LL.PP. 14 settembre 2005 "*Norme tecniche per le costruzioni*";
- D. Lgs. n. 152 del 03 aprile 2006 "*Norme in materia ambientale*" e s.m.i.;
- D.Min.LL.PP. 14 gennaio 2008 "*Nuove norme tecniche per le costruzioni*";
- Circolare Min.LL.PP. 2 febbraio 2009 n. 617 "*Istruzioni per l'applicazione delle "Nuove norme tecniche per le costruzioni" di cui al D.M. 14 gennaio 2008*";
- D.Min.LL.PP. 17 gennaio 2018 "*Aggiornamento delle norme tecniche per le costruzioni*";

2.1. NORME REGIONALI

- Legge della Regione Emilia-Romagna n. 47 del 7 dicembre 1978 "*Tutela ed uso del territorio*";
- Legge della Regione Emilia-Romagna n. 20 del 24 marzo 2000 "*Disciplina generale sulla tutele e l'uso del territorio*";
- Legge della Regione Emilia-Romagna n. 17 del 18 luglio 1991 "*Disciplina delle Attività Estrattive"* e s.m.i.;
- Legge della Regione Emilia Romagna n 9 del 18 maggio 1999 "*Disciplina della procedura di valutazione dell'impatto ambientale*";
- Delibera della Giunta Regionale n. 1117 del 11 luglio 2000 "*Direttiva regionale concernente le procedure amministrative e le norme tecniche relative alla gestione del vincolo idrogeologico, redatta ai sensi ed in attuazione degli artt. 148, 149, 150 e 151 della L.R. 21 aprile 1999 n. 3 "Riforma del sistema regionale e locale'"*";
- Legge della Regione Emilia-Romagna n. 31 del 25 novembre 2002 "*Disciplina generale dell'edilizia"* e s.m.i;.
- Delibera di Giunta Regionale n.1677 del 24 ottobre 2005, "*Prime indicazioni applicative in merito al decreto ministeriale 14 settembre 2005 (pubblicato sul supplemento ordinario n.159 alla G.U. n.222 del 23 settembre 2005) recante* "Norme tecniche per le costruzioni"";
- Deliberazione dell'Assemblea legislativa n. 112 del 2 maggio 2007:"Approvazione dell'atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, comma 1, della L.R. 20/2000 "Disciplina

generale sulla tutela e l'uso del territorio", in merito a"indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica". (Proposta della Giunta regionale in data 10 gennaio 2007, n.1);

- Legge della Regione Emilia Romagna n 19 del 30 ottobre 2008 "*Norme per la riduzione del rischio sismico*";
- Delibera di Giunta Regionale n.687 del 23 maggio 2011, "*Atto di indirizzo recante l'individuazione degli interventi privi di rilevanza per la pubblica incolumità ai fini sismici e delle varianti in corso d'opera, riguardanti parti strutturali, che non rivestono carattere sostanziale, ai ai sensi dell'articolo 9, comma 4 della L.R. n. 19 del 2008*".
- Delibera di Giunta Regionale n.2193 del 21 dicembre 2015, "*Atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, c. 1, della LR 20/2000 per "Indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica"*.
- Delibera di Giunta Regionale n.630 del 29 aprile 2019, "*Atto di coordinamento tecnico sugli studi di microzonazione sismica per la pianificazione territoriale e urbanistica (artt. 22 e 49, della LR 24/2017)"*.
- Delibera di Giunta Regionale n.476 del 12 aprile 2021, "*Aggiornamento dell'"atto di coordinamento tecnico sugli studi di microzonazione sismica per la pianificazione territoriale e urbanistica (artt. 22 e 49, l.r. n. 24/2017)" di cui alla deliberazione della giunta regionale 29 aprile 2019, n. 630."*.

3. Inquadramento topografico, lineamenti geomorfologici

Il sito di futura realizzazione del campo agrivoltaico si localizza tra gli elementi C.T.R. N° 202163 – SALA BOLOGNESE – e N°220044 – COLOMBAROLA-.

L'area di futura realizzazione del campo agrivoltaico è individuata dai toponimi "*Podere Croce Bianca*", "*Podere Giorgina*" e "*Torre Gamberino*", e sarà posto ad est del centro abitato di Sala Bolognese, tra la Strada Provinciale 18 e lo Scolo Dosoletto; l'accesso all'area potrà avvenire sempre dalla Strada Provinciale 18 e la quota media del piano campagna si aggira tra 23,2 e 23,5 m s.l.m..

Il contesto morfologico di entrambe le aree è di tipo sub pianeggiante; le quote topografiche degradano lievemente verso nord-est, senza particolari elementi che alterino la monotonia morfologica ad eccezione degli argini di fossi e scoli di natura antropica che corrono in direzione sud-ovest nord-est.

Il territorio in esame appartiene alla fascia della media pianura, al di fuori delle conoidi alluvionali (Reno, Savena-Idice) pede-appenniniche, costituitasi tra l'area dell'Alta Pianura Padana Appenninica e la zona di Bassa Pianura Padana.

Le zone di pianura non costituiscono un'unità morfologica piatta ed uniforme; sono infatti

caratterizzate da strisce rilevate, dette dossi, corrispondenti ad alvei antichi (paleoalvei) od attuali, alternati a zone depresse, dette valli, che, fino a quando i corsi d'acqua non sono stati regimati, raccoglievano le acque di esondazione.

Caratteristica comune a tutta la pianura del bolognese, è l'andamento morfologico che vede l'alternanza di dossi e conche morfologiche. I dossi veri e propri hanno forma allungata secondo l'asse del canale fluviale, profilo convesso e gradiente di pendenza, normale all'asse, in genere non superiore allo 0.2%; nei casi più marcati si percepisce anche visivamente che i dossi costituiscono le porzioni di pianura alluvionale più rilevate. Le conche morfologiche, invece, sono zone topograficamente più depresse della pianura alluvionale, in cui le acque di rotta o esondazione, con i loro sedimenti, non sono riuscite ad innalzare il livello del suolo in maniera adeguata rispetto alle aree limitrofe. La principale funzione idrologica di queste aree è quella di fungere da casse di espansione naturali alle piene eccezionali dei canali fluviali, quindi hanno funzione di regimazione ed equilibrio idraulico. Le conoidi dell'alta pianura sono frequentemente dotate di ridotte protezioni naturali delle sottostanti falde.

L'evoluzione della pianura olocenica è fondamentalmente governata sia dalla tettonica, quali le grandi pieghe del ferrarese che hanno determinato nel tempo uno spostamento verso nord-est del corso del Fiume Po, che dalla subsidenza (circa 2 cm/anno); i fenomeni ricorrenti di rotte e tracimazione depositano in sequenza prima i materiali più grossolani e successivamente i materiali più fini nelle aree interfluviali e di conca ove spesso decantano in acque stagnanti (paludi). Pertanto le continue modifiche dei corsi d'acqua, dovute sia alla strutturazione tettonica della pianura che alla subsidenza, hanno prodotto una variegata sovrapposizione di sedimenti rappresentati da lenti sabbiose e/o ghiaiose (paleo alvei) e da sedimenti a tessitura fine (riempimenti dei bacini interfluviali di esondazione).

Per la datazione ed attribuzione idrografica dei paleoalvei dei fiumi della Pianura Padana occorre fare riferimento agli autori più recenti che si sono occupati della ricostruzione paleoidrografica della zona: Pellegrini (1969), Veggiani (1947), Castaldini et Alii (1979), Cremaschi et Alii (1980), Gasperi e Pellegrini (1981, 1984). In base alle informazioni reperite in merito, recenti studi indicherebbero, per i paleoalvei principali presenti nell'area di studio, una datazione risalente al XIII secolo.

La frequente corrispondenza riscontrata nell'area esaminata tra dossi e paleoalvei è spiegabile analizzando, dal punto di vista dei processi di sedimentazione, il modello evolutivo della pianura olocenica, almeno nelle linee generali. I fiumi appenninici, a valle delle conoidi pedemontane, tendono a proseguire verso il collettore principale su alvei pensili formati da sedimenti che il corso d'acqua non è più in grado di portare a carico.

Nel caso di rotte e tracimazioni, le acque si espandono nella pianura depositando, nelle immediate vicinanze dell'alveo, i materiali più grossolani e più lontano, una volta cessato il flusso, i

sedimenti più fini. Questi ultimi sedimenti si costipano di più di quelli costituenti l'alveo e si determinano così, già per processi naturali, dei notevoli dislivelli fra fiumi e territori circostanti.

Per i corsi d'acqua di pianura, non arginati artificialmente, rotte e tracimazioni sono un fenomeno ricorrente che favorisce i cambiamenti d'alveo; in un bacino subsidente l'accrescersi della pianura avviene perciò sia orizzontalmente, con il giustapporsi di diversi successivi corpi d'alveo, che verticalmente, con il sovrapporsi di successivi cicli di riempimento dei bacini di esondazione.

I corsi d'acqua principali hanno tendenzialmente un andamento da Sud a Nord e sono a carattere torrentizio nella zona montana a Sud, con portate massime nei mesi di Marzo e Novembre e portate minime nel periodo Luglio-Agosto; in pianura perdono i caratteri di corsi d'acqua naturali, avendo subito arginature, deviazioni e alterazioni di vario tipo legate ad opere di bonifica. Essi corrono generalmente in pensile; le loro torbide sono state impiegate per lungo tempo allo scopo di bonificare mediante le "casse di colmata", creando in tal modo le pianure bonificate a Nord.

L'alta pianura è essenzialmente caratterizzata dalla presenza dei conoidi alluvionali riferibili alla attività deposizionale del F. Reno, del T. Lavino e del T. Samoggia che hanno modellato la fascia pedecollinare rispettivamente in corrispondenza del settore orientale ed occidentale dell'area in esame. Fra le strutture di conoide principali si interpongono delle strutture minori.

In ultimo si ricorda l'intenso intervento antropico di bonifica del settore bolognese a partire dall'età preromana fino al XIV sec. con notevole variazione dei corsi d'acqua come la deviazione dell'alveo del fiume Reno e la bonifica delle paludi con l'attuale pensilità dei corsi d'acqua nella pianura bolognese.

4. Modello geologico

Come detto, l'area in esame appartiene alla fascia della Media-Bassa Pianura ed è costituita, come il restante comparto di pianura, da terreni di origine pluviale-fluvioglaciale, formati dai sedimenti che, dal periodo post-glaciale sino al periodo storico, fiumi e torrenti vennero via via depositando nel loro vagare.

Il territorio dell'Emilia Romagna è costituito dal versante padano dell'Appennino settentrionale e dalla Pianura Padana a sud del Fiume Po. Pur essendo due ambienti geomorfologici distinguibili, essi risultano strettamente correlati fra loro: il fronte della catena appenninica non coincide con il limite morfologico catena montuosa-pianura, ma è individuabile fra gli archi esterni delle Pieghe Emiliane e Ferraresi (Pieri & Groppi, 1981), sepolte dai sedimenti quaternari della Pianura Padana. Il fronte appenninico sovrascorre verso nord sulla piattaforma padano-veneta; di conseguenza l'evoluzione del territorio dell'Emilia Romagna risulta strettamente legata ai cambiamenti del settore esterno della catena nord-appenninica. Le faglie derivanti dai movimenti dei sovrascorrimenti appenninici danno origine alle manifestazioni sismiche che interessano la Regione.

L'intero territorio del comune di Sala Bolognese risulta compreso fra il *Fronte di accavallamento pedeappenninico* ed il *Fronte di accavallamento esterno* che insiste sull'avampaese, rappresentato dalla Pianura Padana; la zona di alta pianura appartiene strutturalmente alla "Fascia Sepolta" caratterizzata da tettonica di embricazione (ancora attiva) coperta dai depositi continentali quaternari. La parte del territorio del Comune verso le zone pianeggianti, risulta all'interno nel bacino subsidente pliocenico-quaternario della Pianura Padana, costituito da una ampia depressione a stile compressivo colmata da sedimenti mesozoici, terziari e quaternari; da un punto di vista tettonico-sedimentario è importante la subsidenza, avvenuta nel Pleistocene inferiore, che ha provocato la sedimentazione di diverse centinaia di metri di argilla marina. Le strutture tettoniche più significative sono gli accavallamenti a notevole continuità laterale e senso di trasporto tettonico verso nord-est che descrivono una struttura arcuata con una zona frontale (parallela al fronte appenninico), una zona laterale collegata alla linea del Sillaro ed una zona di raccordo a direzione obliqua. Queste strutture sembrano essersi originate già nella fase tettonica del *Messiniano sup*. (*fase intramessiniana*) Ulteriori strutturazioni e riattivazioni, anche molto importanti, sono inoltre evidenti nel *Pliocene* e nel *Pleistocene*, dove gli eventi tettonici lungo la linea del Sillaro si sono invertiti (da trascorrenza destra a trascorrenza sinistra).

La strutturazione neogenica, che ha deformato in tempi "recenti" le Sabbie di Imola (Gialle), si interrompe bruscamente lungo la valle del F. Reno, dove si nota una sensibile dislocazione del fronte appenninico che, nella parte orientale, risulta spostato di 3 km a nord. Queste dislocazioni ad andamento antiappenninico, caratterizzate da una storia geologica assai complessa, sono presenti lungo altri allineamenti come la linea dell'Idice.

Lungo il bordo appenninico esterno e la fascia di pianura antistante, gli elementi traslati ed impilati vengono a formare un vero e proprio prisma di accrezione tettonica neogenico che, sia per l'entità dell'ampliamento, sia per la complessa interferenza dell'attività tettonica con la deposizione, conferiscono al sistema il carattere di una marcata fossa tettonica.

Più a sud il territorio circostante è caratterizzato dal contatto tettonico per faglia verticale fra i terreni delle Successioni Epiliguri, presenti con la F.ne di Pantano (PAT) e F.ne di Cigarello (CIG), con i sottostanti *mélanges* o olistostromi (corpi sedimentari caotici sin-tettonici a tessitura a blocchi in matrice con aspetto brecciato) dell'Oligocene superiore-Miocene inferiore, ed i terreni neoautoctoni rappresentati dalle Argille Azzurre e dalle Sabbie gialle.

Nella media pianura le alluvioni sono per lo più riferibili ai fiumi appenninici, caratterizzati da una rete drenante orientata da SW a NE. Gli apporti fluviali hanno ricoperto i sedimenti marini che, nel settore del margine appenninico tra il T. Samoggia ed il T. Lavino, sono in successione continua dalla base del Pliocene al Pleistocene inferiore.

Di notevole interesse appaiono le strutture tettoniche attive evidenziate nella "Carta Sismotettonica della regione Emilia-Romagna" (figura 1 e 2) Ovvero:

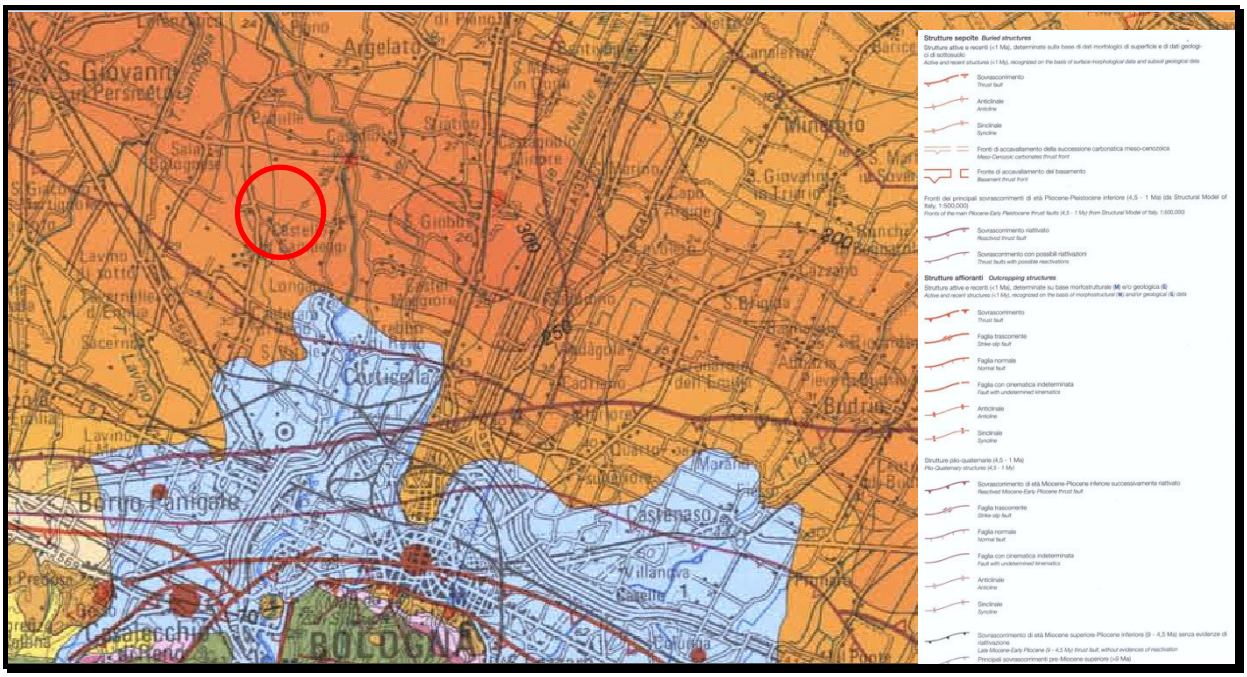


Figura 1: Estratto dalla Carta della Sismotettonica della Regione Emilia-Romagna.

STRUTTURE SEPOLTE

- Sovrascorrimento recente;
- Sovrascorrimento riattivati nell'area pedeappenninica;
- Sovrascorrimento con possibile riattivazione.

Queste strutture tettoniche sono aree sismogenetiche capaci di generare terremoti di cui si parlerà più avanti in testo.

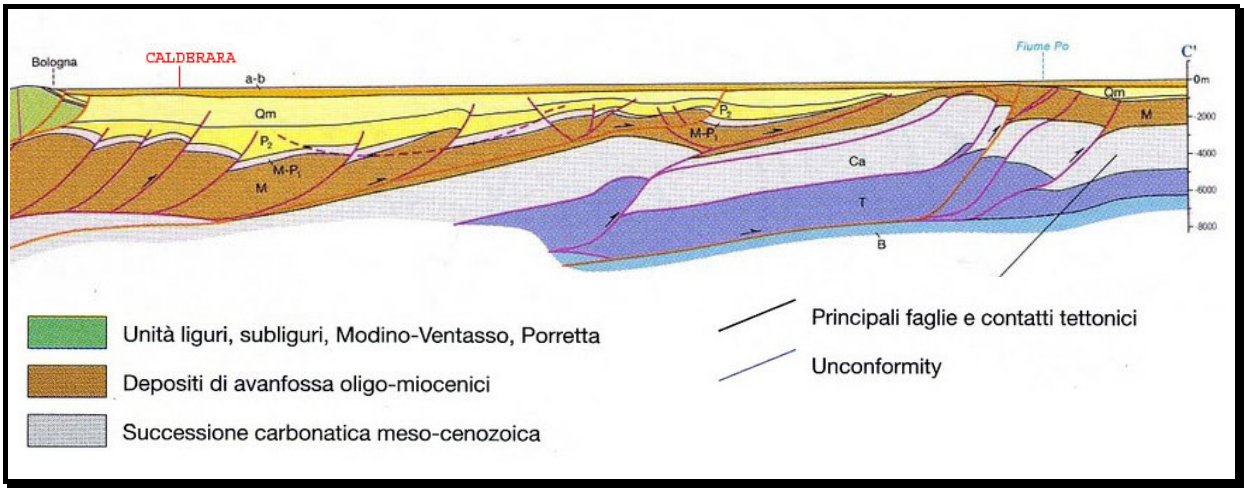


Figura 2: Estratto dalla sezione C-C' della Carta Sismotettonica della Regione Emilia-Romagna.

4.1 LITOSTRATIGRAFIA QUATERNARIA E SUPERFICIALE

Per la descrizione della successione stratigrafica riguardante i depositi quaternari presenti nel settore della pianura bolognese s.l. ospitante il sito oggetto d'intervento, si fa riferimento al quadro stratigrafico del sottosuolo padano adriatico riportato in fig. 3. L'assetto schematizzato evidenzia le principali unita stratigrafiche, definendone la gerarchia in termini di Sequenze Deposizionali.

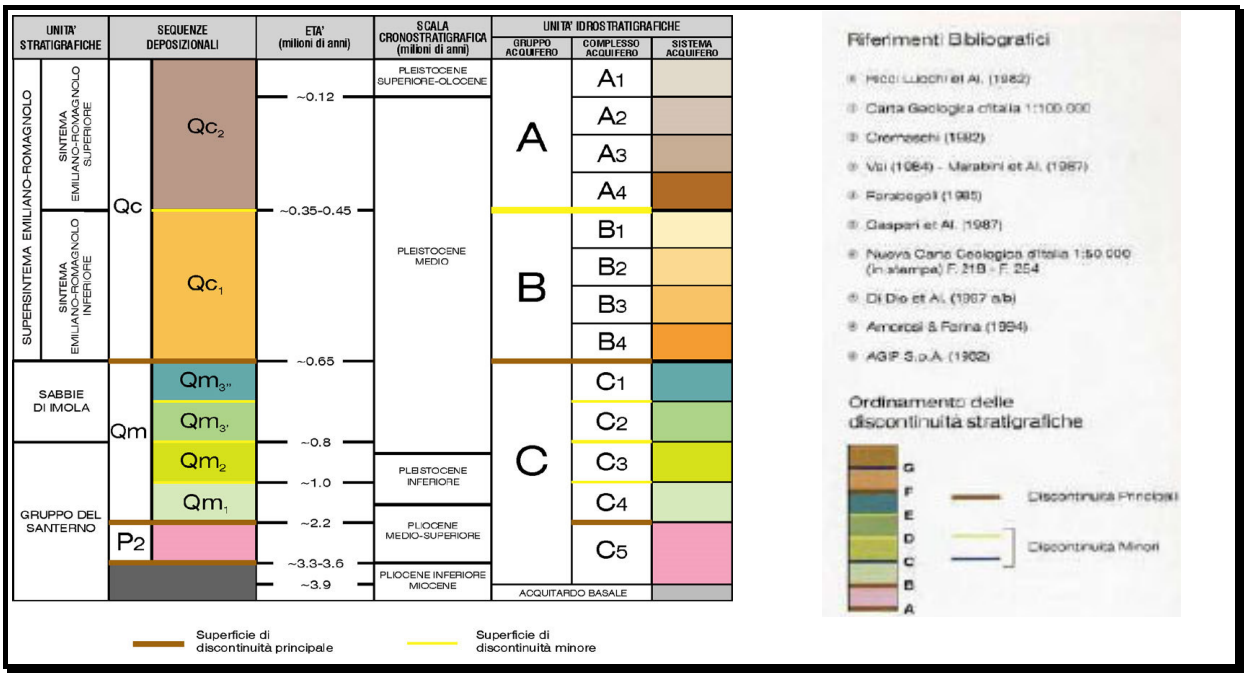


Figura 3: Gruppi acquiferi riferiti allo schema geologico-stratigrafico dell'Emilia-Romagna.

La suddivisione proposta tiene conto del fatto che i processi che hanno portato al riempimento del bacino padano, passando da una sedimentazione marina ad una continentale, sono avvenuti a seguito di eventi tettonico sedimentari generalmente molto intensi e discontinui, separati nel tempo da periodi di forte subsidenza bacinale e movimenti ridotti delle strutture compressive; la sussistenza e la successione di tali eventi è testimoniata dalle numerose superfici di discontinuità stratigrafica individuate e cartografate sul Margine Appenninico Padano. Attraverso i dati sismici e di pozzo, è stato possibile estendere tali superfici di discontinuità anche al sottosuolo della pianura e definirne, conseguentemente, il quadro stratigrafico. In tal senso, facendo riferimento allo schema di figura 2, i depositi plioquaternari di riempimento del bacino padano possono essere suddivisi, sulla base delle principali superfici di discontinuità riconosciute, in 3 Sequenze Principali, ovvero in 3 Supersintemi (o Allogruppi), secondo la terminologia delle Unconformity Bounded Stratigraphic Units (UBSU) utilizzata nella cartografia geologica di base della pianura (Carta Geologica in scala 1:50.000 della Regione Emilia Romagna):

1. Supersintema del Pliocene medio superiore;
2. Supersintema del Quaternario Marino;
3. Superintema Emiliano Romagnolo.

Tali sequenze rappresentano, da un punto di vista sedimentologico, la risposta alle tre principali fasi tettoniche di sollevamento regionale verificatesi, la prima tra circa 3.9 e 3.4 milioni di anni, la seconda tra 2.4 e 2.2 m.a., e la terza tra 0.80 e 0.65 m.a..

La presenza di superfici di discontinuità minori, legate a eventi tettonici secondari a carattere più locale, o ad oscillazioni climatiche eustatiche, hanno poi permesso di suddividere le Sequenze Principali in sequenze di rango inferiore, ovvero in Sintemi e Subsintemi. Tralasciando le due Sequenze Principali più antiche (Supersintema del *Pliocene medio-superiore* e Supersintema del Quaternario Marino), di scarso interesse per il presente studio data la loro profondità, si riportano di seguito i principali elementi caratterizzanti il Supersintema Emiliano Romagnolo (SER o AES), corrispondente alla porzione sommitale dei sedimenti di riempimento del bacino padano, la cui deposizione è avvenuta, come già ricordato, in risposta al sollevamento tettonico iniziato alla fine del *Pleistocene inferiore* e continuata nel *Pleistocene medio* fino a circa 0.65 m.a. Il Supesintema Emiliano Romagnolo, suddiviso nel Sintema Emiliano Romagnolo Inferiore (SERI o AEI), compreso tra 0.65 e 0.45 m.a., e nel Sistema Emiliano Romagnolo Superiore (SERS o AES), compreso tra 0.45 m.a. e l'attuale, è definito dall'insieme dei depositi quaternari di origine continentale affioranti sul margine appenninico padano e dai sedimenti ad essi correlati nel sottosuolo della pianura e del mare.

Delle due sequenze deposizionali di rango inferiore, il Sintema Emiliano Romagnolo Inferiore, il cui tetto è stato individuato a profondità mediamente comprese tra 220 e 280 metri, risulta essere caratterizzato da cicli deposizionali trasgressivo regressivi costituti da alternanze di depositi fini limoso argillosi e grossolani sabbioso ghiaiosi, riconducibili ad ambienti di piana alluvionale e, soprattutto, di piana fluvio-deltizia e piana costiera. Anche per quanto riguarda il Sintema Emiliano Romagnolo Superiore, i pertinenti depositi risultano essere organizzati in diversi cicli deposizionali sovrapposti, in cui sedimenti prevalentemente fini, riconducibili ad ambienti di argine e di piana inondabile, si alternano a sedimenti più grossolani, riconducibili ad ambienti di canale fluviale. Essendosi ormai esaurite le principali fasi tettoniche, la strutturazione deposizionale di tipo ciclico sopra schematizzata è da ricondurre, principalmente, a variazioni climatiche ed, in particolare, alle diverse fasi glaciali e interglaciali che si sono alternate durante il *Pleistocene*, nonché all'azione combinata della subsidenza, legata sia a cause tettoniche profonde, sia alla compattazione differenziale dei sedimenti plio-quaternari. Da un punto di vista paleogeografico le diverse fasi climatiche hanno determinato movimenti significativi della linea di costa adriatica, con avanzamenti massimi in corrispondenza delle fasi glaciali (regressione), ed arretramenti in corrispondenza delle fasi interglaciali (trasgressione). Al riguardo, si stima che durante la fase culminante dell'ultimo periodo glaciale (Wurm), iniziato circa 70.000 anni fa e terminato circa 15.000 anni fa, l'abbassamento del livello marino sia stato di quasi

100 metri rispetto al livello attuale; ciò ha portato ad una fase di forte alluvionamento dei corsi d'acqua ed alla deposizione di ingenti spessori di sedimenti continentali terrestri, lacustri e fluvio palustri, con conseguente espansione della pianura su gran parte dell'Adriatico settentrionale.

Gli ambienti deposizionali prevalenti dei sedimenti presenti sono depositi di canale, argine e rotta fluviale, oltre che di piana inondabile in aree interfluviali.

Entrambe le aree di studio sono dunque dominate da depositi alluvionali riferibili al Sistema Emiliano Romagnolo superiore AES della "Nuova Carta Geologica della Regione Emilia-Romagna"; si tratta di ghiaie, sabbie, limi ed argille di piana intravalliva, di conoide e di piana alluvionale. Sintema parzialmente suddiviso in subsintemi limitati, in affioramento, da scarpate di terrazzo fluviale e paleosuoli e nel sottosuolo della pianura da bruschi contatti fra depositi fini alluvionali e palustri su depositi grossolani di conoide e di piana (*Pleistocene medio – Olocene*).

Come meglio precisato le aree si trovano all'interno dei terreni dell'Unità di Modena AES8a; l'AES8a è caratterizzato da ghiaie, sabbie, limi ed argille. Il limite superiore, sempre affiorante, è dato da un suolo calcareo di colore bruno olivastro e bruno grigiastro privo di reperti archeologici romani, o più antichi, non rimaneggiati. Il limite inferiore è dato da una superficie di erosione fluviale nelle aree intra, il cui spessore massimo in pianura risulta 7 metri, nel sottosuolo circa 10m (*Età post-romana (IV-VI sec. d.C. - Attuale; datazione archeologica)*).

I sedimenti neoautoctoni alluvionali poggiano in profondità sui sedimenti continentali della Successione neogenico - quaternaria del margine appenninico padano

Dal punto di vista stratigrafico, quindi, il territorio in esame si presenta di una complessità non trascurabile dovuta ad interazioni strutturali fra unità litostratigrafiche differenti mentre, dal punto di vista stratigrafico locale, l'area di futuro intervento è più facilmente definibile.

Da ricerche bibliografiche si rileva che la litologia di superficie è costituita da suoli a diffusa componente organica ed a grado di drenaggio interno medio basso che ricoprono con continuità l'area fino alla roccia alterata ed alla roccia madre sottostante.

Sono suoli derivati da sedimenti alluvionali e lacustri recenti ("Carta dei suoli argillosi d'Italia"), principalmente *Eutric Fluvisols*, *Calcaric Fluvisol*, *Eutric* e *Fluvi-Eutric Cambisols, Fluvi-Vertic Cambisols*.

4.2 IDROLOGIA SUPERFICIALE E IDROGEOLOGIA

Quanto di seguito riportato è stato in parte tratto dalla Relazione Tecnica contenuta nella pubblicazione "Riserve Idriche Sotterranee della Regione Emilia Romagna" (edizioni S.E.L.C.A.– Firenze).

Nel sottosuolo della Pianura Padana e sul Margine Appenninico Padano, sono stati riconosciuti tre Gruppi Acquiferi separati da barriere di permeabilità con estensione regionale, informalmente denominati Gruppo Acquifero **A**, **B** e **C** a partire da piano campagna. Il Gruppo Acquifero **A** è

attualmente sfruttato in modo intensivo, il Gruppo Acquifero **B** è sfruttato solo localmente, il Gruppo Acquifero **C**, isolato rispetto la superficie per gran parte della sua estensione, è raramente sfruttato.

I Gruppi Acquiferi **A**, **B**, **C** sono a loro volta suddivisi in tredici U.L.S. (Unità Litostratigrafico–Sequenziale), gerarchicamente inferiori, denominati Complessi Acquiferi.

La differenziazione gerarchica si basa su:

- volume complessivo di acquiferi utili in ciascuna Unità;
- spessore, continuità ed estensione areale del livello acquitardo o impermeabile di ciascuna Unità.

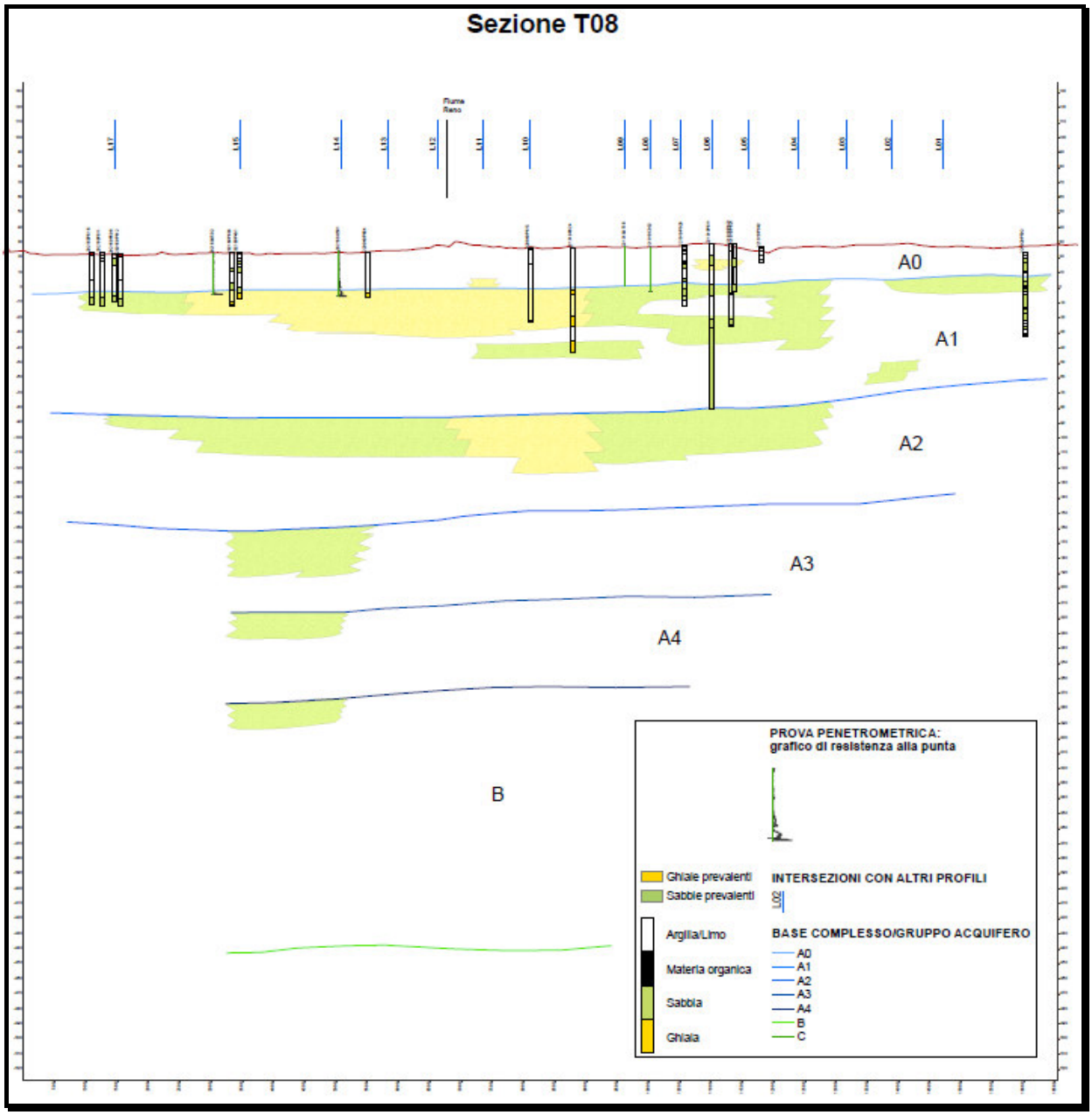


Figura 4: Schema dei rapporti stratigrafici della pianura Bolognese – Sezione T08.

Per quanto riguarda l'area di Sala Bolognese, il limite basale del gruppo acquifero **A** verrebbe indicato a circa -250 m dal livello del mare e per il gruppo acquifero **B** dovrebbe essere compreso all'incirca intorno ai -400 m di profondità dal livello del mare, con approfondimento passando da Sud, Sud- Est a Nord- Ovest e risollevamento dovuto alle pieghe sinclinaliche ed anticlinaliche delle varie unità tettoniche sottostanti.

Per quanto riguarda lo spessore cumulativo degli acquiferi utili relativi al gruppo acquifero **A**, intendendo per acquiferi utili quelli sfruttabili per uso idropotabile e/o per uso agricolo-industriale e la cui base corrisponde all'interfaccia tra acqua dolce e salmastra, i dati a disposizione evidenziano come, nella zona del territorio Comunale di Sala Bolognese, la potenza totale risulta variabile tra 80,00 m e 120,0 m circa e per quello B tra 40,0 m e 60,0 mentre.

Per quanto riguarda lo spessore cumulativo degli acquiferi utili relativi al gruppo acquifero **C**, intendendo per acquiferi utili quelli sfruttabili per uso idropotabile e/o per uso agricolo-industriale e la cui base corrisponde all'interfaccia tra acqua dolce e salmastra, i dati a disposizione evidenziano come, nella zona del territorio Comunale di Sala Bolognese, la potenza totale risulta di 100,0 m circa, a una profondità di -700 m dal livello del mare.

A migliore definizione si ricorda inoltre come, dal punto di vista idrogeologico, si intenda acquifero "*una formazione idrogeologica permeabile che permette il deflusso significativo di una falda idrica sotterranea e la captazione di quantità apprezzabili d'acqua con mezzi economici*".

In base alla definizione sopra riportata, la falda deve quindi avere un deflusso, il quale dovrà essere caratterizzato da spostamenti a prevalente componente orizzontale. Tale condizione è realizzabile in terreni dotati di adeguate caratteristiche di permeabilità e quindi, solo in tali casi, è identificabile una falda freatica in senso stretto. Nei restanti casi l'acqua presente corrisponde in realtà ad acqua di saturazione o di infiltrazione superficiale a movimento prevalentemente verticale anche se, di fatto, viene anch'essa comunemente definita "falda freatica".

Sulla base delle notizie bibliografiche, delle formazioni geologiche presenti e della posizione dell'area di studio (area di media pianura) la prima falda superficiale risulta a carattere stagionale, legata alle condizioni meteoclimatiche, e si trova nei primi metri a contatto fra litotipi diversi (sabbie e ghiaie permeate d'acqua a contatto con argille impermeabili); più probabile invece la presenza di falde più profonde determinate dal controllo tettonico (faglie e fessurazioni delle rocce sottostanti) e da contatti fra litotipi a differente grado di permeabilità che consentono il formarsi di riserve idriche sotterranee come nel caso delle Sabbie di Imola con l'acquifero del gruppo **C**; in considerazione dell'assetto morfologico e clivometrico del piano campagna non si rilevano settori con problemi di deflusso difficoltoso. Si rammenta comunque che, data la caratterizzazione litologica dei terreni presenti nell'area, sono assai probabili falde a carattere stagionale che permeano i primi metri di terreno. E' quindi consigliabile in fase di progettazione considerare queste acque di circolazione superficiale ed interagire con esse.

Si rammenta comunque, che, data la caratterizzazione litologica dei terreni presenti nell'area, sono pertanto assai probabili falde a carattere stagionale che permeano i primi metri di terreno. E' quindi consigliabile, in fase di progettazione, considerare queste acque di circolazione superficiale ed interagire con esse.

I litotipi presenti, sabbie, ghiaie, limi sabbiosi e argilla, sono caratterizzati i primi da un grado di porosità alto ed una elevata permeabilità (dovuta al grado di addensamento della sabbia), con porosità totale compresa fra 5÷20%. I secondi (argille) sono caratterizzati da una porosità primaria alta ed una secondaria bassa; la permeabilità è data fondamentalmente dalla porosità (sono rocce tendenzialmente impermeabili).

La circolazione idrica superficiale deriva direttamente dalle acque di infiltrazione e di ruscellamento; sono dunque importanti i meccanismi di percolazione (discesa dell'acqua verso il basso attraverso il terreno), con movimenti d'acqua lungo gli interstrati fra i litotipi a grado di permeabilità differente, ed i fenomeni sia capillari che di evapotraspirazione (risalita dell'acqua verso l'alto).

La rete idrografica superficiale è rappresentata fossi naturali ed antropici (es. Scolo Dosoletto e Canale Collettore Acque basse Bagnetto) che confluiscono a nord verso le reti di Bonifica o verso il Torrente Samoggia o il Torrente Lavino, quali collettori naturale principali, ed è caratterizzata da corsi d'acqua a carattere stagionale con forti piene nei periodi di maggiori piovaschi, e portate quasi nulla nei periodi di magra.

In perfetta coerenza con quanto sopra riportato, per l'area in esame si possono indicare le seguenti caratteristiche idrogeologiche:

- direzione di deflusso: da Sud- Ovest verso Nord- Est;

Dai riscontri dei dati storici si può riscontrare come le aree in esame ed i suoi immediati dintorni possano essere interessate da fenomeni di alluvionamenti locali.

Alcune veloci considerazioni sullo stato degli acquiferi della pianura bolognese.

Gli acquiferi della pianura alluvionale costituiscono l'acquedotto naturale per eccellenza e sono utilizzati da millenni per rifornire d'acqua le comunità umane e le città. Il bolognese non fa eccezione: fino all'inizio del 1900 molte migliaia di pozzi freatici punteggiavano la pianura agricola e si concentravano nei paesi e nella città.

La prima ricostruzione del campo di moto del freatico bolognese è stata ottenuta nel 1994 (G. Viel, 1995), controllata per condizioni di piena nel 1996, successivamente arricchita di nuovi dati nel 1998 (G.P. Artioli et Al, 1997; G. Viel, 1998) e nel 2002 (G. Viel, S. Sangiorgi et Al, 2003). Il confronto tra le condizioni di piena e di magra dell'insieme delle falde superficiali è stato possibile solo nella pianura in destra Reno, fin poco oltre l'Idice, su un intervallo temporale di circa 6 anni. L'esito ottenuto mostra come le escursioni siano in genere di entità modesta (attorno o inferiori al metro), i valori negativi maggiori (fino oltre 4 metri) si distribuiscano lungo il Reno (Castel Maggiore, Calderara, Sala

Bolognese), e tra Bentivoglio e Minerbio (Cà de Fabbri). Anche al confine orientale del Comune di Budrio si sono rilevate tendenze ad escursioni molto forti anche maggiori di 2 metri; qui però la falda superficiale è confinata e questi abbassamenti sono da connettere ad eccessivi prelievi locali.

Il campo di moto della falda superficiale risulta fortemente condizionato dalla presenza di 3 ampie aree, in cui il freatico è depresso fino alla sua scomparsa, che contengono i 5 maggiori campi di sollevamento dell'acquedotto bolognese. Ai margini settentrionali di queste 3 aree di abbassamento freatico si assiste all'inversione del senso di moto naturale delle acque sotterranee: sono dirette dalla pianura verso l'Appennino.

Dalla carta delle piezometrie medie relative agli anni 2005 e 2006 per la conoide del Reno-Savena (fig. 5, Progetto IA/RER_06_003), si osservano come le isopieze relative alla porzione centro orientale della conoide mostrano la situazione idrogeologica più profonda, in cui si osservano gli effetti dei prelievi dei campi pozzi acquedottistici che richiamando acqua da ovest generano una depressione piezometrica anche nella zona in esame con valori piezometrici fra -10,0 e 0,0 m s.l.m.

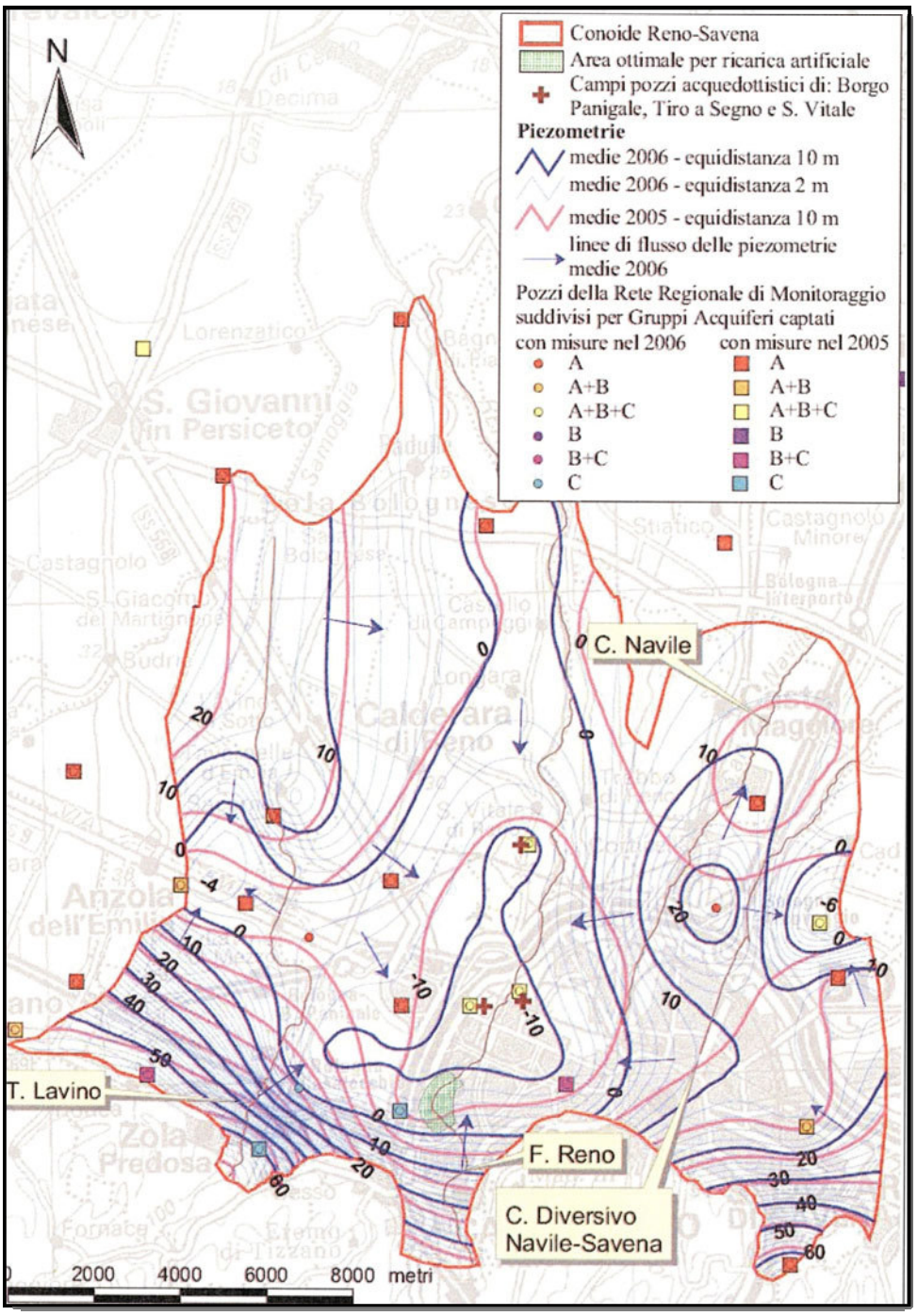


Figura 5: Estratto dalla Carta delle piezometrie medie relative agli anni 2005 e 2006 per la conoide del Reno-Savena (Progetto IA/RER_06_003)

Tutto ciò è il prodotto dall'eccessivo prelievo ed estrazione di acqua dalle falde che nell'area di studio ha evidenziato una grande area di forte soggiacenza (G. Viel) corrispondente agli apparati deposizionali del Reno, e del Lavino (oltre -70 metri). Si tratta di un immenso territorio corrispondente

ai Comuni di: Bologna (pianura ovest), Zola Predosa (pianura), Anzola, Calderara, Castel Maggiore (interamente), Casalecchio (pianura), Sala Bolognese, Argelato, Bentivoglio, S. Giorgio di Piano (in parte), caratterizzato da un cono dinamico prodotto dal prelievo delle stazioni di pompaggio HERA.

4.3 SUBSIDENZA

Entrambe le aree, in considerazione dell'enorme spessore di sedimenti alluvionali a granulometria fine e degli elevati prelievi di acqua di falda idrica sotterranea, è soggetta ad una progressiva e continua subsidenza. Dagli studi più recenti eseguiti sull'abbassamento del suolo nella pianura bolognese (Figura 6 e 7) si evidenzia come, il valore della subsidenza in questo settore della pianura sia dell'ordine di 10÷30 mm/anno (2002-2006), con valori maggiori nel settore SO, nei pressi di Calderara di Reno (circa 30 mm/anno) e minori verso la parte nord. Per quanto concerne invece la Cartografia Interattiva di Arpae, nel periodo temporale 2016-2021 (Figura 7), l'area di Sala Bolognese è stata soggetta a un abbassamento medio tra -15 e -17,5 mm/anno. L'andamento delle isocinetiche di abbassamento del suolo è irregolare in quanto influenzato dalle maggiori quantità di acqua di falda prelevate in corrispondenza dei paleoalvei (maggiore concentrazione di emungimenti). Il fenomeno della subsidenza nella pianura bolognese è generato in minima parte da un progressivo costipamento dei sedimenti alluvionali (subsidenza naturale) e prevalentemente da un eccessivo emungimento delle acque sotterranee (subsidenza artificiale).

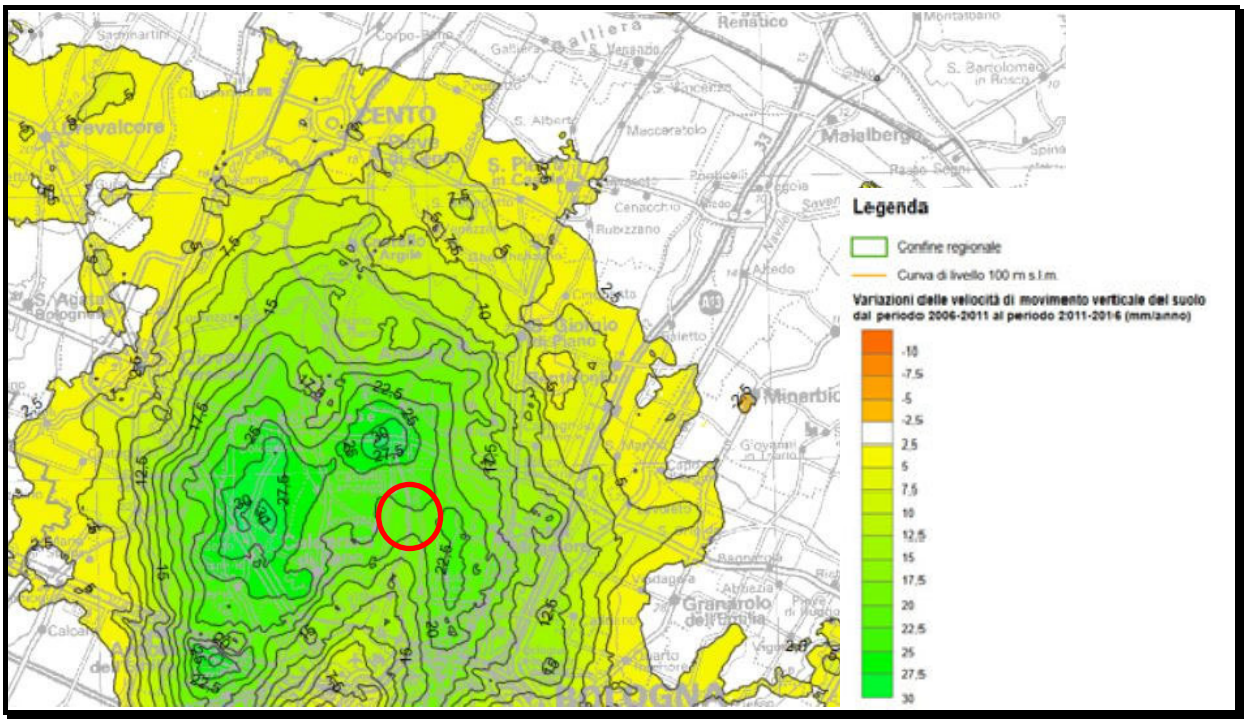


Figura 6: Estratto dalla Carta della velocità del movimento verticale del suolo nel periodo 2006-2016 "Cartografia Regione Emilia-Romagna".

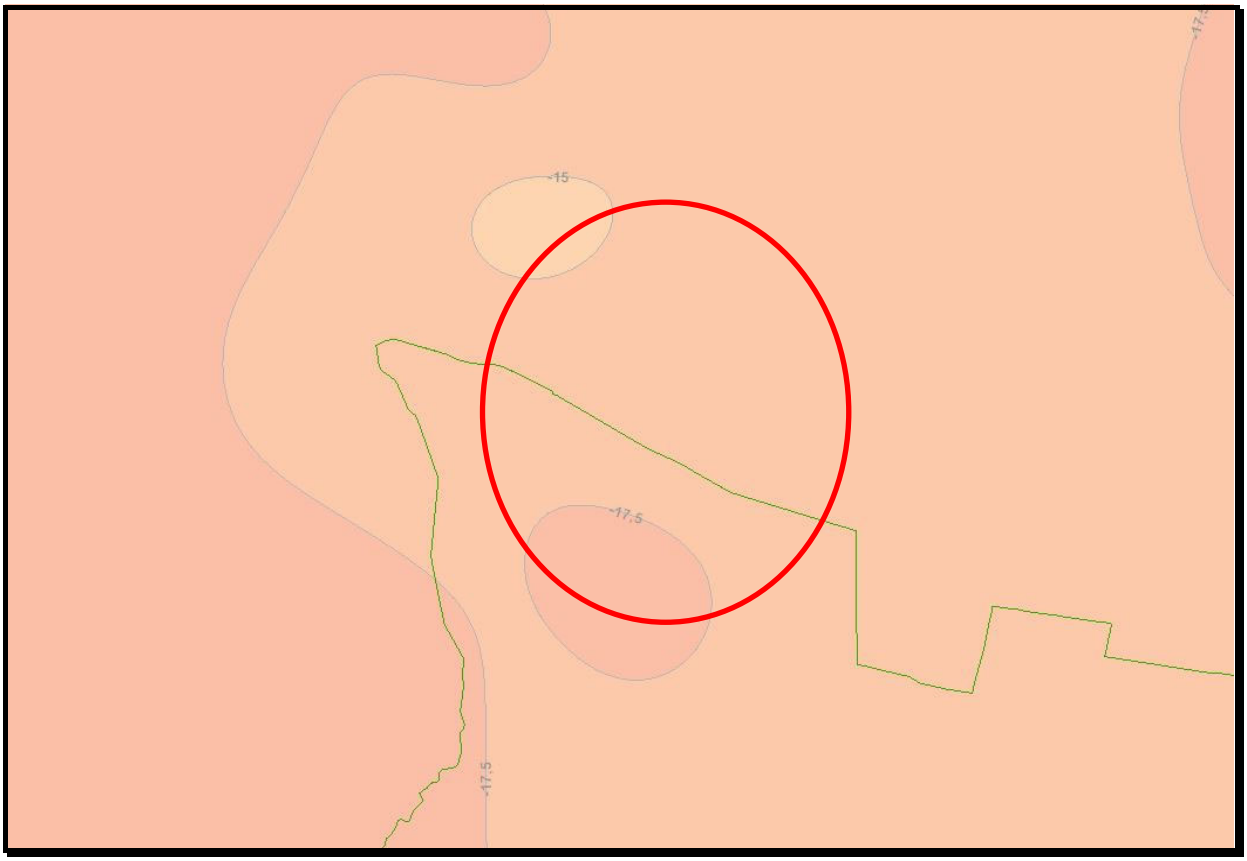


Figura 7: Estratto dalla Cartografia interattiva di ARPAE – Suolo-Subsidenza.

5. Vincoli Urbanistici

Secondo il P.T.M. – Piano Territoriale Metropolitano della Provincia di Bologna, aggiornato al 16 maggio 2022, l'area in esame si trova all'interno dei seguenti vincoli:

- Tav.1 "Carta della Struttura" – aree agricole della pianura alluvionale (art. 16 e 18);
- Tav.2 "Carta degli ecosistemi" – aree agricole della pianura alluvionale (art. 16 e 18);
- Tav.3 "Carta di area vasta del rischio idraulico, rischio da frana e dell'assetto dei versanti":
  - area sottoposta a controllo degli apporti d'acqua di pianura;
  - scenario P3 derivante dal Reticolo Naturale Secondario di Pianura – RSP (Art. 30);
  - scenario P3 derivante dal Reticolo Naturale Principale e Secondario di Pianura – RP (Art. 30);
  - scenario P2 derivante dal Reticolo Naturale Secondario di Pianura – RSP (Art. 30);
  - scenario P3 derivante dal Reticolo Naturale Principale di Pianura – RP (Art. 30);
  - scenario P1 derivante dal Reticolo Naturale Principale e Secondario di Pianura – RP (Art. 30);

- Tav.4 “Carta di area vasta delle aree suscettibili di effetti locali”: Area C – sedimenti prevalentemente fini di pianura.

Secondo il P.S.C. – Piano Strutturale Comunale dell’Unione Terre d’Acqua, nella carta QC.6/T2 inerente il Suolo – Sottosuolo – Acqua, l’area risulta interessata da:

- Aree morfologicamente depresse e/o a debolissima pendenza;
- Criticità idraulica (segnalazione del Consorzio di Bonifica Reno Palata);
- Subsidenza totale del periodo 1983 – 1999 → 600-800 mm.

Va sottolineato come l’area non attraversi zone di attenzione per instabilità da liquefazione o densificazione (Area L), tuttavia, per la tipologia di progetto in questione, si ritiene prudente effettuare un’analisi di Risposta Sismica Locale di III livello.

6. Indagini geognostiche, prospezioni geofisiche e prove di laboratorio

Come precedentemente indicato, per approfondire la conoscenza diretta della litologia, della geometria e delle caratteristiche meccaniche del sottosuolo, nel novembre 2024 si è fatta eseguire una campagna indagini geognostiche formata da 15 indagini penetrometriche di tipo statico meccanico (Cone Penetration Test). Per quanto riguarda le prove penetrometriche con punta elettrica e piezocono (CPTu) ne sono state effettuate 8.

La campagna di indagini geognostiche è stata completata con due prelievi di campioni indisturbati con fustella a pareti sottili tipo shelby destinati ad un laboratorio geotecnica per prove sui materiali che si andranno a sommare alle precedenti valutazioni fatte sui materiali.

Per quanto riguarda l’indagine sismica, verrà presa in considerazione un’indagine sismica condotta nelle immediate vicinanze dell’area di progetto, effettuata con la metodologia M.A.S.W. associata a tomografo digitale TROMINO ENGY” (*Micromed* S.p.A.).

Tutte le indagini sono ubicate nella planimetria di Tav. 2.

6.1 PROVE PENETROMETRICHE STATICHE MECCANICHE (CPT)

La prova penetrometrica statica CPT (di tipo meccanico), eseguita con uno strumento avente una spinta nominale pari a 200 kN, consiste essenzialmente nella misura della resistenza alla penetrazione di una punta meccanica di dimensioni e caratteristiche standardizzate, infissa nel terreno a velocità costante (v = 2 cm/s ± 0.5 cm/s).

La penetrazione avviene attraverso un dispositivo di spinta (martinetto idraulico) opportunamente zavorrato, che agisce su una batteria doppia di aste (aste esterne cave ed aste interne piene coassiali), alla cui estremità inferiore è collegata la punta. Lo sforzo necessario per

l'infissione viene determinato a mezzo di un opportuno sistema di misura, collegato al martinetto idraulico.

Le caratteristiche del penetrometro da 200 kN utilizzato sono le seguenti:

- Punta conica meccanica ϕ =35.7 mm, angolo di apertura α=60° (area punta Ap = 10 cm²).
- Manicotto laterale di attrito tipo "Begemann" (ϕ =37.5 mm, h =133 mm, sup. lat. Am = 150 cm²).
- Velocità di avanzamento costante V = 2 cm/sec (± 0.5 cm/sec).

Sulla batteria di aste esterne può essere installato un anello allargatore per diminuire l'attrito sulle aste, facilitandone l'approfondimento.

Nei diagrammi di resistenza e nelle analoghe tabelle allegate sono riportati i seguenti valori di resistenza, rilevati ad intervalli regolari di 20 cm:

- Rp (kg/cm²) = resistenza alla punta (conica)
- RL (kg/cm²) = resistenza laterale (manicotto)

6.2 PROVE PENETROMETRICHE STATICHE ELETTRICHE CON PIEZOCONO (CPTU)

La prova con punta elettrica con piezocono (CPTu) è l'evoluzione della prova penetrometrica statica con punta meccanica (CPT). I valori di resistenza del terreno non vengono più rilevati con un sistema di aste scorrevoli che trasmettono i carichi (di rottura del terreno) ad un manometro (o cella di carico) di superficie, bensì con degli estensimetri posti direttamente all'interno della punta. Questi estensimetri, con deformazioni meno che millimetriche dei componenti della punta (cono e manicotto), producono dei segnali elettrici proporzionali alle variazioni di carico e quindi alle componenti di resistenza del terreno. I segnali elettrici (analogici) vengono digitalizzati con convertitori direttamente posti all'interno della punta (nel caso ormai più frequente di "digital cone") e vengono memorizzati in un circuito interno. I segnali digitalizzati possono essere inviati direttamente in superficie dove è presente (oltre al circuito di sincronizzazione della profondità) una apposita "centralina" con funzioni di memorizzazione, stampante, salvataggio dati su dischetto ed eventuale trasmissione a PC.

Nella punta CPTu, oltre ai sensori che sono nella punta CPTE, è presente anche un sensore di pressione. Il sensore misura la pressione interstiziale attraverso un filtro poroso in bronzo, ubicato tra la base del cono ed il manicotto, disareato e saturato con olio siliconico.

Le caratteristiche del penetrometro elettrico sono identiche a quelle dello statico:

- Punta conica ϕ =35.7 mm, angolo di apertura α=60° (area punta Ap = 10 cm²).
- Manicotto laterale (ϕ =37.5 mm, h =133 mm, sup. lat. Am = 150 cm²).
- Velocità di avanzamento costante V = 2 cm/sec (± 0.5 cm/sec).

Inoltre il penetrometro statico elettrico è stato fatto oggetto di standardizzazione (ASTM, 1979).

6.3 INDAGINI GEOFISICHE

E' stata condotta una seconda campagna di indagini di tipo geofisico per mezzo del tomografo digitale Tromino.

Il Tromino misura il rumore di fondo (microtremore) e lo utilizza come funzione di eccitazione per identificare in maniera passiva le frequenze di risonanza degli edifici e del suolo sede del futuro intervento edilizio ed in prima approssimazione le Vseq. Le frequenze di risonanza, specie se combaciano quella del suolo con quella tipica del fabbricato in costruzione, sono in diretta relazione con l'amplificazione sismica considerata da molti la prima causa di danno e di distruzione durante un terremoto.

Il rumore di fondo (microtremore) presente ovunque sulla superficie terrestre ed associato sia a fenomeni atmosferici che all'attività antropica, è relativo ad oscillazioni molto piccole (10^{-15} m/s^2), con componenti spettrali che vengono scarsamente attenuate nello spazio e misurabili con tecniche di acquisizione passive.

Tutte le onde elastiche, dalla sorgente al sito, subiscono modifiche al loro tragitto ed attenuazioni in relazione alla natura del suolo attraversato; le informazioni stratigrafiche contenute nei microtremori sono sovrapposte al rumore casuale e possono essere estratte attraverso metodologie come quella di Nakamura dei rapporti spettrali (HVSR – horizontal to vertical spectral ratio).

Tale tecnica è utilizzata anche per la determinazione dell'amplificazione sismica locale e per stimare le frequenze principali di risonanza del sottosuolo, dati molto utili per la progettazione ingegneristica nelle strutture.

Il metodo considera i microtremori come composti in massima parte da onde di superficie (di Rayleigh) nelle componenti orizzontali e verticali, che vengono amplificate per effetto di sito a causa della presenza di discontinuità stratigrafiche nel sottosuolo. E' quindi possibile ricostruire la forma spettrale del microtremore, in cui i picchi alle diverse frequenze rappresentano il rapporto tra la componente orizzontale e verticale dei segnali registrati.

La frequenza dei diversi picchi è funzione della velocità delle onde sismiche nei diversi strati e del loro spessore, secondo la seguente relazione:

$$f = V_s/4h$$

La curva HVSR/f mostra quindi come massimi relativi le frequenze di risonanza dei vari strati alle diverse profondità, per cui conoscendo attraverso i sondaggi o prove penetrometriche gli spessori degli strati è possibile ottenere una stima della velocità delle onde sismiche nel sottosuolo e nello specifico anche una misura della Vseq.

Le indagini sono state inoltre condotte con la metodologia MASW (Multichannel Analysis of Surface Waves). Nella maggior parte delle indagini sismiche per le quali si utilizzano le onde compressive, più di due terzi dell'energia sismica totale generata viene trasmessa nella forma di onde

di Rayleigh, la componente principale delle onde superficiali. Ipotizzando una variazione di velocità dei terreni in senso verticale, ciascuna componente di frequenza dell'onda superficiale ha una diversa velocità di propagazione (chiamata velocità di fase) che, a sua volta, corrisponde ad una diversa lunghezza d'onda per ciascuna frequenza che si propaga. Questa proprietà si chiama dispersione. Sebbene le onde superficiali siano considerate rumore per le indagini sismiche che utilizzano le onde di corpo (riflessione e rifrazione), la loro proprietà dispersiva può essere utilizzata per studiare le proprietà elastiche dei terreni superficiali. La costruzione di un profilo verticale di velocità delle onde di taglio (Vs), ottenuto dall'analisi delle onde piane della modalità fondamentale delle onde di Rayleigh è una delle pratiche più comuni per utilizzare le proprietà dispersive delle onde superficiali. Questo tipo di analisi fornisce i parametri fondamentali comunemente utilizzati per valutare la rigidezza superficiale, una proprietà critica per molti studi geotecnici.

Nelle prospezioni sismiche per le quali si utilizzano le onde di tipo P, la maggior parte dell'energia sismica totale generata si propaga come onde superficiali di tipo Rayleigh. Ipotizzando una variazione di velocità dei terreni in senso verticale, ciascuna componente in frequenza di queste onde è caratterizzata da una diversa velocità di propagazione (chiamata velocità di fase) e quindi da una diversa lunghezza d'onda. Questa proprietà si chiama dispersione. Sebbene le onde superficiali siano considerate rumore per le indagini sismiche che utilizzano le onde di volume (riflessione e rifrazione), la loro proprietà dispersiva può essere utilizzata per studiare le proprietà elastiche dei terreni superficiali.

La costruzione di un profilo verticale di velocità delle onde di taglio (Vs), ottenuto dall'analisi delle onde piane della modalità fondamentale delle onde di Rayleigh è una delle pratiche più comuni per utilizzare le proprietà dispersive delle onde superficiali.

Per ottenere un profilo verticale di velocità Vs bisogna produrre un treno d'onde superficiali a banda larga e registrarlo minimizzando il rumore. Sono state utilizzate una molteplicità di tecniche diverse nel tempo per ricavare la curva di dispersione, ciascuna con i suoi vantaggi e svantaggi.

La configurazione base di campo e la routine di acquisizione per la procedura MASW sono generalmente le stesse utilizzate in una convenzionale indagine a rifrazione. MASW può essere efficace anche con solo dodici canali di registrazione collegati a geofoni verticali a bassa frequenza (4.5 Hz).

Le componenti a bassa frequenza (lunghezze d'onda maggiori), sono caratterizzate da forte energia e grande capacità di penetrazione, mentre le componenti ad alta frequenza (lunghezze d'onda corte), hanno meno energia e una penetrazione superficiale. Grazie a queste proprietà, una metodologia che utilizzi le onde superficiali può fornire informazioni sulle variazioni delle proprietà elastiche dei materiali prossimi alla superficie al variare della profondità. La velocità delle onde S (Vs) è il fattore dominante che governa le caratteristiche della dispersione.

La procedura MASW può sintetizzarsi in tre stadi distinti:

1 - acquisizione dei dati sperimentali;

2 - estrazione della curva di dispersione;

3 - inversione della curva di dispersione per ottenere il profilo verticale delle Vs (profilo 1-D), che descrive la variazione di Vs con la profondità.

Una mappa bidimensionale (mappa 2-D) può essere costruita accostando e sovrapponendo più profili 1-D consecutivi.

Il principale vantaggio di un metodo di registrazione multicanale è la capacità di riconoscimento dei diversi comportamenti, che consente di identificare ed estrarre il segnale utile dall'insieme di varie e differenti tipologie di onde sismiche. Quando un impatto è applicato sulla superficie del terreno, tutte queste onde vengono simultaneamente generate con differenti proprietà di attenuazione, velocità e contenuti spettrali. Queste proprietà sono individualmente identificabili in una registrazione multicanale e lo stadio successivo del processo fornisce grande versatilità nell'estrazione delle informazioni utili.

6.4. PROVE DI LABORATORIO

In fase delle indagini, durante la campagna di prove penetrometriche, sono stati prelevati due campioni indisturbati di terreno con fustella a pareti sottili tipo shelby (per le profondità si rimanda alla tabella seguente) per le necessarie prove di laboratorio; oltre alla descrizione geotecnica è stata effettuata la prova di taglio diretto consolidata drenata (CD).

La prova di taglio diretto (CD) consiste nel sottoporre un campione di terreno, opportunamente preparato, a due forze poste su piani ortogonali tra di loro, una verticale ed una di taglio o orizzontale.

Il campione di terreno viene inserito all'interno di due telai quadrati sovrapposti (scatola di Casagrande) di cui uno è scorrevole rispetto all'altro. Attraverso il telaio superiore si applica uno sforzo di compressione verticale e uno sforzo orizzontale. Il campione di terreno si rompe per un valore dello sforzo orizzontale in corrispondenza del piano di separazione tra i due telai. Conoscendo le forze esterne e la sezione del campione si possono ricavare i valori delle tensioni σ e τ della retta di Coulomb. Eseguendo diverse prove si ottengono i corrispondenti valori di rottura di τ in base ai quali si può tracciare la retta di Coulomb $\tau = c + \sigma \text{ tg } \Phi$, dove Φ è l'angolo d'attrito critico del terreno. Durante la prova si controlla la velocità di applicazione del carico, misurando con un dinamometro il valore dello sforzo orizzontale al crescere della deformazione. Si può quindi tracciare il diagramma τ – deformazione per diversi valori dello sforzo verticale, e determinare quindi il massimo valore di τ. Generalmente si eseguono tre prove di taglio a carichi normali crescenti e si traccia su un grafico τ / σ la retta che media i tre punti trovati; la pendenza di questa retta rappresenta Φ e l'intercetta all'asse delle σ rappresenta c.

Di seguito, si elencano le prove effettuate (tabella 1) le cui risultanze (certificati) sono allegate in appendice:

campione	profondità campione (m)	descrizione geotecnica del campione	determinazione limiti	Colonna risonante	Analisi granulometrica combinata	Taglio diretto CD
CPT10 – C1	0,80 – 1,40	X				X
CPT10 – C2	2,00 – 2,60	X				X

Tab. 1: riepilogo profondità e prove effettuate sui campioni indisturbati

7. Correlazioni adottate

7.1 INTERPRETAZIONI PER LE CPT

Di seguito vengono riportate le principali correlazioni per quanto riguarda le CPT meccaniche adottate tramite software di elaborazioni prove penetrometriche (es. Fondazioni 2011) per le valutazioni litologiche e geotecniche al fine di fornire utili indicazioni in merito al tipo di parametro utilizzato ed a come ci si è pervenuti.

7.1.1 INTERPRETAZIONI LITOLOGICHE

Valutazioni in base al rapporto: F = (Rp / RL) (Begemann 1965 - Raccomandazioni A.G.I. 1977) valide in via approssimata per terreni immersi in falda:

F = Rp / RL	NATURA LITOLOGICA	PROPRIETA'
F < 15	TORBE ED ARGILLE ORGANICHE	COESIVE
15 < F ≤ 30	LIMI ED ARGILLE	COESIVE
30 < F ≤ 60	LIMI SABBIOSI E SABBIE LIMOSE	GRANULARI
F > 60	SABBIE E SABBIE CON GHIAIA	GRANULARI

Vengono inoltre riportate le valutazioni stratigrafiche fornite da Schmertmann (1978), ricavabili in base ai valori di Rp e di FR = (RL / Rp) %:

- AO = argilla organica e terreni misti
- Att = argilla (inorganica) molto tenera
- At = argilla (inorganica) tenera
- Am = argilla (inorganica) di media consistenza
- Ac = argilla (inorganica) consistente
- Acc = argilla (inorganica) molto consistente
- ASL = argilla sabbiosa e limosa
- SAL = sabbia e limo / sabbia e limo argilloso
- Ss = sabbia sciolta
- Sm = sabbia mediamente addensata
- Sd = sabbia densa o cementata
- SC = sabbia con molti fossili, calcareniti

Secondo Schmertmann il valore della resistenza laterale da usarsi, dovrebbe essere pari a:

- 1/3 ± 1/2 di quello misurato per depositi sabbiosi
- quello misurato (inalterato) per depositi coesivi.

7.1.2 CORRELAZIONI GEOTECNICHE

PARAMETRI GEOTECNICI (validità orientativa) - simboli - correlazioni - bibliografia

- γ' = peso dell'unità di volume (efficace) del terreno [correlazioni: γ' - Rp - natura] (Terzaghi & Peck 1967 -Bowles 1982)
- $\sigma'vo$ = tensione verticale geostatica (efficace) del terreno (valutata in base ai valori di γ')
- Cu = coesione non drenata (terreni coesivi) [correlazioni: Cu - Rp]
- OCR = grado di sovra consolidazione (terreni coesivi) [correlazioni: OCR - Cu - $\sigma'vo$] (Ladd et al. 1972 / 1974 / 1977 - Lancellotta 1983)
- Eu = modulo di deformazione non drenato (terr.coes.) [correl.: Eu - Cu - OCR - Ip Ip= ind.plast.] Eu50 - Eu25 corrispondono rispettivamente ad un grado di mobilitazione dello sforzo deviatorico pari al 50-25% (Duncan & Buchigani 1976)
- E' = modulo di deformazione drenato (terreni granulari) [correlazioni: E' - Rp] E'50 - E'25 corrispondono rispettivamente ad un grado di mobilitazione dello sforzo deviatorico pari al 50-25% (coeff. di sicurezza F = 2 - 4 rispettivamente) (Schmertmann 1970 / 1978 - Jamiolkowski et al. 1983)
- Mo = modulo di deformazione edometrico (terreni coesivi e granulari) [correl.: Mo - Rp - natura] (Sanglerat 1972 - Mitchell & Gardner 1975 - Ricceri et al. 1974 - Holden 1973)
- Dr = densità relativa (terreni gran. N. C. - normalmente consolidati) [correlazioni: Dr - Rp - $\sigma'vo$] (Schmertmann 1976)
- Ø' = angolo di attrito interno efficace (terreni granulari N.C.) [correl.: – Meyerhof (1956/1976) ØMe - sabbie limose
- F.L. = accelerazione al suolo che può causare liquefazione (terreni granulari) (g = acc.gravità)(Seed & Idriss 1971 - Sirio 1976) [correlazioni : (Amax/g) - Dr]

8. Valutazioni geolitologiche

Nell'area di Sala Bolognese, la litologia di superficie, al disotto del terreno agricolo, è costituita da terreni con forte eteropia di facies, sia verticale che orizzontale, in quanto si tratta di sedimenti di depositi fluviali medio-fini. Si tratta principalmente di terreni arillo limosi/ limo argillosi, aventi tratti sabbiosi inorganici e facies maggiormente organiche e poco consistenti.

Dall'analisi dei risultati delle prove penetrometriche, osservabili nei diagrammi e nelle tabelle

allegate, si possono sintetizzare, per la porzione di sottosuolo in esame, le seguenti informazioni stratigrafiche ottenute mediante il già ricordato riconoscimento di massima dei terreni attraversati:

Punto 1 – Prova penetrometrica CPT 1

da p.c. a -0,4 m	terreno agricolo;
da -0,4 a -0,8 m	argille limose, moderatamente consistenti;
da -0,8 a -1,6 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -1,6 a -4,2 m	argille limose, moderatamente consistenti;
da -4,2 a -4,4 m	sabbie limose, poco addensate;
da -4,4 a -4,8 m	argille limose, moderatamente consistenti;
da -4,8 a -5,2 m	argille a tratti organiche, poco consistenti;
da -5,2 a -7,2 m	argille limose, moderatamente consistenti;
da -7,2 a -8,0 m	argille a tratti organiche, poco consistenti;
da -8,0 a -10,0 m	argille limose, moderatamente consistenti.

Punto 2 – Prova penetrometrica CPT 3

da p.c. a -1,2 m	argille limose, moderatamente consistenti;
da -1,2 a -1,8 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -1,8 a -2,2 m	argille limose, moderatamente consistenti;
da -2,2 a -2,4 m	argille a tratti organiche, poco consistenti;
da -2,4 a -2,6 m	argille limose, moderatamente consistenti;
da -2,6 a -3,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -3,0 a -4,0 m	argille limose, moderatamente consistenti;
da -4,0 a -5,4 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -5,4 a -6,4 m	argille limose, moderatamente consistenti;
da -6,4 a -6,6 m	argille a tratti organiche, poco consistenti;
da -6,6 a -6,8 m	argille limose, moderatamente consistenti;
da -6,8 a -7,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -7,0 a -10,0 m	argille limose, moderatamente consistenti.

Punto 3 – Prova penetrometrica CPT 4

da p.c. a -0,6 m	terreno agricolo;
da -0,6 a -2,0 m	sabbie limose/limi sabbiosi, moderatamente consistenti;
da -2,0 a -3,6 m	argille limose, moderatamente consistenti;
da -3,6 a -4,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -4,0 a -4,8 m	argille limose, moderatamente consistenti;
da -4,8 a -5,2 m	sabbie limose, poco addensate;
da -5,2 a -9,4 m	argille limose, moderatamente consistenti;
da -9,4 a -10,0 m	sabbie limose, poco addensate.

Punto 4 – Prova penetrometrica CPT 5

da p.c. a -3,4 m	argille limose, moderatamente consistenti;
da -3,4 a -3,8 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -3,8 a -4,0 m	argille limose, moderatamente consistenti;
da -4,0 a -4,6 m	argille a tratti organiche, poco consistenti;
da -4,6 a -5,0 m	argille limose, moderatamente consistenti;
da -5,0 a -5,2 m	argille a tratti organiche, poco consistenti;
da -5,2 a -7,0 m	argille limose, moderatamente consistenti;
da -7,0 a -8,4 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -8,4 a -10,0 m	argille limose, moderatamente consistenti.

Punto 5 – Prova penetrometrica CPT 6

da p.c. a -0,4 m	terreno agricolo;
da -0,4 a -3,0 m	argille limose, moderatamente consistenti;
da -3,0 a -7,6 m	argille a tratti organiche, poco consistenti;
da -7,6 a -8,4 m	argille limose, moderatamente consistenti;
da -8,4 a -10,0 m	argille a tratti organiche, poco consistenti.

Punto 6 – Prova penetrometrica CPT 7

da p.c. a -0,6 m	terreno agricolo;
da -0,6 a -2,2 m	argille limose, moderatamente consistenti;
da -2,2 a -6,0 m	argille a tratti organiche, poco consistenti;
da -6,0 a -6,4 m	argille limose, moderatamente consistenti;
da -6,4 a -7,0 m	sabbie limose, poco addensate;
da -7,0 a - 7,2 m	argille limose, moderatamente consistenti;
da -7,2 a -7,8 m	sabbie limose, poco addensate;
da -7,8 a -8,2 m	argille limose, moderatamente consistenti;
da -8,2 a -12,0 m	sabbie medio fini, moderatamente addensate.

Punto 7 – Prova penetrometrica CPT 8

da p.c. a -0,4 m	terreno agricolo;
da -0,4 a -3,4 m	argille limose, moderatamente consistenti;
da -3,4 a -3,6 m	sabbie medio fini, moderatamente addensate;
da -3,6 a -4,0 m	argille limose, moderatamente consistenti;
da -4,0 a -5,8 m	argille a tratti organiche, poco consistenti;
da -5,8 a -6,2 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -6,2 a -7,4 m	argille a tratti organiche, poco consistenti;
da -7,4 a -12,0 m	sabbie medio fini, moderatamente addensate.

Punto 8 – Prova penetrometrica CPT 9

da p.c. a -0,4 m	terreno agricolo;

da -0,4 a -2,8 m	argille a tratti organiche, poco consistenti;
da -2,8 a -3,0 m	argille limose, moderatamente consistenti;
da -3,0 a -3,4 m	sabbie medio fini, moderatamente addensate;
da -3,4 a -3,6 m	argille limose, moderatamente consistenti;
da -3,6 a -5,8 m	sabbie medio fini, moderatamente addensate;
da -5,8 a -6,2 m	argille limose, moderatamente consistenti;
da -6,2 a -6,8 m	sabbie medio fini, moderatamente addensate;
da -6,8 a -7,4 m	argille a tratti organiche, poco consistenti;
da -7,4 a -8,2 m	sabbie medio fini, moderatamente addensate;
da -8,2 a -8,4 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -8,4 a -8,6 m	argille limose, moderatamente consistenti;
da -8,6 a -9,2 m	sabbie medio fini, moderatamente addensate;
da -9,2 a -12,0 m	argille a tratti organiche, poco consistenti.

Punto 9 – Prova penetrometrica CPT 10

da p.c. a -3,6 m	argille limose, moderatamente consistenti;
da -3,6 a -4,6 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -4,6 a -4,8 m	sabbie medio fini, moderatamente addensate;
da -4,8 a -5,0 m	argille a tratti organiche, poco consistenti;
da -5,0 a -5,8 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -5,8 a -7,8 m	argille limose, moderatamente consistenti;
da -7,8 a -8,8 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -8,8 a -9,0 m	argille limose, moderatamente consistenti;
da -9,0 a -10,8 m	argille a tratti organiche, poco consistenti;
da -10,8 a -11,0 m	argille limose, moderatamente consistenti;
da -11,0 a -11,4 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -11,4 a -12,0 m	argille limose, moderatamente consistenti.

Punto 10 – Prova penetrometrica CPT 11

da p.c. a -2,8 m	argille limose, moderatamente consistenti;
da -2,8 a -3,4 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -3,4 a -3,6 m	argille limose, moderatamente consistenti;
da -3,6 a -4,2 m	argille a tratti organiche, poco consistenti;
da -4,2 a -4,4 m	argille limose, moderatamente consistenti;
da -4,4 a -4,6 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -4,6 a -8,2 m	argille limose, moderatamente consistenti;
da -8,2 a -9,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -9,0 a -10,2 m	argille a tratti organiche, poco consistenti;
da -10,2 a -12,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti.

Punto 11 – Prova penetrometrica CPT 12

da p.c. a -1,2 m	argille limose, moderatamente consistenti;
da -1,2 a -2,4 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -2,4 a -4,2 m	argille limose, moderatamente consistenti;
da -4,2 a -4,6 m	argille a tratti organiche, poco consistenti;
da -4,6 a -5,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -5,0 a -6,6 m	sabbie medio fini, moderatamente addensate;
da -6,6 a -6,8 m	argille a tratti organiche, poco consistenti;
da -6,8 a -7,4 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -7,4 a -8,6 m	argille limose, moderatamente consistenti;
da -8,6 a -9,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -9,0 a -10,4 m	argille limose, moderatamente consistenti;
da -10,4 a -11,0 m	argille a tratti organiche, poco consistenti;
da -11,0 a -11,6 m	argille limose, moderatamente consistenti.

Punto 12 – Prova penetrometrica CPT 13

da p.c. a -0,6 m	terreno agricolo;
da -0,6 a -7,4 m	argille limose, moderatamente consistenti;
da -7,4 a -8,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -8,0 a -9,6 m	argille a tratti organiche, poco consistenti;
da -9,6 a -10,8 m	sabbie medio fini, moderatamente addensate;
da -10,8 a -12,0 m	argille limose, moderatamente consistenti.

Punto 13 – Prova penetrometrica CPT 14

da p.c. a -0,6 m	terreno agricolo;
da -0,6 a -3,6 m	argille limose, moderatamente consistenti;
da -3,6 a -4,6 m	argille a tratti organiche, poco consistenti;
da -4,6 a -5,8 m	sabbie medio fini, moderatamente addensate;
da -5,8 a -7,6 m	argille limose, moderatamente consistenti;
da -7,6 a -8,8 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -8,8 a -10,0 m	argille a tratti organiche, poco consistenti;
da -10,0 a -10,4 m	sabbie medio fini, moderatamente addensate;
da -10,4 a -12,0 m	argille limose, moderatamente consistenti.

Punto 14 – Prova penetrometrica CPT 15

da p.c. a -5,6 m	argille limose, moderatamente consistenti;
da -5,6 a -6,2 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -6,2 a -7,2 m	argille limose, moderatamente consistenti;

da -7,2 a -7,8 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -7,8 a -9,8 m	argille a tratti organiche, poco consistenti;
da -9,8 a -10,2 m	argille limose, moderatamente consistenti;
da -10,2 a -12,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti.

Punto 15 – Prova penetrometrica CPT 16

da p.c. a -0,6 m	terreno agricolo;
da -0,6 a -3,6 m	argille limose, moderatamente consistenti;
da -3,6 a -3,8 m	sabbie medio fini, moderatamente addensate;
da -3,8 a -4,6 m	argille limose, moderatamente consistenti;
da -4,6 a -4,8 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -4,8 a -5,8 m	argille limose, moderatamente consistenti;
da -5,8 a -6,2 m	sabbie medio fini, moderatamente addensate;
da -6,2 a -7,2 m	argille limose, moderatamente consistenti;
da -7,2 a -9,0 m	sabbie limose/limi sabbiosi, moderatamente consistenti;
da -9,0 a -12,2 m	argille a tratti organiche, poco consistenti.

Punto 16 – Prova penetrometrica CPTu 1

da p.c. a -0,38 m	terreno agricolo;
da -0,38 a -1,24 m	argille limose, moderatamente consistenti;
da -1,24 a -1,64 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -1,64 a -1,94 m	argille limose, moderatamente consistenti;
da -1,94 a -3,64 m	argille a tratti organiche, poco consistenti;
da -3,64 a -3,88 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -3,88 a -4,36 m	argille a tratti organiche, poco consistenti;
da -4,36 a -4,66 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -4,66 a -5,14 m	argille limose, moderatamente consistenti;
da -5,14 a -9,56 m	argille a tratti organiche, poco consistenti;
da -9,56 a -9,72 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -9,72 a -11,22 m	argille a tratti organiche, poco consistenti;
da -11,22 a -11,84 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -11,84 a -15,06 m	argille limose, moderatamente consistenti;
da -15,06 a -15,62 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti.

Punto 17 – Prova penetrometrica CPTu 2

da p.c. a -0,50 m	terreno agricolo;
da -0,50 a -1,58 m	sabbie limose/limi sabbiosi, moderatamente consistenti;

da -1,58 a -3,84 m	argille limose, moderatamente consistenti;
da -3,84 a -5,80 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -5,80 a -6,48 m	argille limose, moderatamente consistenti;
da -6,48 a -7,50 m	argille a tratti organiche, poco consistenti;
da -7,50 a -8,40 m	argille limose, moderatamente consistenti;
da -8,40 a -10,4 m	argille a tratti organiche, poco consistenti;
da -10,4 a -11,56 m	argille limose, moderatamente consistenti;
da -11,52 a -12,0 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -12,0 a -14,04 m	argille limose, moderatamente consistenti;
da -14,04 a -14,88 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -14,88 a -15,54 m	argille limose, moderatamente consistenti.

Punto 18 – Prova penetrometrica CPTu 3

da p.c. a -0,96 m	terreno agricolo;
da -0,96 a -5,20 m	argille limose, moderatamente consistenti;
da -5,20 a -7,16 m	argille a tratti organiche, poco consistenti;
da -7,16 a -8,20 m	argille limose, moderatamente consistenti;
da -8,20 a -9,10 m	argille a tratti organiche, poco consistenti;
da -9,10 a -9,82 m	argille limose, moderatamente consistenti;
da -9,82 a -10,12 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -10,12 a -12,94 m	argille a tratti organiche, poco consistenti;
da -12,94 a -13,9 m	argille limose, moderatamente consistenti;
da -13,9 a -14,96 m	sabbie limose, poco addensate;
da -14,96 a -15,6 m	argille limose, moderatamente consistenti.

Punto 19 – Prova penetrometrica CPTu 4

da p.c. a -0,52 m	terreno agricolo;
da -0,52 a -5,46 m	argille limose, moderatamente consistenti;
da -5,46 a -7,26 m	argille a tratti organiche, poco consistenti;
da -7,26 a -8,32 m	argille limose, moderatamente consistenti;
da -8,32 a -8,56 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -8,56 a -10,14 m	argille limose, moderatamente consistenti;
da -10,14 a -10,98 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -10,98 a -12,68 m	argille limose, moderatamente consistenti;
da -12,68 a -13,34 m	argille a tratti organiche, poco consistenti;
da -13,34 a -15,64 m	argille limose, moderatamente consistenti.

Punto 20 – Prova penetrometrica CPTu 5

da p.c. a -0,7 m	terreno agricolo;
da -0,7 a -3,86 m	argille limose, moderatamente consistenti;
da -3,86 a -4,68 m	argille a tratti organiche, poco consistenti;
da -4,68 a -5,3 m	argille limose, moderatamente consistenti;

da -5,3 a -5,7 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -5,7 a -10,0 m	argille limose, moderatamente consistenti;
da -10,0 a -10,86 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -10,86 a -13,54 m	argille limose, moderatamente consistenti;
da -13,54 a -15,1 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti.

Punto 21 – Prova penetrometrica CPTu 6

da p.c. a -0,64 m	terreno agricolo;
da -0,64 a -2,84 m	argille limose, moderatamente consistenti;
da -2,84 a -3,16 m	argille a tratti organiche, poco consistenti;
da -3,16 a -5,74 m	argille limose, moderatamente consistenti;
da -5,74 a -6,56 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -6,56 a -8,04 m	argille limose, moderatamente consistenti;
da -8,04 a -11,36 m	argille a tratti organiche, poco consistenti;
da -11,36 a -15,74 m	argille limose, moderatamente consistenti.

Punto 22 – Prova penetrometrica CPTu 7

da p.c. a -0,34 m	terreno agricolo;
da -0,34 a -1,7 m	argille limose, moderatamente consistenti;
da -1,7 a -3,12 m	argille a tratti organiche, poco consistenti;
da -3,12 a -4,3 m	argille limose, moderatamente consistenti;
da -4,3 a -6,68 m	argille a tratti organiche, poco consistenti;
da -6,68 a -6,9 m	argille limose, moderatamente consistenti;
da -6,9 a -8,68 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti
da -8,68 a -11,5 m	argille limose, moderatamente consistenti;
da -11,5 a -11,76 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -11,76 a -14,72 m	argille limose, moderatamente consistenti;
da -14,72 a -15,2 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -15,2 a -15,66 m	argille limose, moderatamente consistenti.

Punto 23 – Prova penetrometrica CPTu 8

da p.c. a -0,30 m	terreno agricolo;
da -0,30 a -0,80 m	argille limose, moderatamente consistenti;
da -0,80 a -1,70 m	sabbie limose, poco addensate;
da -1,70 a -4,20 m	argille limose, moderatamente consistenti;
da -4,20 a -6,76 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti;
da -6,76 a -8,14 m	argille a tratti organiche, poco consistenti;
da -8,14 a -11,68 m	limi argillosi, inorganici, a tratti debolmente sabbiosi, moderatamente consistenti.

Questo tipo di terreni fini spesso porta a mal distinguere la parte coesiva dalla parte granulare fine specialmente, come detto, con la punta meccanica begemann.

Si tratta nei primi metri di depositi alluvionali, costituiti da materiali coesivi prevalenti, ai primi stadi di alterazione pedogenetica, con fronte di alterazione < 1 m (50÷100 cm); al tetto sono presenti suoli calcarei con differenziazione in orizzonti A-C.

Le indicazioni riportate hanno ovviamente carattere generale ed indicativo e non possono in alcun modo sostituire gli opportuni approfondimenti necessari alle fasi esecutive.

9. Sismicità dell'area

9.1 MACROSISMICITA'

Un passo fondamentale nella valutazione del rischio sismico di un'area è l'identificazione delle faglie attive. Sebbene esistano, infatti, strutture a scorrimento lento asismico (*fault creep* o *tectonic creep*), molte delle faglie attive sono considerate sorgenti sismiche in quanto lo scorrimento istantaneo dei due lati delle stesse, che avviene allorché lo stress supera la resistenza delle rocce, genera il rilascio di onde elastiche che si propagano in tutte le direzioni. A tali faglie sismogenetiche è associato il maggior rischio.

Per la definizione di faglia attiva si fa normalmente riferimento alla possibilità che una faglia può attivarsi in un intervallo di tempo futuro che interessa la nostra società. D'altra parte le faglie che hanno la maggiore probabilità di muoversi in un futuro prossimo sono da ricercarsi tra quelle che si sono mosse nelle fasi più recenti della storia geologica. Così una delle definizioni più comunemente accettata è quella della U.S Nuclear Regulatory Commission (1982), che definisce attive le faglie che presentano un'attivazione negli ultimi 35.000 anni o almeno due negli ultimi 500.000 anni.

La Carta sismotettonica della Regione Emilia Romagna alla scala 1:250.000, oltre alla definizione della pericolosità sismica locale e all'individuazione di strutture potenzialmente sismogenetiche, offre anche un quadro delle relazioni fra attività tettonica attuale e i rischi naturali. In detto lavoro, infatti, l'analisi comparata della sismicità e delle strutture attive, evidenti per la loro espressione sia morfologica che geologica, unitamente ad una riconsiderazione dei dati disponibili sui movimenti verticali del suolo (sollevamento dei terrazzi alluvionali, subsidenza, evoluzione del reticolo idrografico) e alla ricostruzione delle isobate delle 2 principali e più recenti superfici di discontinuità del sottosuolo (rispettivamente 450.000 anni, base del SERS, e 10.000 anni, base dell'Olocene), ha permesso di ottenere un quadro neotettonico e sismotettonico ben definito del territorio indagato.

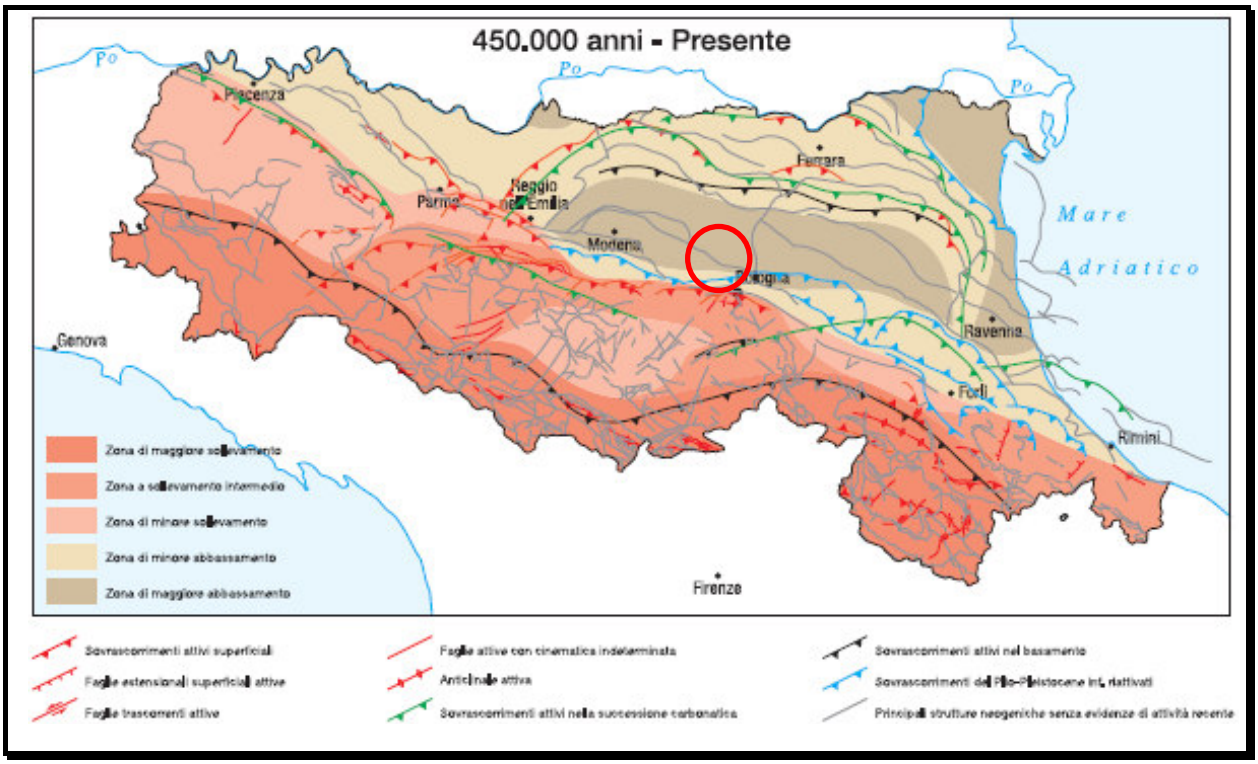


Figura 8: schema di sintesi sull'attività neotettonica in Emilia-Romagna.

Esaminando la Fig. 9.1 (fig. 8) delle Note Illustrative della Carta sismotettonica della Regione Emilia Romagna, che può essere considerata lo schema di sintesi sull'attività neotettonica in Emilia-Romagna, emerge che le zone a maggiore sollevamento, con tassi >1 mm/anno, sono individuabili nella parte alta della catena, corrispondente al settore a monte del principale raddoppio crostale a conferma dell'attività di questa struttura. L'area a sollevamento intermedio, con tassi mediamente ≥1 mm/anno, corrisponde al settore immediatamente retrostante la struttura superficiale del margine che da Bologna si estende verso NW fino alla valle del Taro. Le aree a minore sollevamento (<1 mm/anno) si collocano immediatamente a valle della struttura crostale. La zona di Sala Bolognese si trova a cavallo fra le zone a maggiore abbassamento e quelle a minor abbassamento. I meccanismi focali calcolati risultano compressivi e trascorrenti indicando direzioni di compressione sia NE-SW che NW-SE. I meccanismi focali distensivi sono nettamente secondari. Risulta quindi che la cinematica delle principali strutture attive superficiali è di tipo transpressivo.

La sismicità crostale, con ipocentri mediamente compresi tra 15 e 35 km, mostra una distribuzione simile a quella più superficiale ma con una densità inferiore. Anche in questo caso i meccanismi focali risultano compressivi e trascorrenti con direzioni di compressione sia NW-SE che NE-SW ed i meccanismi distensivi sono rari e ben localizzati.

La sismicità più profonda, con ipocentri oltre i 35 km, fino ad oltre 50 km, è sempre diffusa nel settore di catena e in corrispondenza del margine appenninico-padano.

Risulta così un modello geodinamico attivo in cui le strutture superficiali della copertura, quelle crostali e quelle del mantello, sebbene tra loro distinte, sono tutte coerenti e inquadrabili in un sistema transpressivo che rispetto alle zone esterne dell'avampaese padano, relativamente stabili, assume il significato di un sistema di ordine inferiore all'interno di una zona di trascorrenza destra.

9.2 LA ZONAZIONE SISMOGENETICA ZS9

La zona di Sala Bolognese risulta all'interno dalla zona sismogenetica 912 denominata "*Dorsale Ferrarese*" non distante della zona sismogenetica 913 denominata "*Appennino Emiliano-Romagnolo*". La Fig. 9 (Zonazione sismogenetica ZS9) mostra il comportamento cinematico atteso delle strutture sismogenetiche nelle varie zone del territorio nazionale.

La zonazione sismogenetica ZS9 prodotta dal Gruppo Nazionale per la Difesa dai Terremoti rappresenta l'evoluzione di precedenti zonazioni prodotte dalla comunità scientifica nazionale con riferimento al territorio italiano e settori immediatamente confinanti. La ZS9 propone la suddivisione del territorio nazionale in fasce che presentano al loro interno requisiti di omogeneità in relazione alle caratteristiche geo-strutturali, cinematiche e sismiche. Le 42 zone-sorgente di ZS9 sono state identificate con un numero (da 901 a 936) o con una lettera (da A a F). Una base essenziale per la zonazione del territorio è rappresentata dal modello sismotettonico dell'area italiana, e contributi rilevanti per la definizione delle singole zone sono forniti dai cataloghi sismici disponibili. In particolare ZS9 è costruita facendo riferimento al modello sismotettonico di Meletti et al. (2000), rivisto ed integrato negli anni successivi alla sua formulazione. Inoltre ZS9 è definita sulla scorta delle informazioni disponibili dai cataloghi CPTI2 (catalogo parametrico dei terremoti italiani) e DISS (database delle sorgenti sismogenetiche). ZS9, come le versioni precedenti, è utilizzato per fornire i dati delle sorgenti-tipo e dei patterns sismici nei vari settori del territorio nazionale utili per le stime di pericolosità sismica.

La Zonazione ZS9 non introduce drastici elementi di novità rispetto alle precedenti zonazioni, in modo particolare rispetto a ZS4 che rappresenta una sorta di caposaldo nell'evoluzione del processo di zonazione. Infatti, il modello sismotettonico di riferimento di ZS9 è molto simile a quello utilizzato per la redazione di ZS4. Il vero elemento di novità è rappresentato dall'impiego di un catalogo sismico più aggiornato (CPTI2) e dall'introduzione delle conoscenze più recenti sulla geometria delle sorgenti sismogenetiche (database DISS).

Negli ultimi anni, infatti, la quantità di informazioni sulla sismogenesi del territorio italiano (sia per quanto riguarda gli aspetti geometrici delle sorgenti che per quanto attiene al loro comportamento atteso) è notevolmente aumentata rispetto a quella disponibile nel periodo in cui i ricercatori procedevano alla realizzazione di ZS4. Tali conoscenze rappresentano uno degli elementi chiave per il tracciamento delle nuove zone.

Figura 9: Zonazione sismogenetica ZS9. Le diverse zone sono individuate da un numero; le zone individuate con una lettera non sono state utilizzate per la valutazione della pericolosità sismica.

Un altro elemento di novità rispetto al passato è rappresentato dall'utilizzo del database delle soluzioni dei meccanismi focali dei terremoti italiani (EMMA; Vannucci e Gasperini, 2003). Tale database contiene meccanismi tratti da cataloghi on-line (come il catalogo CMT dell'Università di Harvard, il catalogo dell'ETH di Zurigo e il catalogo RCMT dell'INGV) o dalla letteratura cartacea pubblicata. Tra tutti i meccanismi contenuti nel database sono stati selezionati quelli che ricadono all'interno delle zone sorgente di ZS9: si tratta di 1051 records relativi a terremoti avvenuti tra il 1905 ed il 2003, con magnitudo Mw compresa tra 1.9 e 6.6. Il numero di eventi per zona sorgente è estremamente variabile, poiché si va da zone per le quali si hanno solo 1 o 2 meccanismi disponibili a zone con diverse decine di meccanismi; solo in 12 zone sulle 36 utilizzate per il calcolo della pericolosità sismica si hanno meno di 10 soluzioni di meccanismi focali. Per ogni zona di ZS9 sono state determinate le somme delle componenti del momento tensore, utilizzando tutti i dati disponibili e avendo cura di scegliere il meccanismo più affidabile nel caso di soluzioni multiple per lo stesso evento. Ogni zonizzazione sismogenetica è caratterizzata da un definito modello cinematico il quale

sfrutta una serie di relazioni di attenuazione stimate sulla base di misurazioni accelerometriche effettuate sia sul territorio nazionale che europeo. Sulla base di tali zone, per tutto il territorio italiano, sono state sviluppate le carte della pericolosità sismica.

Nella Zona Sismogenetica 913 sono previsti, sulla base dei meccanismi focali, valori di massima magnitudo pari a M_{wmax} = 5,91±6.14 mentre nella Zona Sismogenetica 912 sono previsti, sulla base dei meccanismi focali, valori di massima magnitudo pari a M_{wmax} = 6,14.

9.3 SISMICITA' DEL TERRITORIO

Ai sensi della legge 02.02.1974 n. 64, secondo il DM del 03.06.1981, si rileva che in base all'Elenco dei Comuni ad alto rischio sismico (Legge 22.12.1997 n. 449, art. 12) allegato all'Ordinanza P.C.M.12.06.1998 il territorio comunale di Sala Bolognese non era classificato.

Alla luce nuova normativa sismica, con l'entrata in vigore del O.P.C.M 3274 del 20 marzo 2003 ed in relazione alle emanazioni delle delibere della Giunta regionale 2329/2004 e 1677/2005, i territori comunali diventano entrambi "zona 3" e nello specifico alla zona 3. La storia sismica dei due comuni è stata desunta dal "DBMI15, un database di osservazioni macrosismiche di terremoti italiani utilizzati per la compilazione del catalogo parametrico CPTI15, database realizzato dal Gruppo Nazionale per la Difesa dei Terremoti che contiene i dati macrosismici provenienti da studi dello stesso GNDT e di altri enti.

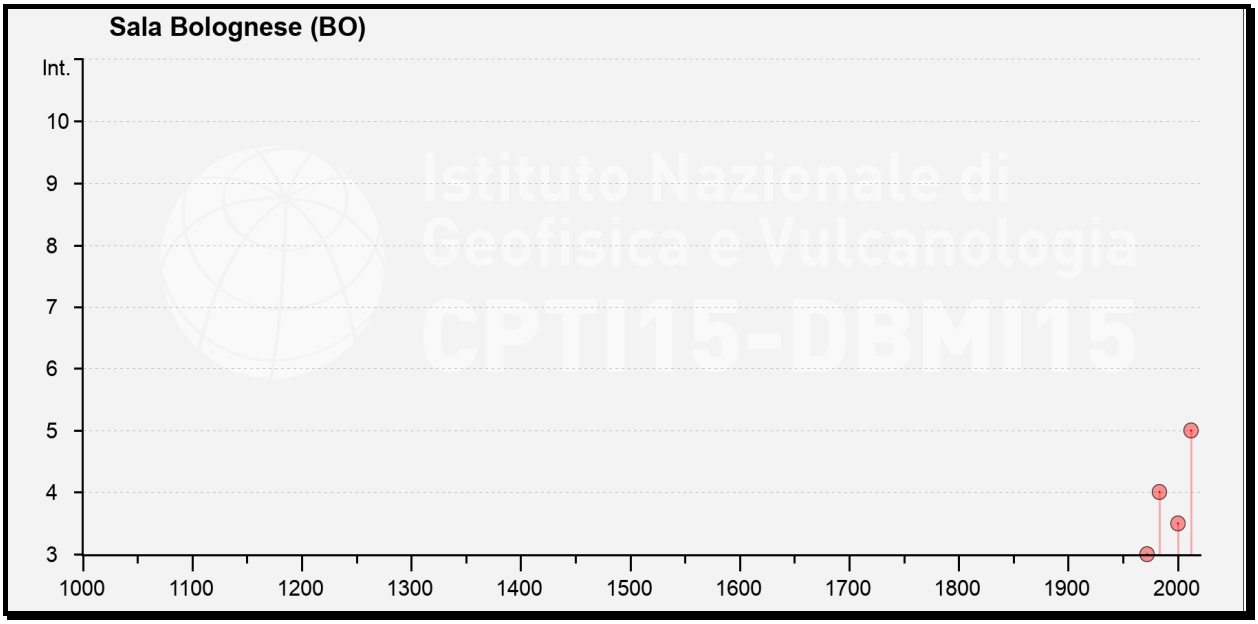


Fig.10: grafico rappresentante la storia sismica di Sala Bolognese (BO).

In figura 10 viene riportato il diagramma del comune di Sala Bolognese, mentre in Tab. 2 sono elencati gli eventi di maggior intensità al sito.

Seismic history of	Sala Bolognese
PlaceID	IT_40114
Coordinates (lat, lon)	44.613, 11.256
Municipality (ISTAT 2015)	Sala Bolognese
Province	Bologna
Region	Emilia-Romagna
No. of reported earthquakes	6

Int. at place	Year	Mo	Da	EpicentralArea	Io	Mw
3	1972	10	25	Appennino settentriona	5	4.87
4	1983	11	9	Parmense	6-7	5.04
NF	1992	4	17	Appennino bolognese	4-5	4.11
3-4	2000	6	18	Pianura emiliana	5-6	4.4
NF	2002	6	18	Frignano	4	4.3
5	2012	5	29	Pianura emiliana	7-8	5.9

Tab. 2: eventi sismici i cui effetti si sono sentiti nel territorio di Sala Bolognese

Dalla lettura di Tab. 2 si evidenzia che il massimo evento sismico censito nel comune di Sala Bolognese si è verificato il 10 maggio 2000. L'epicentro è indicato genericamente in Emilia Romagna. Il terremoto è stato caratterizzato da una magnitudo momento, calcolata sulle onde di superficie (Mw) pari a 4,86 ed una intensità epicentrale pari a 5-6. Non sono ancora inseriti nel database gli ultimi recenti eventi

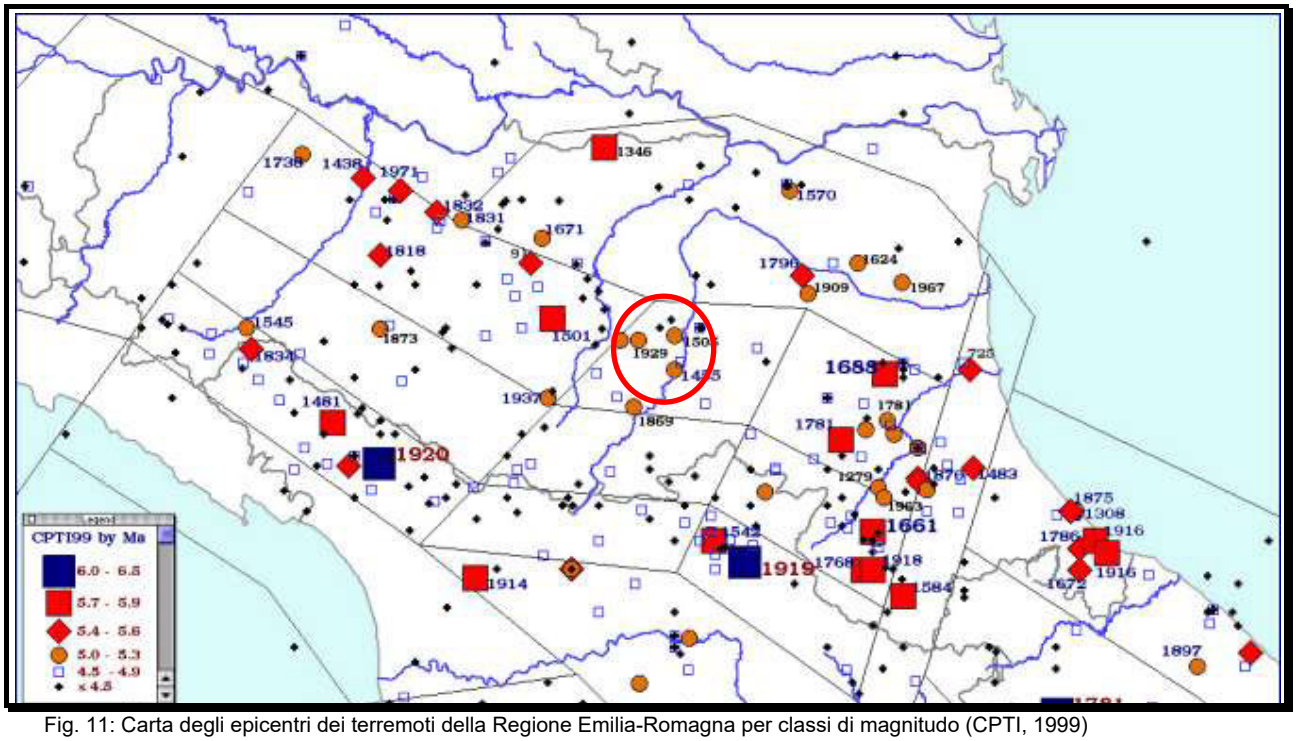


Fig. 11: Carta degli epicentri dei terremoti della Regione Emilia-Romagna per classi di magnitudo (CPTI, 1999)

Sopra viene riportata la mappa (figura 11) con l'indicazione degli epicentri dei terremoti storici della regione Emilia-Romagna con individuata l'area di studio, coincidente quasi con l'epicentro del terremoto del 1929 e non distante dall'epicentro dei terremoti occorso nel bolognese del 1505 e nel modenese nel 1501.

Come precedentemente indicato, l'area di studio si trova vicino al confine delle zone sismogenetica 913 con valori di massima magnitudo attesa pari a M_{wmax} = 5,91 e 912 con valori di massima magnitudo attesa pari a M_{wmax} = 6,14; aumentando il dettaglio delle informazioni disponibili dal catalogo delle sorgenti sismogenetiche italiane DISS 3.2.1 si evince che l'area di studio si colloca a ridosso della fascia sismogenetica ITCS047 "*Castelvetro di Modena-Castel San Pietro Terme*" a cui viene attribuita una magnitudo momento massima pari a M_{wmax} = 5,60 non lontana da un'altra importante fascia sismogenetica quale la ITCS051 "*Novi-Poggio Renatico*", a cui viene attribuita una magnitudo momento massima pari a M_{wmax} = 5,90. Inoltre sono state individuate non lontano dall'area di studio due faglie sismogenetiche identificate con ITIS103 "*Crespellano*" con una magnitudo momento massima attribuita pari a M_{wmax} = 5,60 e ITIS091 "*Casalecchio di Reno*" con una magnitudo momento massima attribuita pari a M_{wmax} = 5,50. Si ricorda velocemente che una sorgente sismogenetica composita è una regione allungata, contenente un numero imprecisato di sorgenti sismogenetiche allineate che non possono essere individuate singolarmente.

Pertanto il territorio sismicamente è stato interessato da eventi significativi di cui bisognerà tenere conto in fase progettuale.

9.4 VALUTAZIONE DELLA VS_{EQ}

E' possibile calcolare il valore della V_{seq} in più modi:

1. con misure dirette di V_s (da prove Down Hole, ReMI, ecc.);
2. con misure indirette di V_s (mediante la V_p di indagini sismiche di superficie, previa conoscenza del Modulo di Poisson per gli strati investigati);
3. con indagini SPT o comunque prove penetrometriche correlabili alle SPT, mediante la correlazione di Ohta e Goto (1978) tra N_{spt} e V_s;
4. con indagini SPT o comunque prove penetrometriche correlabili alle SPT, mediante la correlazione di Motonori e Yoshida (1988) tra N_{spt} e V_s.

e nel caso in cui non si abbia a disposizione misure dirette o bibliografiche, si utilizzano le procedure indicate ai punti 3 e 4; si deve comunque considerare che deriveranno indicazioni circa la categoria di suolo di fondazione e Vs affette da un certo margine di errore dovuto in parte alla schematizzazione della stratigrafia (normalizzazione).

FORMULA DI OHTA E GOTO (1978):

$V_s = 54.33 \times (N_{spt})^{0.173} \times \alpha \times \beta \times (Z / 0.303)^{0.193}$

α = fattore di età (Olocene = 1.000: Pleistocene = 1.303);

β = fattore geologico (argille = 1.000; sabbie = 1.086);
Z = profondità in metri;
N_{spt} = numero di colpi di una prova SPT.

FORMULA DI YOSHIDA E MOTONORI (1988)

$V_s = \beta \times (N_{spt})^{0.25} \times \sigma'_{v0}{}^{0.14}$
β = fattore geologico (qualunque terreno = 55; sabbia fine = 49);
σ'_{v0} = pressione verticale (γ' h);
N_{spt} = numero di colpi di una prova SPT.

Per correlare I dati delle CPT (qc) a quelli della S.P.T. (N_{spt}) utilizzeremo:

- N_{spt} = qc/4,5 (correlazione di Robertson et al. per sabbie – qc in kg/cm^2);
- N_{spt} = qc/5 (correlazione sperimentale relativa a terreni coesivi nel bolognese)

Essendo stata effettuata un'indagine sismiche con metodologia M.A.S.W. e tomografo digitale Tromino debitamente tarata sulle indagini penetrometriche effettuate, e confrontando il dato alla Tabella 3.2.II delle NTC2018, è stato pertanto possibile ricavare direttamente il valore della V_{s30}

La V_{sEQ} ricavata dalla formula:

$$V_{sEQ} = 30/ \Sigma h_i/v_i,$$

nel caso specifico è risultata: V_{sEQ} = 188,0 m/sec;
il sito esaminato presenta un suolo di fondazione di tipo **C** ovvero:
"*Depositi di terreni a grana grossa mediamente addensati o terreni a grana fina mediamente consistenti con profondità del substrato superiori a 30 m, caratterizzati da un miglioramento delle proprietà meccaniche con la profondità e da valori di velocità equivalente compresi tra 180 m/s e 360 m/s.".*

In relazione alla frequenza tipica di vibrazione dei terreni investigata la frequenza massima significativa riscontrata presenta un picco attorno a circa 0,84±0,1 Hz in quanto è ascrivibile a discontinuità stratigrafiche importanti e che possono quindi dare origine a modificazioni del segnale sismico. Meno significative, per l'opera in progetto, appaiono le altre frequenze superiori ai 10 Hz che non possono essere considerate rappresentative di una corretta interazione struttura/terreni, in quanto sono riconducibili a discontinuità molto superficiali.

Pertanto in considerazione della tipologia strutturale da realizzarsi, si dovranno evitare accoppiamenti fra le modalità di vibrazione delle strutture e le modalità di vibrazione dei terreni di fondazione di cui sopra ovvero evitare effetti di risonanza.

9.5 PERICOLOSITÀ SISMICA DI BASE E SISMICITA' DELL'AREA DI STUDIO

Per la verifica si deve partire dalle azioni sismiche di progetto, che si definiscono a partire dalla "**Pericolosità sismica di base**" del sito di costruzione che costituisce l'elemento di conoscenza

primario per la determinazione delle azioni sismiche ed è funzione delle coordinate geografiche del sito di realizzazione dell'opera e del Tempo di Ritorno.

Per pericolosità sismica di base si intende la probabilità (denominata Probabilità di eccedenza o di superamento nel periodo di riferimento P_{VR}) che, in un fissato lasso di tempo (periodo di riferimento V_R espresso in anni) nel sito si verifichi un evento sismico di entità almeno pari ad un valore prefissato

La pericolosità sismica è definita da:

a_g = accelerazione sismica massima attesa di un sito di riferimento rigido con superficie topografica orizzontale;

F_0 = valore massimo di amplificazione dello spettro in accelerazione orizzontale.

I valori dei parametri a_g ed F_0 relativi alla pericolosità sismica su reticolo geografico di riferimento sono forniti nelle tabelle riportate nell'ALLEGATO B al Testo unico 2008.

Sulla scorta del D.M 17 gennaio 2018 "*NORME TECNICHE PER LE COSTRUZIONI*" ed in base alla nuova classificazione sismica dei comuni italiani (allegato 1, punto 3 dell'OPCM 3274 del 20 marzo 2003) per i comuni appartenenti alla categoria sismica 3 la valutazione della a_g viene ora definita dal sito in base alla Latitudine ed alla longitudine che nello specifico:

WGS84	
Latitudine	44.604414°
Longitudine	11.277177°

ED50	
Latitudine	44,605351°
Longitudine	11.278179°

Il sito dell'INGV fornisce un a_g su suolo rigido per il comparto in questione compreso fra 0.150÷0.175 (nello specifico 0.164g), considerando un tempo di ritorno di 475 anni (VN = 50 anni, opera di classe II, cfr indicata per la pianificazione) con probabilità di eccedenza del 10% in 50 anni (50° percentile). In allegato sono riportate i valori di a_g (accelerazione massima orizzontale del terreno), F_o (valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale) e T_c (periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale) per i vari Stati Limite di Esercizio SLE (di Operatività (SLO) e di Danno (SLD)) e Stati Limite Ultimi SLU (di Salvaguardia della Vita (SLV) e di prevenzione al Collasso (SLC)) con relative probabilità di superamento nella Vita di Riferimento V_R della costruzione.

10. Modellazione sismica

10.1 PERIODO DI RIFERIMENTO, VITA NOMINALE E CLASSE D'USO

Il tempo di ritorno è valutato in funzione della Periodo di riferimento V_R ed in base alla corrispondente probabilità di del suo superamento allo stato limite che si intende verificare.

Il Periodo di riferimento viene calcolata in funzione della Vita nominale V_N per coefficiente d'uso C_U

$$V_R = V_N \times C_U$$

Vita nominale V_N indica in numero di anni nel quale la struttura deve essere usata per lo scopo per cui è progettata.

	Tipi di costruzione	Vita nominale V_N (in anni)
1	Opere provvisorie – Opere provvisionali - Strutture in fase costruttiva1 °	**≤10**
2	Opere ordinarie, ponti, opere infrastrutturali e dighe di dimensioni contenute o di importanza normale	**≥50**
3	Grandi opere, ponti, opere infrastrutturali e dighe di grandi dimensioni o di importanza strategica	**≥100**

Tabella 3: Tab. 2.4.I Norme Tecniche 2018

Coefficiente d'uso C_U: parametro definito in base alla classe d'uso della struttura in funzione del livello di affollamento e dell'interesse strategico.

	Classe d'uso	Coefficiente d'uso C_U
I	Costruzioni con presenza solo occasionale di persone, edifici agricoli.	**0.7**
II	Costruzioni il cui uso preveda normali affollamenti, senza contenuti pericolosi per l'ambiente e senza funzioni pubbliche e sociali essenziali. Industrie con attività non pericolose per l'ambiente. Ponti, opere infrastrutturali, reti viarie non ricadenti in Classe d'uso III o in Classe d'uso IV, reti ferroviarie la cui interruzione non provochi situazioni di emergenza. Dighe il cui collasso non provochi conseguenze rilevanti.	**1.0**
III	Costruzioni il cui uso preveda affollamenti significativi. Industrie con attività pericolose per l'ambiente. Reti viarie extraurbane non ricadenti in Classe d'uso IV. Ponti e reti ferroviarie la cui interruzione provochi situazioni di emergenza. Dighe rilevanti per le conseguenze di un loro eventuale collasso.	**1.5**
IV	Costruzioni con funzioni pubbliche o strategiche importanti, anche con riferimento alla gestione della protezione civile in caso di calamità. Industrie con attività particolarmente pericolose per l'ambiente. Reti viarie di tipo A o B, di cui al D.M. 5 novembre 2001, n. 6792, "Norme funzionali e geometriche per la costruzione delle strade", e di tipo C quando appartenenti ad itinerari di collegamento tra capoluoghi di provincia non altresì serviti da strade di tipo A o B. Ponti e reti ferroviarie di importanza critica per il mantenimento delle vie di comunicazione, particolarmente dopo un evento sismico. Dighe connesse al funzionamento di acquedotti e a impianti di produzione di energia elettrica.	**2.0**

Tabella 4: Tab. 2.4.II Norme Tecniche 2018

Nei confronti delle azioni sismiche gli stati limite ultimi (SLU) e gli stati limite di esercizio (SLE) sono definitivi riferendosi alle prestazioni della costruzione nel suo complesso includendo elementi strutturali, non strutturali ed impianti.

Stato limite di operatività (SLO)
Stato limite di danno (SLD)
Stato limite Ultimo di salvaguardia della vita (SLV)
Stato limite Ultimo di prevenzione del collasso (SLC)
La probabilità di superamento nel periodo di riferimento le PVR sono definite in funzione degli stati limite considerati.

Stati limite		P_{VR}: Probabilità di superamento nel periodo di riferimento V_R
SLE	**SLO**	**81 %**
	SLD	**63 %**
SLU	**SLV**	**10 %**
	SLC	**5 %**

Tabella 5: Tab. 3.2.I Norme Tecniche 2018

Fissata quindi la vita di riferimento e lo stato limite si ricava il tempo di ritorno:

$$T_R = - V_R / (\ln (1- P_{VR}))$$

Nel caso di studio, in quanto pianificazione, si terrà conto di un tempo di ritorno di 332 anni come da “Atto di indirizzo n. e coordinamento tecnico n. 112/2007 ai sensi dell’art. 16, c. 1, della L. R. 20/2000 per “Indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica””:

V_N (1) $\geq$ 50

C_U (I) = 0,7

V_R = 50 anni

9.2 AZIONE SISMICA DI PROGETTO

Per definire l’azione sismica di progetto è necessario valutare la “Risposta Sismica Locale” e cioè quelle modifiche che un segnale sismico subisce rispetto a quello di base di un sito di riferimento rigido e con superficie topografica orizzontale.

$$a_{max} = a_g \times S_t \times S_s$$

S_s = Coefficiente di Amplificazione Stratigrafica
S_t = Coefficiente di Amplificazione Topografica

In condizioni sismiche la norma prescrive le stesse verifiche da realizzarsi in condizioni statiche con l'introduzione dei coefficienti sismici kh e kv che devono essere calcolati mediante le espressioni:

$$\mathbf{k}_h = \beta_s (a_{max} / g)$$

$$\mathbf{k}_v = \pm 0.5\ \mathbf{k}_h$$

β_S= coefficiente di riduzione dell'accelerazione massima attesa al sito

il coefficiente di riduzione si calcola in funzione della categoria del sottosuolo e della zona geografica tramite il valore di a_g (SLV).

	Categoria del sottosuolo	
	A	**B, C, D, E**
	β_s	β_s
$0.2 < a_g \leq 0.4$	0.30	0.28
$0.1 < a_g \leq 0.2$	0.27	0.24
$a_g \leq 0.1$	0.20	0.20

Tabella 6: Tab. 7.11.I - Norme Tecniche 2018

Entrambi i siti sono soggetti ad un coefficiente di amplificazione sismica locale di PGA S=1.45, dato da:

$$S = S_S \times S_T$$

In quanto la categoria topografica del sito inerente il sito di studio ricade nella T1 (S_T= 1,0 coefficiente di amplificazione topografica in quanto l'area di studio si trova in area sub-pianeggiante "*Superfici pianeggianti*, p*endii e rilievi isolati con inclinazione media ≤ 15°*", ed S_S (coefficiente di amplificazione stratigrafica in SLV per terreni in categoria suoli **C**) = 1.45.

Nel caso di Sala Bolognese si rileva che per sottosuoli di categoria **C** l'**SLD** sarà:

Prob. Sup. %	Tr (anni)	ag (g)	Fo	Tc (sec)	Cc	Ss	St	Kh	Kv	a_{maz} (m/s^2)	β
63	35	0,061	2,513	0,272	1,61	1,5	1,0	0,018	0,009	0,892	0,20

e per l'**SLV**:

Prob. Sup. %	Tr (anni)	ag (g)	Fo	Tc (sec)	Cc	Ss	St	Kh	Kv	a_{maz} (m/s^2)	β
10	475	0,164	2,485	0,2501	1,60	1,45	1,0	0,057	0,029	2,331	0,24

10.3 ANALISI DI RISPOSTA SISMICA LOCALE RSL - ANALISI DI II LIVELLO

Dai dati della Regione Emilia Romagna, nell'atto di "*indirizzo e coordinamento tecnico ai sensi dell'art. 16, comma 1, della L.R. 20/2000 "Disciplina generale sulla tutela e l'uso del territorio", in merito a "Atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, c. 1, della LR 20/2000 per "Indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica (DGR 476/2021)*", si evidenzia per le porzioni di territorio comunale riferite a Sala Bolognese vi sia un valore di accelerazione massima orizzontale di picco al suolo rigido, cioè per T = 0, espressa in frazione dell'accelerazione di gravità g (a_{refg}) = 0.161 e, in caso di substrato profondo (significativo contrasto di impedenza a circa 100 m da p.c. e dal tetto del substrato rigido a circa 150 m da p.c. – PIANURA 2), utilizzando le relative tabelle, riportate nell'Allegato 2 degli Indirizzi regionali per la microzonazione sismica, sono così calcolati i seguenti fattori di amplificazione F.A sismica rispetto ad un suolo di riferimento:

- 1,7 = fattore di amplificazione in termini di rapporto di accelerazione massima orizzontale (PGA/PGA_0)
- 2,0 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI0) per 0.1s < T_o < 0.5s
- 3,1 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI0) per 0.5s < T_o < 1.0s
- 3,6 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI0) per 0.5s < T_o < 1.5s

Adottando i parametri forniti nell'atto di indirizzo della regione Emilia-Romagna l'accelerazione massima attesa al sito per lo stato limite SLV sarà data da:

$$a_{max} = a_{refg} \times FA = 2,684$$

con:

a_{refg} = 0,161

FA = 1,70

e i coefficienti sismici kh e kv avranno valore:

$$k_h = (\beta_s \times a_{max}) / g = 0.066$$

$k_v = 0.033$

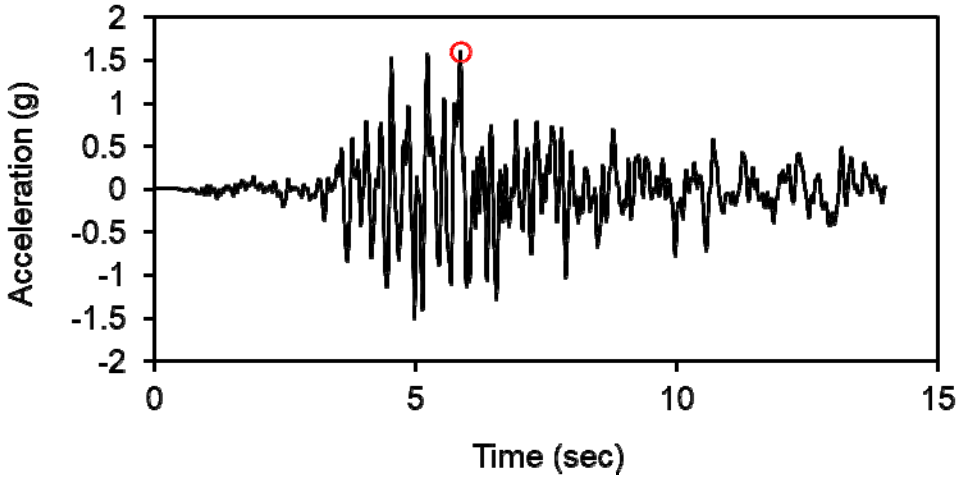
10.4 ANALISI DI RISPOSTA SISMICA LOCALE RSL - ANALISI DI III LIVELLO

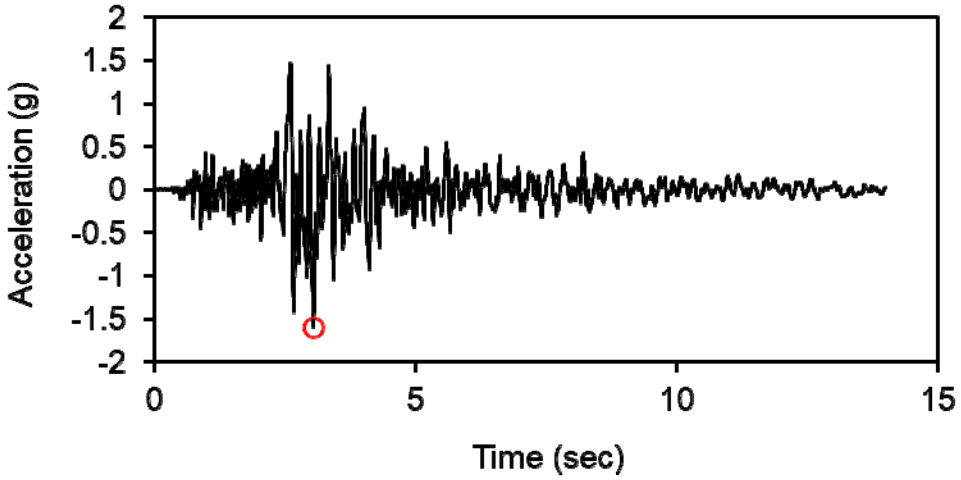
Qui di seguito viene effettuato lo studio di risposta sismica locale al fine di determinare i coefficienti di amplificazione sismica rispetto al suolo di riferimento, in termini di rapporto di accelerazione massima orizzontale (PGA/PGA_0). Questo studio rientra in un'analisi di III livello a norma NTC2018 e sulla base di quanto indicato nel" *Atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, c. 1, della L. R. 20/2000 per "Indirizzi per gli studi di microzonazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica"*".

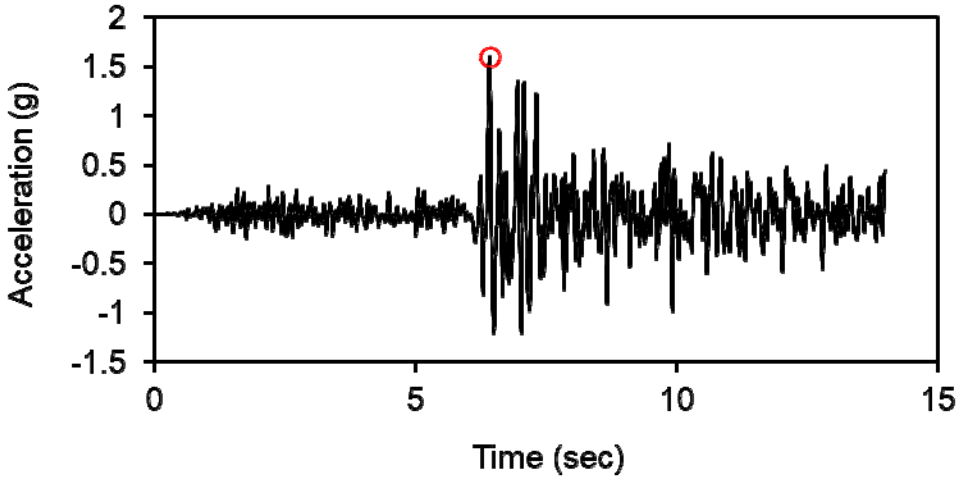
Per l'input sismico sono stati utilizzati i dati forniti dalla Regione Emilia-Romagna per il territorio di Sala Bolognese e, nello specifico, sono stati impiegati sette segnali di riferimento (figura 12), già scalati che sono stati selezionati dalla banca dati accelerometrica "European Strong Motion database" attraverso una procedura che valuta la similarità tra una forma spettrale di riferimento e la forma degli spettri di risposta dei segnali contenuti nella banca dati ISESD e ITACA.

Magnitude (Mw)	Epic.Distance (Km)	Scaling_Factor	Source File_Name
6.2	29.9	2.13%	ESM EU.HRZ..HNE.D.19790524.172317.C.ACC.ASC
5.74	12.57	1.40%	NGA RSN146_COYOTELK_G01320.AT2
5.99	54.21	2.64%	NGA RSN703_WHITTIER.A_A-VAS000.AT2
6.93	83.53	1.56%	NGA RSN804_LOMAP_SSF205.AT2
6.69	38.07	1.17%	NGA RSN1091_NORTHR_VAS090.AT2
6.6	31	0.66%	KiKnet SMNH100010061330.EW2
5.9	14.4	2.78%	ESM IT.SLO..HGE.D.20161026.191806.C.ACC.ASC

Tabella 7: Elenco accelerogrammi tratti da Rexel.


Acceleration (g)
2
1.5
1
0.5
0
-0.5
-1
-1.5
-2
0
5
10
15
Time (sec)


Acceleration (g)
2
1.5
1
0.5
0
-0.5
-1
-1.5
-2
0
5
10
15
Time (sec)


Acceleration (g)
2
1.5
1
0.5
0
-0.5
-1
-1.5
0
5
10
15
Time (sec)

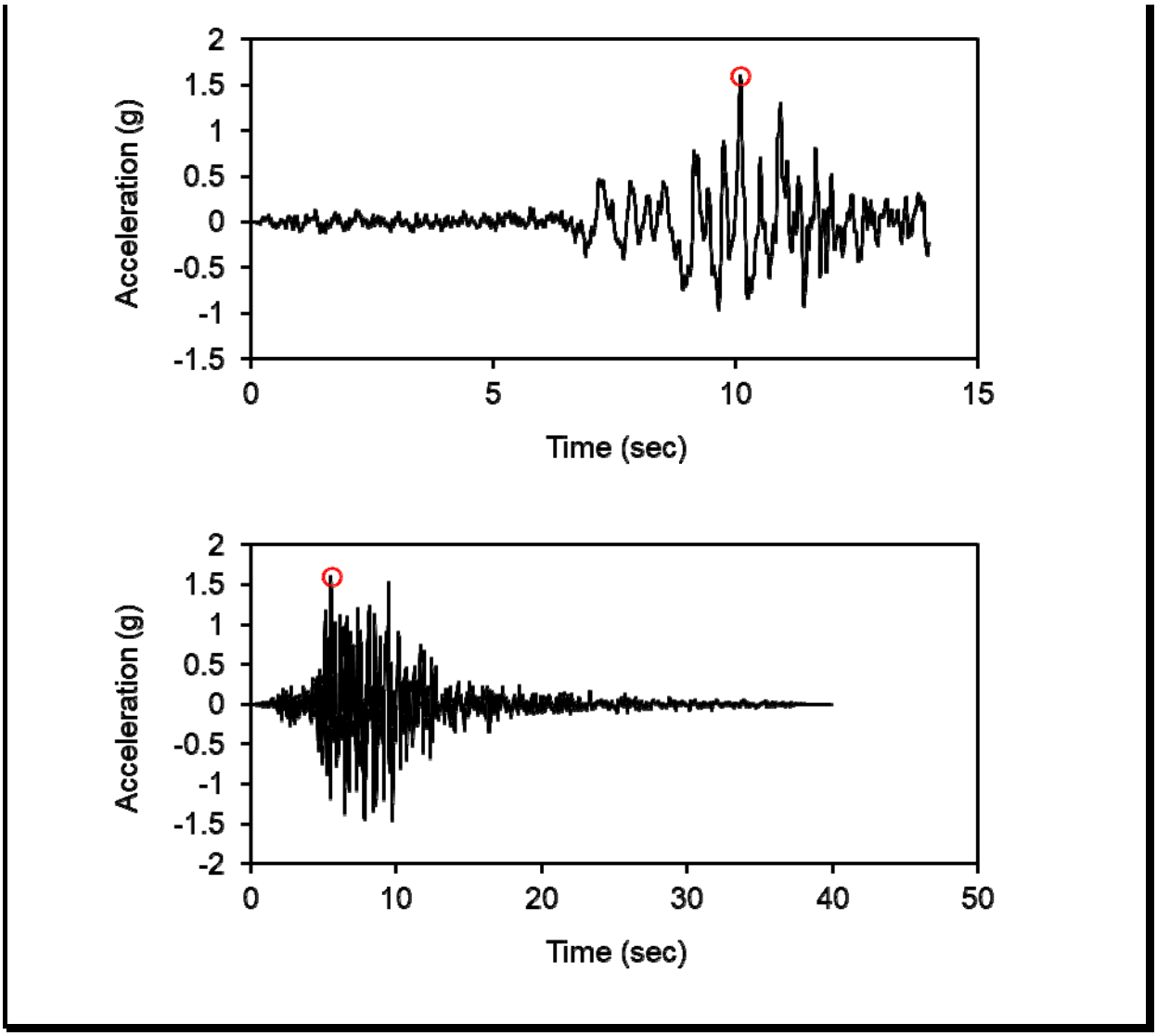


Fig. 12: accelerogrammi dei segnali di riferimento per Sala Bolognese forniti dalla Regione Emilia Romagna

Come programma numerico di analisi si è optato per il programma EERA (Equivalent-linear Earthquake site Response Analisys of Layered Soil Deposits), basato sul codice SHAKE 91 per quanto concerne le soluzioni relative alle propagazioni delle onde di taglio.

Il codice di calcolo EERA valuta la risposta sismica di un deposito di terreno, schematizzandolo come un sistema di N strati orizzontali omogenei, isotropi e visco-elastici, sovrastanti un semispazio uniforme, attraversati da un treno di onde di taglio che incidono verticalmente le superfici. Ogni strato è descritto per mezzo dello spessore H, del modulo di taglio massimo G_{max} o dalla corrispondente velocità massima V_{max}, dal valore dello smorzamento D, dal peso dell'unità di volume γ (o dalla densità di massa $\rho = \gamma / g$) e dalle curve di decadimento del modulo di rigidezza a taglio normalizzato (G / G_0 - γ) e le corrispondenti curve dello smorzamento (D - γ) con la deformazione di taglio γ.

L'analisi di tipo lineare equivalente che consiste nell'esecuzione di una sequenza di analisi lineari complete con aggiornamento successivo dei parametri di rigidezza e smorzamento fino al soddisfacimento di un prefissato criterio di convergenza. Il calcolo è stato eseguito inserendo come segnale di input, i sette segnali precedentemente identificati (fig. 12), provvedendo al taglio delle frequenze superiori ai 25 Hz, scalati sulla base di un valore di accelerazione massima orizzontale di picco (PGA) su un suolo di riferimento di tipo A, per T=0, espressa in frazione dell'accelerazione di gravità (a_{refg} - 10% di probabilità di superamento in 50 anni) pari a **0.164g**.

Per le curve di variazione del modulo di rigidezza a taglio G e del fattore di smorzamento D (damping ratio) in funzione della deformazione per le diverse tipologie di materiali, sono state impiegate quelle già presenti nel codice di calcolo in quanto ritenute sufficientemente assimilabili alla modellazione dell'area di studio.

Per la verifica della risposta sismica locale, in base alle indagini svolte sia di tipo geotecnico che di tipo geofisico, è stato modellato il sottosuolo fino al bedrock dedotto dalle sezioni geologiche disponibili, dalle indagini geofisiche effettuate e dalle indicazioni di letteratura in merito. Di seguito viene schematizzato il modello utilizzato per l'analisi:

Inserito il modello nel programma di calcolo, l'elaborazione, svolta sui n. 7 terremoti di riferimento, ha fornito i seguenti risultati, in termini di spettro di risposta elastico in accelerazione massima orizzontale in superficie per un valore di smorzamento critico pari al 5% (figura 13 e 14):

livello	profondità banco	spessore banco	litologia prevalente	Vs (m/s)
1	20,0	20,4	Argille limose	160
2	80,0	60,0	Argille limose	290
3	150,0	70,0	Limi Argillosi	530
4	inf	inf	Ghiaie	800

Tabella 8: modello geologico di riferimento

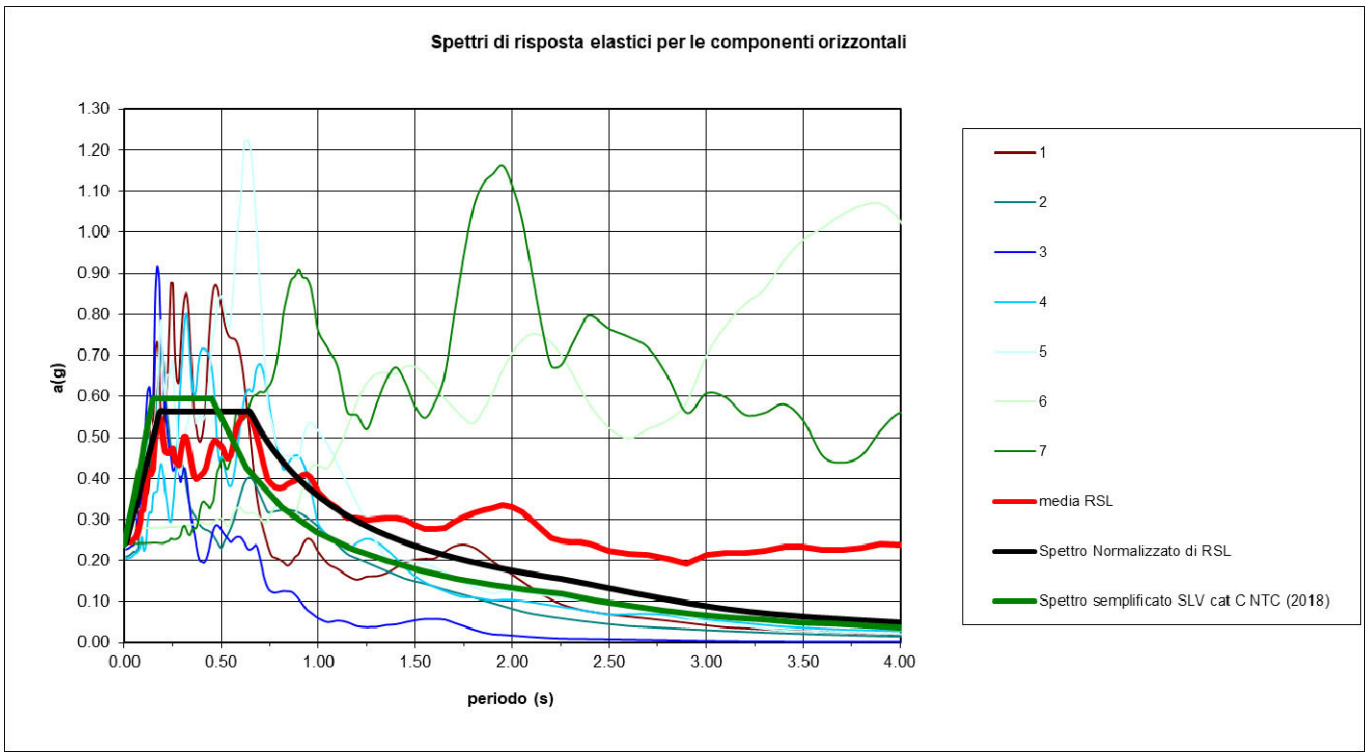


Fig. 13: risultato dell'analisi di risposta sismica locale per gli spettri di risposta con periodo di ritorno di 475 anni e smorzamento pari al 5%

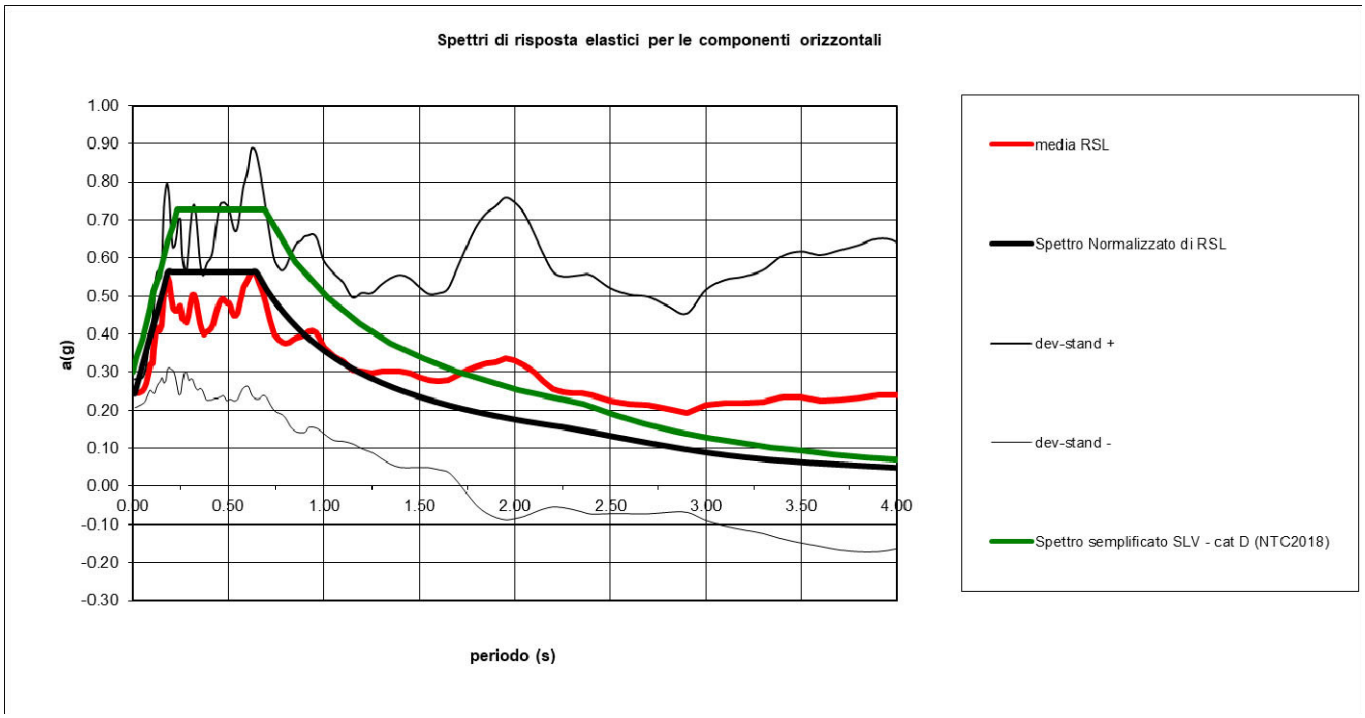


Fig. 14: risultato dell'analisi di risposta sismica locale per gli spettri di risposta con periodo di ritorno di 475 anni e smorzamento pari al 5% con spettro medio su 10 accelerogrammi e relativa deviazione standard

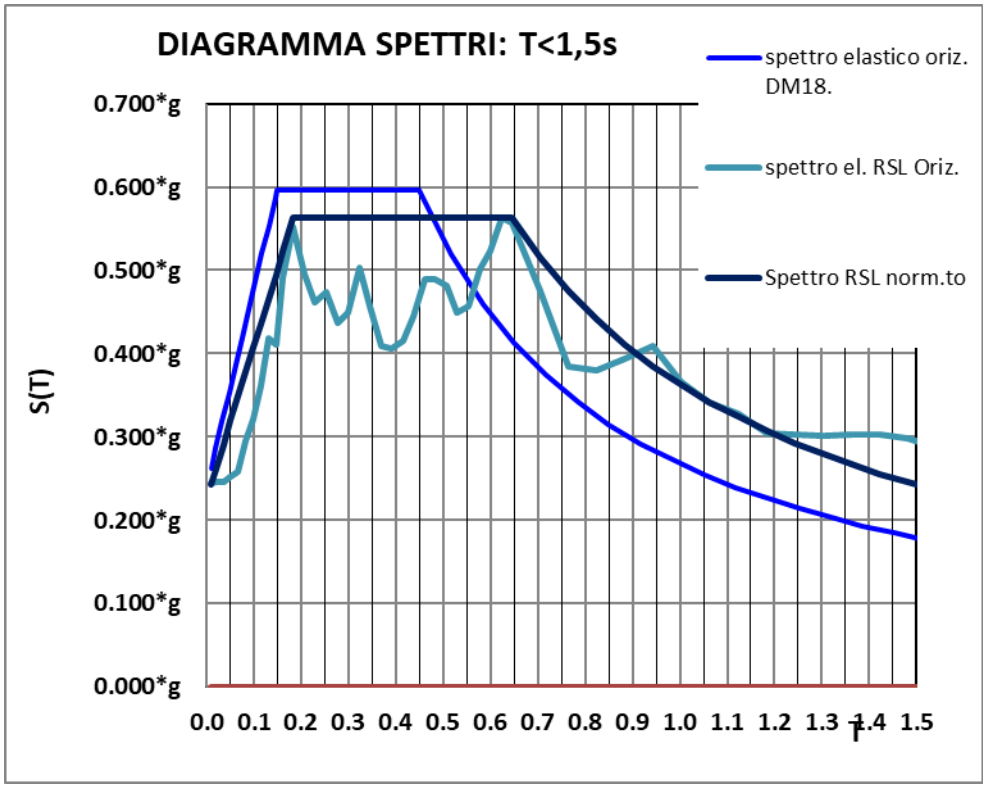


Fig. 15: raffronto fra lo spettro medio della RSL lo spettro normalizzato di RSL e lo spettro elastico da NTC2018 per suoli di categoria C (SLV) per un periodo 0.0 < T < 1,5 s.

Come si può notare (fig.15) l'analisi di risposta sismica locale (RSL) restituisce uno spettro **medio** più severo rispetto allo spettro di normativa per un suolo di categoria **C**.

L'analisi di risposta sismica locale RSL fornisce una PGA sulla superficie pari a 0.22g, come quella calcolata in base ai dati (accelerogrammi) regionali e inferiore a quanto previsto da normativa, ovvero 0.24g (NTC 2018).

In base all'analisi della Risposta Sismica Locale (figura 13 e 14) risulta che i fattori di amplificazione F.A sismici rispetto ad un suolo di riferimento risultano:

- 1,372 = fattore di amplificazione in termini di rapporto di accelerazione massima orizzontale (PGA/PGA_0) rispetto allo spettro di RSL Normalizzato e lo Spettro Semplificato NTC 2018 su suolo rigido (TR 475 anni);
- 1,59 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI_0) per $0.1s < T_o < 0.5s$
- 2,279 = fattore di amplificazione in termini di rapporto di Intensità di Housner (SI/SI_0) per $0.5s < T_o < 1.0s$

Appare evidente che in questo caso i valori di normativa appaiono meno severi e conservativi rispetto a quelli di RSL; si rimanda pertanto al progettista la scelta del modello da seguire.

Di notevole interesse appare inoltre il fattore di amplificazione massima in funzione della frequenza (figura 16) ovvero è risultato un fattore di amplificazione massima (F.A.) pari a 2,62 alla frequenza di 0,6 Hz, abbastanza in accordo con quanto evidenziato dalla registrazione strumentale con tomografo digitale Tromino che indicava frequenze di sito possibili di amplificazione a circa 0,84±0,1 Hz. Pertanto si consiglia di evitare accoppiamenti in frequenza riguardante i fabbricati in progetto riferiti alle frequenze sopra indicate per evitare fenomeni di risonanza che risulterebbero sensibilmente più distruttivi di quanto ci si potrebbe attendere. In questo senso, una generale relazione empirica che lega la frequenza di vibrazione di un edificio e la sua altezza è la seguente: f = (10÷12)/n.piani.

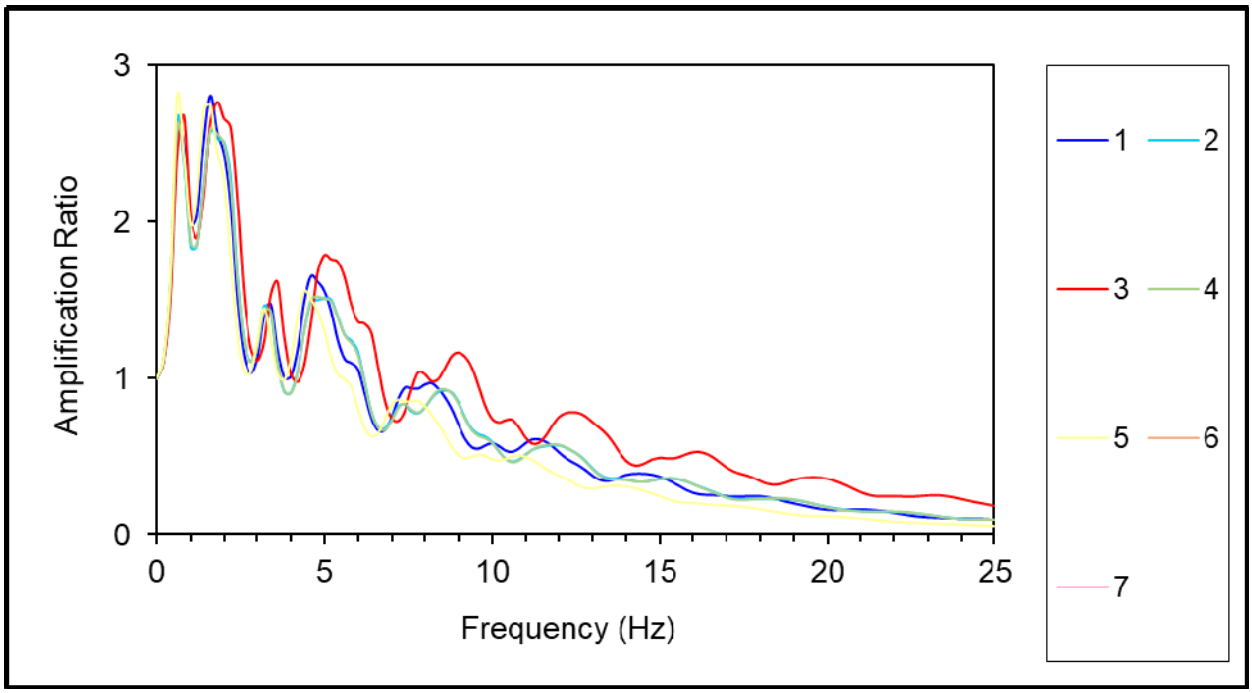


Fig. 16: fattore di amplificazione F.A. in funzione della frequenza

In ultimo vengono di seguito forniti i parametri indipendenti (per un periodo di ritorno di 475 anni), sia da NTC 2018 che da riferimento regionale e i parametri dipendenti riferiti allo spettro normalizzato di RSL, utili ai fini dei calcoli ingegneristici.

PARAMETRI INDIPENDENTI:

a_{refg} = 0,164 g (fornito dalla regione Emilia Romagna e dall'NTC 2018)

F_0 = 2,501

T^*_c = 0,282 s

PARAMETRI DIPENDENTI:

S = 1,37 (da RSL)

S = 1,45 (da NTC 2018)

Tb = 0,18	Se(T) = 0,563 g
Tc = 0,65	Se(T) = 0,563 g
Td = 2,26	Se(T) = 0,161 g

10.5 VALUTAZIONE DELLA POSSIBILITÀ DI OCCORRENZA DI FENOMENI DI LIQUEFAZIONE

Con riferimento all'Atto di indirizzo e coordinamento tecnico ai sensi dell'art. 16, c. 1, della L. R. 20/2000 per "Indirizzi per gli studi di micro zonizzazione sismica in Emilia-Romagna per la pianificazione territoriale e urbanistica" del 2 maggio 2007 (progr. 112) dell'Assemblea legislativa della Regione Emilia-Romagna ed in particolare in relazione all'allegato 3 della stessa, è stata condotta una valutazione sulla possibilità di fenomeni di liquefazione dei terreni presenti nell'area di studio.

Il fenomeno della liquefazione (termine coniato da Mogani e Kubo nel 1953) interessa quei depositi sabbiosi saturi che, nel corso di un terremoto o più genericamente durante e immediatamente dopo una sollecitazione di tipo ciclico, subiscono una drastica riduzione della resistenza al taglio, a seguito della quale le condizioni di stabilità non sono più garantite e la massa di terreno interessata dal fenomeno comincia ad assestarsi (nel caso di un deposito orizzontale) fino a che la nuova configurazione del terreno non è compatibile con la nuova diminuita resistenza al taglio. In condizioni di sisma, vi possono anche essere effetti di "riordino" dei sedimenti, con possibilità di cedimenti significativi e che possono coinvolgere sia i depositi granulari poco addensati e recenti (olocenici), sia i sedimenti fini poco coesivi.

Risulta di fondamentale importanza la corretta conoscenza geologica di tutte quelle strutture suscettibili alla liquefazione di cui tutt'ora sono presenti notevoli lacune; studi relativamente aggiornati (Youd e Perkins - 1978; Mori et al. - 1978; CNR - 1983) hanno evidenziato come i sedimenti alluvionali e deltizi sono maggiormente suscettibili alla liquefazione se sono di deposizione recente o recentissima (depositi olocenici o addirittura minori di 500 anni). Dalle informazioni ottenute dal PTM – Piano Territoriale Metropolitano del Comune di Bologna, Tavola 4 *Carta di area vasta delle aree suscettibili di effetti locali* (Fig. 17) possiamo notare come i due siti di studio siano interessati da terreni "C – sedimenti prevalente fini di pianura; tuttavia, prudentemente, viene effettuata comunque la verifica alla liquefazione vedendo la natura dei terreni rilevati tramite le indagini geognostiche.

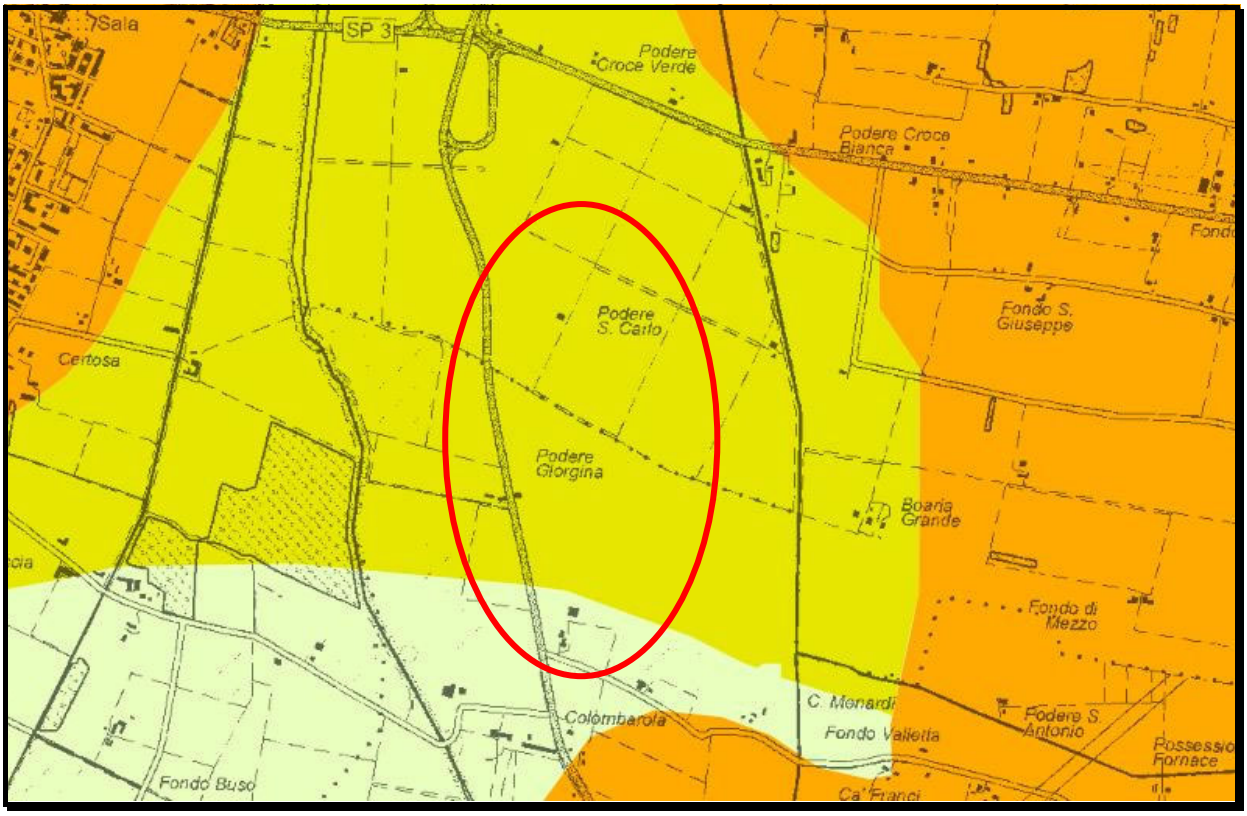


Figura 17: Estratto dalla Tav. 4 – "Carta delle aree suscettibili di effetti locali" del PTM di Bologna.

In base alle elaborazioni delle indagini svolte nei siti, la litologia di superficie prevalente risulta essere limo argilloso e argillo limosa con lenti decimetriche (raramente metriche) di materiali granulari (prevalentemente sabbia); pertanto, da queste informazioni le indicazioni preliminari sulla pericolosità del potenziale di liquefazione in relazione alle litologie riscontrate risulterebbe da moderata ad alta.

Tuttavia, nel recente terremoto del maggio 2012, nell'area di studio non si sono verificati fenomeni di liquefazione.

La probabilità che nei terreni sabbiosi saturi si verifichino fenomeni di liquefazione è bassa o nulla se si verifica almeno una delle seguenti condizioni:

1. Accelerazione massima attesa in superficie in condizioni *free-field* minore di 0,1g;

2. Accelerazione massima attesa in superficie in condizioni *free-field* minore di 0,15g e terreni con caratteristiche ricadenti in una delle tre seguenti categorie:

- − frazione di fine, FC, superiore al 20%, con indice di plasticità PI > 10;
- − FC ≥ 35% e resistenza $(N_1)_{60}$ > 20;
- − FC ≤ 5% e resistenza $(N_1)_{60}$ > 25

dove $(N_1)_{60}$ è il valore normalizzato della resistenza penetrometrica della prova SPT, definito dalla relazione: $(N_1)_{60} = N_{SPT}C_N$ in cui il coefficiente C_N è ricavabile dall'espressione

$$C_N = \left(\frac{p_a}{\sigma'_v} \right)^{0.5}$$

essendo p_a la pressione atmosferica e σ'v la pressione efficace verticale.

3. Distribuzione granulometrica esterna alle zone indicate nella Figura 18(a) nel caso di materiale con coefficiente di uniformità Uc < 3.5 ed in Figura 18(b) per coefficienti di uniformità Uc > 3.5.

4. Profondità media stagionale della falda superiore ai 15 m dal piano campagna.

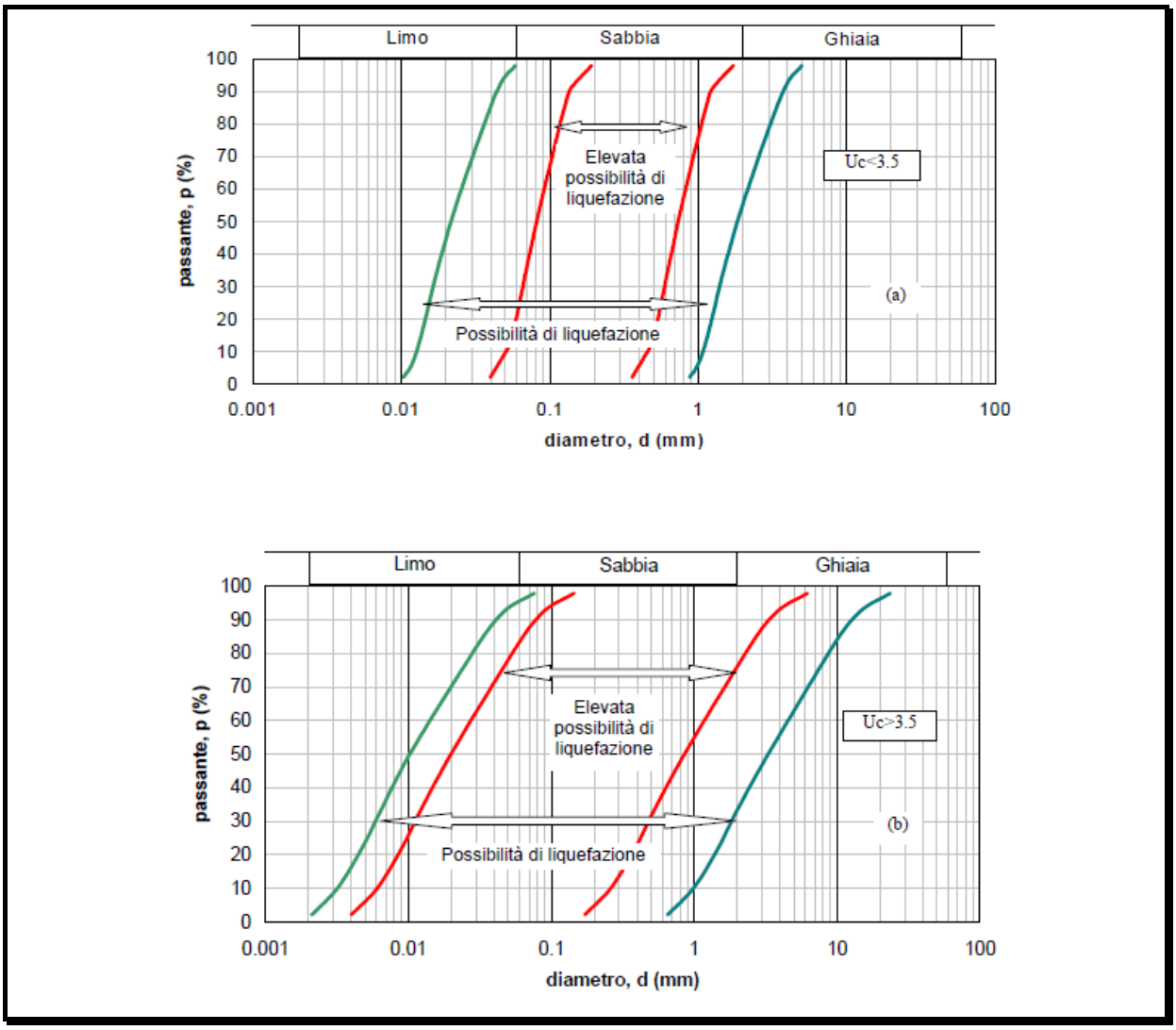


Fig. 18: Fasce granulometriche per la valutazione preliminare della suscettibilità alla liquefazione di un terreno per i terreni a granulometria uniforme (a) ed estesa (b) (da AGI 2005)

Molti Autori hanno evidenziato una correlazione positiva tra età e tipo di deposito alluvionale continentale, riguardo la propensione alla liquefazione:

1) Youd e Perkins, 1978 – hanno composto una tabella che sintetizza i dati raccolti durante terremoti "strong motion" dell'area di S. Diego (California), da cui risulta che i sedimenti deposti da corsi d'acqua (piana alluvionale di esondazione, canale fluviale, delta fluviali, estuari) dimostrano una probabilità di liquefazione da alta a molto alta se di età minore di 500 anni o Olocenica, gli stessi depositi se di età pleistocenica o pre-pleistocenica hanno invece una "bassa" probabilità di liquefarsi. Cioè l'osservazione dimostra che sono solamente i sedimenti di deposizione recente (olocene) e recentissima (meno di 500 anni) a presentare un'alta pericolosità per la liquefazione.

2) Mori et Al, 1978 – dimostrano che la suscettibilità alla liquefazione decresce nei sedimenti di età maggiore di 500 anni, con scarti anche molto alti (maggiori del 50%). Tolno, 1975 dimostra l'incremento di densità secca (stato di addensamento) del sedimento in relazione all'aumento di vetustà (dall'Olocene al terziario)

3) Iwasaki et Al, 1982 – dimostra per terremoti giapponesi la correlazione diretta tra probabilità di liquefazione e letti di fiumi recenti e antichi;

4) CNR, 1983 – ripropone la correlazione diretta tra sedimenti fluviali e deltizi continentali ed età del deposito (i più recenti sono più suscettibili alla liquefazione).

In conclusione la letteratura geologica, ormai ben consolidata e verificata, indica che le maggiori probabilità di liquefazione si hanno nei sedimenti granulari saturi recenti e recentissimi. Ciò significa che gli alvei abbandonati e sepolti dei corsi d'acqua possono costituire fonte di pericolo di liquefazione anche per sismi di magnitudo modesta come quelli previsti per il territorio bolognese (M=5,5÷5.6).

Per ogni verticale di indagine effettuata la stima del potenziale di liquefazione potrà essere effettuata con i metodi semplificati e a tal fine in ogni verticale dovrà essere valutato il picco di accelerazione a_{max} alla superficie del deposito; facendo riferimento a quanto esposto nel capitolo 9.4 in merito alla categoria di suolo, le verifiche verranno effettuate nei confronti della situazione più cautelativa, ovvero quella di normativa in quanto la verifica di RSL ha dato valori di F.A. sensibilmente inferiori rispetto alla norma.

Le verifiche della suscettibilità alla liquefazione e dei cedimenti potenziali indotti da sisma vengono valutati utilizzando correlazioni empiriche basate sui risultati della prova CPTu (es. P.K Robertson 1990; 1998; 2009-2010).

I dati ricavati dalle prove penetrometriche sono stati elaborati secondo le procedure semplificate di verifica della liquefacibilità e stima dei cedimenti sismici attualmente più accreditate, basate sulle esperienze di Seed e Idriss (1971), Imai & Tonouchi (1982), Robertson e Campanella (1985) e di Robertson & Wride (1998), recentemente aggiornate dallo stesso P.K. Robertson (2009-2010). Le analisi svolte seguono, inoltre, le note procedure di riferimento dettate dall'NCEER. Questo approccio valuta la propensione alla liquefazione e stima i cedimenti post sisma sia nei sedimenti granulari saturi

e insaturi, sia nei sedimenti fini, poco coesivi. Per la verifica alla propensione alla liquefazione dei sedimenti e dei cedimenti post sisma dell'area di sedime si è ricorsi al software "Cliq", sviluppato dalla GeoLogiki Geotechnical Engineers in collaborazione con lo stesso P.K. Roberson.

Si è inoltre tenuto conto di una quota piezometrica da sisma saliente fino a un massimo pari a quota campagna (così come si è verificato nel recente terremoto Emiliano del 20 e 29 maggio 2012).

Per il metodo semplificato sono riportati sia in testo che negli elaborati allegati le metodologie semplificate che utilizzano le prove CPTu di seguito indicate:

- metodo di Robertson e Wride (1998) e Robertson (2009);

I metodi semplificati prevedono la verifica di un coefficiente di sicurezza dato da:

$$F_L = \frac{CRR}{CSR} \cdot MSF$$

dove, da Seed & Idriss (1971):

- $CRR = \frac{\tau_{ult}}{\sigma'_{v0}}$ è la resistenza normalizzata (rispetto alla pressione efficace verticale iniziale (σ'_{v0})) valutabile tramite abachi o prove quali SPT e CPT e da misure della velocità delle onde di taglio Vs;

- $CSR = \frac{\tau_{media}}{\sigma'_{v0}} = 0.65 \frac{a_{max}}{g} \frac{\sigma_v}{\sigma'_v} r_d$ è la tensione indotta dal terremoto;
- a_{max} è l'accelerazione di gravità
- σ_v e σ'_v sono rispettivamente la tensione verticale e la tensione efficace verticale alla profondità considerata;
- r_d è un coefficiente riduttivo dell'azione sismica che porta in conto la deformabilità del sottosuolo e che può essere determinato con la relazione semplificata $r_d = 1 - 0.015z$;
- *MSF* è un fattore di scala che può essere valutato in funzione della magnitudo dei terremoti attesi.

In anni recenti l'aumento della base statistica di dati CPT ha reso possibile lo sviluppo di tecniche di analisi del potenziale di liquefazione direttamente basate sui risultati di prove CPT e molto affidabili come il metodo semplificato di Robertson e Wride (1998). A riprova della bontà di tale metodo si rimanda al lavoro del dicembre 2004 che vedeva come responsabile la Prof.ssa ing. Teresa Crespellani "R*elazione generale, descrittiva dei criteri seguiti nella programmazione e nell'esecuzione delle prove geotecniche dinamiche effettuate in laboratorio e in sito, e contenente i risultati dell'attività di ricerca svolta per la caratterizzazione dei terreni in campo statico e dinamico*" in cui si è potuto verificare che esiste una buona corrispondenza tra i valori del rischio di liquefazione ottenuti nel lavoro effettuato con la procedura semplificata di Robertson e Wride e quelli ottenuti con la metodologia basata su prove triassiali cicliche condotte su provini ricostruiti in laboratorio in condizioni simulanti da

vicino quelle in sito durante il terremoto di progetto.

Si chiarisce comunque che il metodo elaborato da Robertson e Wride (1998), aggiornato dallo stesso Robertson (2009), si basa sull'elaborazioni di dati provenienti da CPTE e/o CPTU e un po' meno per le Cpt meccaniche.

La curva base per sabbia pulita della figura 24 può essere approssimata dalla seguente equazione (Robertson e Wride, 1998)

se $(q_{c1N})_{cs} < 50$ $$CRR_{7.5} = 0.833\left[\frac{(q_{c1N})_{cs}}{1000}\right] + 0.05$$

se $50 \leq (q_{c1N})_{cs} < 160$ $$CRR_{7.5} = 93\left[\frac{(q_{c1N})_{cs}}{1000}\right]^3 + 0.08$$

dove $(q_{c1N})_{cs}$ rappresenta la resistenza alla punta penetrometrica normalizzata a 1 atm (100 kPa). La procedura CPT richiede la normalizzazione della resistenza alla punta utilizzando le seguenti relazioni:

$$q_{c1N} = C_Q\left(\frac{q_c}{p_a}\right) \qquad C_Q = \left(\frac{p_a}{\sigma'_{v0}}\right)^n \quad (16b)$$

C_Q è il fattore di normalizzazione

p_a è la pressione atmosferica (1 atm) o comunque nella stessa unità di misura di σ'_{v0}

n è un esponente che varia col tipo di terreno

q_c è la resistenza alla punta del penetrometro statico.

A profondità basse C_Q diventa elevato per la bassa pressione verticale geostatica.

Comunque non vanno applicati valori di C_Q maggiori di 1.7. Il valore di n varia da 0.5 a 1.0 in funzione delle caratteristiche granulometriche del terreno (Olsen 1997).

Il rapporto di attrito (la resistenza laterale f_s divisa per la resistenza q_c) generalmente cresce al crescere del contenuto in fini e della plasticità del terreno, consentendo una stima approssimata del tipo di terreno e del contenuto in fini dai dati CPT.

Robertson e Wride (1998) hanno costruito l'abaco riprodotto in Figura 19 per la stima del tipo di terreno.

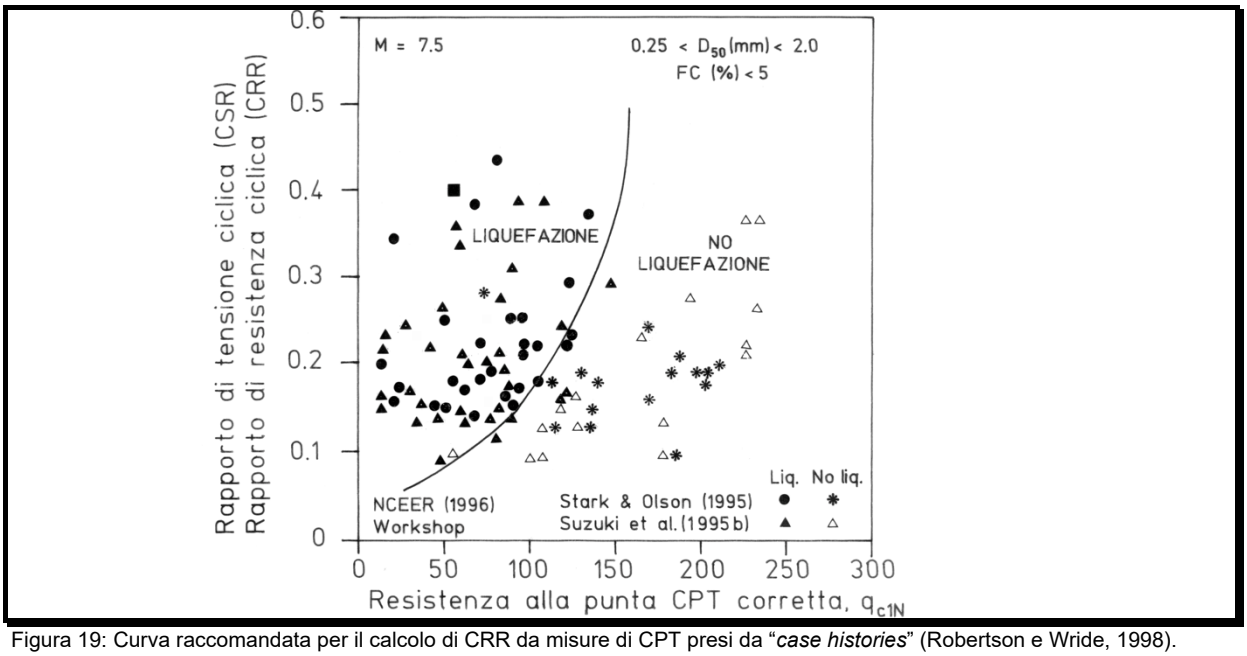


Figura 19: Curva raccomandata per il calcolo di CRR da misure di CPT presi da "*case histories*" (Robertson e Wride, 1998).

Per le verifiche a liquefazione del sito sono state perseguite tre metodologie per ottenere la Magnitudo del momento sismico (Mw) di riferimento per il calcolo:

1. tramite le zone sismogenetiche ZS9, che indicano una magnitudo massima per ogni zona (al più si può discretizzare in base al database DISS);
2. tramite la consultazione del Catalogo Parametrico dei Terremoti italiani (CPTI) (sito emidius.mi.ingv.it/cpti11) con individuazione del sito e il filtro di tutti i terremoti presenti in un'area circolare di 50 km di raggio (riferendosi al lavoro di Galli et *alli*, per cui sono da ritenersi poco probabili fenomeni di liquefazione ubicati oltre i 50 km di distanza dall'epicentro) oltre alla verifica del database DISS 3.1;
3. Tramite la mappa interattiva di pericolosità sismica dell'INGV (indirizzo esse1-gis.mi.ingv.it), in cui è possibile calcolare il terremoto di scenario basandosi sul concetto di disaggregazione della pericolosità sismica in cui si sommano i contributi dovuti alle singole coppie magnitudo-distanza degli epicentri ricadenti all'interno dell'area di riferimento (50 km).

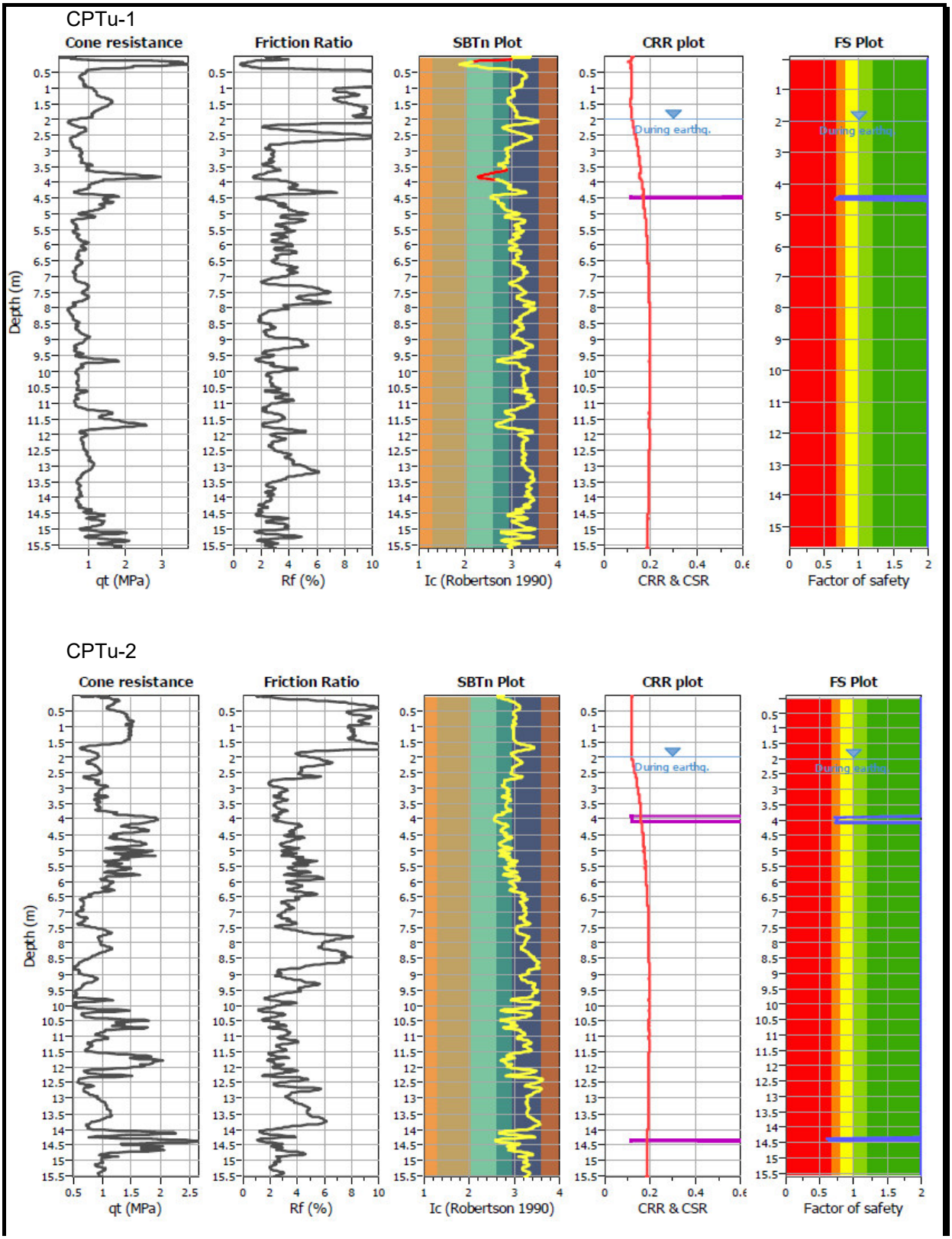
Il primo metodo non considera il tempo di ritorno come da normativa pertanto risulta eccessivamente gravoso mentre il secondo metodo è sicuramente meno oneroso. Di seguito si riportano i valori di Mw ottenuti per ognuno dei metodi applicati:

1. Mw = 6,14 Zona sismogenetica 612;

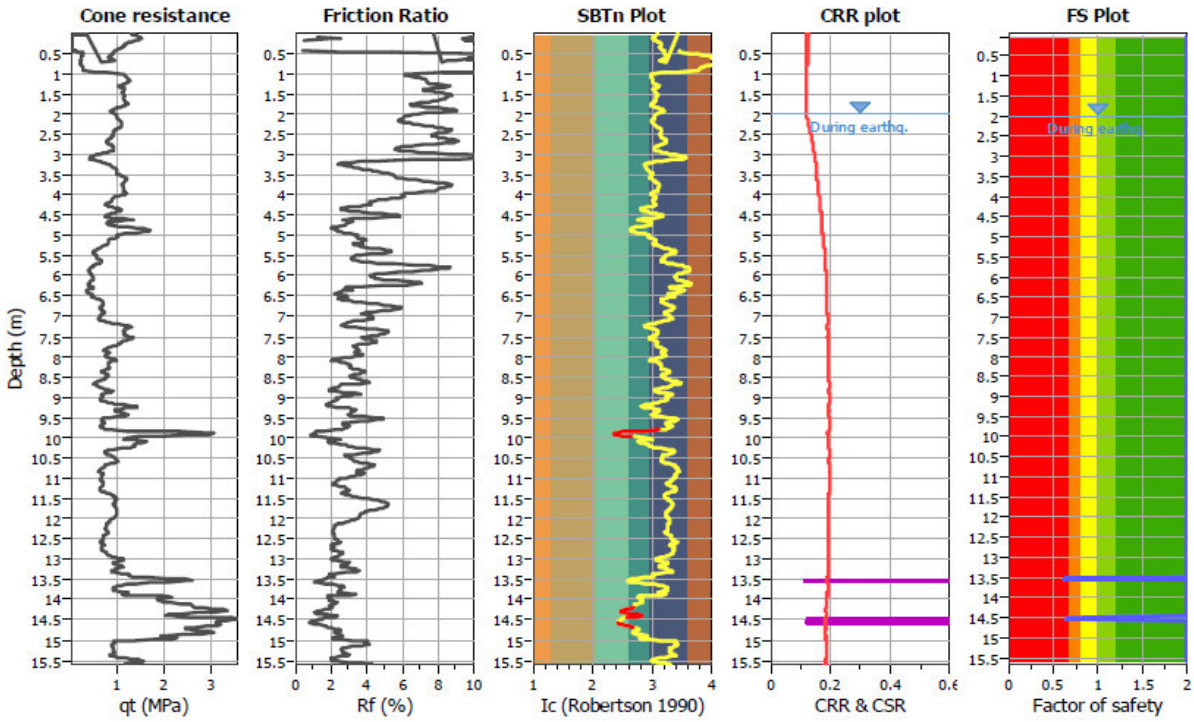
2. SISMA DI RIFERIMENTO
   - 29 maggio 2012 con epicentro a Finale Emilia (MO) (lat. 44.905800– lon. 11.234248);
   - distanza dell'area di studio dall'epicentro ~ 13 Km;
   - magnitudo Mw riferita al terremoto di riferimento pari a ≈ 5.9;
   - $a_{max} = a_g \times S_t \times S_s = a_{refg} \times S_t \times S_s = 0.157 \times 1.59 \approx 0.25$ (per terreni di categoria C)
3. Mw = 5,06 con distanza epicentrale di 20,7km (metodo della disaggregazione)

Come anticipato è stato effettuato un campionamento, durante la campagna di indagini, con prelievo di un campione indisturbato con fustella a pareti sottili di tipo shelby e sottoposta ad analisi granulometrica per vagliatura e sedimentazione i cui esiti sono stati sovrapposti al fuso granulometrico di possibile liquefazione proposto da AGI e dalla Delibera regionale (Atto di indirizzo e coordinamento tecnico prog. 112). Gli esiti dimostrano che le sabbie del campione sono perfettamente comprese entro il fuso granulometrico suscettibile di liquefazione con Uc > 3,5 (fig. 23). Le verifiche sono state condotte secondo il metodo di Idriss e Boulanger (2014) tramite programma di calcolo automatico della liquefacibilità e dei cedimenti post sisma con il software "Cliq", sviluppato dalla GeoLogismiki Geotechnical Engineers in collaborazione con P.K. Roberson. Le verifiche sono state comunque condotte nelle condizioni peggiorative ovvero con Mw = 6,14 (zona sismogenetica 612) e a_{gmax} = 0.22 g (come da RSL) e falda durante l'evento sismico fino ad un massimo tra -2,0 e -2,5 m da p.c.. Di seguito si riportano le verifiche effettuate sulle prove CPTu-1, CPTu-2, CPTu-3, CPTu-4, CPTu-5, CPTu-6, CPTu-7 e CPTu-8 (fig.20).

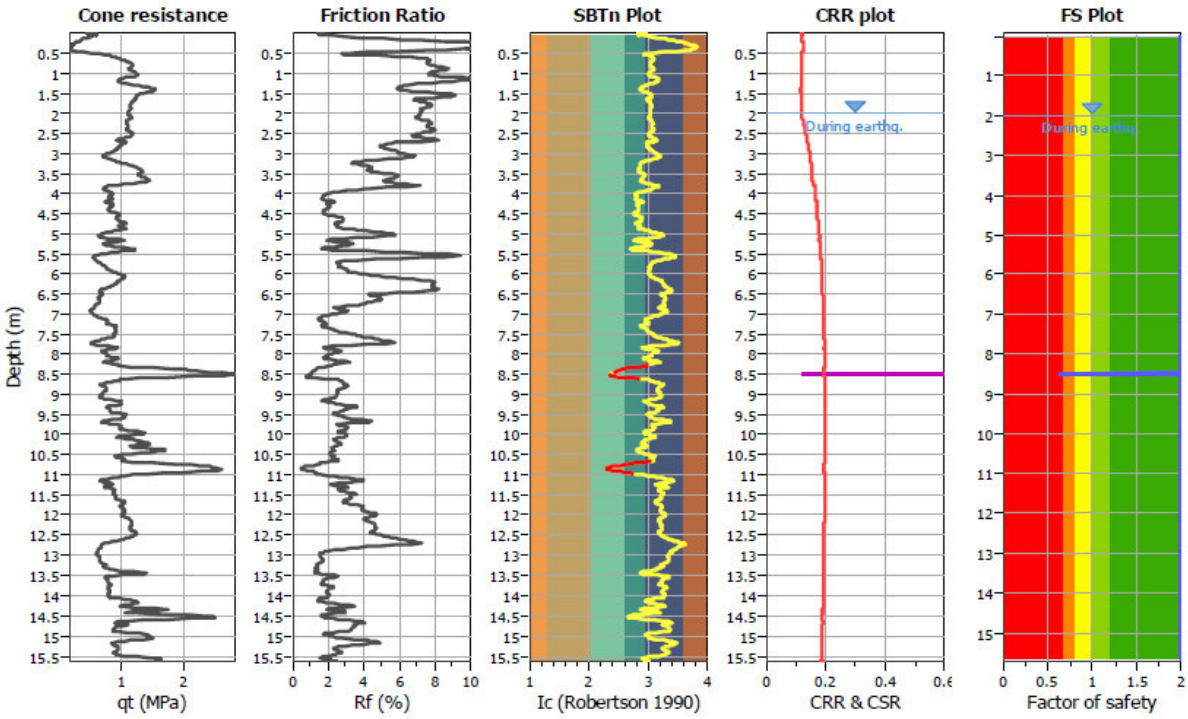
10.5.1 VERIFICA IN CONDIZIONI DI TERRENO DI CATEGORIA C (AMAX = 0.22g)



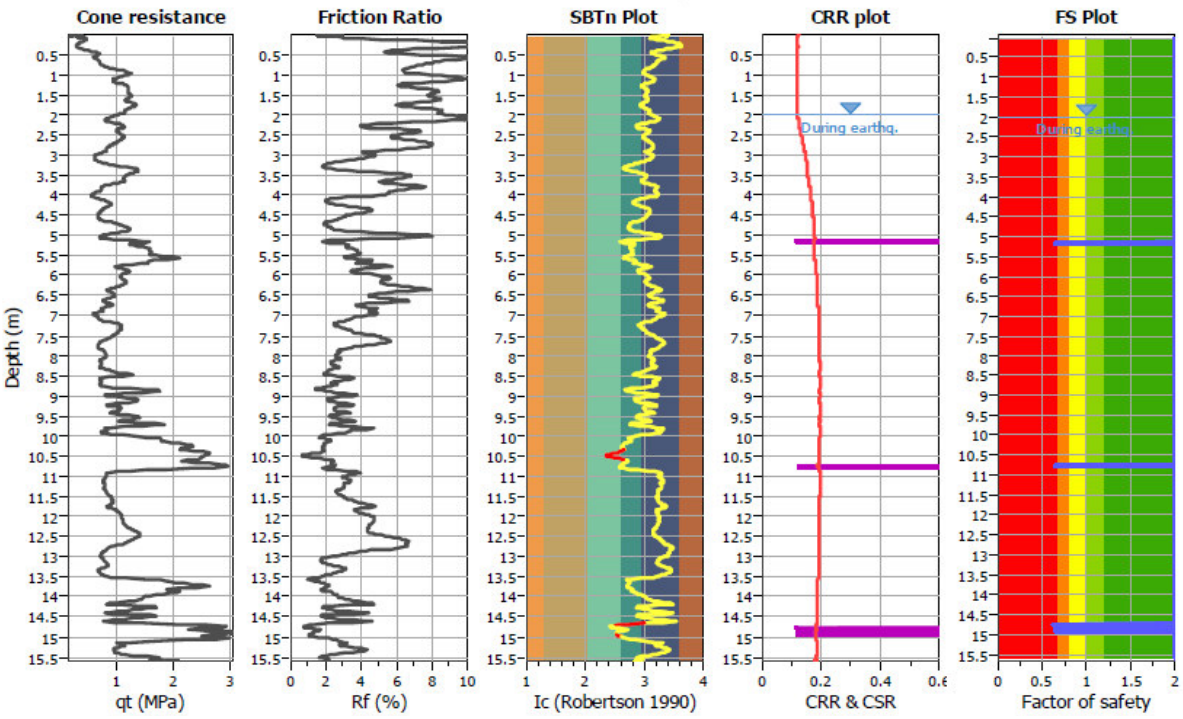
CPTu-3


Cone resistance
Friction Ratio
SBTn Plot
CRR plot
FS Plot
Depth (m)
During earthq.
qt (MPa)
Rf (%)
Ic (Robertson 1990)
CRR & CSR
Factor of safety

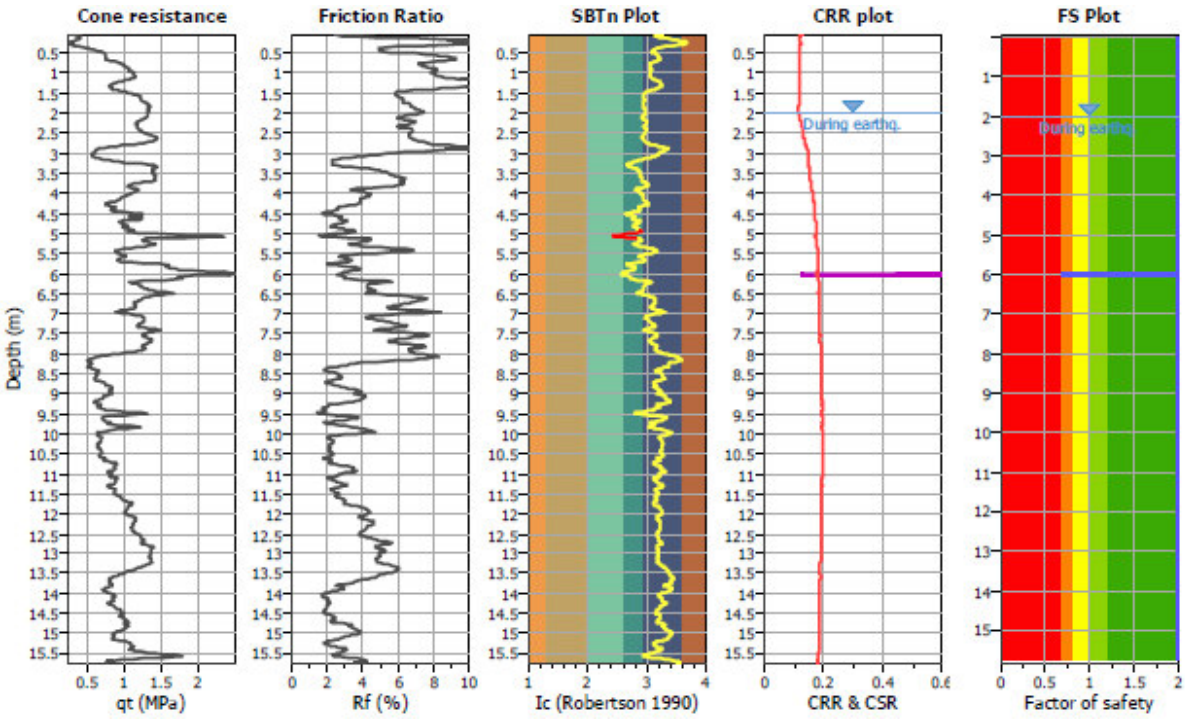
CPTu-4


Cone resistance
Friction Ratio
SBTn Plot
CRR plot
FS Plot
Depth (m)
During earthq.
qt (MPa)
Rf (%)
Ic (Robertson 1990)
CRR & CSR
Factor of safety

CPTu-5


Cone resistance
Friction Ratio
SBTn Plot
CRR plot
FS Plot
Depth (m)
During earthq.
qt (MPa)
Rf (%)
Ic (Robertson 1990)
CRR & CSR
Factor of safety

CPTu-6


Cone resistance
Friction Ratio
SBTn Plot
CRR plot
FS Plot
Depth (m)
During earthq.
qt (MPa)
Rf (%)
Ic (Robertson 1990)
CRR & CSR
Factor of safety

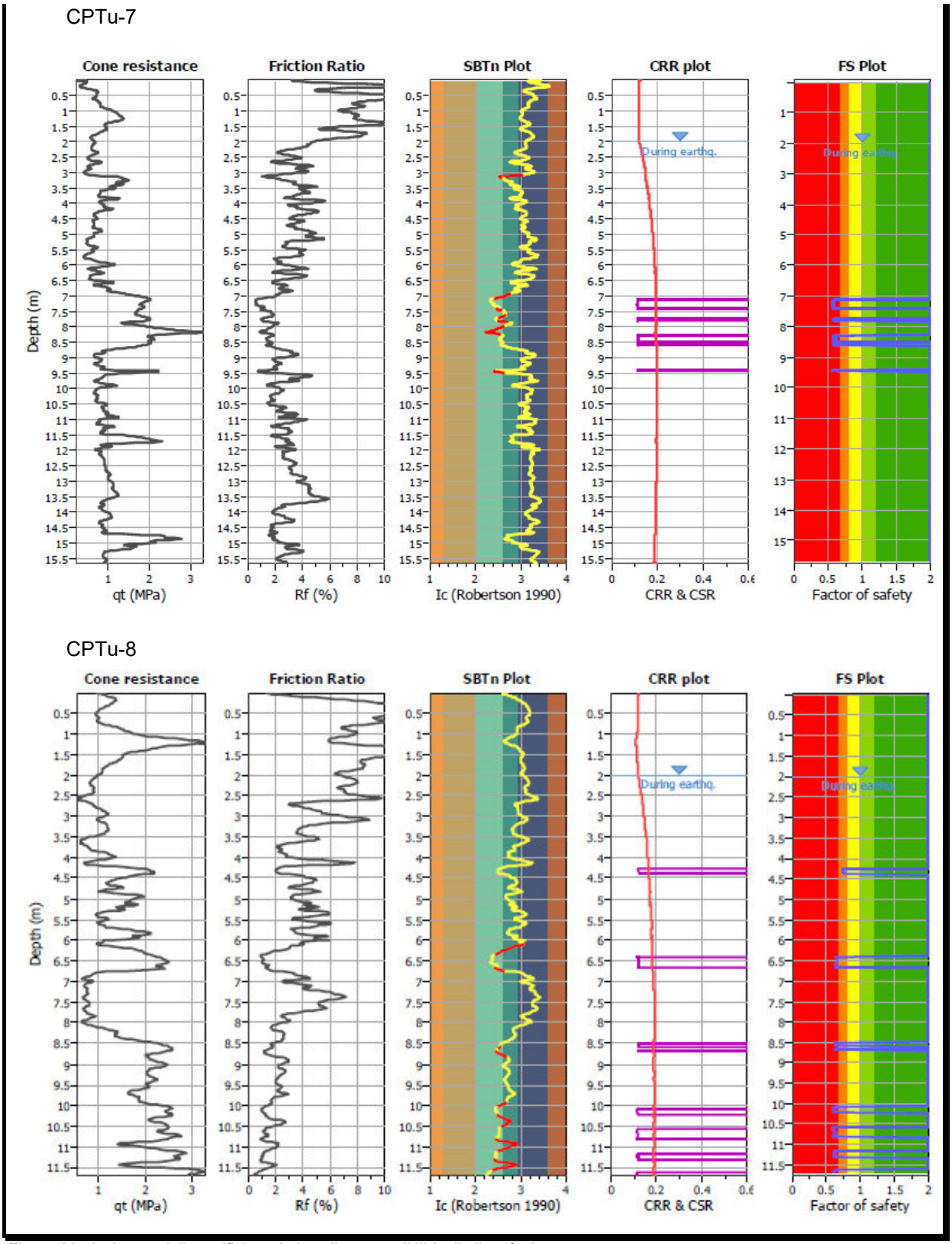


Figura 20: risultanza delle verifiche relative alla suscettibilità alla liquefazione.

Risulta, quindi, una pericolosità ed una propensione alla liquefazione piuttosto media per quanto riguarda l'area di sedime del futuro campo agrivoltaico; da sottolineare la diversità di potenziale di liquefazione fra le diverse zone e i differenti cedimenti strutturali.

Pertanto, dati i valori certamente cautelativi della Mw (valore massimo attesa per la zona sismogenetica 912) e dell'a_{gmax}, ottenuto dalla RSL, l'area di studio risulta suscettibile alla liquefazione per l'area dell'agrivoltaico. Per queste aree si ritiene l'adozione di fondazioni superficiali a platea a garantire la sicurezza in caso di sisma per le opere connesse.

10.6 INDICE DEL POTENZIALE DI LIQUEFAZIONE E CEDIMENTI ATTESI

Per poter procedere alla rappresentazione del rischio di liquefazione occorre riferirsi a valori numerici associati ad ogni verticale di prova. Un indice sintetico, rappresentativo del rischio di liquefazione, applicabile a tutti i metodi che prevedono il calcolo del profilo del fattore di sicurezza, è l'indice del potenziale di liquefazione IP_L, introdotto da Iwasaki et al. (1978):

$$P_L = \int_0^{z_{crit}} F(z) \cdot w(z) \cdot dz$$

in cui F(z) è una funzione che per F.L. > 1 assume valore zero e per F.L. < 1 ne è il complemento ad 1, e $w(z) = 10 - 10 \cdot (z/z_{crit})$ è una funzione linearmente decrescente della profondità, z_{crit} è la profondità oltre la quale sono da escludersi fenomeni di liquefazione, il cui valore è per la maggior parte degli Autori = 20 m.

Valore di I_L	Rischio di liquefazione
$IP_L = 0$	Molto basso
$0 < IP_L \leq 2$	Basso
$2 < IP_L \leq 5$	Moderato
$5 < IP_L \leq 15$	Alto
$15 < IP_L$	Molto alto

Tabella 9: Indice di liquefazione e livello associato di rischio.

I risultati sul valore dell'indice del potenziale di liquefazione, sono stati calcolati con il metodo di Idriss & Boulanger (2014), mentre per la discretizzazione del potenziale di liquefazione, in base ai colloqui intercorsi, è stata assunta secondo le classi di pericolosità di Sonmerz (2003) e Riga (2007), già ripresa nella DGR 630/2019 per quanto riguarda la pianificazione territoriale; inoltre le indagini, elaborate con il software Cliq della Geologismiki in collaborazione con il prof. P.K. Robertson, sono state valutate con l'esclusione delle fasce di transizione; in questo caso sono stati esclusi dal calcolo del potenziale di liquefazione tutte le fasce tessiturali di transizione (es limi sabbiosi) con I_c compreso

fra 1,7 e 3,0 e che nel contempo rispettino il criterio degli strati sottili così come indicato dallo stesso Robertson. Il software elimina i dati quando il cono (la punta della prova penetrometrica elettrica) è in transizione da argilla a sabbia o viceversa. Per fare ciò il software richiede un intervallo di valori Ic oltre i quali verrà definita la transizione (in genere tra 1,80 <Ic <3,0) ed un tasso di variazione di Ic. Le transizioni si verificano in genere quando il tasso di variazione di Ic è rapido.

In questo caso il potenziale di liquefazione è elevato in quanto non siamo più in presenza di uno strato liquefacibile, intercalato da lenti di materiali fini che ne riducono il potenziale; di seguito le risultanze:

RISULTANZE VERIFICA DELL'INDICE DEL POTENZIALE DI LIQUEFAZIONE

Cptu-1:	IP_L = 0,24	Rischio di Liquefazione BASSO
Cptu-2:	IP_L = 0,47	Rischio di Liquefazione BASSO
Cptu-3:	IP_L = 0,1	Rischio di Liquefazione BASSO
Cptu-4:	IP_L = 0,04	Rischio di Liquefazione MOLTO BASSO
Cptu-5:	IP_L = 0,22	Rischio di Liquefazione BASSO
Cptu-6:	IP_L = 0,12	Rischio di Liquefazione BASSO
Cptu-7:	IP_L = 1,76	Rischio di Liquefazione BASSO
Cptu-8:	IP_L = 2,37	Rischio di Liquefazione MODERATO

RISULTANZE VERIFICA DEI CEDIMENTI POST SISMICI ATTESI

Cptu-1:	cedimento	0,41 cm
Cptu-2:	cedimento	1,02 cm
Cptu-3:	cedimento	0,39 cm
Cptu-4:	cedimento	0,07 cm
Cptu-5:	cedimento	0,66 cm
Cptu-6:	cedimento	0,22 cm
Cptu-7:	cedimento	2,91 cm
Cptu-8:	cedimento	4,73 cm

In questo caso viene dimostrata un indice del potenziale di Liquefazione BASSO. Di seguito, figura 21, si riportano i grafici comparativi fra la verticale di indagine e con vari autori a confronto.

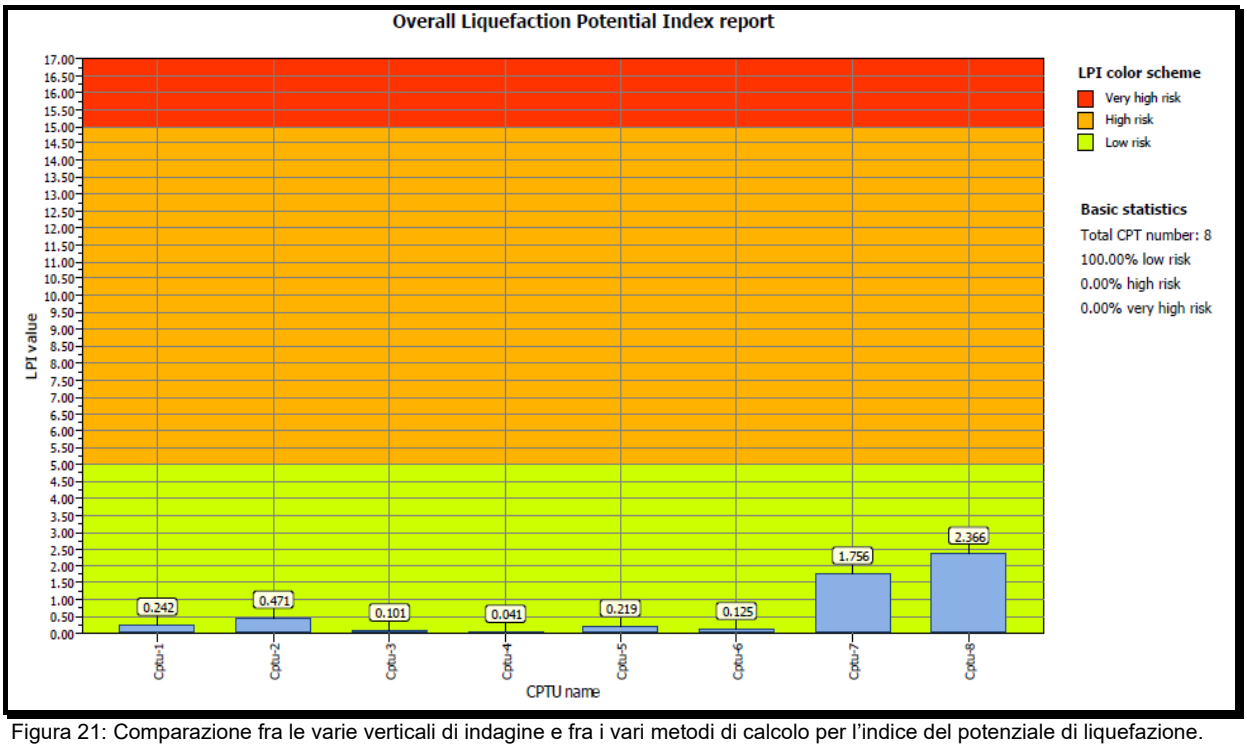


Figura 21: Comparazione fra le varie verticali di indagine e fra i vari metodi di calcolo per l'indice del potenziale di liquefazione.

Un altro parametro è l'indice di Severità di Liquefazione (Liquefaction Severity Number LSN) sulla base delle fasce di severità proposte da Tonkin e Taylor

0 < LSN < 10	Assenza di liquefazione/ minime espressioni di liquefazione
10 < LSN < 20	Minime espressioni di liquefazione
20 < LSN < 30	Moderate espressioni di liquefazione
30 < LSN < 40	Da moderate a severe espressioni di liquefazione
40 < LSN < 50	Maggiori espressioni di liquefazione
LSN > 50	Danni gravi

Tabella 10: Severità di liquefazione in base al parametro LSN (Tonkin e Taylor, 2013).

Le manifestazioni superficiali sono condizionate dal rapporto tra strati liquefacibili/non e dalla relativa posizione stratigrafica; ovvero viene messo in relazione al possibile danno superficiale atteso in relazione alla posizione dello strato liquefacibile.

I risultati sul valore dell'indice di severità di liquefazione, sono stati calcolati con il metodo di Idriss & Boulanger (2014); di seguito le risultanze:

RISULTANZE VERIFICA DELL'INDICE DI SEVERITÀ DI LIQUEFAZIONE

Cptu-1: LSN =0,905 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-2: LSN =2,118 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-3: LSN =0,27 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-4: LSN =0,088 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-5: LSN =0,588 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-6: LSN =0,362 Danni gravi;
Cptu-7: LSN =3,696 Assenza di liquefazione/minime espressioni di liquefazione;
Cptu-8: LSN =5,898 Assenza di liquefazione/minime espressioni di liquefazione;

Correlando l'indice IPL con l'indice LSN si evince come, per l'area di studio, la suscettibilità alla liquefazione risulti medio bassa. Ciò sottolinea l'estrema eterogeneità dell'area e quindi promuovere una maggiore attenzione ai cedimenti differenziali

Di seguito i grafici comparativi per la verticale di indagine e per le varie metodologie a confronto (figura 22).

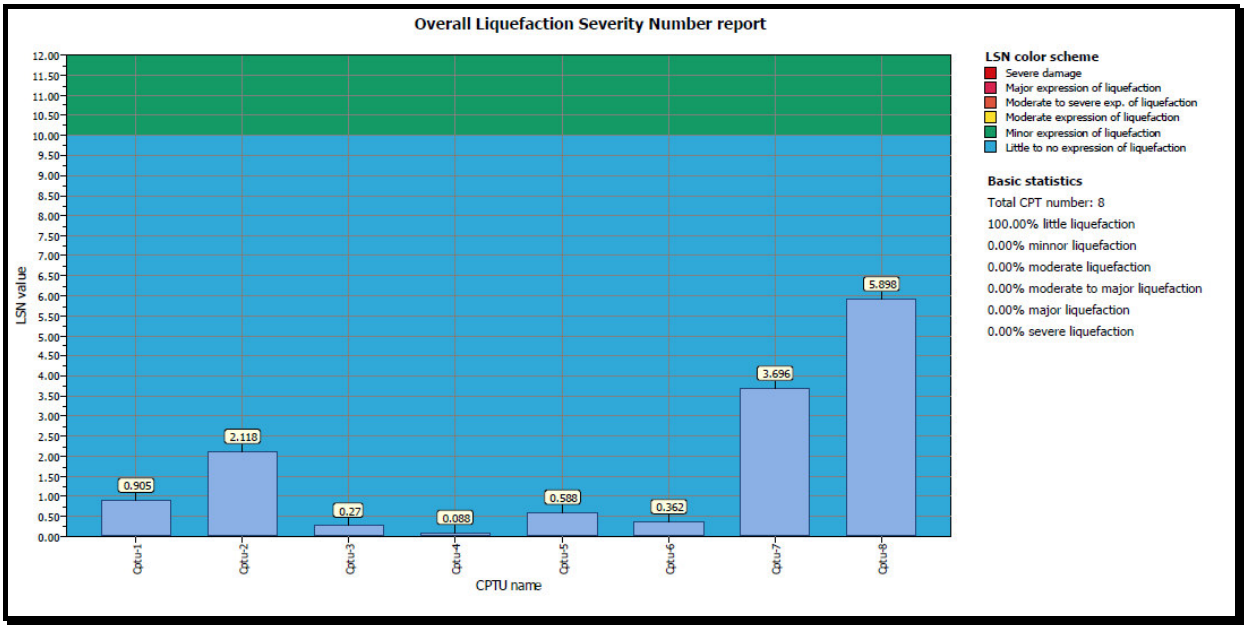


Figura 22: Comparazione fra le varie verticali di indagine e fra i vari metodi di calcolo per l'indice del potenziale di liquefazione.

Da tutte le verifiche effettuate si pone l'ovvio accento della MEDIO/BASSA sensibilità generale dell'area di sedime alla liquefazione. Appare comunque corretta l'adozione di fondazioni a platea.

11. Considerazioni conclusive

In base a quanto sinora riportato, è possibile concludere che l'area in esame è situata in una zona avente elementi di pericolosità geologica e di conseguenza, nel complesso, vulnerabile.

Come precedentemente ricordato, impiegando prove geofisiche, sondaggi penetrometrici meccanici effettuati nell'area di studio, si è rilevato la presenza di materiali limo argillosi e argillo limosi prevalenti nei primi metri di successione seguiti da livelli con alternanze coesivi granulari fini e da livelli metrici e lenticolari di materiali granulari incoerenti (sabbie) poggianti su argille mediamente consistenti.

Tali livelli, di natura alluvionale/tracimazione, sono poggianti su substrato (Pliocenico), rinvenibile a profondità elevata data la natura tettonica del cambio fra l'area pedecollinare e la Pianura.

Per quanto riguarda la vulnerabilità degli acquiferi definita, dalle carte tematiche consultate e citate, risulta una vulnerabilità medio-bassa per la presenza di terreni coesivi impermeabili superficiali e di limi sabbiosi – sabbie limose (alternati ad argille limose) che aumentano la vulnerabilità.

Per quanto riguarda le verifiche alla propensione alla liquefazione dei terreni presenti, ci si rifà a quanto già affermato nei capitoli precedenti, ovvero l'area risulta generalmente con un potenziale di liquefazione medio/basso.

Infatti, è stata effettuata una valutazione sulla probabilità di liquefazione dei terreni con il metodo di Idriss & Boulanger (2014) per la verticale di indagine effettuate; è risultata una propensione alla liquefazione BASSA.

Oltre all'indice del potenziale di liquefazione IPL, è stato valutato anche l'indice di severità a liquefazione LSN che fornisce importanti informazioni sulla reale espressione di fenomeni di liquefazione in relazione alle opere in superficie; in quest'ultimo caso è risultato una severità generale media.

Inoltre la caratterizzazione sismica dei luoghi (in accordo con le prove penetrometriche e con le analisi svolte nelle schede di microzonazione) ha definito l'appartenenza dei suoli alla categoria **C** con $Vs_{eq} \approx 188{,}0$ m/s con frequenze di sito pari a 0,84±0,1 Hz, indice di importanti contrasti di impedenza che possono dare origine a significative variazioni del moto dell'onda sismica. Va posta pertanto attenzione evitando effetti di risonanza fra le opere in progetto ed i terreni di fondazione.

Data la presenza di terreni superficiali agricoli, si consiglia l'appoggio delle fondazioni almeno al di sotto del primo strato (circa -0,8÷-1,0 m da p.c), al fine di evitare di appoggiare le strutture di

fondazione al di sopra di terreni eccessivamente cedevoli; inoltre, dai dati ottenuti dalle CPTu, si è potuto notare come le temperature stagionali hanno avuto influenza sui terreni coesivi fino a circa -3,0 m dal piano campagna. Questo ad indicare che, in ragione della stagionalità, saranno presenti fenomeni di variazione volumetrica della frazione coesiva con abbassamenti e rigonfiamenti dell'intera successione stratigrafica fino a – 3,0 m.

Grande attenzione si dovrà prestare agli eventuali cedimenti differenziali in relazione alle differenze riscontrate fra le varie verticali di indagine.

Sulla scorta di quanto rilevato nell'ambito del presente studio, osservando le prescrizioni precedentemente esposte, non si ravvedono elementi sfavorevoli dal punto di vista idrogeologico e geologico per l'area oggetto di studio e si ritiene fattibile la realizzazione delle opere in progetto.

Dott.ssa geol. Giulia Gardosi dott. geol. Maurizio Zamboni

Firmato digitalmente da

Giulia Gardosi

CN = Giulia Gardosi
O = Ordine dei Geologi dell'Emilia Romagna
C = IT

Firmato digitalmente da

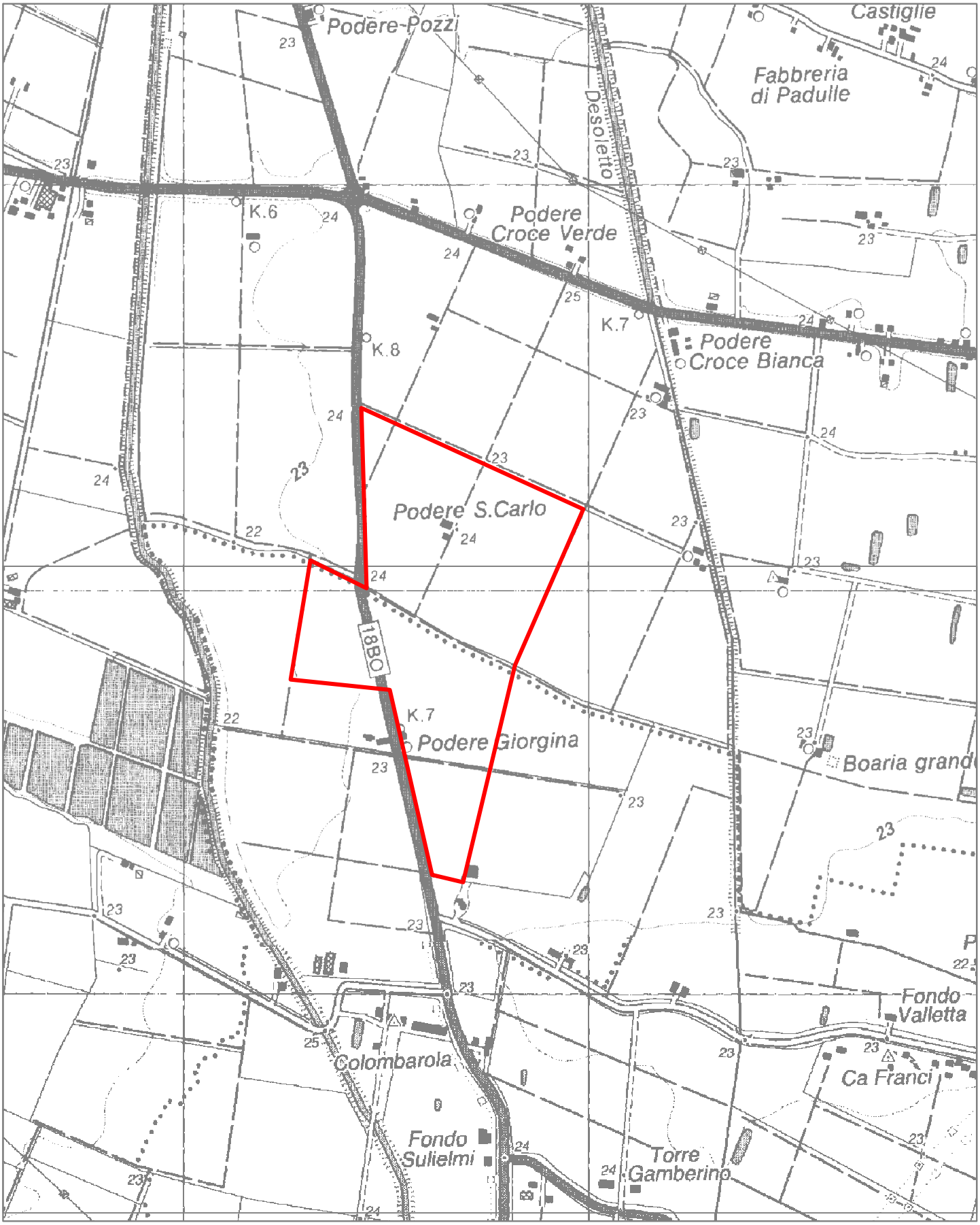
Maurizio Zamboni

CN = Zamboni Maurizio
O = Ordine dei Geologi dell'Emilia Romagna
C = IT

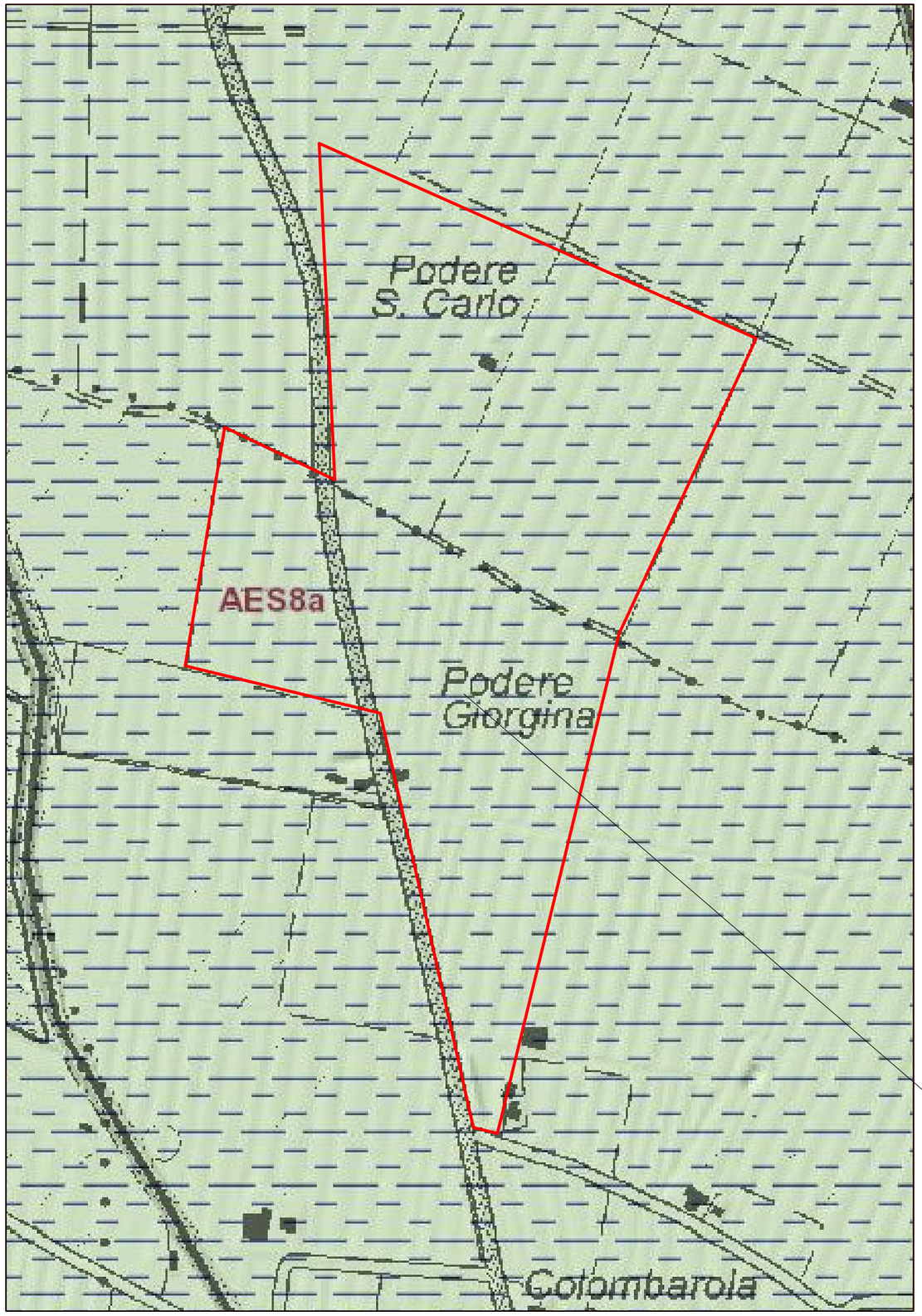
Tavole

- corografia	1 : 25.000-
carta geologica	1 : 10.000-
- Tav-1 - inquadramento territoriale	1 : 10.000-
- Tav-2 – ubicazione indagini	1 : 10.000-
- Tav-3a– stratigrafia interpretativa	1 : 200-
- Tav-3b– stratigrafia interpretativa	1 : 200-
- Tav-3c– stratigrafia interpretativa	1 : 200-

Corografia



Stralcio dalla Tavola. N° 202SE –SAN GIOVANNI IN PERSICETO– e N°220NE –BOLOGNA NORD/OVEST– con indicata l'area di intervento – scala 1:25.000 –



PADULLE **SEZIONE N° 202160 -scala 1:10.000-**

CALDERARA DI RENO **SEZIONE N° 22040 -scala 1:10.000-**

SUCCESSIONE NEOGENICO-QUATERNARIA DEL MARGINE APPENNINICO PADANO

AES8 **Subsintema di Ravenna**

AES8a **Unità di Modena**

SEGNI CONVENZIONALI

60 Strati diritti.

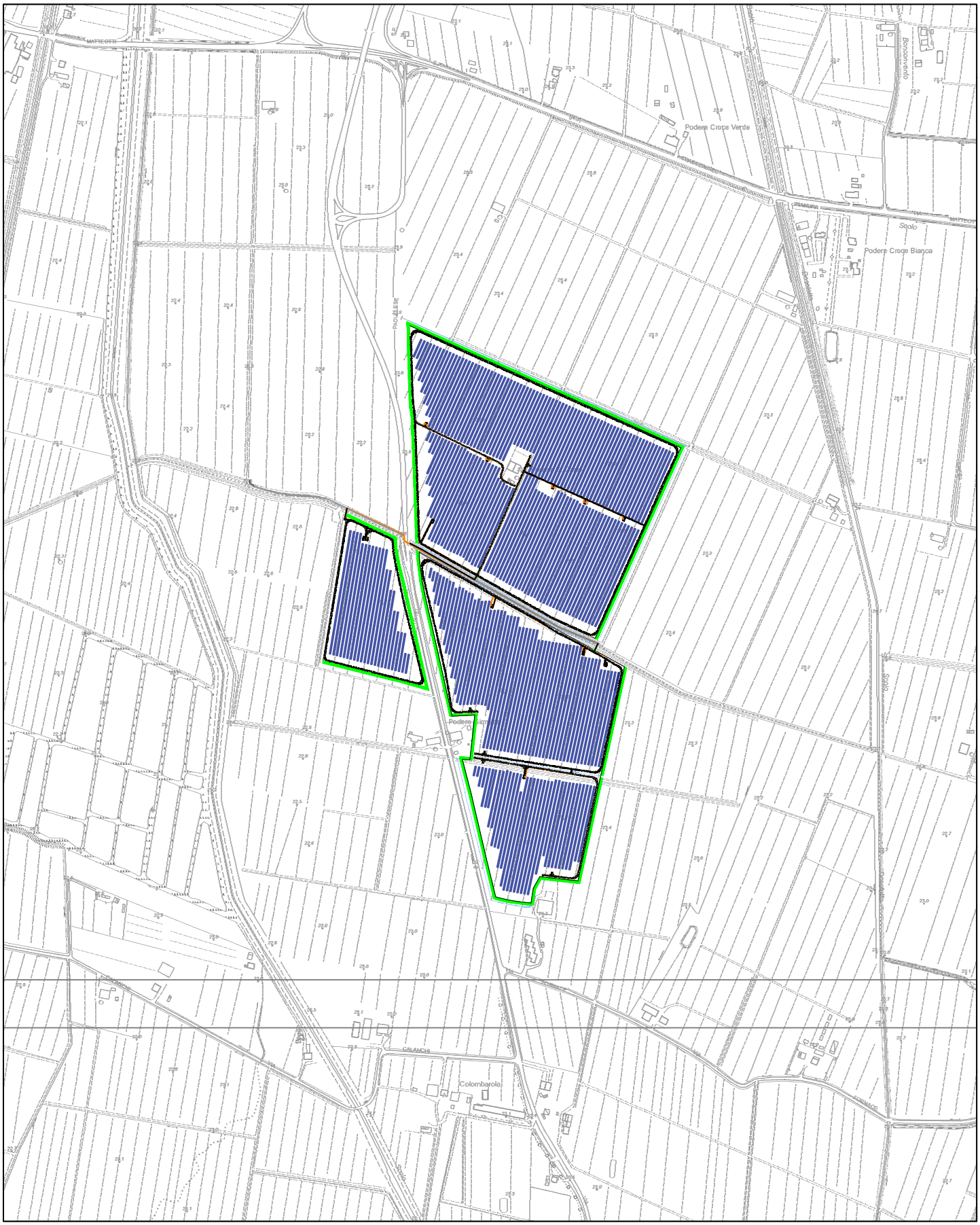
Limite stratigrafico.

Faglia certa

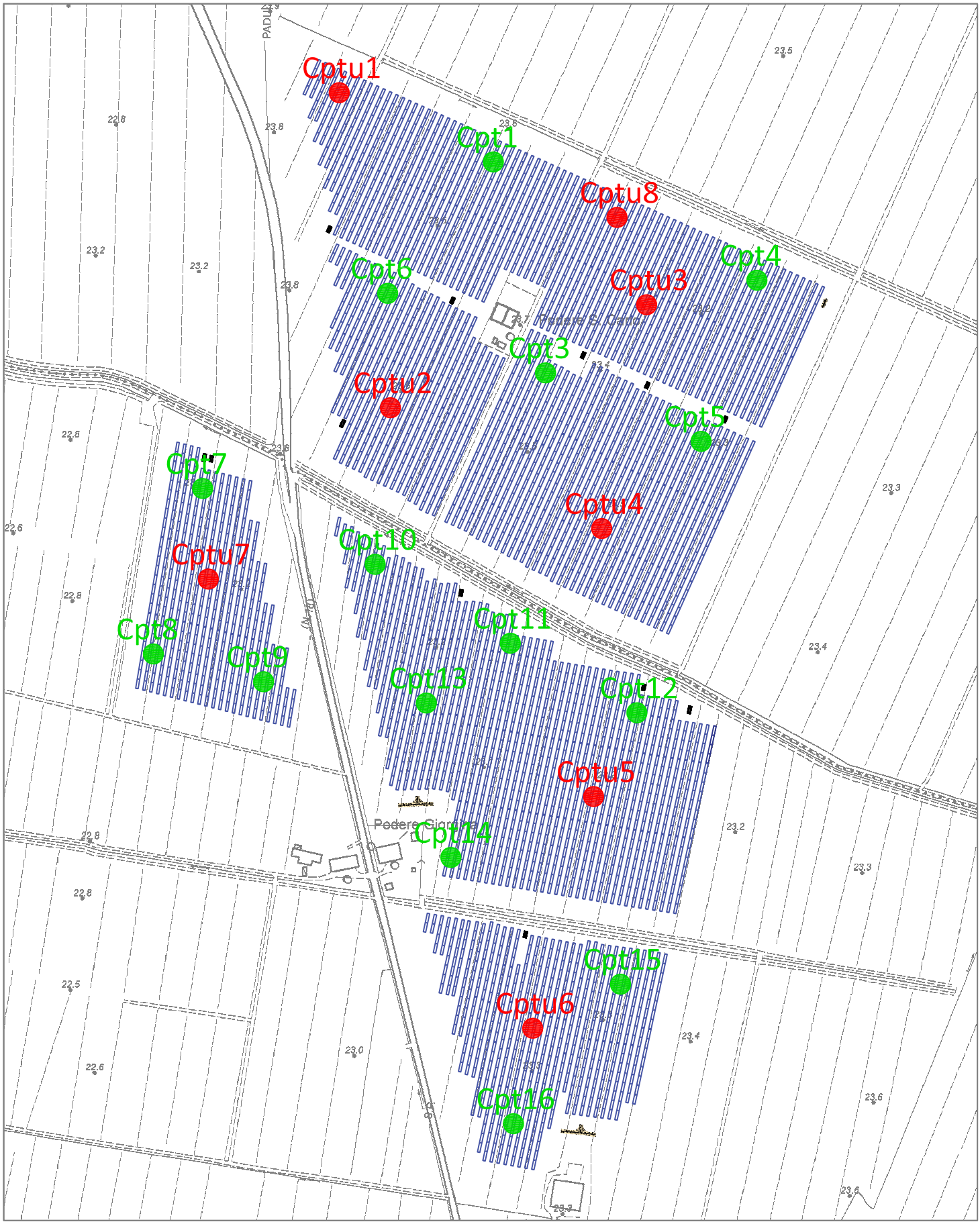
Faglia dedotta

Sovrascorrimento certo

area di studio



Stralcio dagli Elementi C.T.R. N° 202163 –SALA BOLOGNESE– e N° 220044 –COLOMBARA–
con indicata l'area di intervento – scala 1:10.000 –



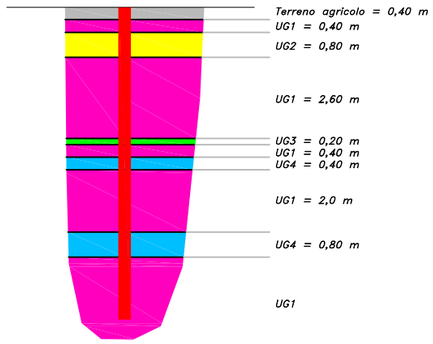
Ubicazione sondaggi penetrometrici sulla planimetria di progetto – scala 1:10.000

Cpt1 *sondaggio penetrometrico statico meccanico*

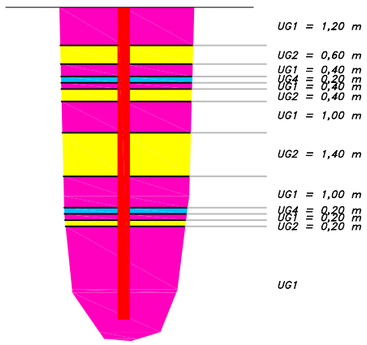
CPTu1 *sondaggio penetrometrico statico con piezocono*

Tavola 3a

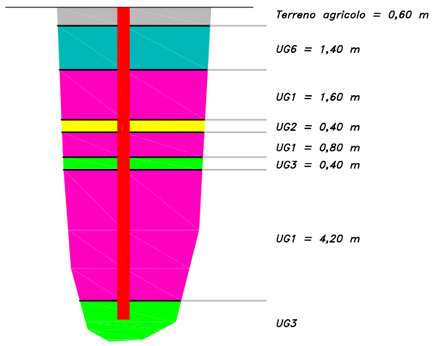
CPT-1



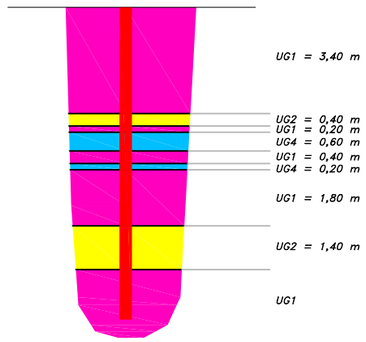
CPT-3



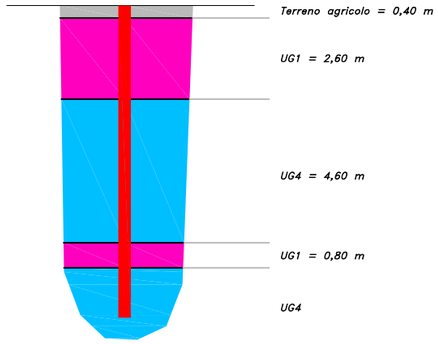
CPT-4



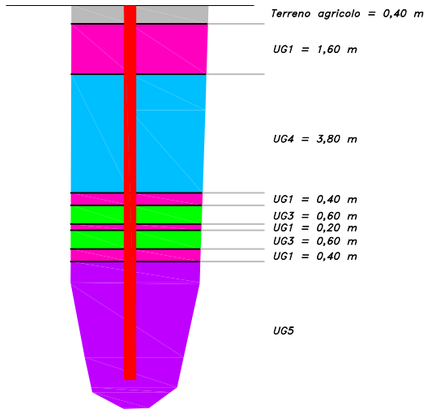
CPT-5



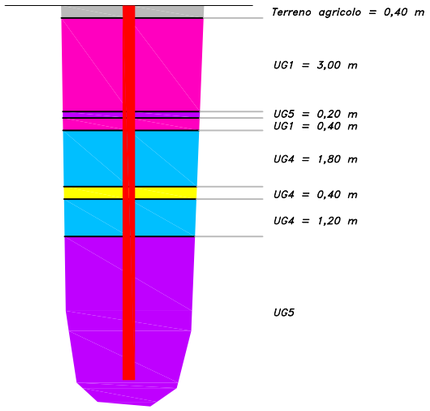
CPT-6



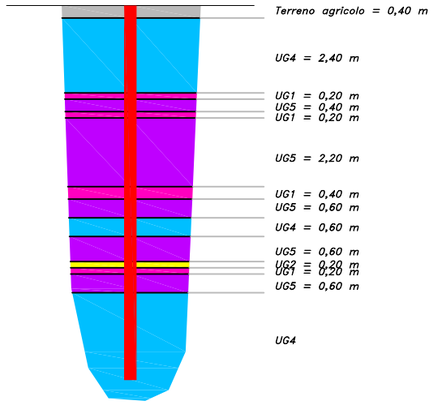
CPT-7



CPT-8



CPT-9



LEGENDA

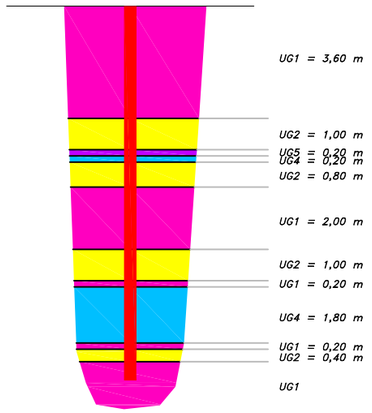
- terreno agricolo
- UG1 – argille limose, moderatamente consistenti
- UG2 – limi argillosi, inorganici, a tratti debolmente sabbiosi moderatamente consistenti
- UG3 – sabbie limose, poco addensate
- UG4 – argille, a tratti organiche, poco consistenti
- UG5 – sabbie medio fini, moderatamente addensate
- UG6 – sabbie limose/limi sabbiosi, moderatamente consistenti

Sezione stratigrafica interpretativa – scala 1:200

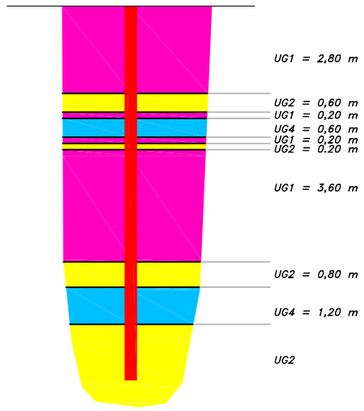
CPT-1 *prova penetrometrica statica meccanica*

CPTu-1 *prova penetrometrica elettrica con piezocono*

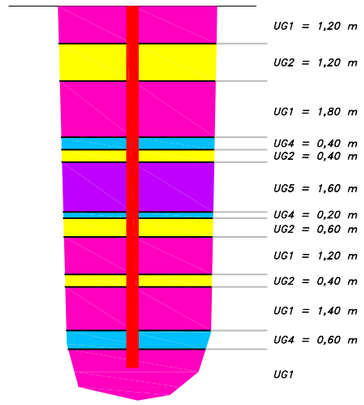
CPT-10



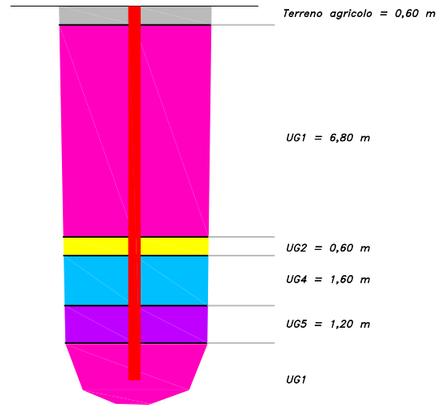
CPT-11



CPT-12



CPT-13



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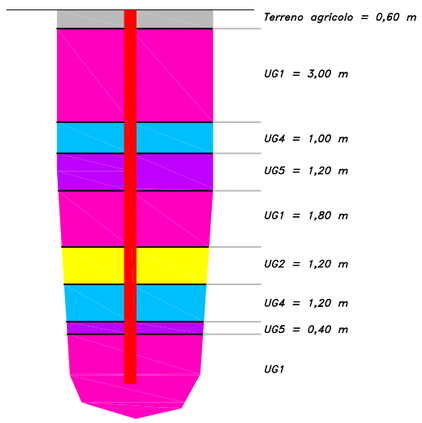
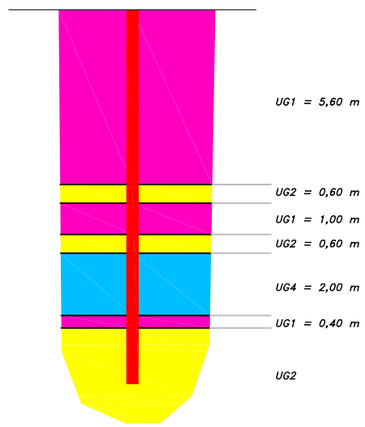
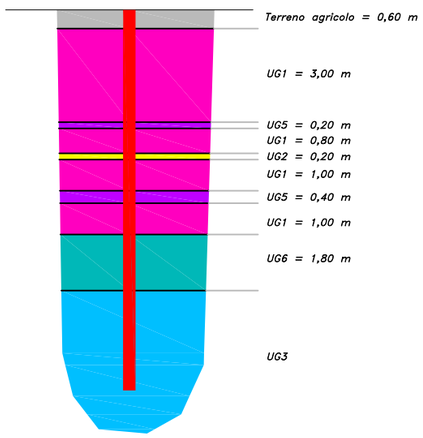


CPT-15



CPT-16



LEGENDA

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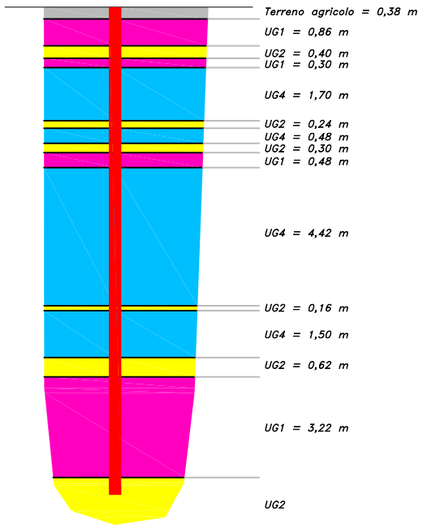
Sezione stratigrafica interpretativa – scala 1:200

CPT-1 *prova penetrometrica statica meccanica*

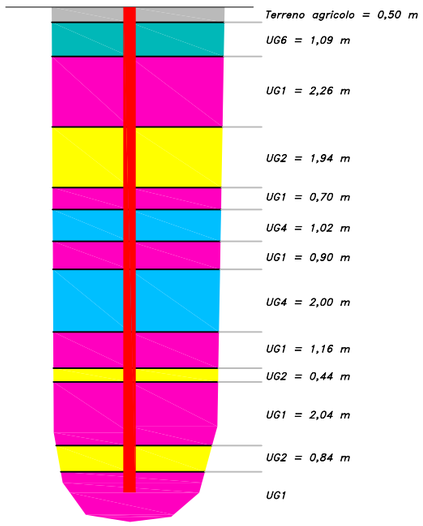
CPTu-1 *prova penetrometrica elettrica con piezocono*

Tavola 3c

CPTu-1



CPTu-2



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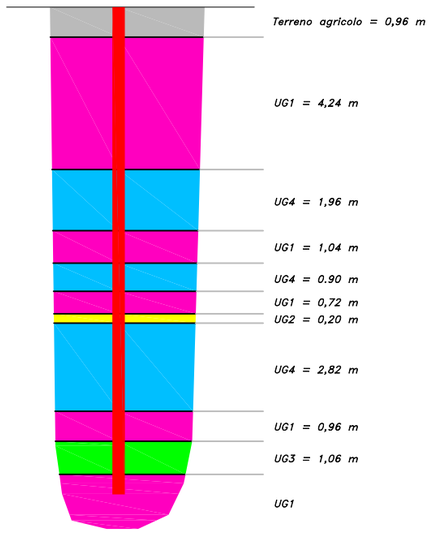

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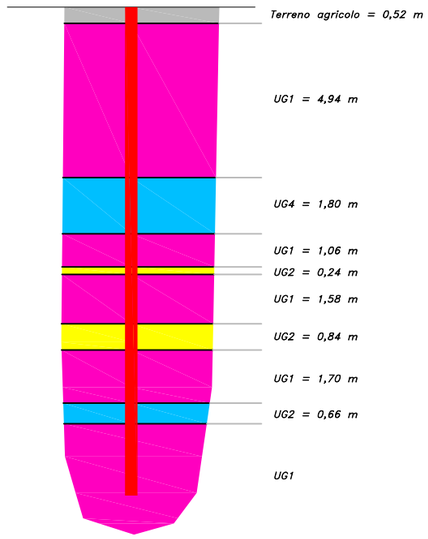

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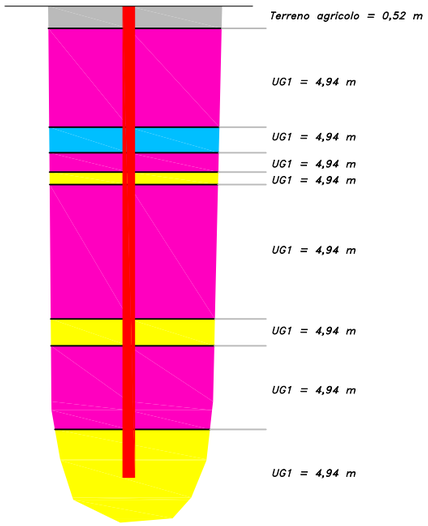
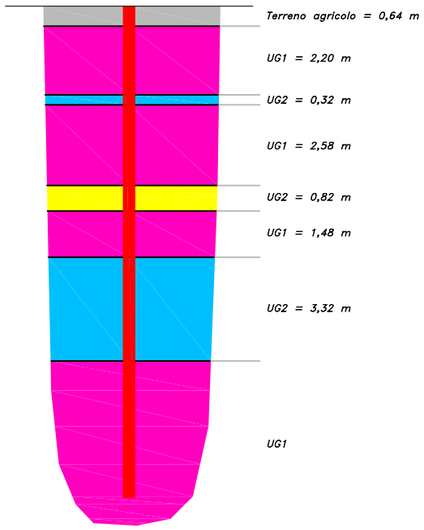
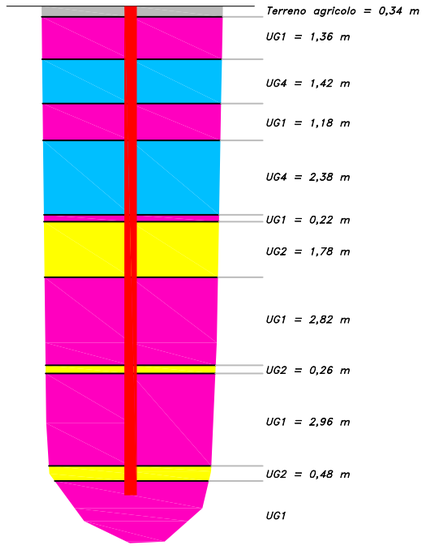


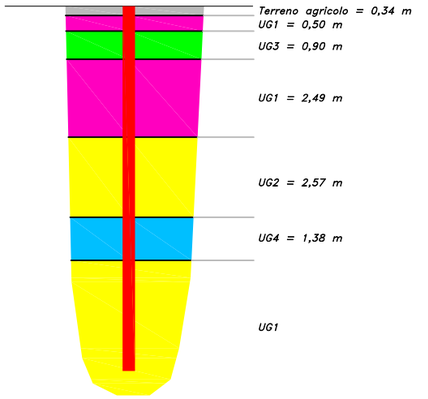
CPTu-6



CPTu-7



CPTu-8



LEGENDA

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- UG3 – sabbie limose, poco addensate
- UG4 – argille, a tratti organiche, poco consistenti
- UG5 – sabbie medio fini, moderatamente addensate
- UG6 – sabbie limose/limi sabbiosi, moderatamente consistenti

Sezione stratigrafica interpretativa – scala 1:200

CPT-1 *prova penetrometrica statica meccanica*

CPTu-1 *prova penetrometrica elettrica con piezocono*

Elenco Allegati

Allegato 1: prove penetrometriche statiche meccaniche

Allegato 2: prove penetrometriche elettriche con piezocono

Allegato 3: indagini geofisiche

Allegato 4: report liquefazione

ALLEGATO I

- PROVE PENETROMETRICHE STATICHE MECCANICHE-

DIAGRAMMI DI RESISTENZA

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TABELLE VALORI DI RESISTENZA

--

VALUTAZIONI LITOLOGICHE

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PARAMETRI GEOTECNICI

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

LEGENDA VALORI DI RESISTENZA
FATTORI DI CONVERSIONE

Strumento utilizzato:
TG63-200 - Pagani - Piacenza

Caratteristiche:

- punta conica meccanica Ø 35.7 mm, area punta Ap = 10 cm²

- punta conica meccanica angolo di apertura: α = 60°

- manicotto laterale di attrito tipo 'Begemann' (Ø = 35.7 mm - h = 133 mm - Am = 150 cm²)

- velocità di avanzamento costante V = 2 cm/sec (± 0,5 cm / sec)

- spinta max nominale dello strumento Smax variabile a seconda del tipo

- costante di trasformazione CT = SPINTA (Kg) / LETTURA DI CAMPAGNA
  (dato tecnico legato alle caratteristiche del penetrometro utilizzato, fornito dal costruttore)

fase 1 - resistenza alla punta: qc (kg/cm²) = (L1) x CT /10

fase 2 - resistenza laterale locale: fs (kg/cm²) = [(L2) - (L1)] x CT / 150

fase 3 - resistenza totale : Rt (kg/cm²) = (Lt) x CT

- Prima lettura = lettura di campagna durante l' infissione della sola punta (fase 1)
- Seconda lettura = lettura di campagna relativa all'infissione di punta e manicotto (fase 2)
- Terza lettura = lettura di campagna relativa all'infissione delle aste esterne (fase 3)

N.B. : la spinta S (Kg) , corrispondente a ciascuna fase , si ottiene moltiplicando la corrispondente lettura di campagna L per la costante di trasformazione CT .

N.B. : causa la distanza intercorrente (20 cm circa) fra il centro del manicotto laterale e la punta conica del penetrometro , la resistenza laterale locale fs viene computata 20 cm sopra la punta .

CONVERSIONI
1 kN (kiloNewton) = 1000 N $\approx$ 100 kg = 0,1 t
1 MN (megaNewton) = 1.000 kN = 1.000.000 N $\approx$ 100 t
1 kPa (kiloPascal) = 1 kN/m² = 0,001 MN/m² = 0,001 MPa $\approx$ 0,1 t/m² = 0,01 kg/cm²
1 MPa (megaPascal) = 1 MN/m² = 1.000 kN/m² = 1000 kPa $\approx$ 100 t/m² = 10 kg/cm²
1 kg/cm² = 10 t/m² $\approx$ 100 kN/m² = 100 kPa = 0,1 MN/m² = 0,1 MPa
1 t = 1000 kg $\approx$ 10 kN

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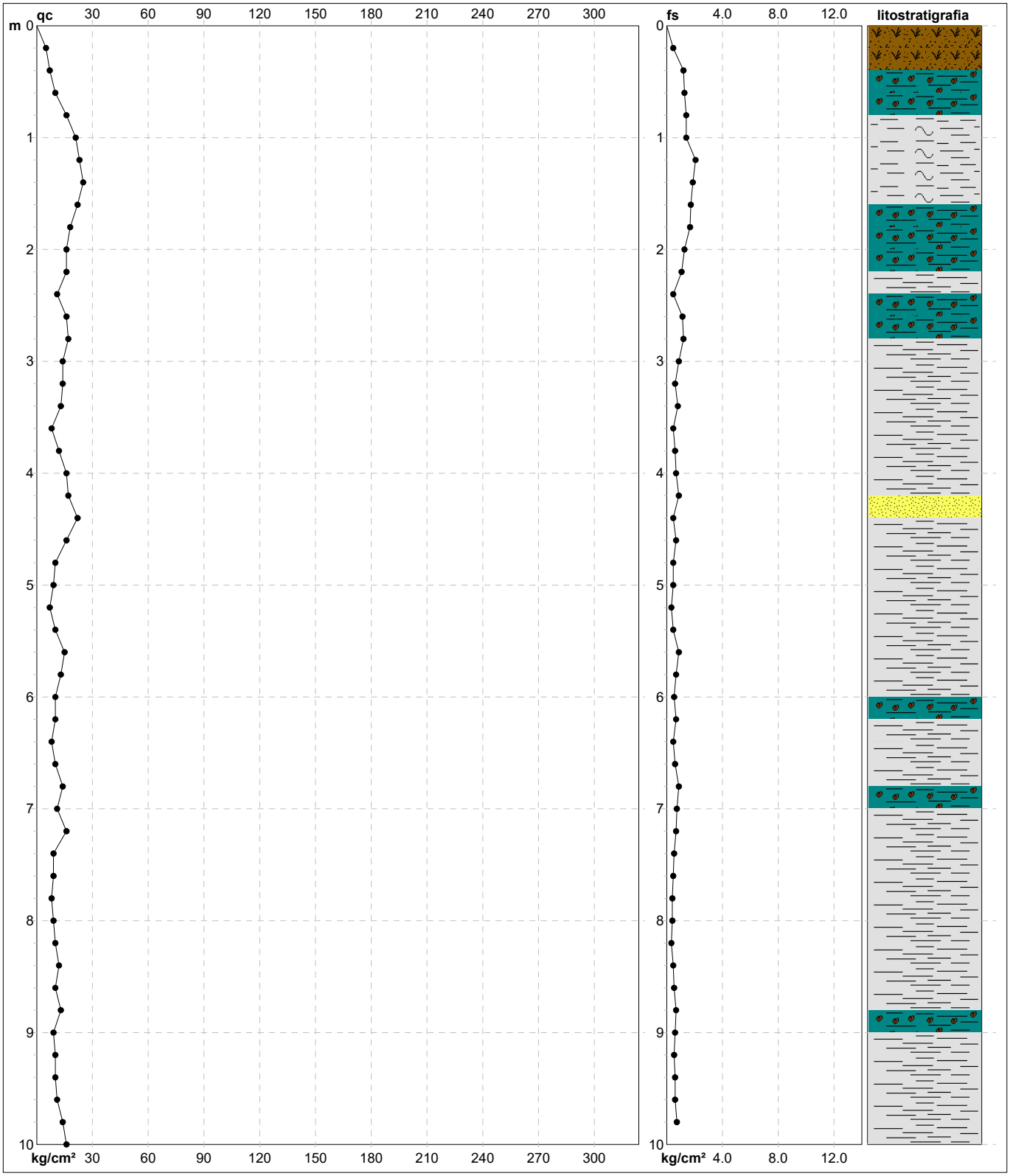
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	1
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.: kg/cm²	Data esec.: 25/11/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala: 1:50	
Località:	Sala Bolognese (BO)	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	1
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 25/11/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	5.0	11.0		5.00	0.47	11	9.4
0.40	7.0	14.0		7.00	1.20	6	17.1
0.60	10.0	28.0		10.00	1.27	8	12.7
0.80	16.0	35.0		16.00	1.40	11	8.8
1.00	21.0	42.0		21.00	1.40	15	6.7
1.20	23.0	44.0		23.00	2.07	11	9.0
1.40	25.0	56.0		25.00	1.87	13	7.5
1.60	22.0	50.0		22.00	1.73	13	7.9
1.80	18.0	44.0		18.00	1.67	11	9.3
2.00	16.0	41.0		16.00	1.27	13	7.9
2.20	16.0	35.0		16.00	1.07	15	6.7
2.40	11.0	27.0		11.00	0.47	23	4.3
2.60	16.0	23.0		16.00	1.13	14	7.1
2.80	17.0	34.0		17.00	1.20	14	7.1
3.00	14.0	32.0		14.00	0.87	16	6.2
3.20	14.0	27.0		14.00	0.60	23	4.3
3.40	13.0	22.0		13.00	0.80	16	6.2
3.60	8.0	20.0		8.00	0.47	17	5.9
3.80	12.0	19.0		12.00	0.60	20	5.0
4.00	16.0	25.0		16.00	0.67	24	4.2
4.20	17.0	27.0		17.00	0.87	20	5.1
4.40	22.0	35.0		22.00	0.47	47	2.1
4.60	16.0	23.0		16.00	0.67	24	4.2
4.80	10.0	20.0		10.00	0.47	21	4.7
5.00	9.0	16.0		9.00	0.47	19	5.2
5.20	7.0	14.0		7.00	0.33	21	4.7
5.40	10.0	15.0		10.00	0.47	21	4.7
5.60	15.0	22.0		15.00	0.87	17	5.8
5.80	13.0	26.0		13.00	0.67	19	5.2
6.00	10.0	20.0		10.00	0.53	19	5.3
6.20	10.0	18.0		10.00	0.67	15	6.7
6.40	8.0	18.0		8.00	0.47	17	5.9
6.60	10.0	17.0		10.00	0.60	17	6.0
6.80	14.0	23.0		14.00	0.87	16	6.2
7.00	11.0	24.0		11.00	0.73	15	6.6
7.20	16.0	27.0		16.00	0.67	24	4.2
7.40	9.0	19.0		9.00	0.53	17	5.9
7.60	9.0	17.0		9.00	0.47	19	5.2
7.80	8.0	15.0		8.00	0.40	20	5.0
8.00	9.0	15.0		9.00	0.40	23	4.4
8.20	10.0	16.0		10.00	0.33	30	3.3
8.40	12.0	17.0		12.00	0.47	26	3.9
8.60	10.0	17.0		10.00	0.53	19	5.3
8.80	13.0	21.0		13.00	0.67	19	5.2
9.00	9.0	19.0		9.00	0.60	15	6.7
9.20	10.0	19.0		10.00	0.53	19	5.3
9.40	10.0	18.0		10.00	0.60	17	6.0
9.60	11.0	20.0		11.00	0.60	18	5.5
9.80	14.0	23.0		14.00	0.73	19	5.2
10.00	16.0	27.0		16.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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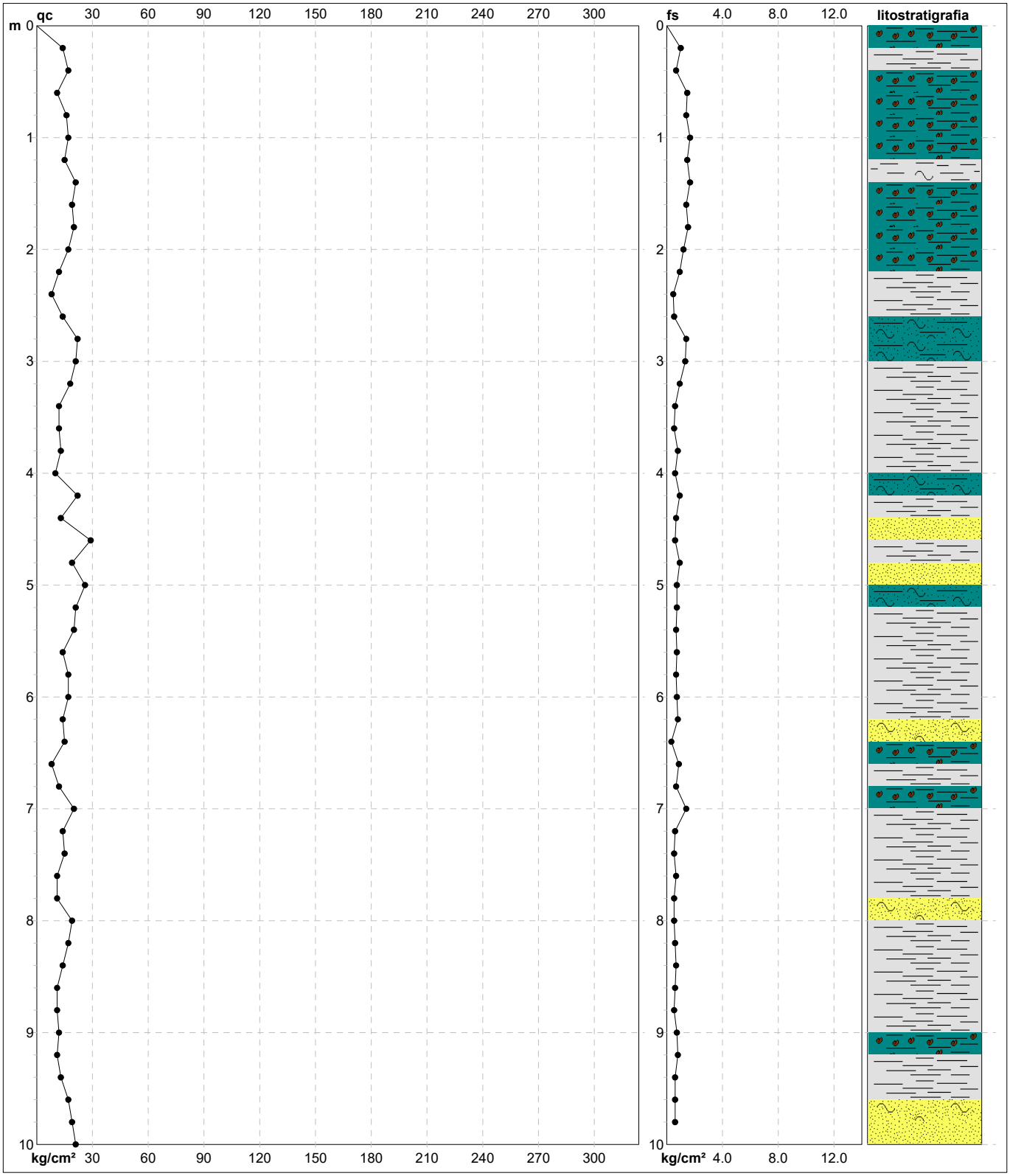
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	3
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.: kg/cm²	Data esec.: 08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala: 1:50	
Località:	Sala Bolognese (BO)	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	3
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	14.0	30.0		14.00	1.00	14	7.1
0.40	17.0	32.0		17.00	0.67	25	3.9
0.60	11.0	21.0		11.00	1.47	7	13.4
0.80	16.0	38.0		16.00	1.40	11	8.8
1.00	17.0	38.0		17.00	1.67	10	9.8
1.20	15.0	40.0		15.00	1.47	10	9.8
1.40	21.0	43.0		21.00	1.67	13	8.0
1.60	19.0	44.0		19.00	1.40	14	7.4
1.80	20.0	41.0		20.00	1.53	13	7.7
2.00	17.0	40.0		17.00	1.20	14	7.1
2.20	12.0	30.0		12.00	0.93	13	7.8
2.40	8.0	22.0		8.00	0.47	17	5.9
2.60	14.0	21.0		14.00	0.53	26	3.8
2.80	22.0	30.0		22.00	1.40	16	6.4
3.00	21.0	42.0		21.00	1.33	16	6.3
3.20	18.0	38.0		18.00	0.93	19	5.2
3.40	12.0	26.0		12.00	0.60	20	5.0
3.60	12.0	21.0		12.00	0.53	23	4.4
3.80	13.0	21.0		13.00	0.80	16	6.2
4.00	10.0	22.0		10.00	0.60	17	6.0
4.20	22.0	31.0		22.00	0.93	24	4.2
4.40	13.0	27.0		13.00	0.67	19	5.2
4.60	29.0	39.0		29.00	0.60	48	2.1
4.80	19.0	28.0		19.00	0.93	20	4.9
5.00	26.0	40.0		26.00	0.73	36	2.8
5.20	21.0	32.0		21.00	0.73	29	3.5
5.40	20.0	31.0		20.00	0.67	30	3.4
5.60	14.0	24.0		14.00	0.73	19	5.2
5.80	17.0	28.0		17.00	0.67	25	3.9
6.00	17.0	27.0		17.00	0.73	23	4.3
6.20	14.0	25.0		14.00	0.80	18	5.7
6.40	15.0	27.0		15.00	0.33	45	2.2
6.60	8.0	13.0		8.00	0.87	9	10.9
6.80	12.0	25.0		12.00	0.67	18	5.6
7.00	20.0	30.0		20.00	1.40	14	7.0
7.20	14.0	35.0		14.00	0.60	23	4.3
7.40	15.0	24.0		15.00	0.53	28	3.5
7.60	11.0	19.0		11.00	0.67	16	6.1
7.80	11.0	21.0		11.00	0.53	21	4.8
8.00	19.0	27.0		19.00	0.53	36	2.8
8.20	17.0	25.0		17.00	0.60	28	3.5
8.40	14.0	23.0		14.00	0.67	21	4.8
8.60	11.0	21.0		11.00	0.60	18	5.5
8.80	11.0	20.0		11.00	0.53	21	4.8
9.00	12.0	20.0		12.00	0.73	16	6.1
9.20	11.0	22.0		11.00	0.80	14	7.3
9.40	13.0	25.0		13.00	0.60	22	4.6
9.60	17.0	26.0		17.00	0.60	28	3.5
9.80	19.0	28.0		19.00	0.60	32	3.2
10.00	21.0	30.0		21.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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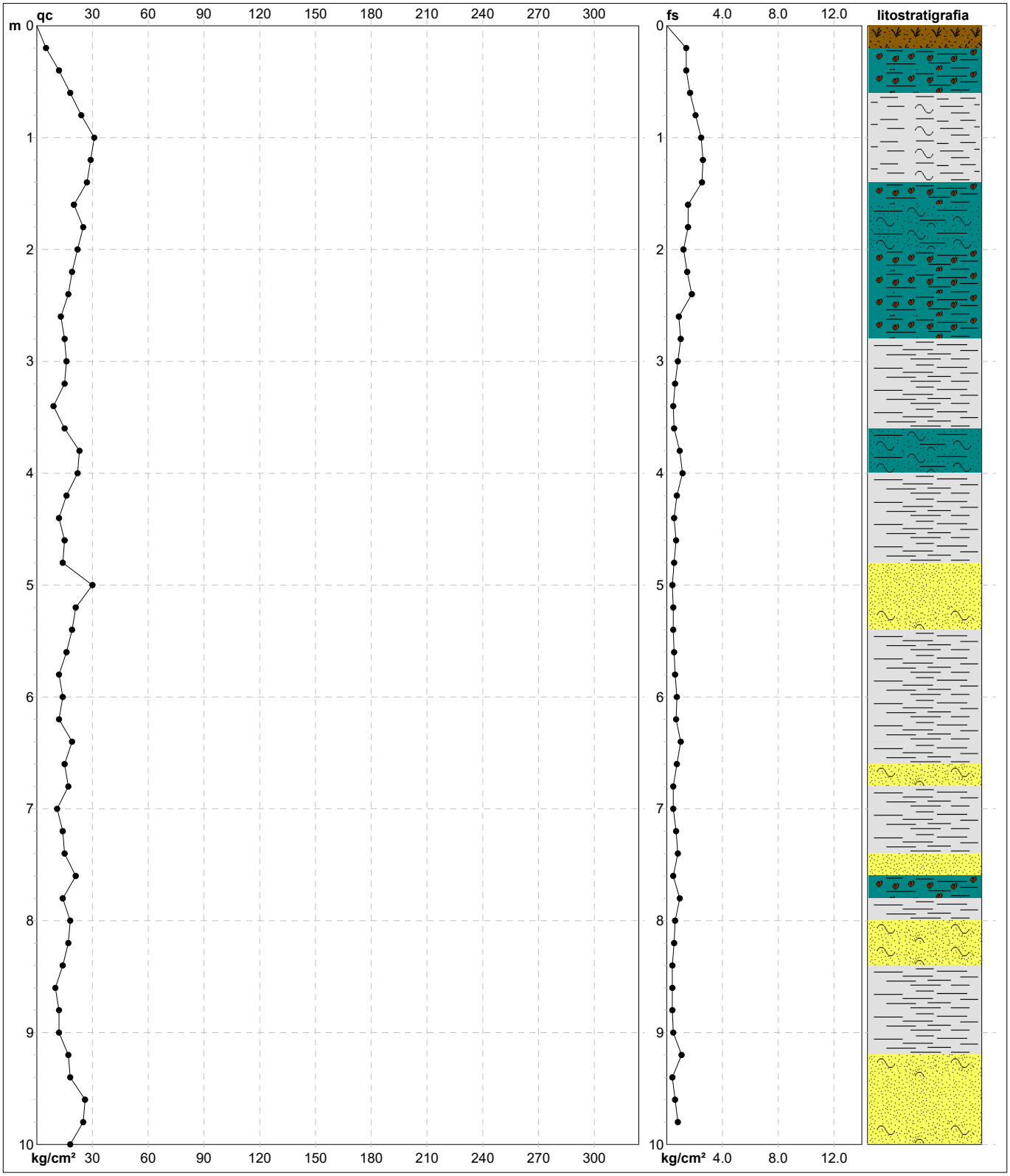
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	4
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.: kg/cm²	Data esec.: 08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala: 1:50	
Località:	Sala Bolognese (BO)	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	4
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	5.0	10.0		5.00	1.40	4	28.0
0.40	12.0	33.0		12.00	1.40	9	11.7
0.60	18.0	39.0		18.00	1.67	11	9.3
0.80	24.0	49.0		24.00	2.07	12	8.6
1.00	31.0	62.0		31.00	2.47	13	8.0
1.20	29.0	66.0		29.00	2.60	11	9.0
1.40	27.0	66.0		27.00	2.53	11	9.4
1.60	20.0	58.0		20.00	1.53	13	7.7
1.80	25.0	48.0		25.00	1.53	16	6.1
2.00	22.0	45.0		22.00	1.20	18	5.5
2.20	19.0	37.0		19.00	1.47	13	7.7
2.40	17.0	39.0		17.00	1.80	9	10.6
2.60	13.0	40.0		13.00	0.87	15	6.7
2.80	15.0	28.0		15.00	1.00	15	6.7
3.00	16.0	31.0		16.00	0.80	20	5.0
3.20	15.0	27.0		15.00	0.60	25	4.0
3.40	9.0	18.0		9.00	0.47	19	5.2
3.60	15.0	22.0		15.00	0.53	28	3.5
3.80	23.0	31.0		23.00	0.93	25	4.0
4.00	22.0	36.0		22.00	1.13	19	5.1
4.20	16.0	33.0		16.00	0.73	22	4.6
4.40	12.0	23.0		12.00	0.53	23	4.4
4.60	15.0	23.0		15.00	0.67	22	4.5
4.80	14.0	24.0		14.00	0.53	26	3.8
5.00	30.0	38.0		30.00	0.40	75	1.3
5.20	21.0	27.0		21.00	0.47	45	2.2
5.40	19.0	26.0		19.00	0.47	40	2.5
5.60	16.0	23.0		16.00	0.53	30	3.3
5.80	12.0	20.0		12.00	0.60	20	5.0
6.00	14.0	23.0		14.00	0.73	19	5.2
6.20	12.0	23.0		12.00	0.67	18	5.6
6.40	19.0	29.0		19.00	1.00	19	5.3
6.60	15.0	30.0		15.00	0.73	21	4.9
6.80	17.0	28.0		17.00	0.47	36	2.8
7.00	11.0	18.0		11.00	0.47	23	4.3
7.20	14.0	21.0		14.00	0.67	21	4.8
7.40	15.0	25.0		15.00	0.80	19	5.3
7.60	21.0	33.0		21.00	0.47	45	2.2
7.80	14.0	21.0		14.00	0.93	15	6.6
8.00	18.0	32.0		18.00	0.60	30	3.3
8.20	17.0	26.0		17.00	0.53	32	3.1
8.40	14.0	22.0		14.00	0.40	35	2.9
8.60	10.0	16.0		10.00	0.40	25	4.0
8.80	12.0	18.0		12.00	0.40	30	3.3
9.00	12.0	18.0		12.00	0.47	26	3.9
9.20	17.0	24.0		17.00	1.07	16	6.3
9.40	18.0	34.0		18.00	0.40	45	2.2
9.60	26.0	32.0		26.00	0.60	43	2.3
9.80	25.0	34.0		25.00	0.80	31	3.2
10.00	18.0	30.0		18.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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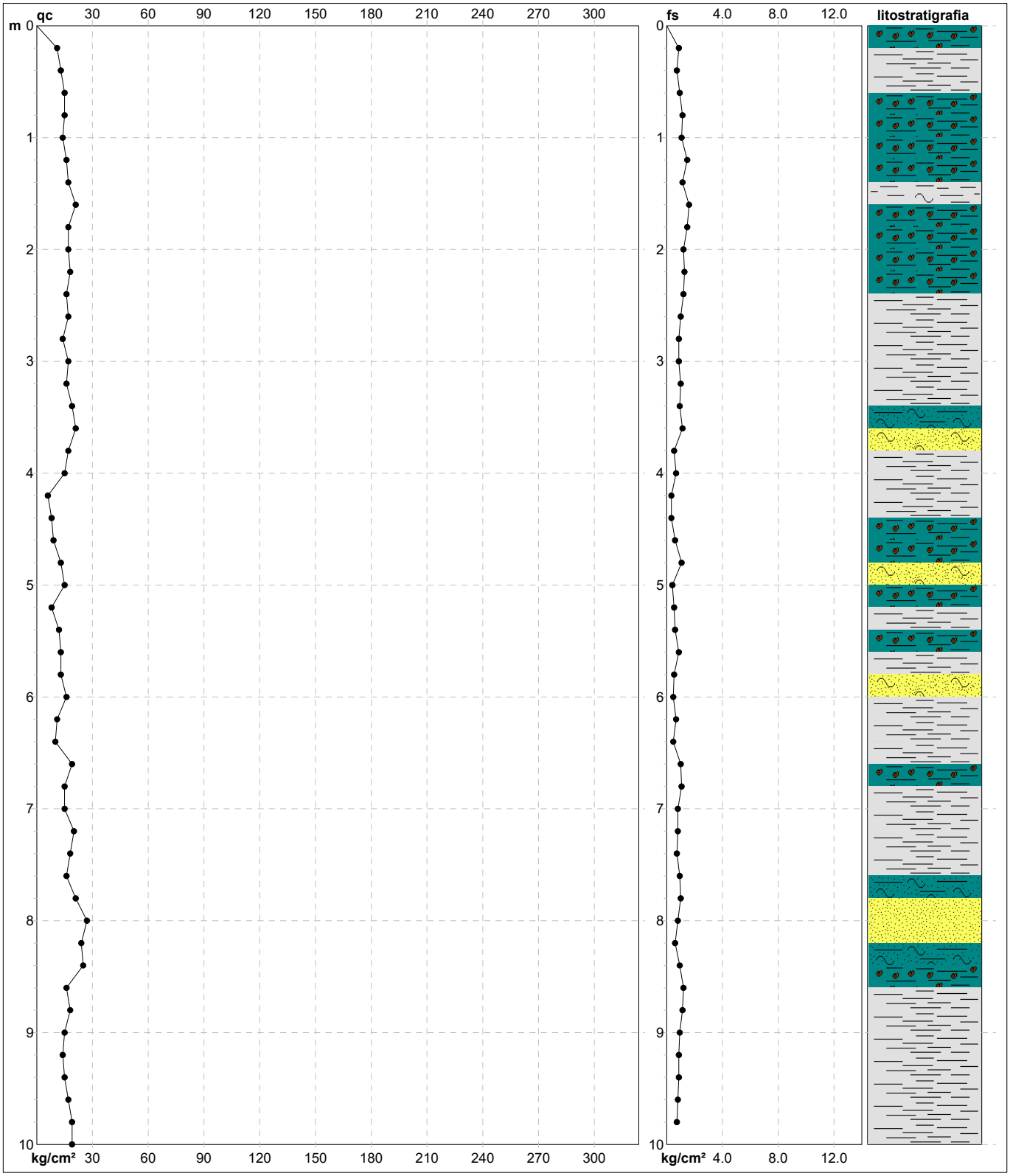
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	5
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:50	
Località:	**Sala Bolognese (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	5
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	11.0	22.0		11.00	0.87	13	7.9
0.40	13.0	26.0		13.00	0.73	18	5.6
0.60	15.0	26.0		15.00	0.93	16	6.2
0.80	15.0	29.0		15.00	1.13	13	7.5
1.00	14.0	31.0		14.00	1.07	13	7.6
1.20	16.0	32.0		16.00	1.47	11	9.2
1.40	17.0	39.0		17.00	1.13	15	6.6
1.60	21.0	38.0		21.00	1.60	13	7.6
1.80	17.0	41.0		17.00	1.47	12	8.6
2.00	17.0	39.0		17.00	1.20	14	7.1
2.20	18.0	36.0		18.00	1.27	14	7.1
2.40	16.0	35.0		16.00	1.20	13	7.5
2.60	17.0	35.0		17.00	1.00	17	5.9
2.80	14.0	29.0		14.00	0.87	16	6.2
3.00	17.0	30.0		17.00	0.87	20	5.1
3.20	16.0	29.0		16.00	1.00	16	6.3
3.40	19.0	34.0		19.00	0.93	20	4.9
3.60	21.0	35.0		21.00	1.13	19	5.4
3.80	17.0	34.0		17.00	0.53	32	3.1
4.00	15.0	23.0		15.00	0.67	22	4.5
4.20	6.0	16.0		6.00	0.33	18	5.5
4.40	8.0	13.0		8.00	0.33	24	4.1
4.60	9.0	14.0		9.00	0.60	15	6.7
4.80	13.0	22.0		13.00	1.07	12	8.2
5.00	15.0	31.0		15.00	0.40	38	2.7
5.20	8.0	14.0		8.00	0.53	15	6.6
5.40	12.0	20.0		12.00	0.60	20	5.0
5.60	13.0	22.0		13.00	0.87	15	6.7
5.80	13.0	26.0		13.00	0.53	25	4.1
6.00	16.0	24.0		16.00	0.47	34	2.9
6.20	11.0	18.0		11.00	0.67	16	6.1
6.40	10.0	20.0		10.00	0.47	21	4.7
6.60	19.0	26.0		19.00	1.00	19	5.3
6.80	15.0	30.0		15.00	1.07	14	7.1
7.00	15.0	31.0		15.00	0.80	19	5.3
7.20	20.0	32.0		20.00	0.80	25	4.0
7.40	18.0	30.0		18.00	0.73	25	4.1
7.60	16.0	27.0		16.00	0.93	17	5.8
7.80	21.0	35.0		21.00	1.00	21	4.8
8.00	27.0	42.0		27.00	0.80	34	3.0
8.20	24.0	36.0		24.00	0.60	40	2.5
8.40	25.0	34.0		25.00	0.93	27	3.7
8.60	16.0	30.0		16.00	1.20	13	7.5
8.80	18.0	36.0		18.00	1.13	16	6.3
9.00	15.0	32.0		15.00	0.93	16	6.2
9.20	14.0	28.0		14.00	0.87	16	6.2
9.40	15.0	28.0		15.00	0.87	17	5.8
9.60	17.0	30.0		17.00	0.80	21	4.7
9.80	19.0	31.0		19.00	0.73	26	3.8
10.00	19.0	30.0		19.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

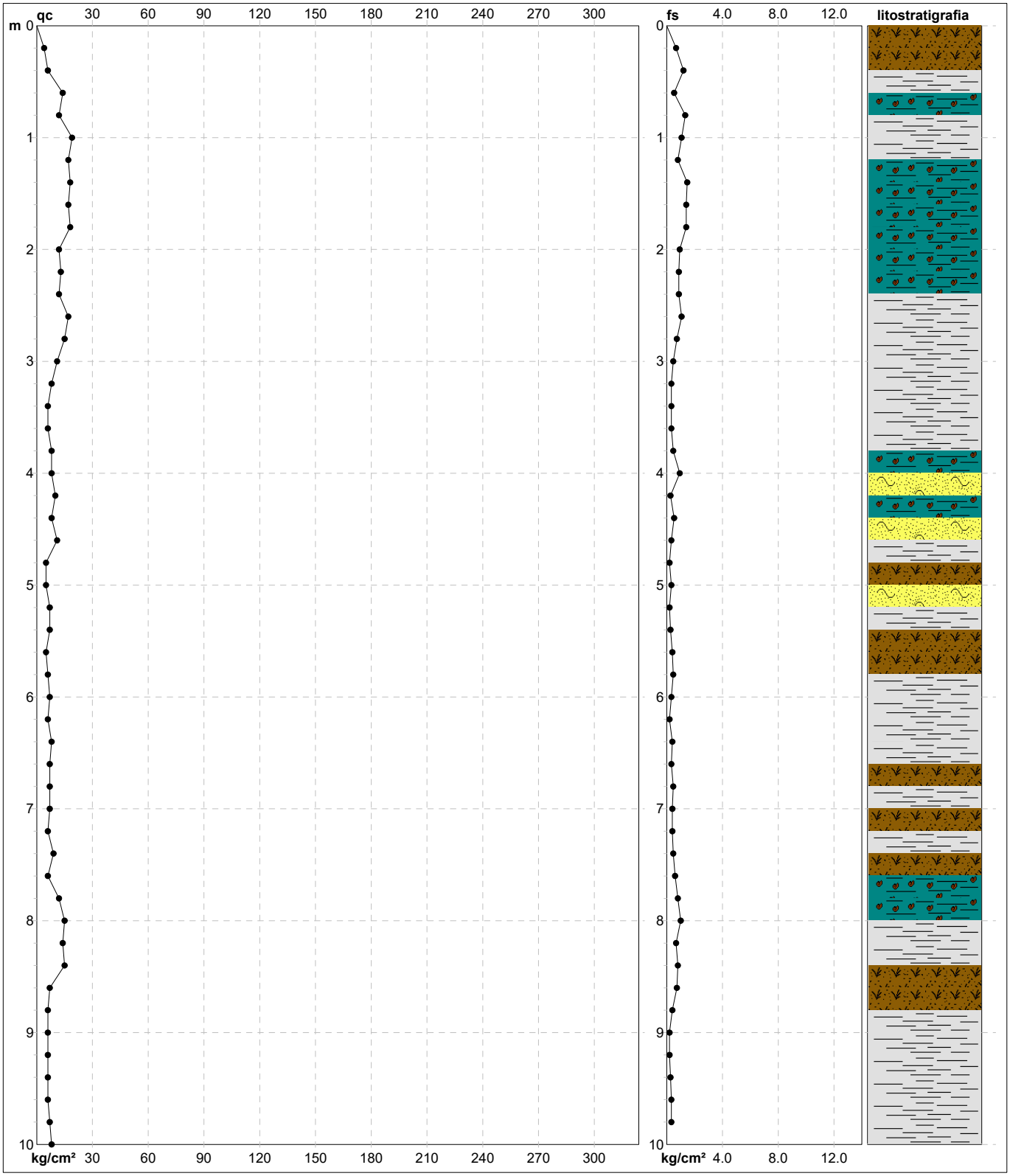
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	6
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:50	
Località:	**Sala Bolognese (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	6
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	9.0		4.00	0.67	6	16.8
0.40	6.0	16.0		6.00	1.20	5	20.0
0.60	14.0	32.0		14.00	0.53	26	3.8
0.80	12.0	20.0		12.00	1.33	9	11.1
1.00	19.0	39.0		19.00	1.07	18	5.6
1.20	17.0	33.0		17.00	0.80	21	4.7
1.40	18.0	30.0		18.00	1.47	12	8.2
1.60	17.0	39.0		17.00	1.40	12	8.2
1.80	18.0	39.0		18.00	1.40	13	7.8
2.00	12.0	33.0		12.00	0.93	13	7.8
2.20	13.0	27.0		13.00	0.87	15	6.7
2.40	12.0	25.0		12.00	0.87	14	7.3
2.60	17.0	30.0		17.00	1.07	16	6.3
2.80	15.0	31.0		15.00	0.73	21	4.9
3.00	11.0	22.0		11.00	0.47	23	4.3
3.20	8.0	15.0		8.00	0.33	24	4.1
3.40	6.0	11.0		6.00	0.33	18	5.5
3.60	6.0	11.0		6.00	0.33	18	5.5
3.80	8.0	13.0		8.00	0.47	17	5.9
4.00	8.0	15.0		8.00	0.93	9	11.6
4.20	10.0	24.0		10.00	0.27	37	2.7
4.40	8.0	12.0		8.00	0.53	15	6.6
4.60	11.0	19.0		11.00	0.33	33	3.0
4.80	5.0	10.0		5.00	0.20	25	4.0
5.00	5.0	8.0		5.00	0.33	15	6.6
5.20	7.0	12.0		7.00	0.20	35	2.9
5.40	7.0	10.0		7.00	0.27	26	3.9
5.60	5.0	9.0		5.00	0.40	13	8.0
5.80	6.0	12.0		6.00	0.47	13	7.8
6.00	7.0	14.0		7.00	0.33	21	4.7
6.20	6.0	11.0		6.00	0.20	30	3.3
6.40	8.0	11.0		8.00	0.40	20	5.0
6.60	7.0	13.0		7.00	0.33	21	4.7
6.80	7.0	12.0		7.00	0.47	15	6.7
7.00	7.0	14.0		7.00	0.40	18	5.7
7.20	6.0	12.0		6.00	0.40	15	6.7
7.40	9.0	15.0		9.00	0.47	19	5.2
7.60	6.0	13.0		6.00	0.60	10	10.0
7.80	12.0	21.0		12.00	0.80	15	6.7
8.00	15.0	27.0		15.00	1.00	15	6.7
8.20	14.0	29.0		14.00	0.67	21	4.8
8.40	15.0	25.0		15.00	0.80	19	5.3
8.60	7.0	19.0		7.00	0.73	10	10.4
8.80	6.0	17.0		6.00	0.40	15	6.7
9.00	6.0	12.0		6.00	0.20	30	3.3
9.20	6.0	9.0		6.00	0.20	30	3.3
9.40	6.0	9.0		6.00	0.27	22	4.5
9.60	6.0	10.0		6.00	0.33	18	5.5
9.80	7.0	12.0		7.00	0.33	21	4.7
10.00	8.0	13.0		8.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

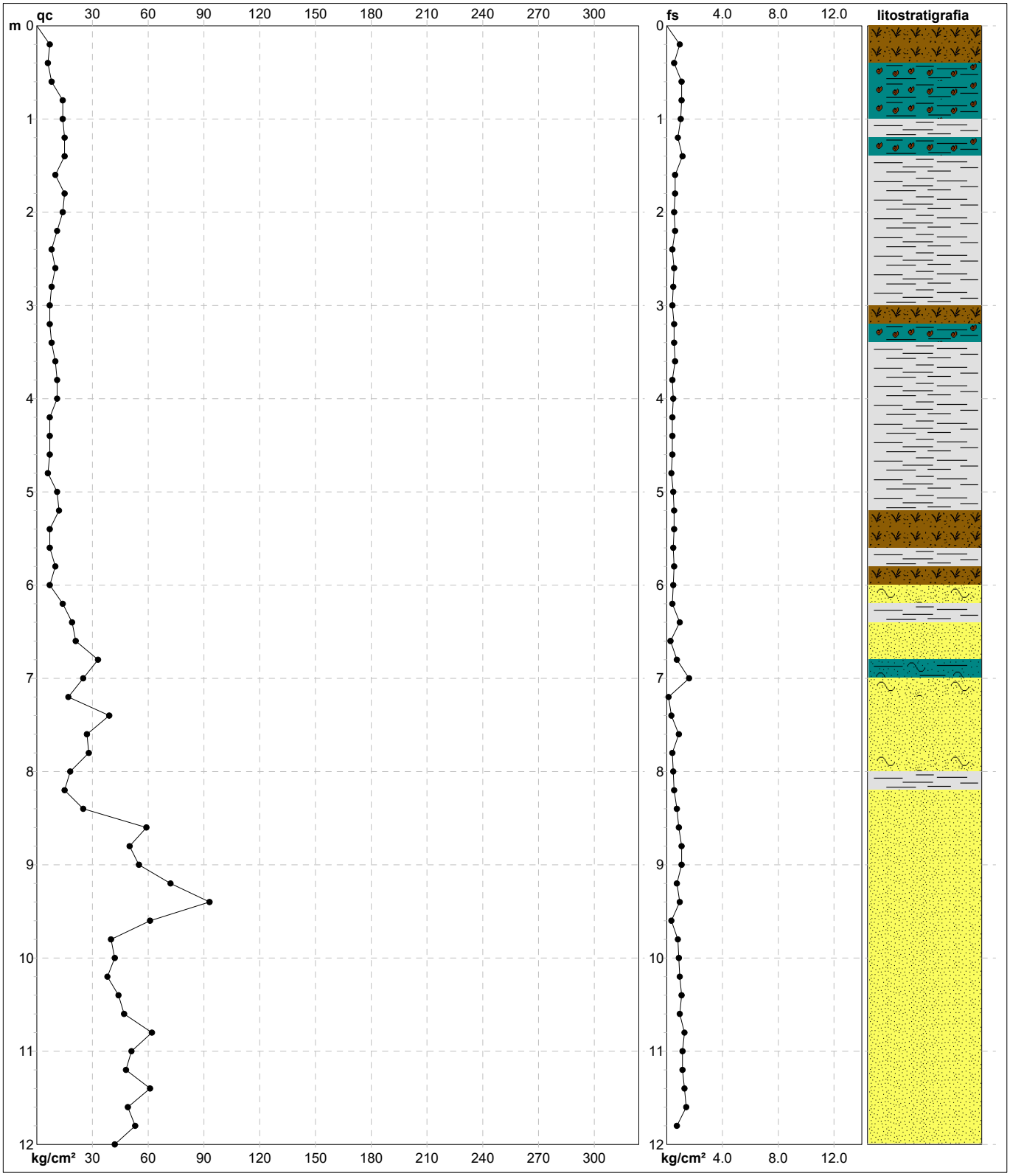
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	7
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.: kg/cm²	Data esec.: 08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala: 1:60	
Località:	Sala Bolognese (BO)	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	7
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	7.0	14.0		7.00	0.93	8	13.3
0.40	6.0	20.0		6.00	0.53	11	8.8
0.60	8.0	16.0		8.00	1.07	7	13.4
0.80	14.0	30.0		14.00	1.07	13	7.6
1.00	14.0	30.0		14.00	1.00	14	7.1
1.20	15.0	30.0		15.00	0.80	19	5.3
1.40	15.0	27.0		15.00	1.13	13	7.5
1.60	10.0	27.0		10.00	0.60	17	6.0
1.80	15.0	24.0		15.00	0.60	25	4.0
2.00	14.0	23.0		14.00	0.53	26	3.8
2.20	11.0	19.0		11.00	0.60	18	5.5
2.40	8.0	17.0		8.00	0.40	20	5.0
2.60	10.0	16.0		10.00	0.53	19	5.3
2.80	8.0	16.0		8.00	0.47	17	5.9
3.00	7.0	14.0		7.00	0.40	18	5.7
3.20	7.0	13.0		7.00	0.53	13	7.6
3.40	8.0	16.0		8.00	0.53	15	6.6
3.60	10.0	18.0		10.00	0.60	17	6.0
3.80	11.0	20.0		11.00	0.40	28	3.6
4.00	11.0	17.0		11.00	0.47	23	4.3
4.20	7.0	14.0		7.00	0.40	18	5.7
4.40	7.0	13.0		7.00	0.40	18	5.7
4.60	7.0	13.0		7.00	0.40	18	5.7
4.80	6.0	12.0		6.00	0.33	18	5.5
5.00	11.0	16.0		11.00	0.47	23	4.3
5.20	12.0	19.0		12.00	0.53	23	4.4
5.40	7.0	15.0		7.00	0.53	13	7.6
5.60	7.0	15.0		7.00	0.47	15	6.7
5.80	10.0	17.0		10.00	0.53	19	5.3
6.00	7.0	15.0		7.00	0.47	15	6.7
6.20	14.0	21.0		14.00	0.40	35	2.9
6.40	19.0	25.0		19.00	0.93	20	4.9
6.60	21.0	35.0		21.00	0.27	78	1.3
6.80	33.0	37.0		33.00	0.73	45	2.2
7.00	25.0	36.0		25.00	1.60	16	6.4
7.20	17.0	41.0		17.00	0.13	131	0.8
7.40	39.0	41.0		39.00	0.33	118	0.8
7.60	27.0	32.0		27.00	0.87	31	3.2
7.80	28.0	41.0		28.00	0.40	70	1.4
8.00	18.0	24.0		18.00	0.47	38	2.6
8.20	15.0	22.0		15.00	0.53	28	3.5
8.40	25.0	33.0		25.00	0.73	34	2.9
8.60	59.0	70.0		59.00	0.87	68	1.5
8.80	50.0	63.0		50.00	1.07	47	2.1
9.00	55.0	71.0		55.00	1.07	51	1.9
9.20	72.0	88.0		72.00	0.73	99	1.0
9.40	93.0	104.0		93.00	0.93	100	1.0
9.60	61.0	75.0		61.00	0.33	185	0.5
9.80	40.0	45.0		40.00	0.80	50	2.0
10.00	42.0	54.0		42.00	0.87	48	2.1
10.20	38.0	51.0		38.00	0.93	41	2.4
10.40	44.0	58.0		44.00	1.07	41	2.4
10.60	47.0	63.0		47.00	0.93	51	2.0
10.80	62.0	76.0		62.00	1.27	49	2.0
11.00	51.0	70.0		51.00	1.13	45	2.2
11.20	48.0	65.0		48.00	1.13	42	2.4
11.40	61.0	78.0		61.00	1.27	48	2.1
11.60	49.0	68.0		49.00	1.40	35	2.9
11.80	53.0	74.0		53.00	0.73	73	1.4
12.00	42.0	53.0		42.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

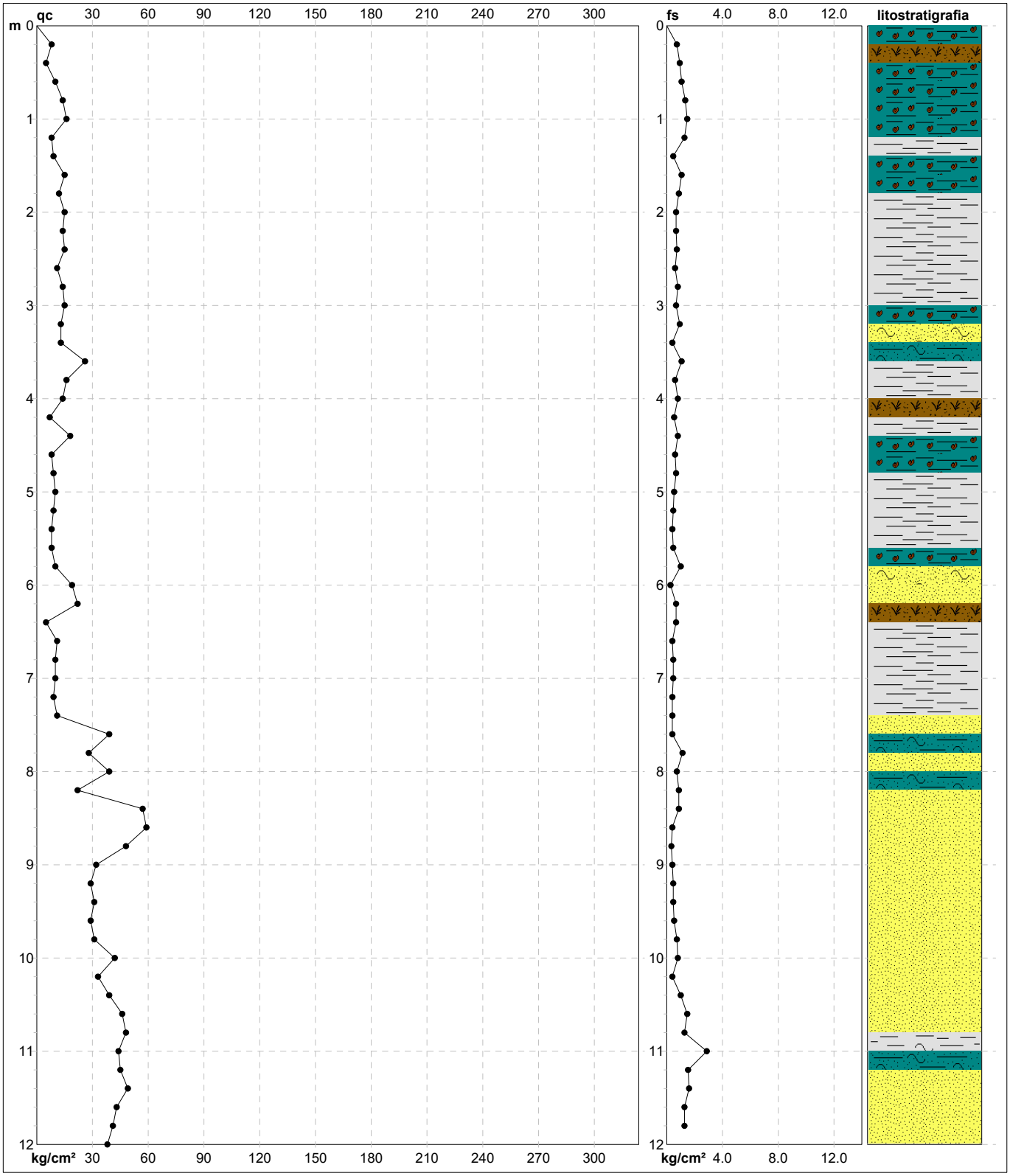
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	8
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.: kg/cm²	Data esec.: 08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala: 1:60	
Località:	Sala Bolognese (BO)	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	8
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	8.0	20.0		8.00	0.73	11	9.1
0.40	5.0	16.0		5.00	0.93	5	18.6
0.60	10.0	24.0		10.00	1.07	9	10.7
0.80	14.0	30.0		14.00	1.33	11	9.5
1.00	16.0	36.0		16.00	1.47	11	9.2
1.20	8.0	30.0		8.00	1.27	6	15.9
1.40	9.0	28.0		9.00	0.47	19	5.2
1.60	15.0	22.0		15.00	1.07	14	7.1
1.80	12.0	28.0		12.00	0.87	14	7.3
2.00	15.0	28.0		15.00	0.67	22	4.5
2.20	14.0	24.0		14.00	0.67	21	4.8
2.40	15.0	25.0		15.00	0.73	21	4.9
2.60	11.0	22.0		11.00	0.60	18	5.5
2.80	14.0	23.0		14.00	0.80	18	5.7
3.00	15.0	27.0		15.00	0.67	22	4.5
3.20	13.0	23.0		13.00	0.93	14	7.2
3.40	13.0	27.0		13.00	0.40	33	3.1
3.60	26.0	32.0		26.00	1.07	24	4.1
3.80	16.0	32.0		16.00	0.60	27	3.8
4.00	14.0	23.0		14.00	0.80	18	5.7
4.20	7.0	19.0		7.00	0.53	13	7.6
4.40	18.0	26.0		18.00	0.80	23	4.4
4.60	8.0	20.0		8.00	0.60	13	7.5
4.80	9.0	18.0		9.00	0.67	13	7.4
5.00	10.0	20.0		10.00	0.53	19	5.3
5.20	9.0	17.0		9.00	0.47	19	5.2
5.40	8.0	15.0		8.00	0.40	20	5.0
5.60	8.0	14.0		8.00	0.47	17	5.9
5.80	10.0	17.0		10.00	1.00	10	10.0
6.00	19.0	34.0		19.00	0.27	70	1.4
6.20	22.0	26.0		22.00	0.67	33	3.0
6.40	5.0	15.0		5.00	0.67	7	13.4
6.60	11.0	21.0		11.00	0.40	28	3.6
6.80	10.0	16.0		10.00	0.47	21	4.7
7.00	10.0	17.0		10.00	0.47	21	4.7
7.20	9.0	16.0		9.00	0.40	23	4.4
7.40	11.0	17.0		11.00	0.40	28	3.6
7.60	39.0	45.0		39.00	0.40	98	1.0
7.80	28.0	34.0		28.00	1.13	25	4.0
8.00	39.0	56.0		39.00	0.73	53	1.9
8.20	22.0	33.0		22.00	0.87	25	4.0
8.40	57.0	70.0		57.00	0.87	66	1.5
8.60	59.0	72.0		59.00	0.40	148	0.7
8.80	48.0	54.0		48.00	0.33	145	0.7
9.00	32.0	37.0		32.00	0.40	80	1.3
9.20	29.0	35.0		29.00	0.47	62	1.6
9.40	31.0	38.0		31.00	0.47	66	1.5
9.60	29.0	36.0		29.00	0.53	55	1.8
9.80	31.0	39.0		31.00	0.73	42	2.4
10.00	42.0	53.0		42.00	0.80	53	1.9
10.20	33.0	45.0		33.00	0.40	83	1.2
10.40	39.0	45.0		39.00	1.00	39	2.6
10.60	46.0	61.0		46.00	1.47	31	3.2
10.80	48.0	70.0		48.00	1.27	38	2.6
11.00	44.0	63.0		44.00	2.87	15	6.5
11.20	45.0	88.0		45.00	1.53	29	3.4
11.40	49.0	72.0		49.00	1.60	31	3.3
11.60	43.0	67.0		43.00	1.27	34	3.0
11.80	41.0	60.0		41.00	1.27	32	3.1
12.00	38.0	57.0		38.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

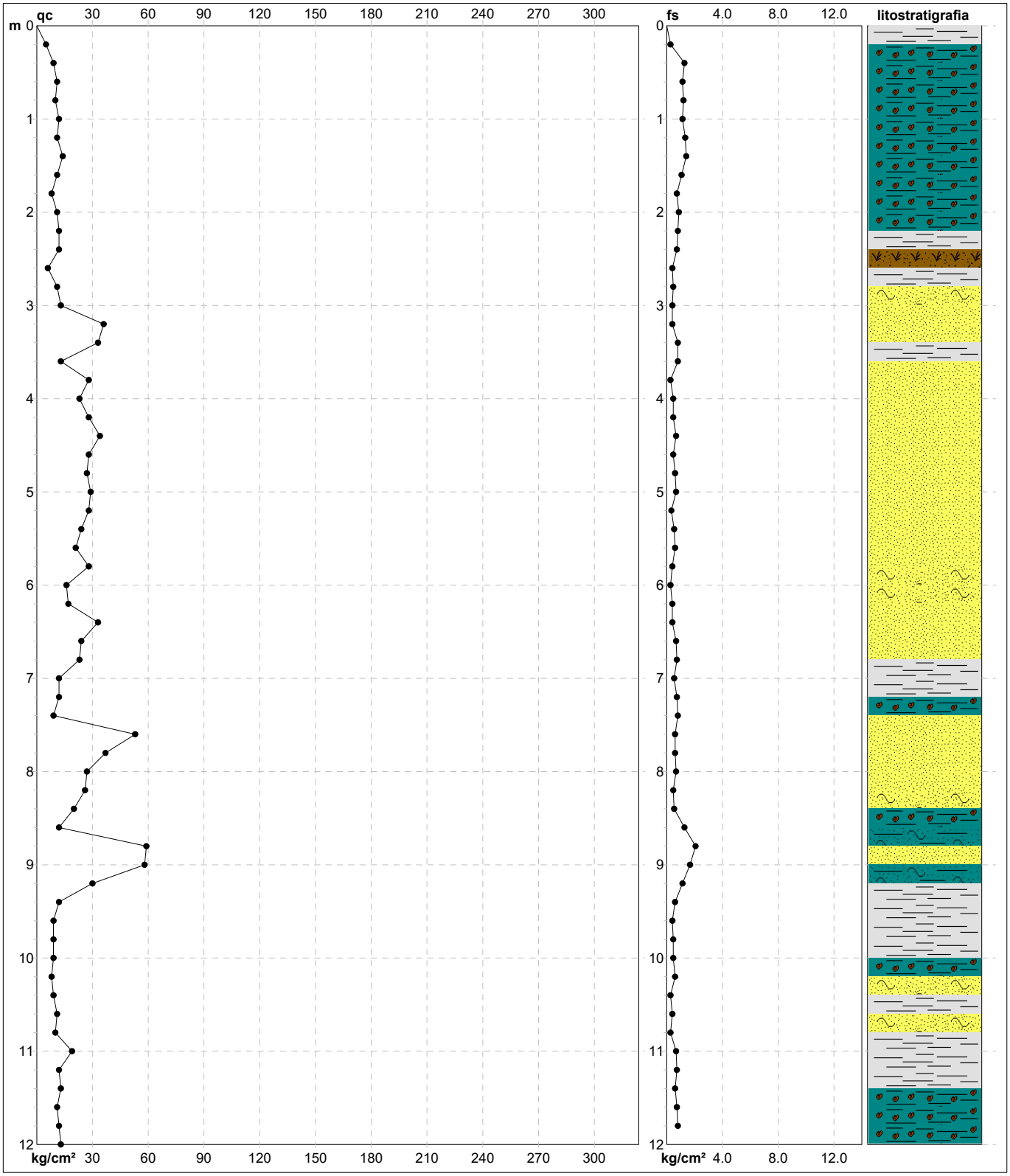
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	9
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:60	
Località:	**Sala Bolognese (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	9
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	5.0	10.0		5.00	0.27	19	5.4
0.40	9.0	13.0		9.00	1.27	7	14.1
0.60	11.0	30.0		11.00	1.13	10	10.3
0.80	10.0	27.0		10.00	1.20	8	12.0
1.00	12.0	30.0		12.00	1.13	11	9.4
1.20	11.0	28.0		11.00	1.33	8	12.1
1.40	14.0	34.0		14.00	1.40	10	10.0
1.60	11.0	32.0		11.00	1.07	10	9.7
1.80	8.0	24.0		8.00	0.73	11	9.1
2.00	11.0	22.0		11.00	0.87	13	7.9
2.20	12.0	25.0		12.00	0.80	15	6.7
2.40	12.0	24.0		12.00	0.73	16	6.1
2.60	6.0	17.0		6.00	0.40	15	6.7
2.80	11.0	17.0		11.00	0.47	23	4.3
3.00	13.0	20.0		13.00	0.40	33	3.1
3.20	36.0	42.0		36.00	0.40	90	1.1
3.40	33.0	39.0		33.00	0.80	41	2.4
3.60	13.0	25.0		13.00	0.80	16	6.2
3.80	28.0	40.0		28.00	0.27	104	1.0
4.00	23.0	27.0		23.00	0.47	49	2.0
4.20	28.0	35.0		28.00	0.47	60	1.7
4.40	34.0	41.0		34.00	0.67	51	2.0
4.60	28.0	38.0		28.00	0.47	60	1.7
4.80	27.0	34.0		27.00	0.60	45	2.2
5.00	29.0	38.0		29.00	0.67	43	2.3
5.20	28.0	38.0		28.00	0.33	85	1.2
5.40	24.0	29.0		24.00	0.53	45	2.2
5.60	21.0	29.0		21.00	0.60	35	2.9
5.80	28.0	37.0		28.00	0.40	70	1.4
6.00	16.0	22.0		16.00	0.27	59	1.7
6.20	17.0	21.0		17.00	0.40	43	2.4
6.40	33.0	39.0		33.00	0.40	83	1.2
6.60	24.0	30.0		24.00	0.67	36	2.8
6.80	23.0	33.0		23.00	0.73	32	3.2
7.00	12.0	23.0		12.00	0.53	23	4.4
7.20	12.0	20.0		12.00	0.73	16	6.1
7.40	9.0	20.0		9.00	0.80	11	8.9
7.60	53.0	65.0		53.00	0.60	88	1.1
7.80	37.0	46.0		37.00	0.60	62	1.6
8.00	27.0	36.0		27.00	0.67	40	2.5
8.20	26.0	36.0		26.00	0.47	55	1.8
8.40	20.0	27.0		20.00	0.53	38	2.7
8.60	12.0	20.0		12.00	1.27	9	10.6
8.80	59.0	78.0		59.00	2.07	29	3.5
9.00	58.0	89.0		58.00	1.67	35	2.9
9.20	30.0	55.0		30.00	1.13	27	3.8
9.40	12.0	29.0		12.00	0.60	20	5.0
9.60	9.0	18.0		9.00	0.40	23	4.4
9.80	9.0	15.0		9.00	0.47	19	5.2
10.00	9.0	16.0		9.00	0.47	19	5.2
10.20	8.0	15.0		8.00	0.60	13	7.5
10.40	9.0	18.0		9.00	0.27	33	3.0
10.60	11.0	15.0		11.00	0.40	28	3.6
10.80	10.0	16.0		10.00	0.27	37	2.7
11.00	19.0	23.0		19.00	0.67	28	3.5
11.20	12.0	22.0		12.00	0.73	16	6.1
11.40	13.0	24.0		13.00	0.60	22	4.6
11.60	11.0	20.0		11.00	0.73	15	6.6
11.80	12.0	23.0		12.00	0.80	15	6.7
12.00	13.0	25.0		13.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

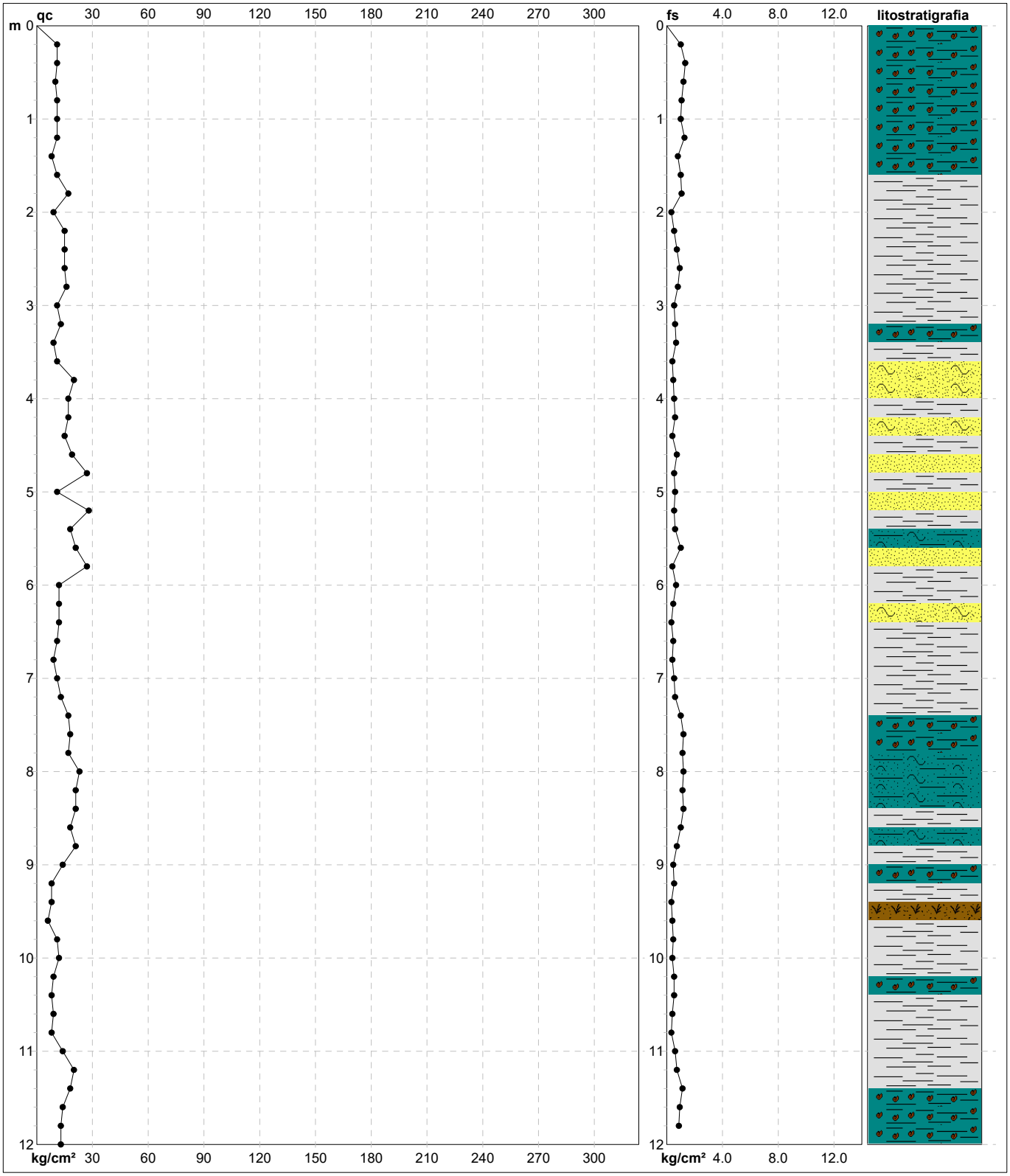
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	10
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:60	
Località:	**Sala Bolognese (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	10
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	11.0	29.0		11.00	1.00	11	9.1
0.40	11.0	26.0		11.00	1.33	8	12.1
0.60	10.0	30.0		10.00	1.20	8	12.0
0.80	11.0	29.0		11.00	1.07	10	9.7
1.00	11.0	27.0		11.00	1.00	11	9.1
1.20	11.0	26.0		11.00	1.27	9	11.5
1.40	8.0	27.0		8.00	0.80	10	10.0
1.60	11.0	23.0		11.00	1.00	11	9.1
1.80	17.0	32.0		17.00	1.07	16	6.3
2.00	9.0	25.0		9.00	0.33	27	3.7
2.20	15.0	20.0		15.00	0.53	28	3.5
2.40	15.0	23.0		15.00	0.73	21	4.9
2.60	15.0	26.0		15.00	0.93	16	6.2
2.80	16.0	30.0		16.00	0.80	20	5.0
3.00	11.0	23.0		11.00	0.53	21	4.8
3.20	13.0	21.0		13.00	0.60	22	4.6
3.40	9.0	18.0		9.00	0.67	13	7.4
3.60	11.0	21.0		11.00	0.40	28	3.6
3.80	20.0	26.0		20.00	0.47	43	2.4
4.00	17.0	24.0		17.00	0.53	32	3.1
4.20	17.0	25.0		17.00	0.60	28	3.5
4.40	15.0	24.0		15.00	0.40	38	2.7
4.60	19.0	25.0		19.00	0.73	26	3.8
4.80	27.0	38.0		27.00	0.53	51	2.0
5.00	11.0	19.0		11.00	0.60	18	5.5
5.20	28.0	37.0		28.00	0.53	53	1.9
5.40	18.0	26.0		18.00	0.60	30	3.3
5.60	21.0	30.0		21.00	1.00	21	4.8
5.80	27.0	42.0		27.00	0.40	68	1.5
6.00	12.0	18.0		12.00	0.67	18	5.6
6.20	12.0	22.0		12.00	0.47	26	3.9
6.40	12.0	19.0		12.00	0.33	36	2.8
6.60	11.0	16.0		11.00	0.47	23	4.3
6.80	9.0	16.0		9.00	0.40	23	4.4
7.00	11.0	17.0		11.00	0.53	21	4.8
7.20	13.0	21.0		13.00	0.60	22	4.6
7.40	17.0	26.0		17.00	1.00	17	5.9
7.60	18.0	33.0		18.00	1.20	15	6.7
7.80	17.0	35.0		17.00	1.13	15	6.6
8.00	23.0	40.0		23.00	1.20	19	5.2
8.20	21.0	39.0		21.00	1.13	19	5.4
8.40	21.0	38.0		21.00	1.20	18	5.7
8.60	18.0	36.0		18.00	1.00	18	5.6
8.80	21.0	36.0		21.00	0.73	29	3.5
9.00	14.0	25.0		14.00	0.47	30	3.4
9.20	8.0	15.0		8.00	0.53	15	6.6
9.40	8.0	16.0		8.00	0.33	24	4.1
9.60	6.0	11.0		6.00	0.40	15	6.7
9.80	11.0	17.0		11.00	0.47	23	4.3
10.00	12.0	19.0		12.00	0.40	30	3.3
10.20	9.0	15.0		9.00	0.53	17	5.9
10.40	8.0	16.0		8.00	0.53	15	6.6
10.60	9.0	17.0		9.00	0.40	23	4.4
10.80	8.0	14.0		8.00	0.33	24	4.1
11.00	14.0	19.0		14.00	0.60	23	4.3
11.20	20.0	29.0		20.00	0.73	27	3.7
11.40	18.0	29.0		18.00	1.13	16	6.3
11.60	14.0	31.0		14.00	0.93	15	6.6
11.80	13.0	27.0		13.00	0.87	15	6.7
12.00	13.0	26.0		13.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

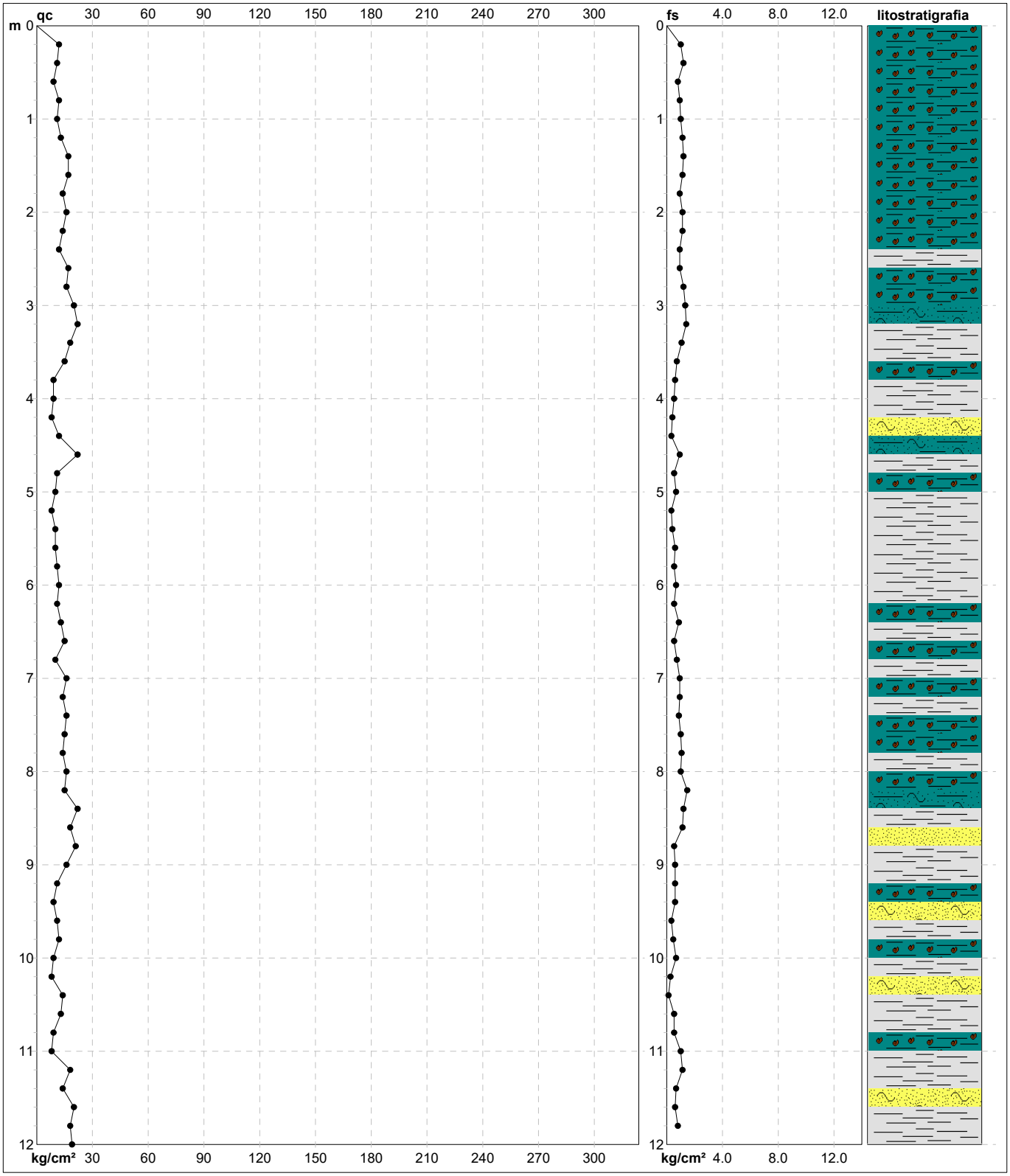
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	11
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.: kg/cm²	Data esec.: 08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala: 1:60	
Località:	Sala Bolognese (BO)	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	11
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	12.0	24.0		12.00	1.00	12	8.3
0.40	11.0	26.0		11.00	1.20	9	10.9
0.60	9.0	27.0		9.00	0.80	11	8.9
0.80	12.0	24.0		12.00	0.93	13	7.8
1.00	11.0	25.0		11.00	1.00	11	9.1
1.20	13.0	28.0		13.00	1.13	12	8.7
1.40	17.0	34.0		17.00	1.20	14	7.1
1.60	17.0	35.0		17.00	1.13	15	6.6
1.80	14.0	31.0		14.00	0.93	15	6.6
2.00	16.0	30.0		16.00	1.13	14	7.1
2.20	14.0	31.0		14.00	1.13	12	8.1
2.40	12.0	29.0		12.00	0.93	13	7.8
2.60	17.0	31.0		17.00	0.93	18	5.5
2.80	16.0	30.0		16.00	1.20	13	7.5
3.00	20.0	38.0		20.00	1.33	15	6.7
3.20	22.0	42.0		22.00	1.40	16	6.4
3.40	18.0	39.0		18.00	1.07	17	5.9
3.60	15.0	31.0		15.00	0.73	21	4.9
3.80	9.0	20.0		9.00	0.60	15	6.7
4.00	9.0	18.0		9.00	0.53	17	5.9
4.20	8.0	16.0		8.00	0.40	20	5.0
4.40	12.0	18.0		12.00	0.33	36	2.8
4.60	22.0	27.0		22.00	0.93	24	4.2
4.80	11.0	25.0		11.00	0.53	21	4.8
5.00	10.0	18.0		10.00	0.67	15	6.7
5.20	8.0	18.0		8.00	0.33	24	4.1
5.40	10.0	15.0		10.00	0.40	25	4.0
5.60	10.0	16.0		10.00	0.60	17	6.0
5.80	11.0	20.0		11.00	0.53	21	4.8
6.00	12.0	20.0		12.00	0.67	18	5.6
6.20	11.0	21.0		11.00	0.53	21	4.8
6.40	13.0	21.0		13.00	0.87	15	6.7
6.60	15.0	28.0		15.00	0.53	28	3.5
6.80	10.0	18.0		10.00	0.73	14	7.3
7.00	16.0	27.0		16.00	0.93	17	5.8
7.20	14.0	28.0		14.00	0.93	15	6.6
7.40	16.0	30.0		16.00	0.87	18	5.4
7.60	15.0	28.0		15.00	1.00	15	6.7
7.80	14.0	29.0		14.00	1.07	13	7.6
8.00	16.0	32.0		16.00	1.00	16	6.3
8.20	15.0	30.0		15.00	1.47	10	9.8
8.40	22.0	44.0		22.00	1.20	18	5.5
8.60	18.0	36.0		18.00	1.13	16	6.3
8.80	21.0	38.0		21.00	0.53	40	2.5
9.00	16.0	24.0		16.00	0.60	27	3.8
9.20	11.0	20.0		11.00	0.60	18	5.5
9.40	9.0	18.0		9.00	0.60	15	6.7
9.60	11.0	20.0		11.00	0.33	33	3.0
9.80	12.0	17.0		12.00	0.47	26	3.9
10.00	9.0	16.0		9.00	0.67	13	7.4
10.20	8.0	18.0		8.00	0.27	30	3.4
10.40	14.0	18.0		14.00	0.13	108	0.9
10.60	13.0	15.0		13.00	0.53	25	4.1
10.80	9.0	17.0		9.00	0.53	17	5.9
11.00	8.0	16.0		8.00	1.00	8	12.5
11.20	18.0	33.0		18.00	1.13	16	6.3
11.40	14.0	31.0		14.00	0.67	21	4.8
11.60	20.0	30.0		20.00	0.60	33	3.0
11.80	18.0	27.0		18.00	0.80	23	4.4
12.00	19.0	31.0		19.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

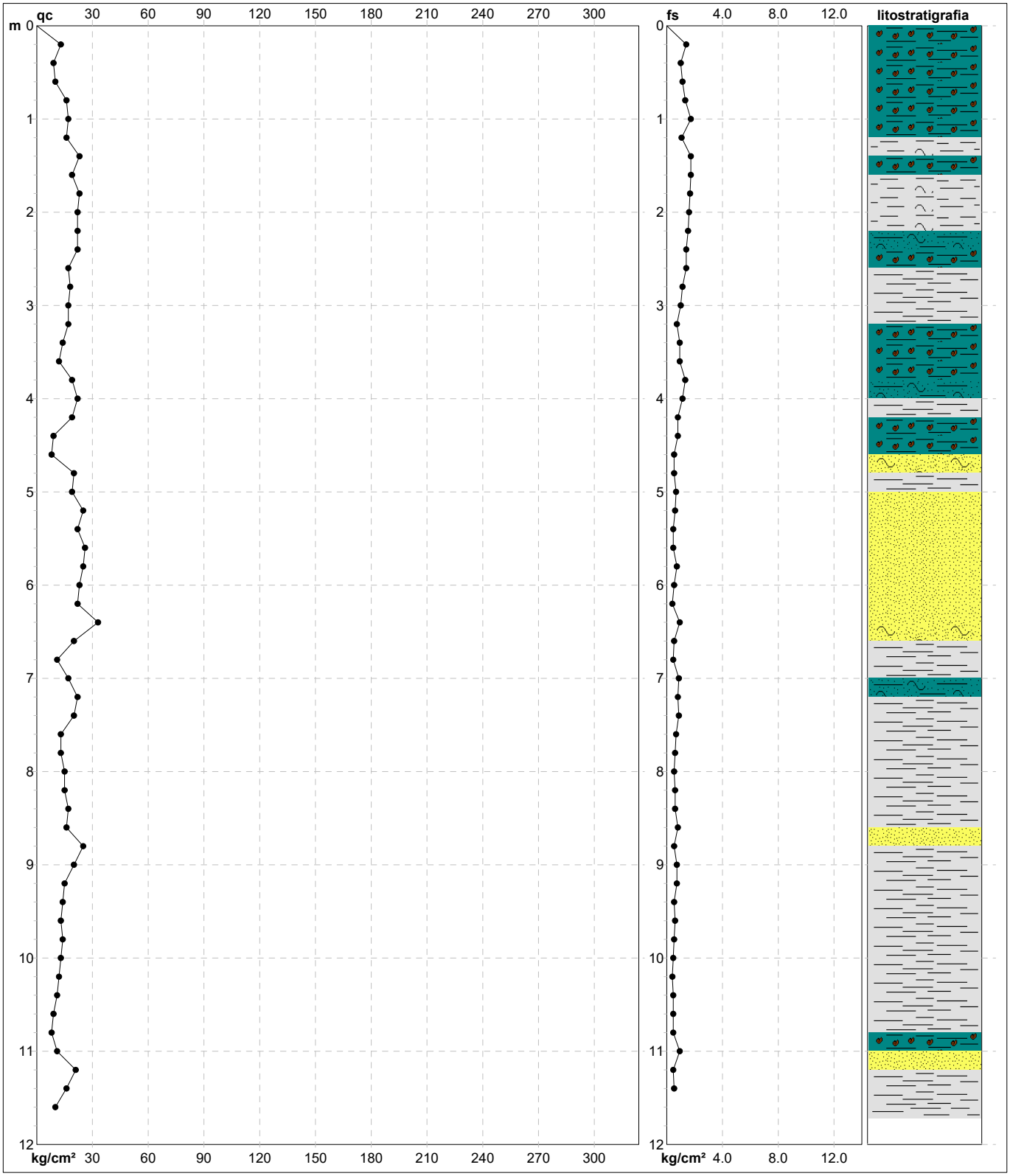
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	12
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:60	
Località:	**Sala Bolognese (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	12
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	13.0	24.0		13.00	1.40	9	10.8
0.40	9.0	30.0		9.00	1.00	9	11.1
0.60	10.0	25.0		10.00	1.13	9	11.3
0.80	16.0	33.0		16.00	1.33	12	8.3
1.00	17.0	37.0		17.00	1.73	10	10.2
1.20	16.0	42.0		16.00	1.07	15	6.7
1.40	23.0	39.0		23.00	1.73	13	7.5
1.60	19.0	45.0		19.00	1.73	11	9.1
1.80	23.0	49.0		23.00	1.67	14	7.3
2.00	22.0	47.0		22.00	1.60	14	7.3
2.20	22.0	46.0		22.00	1.53	14	7.0
2.40	22.0	45.0		22.00	1.40	16	6.4
2.60	17.0	38.0		17.00	1.40	12	8.2
2.80	18.0	39.0		18.00	1.13	16	6.3
3.00	17.0	34.0		17.00	1.00	17	5.9
3.20	17.0	32.0		17.00	0.73	23	4.3
3.40	14.0	25.0		14.00	0.93	15	6.6
3.60	12.0	26.0		12.00	0.93	13	7.8
3.80	19.0	33.0		19.00	1.33	14	7.0
4.00	22.0	42.0		22.00	1.13	19	5.1
4.20	19.0	36.0		19.00	0.80	24	4.2
4.40	9.0	21.0		9.00	0.80	11	8.9
4.60	8.0	20.0		8.00	0.53	15	6.6
4.80	20.0	28.0		20.00	0.53	38	2.7
5.00	19.0	27.0		19.00	0.67	28	3.5
5.20	25.0	35.0		25.00	0.60	42	2.4
5.40	22.0	31.0		22.00	0.47	47	2.1
5.60	26.0	33.0		26.00	0.47	55	1.8
5.80	25.0	32.0		25.00	0.73	34	2.9
6.00	23.0	34.0		23.00	0.53	43	2.3
6.20	22.0	30.0		22.00	0.40	55	1.8
6.40	33.0	39.0		33.00	0.93	35	2.8
6.60	20.0	34.0		20.00	0.53	38	2.7
6.80	11.0	19.0		11.00	0.47	23	4.3
7.00	17.0	24.0		17.00	0.87	20	5.1
7.20	22.0	35.0		22.00	0.80	28	3.6
7.40	20.0	32.0		20.00	0.87	23	4.4
7.60	13.0	26.0		13.00	0.67	19	5.2
7.80	13.0	23.0		13.00	0.60	22	4.6
8.00	15.0	24.0		15.00	0.53	28	3.5
8.20	15.0	23.0		15.00	0.60	25	4.0
8.40	17.0	26.0		17.00	0.60	28	3.5
8.60	16.0	25.0		16.00	0.80	20	5.0
8.80	25.0	37.0		25.00	0.53	47	2.1
9.00	20.0	28.0		20.00	0.73	27	3.7
9.20	15.0	26.0		15.00	0.73	21	4.9
9.40	14.0	25.0		14.00	0.53	26	3.8
9.60	13.0	21.0		13.00	0.60	22	4.6
9.80	14.0	23.0		14.00	0.53	26	3.8
10.00	13.0	21.0		13.00	0.47	28	3.6
10.20	12.0	19.0		12.00	0.40	30	3.3
10.40	11.0	17.0		11.00	0.47	23	4.3
10.60	9.0	16.0		9.00	0.47	19	5.2
10.80	8.0	15.0		8.00	0.47	17	5.9
11.00	11.0	18.0		11.00	0.93	12	8.5
11.20	21.0	35.0		21.00	0.47	45	2.2
11.40	16.0	23.0		16.00	0.53	30	3.3
11.60	10.0	18.0		10.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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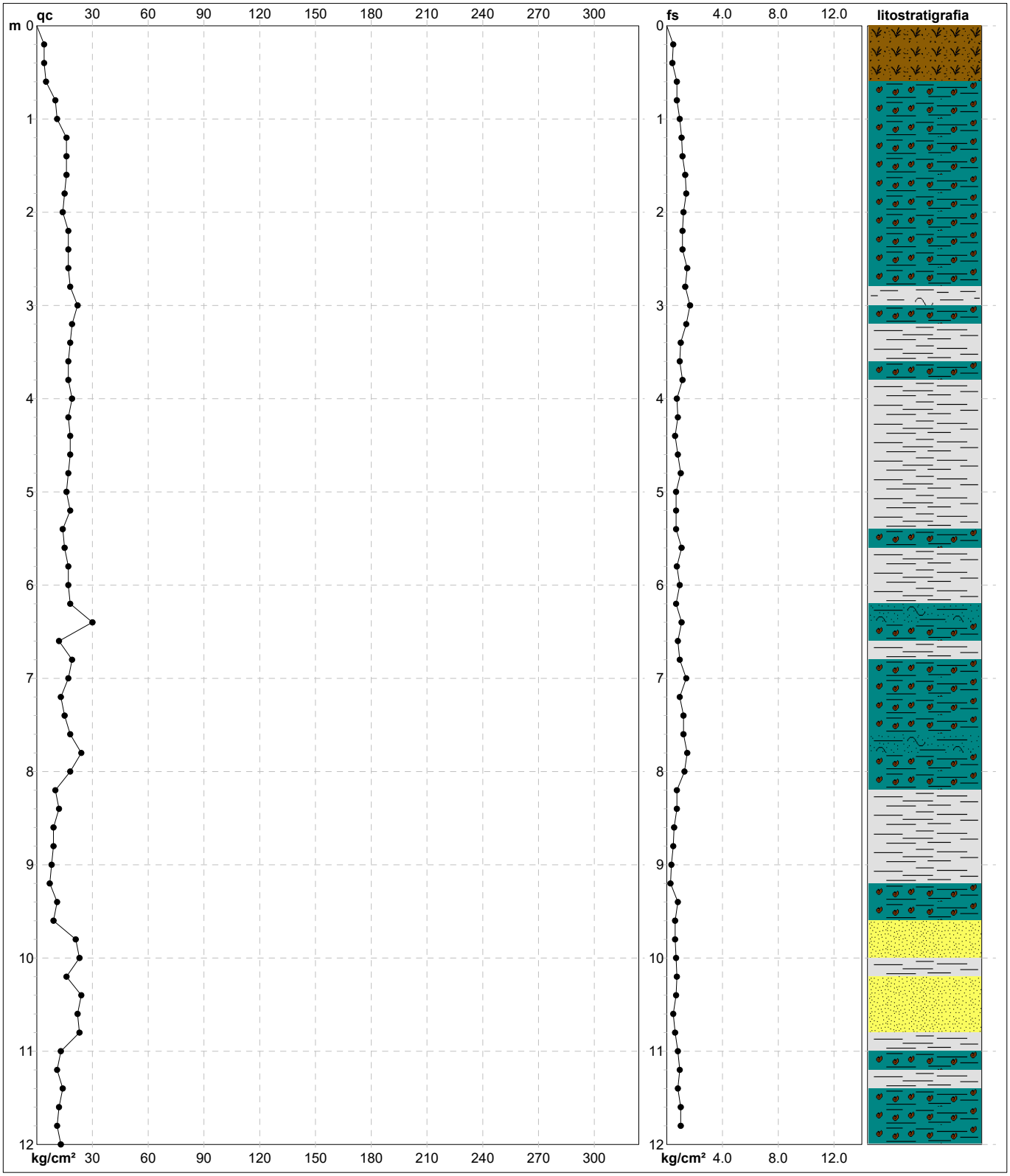
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	13
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.: kg/cm²	Data esec.: 08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala: 1:60	
Località:	Sala Bolognese (BO)	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	13
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	4.0	8.0		4.00	0.47	9	11.8
0.40	4.0	11.0		4.00	0.40	10	10.0
0.60	5.0	11.0		5.00	0.73	7	14.6
0.80	10.0	21.0		10.00	0.73	14	7.3
1.00	11.0	22.0		11.00	0.93	12	8.5
1.20	16.0	30.0		16.00	1.07	15	6.7
1.40	16.0	32.0		16.00	1.13	14	7.1
1.60	16.0	33.0		16.00	1.33	12	8.3
1.80	15.0	35.0		15.00	1.40	11	9.3
2.00	14.0	35.0		14.00	1.20	12	8.6
2.20	17.0	35.0		17.00	1.13	15	6.6
2.40	17.0	34.0		17.00	1.13	15	6.6
2.60	17.0	34.0		17.00	1.47	12	8.6
2.80	18.0	40.0		18.00	1.33	14	7.4
3.00	22.0	42.0		22.00	1.67	13	7.6
3.20	19.0	44.0		19.00	1.40	14	7.4
3.40	18.0	39.0		18.00	1.00	18	5.6
3.60	17.0	32.0		17.00	0.93	18	5.5
3.80	17.0	31.0		17.00	1.13	15	6.6
4.00	19.0	36.0		19.00	0.73	26	3.8
4.20	17.0	28.0		17.00	0.80	21	4.7
4.40	18.0	30.0		18.00	0.60	30	3.3
4.60	18.0	27.0		18.00	0.80	23	4.4
4.80	17.0	29.0		17.00	1.00	17	5.9
5.00	16.0	31.0		16.00	0.67	24	4.2
5.20	18.0	28.0		18.00	0.67	27	3.7
5.40	14.0	24.0		14.00	0.67	21	4.8
5.60	15.0	25.0		15.00	1.07	14	7.1
5.80	17.0	33.0		17.00	0.73	23	4.3
6.00	17.0	28.0		17.00	0.93	18	5.5
6.20	18.0	32.0		18.00	0.67	27	3.7
6.40	30.0	40.0		30.00	1.07	28	3.6
6.60	12.0	28.0		12.00	0.80	15	6.7
6.80	19.0	31.0		19.00	0.93	20	4.9
7.00	17.0	31.0		17.00	1.40	12	8.2
7.20	13.0	34.0		13.00	0.93	14	7.2
7.40	15.0	29.0		15.00	1.20	13	8.0
7.60	18.0	36.0		18.00	1.20	15	6.7
7.80	24.0	42.0		24.00	1.47	16	6.1
8.00	18.0	40.0		18.00	1.27	14	7.1
8.20	10.0	29.0		10.00	0.73	14	7.3
8.40	12.0	23.0		12.00	0.73	16	6.1
8.60	9.0	20.0		9.00	0.53	17	5.9
8.80	9.0	17.0		9.00	0.47	19	5.2
9.00	8.0	15.0		8.00	0.33	24	4.1
9.20	7.0	12.0		7.00	0.27	26	3.9
9.40	11.0	15.0		11.00	0.80	14	7.3
9.60	9.0	21.0		9.00	0.60	15	6.7
9.80	21.0	30.0		21.00	0.60	35	2.9
10.00	23.0	32.0		23.00	0.67	34	2.9
10.20	16.0	26.0		16.00	0.73	22	4.6
10.40	24.0	35.0		24.00	0.67	36	2.8
10.60	22.0	32.0		22.00	0.47	47	2.1
10.80	23.0	30.0		23.00	0.60	38	2.6
11.00	13.0	22.0		13.00	0.80	16	6.2
11.20	11.0	23.0		11.00	0.93	12	8.5
11.40	14.0	28.0		14.00	0.80	18	5.7
11.60	12.0	24.0		12.00	1.00	12	8.3
11.80	11.0	26.0		11.00	1.00	11	9.1
12.00	13.0	28.0		13.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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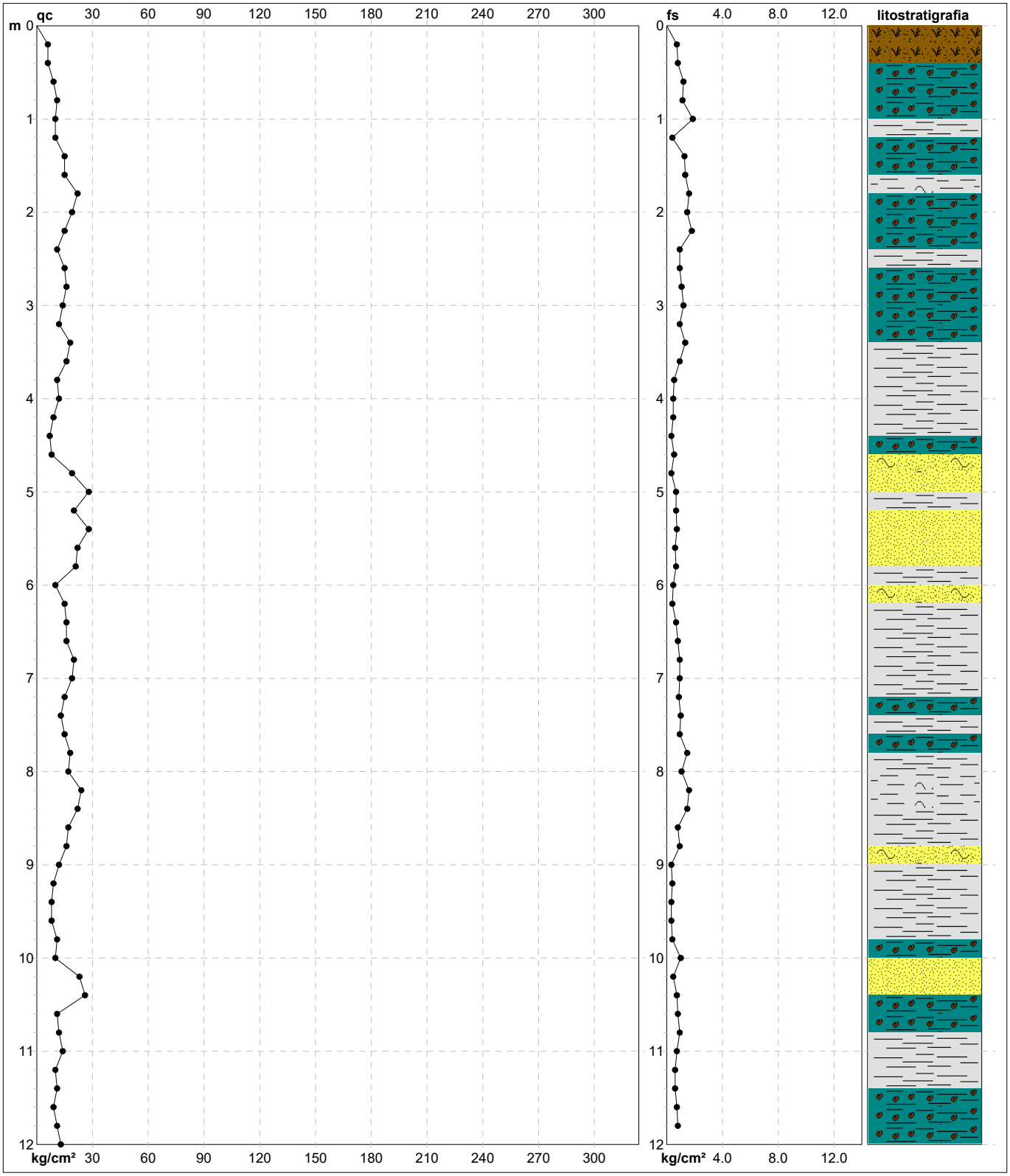
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	14
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:60	
Località:	**Sala Bolognese (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	14
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	6.0	13.0		6.00	0.73	8	12.2
0.40	6.0	17.0		6.00	0.80	8	13.3
0.60	9.0	21.0		9.00	1.20	8	13.3
0.80	11.0	29.0		11.00	1.13	10	10.3
1.00	10.0	27.0		10.00	1.87	5	18.7
1.20	10.0	38.0		10.00	0.40	25	4.0
1.40	15.0	21.0		15.00	1.27	12	8.5
1.60	15.0	34.0		15.00	1.33	11	8.9
1.80	22.0	42.0		22.00	1.60	14	7.3
2.00	19.0	43.0		19.00	1.47	13	7.7
2.20	15.0	37.0		15.00	1.80	8	12.0
2.40	11.0	38.0		11.00	0.93	12	8.5
2.60	15.0	29.0		15.00	0.93	16	6.2
2.80	16.0	30.0		16.00	1.07	15	6.7
3.00	14.0	30.0		14.00	1.20	12	8.6
3.20	12.0	30.0		12.00	0.93	13	7.8
3.40	18.0	32.0		18.00	1.33	14	7.4
3.60	16.0	36.0		16.00	0.93	17	5.8
3.80	11.0	25.0		11.00	0.53	21	4.8
4.00	12.0	20.0		12.00	0.47	26	3.9
4.20	9.0	16.0		9.00	0.47	19	5.2
4.40	7.0	14.0		7.00	0.33	21	4.7
4.60	8.0	13.0		8.00	0.53	15	6.6
4.80	19.0	27.0		19.00	0.33	58	1.7
5.00	28.0	33.0		28.00	0.67	42	2.4
5.20	20.0	30.0		20.00	0.67	30	3.4
5.40	28.0	38.0		28.00	0.73	38	2.6
5.60	22.0	33.0		22.00	0.60	37	2.7
5.80	21.0	30.0		21.00	0.67	31	3.2
6.00	10.0	20.0		10.00	0.47	21	4.7
6.20	15.0	22.0		15.00	0.40	38	2.7
6.40	16.0	22.0		16.00	0.67	24	4.2
6.60	16.0	26.0		16.00	0.80	20	5.0
6.80	20.0	32.0		20.00	0.93	22	4.7
7.00	19.0	33.0		19.00	0.93	20	4.9
7.20	15.0	29.0		15.00	0.87	17	5.8
7.40	13.0	26.0		13.00	1.00	13	7.7
7.60	15.0	30.0		15.00	0.93	16	6.2
7.80	18.0	32.0		18.00	1.47	12	8.2
8.00	17.0	39.0		17.00	1.07	16	6.3
8.20	24.0	40.0		24.00	1.60	15	6.7
8.40	22.0	46.0		22.00	1.47	15	6.7
8.60	17.0	39.0		17.00	0.80	21	4.7
8.80	16.0	28.0		16.00	0.93	17	5.8
9.00	12.0	26.0		12.00	0.33	36	2.8
9.20	9.0	14.0		9.00	0.40	23	4.4
9.40	8.0	14.0		8.00	0.33	24	4.1
9.60	8.0	13.0		8.00	0.33	24	4.1
9.80	11.0	16.0		11.00	0.40	28	3.6
10.00	10.0	16.0		10.00	1.00	10	10.0
10.20	23.0	38.0		23.00	0.47	49	2.0
10.40	26.0	33.0		26.00	0.73	36	2.8
10.60	11.0	22.0		11.00	0.80	14	7.3
10.80	12.0	24.0		12.00	0.93	13	7.8
11.00	14.0	28.0		14.00	0.73	19	5.2
11.20	10.0	21.0		10.00	0.60	17	6.0
11.40	11.0	20.0		11.00	0.60	18	5.5
11.60	9.0	18.0		9.00	0.73	12	8.1
11.80	11.0	22.0		11.00	0.80	14	7.3
12.00	13.0	25.0		13.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota: FON053

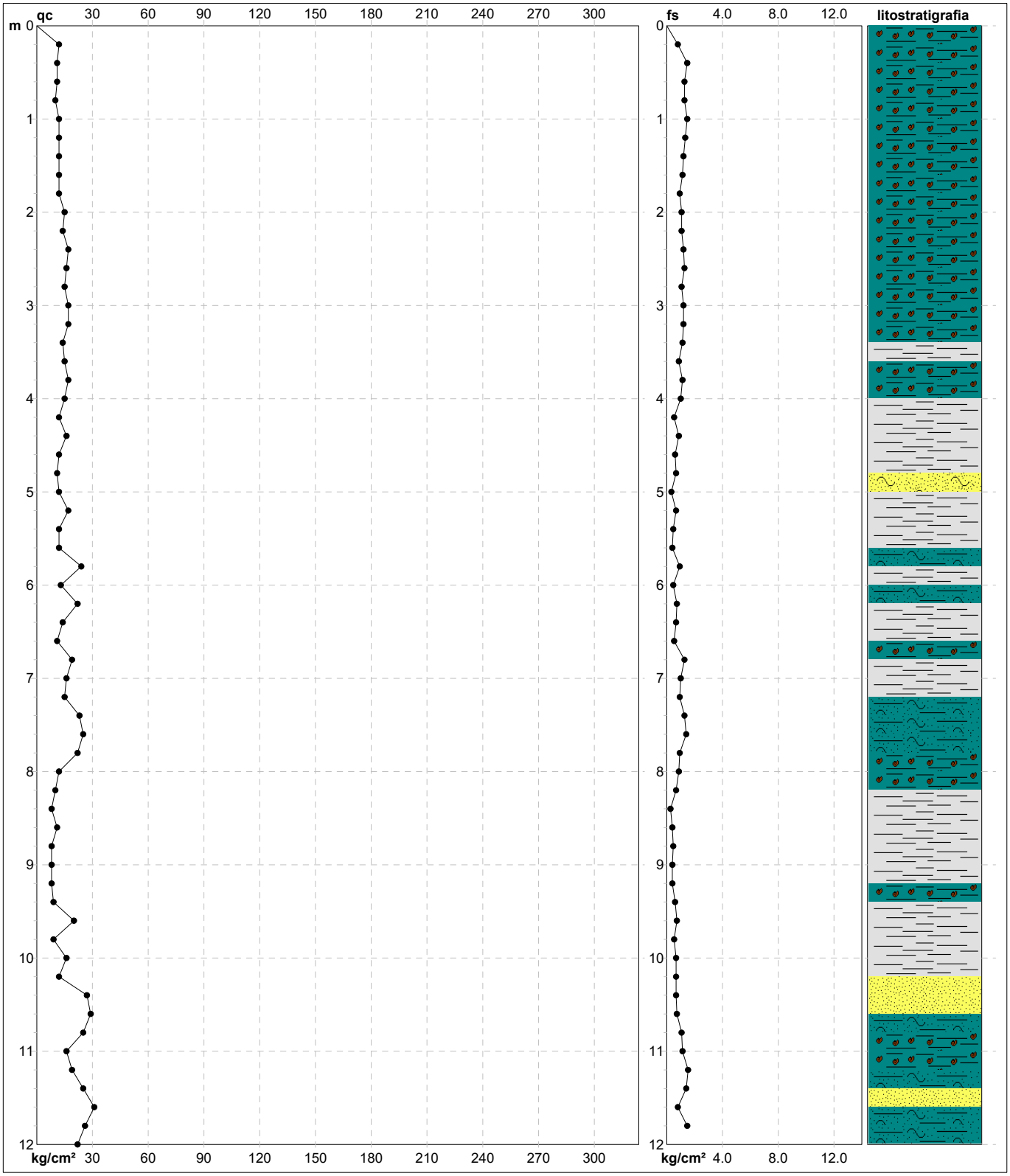
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	15
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:60	
Località:	**Sala Bolognese (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	15
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	12.0	20.0		12.00	0.80	15	6.7
0.40	11.0	23.0		11.00	1.47	7	13.4
0.60	11.0	33.0		11.00	1.27	9	11.5
0.80	10.0	29.0		10.00	1.27	8	12.7
1.00	12.0	31.0		12.00	1.47	8	12.3
1.20	12.0	34.0		12.00	1.33	9	11.1
1.40	12.0	32.0		12.00	1.20	10	10.0
1.60	12.0	30.0		12.00	1.13	11	9.4
1.80	12.0	29.0		12.00	0.93	13	7.8
2.00	15.0	29.0		15.00	1.07	14	7.1
2.20	14.0	30.0		14.00	1.07	13	7.6
2.40	17.0	33.0		17.00	1.20	14	7.1
2.60	16.0	34.0		16.00	1.27	13	7.9
2.80	15.0	34.0		15.00	1.07	14	7.1
3.00	17.0	33.0		17.00	1.20	14	7.1
3.20	17.0	35.0		17.00	1.20	14	7.1
3.40	14.0	32.0		14.00	1.13	12	8.1
3.60	15.0	32.0		15.00	0.87	17	5.8
3.80	17.0	30.0		17.00	1.13	15	6.6
4.00	15.0	32.0		15.00	1.00	15	6.7
4.20	12.0	27.0		12.00	0.53	23	4.4
4.40	16.0	24.0		16.00	0.87	18	5.4
4.60	12.0	25.0		12.00	0.60	20	5.0
4.80	11.0	20.0		11.00	0.67	16	6.1
5.00	12.0	22.0		12.00	0.33	36	2.8
5.20	17.0	22.0		17.00	0.67	25	3.9
5.40	12.0	22.0		12.00	0.47	26	3.9
5.60	12.0	19.0		12.00	0.40	30	3.3
5.80	24.0	30.0		24.00	0.93	26	3.9
6.00	13.0	27.0		13.00	0.47	28	3.6
6.20	22.0	29.0		22.00	0.73	30	3.3
6.40	14.0	25.0		14.00	0.67	21	4.8
6.60	11.0	21.0		11.00	0.53	21	4.8
6.80	19.0	27.0		19.00	1.27	15	6.7
7.00	16.0	35.0		16.00	1.00	16	6.3
7.20	15.0	30.0		15.00	0.93	16	6.2
7.40	23.0	37.0		23.00	1.27	18	5.5
7.60	25.0	44.0		25.00	1.40	18	5.6
7.80	22.0	43.0		22.00	0.93	24	4.2
8.00	12.0	26.0		12.00	0.87	14	7.3
8.20	10.0	23.0		10.00	0.67	15	6.7
8.40	8.0	18.0		8.00	0.27	30	3.4
8.60	11.0	15.0		11.00	0.40	28	3.6
8.80	8.0	14.0		8.00	0.47	17	5.9
9.00	8.0	15.0		8.00	0.40	20	5.0
9.20	8.0	14.0		8.00	0.40	20	5.0
9.40	9.0	15.0		9.00	0.60	15	6.7
9.60	20.0	29.0		20.00	0.73	27	3.7
9.80	9.0	20.0		9.00	0.53	17	5.9
10.00	16.0	24.0		16.00	0.67	24	4.2
10.20	12.0	22.0		12.00	0.67	18	5.6
10.40	27.0	37.0		27.00	0.67	40	2.5
10.60	29.0	39.0		29.00	0.73	40	2.5
10.80	25.0	36.0		25.00	1.07	23	4.3
11.00	16.0	32.0		16.00	1.13	14	7.1
11.20	19.0	36.0		19.00	1.53	12	8.1
11.40	25.0	48.0		25.00	1.40	18	5.6
11.60	31.0	52.0		31.00	0.80	39	2.6
11.80	26.0	38.0		26.00	1.47	18	5.7
12.00	22.0	44.0		22.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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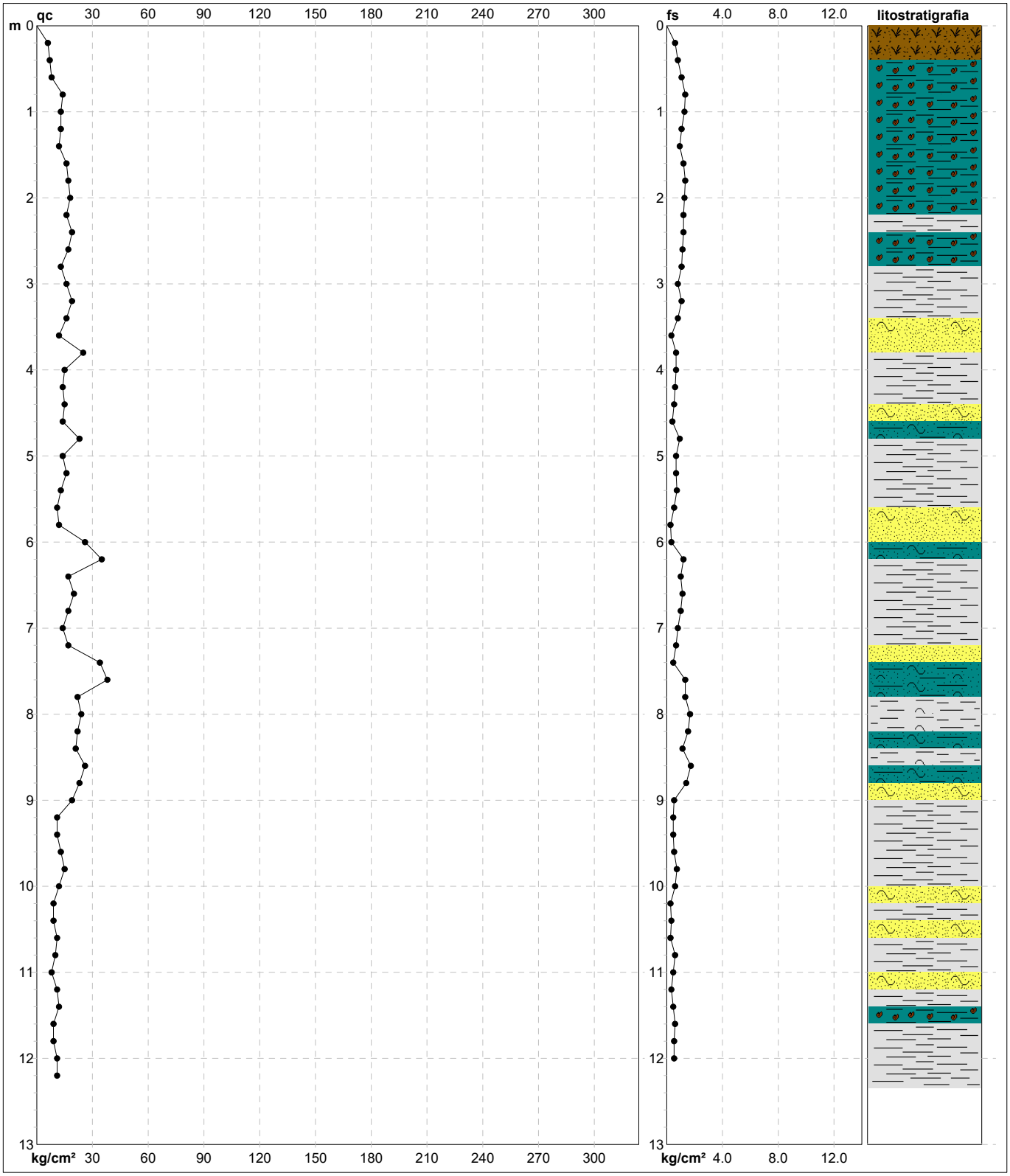
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI DI RESISTENZA E LITOLOGIA

CPT	16
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 25/11/2024
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:65	
Località:	**Sala Bolognese (BO)**	Pagina: 1	Quota inizio: Piano Campagna
		Elaborato:	Falda: Non rilevata



Litologia:	Begemann [qc + qc/fs] 4 Zone	Preforo:	m
Penetrometro:	TG63-200	Corr.astine:	kg/ml
Responsabile:	Dott. Geol. Maurizio Zamboni	Cod.ISTAT:	037050
Assistente:		Cod. punta:	

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
LETTURE CAMPAGNA E VALORI TRASFORMATI

CPT	16
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 25/11/2024
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %
0.20	6.0	12.0		6.00	0.60	10	10.0
0.40	7.0	16.0		7.00	0.80	9	11.4
0.60	8.0	20.0		8.00	1.07	7	13.4
0.80	14.0	30.0		14.00	1.33	11	9.5
1.00	13.0	33.0		13.00	1.27	10	9.8
1.20	13.0	32.0		13.00	1.07	12	8.2
1.40	12.0	28.0		12.00	0.93	13	7.8
1.60	16.0	30.0		16.00	1.20	13	7.5
1.80	17.0	35.0		17.00	1.33	13	7.8
2.00	18.0	38.0		18.00	1.27	14	7.1
2.20	16.0	35.0		16.00	1.20	13	7.5
2.40	19.0	37.0		19.00	1.20	16	6.3
2.60	17.0	35.0		17.00	1.13	15	6.6
2.80	13.0	30.0		13.00	1.07	12	8.2
3.00	16.0	32.0		16.00	0.80	20	5.0
3.20	19.0	31.0		19.00	1.07	18	5.6
3.40	16.0	32.0		16.00	0.80	20	5.0
3.60	12.0	24.0		12.00	0.33	36	2.8
3.80	25.0	30.0		25.00	0.67	37	2.7
4.00	15.0	25.0		15.00	0.67	22	4.5
4.20	14.0	24.0		14.00	0.60	23	4.3
4.40	15.0	24.0		15.00	0.53	28	3.5
4.60	14.0	22.0		14.00	0.40	35	2.9
4.80	23.0	29.0		23.00	0.93	25	4.0
5.00	14.0	28.0		14.00	0.67	21	4.8
5.20	16.0	26.0		16.00	0.67	24	4.2
5.40	13.0	23.0		13.00	0.73	18	5.6
5.60	11.0	22.0		11.00	0.53	21	4.8
5.80	12.0	20.0		12.00	0.27	44	2.3
6.00	26.0	30.0		26.00	0.33	79	1.3
6.20	35.0	40.0		35.00	1.20	29	3.4
6.40	17.0	35.0		17.00	1.00	17	5.9
6.60	20.0	35.0		20.00	1.13	18	5.7
6.80	17.0	34.0		17.00	1.00	17	5.9
7.00	14.0	29.0		14.00	0.80	18	5.7
7.20	17.0	29.0		17.00	0.67	25	3.9
7.40	34.0	44.0		34.00	0.47	72	1.4
7.60	38.0	45.0		38.00	1.33	29	3.5
7.80	22.0	42.0		22.00	1.33	17	6.0
8.00	24.0	44.0		24.00	1.67	14	7.0
8.20	22.0	47.0		22.00	1.53	14	7.0
8.40	21.0	44.0		21.00	1.13	19	5.4
8.60	26.0	43.0		26.00	1.73	15	6.7
8.80	23.0	49.0		23.00	1.40	16	6.1
9.00	19.0	40.0		19.00	0.53	36	2.8
9.20	11.0	19.0		11.00	0.47	23	4.3
9.40	11.0	18.0		11.00	0.47	23	4.3
9.60	13.0	20.0		13.00	0.53	25	4.1
9.80	15.0	23.0		15.00	0.73	21	4.9
10.00	12.0	23.0		12.00	0.60	20	5.0
10.20	9.0	18.0		9.00	0.27	33	3.0
10.40	9.0	13.0		9.00	0.33	27	3.7
10.60	11.0	16.0		11.00	0.27	41	2.5
10.80	10.0	14.0		10.00	0.60	17	6.0
11.00	8.0	17.0		8.00	0.47	17	5.9
11.20	11.0	18.0		11.00	0.33	33	3.0
11.40	12.0	17.0		12.00	0.47	26	3.9
11.60	9.0	16.0		9.00	0.60	15	6.7
11.80	9.0	18.0		9.00	0.53	17	5.9
12.00	11.0	19.0		11.00	0.53	21	4.8
12.20	11.0	19.0		11.00			

H m	L1 -	L2 -	Lt -	qc kg/cm²	fs kg/cm²	F -	Rf %

H = profondità
L1 = prima lettura (punta)
L2 = seconda lettura (punta + laterale)
Lt = terza lettura (totale)
CT =10.00 costante di trasformazione

qc = resistenza di punta
fs = resistenza laterale calcolata alla stessa quota di qc
F = rapporto Begemann (qc / fs)
Rf = rapporto Schmertmann (fs / qc)*100

nota:

FON053

Software by dott. Geol. Diego Merlin 0425-840820

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LEGENDA VALUTAZIONI LITOLOGICHE CORRELAZIONI GENERALI

Valutazioni in base al rapporto: F = (qc / fs)
Begemann 1965 - Raccomandazioni A.G.I. 1977
Valide in via approssimata per terreni immersi in falda :

	F = qc / fs	NATURA LITOLOGICA	PROPRIETA'
	F ≤ 15 kg/cm²	TORBE ED ARGILLE ORGANICHE	COESIVE
15 kg/cm² <	F ≤ 30 kg/cm²	LIMI ED ARGILLE	COESIVE
30 kg/cm² <	F ≤ 60 kg/cm²	LIMI SABBIOSI E SABBIE LIMOSE	GRANULARI
	F > 60 kg/cm²	SABBIE E SABBIE CON GHIAIA	GRANULARI

Vengono inoltre riportate le valutazioni stratigrafiche fornite da Schmertmann (1978), ricavabili in base ai valori di qc e di FR = (fs / qc) % :

- AO = argilla organica e terreni misti
- Att = argilla (inorganica) molto tenera
- At = argilla (inorganica) tenera
- Am = argilla (inorganica) di media consistenza
- Ac = argilla (inorganica) consistente
- Acc = argilla (inorganica) molto consistente
- ASL = argilla sabbiosa e limosa
- SAL = sabbia e limo / sabbia e limo argilloso
- Ss = sabbia sciolta
- Sm = sabbia mediamente addensata
- Sd = sabbia densa o cementata
- SC = sabbia con molti fossili, calcareniti

Secondo Schmertmann il valore della resistenza laterale da usarsi, dovrebbe essere pari a:

- 1/3 ± - 1/2 di quello misurato , per depositi sabbiosi
- quello misurato (inalterato) , per depositi coesivi.

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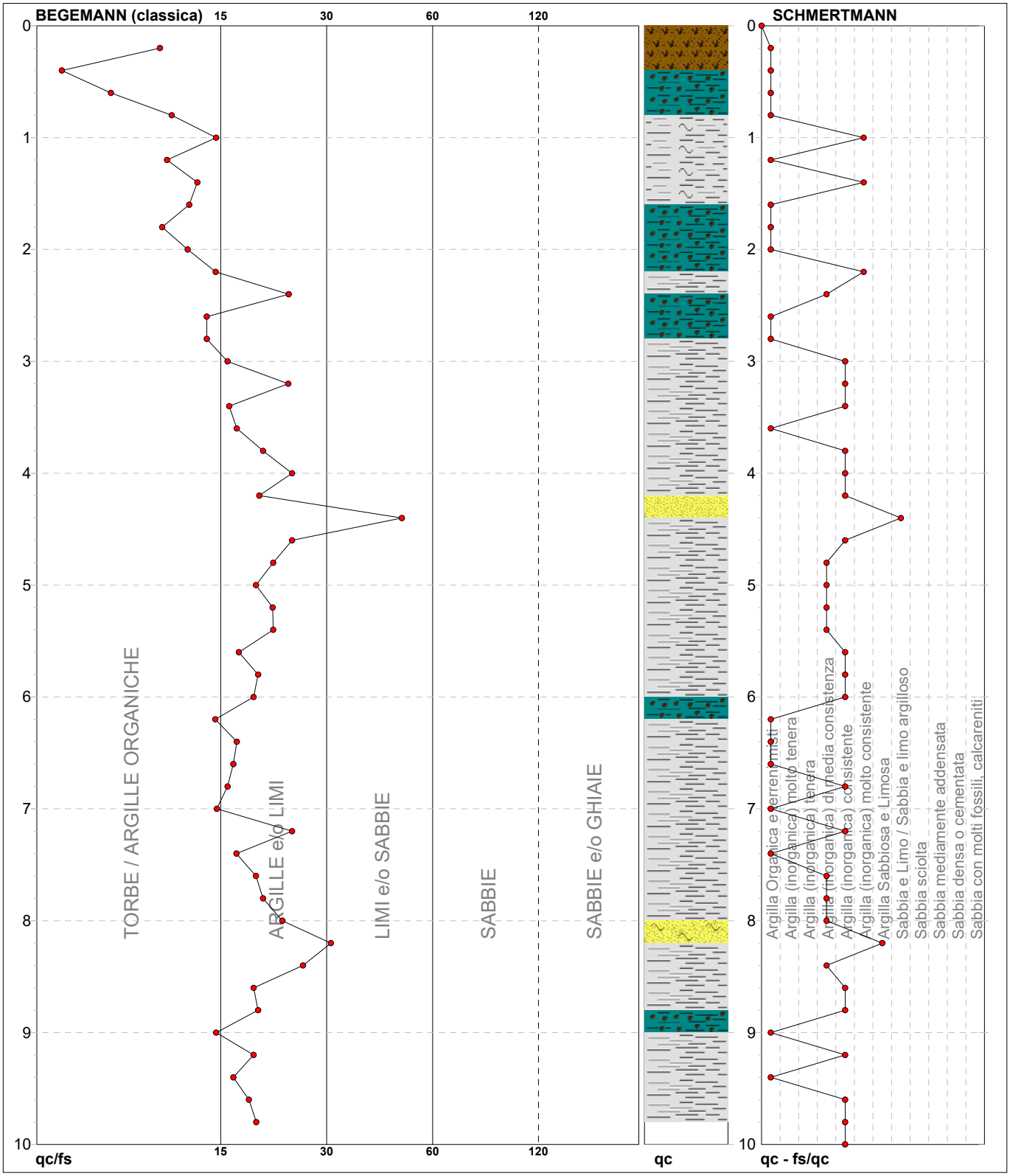
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	1
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	25/11/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:50		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	15 punti,	30.61%
Argille e/o Limi :	32 punti,	65.31%
Limi e/o Sabbie :	2 punti,	4.08%

Argilla Organica e terreni misti:	18 punti,	36.73%
Argilla (inorganica) media consist.:	9 punti,	18.37%
Argilla (inorganica) consistente:	17 punti,	34.69%
Argilla (inorganica) molto consist.:	3 punti,	6.12%
Argilla Sabbiosa e Limosa:	1 punti,	2.04%
Sabbia e Limo / Sabbia e limo arg.:	1 punti,	2.04%

nota:

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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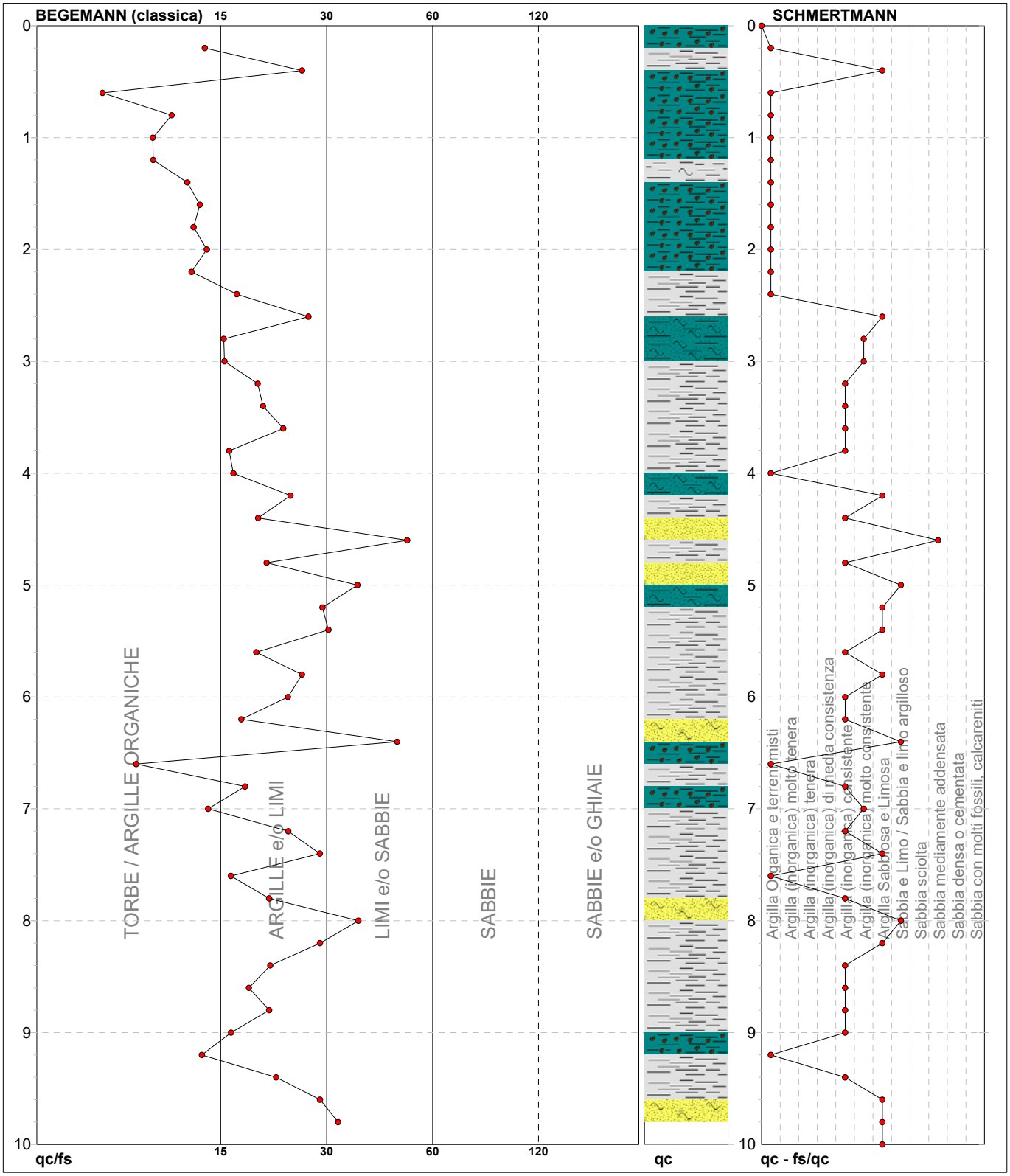
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	3
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:50		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	13 punti, 26.53%	Argilla Organica e terreni misti:	15 punti, 30.61%	Argilla Sabbiosa e Limosa:	10 punti, 20.41%
Argille e/o Limi :	31 punti, 63.27%	Argilla (inorganica) consistente:	17 punti, 34.69%	Sabbia e Limo / Sabbia e limo arg.:	3 punti, 6.12%
Limi e/o Sabbie :	5 punti, 10.20%	Argilla (inorganica) molto consist.:	3 punti, 6.12%	Sabbia mediamente addensata:	1 punti, 2.04%

nota: FON053

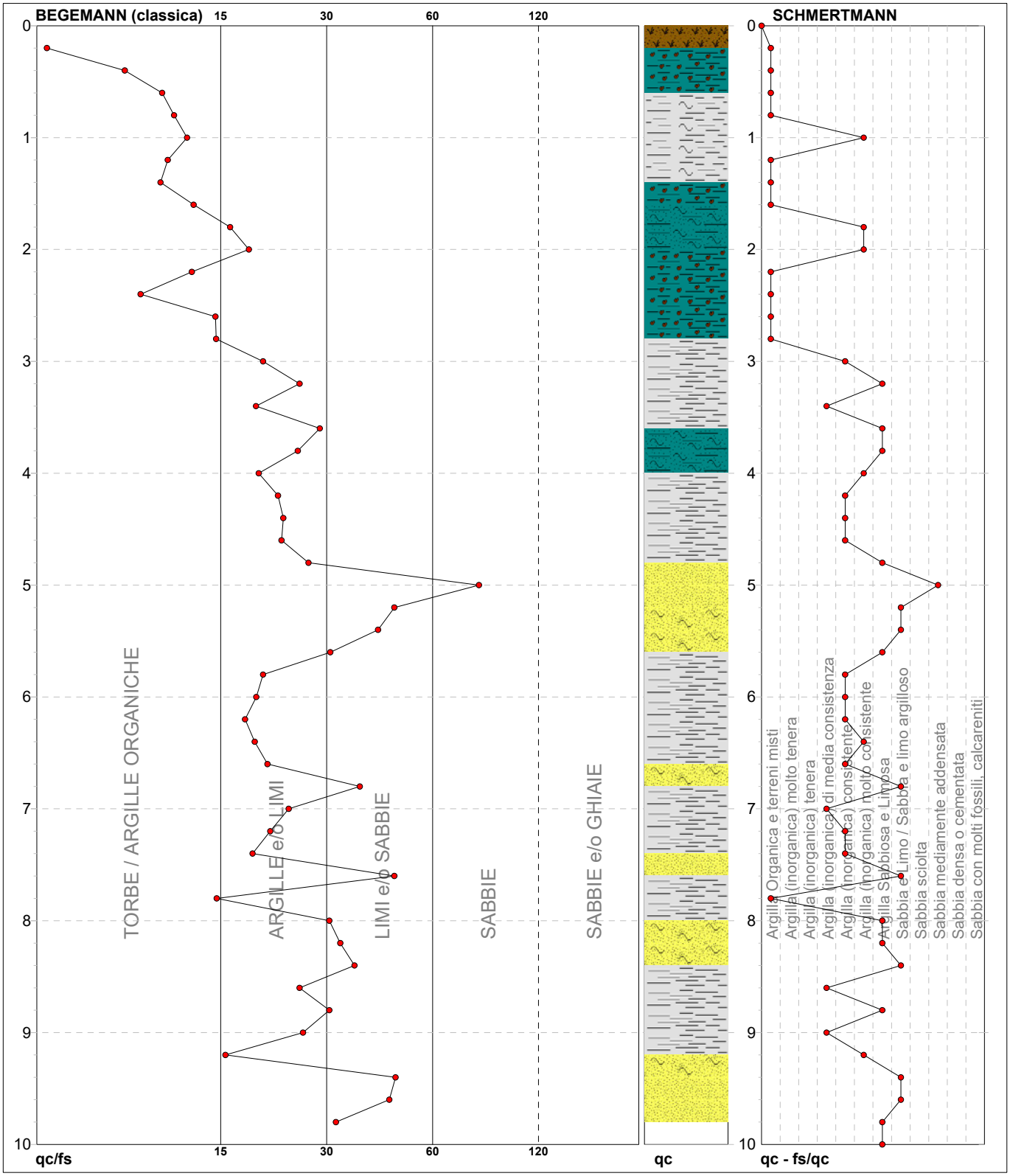
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	4
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:50		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	12 punti,	24.49%	Argilla Organica e terreni misti:	12 punti,	24.49%	Argilla Sabbiosa e Limosa:	9 punti, 18.37%
Argille e/o Limi :	26 punti,	53.06%	Argilla (inorganica) media consist.:	4 punti,	8.16%	Sabbia e Limo / Sabbia e limo arg.:	7 punti, 14.29%
Limi e/o Sabbie :	10 punti,	20.41%	Argilla (inorganica) consistente:	10 punti,	20.41%	Sabbia mediamente addensata:	1 punti, 2.04%
Sabbie:	1 punti,	2.04%	Argilla (inorganica) molto consist.:	6 punti,	12.24%		

nota: FON053

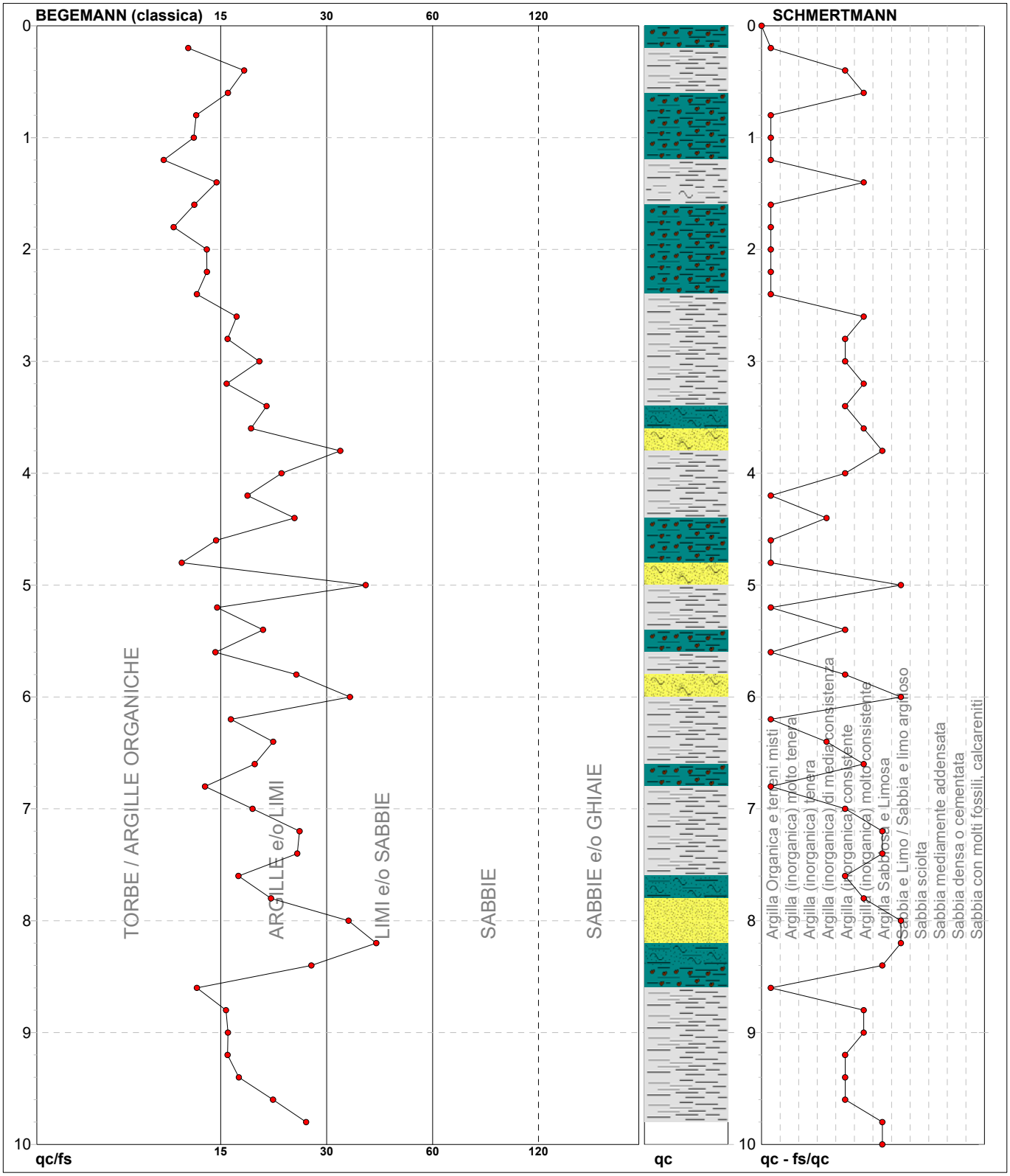
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	5
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.: kg/cm²	Data esec.: 08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala: 1:50	
Località:	Sala Bolognese (BO)	Pagina: 1	
		Elaborato:	Falda: Non rilevata



Torbe / Argille org. :	14 punti, 28.57%	Argilla Organica e terreni misti:	17 punti, 34.69%	Argilla Sabbiosa e Limosa:	5 punti, 10.20%
Argille e/o Limi :	30 punti, 61.22%	Argilla (inorganica) media consist.:	2 punti, 4.08%	Sabbia e Limo / Sabbia e limo arg.:	4 punti, 8.16%
Limi e/o Sabbie :	5 punti, 10.20%	Argilla (inorganica) consistente:	12 punti, 24.49%		
		Argilla (inorganica) molto consist.:	9 punti, 18.37%		

nota: FON053

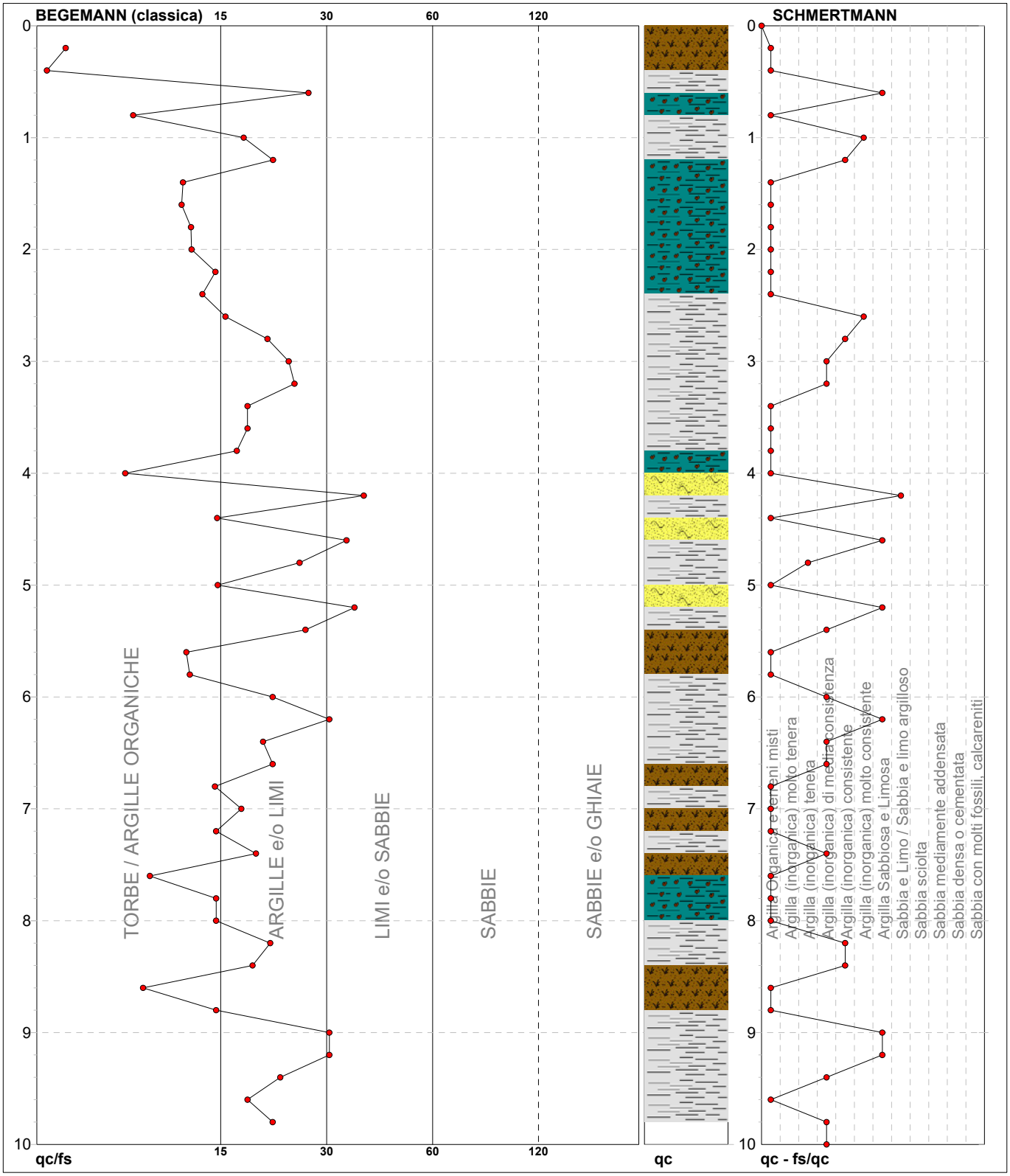
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	6
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:50		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	19 punti,	38.78%	Argilla Organica e terreni misti:	26 punti,	53.06%	Argilla Sabbiosa e Limosa:	6 punti, 12.24%
Argille e/o Limi :	27 punti,	55.10%	Argilla (inorganica) tenera:	1 punti,	2.04%	Sabbia e Limo / Sabbia e limo arg.:	1 punti, 2.04%
Limi e/o Sabbie :	3 punti,	6.12%	Argilla (inorganica) media consist.:	9 punti,	18.37%		
			Argilla (inorganica) consistente:	4 punti,	8.16%		
			Argilla (inorganica) molto consist.:	2 punti,	4.08%		

nota: FON053

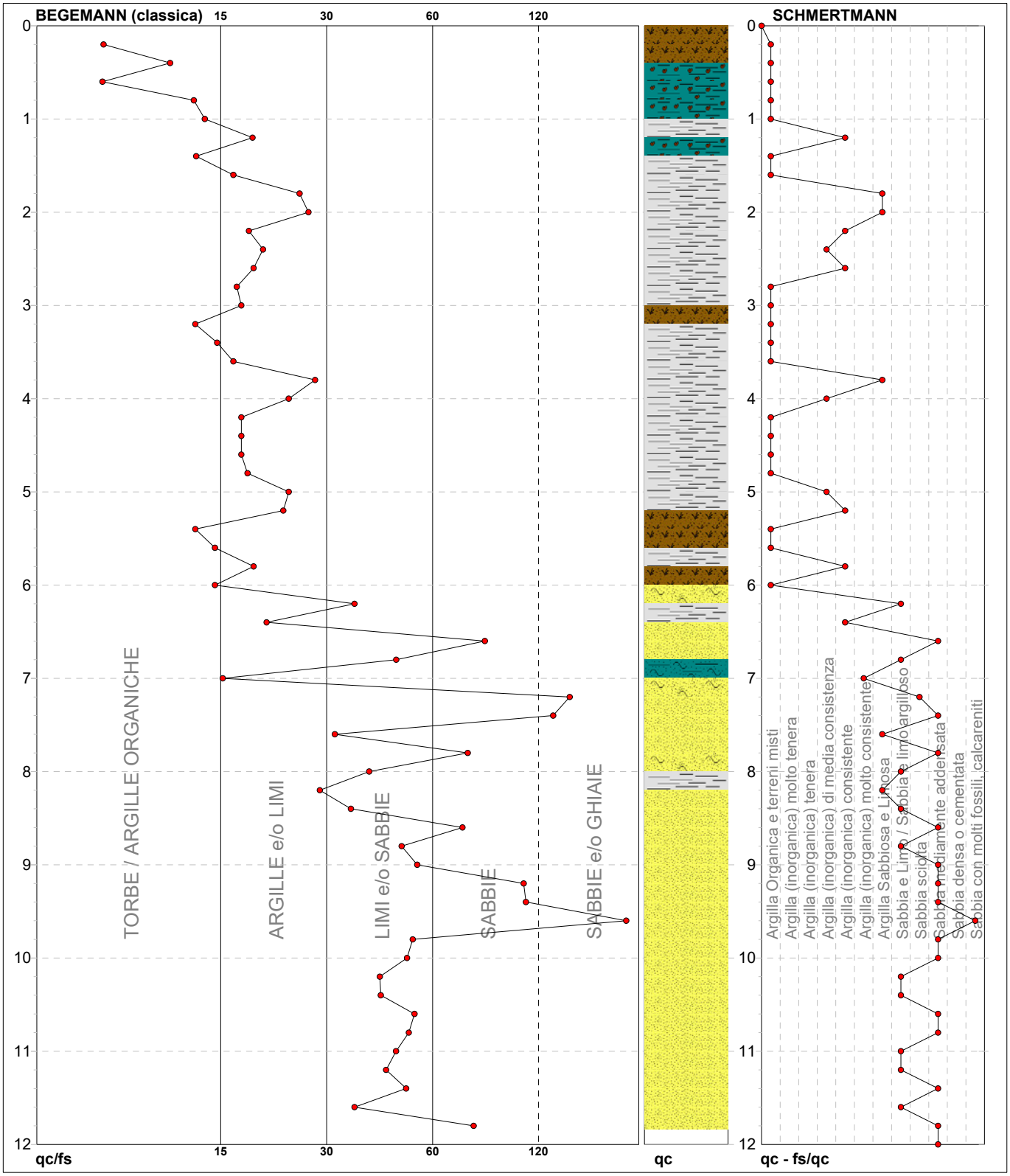
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	7
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:60		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	10 punti,	16.95%	Argilla Organica e terreni misti:	19 punti,	32.20%	Argilla Sabbiosa e Limosa:	5 punti, 8.47%
Argille e/o Limi :	23 punti,	38.98%	Argilla (inorganica) media consist.:	3 punti,	5.08%	Sabbia e Limo / Sabbia e limo arg.:	10 punti, 16.95%
Limi e/o Sabbie :	17 punti,	28.81%	Argilla (inorganica) consistente:	6 punti,	10.17%	Sabbia sciolta:	1 punti, 1.69%
Sabbie:	7 punti,	11.86%	Argilla (inorganica) molto consist.:	1 punti,	1.69%	Sabbia mediamente addensata:	13 punti, 22.03%
Sabbie e/o Ghiaie :	2 punti,	3.39%				Sabbia con molti fossili, calcareniti:	1 punti, 1.69%

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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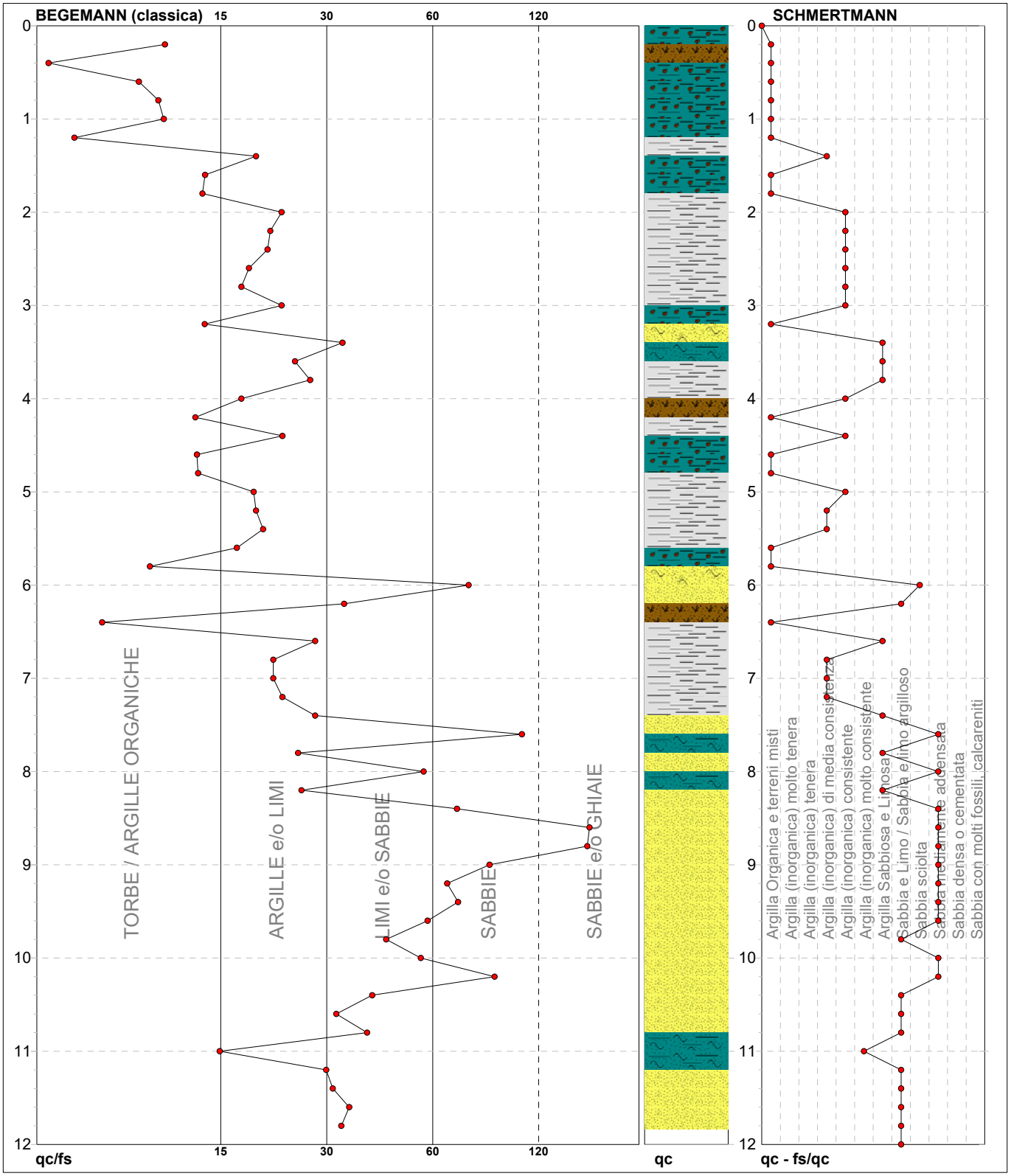
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	8
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:60		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	14 punti, 23.73%	Argilla Organica e terreni misti:	15 punti, 25.42%	Argilla Sabbiosa e Limosa:	7 punti, 11.86%
Argille e/o Limi :	24 punti, 40.68%	Argilla (inorganica) media consist.:	6 punti, 10.17%	Sabbia e Limo / Sabbia e limo arg.:	9 punti, 15.25%
Limi e/o Sabbie :	12 punti, 20.34%	Argilla (inorganica) consistente:	9 punti, 15.25%	Sabbia sciolta:	1 punti, 1.69%
Sabbie:	7 punti, 11.86%	Argilla (inorganica) molto consist.:	1 punti, 1.69%	Sabbia mediamente addensata:	11 punti, 18.64%
Sabbie e/o Ghiaie :	2 punti, 3.39%				

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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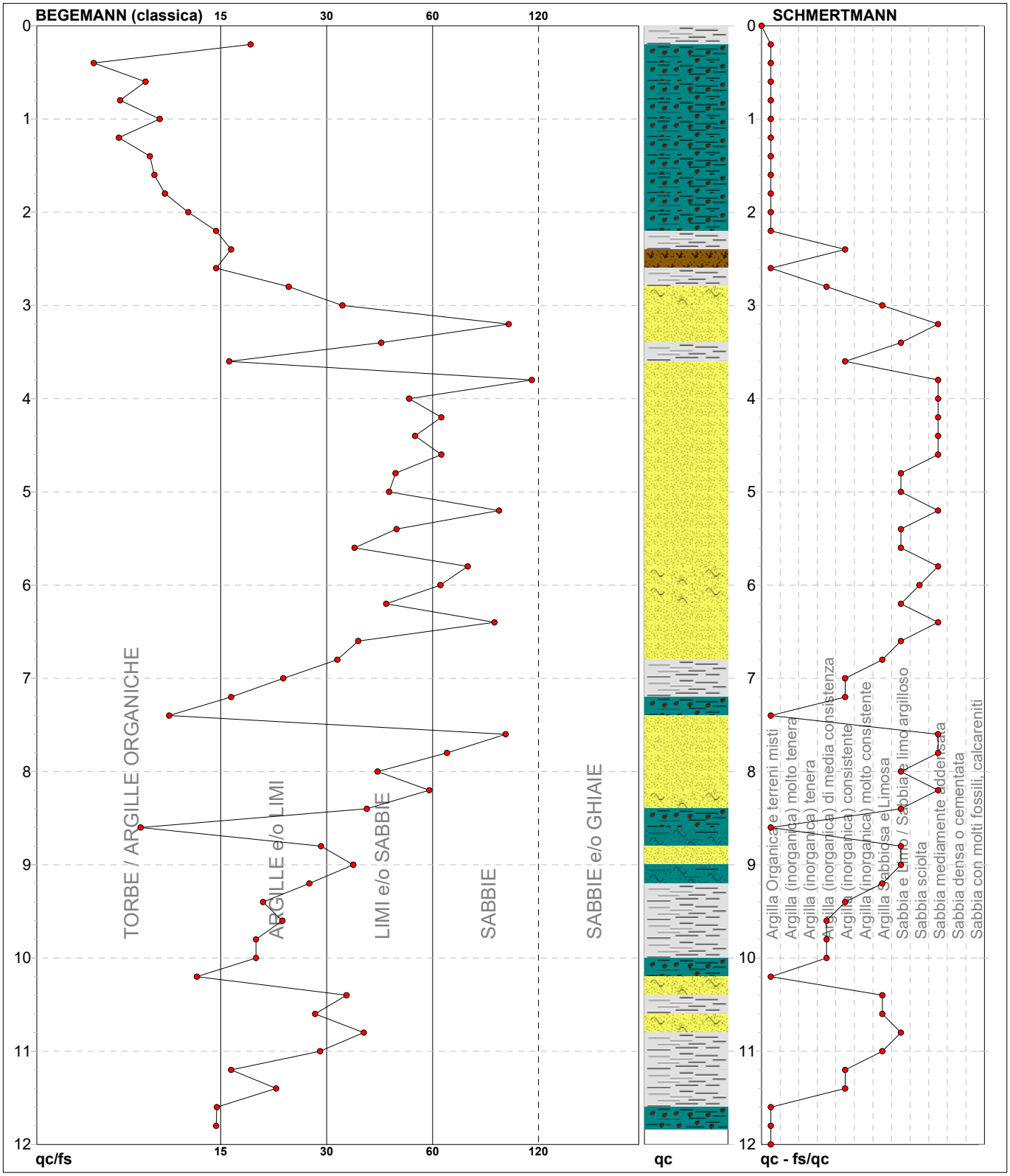
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	9
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:60		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	15 punti, 25.42%	Argilla Organica e terreni misti:	17 punti, 28.81%	Sabbia e Limo / Sabbia e limo arg.:	12 punti, 20.34%
Argille e/o Limi :	17 punti, 28.81%	Argilla (inorganica) media consist.:	4 punti, 6.78%	Sabbia sciolta:	1 punti, 1.69%
Limi e/o Sabbie :	20 punti, 33.90%	Argilla (inorganica) consistente:	7 punti, 11.86%	Sabbia mediamente addensata:	12 punti, 20.34%
Sabbie:	7 punti, 11.86%				

nota: FON053

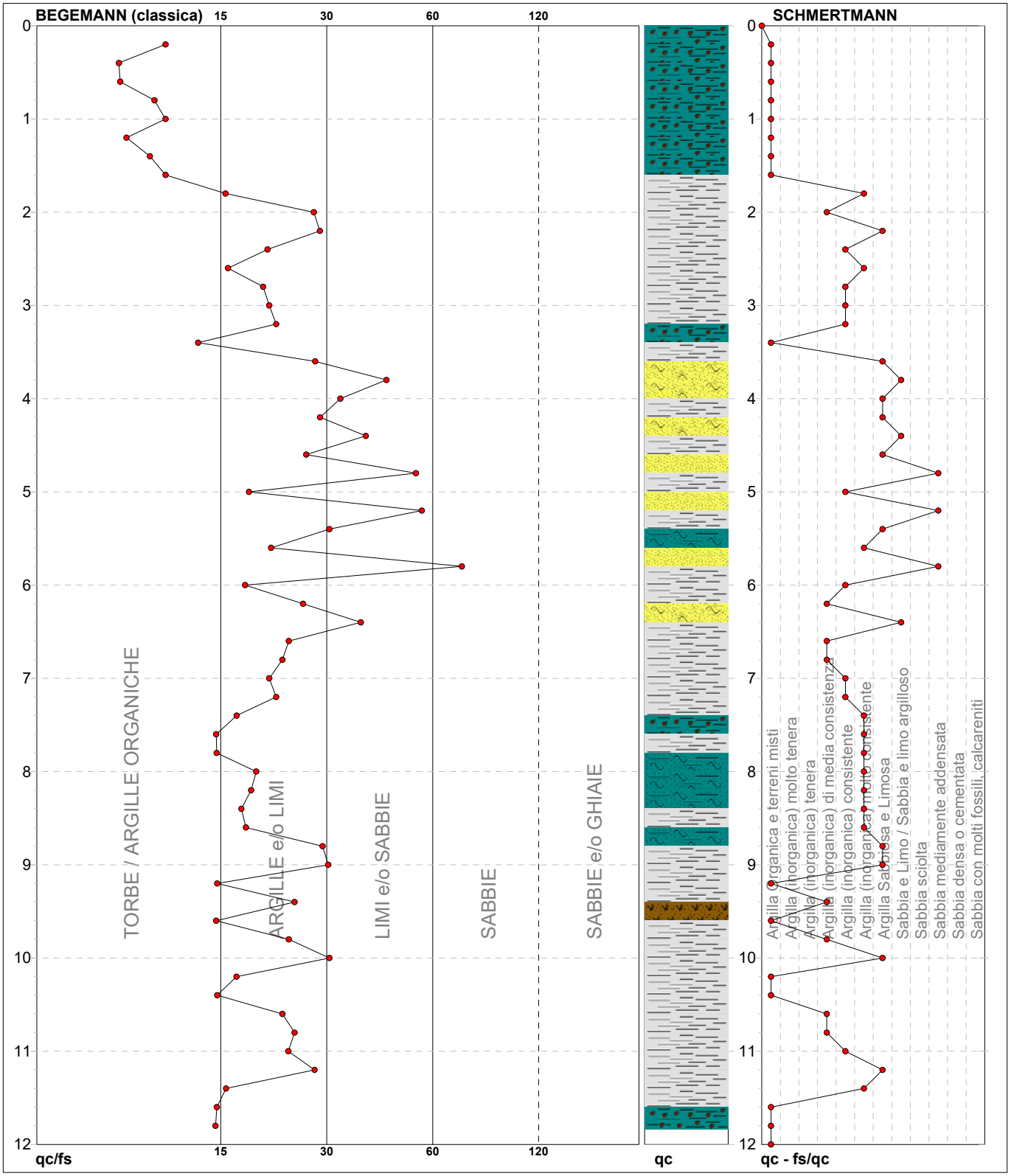
Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	10
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:60		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	12 punti,	20.34%	Argilla Organica e terreni misti:	15 punti,	25.42%	Argilla Sabbiosa e Limosa:	10 punti, 16.95%
Argille e/o Limi :	40 punti,	67.80%	Argilla (inorganica) media consist.:	8 punti,	13.56%	Sabbia e Limo / Sabbia e limo arg.:	3 punti, 5.08%
Limi e/o Sabbie :	6 punti,	10.17%	Argilla (inorganica) consistente:	9 punti,	15.25%	Sabbia mediamente addensata:	3 punti, 5.08%
Sabbie:	1 punti,	1.69%	Argilla (inorganica) molto consist.:	11 punti,	18.64%		

nota: FON053

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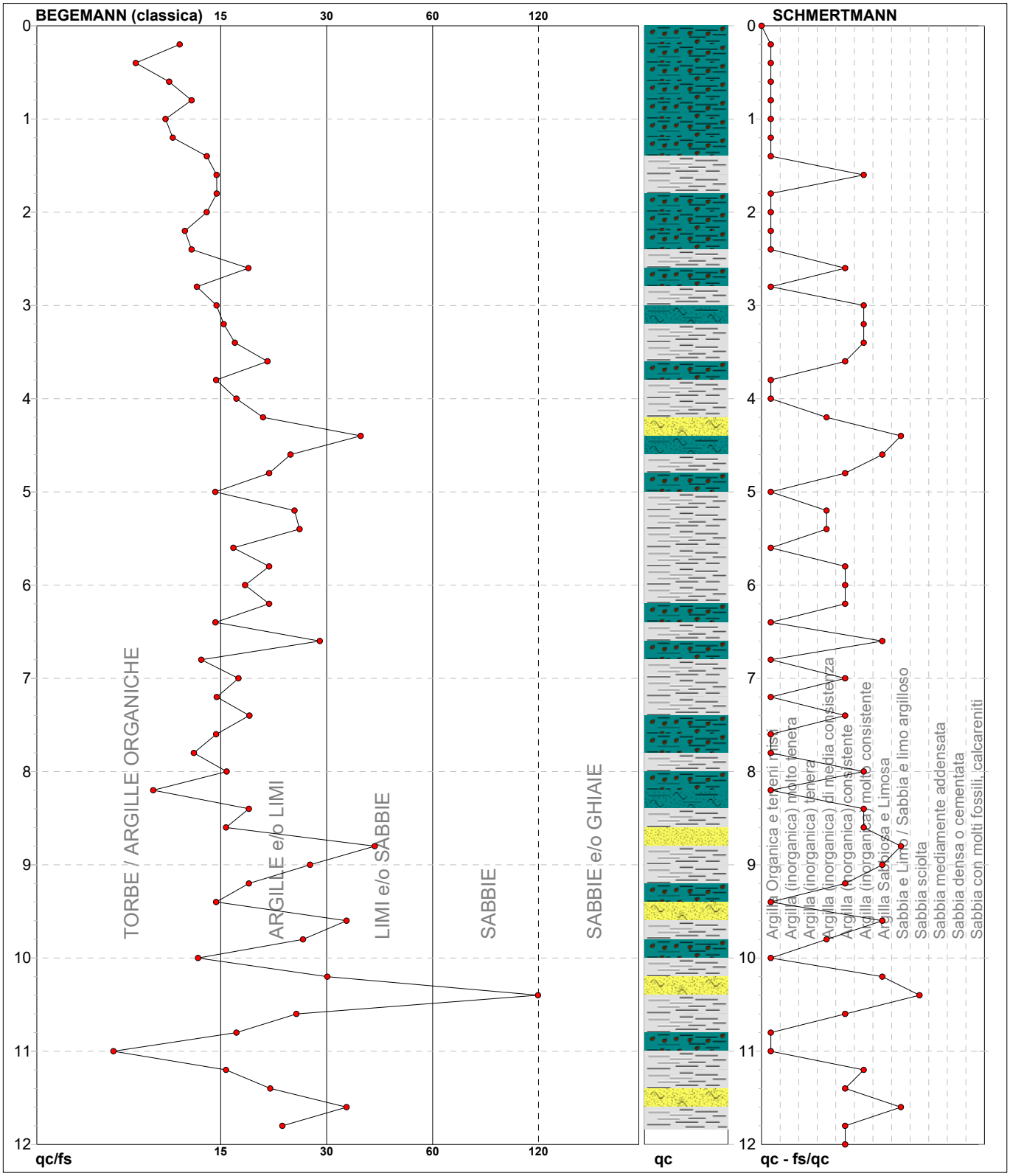
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	11
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:60		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	21 punti,	35.59%	Argilla Organica e terreni misti:	26 punti,	44.07%	Argilla Sabbiosa e Limosa:	5 punti, 8.47%
Argille e/o Limi :	33 punti,	55.93%	Argilla (inorganica) media consist.:	4 punti,	6.78%	Sabbia e Limo / Sabbia e limo arg.:	3 punti, 5.08%
Limi e/o Sabbie :	4 punti,	6.78%	Argilla (inorganica) consistente:	12 punti,	20.34%	Sabbia sciolta:	1 punti, 1.69%
Sabbie:	1 punti,	1.69%	Argilla (inorganica) molto consist.:	8 punti,	13.56%		

nota: FON053

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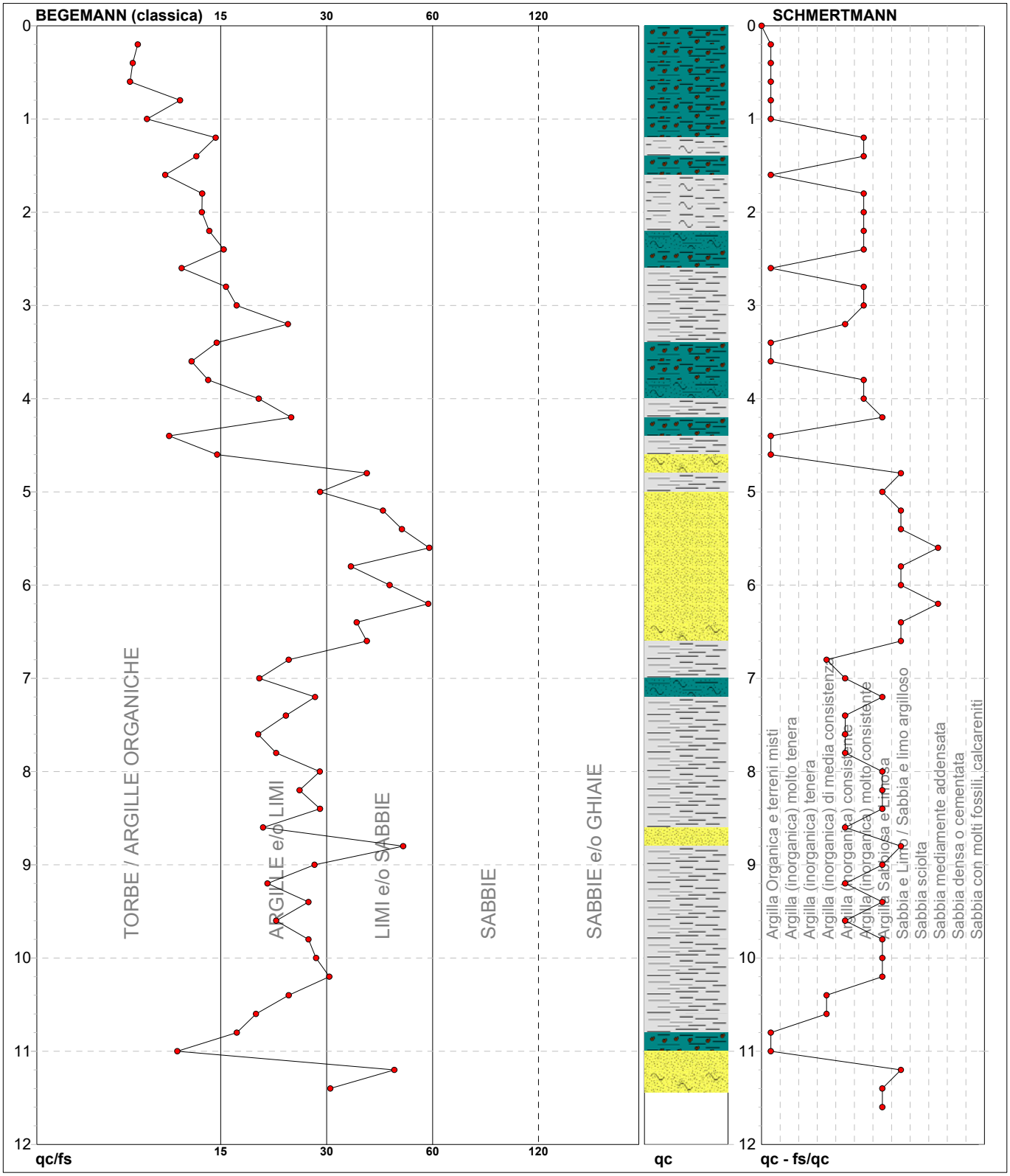
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	12
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:60		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	16 punti, 27.12%	Argilla Organica e terreni misti:	13 punti, 22.03%	Argilla Sabbiosa e Limosa:	12 punti, 20.34%
Argille e/o Limi :	29 punti, 49.15%	Argilla (inorganica) media consist.:	3 punti, 5.08%	Sabbia e Limo / Sabbia e limo arg.:	9 punti, 15.25%
Limi e/o Sabbie :	12 punti, 20.34%	Argilla (inorganica) consistente:	8 punti, 13.56%	Sabbia mediamente addensata:	2 punti, 3.39%
		Argilla (inorganica) molto consist.:	10 punti, 16.95%		

nota: FON053

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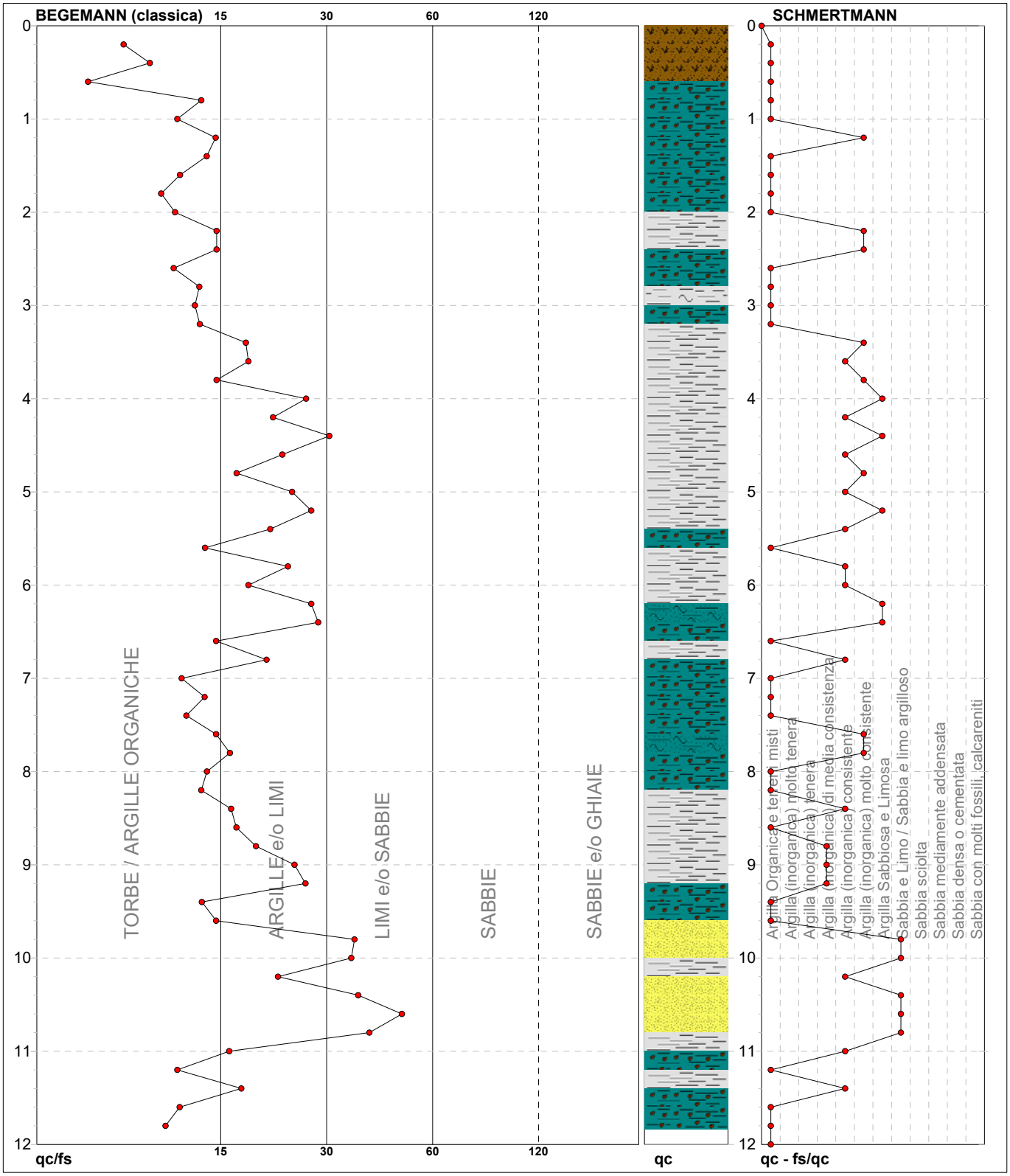
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	13
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:60		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	27 punti,	45.76%	Argilla Organica e terreni misti:	26 punti,	44.07%	Argilla Sabbiosa e Limosa:	5 punti, 8.47%
Argille e/o Limi :	27 punti,	45.76%	Argilla (inorganica) media consist.:	3 punti,	5.08%	Sabbia e Limo / Sabbia e limo arg.:	5 punti, 8.47%
Limi e/o Sabbie :	5 punti,	8.47%	Argilla (inorganica) consistente:	12 punti,	20.34%		
			Argilla (inorganica) molto consist.:	8 punti,	13.56%		

nota: FON053

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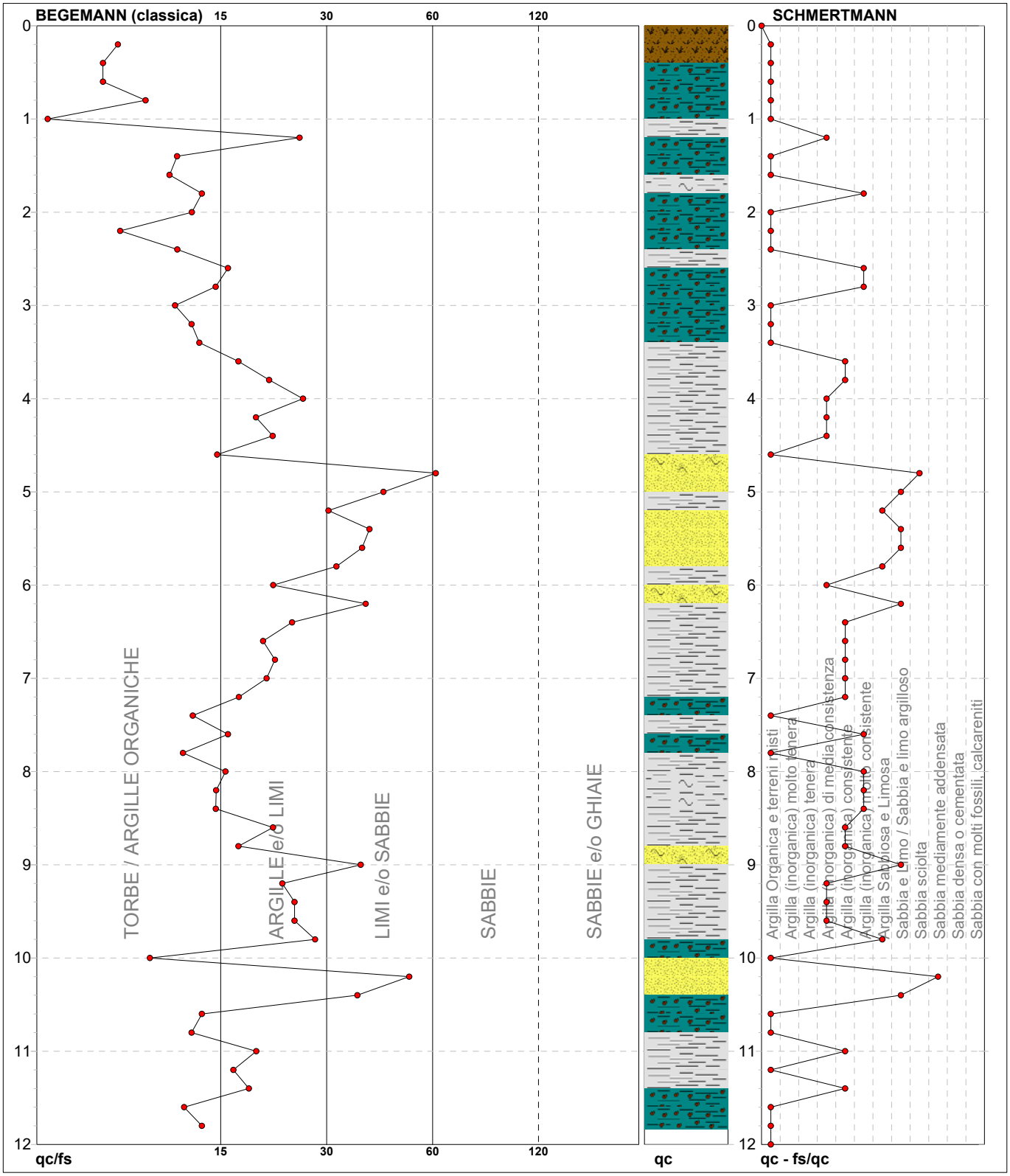
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	14
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	08/06/2007
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:60		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	24 punti, 40.68%	Argilla Organica e terreni misti:	22 punti, 37.29%	Argilla Sabbiosa e Limosa:	3 punti, 5.08%
Argille e/o Limi :	26 punti, 44.07%	Argilla (inorganica) media consist.:	8 punti, 13.56%	Sabbia e Limo / Sabbia e limo arg.:	6 punti, 10.17%
Limi e/o Sabbie :	9 punti, 15.25%	Argilla (inorganica) consistente:	11 punti, 18.64%	Sabbia sciolta:	1 punti, 1.69%
		Argilla (inorganica) molto consist.:	7 punti, 11.86%	Sabbia mediamente addensata:	1 punti, 1.69%

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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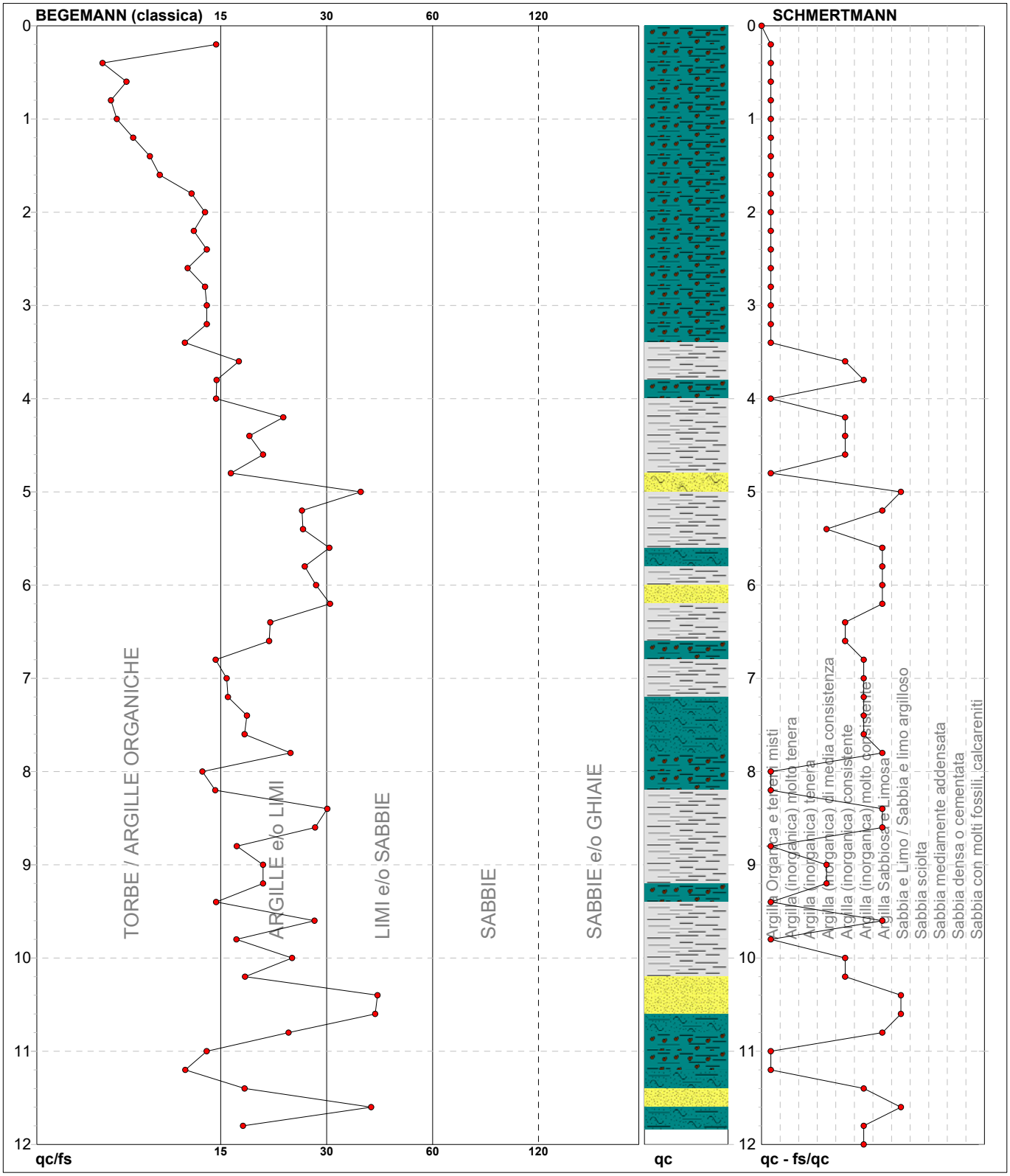
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	15
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Scala: 1:60	
Località:	**Sala Bolognese (BO)**	Pagina: 1	
		Elaborato:	Falda: Non rilevata



Torbe / Argille org. :	24 punti,	40.68%
Argille e/o Limi :	30 punti,	50.85%
Limi e/o Sabbie :	5 punti,	8.47%

Argilla Organica e terreni misti:	26 punti,	44.07%
Argilla (inorganica) media consist.:	3 punti,	5.08%
Argilla (inorganica) consistente:	8 punti,	13.56%
Argilla (inorganica) molto consist.:	8 punti,	13.56%
Argilla Sabbiosa e Limosa:	10 punti,	16.95%
Sabbia e Limo / Sabbia e limo arg.:	4 punti,	6.78%

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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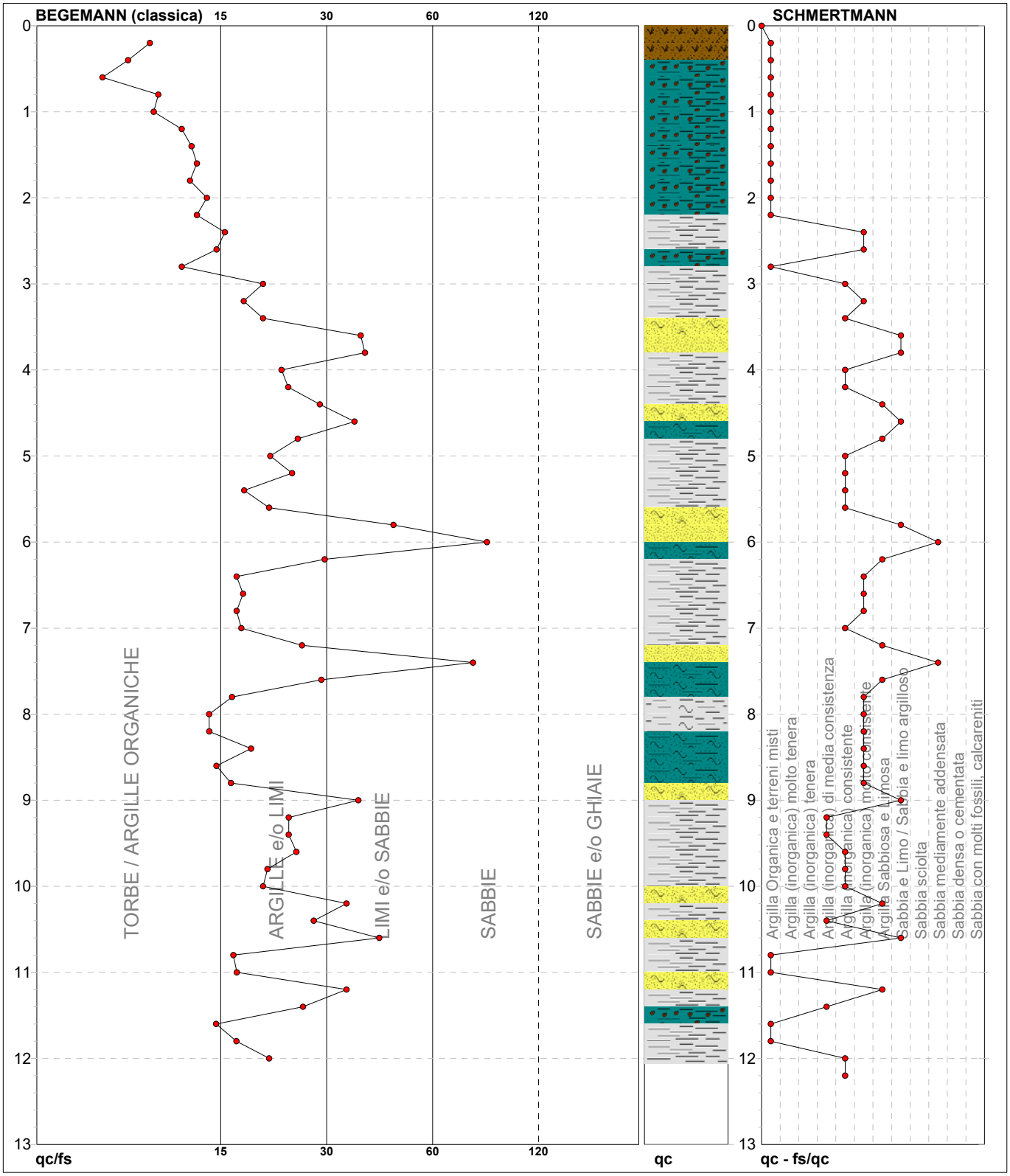
PROVA PENETROMETRICA STATICA MECCANICA
DIAGRAMMI LITOLOGIA

CPT	16
riferimento	78-2024

Committente:	GreenGo s.r.l.	U.M.:	kg/cm²	Data esec.:	25/11/2024
Cantiere:	Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´	Scala:	1:65		
Località:	Sala Bolognese (BO)	Pagina:	1		
		Elaborato:		Falda:	Non rilevata



Torbe / Argille org. :	15 punti, 23.44%	Argilla Organica e terreni misti:	16 punti, 25.00%	Argilla Sabbiosa e Limosa:	7 punti, 10.94%
Argille e/o Limi :	35 punti, 54.69%	Argilla (inorganica) media consist.:	4 punti, 6.25%	Sabbia e Limo / Sabbia e limo arg.:	6 punti, 9.38%
Limi e/o Sabbie :	8 punti, 12.50%	Argilla (inorganica) consistente:	13 punti, 20.31%	Sabbia mediamente addensata:	2 punti, 3.13%
Sabbie:	2 punti, 3.13%	Argilla (inorganica) molto consist.:	12 punti, 18.75%		

nota: FON053

Software by dott. Geol. Diego Merlin 0425-840820

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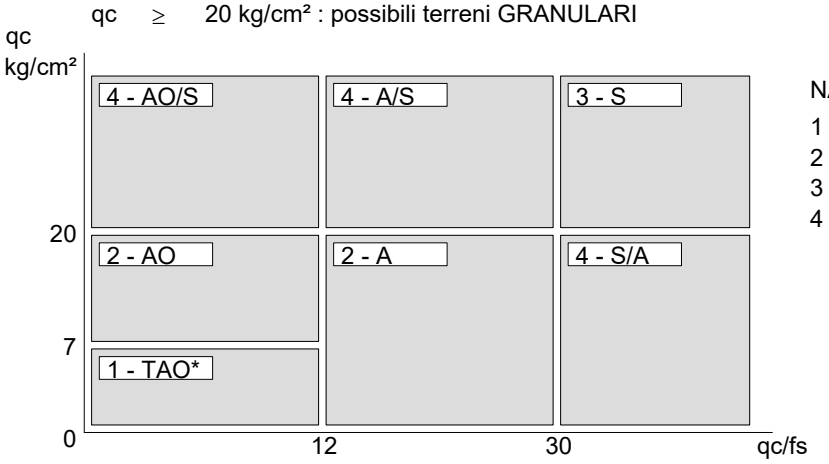
LEGENDA PARAMETRI GEOTECNICI
SPECIFICHE TECNICHE

Le scelte litologiche vengono effettuate in base al rapporto qc / fs (Begemann 1965 - A.G.I. 1977) prevedendo altresì la possibilità di casi dubbi :

qc ≤ 20 kg/cm² : possibili terreni COESIVI — anche se (qc / fs) > 30

qc ≥ 20 kg/cm² : possibili terreni GRANULARI — anche se (qc / fs) < 30



NATURA LITOLOGICA
1 - COESIVA (TORBOSA) ALTA COMPRIM.
2 - COESIVA IN GENERE
3 - GRANULARE
4 - COESIVA / GRANULARE

PARAMETRI GEOTECNICI (validità orientativa) - simboli - correlazioni - bibliografia

γ' = peso dell' unità di volume (efficace) del terreno [correlazioni : γ' - qc - natura]
(Terzaghi & Peck 1967 - Bowles 1982)

$\sigma'vo$ = tensione verticale geostatica (efficace) del terreno (valutata in base ai valori di γ')

Cu = coesione non drenata (terreni coesivi) [correlazioni : Cu - qc]

OCR = grado di sovra consolidazione (terreni coesivi) [correlazioni : OCR - Cu - σ 'vo]
(Ladd et al. 1972 / 1974 / 1977 - Lancellotta 1983)

Eu = modulo di deformazione non drenato (terreni coesivi) [correl. : Eu - Cu - OCR - Ip Ip= ind.plast.]
Eu50 - Eu25 corrispondono rispettivamente ad un grado di mobilitazione dello sforzo deviatorico pari al 50-25% (Duncan & Buchigani 1976)

E' = modulo di deformazione drenato (terreni granulari) [correlazioni : E' - qc]
E'50 - E'25 corrispondono rispettivamente ad un grado di mobilitazione dello sforzo deviatorico pari al 50-25% (coeff. di sicurezza F = 2 - 4 rispettivamente)
Schmertmann 1970 / 1978 - Jamiolkowski ed altri 1983)

Mo = modulo di deformazione edometrico (terreni coesivi e granulari) [correl. : Mo - qc - natura]
Sanglerat 1972 - Mitchell & Gardner 1975 - Ricceri et al. 1974 - Holden 1973)

Dr = densità relativa (terreni granulari N. C. - normalmente consolidati)
[correlazioni : Dr - Rp - σ 'vo (Schmertmann 1976)]

Ø' = angolo di attrito interno efficace (terreni granulari N.C.) [correl. : Ø' - Dr - qc σ 'vo)
ØCa - Caquot (1948) — ØKo - Koppejan (1948)
ØDB - De Beer (1965) — ØSc - Schmertmann (1978)
ØDM - Durgunoglu & Mitchell (1975) (sabbie N.C.) — ØMe - Meyerhof (1956 / 1976) (sabbie limose)

F.L. = fattore di liquefazione (F.L.s = Sabbie Pulite, F.L.l = Sabbie Limose)

Vs = velocità di propagazione delle onde sismiche (Iyisan 1996)

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PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT 1
riferimento **78-2024**

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 25/11/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	5.00	10.64	1	1.46	0.03	101	0.25	91.9	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	7.00	5.83	1	1.46	0.06	115	0.35	58.9	14.0	21.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	10.00	7.87	2	1.90	0.10	132	0.50	49.1	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
0.80	16.00	11.43	2	1.96	0.14	157	0.70	48.5	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.00	21.00	15.00	4	1.93	0.17	174	0.82	43.8	140.0	210.0	63.0	61	39	34	31	29	38	27	--	--	35.0	52.5	63.0
1.20	23.00	11.11	4	1.94	0.21	180	0.87	36.4	147.5	221.3	69.0	59	38	33	30	28	37	28	--	--	38.3	57.5	69.0
1.40	25.00	13.37	4	1.94	0.25	186	0.91	31.2	154.5	231.8	75.0	58	38	33	30	28	37	28	--	--	41.7	62.5	75.0
1.60	22.00	12.72	4	1.93	0.29	177	0.85	23.9	143.8	215.8	66.0	50	37	31	28	26	35	28	--	--	36.7	55.0	66.0
1.80	18.00	10.78	2	1.98	0.33	164	0.75	17.5	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
2.00	16.00	12.60	2	1.96	0.37	157	0.70	13.9	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.20	16.00	14.95	2	1.96	0.41	157	0.70	12.2	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.40	11.00	23.40	2	1.91	0.45	137	0.54	7.9	107.6	161.4	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.60	16.00	14.16	2	1.96	0.49	157	0.70	9.8	118.6	177.9	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.80	17.00	14.17	2	1.97	0.53	161	0.72	9.4	125.5	188.3	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.00	14.00	16.09	2	1.94	0.56	150	0.64	7.3	139.4	209.1	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.20	14.00	23.33	2	1.94	0.60	150	0.64	6.7	153.6	230.4	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	13.00	16.25	2	1.93	0.64	145	0.60	5.8	171.2	256.8	46.5	--	--	--	--	--	--	--	--	--	--	--	--
3.60	8.00	17.02	2	1.86	0.68	121	0.40	3.2	189.3	283.9	35.2	--	--	--	--	--	--	--	--	--	--	--	--
3.80	12.00	20.00	2	1.92	0.72	141	0.57	4.7	199.3	298.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
4.00	16.00	23.88	2	1.96	0.76	157	0.70	5.7	203.5	305.3	51.8	--	--	--	--	--	--	--	--	--	--	--	--
4.20	17.00	19.54	2	1.97	0.80	161	0.72	5.6	214.9	322.4	54.1	--	--	--	--	--	--	--	--	--	--	--	--
4.40	22.00	46.81	3	1.86	0.83	177	--	--	--	--	--	24	34	26	23	21	30	28	--	--	36.7	55.0	66.0
4.60	16.00	23.88	2	1.96	0.87	157	0.70	4.7	242.3	363.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
4.80	10.00	21.28	2	1.90	0.91	132	0.50	3.0	247.9	371.8	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.00	9.00	19.15	2	1.88	0.95	127	0.45	2.5	239.2	358.9	37.8	--	--	--	--	--	--	--	--	--	--	--	--
5.20	7.00	21.21	2	1.84	0.98	115	0.35	1.7	200.8	301.2	32.2	--	--	--	--	--	--	--	--	--	--	--	--
5.40	10.00	21.28	2	1.90	1.02	132	0.50	2.6	262.7	394.1	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.60	15.00	17.24	2	1.95	1.06	154	0.67	3.5	299.3	449.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
5.80	13.00	19.40	2	1.93	1.10	145	0.60	3.0	299.7	449.5	46.5	--	--	--	--	--	--	--	--	--	--	--	--
6.00	10.00	18.87	2	1.90	1.14	132	0.50	2.2	273.0	409.6	40.0	--	--	--	--	--	--	--	--	--	--	--	--
6.20	10.00	14.93	2	1.90	1.18	132	0.50	2.2	275.7	413.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
6.40	8.00	17.02	2	1.86	1.21	121	0.40	1.6	232.2	348.3	35.2	--	--	--	--	--	--	--	--	--	--	--	--
6.60	10.00	16.67	2	1.90	1.25	132	0.50	2.0	280.1	420.2	40.0	--	--	--	--	--	--	--	--	--	--	--	--
6.80	14.00	16.09	2	1.94	1.29	150	0.64	2.6	333.1	499.7	48.2	--	--	--	--	--	--	--	--	--	--	--	--
7.00	11.00	15.07	2	1.91	1.33	137	0.54	2.0	299.9	449.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
7.20	16.00	23.88	2	1.96	1.37	157	0.70	2.7	359.2	538.8	51.8	--	--	--	--	--	--	--	--	--	--	--	--
7.40	9.00	16.98	2	1.88	1.41	127	0.45	1.5	262.3	393.4	37.8	--	--	--	--	--	--	--	--	--	--	--	--
7.60	9.00	19.15	2	1.88	1.44	127	0.45	1.5	263.1	394.7	37.8	--	--	--	--	--	--	--	--	--	--	--	--
7.80	8.00	20.00	2	1.86	1.48	121	0.40	1.2	237.3	356.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
8.00	9.00	22.50	2	1.88	1.52	127	0.45	1.4	264.7	397.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
8.20	10.00	30.30	4	1.86	1.55	132	0.50	1.5	291.3	436.9	40.0	--	31	19	15	15	25	26	--	--	16.7	25.0	30.0
8.40	12.00	25.53	2	1.92	1.59	141	0.57	1.7	327.3	491.0	44.6	--	--	--	--	--	--	--	--	--	--	--	--
8.60	10.00	18.87	2	1.90	1.63	132	0.50	1.4	293.0	439.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
8.80	13.00	19.40	2	1.93	1.67	145	0.60	1.8	345.8	518.7	46.5	--	--	--	--	--	--	--	--	--	--	--	--
9.00	9.00	15.00	2	1.88	1.71	127	0.45	1.2	267.6	401.3	37.8	--	--	--	--	--	--	--	--	--	--	--	--
9.20	10.00	18.87	2	1.90	1.75	132	0.50	1.3	295.1	442.7	40.0	--	--	--	--	--	--	--	--	--	--	--	--
9.40	10.00	16.67	2	1.90	1.78	132	0.50	1.3	295.7	443.6	40.0	--	--	--	--	--	--	--	--	--	--	--	--
9.60	11.00	18.33	2	1.91	1.82	137	0.54	1.4	315.8	473.7	42.5	--	--	--	--	--	--	--	--	--	--	--	--
9.80	14.00	19.18	2	1.94	1.86	150	0.64	1.6	367.4	551.1	48.2	--	--	--	--	--	--	--	--	--	--	--	--
10.00	16.00	--	3	1.84	1.90	157	--	--	--	--	--	--	31	20	17	16	25	27	--	--	26.7	40.0	48.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	3
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	14.00	14.00	2	1.94	0.04	150	0.64	99.9	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
0.40	17.00	25.37	2	1.97	0.08	161	0.72	99.9	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
0.60	11.00	7.48	2	1.91	0.12	137	0.54	42.4	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	16.00	11.43	2	1.96	0.16	157	0.70	40.8	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.00	17.00	10.18	2	1.97	0.20	161	0.72	32.3	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.20	15.00	10.20	2	1.95	0.23	154	0.67	23.2	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	21.00	12.57	4	1.93	0.27	174	0.82	25.0	140.0	210.0	63.0	50	37	31	28	27	36	27	--	--	35.0	52.5	63.0
1.60	19.00	13.57	2	1.99	0.31	168	0.78	19.6	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
1.80	20.00	13.07	4	1.93	0.35	171	0.80	17.6	136.0	204.0	60.0	42	36	30	27	25	34	27	--	--	33.3	50.0	60.0
2.00	17.00	14.17	2	1.97	0.39	161	0.72	13.6	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.20	12.00	12.90	2	1.92	0.43	141	0.57	9.0	101.7	152.5	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.40	8.00	17.02	2	1.86	0.47	121	0.40	5.2	127.8	191.7	35.2	--	--	--	--	--	--	--	--	--	--	--	--
2.60	14.00	26.42	2	1.94	0.50	150	0.64	8.4	120.0	180.0	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.80	22.00	15.71	4	1.93	0.54	177	0.85	10.9	143.8	215.8	66.0	35	35	28	25	24	32	28	--	--	36.7	55.0	66.0
3.00	21.00	15.79	4	1.93	0.58	174	0.82	9.7	140.9	211.4	63.0	32	35	28	24	23	31	27	--	--	35.0	52.5	63.0
3.20	18.00	19.35	2	1.98	0.62	164	0.75	7.9	149.5	224.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	12.00	20.00	2	1.92	0.66	141	0.57	5.2	180.7	271.0	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.60	12.00	22.64	2	1.92	0.70	141	0.57	4.9	193.4	290.0	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.80	13.00	16.25	2	1.93	0.74	145	0.60	4.9	204.0	305.9	46.5	--	--	--	--	--	--	--	--	--	--	--	--
4.00	10.00	16.67	2	1.90	0.78	132	0.50	3.6	218.8	328.2	40.0	--	--	--	--	--	--	--	--	--	--	--	--
4.20	22.00	23.66	4	1.93	0.81	177	0.85	6.6	208.7	313.0	66.0	25	34	26	23	22	30	28	--	--	36.7	55.0	66.0
4.40	13.00	19.40	2	1.93	0.85	145	0.60	4.1	237.9	356.9	46.5	--	--	--	--	--	--	--	--	--	--	--	--
4.60	29.00	48.33	3	1.87	0.89	197	--	--	--	--	--	32	35	27	24	22	31	29	--	--	48.3	72.5	87.0
4.80	19.00	20.43	2	1.99	0.93	168	0.78	5.0	256.5	384.7	58.1	--	--	--	--	--	--	--	--	--	--	--	--
5.00	26.00	35.62	3	1.87	0.97	189	--	--	--	--	--	27	34	26	23	22	30	28	--	--	43.3	65.0	78.0
5.20	21.00	28.77	4	1.93	1.01	174	0.82	4.9	278.3	417.5	63.0	18	33	25	22	20	28	27	--	--	35.0	52.5	63.0
5.40	20.00	29.85	4	1.93	1.04	171	0.80	4.5	291.1	436.7	60.0	16	33	24	21	20	28	27	--	--	33.3	50.0	60.0
5.60	14.00	19.18	2	1.94	1.08	150	0.64	3.2	301.7	452.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
5.80	17.00	25.37	2	1.97	1.12	161	0.72	3.6	316.8	475.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
6.00	17.00	23.29	2	1.97	1.16	161	0.72	3.5	327.3	491.0	54.1	--	--	--	--	--	--	--	--	--	--	--	--
6.20	14.00	17.50	2	1.94	1.20	150	0.64	2.8	321.9	482.8	48.2	--	--	--	--	--	--	--	--	--	--	--	--
6.40	15.00	45.45	4	1.89	1.24	154	0.67	2.9	334.4	501.5	49.5	2	31	22	19	18	25	27	--	--	25.0	37.5	45.0
6.60	8.00	9.20	2	1.86	1.28	121	0.40	1.5	233.8	350.6	35.2	--	--	--	--	--	--	--	--	--	--	--	--
6.80	12.00	17.91	2	1.92	1.31	141	0.57	2.2	313.0	469.5	44.6	--	--	--	--	--	--	--	--	--	--	--	--
7.00	20.00	14.29	4	1.93	1.35	171	0.80	3.3	377.5	566.2	60.0	9	32	23	20	19	26	27	--	--	33.3	50.0	60.0
7.20	14.00	23.33	2	1.94	1.39	150	0.64	2.4	343.0	514.5	48.2	--	--	--	--	--	--	--	--	--	--	--	--
7.40	15.00	28.30	2	1.95	1.43	154	0.67	2.4	356.9	535.4	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.60	11.00	16.42	2	1.91	1.47	137	0.54	1.8	306.3	459.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
7.80	11.00	20.75	2	1.91	1.51	137	0.54	1.7	307.8	461.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
8.00	19.00	35.85	4	1.92	1.54	168	0.78	2.7	402.9	604.3	58.1	4	32	22	19	18	25	27	--	--	31.7	47.5	57.0
8.20	17.00	28.33	2	1.97	1.58	161	0.72	2.4	390.1	585.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
8.40	14.00	20.90	2	1.94	1.62	150	0.64	1.9	358.1	537.2	48.2	--	--	--	--	--	--	--	--	--	--	--	--
8.60	11.00	18.33	2	1.91	1.66	137	0.54	1.5	312.4	468.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
8.80	11.00	20.75	2	1.91	1.70	137	0.54	1.5	313.3	470.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
9.00	12.00	16.44	2	1.92	1.74	141	0.57	1.6	331.9	497.8	44.6	--	--	--	--	--	--	--	--	--	--	--	--
9.20	11.00	13.75	2	1.91	1.78	137	0.54	1.4	315.0	472.4	42.5	--	--	--	--	--	--	--	--	--	--	--	--
9.40	13.00	21.67	2	1.93	1.81	145	0.60	1.6	350.5	525.7	46.5	--	--	--	--	--	--	--	--	--	--	--	--
9.60	17.00	28.33	2	1.97	1.85	161	0.72	1.9	407.5	611.3	54.1	--	--	--	--	--	--	--	--	--	--	--	--
9.80	19.00	31.67	4	1.92	1.89	168	0.78	2.1	431.8	647.8	58.1	--	31	21	18	17	25	27	--	--	31.7	47.5	57.0
10.00	21.00	--	3	1.85	1.93	174	--	--	--	--	--	2	32	22	18	17	25	27	--	--	35.0	52.5	63.0

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Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT 4
riferimento **78-2024**

Committente: **GreenGo s.r.l.**
Cantiere: **Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**
Località: **Sala Bolognese (BO)**

U.M.: **kg/cm²**
Pagina: 1
Elaborato:

Data esec.: 08/06/2007
Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	5.00	3.57	1	1.46	0.03	101	0.25	91.9	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	12.00	8.57	2	1.92	0.07	141	0.57	90.5	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
0.60	18.00	10.78	2	1.98	0.11	164	0.75	71.4	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
0.80	24.00	11.59	4	1.94	0.15	183	0.89	60.0	151.1	226.7	72.0	70	40	35	32	30	39	28	--	--	40.0	60.0	72.0
1.00	31.00	12.55	4	1.97	0.19	202	1.03	53.8	175.7	263.5	93.0	73	40	35	32	30	39	29	--	--	51.7	77.5	93.0
1.20	29.00	11.15	4	1.96	0.22	197	0.98	39.8	167.1	250.7	87.0	66	39	34	31	29	38	29	--	--	48.3	72.5	87.0
1.40	27.00	10.67	4	1.95	0.26	192	0.95	31.1	161.1	241.6	81.0	60	38	33	30	28	37	28	--	--	45.0	67.5	81.0
1.60	20.00	13.07	4	1.93	0.30	171	0.80	21.2	136.0	204.0	60.0	46	37	31	28	26	35	27	--	--	33.3	50.0	60.0
1.80	25.00	16.34	4	1.94	0.34	186	0.91	21.4	154.5	231.8	75.0	51	37	31	28	26	35	28	--	--	41.7	62.5	75.0
2.00	22.00	18.33	4	1.93	0.38	177	0.85	17.1	143.8	215.8	66.0	44	36	30	27	25	34	28	--	--	36.7	55.0	66.0
2.20	19.00	12.93	2	1.99	0.42	168	0.78	13.5	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.40	17.00	9.44	2	1.97	0.46	161	0.72	11.1	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.60	13.00	14.94	2	1.93	0.50	145	0.60	8.0	119.4	179.1	46.5	--	--	--	--	--	--	--	--	--	--	--	--
2.80	15.00	15.00	2	1.95	0.54	154	0.67	8.2	127.9	191.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
3.00	16.00	20.00	2	1.96	0.58	157	0.70	8.0	138.4	207.6	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.20	15.00	25.00	2	1.95	0.61	154	0.67	7.0	154.6	231.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
3.40	9.00	19.15	2	1.88	0.65	127	0.45	3.9	182.5	273.7	37.8	--	--	--	--	--	--	--	--	--	--	--	--
3.60	15.00	28.30	2	1.95	0.69	154	0.67	6.0	182.9	274.4	49.5	--	--	--	--	--	--	--	--	--	--	--	--
3.80	23.00	24.73	4	1.94	0.73	180	0.87	7.8	176.5	264.8	69.0	29	35	27	24	22	31	28	--	--	38.3	57.5	69.0
4.00	22.00	19.47	4	1.93	0.77	177	0.85	7.1	192.1	288.1	66.0	26	34	26	23	22	30	28	--	--	36.7	55.0	66.0
4.20	16.00	21.92	2	1.96	0.81	157	0.70	5.2	221.4	332.1	51.8	--	--	--	--	--	--	--	--	--	--	--	--
4.40	12.00	22.64	2	1.92	0.85	141	0.57	3.8	237.9	356.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
4.60	15.00	22.39	2	1.95	0.89	154	0.67	4.4	247.1	370.6	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.80	14.00	26.42	2	1.94	0.92	150	0.64	3.9	258.7	388.0	48.2	--	--	--	--	--	--	--	--	--	--	--	--
5.00	30.00	75.00	3	1.88	0.96	199	--	--	--	--	--	32	35	27	24	22	30	29	--	--	50.0	75.0	90.0
5.20	21.00	44.68	3	1.85	1.00	174	--	--	--	--	--	18	33	25	22	20	28	27	--	--	35.0	52.5	63.0
5.40	19.00	40.43	4	1.92	1.04	168	0.78	4.4	289.5	434.3	58.1	14	33	24	21	20	28	27	--	--	31.7	47.5	57.0
5.60	16.00	30.19	4	1.90	1.07	157	0.70	3.6	303.5	455.2	51.8	7	32	23	20	19	26	27	--	--	26.7	40.0	48.0
5.80	12.00	20.00	2	1.92	1.11	141	0.57	2.7	293.8	440.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.00	14.00	19.18	2	1.94	1.15	150	0.64	3.0	314.5	471.7	48.2	--	--	--	--	--	--	--	--	--	--	--	--
6.20	12.00	17.91	2	1.92	1.19	141	0.57	2.5	302.5	453.8	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.40	19.00	19.00	2	1.99	1.23	168	0.78	3.5	347.1	520.6	58.1	--	--	--	--	--	--	--	--	--	--	--	--
6.60	15.00	20.55	2	1.95	1.27	154	0.67	2.8	338.8	508.3	49.5	--	--	--	--	--	--	--	--	--	--	--	--
6.80	17.00	36.17	4	1.91	1.31	161	0.72	3.0	357.1	535.7	54.1	5	32	23	19	18	26	27	--	--	28.3	42.5	51.0
7.00	11.00	23.40	2	1.91	1.35	137	0.54	2.0	300.8	451.2	42.5	--	--	--	--	--	--	--	--	--	--	--	--
7.20	14.00	20.90	2	1.94	1.38	150	0.64	2.4	342.4	513.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
7.40	15.00	18.75	2	1.95	1.42	154	0.67	2.4	356.3	534.4	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.60	21.00	44.68	3	1.85	1.46	174	--	--	--	--	--	9	32	23	20	19	26	27	--	--	35.0	52.5	63.0
7.80	14.00	15.05	2	1.94	1.50	150	0.64	2.2	351.0	526.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
8.00	18.00	30.00	4	1.91	1.54	164	0.75	2.6	394.5	591.7	56.2	3	32	22	19	18	25	27	--	--	30.0	45.0	54.0
8.20	17.00	32.08	4	1.91	1.58	161	0.72	2.4	389.4	584.1	54.1	--	31	22	18	17	25	27	--	--	28.3	42.5	51.0
8.40	14.00	35.00	4	1.89	1.61	150	0.64	2.0	357.6	536.4	48.2	--	31	21	17	16	25	26	--	--	23.3	35.0	42.0
8.60	10.00	25.00	2	1.90	1.65	132	0.50	1.4	293.4	440.1	40.0	--	--	--	--	--	--	--	--	--	--	--	--
8.80	12.00	30.00	4	1.88	1.69	141	0.57	1.6	330.5	495.7	44.6	--	31	20	16	15	25	26	--	--	20.0	30.0	36.0
9.00	12.00	25.53	2	1.92	1.73	141	0.57	1.6	331.6	497.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
9.20	17.00	15.89	2	1.97	1.77	161	0.72	2.1	402.9	604.3	54.1	--	--	--	--	--	--	--	--	--	--	--	--
9.40	18.00	45.00	4	1.91	1.80	164	0.75	2.1	416.1	624.2	56.2	--	31	21	18	17	25	27	--	--	30.0	45.0	54.0
9.60	26.00	43.33	3	1.87	1.84	189	--	--	--	--	--	11	33	23	20	19	26	28	--	--	43.3	65.0	78.0
9.80	25.00	31.25	3	1.86	1.88	186	--	--	--	--	--	9	32	23	19	18	26	28	--	--	41.7	62.5	75.0
10.00	18.00	--	3	1.85	1.92	164	--	--	--	--	--	--	31	21	17	17	25	27	--	--	30.0	45.0	54.0

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Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT 5
riferimento **78-2024**

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	11.00	12.64	2	1.91	0.04	137	0.54	99.9	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	13.00	17.81	2	1.93	0.08	145	0.60	82.8	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	15.00	16.13	2	1.95	0.12	154	0.67	56.0	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	15.00	13.27	2	1.95	0.15	154	0.67	39.0	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.00	14.00	13.08	2	1.94	0.19	150	0.64	27.8	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.20	16.00	10.88	2	1.96	0.23	157	0.70	24.7	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.40	17.00	15.04	2	1.97	0.27	161	0.72	21.3	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.60	21.00	13.13	4	1.93	0.31	174	0.82	21.2	140.0	210.0	63.0	47	37	31	28	26	35	27	--	--	35.0	52.5	63.0
1.80	17.00	11.56	2	1.97	0.35	161	0.72	15.5	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.00	17.00	14.17	2	1.97	0.39	161	0.72	13.6	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.20	18.00	14.17	2	1.98	0.43	164	0.75	12.6	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
2.40	16.00	13.33	2	1.96	0.47	157	0.70	10.3	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.60	17.00	17.00	2	1.97	0.51	161	0.72	9.8	123.5	185.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.80	14.00	16.09	2	1.94	0.55	150	0.64	7.6	133.3	199.9	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.00	17.00	19.54	2	1.97	0.59	161	0.72	8.2	140.0	210.0	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.20	16.00	16.00	2	1.96	0.63	157	0.70	7.2	155.5	233.2	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.40	19.00	20.43	2	1.99	0.67	168	0.78	7.6	162.0	243.0	58.1	--	--	--	--	--	--	--	--	--	--	--	--
3.60	21.00	18.58	4	1.93	0.70	174	0.82	7.6	171.2	256.8	63.0	27	34	27	23	22	30	27	--	--	35.0	52.5	63.0
3.80	17.00	32.08	4	1.91	0.74	161	0.72	6.1	195.4	293.2	54.1	18	33	25	22	21	29	27	--	--	28.3	42.5	51.0
4.00	15.00	22.39	2	1.95	0.78	154	0.67	5.2	214.4	321.6	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.20	6.00	18.18	2	1.82	0.82	109	0.30	1.8	171.1	256.7	28.8	--	--	--	--	--	--	--	--	--	--	--	--
4.40	8.00	24.24	2	1.86	0.85	121	0.40	2.4	213.8	320.7	35.2	--	--	--	--	--	--	--	--	--	--	--	--
4.60	9.00	15.00	2	1.88	0.89	127	0.45	2.7	233.2	349.9	37.8	--	--	--	--	--	--	--	--	--	--	--	--
4.80	13.00	12.15	2	1.93	0.93	145	0.60	3.7	262.7	394.0	46.5	--	--	--	--	--	--	--	--	--	--	--	--
5.00	15.00	37.50	4	1.89	0.97	154	0.67	3.9	271.1	406.7	49.5	8	32	23	20	19	27	27	--	--	25.0	37.5	45.0
5.20	8.00	15.09	2	1.86	1.01	121	0.40	2.0	224.4	336.5	35.2	--	--	--	--	--	--	--	--	--	--	--	--
5.40	12.00	20.00	2	1.92	1.04	141	0.57	3.0	283.9	425.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
5.60	13.00	14.94	2	1.93	1.08	145	0.60	3.0	296.8	445.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
5.80	13.00	24.53	2	1.93	1.12	145	0.60	2.9	303.0	454.5	46.5	--	--	--	--	--	--	--	--	--	--	--	--
6.00	16.00	34.04	4	1.90	1.16	157	0.70	3.3	324.7	487.0	51.8	5	32	23	19	18	26	27	--	--	26.7	40.0	48.0
6.20	11.00	16.42	2	1.91	1.20	137	0.54	2.3	291.2	436.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.40	10.00	21.28	2	1.90	1.24	132	0.50	2.0	279.3	418.9	40.0	--	--	--	--	--	--	--	--	--	--	--	--
6.60	19.00	19.00	2	1.99	1.28	168	0.78	3.4	358.1	537.1	58.1	--	--	--	--	--	--	--	--	--	--	--	--
6.80	15.00	14.02	2	1.95	1.31	154	0.67	2.7	344.7	517.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.00	15.00	18.75	2	1.95	1.35	154	0.67	2.6	349.2	523.8	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.20	20.00	25.00	4	1.93	1.39	171	0.80	3.1	385.3	578.0	60.0	9	32	23	20	19	26	27	--	--	33.3	50.0	60.0
7.40	18.00	24.66	2	1.98	1.43	164	0.75	2.8	381.7	572.5	56.2	--	--	--	--	--	--	--	--	--	--	--	--
7.60	16.00	17.20	2	1.96	1.47	157	0.70	2.5	370.4	555.6	51.8	--	--	--	--	--	--	--	--	--	--	--	--
7.80	21.00	21.00	4	1.93	1.51	174	0.82	2.9	409.9	614.8	63.0	8	32	23	19	18	26	27	--	--	35.0	52.5	63.0
8.00	27.00	33.75	3	1.87	1.55	192	--	--	--	--	--	16	33	24	21	20	27	28	--	--	45.0	67.5	81.0
8.20	24.00	40.00	3	1.86	1.58	183	--	--	--	--	--	12	33	23	20	19	26	28	--	--	40.0	60.0	72.0
8.40	25.00	26.88	4	1.94	1.62	186	0.91	3.0	445.3	668.0	75.0	13	33	23	20	19	27	28	--	--	41.7	62.5	75.0
8.60	16.00	13.33	2	1.96	1.66	157	0.70	2.1	385.2	577.8	51.8	--	--	--	--	--	--	--	--	--	--	--	--
8.80	18.00	15.93	2	1.98	1.70	164	0.75	2.3	409.1	613.7	56.2	--	--	--	--	--	--	--	--	--	--	--	--
9.00	15.00	16.13	2	1.95	1.74	154	0.67	1.9	377.1	565.6	49.5	--	--	--	--	--	--	--	--	--	--	--	--
9.20	14.00	16.09	2	1.94	1.78	150	0.64	1.7	364.7	547.1	48.2	--	--	--	--	--	--	--	--	--	--	--	--
9.40	15.00	17.24	2	1.95	1.82	154	0.67	1.8	380.4	570.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
9.60	17.00	21.25	2	1.97	1.86	161	0.72	1.9	407.7	611.6	54.1	--	--	--	--	--	--	--	--	--	--	--	--
9.80	19.00	26.03	2	1.99	1.90	168	0.78	2.1	432.1	648.2	58.1	--	--	--	--	--	--	--	--	--	--	--	--
10.00	19.00	--	3	1.85	1.93	168	--	--	--	--	--	--	31	21	18	17	25	27	--	--	31.7	47.5	57.0

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Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
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40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	6
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	4.00	5.97	1	1.46	0.03	93	0.20	69.6	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	6.00	5.00	1	1.46	0.06	109	0.30	48.6	12.0	18.0	9.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	14.00	26.42	2	1.94	0.10	150	0.64	65.7	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
0.80	12.00	9.02	2	1.92	0.14	141	0.57	37.9	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.00	19.00	17.76	2	1.99	0.18	168	0.78	40.3	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
1.20	17.00	21.25	2	1.97	0.21	161	0.72	28.6	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.40	18.00	12.24	2	1.98	0.25	164	0.75	24.3	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
1.60	17.00	12.14	2	1.97	0.29	161	0.72	19.4	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.80	18.00	12.86	2	1.98	0.33	164	0.75	17.3	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
2.00	12.00	12.90	2	1.92	0.37	141	0.57	10.7	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.20	13.00	14.94	2	1.93	0.41	145	0.60	10.2	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
2.40	12.00	13.79	2	1.92	0.45	141	0.57	8.5	106.5	159.8	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.60	17.00	15.89	2	1.97	0.49	161	0.72	10.3	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.80	15.00	20.55	2	1.95	0.53	154	0.67	8.4	125.3	187.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
3.00	11.00	23.40	2	1.91	0.57	137	0.54	5.9	150.5	225.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.20	8.00	24.24	2	1.86	0.60	121	0.40	3.8	169.9	254.8	35.2	--	--	--	--	--	--	--	--	--	--	--	--
3.40	6.00	18.18	2	1.82	0.64	109	0.30	2.4	160.2	240.3	28.8	--	--	--	--	--	--	--	--	--	--	--	--
3.60	6.00	18.18	2	1.82	0.68	109	0.30	2.3	163.3	244.9	28.8	--	--	--	--	--	--	--	--	--	--	--	--
3.80	8.00	17.02	2	1.86	0.71	121	0.40	3.1	195.7	293.6	35.2	--	--	--	--	--	--	--	--	--	--	--	--
4.00	8.00	8.60	2	1.86	0.75	121	0.40	2.9	201.6	302.5	35.2	--	--	--	--	--	--	--	--	--	--	--	--
4.20	10.00	37.04	4	1.86	0.79	132	0.50	3.6	222.1	333.2	40.0	--	31	22	19	18	25	26	--	--	16.7	25.0	30.0
4.40	8.00	15.09	2	1.86	0.82	121	0.40	2.5	210.8	316.3	35.2	--	--	--	--	--	--	--	--	--	--	--	--
4.60	11.00	33.33	4	1.87	0.86	137	0.54	3.5	242.8	364.2	42.5	--	31	22	19	18	25	26	--	--	18.3	27.5	33.0
4.80	5.00	25.00	2	1.80	0.90	101	0.25	1.3	148.0	221.9	25.0	--	--	--	--	--	--	--	--	--	--	--	--
5.00	5.00	15.15	2	1.80	0.93	101	0.25	1.2	148.5	222.7	25.0	--	--	--	--	--	--	--	--	--	--	--	--
5.20	7.00	35.00	4	1.83	0.97	115	0.35	1.8	200.3	300.4	32.2	--	31	20	16	15	25	26	--	--	11.7	17.5	21.0
5.40	7.00	25.93	2	1.84	1.01	115	0.35	1.7	201.6	302.3	32.2	--	--	--	--	--	--	--	--	--	--	--	--
5.60	5.00	12.50	1	1.46	1.04	101	0.25	1.1	32.4	48.6	7.5	--	--	--	--	--	--	--	--	--	--	--	--
5.80	6.00	12.77	1	1.46	1.07	109	0.30	1.3	38.4	57.7	9.0	--	--	--	--	--	--	--	--	--	--	--	--
6.00	7.00	21.21	2	1.84	1.10	115	0.35	1.5	204.2	306.3	32.2	--	--	--	--	--	--	--	--	--	--	--	--
6.20	6.00	30.00	4	1.82	1.14	109	0.30	1.2	178.4	267.6	28.8	--	31	18	14	14	25	26	--	--	10.0	15.0	18.0
6.40	8.00	20.00	2	1.86	1.18	121	0.40	1.6	231.1	346.7	35.2	--	--	--	--	--	--	--	--	--	--	--	--
6.60	7.00	21.21	2	1.84	1.21	115	0.35	1.3	206.4	309.7	32.2	--	--	--	--	--	--	--	--	--	--	--	--
6.80	7.00	14.89	1	1.46	1.24	115	0.35	1.3	44.8	67.3	10.5	--	--	--	--	--	--	--	--	--	--	--	--
7.00	7.00	17.50	2	1.84	1.28	115	0.35	1.2	207.5	311.2	32.2	--	--	--	--	--	--	--	--	--	--	--	--
7.20	6.00	15.00	1	1.46	1.31	109	0.30	1.0	39.0	58.5	9.0	--	--	--	--	--	--	--	--	--	--	--	--
7.40	9.00	19.15	2	1.88	1.35	127	0.45	1.6	260.7	391.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
7.60	6.00	10.00	1	1.46	1.37	109	0.30	0.9	39.0	58.5	9.0	--	--	--	--	--	--	--	--	--	--	--	--
7.80	12.00	15.00	2	1.92	1.41	141	0.57	2.0	319.2	478.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
8.00	15.00	15.00	2	1.95	1.45	154	0.67	2.4	358.8	538.3	49.5	--	--	--	--	--	--	--	--	--	--	--	--
8.20	14.00	20.90	2	1.94	1.49	150	0.64	2.2	350.5	525.7	48.2	--	--	--	--	--	--	--	--	--	--	--	--
8.40	15.00	18.75	2	1.95	1.53	154	0.67	2.2	365.0	547.4	49.5	--	--	--	--	--	--	--	--	--	--	--	--
8.60	7.00	9.59	1	1.46	1.56	115	0.35	1.0	45.5	68.3	10.5	--	--	--	--	--	--	--	--	--	--	--	--
8.80	6.00	15.00	1	1.46	1.59	109	0.30	0.8	39.0	58.5	9.0	--	--	--	--	--	--	--	--	--	--	--	--
9.00	6.00	30.00	4	1.82	1.62	109	0.30	0.8	180.0	270.0	28.8	--	31	16	13	12	25	26	--	--	10.0	15.0	18.0
9.20	6.00	30.00	4	1.82	1.66	109	0.30	0.7	180.0	270.0	28.8	--	31	16	12	12	25	26	--	--	10.0	15.0	18.0
9.40	6.00	22.22	2	1.82	1.70	109	0.30	0.7	180.0	270.0	28.8	--	--	--	--	--	--	--	--	--	--	--	--
9.60	6.00	18.18	2	1.82	1.73	109	0.30	0.7	180.0	270.0	28.8	--	--	--	--	--	--	--	--	--	--	--	--
9.80	7.00	21.21	2	1.84	1.77	115	0.35	0.8	210.0	315.0	32.2	--	--	--	--	--	--	--	--	--	--	--	--
10.00	8.00	--	3	1.82	1.81	121	--	--	--	--	--	--	31	17	14	13	25	26	--	--	13.3	20.0	24.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT 7
riferimento **78-2024**

Committente: **GreenGo s.r.l.**
Cantiere: **Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**
Località: **Sala Bolognese (BO)**

U.M.: **kg/cm²**
Pagina: 1
Elaborato:

Data esec.: 08/06/2007
Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	7.00	7.53	1	1.46	0.03	115	0.35	99.9	14.0	21.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	6.00	11.32	1	1.46	0.06	109	0.30	48.6	12.0	18.0	9.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	8.00	7.48	2	1.86	0.10	121	0.40	37.6	68.0	102.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
0.80	14.00	13.08	2	1.94	0.13	150	0.64	43.9	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.00	14.00	14.00	2	1.94	0.17	150	0.64	31.9	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.20	15.00	18.75	2	1.95	0.21	154	0.67	26.3	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	15.00	13.27	2	1.95	0.25	154	0.67	21.3	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.60	10.00	16.67	2	1.90	0.29	132	0.50	12.4	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
1.80	15.00	25.00	2	1.95	0.33	154	0.67	15.2	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.00	14.00	26.42	2	1.94	0.37	150	0.64	12.5	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.20	11.00	18.33	2	1.91	0.41	137	0.54	8.9	96.0	144.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.40	8.00	20.00	2	1.86	0.44	121	0.40	5.5	119.7	179.6	35.2	--	--	--	--	--	--	--	--	--	--	--	--
2.60	10.00	18.87	2	1.90	0.48	132	0.50	6.6	123.2	184.7	40.0	--	--	--	--	--	--	--	--	--	--	--	--
2.80	8.00	17.02	2	1.86	0.52	121	0.40	4.5	144.3	216.4	35.2	--	--	--	--	--	--	--	--	--	--	--	--
3.00	7.00	17.50	2	1.84	0.55	115	0.35	3.5	156.4	234.6	32.2	--	--	--	--	--	--	--	--	--	--	--	--
3.20	7.00	13.21	1	1.46	0.58	115	0.35	3.3	32.1	48.1	10.5	--	--	--	--	--	--	--	--	--	--	--	--
3.40	8.00	15.09	2	1.86	0.62	121	0.40	3.6	175.3	262.9	35.2	--	--	--	--	--	--	--	--	--	--	--	--
3.60	10.00	16.67	2	1.90	0.66	132	0.50	4.4	183.8	275.7	40.0	--	--	--	--	--	--	--	--	--	--	--	--
3.80	11.00	27.50	2	1.91	0.70	137	0.54	4.5	194.3	291.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.00	11.00	23.40	2	1.91	0.74	137	0.54	4.2	205.3	308.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.20	7.00	17.50	2	1.84	0.77	115	0.35	2.3	189.2	283.8	32.2	--	--	--	--	--	--	--	--	--	--	--	--
4.40	7.00	17.50	2	1.84	0.81	115	0.35	2.2	192.0	288.0	32.2	--	--	--	--	--	--	--	--	--	--	--	--
4.60	7.00	17.50	2	1.84	0.85	115	0.35	2.1	194.4	291.6	32.2	--	--	--	--	--	--	--	--	--	--	--	--
4.80	6.00	18.18	2	1.82	0.88	109	0.30	1.6	173.4	260.0	28.8	--	--	--	--	--	--	--	--	--	--	--	--
5.00	11.00	23.40	2	1.91	0.92	137	0.54	3.2	255.9	383.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
5.20	12.00	22.64	2	1.92	0.96	141	0.57	3.3	268.1	402.1	44.6	--	--	--	--	--	--	--	--	--	--	--	--
5.40	7.00	13.21	1	1.46	0.99	115	0.35	1.7	43.3	65.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
5.60	7.00	14.89	1	1.46	1.02	115	0.35	1.7	43.6	65.4	10.5	--	--	--	--	--	--	--	--	--	--	--	--
5.80	10.00	18.87	2	1.90	1.06	132	0.50	2.5	266.0	399.0	40.0	--	--	--	--	--	--	--	--	--	--	--	--
6.00	7.00	14.89	1	1.46	1.08	115	0.35	1.5	44.1	66.1	10.5	--	--	--	--	--	--	--	--	--	--	--	--
6.20	14.00	35.00	4	1.89	1.12	150	0.64	3.1	309.3	463.9	48.2	2	31	22	19	18	25	26	--	--	23.3	35.0	42.0
6.40	19.00	20.43	2	1.99	1.16	168	0.78	3.8	327.2	490.9	58.1	--	--	--	--	--	--	--	--	--	--	--	--
6.60	21.00	77.78	3	1.85	1.20	174	--	--	--	--	--	14	33	24	21	20	27	27	--	--	35.0	52.5	63.0
6.80	33.00	45.21	3	1.88	1.24	207	--	--	--	--	--	29	35	26	23	22	30	29	--	--	55.0	82.5	99.0
7.00	25.00	15.63	4	1.94	1.28	186	0.91	4.1	356.1	534.1	75.0	18	33	25	21	20	28	28	--	--	41.7	62.5	75.0
7.20	17.00	130.77	4	1.91	1.31	161	0.72	3.0	358.1	537.1	54.1	4	32	23	19	18	26	27	--	--	28.3	42.5	51.0
7.40	39.00	118.18	3	1.90	1.35	220	--	--	--	--	--	32	35	26	23	22	30	30	--	--	65.0	97.5	117.0
7.60	27.00	31.03	3	1.87	1.39	192	--	--	--	--	--	19	34	25	21	20	28	28	--	--	45.0	67.5	81.0
7.80	28.00	70.00	3	1.87	1.43	194	--	--	--	--	--	20	34	25	21	20	28	28	--	--	46.7	70.0	84.0
8.00	18.00	38.30	4	1.91	1.46	164	0.75	2.7	386.0	579.0	56.2	4	32	22	19	18	25	27	--	--	30.0	45.0	54.0
8.20	15.00	28.30	2	1.95	1.50	154	0.67	2.3	363.0	544.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
8.40	25.00	34.25	3	1.86	1.54	186	--	--	--	--	--	14	33	24	20	19	27	28	--	--	41.7	62.5	75.0
8.60	59.00	67.82	3	1.93	1.58	257	--	--	--	--	--	43	36	28	25	23	31	32	--	--	98.3	147.5	177.0
8.80	50.00	46.73	3	1.92	1.62	242	--	--	--	--	--	36	36	27	24	22	30	31	--	--	83.3	125.0	150.0
9.00	55.00	51.40	3	1.93	1.66	251	--	--	--	--	--	39	36	27	24	23	31	31	--	--	91.7	137.5	165.0
9.20	72.00	98.63	3	1.95	1.70	277	--	--	--	--	--	48	37	28	25	24	32	32	--	--	120.0	180.0	216.0
9.40	93.00	100.00	3	1.99	1.73	305	--	--	--	--	--	56	38	30	27	25	33	33	--	--	155.0	232.5	279.0
9.60	61.00	184.85	3	1.94	1.77	260	--	--	--	--	--	41	36	27	24	23	31	32	--	--	101.7	152.5	183.0
9.80	40.00	50.00	3	1.90	1.81	222	--	--	--	--	--	26	34	25	22	21	29	30	--	--	66.7	100.0	120.0
10.00	42.00	48.28	3	1.90	1.85	226	--	--	--	--	--	27	35	25	22	21	29	30	--	--	70.0	105.0	126.0
10.20	38.00	40.86	3	1.90	1.89	218	--	--	--	--	--	23	34	25	21	20	28	30	--	--	63.3	95.0	114.0
10.40	44.00	41.12	3	1.91	1.93	230	--	--	--	--	--	28	35	25	22	21	29	31	--	--	73.3	110.0	132.0
10.60	47.00	50.54	3	1.91	1.96	236	--	--	--	--	--	30	35	26	22	21	29	31	--	--	78.3	117.5	141.0
10.80	62.00	48.82	3	1.94	2.00	262	--	--	--	--	--	39	36	27	24	22	30	32	--	--	103.3	155.0	186.0
11.00	51.00	45.13	3	1.92	2.04	243	--	--	--	--	--	31	35	26	23	21	29	31	--	--	85.0	127.5	153.0
11.20	48.00	42.48	3	1.91	2.08	238	--	--	--	--	--	29	35	25	22	21	29	31	--	--	80.0	120.0	144.0
11.40	61.00	48.03	3	1.94	2.12	260	--	--	--	--	--	37	36	26	23	22	30	32	--	--	101.7	152.5	183.0
11.60	49.00	35.00	3	1.92	2.16	240	--	--	--	--	--	29	35	25	22	21	29	31	--	--	81.7	122.5	147.0
11.80	53.00	72.60	3	1.92	2.19	247	--	--	--	--	--	31	35	26	22	21	29	31	--	--	88.3	132.5	159.0
12.00	42.00	--	3	1.90	2.23	226	--	--	--	--	--	23	34	24	21	20	28	30	--	--	70.0	105.0	126.0

FON053

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	8
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	8.00	10.96	2	1.86	0.04	121	0.40	99.9	68.0	102.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
0.40	5.00	5.38	1	1.46	0.07	101	0.25	32.9	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	10.00	9.35	2	1.90	0.10	132	0.50	44.5	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
0.80	14.00	10.53	2	1.94	0.14	150	0.64	40.5	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.00	16.00	10.88	2	1.96	0.18	157	0.70	33.5	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.20	8.00	6.30	2	1.86	0.22	121	0.40	13.3	68.0	102.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
1.40	9.00	19.15	2	1.88	0.26	127	0.45	12.6	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
1.60	15.00	14.02	2	1.95	0.30	154	0.67	17.3	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.80	12.00	13.79	2	1.92	0.33	141	0.57	12.3	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.00	15.00	22.39	2	1.95	0.37	154	0.67	12.9	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.20	14.00	20.90	2	1.94	0.41	150	0.64	10.8	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.40	15.00	20.55	2	1.95	0.45	154	0.67	10.2	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.60	11.00	18.33	2	1.91	0.49	137	0.54	7.0	122.6	183.9	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.80	14.00	17.50	2	1.94	0.53	150	0.64	7.9	127.2	190.8	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.00	15.00	22.39	2	1.95	0.57	154	0.67	7.7	137.8	206.8	49.5	--	--	--	--	--	--	--	--	--	--	--	--
3.20	13.00	13.98	2	1.93	0.61	145	0.60	6.3	158.2	237.3	46.5	--	--	--	--	--	--	--	--	--	--	--	--
3.40	13.00	32.50	4	1.88	0.64	145	0.60	5.8	172.0	258.0	46.5	13	33	25	21	20	28	26	--	--	21.7	32.5	39.0
3.60	26.00	24.30	4	1.95	0.68	189	0.93	9.2	162.5	243.7	78.0	35	35	28	25	23	32	28	--	--	43.3	65.0	78.0
3.80	16.00	26.67	2	1.96	0.72	157	0.70	6.0	191.0	286.6	51.8	--	--	--	--	--	--	--	--	--	--	--	--
4.00	14.00	17.50	2	1.94	0.76	150	0.64	5.0	209.7	314.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
4.20	7.00	13.21	1	1.46	0.79	115	0.35	2.3	40.5	60.7	10.5	--	--	--	--	--	--	--	--	--	--	--	--
4.40	18.00	22.50	2	1.98	0.83	164	0.75	5.5	224.4	336.6	56.2	--	--	--	--	--	--	--	--	--	--	--	--
4.60	8.00	13.33	2	1.86	0.87	121	0.40	2.4	214.9	322.3	35.2	--	--	--	--	--	--	--	--	--	--	--	--
4.80	9.00	13.43	2	1.88	0.90	127	0.45	2.6	234.7	352.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
5.00	10.00	18.87	2	1.90	0.94	132	0.50	2.8	252.7	379.1	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.20	9.00	19.15	2	1.88	0.98	127	0.45	2.4	242.2	363.3	37.8	--	--	--	--	--	--	--	--	--	--	--	--
5.40	8.00	20.00	2	1.86	1.02	121	0.40	2.0	224.9	337.4	35.2	--	--	--	--	--	--	--	--	--	--	--	--
5.60	8.00	17.02	2	1.86	1.05	121	0.40	1.9	226.7	340.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
5.80	10.00	10.00	2	1.90	1.09	132	0.50	2.4	269.4	404.1	40.0	--	--	--	--	--	--	--	--	--	--	--	--
6.00	19.00	70.37	4	1.92	1.13	168	0.78	3.9	316.8	475.2	58.1	12	33	24	20	19	27	27	--	--	31.7	47.5	57.0
6.20	22.00	32.84	3	1.86	1.17	177	--	--	--	--	--	16	33	24	21	20	28	28	--	--	36.7	55.0	66.0
6.40	5.00	7.46	1	1.46	1.20	101	0.25	0.9	32.5	48.8	7.5	--	--	--	--	--	--	--	--	--	--	--	--
6.60	11.00	27.50	2	1.91	1.24	137	0.54	2.2	294.0	441.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.80	10.00	21.28	2	1.90	1.27	132	0.50	2.0	281.3	421.9	40.0	--	--	--	--	--	--	--	--	--	--	--	--
7.00	10.00	21.28	2	1.90	1.31	132	0.50	1.9	283.1	424.6	40.0	--	--	--	--	--	--	--	--	--	--	--	--
7.20	9.00	22.50	2	1.88	1.35	127	0.45	1.6	260.8	391.2	37.8	--	--	--	--	--	--	--	--	--	--	--	--
7.40	11.00	27.50	2	1.91	1.39	137	0.54	1.9	302.8	454.3	42.5	--	--	--	--	--	--	--	--	--	--	--	--
7.60	39.00	97.50	3	1.90	1.42	220	--	--	--	--	--	31	35	26	23	22	30	30	--	--	65.0	97.5	117.0
7.80	28.00	24.78	4	1.96	1.46	194	0.97	3.7	412.9	619.3	84.0	19	34	24	21	20	28	28	--	--	46.7	70.0	84.0
8.00	39.00	53.42	3	1.90	1.50	220	--	--	--	--	--	30	35	26	23	21	29	30	--	--	65.0	97.5	117.0
8.20	22.00	25.29	4	1.93	1.54	177	0.85	3.0	419.5	629.3	66.0	9	32	23	20	19	26	28	--	--	36.7	55.0	66.0
8.40	57.00	65.52	3	1.93	1.58	254	--	--	--	--	--	42	36	28	24	23	31	31	--	--	95.0	142.5	171.0
8.60	59.00	147.50	3	1.93	1.62	257	--	--	--	--	--	42	36	28	25	23	31	32	--	--	98.3	147.5	177.0
8.80	48.00	145.45	3	1.91	1.66	238	--	--	--	--	--	34	35	26	23	22	30	31	--	--	80.0	120.0	144.0
9.00	32.00	80.00	3	1.88	1.69	204	--	--	--	--	--	20	34	24	21	20	28	29	--	--	53.3	80.0	96.0
9.20	29.00	61.70	3	1.87	1.73	197	--	--	--	--	--	16	33	24	20	19	27	29	--	--	48.3	72.5	87.0
9.40	31.00	65.96	3	1.88	1.77	202	--	--	--	--	--	18	33	24	21	20	27	29	--	--	51.7	77.5	93.0
9.60	29.00	54.72	3	1.87	1.81	197	--	--	--	--	--	15	33	24	20	19	27	29	--	--	48.3	72.5	87.0
9.80	31.00	42.47	3	1.88	1.84	202	--	--	--	--	--	17	33	24	20	19	27	29	--	--	51.7	77.5	93.0
10.00	42.00	52.50	3	1.90	1.88	226	--	--	--	--	--	27	34	25	22	21	29	30	--	--	70.0	105.0	126.0
10.20	33.00	82.50	3	1.88	1.92	207	--	--	--	--	--	18	33	24	21	19	27	29	--	--	55.0	82.5	99.0
10.40	39.00	39.00	3	1.90	1.96	220	--	--	--	--	--	23	34	25	21	20	28	30	--	--	65.0	97.5	117.0
10.60	46.00	31.29	3	1.91	2.00	234	--	--	--	--	--	28	35	25	22	21	29	31	--	--	76.7	115.0	138.0
10.80	48.00	37.80	3	1.91	2.03	238	--	--	--	--	--	29	35	25	22	21	29	31	--	--	80.0	120.0	144.0
11.00	44.00	15.33	4	2.00	2.07	230	1.47	4.1	578.8	868.2	132.0	26	34	25	22	20	28	31	--	--	73.3	110.0	132.0
11.20	45.00	29.41	4	2.00	2.11	232	1.50	4.1	590.1	885.1	135.0	26	34	25	22	20	28	31	--	--	75.0	112.5	135.0
11.40	49.00	30.63	3	1.92	2.15	240	--	--	--	--	--	29	35	25	22	21	29	31	--	--	81.7	122.5	147.0
11.60	43.00	33.86	3	1.91	2.19	228	--	--	--	--	--	24	34	25	21	20	28	30	--	--	71.7	107.5	129.0
11.80	41.00	32.28	3	1.90	2.23	224	--	--	--	--	--	22	34	24	21	20	28	30	--	--	68.3	102.5	123.0
12.00	38.00	--	3	1.90	2.27	218	--	--	--	--	--	19	34	24	20	19	27	30	--	--	63.3	95.0	114.0

FON053

Dott. Geol. Maurizio Zamboni
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40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	9
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	5.00	18.52	2	1.80	0.04	101	0.25	70.8	42.5	63.8	25.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	9.00	7.09	2	1.88	0.07	127	0.45	60.4	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
0.60	11.00	9.73	2	1.91	0.11	137	0.54	44.6	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	10.00	8.33	2	1.90	0.15	132	0.50	28.3	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
1.00	12.00	10.62	2	1.92	0.19	141	0.57	25.2	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.20	11.00	8.27	2	1.91	0.23	137	0.54	18.5	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	14.00	10.00	2	1.94	0.27	150	0.64	18.8	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.60	11.00	10.28	2	1.91	0.30	137	0.54	12.8	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.80	8.00	10.96	2	1.86	0.34	121	0.40	7.7	82.8	124.1	35.2	--	--	--	--	--	--	--	--	--	--	--	--
2.00	11.00	12.64	2	1.91	0.38	137	0.54	9.7	91.8	137.7	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.20	12.00	15.00	2	1.92	0.42	141	0.57	9.3	99.5	149.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.40	12.00	16.44	2	1.92	0.46	141	0.57	8.3	108.4	162.6	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.60	6.00	15.00	1	1.46	0.48	109	0.30	3.4	26.4	39.5	9.0	--	--	--	--	--	--	--	--	--	--	--	--
2.80	11.00	23.40	2	1.91	0.52	137	0.54	6.5	134.9	202.4	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.00	13.00	32.50	4	1.88	0.56	145	0.60	6.9	141.4	212.1	46.5	16	33	25	22	21	29	26	--	--	21.7	32.5	39.0
3.20	36.00	90.00	3	1.89	0.60	214	--	--	--	--	--	49	37	30	27	25	34	30	--	--	60.0	90.0	108.0
3.40	33.00	41.25	3	1.88	0.64	207	--	--	--	--	--	45	37	29	26	25	33	29	--	--	55.0	82.5	99.0
3.60	13.00	16.25	2	1.93	0.67	145	0.60	5.5	183.0	274.5	46.5	--	--	--	--	--	--	--	--	--	--	--	--
3.80	28.00	103.70	3	1.87	0.71	194	--	--	--	--	--	37	36	28	25	23	32	28	--	--	46.7	70.0	84.0
4.00	23.00	48.94	3	1.86	0.75	180	--	--	--	--	--	29	35	27	24	22	30	28	--	--	38.3	57.5	69.0
4.20	28.00	59.57	3	1.87	0.79	194	--	--	--	--	--	34	35	28	24	23	31	28	--	--	46.7	70.0	84.0
4.40	34.00	50.75	3	1.89	0.82	209	--	--	--	--	--	40	36	28	25	24	32	29	--	--	56.7	85.0	102.0
4.60	28.00	59.57	3	1.87	0.86	194	--	--	--	--	--	32	35	27	24	22	31	28	--	--	46.7	70.0	84.0
4.80	27.00	45.00	3	1.87	0.90	192	--	--	--	--	--	30	35	27	23	22	30	28	--	--	45.0	67.5	81.0
5.00	29.00	43.28	3	1.87	0.94	197	--	--	--	--	--	31	35	27	24	22	30	29	--	--	48.3	72.5	87.0
5.20	28.00	84.85	3	1.87	0.97	194	--	--	--	--	--	29	35	26	23	22	30	28	--	--	46.7	70.0	84.0
5.40	24.00	45.28	3	1.86	1.01	183	--	--	--	--	--	23	34	26	22	21	29	28	--	--	40.0	60.0	72.0
5.60	21.00	35.00	3	1.85	1.05	174	--	--	--	--	--	17	33	25	21	20	28	27	--	--	35.0	52.5	63.0
5.80	28.00	70.00	3	1.87	1.09	194	--	--	--	--	--	26	34	26	23	21	29	28	--	--	46.7	70.0	84.0
6.00	16.00	59.26	4	1.90	1.12	157	0.70	3.4	316.4	474.6	51.8	6	32	23	20	19	26	27	--	--	26.7	40.0	48.0
6.20	17.00	42.50	4	1.91	1.16	161	0.72	3.5	327.4	491.0	54.1	7	32	23	20	19	26	27	--	--	28.3	42.5	51.0
6.40	33.00	82.50	3	1.88	1.20	207	--	--	--	--	--	29	35	26	23	22	30	29	--	--	55.0	82.5	99.0
6.60	24.00	35.82	3	1.86	1.24	183	--	--	--	--	--	18	33	25	21	20	28	28	--	--	40.0	60.0	72.0
6.80	23.00	31.51	3	1.86	1.27	180	--	--	--	--	--	16	33	24	21	20	27	28	--	--	38.3	57.5	69.0
7.00	12.00	22.64	2	1.92	1.31	141	0.57	2.2	312.9	469.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
7.20	12.00	16.44	2	1.92	1.35	141	0.57	2.1	315.5	473.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
7.40	9.00	11.25	2	1.88	1.39	127	0.45	1.5	261.9	392.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
7.60	53.00	88.33	3	1.92	1.43	247	--	--	--	--	--	41	36	28	25	23	31	31	--	--	88.3	132.5	159.0
7.80	37.00	61.67	3	1.89	1.46	216	--	--	--	--	--	29	35	26	23	21	29	30	--	--	61.7	92.5	111.0
8.00	27.00	40.30	3	1.87	1.50	192	--	--	--	--	--	17	33	24	21	20	27	28	--	--	45.0	67.5	81.0
8.20	26.00	55.32	3	1.87	1.54	189	--	--	--	--	--	15	33	24	20	19	27	28	--	--	43.3	65.0	78.0
8.40	20.00	37.74	4	1.93	1.58	171	0.80	2.7	413.7	620.5	60.0	6	32	22	19	18	25	27	--	--	33.3	50.0	60.0
8.60	12.00	9.45	2	1.92	1.62	141	0.57	1.7	328.1	492.2	44.6	--	--	--	--	--	--	--	--	--	--	--	--
8.80	59.00	28.50	4	2.02	1.66	257	1.97	7.8	400.8	601.2	177.0	42	36	28	24	23	31	32	--	--	98.3	147.5	177.0
9.00	58.00	34.73	3	1.93	1.70	256	--	--	--	--	--	40	36	27	24	23	31	31	--	--	96.7	145.0	174.0
9.20	30.00	26.55	4	1.96	1.73	199	1.00	3.2	480.6	720.9	90.0	17	33	24	21	19	27	29	--	--	50.0	75.0	90.0
9.40	12.00	20.00	2	1.92	1.77	141	0.57	1.5	332.8	499.1	44.6	--	--	--	--	--	--	--	--	--	--	--	--
9.60	9.00	22.50	2	1.88	1.81	127	0.45	1.1	268.7	403.1	37.8	--	--	--	--	--	--	--	--	--	--	--	--
9.80	9.00	19.15	2	1.88	1.85	127	0.45	1.1	269.1	403.6	37.8	--	--	--	--	--	--	--	--	--	--	--	--
10.00	9.00	19.15	2	1.88	1.89	127	0.45	1.0	269.4	404.1	37.8	--	--	--	--	--	--	--	--	--	--	--	--
10.20	8.00	13.33	2	1.86	1.92	121	0.40	0.9	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
10.40	9.00	33.33	4	1.85	1.96	127	0.45	1.0	270.0	405.0	37.8	--	31	17	14	13	25	26	--	--	15.0	22.5	27.0
10.60	11.00	27.50	2	1.91	2.00	137	0.54	1.2	318.6	477.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
10.80	10.00	37.04	4	1.86	2.04	132	0.50	1.1	298.8	448.2	40.0	--	31	18	14	13	25	26	--	--	16.7	25.0	30.0
11.00	19.00	28.36	2	1.99	2.07	168	0.78	1.8	440.8	661.3	58.1	--	--	--	--	--	--	--	--	--	--	--	--
11.20	12.00	16.44	2	1.92	2.11	141	0.57	1.2	339.1	508.6	44.6	--	--	--	--	--	--	--	--	--	--	--	--
11.40	13.00	21.67	2	1.93	2.15	145	0.60	1.3	357.6	536.3	46.5	--	--	--	--	--	--	--	--	--	--	--	--
11.60	11.00	15.07	2	1.91	2.19	137	0.54	1.1	320.7	481.1	42.5	--	--	--	--	--	--	--	--	--	--	--	--
11.80	12.00	15.00	2	1.92	2.23	141	0.57	1.1	340.5	510.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
12.00	13.00	--	3	1.83	2.27	145	--	--	--	--	--	--	31	18	15	14	25	26	--	--	21.7	32.5	39.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

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PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT 10
riferimento **78-2024**

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	11.00	11.00	2	1.91	0.04	137	0.54	99.9	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	11.00	8.27	2	1.91	0.08	137	0.54	71.8	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	10.00	8.33	2	1.90	0.11	132	0.50	39.7	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
0.80	11.00	10.28	2	1.91	0.15	137	0.54	30.2	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.00	11.00	11.00	2	1.91	0.19	137	0.54	22.9	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.20	11.00	8.66	2	1.91	0.23	137	0.54	18.2	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	8.00	10.00	2	1.86	0.27	121	0.40	10.4	68.0	102.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
1.60	11.00	11.00	2	1.91	0.30	137	0.54	12.8	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.80	17.00	15.89	2	1.97	0.34	161	0.72	15.9	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.00	9.00	27.27	2	1.88	0.38	127	0.45	7.7	92.5	138.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
2.20	15.00	28.30	2	1.95	0.42	154	0.67	11.2	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.40	15.00	20.55	2	1.95	0.46	154	0.67	10.0	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.60	15.00	16.13	2	1.95	0.50	154	0.67	9.0	118.2	177.3	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.80	16.00	20.00	2	1.96	0.54	157	0.70	8.7	127.4	191.1	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.00	11.00	20.75	2	1.91	0.58	137	0.54	5.7	154.3	231.4	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.20	13.00	21.67	2	1.93	0.61	145	0.60	6.2	161.3	242.0	46.5	--	--	--	--	--	--	--	--	--	--	--	--
3.40	9.00	13.43	2	1.88	0.65	127	0.45	3.9	182.4	273.6	37.8	--	--	--	--	--	--	--	--	--	--	--	--
3.60	11.00	27.50	2	1.91	0.69	137	0.54	4.6	192.3	288.4	42.5	--	--	--	--	--	--	--	--	--	--	--	--
3.80	20.00	42.55	4	1.93	0.73	171	0.80	7.1	182.3	273.5	60.0	24	34	26	23	22	30	27	--	--	33.3	50.0	60.0
4.00	17.00	32.08	4	1.91	0.77	161	0.72	5.8	204.6	306.9	54.1	18	33	25	22	21	29	27	--	--	28.3	42.5	51.0
4.20	17.00	28.33	2	1.97	0.81	161	0.72	5.5	218.6	327.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
4.40	15.00	37.50	4	1.89	0.84	154	0.67	4.7	234.8	352.2	49.5	11	33	24	21	20	27	27	--	--	25.0	37.5	45.0
4.60	19.00	26.03	2	1.99	0.88	168	0.78	5.3	241.2	361.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
4.80	27.00	50.94	3	1.87	0.92	192	--	--	--	--	--	29	35	27	23	22	30	28	--	--	45.0	67.5	81.0
5.00	11.00	18.33	2	1.91	0.96	137	0.54	3.0	263.2	394.7	42.5	--	--	--	--	--	--	--	--	--	--	--	--
5.20	28.00	52.83	3	1.87	1.00	194	--	--	--	--	--	28	35	26	23	22	30	28	--	--	46.7	70.0	84.0
5.40	18.00	30.00	4	1.91	1.04	164	0.75	4.2	289.1	433.6	56.2	12	33	24	21	19	27	27	--	--	30.0	45.0	54.0
5.60	21.00	21.00	4	1.93	1.07	174	0.82	4.5	299.4	449.1	63.0	17	33	25	21	20	28	27	--	--	35.0	52.5	63.0
5.80	27.00	67.50	3	1.87	1.11	192	--	--	--	--	--	24	34	26	22	21	29	28	--	--	45.0	67.5	81.0
6.00	12.00	17.91	2	1.92	1.15	141	0.57	2.6	298.2	447.2	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.20	12.00	25.53	2	1.92	1.19	141	0.57	2.5	302.3	453.4	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.40	12.00	36.36	4	1.88	1.23	141	0.57	2.4	305.9	458.8	44.6	--	31	21	18	17	25	26	--	--	20.0	30.0	36.0
6.60	11.00	23.40	2	1.91	1.26	137	0.54	2.2	296.0	444.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.80	9.00	22.50	2	1.88	1.30	127	0.45	1.7	259.4	389.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
7.00	11.00	20.75	2	1.91	1.34	137	0.54	2.0	300.5	450.7	42.5	--	--	--	--	--	--	--	--	--	--	--	--
7.20	13.00	21.67	2	1.93	1.38	145	0.60	2.2	330.3	495.5	46.5	--	--	--	--	--	--	--	--	--	--	--	--
7.40	17.00	17.00	2	1.97	1.42	161	0.72	2.7	372.9	559.4	54.1	--	--	--	--	--	--	--	--	--	--	--	--
7.60	18.00	15.00	2	1.98	1.46	164	0.75	2.7	385.1	577.6	56.2	--	--	--	--	--	--	--	--	--	--	--	--
7.80	17.00	15.04	2	1.97	1.50	161	0.72	2.5	381.9	572.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
8.00	23.00	19.17	4	1.94	1.54	180	0.87	3.1	422.7	634.0	69.0	11	33	23	20	19	26	28	--	--	38.3	57.5	69.0
8.20	21.00	18.58	4	1.93	1.57	174	0.82	2.8	419.4	629.0	63.0	7	32	23	19	18	26	27	--	--	35.0	52.5	63.0
8.40	21.00	17.50	4	1.93	1.61	174	0.82	2.7	424.4	636.6	63.0	7	32	23	19	18	26	27	--	--	35.0	52.5	63.0
8.60	18.00	18.00	2	1.98	1.65	164	0.75	2.3	405.3	607.9	56.2	--	--	--	--	--	--	--	--	--	--	--	--
8.80	21.00	28.77	4	1.93	1.69	174	0.82	2.6	433.4	650.1	63.0	6	32	22	19	18	25	27	--	--	35.0	52.5	63.0
9.00	14.00	29.79	2	1.94	1.73	150	0.64	1.8	362.8	544.2	48.2	--	--	--	--	--	--	--	--	--	--	--	--
9.20	8.00	15.09	2	1.86	1.77	121	0.40	1.0	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
9.40	8.00	24.24	2	1.86	1.80	121	0.40	1.0	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
9.60	6.00	15.00	1	1.46	1.83	109	0.30	0.7	39.0	58.5	9.0	--	--	--	--	--	--	--	--	--	--	--	--
9.80	11.00	23.40	2	1.91	1.87	137	0.54	1.3	316.7	475.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
10.00	12.00	30.00	4	1.88	1.91	141	0.57	1.4	335.7	503.6	44.6	--	31	19	15	15	25	26	--	--	20.0	30.0	36.0
10.20	9.00	16.98	2	1.88	1.95	127	0.45	1.0	269.9	404.9	37.8	--	--	--	--	--	--	--	--	--	--	--	--
10.40	8.00	15.09	2	1.86	1.98	121	0.40	0.8	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
10.60	9.00	22.50	2	1.88	2.02	127	0.45	1.0	270.0	405.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
10.80	8.00	24.24	2	1.86	2.06	121	0.40	0.8	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
11.00	14.00	23.33	2	1.94	2.10	150	0.64	1.4	373.3	560.0	48.2	--	--	--	--	--	--	--	--	--	--	--	--
11.20	20.00	27.40	4	1.93	2.14	171	0.80	1.8	454.6	681.8	60.0	--	31	21	17	17	25	27	--	--	33.3	50.0	60.0
11.40	18.00	15.93	2	1.98	2.18	164	0.75	1.7	432.5	648.7	56.2	--	--	--	--	--	--	--	--	--	--	--	--
11.60	14.00	15.05	2	1.94	2.21	150	0.64	1.3	375.5	563.2	48.2	--	--	--	--	--	--	--	--	--	--	--	--
11.80	13.00	14.94	2	1.93	2.25	145	0.60	1.2	359.0	538.5	46.5	--	--	--	--	--	--	--	--	--	--	--	--
12.00	13.00	--	3	1.83	2.29	145	--	--	--	--	--	--	31	18	15	14	25	26	--	--	21.7	32.5	39.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	11
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	12.00	12.00	2	1.92	0.04	141	0.57	99.9	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
0.40	11.00	9.17	2	1.91	0.08	137	0.54	71.5	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	9.00	11.25	2	1.88	0.11	127	0.45	34.9	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
0.80	12.00	12.90	2	1.92	0.15	141	0.57	32.7	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.00	11.00	11.00	2	1.91	0.19	137	0.54	22.9	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.20	13.00	11.50	2	1.93	0.23	145	0.60	21.1	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	17.00	14.17	2	1.97	0.27	161	0.72	21.6	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.60	17.00	15.04	2	1.97	0.31	161	0.72	18.2	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.80	14.00	15.05	2	1.94	0.35	150	0.64	13.4	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.00	16.00	14.16	2	1.96	0.39	157	0.70	13.1	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.20	14.00	12.39	2	1.94	0.43	150	0.64	10.4	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.40	12.00	12.90	2	1.92	0.46	141	0.57	8.2	110.7	166.1	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.60	17.00	18.28	2	1.97	0.50	161	0.72	9.9	123.2	184.7	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.80	16.00	13.33	2	1.96	0.54	157	0.70	8.6	128.5	192.8	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.00	20.00	15.04	4	1.93	0.58	171	0.80	9.4	138.7	208.1	60.0	30	35	27	24	23	31	27	--	--	33.3	50.0	60.0
3.20	22.00	15.71	4	1.93	0.62	177	0.85	9.3	147.6	221.4	66.0	32	35	28	24	23	31	28	--	--	36.7	55.0	66.0
3.40	18.00	16.82	2	1.98	0.66	164	0.75	7.4	162.2	243.2	56.2	--	--	--	--	--	--	--	--	--	--	--	--
3.60	15.00	20.55	2	1.95	0.70	154	0.67	5.9	185.3	278.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
3.80	9.00	15.00	2	1.88	0.74	127	0.45	3.4	206.7	310.1	37.8	--	--	--	--	--	--	--	--	--	--	--	--
4.00	9.00	16.98	2	1.88	0.77	127	0.45	3.2	214.8	322.3	37.8	--	--	--	--	--	--	--	--	--	--	--	--
4.20	8.00	20.00	2	1.86	0.81	121	0.40	2.6	209.3	314.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
4.40	12.00	36.36	4	1.88	0.85	141	0.57	3.8	238.4	357.7	44.6	3	32	23	20	19	26	26	--	--	20.0	30.0	36.0
4.60	22.00	23.66	4	1.93	0.89	177	0.85	5.9	235.5	353.3	66.0	23	34	26	23	21	29	28	--	--	36.7	55.0	66.0
4.80	11.00	20.75	2	1.91	0.92	137	0.54	3.2	256.8	385.1	42.5	--	--	--	--	--	--	--	--	--	--	--	--
5.00	10.00	14.93	2	1.90	0.96	132	0.50	2.8	255.6	383.4	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.20	8.00	24.24	2	1.86	1.00	121	0.40	2.0	224.0	336.1	35.2	--	--	--	--	--	--	--	--	--	--	--	--
5.40	10.00	25.00	2	1.90	1.04	132	0.50	2.5	264.3	396.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.60	10.00	16.67	2	1.90	1.08	132	0.50	2.4	268.0	402.0	40.0	--	--	--	--	--	--	--	--	--	--	--	--
5.80	11.00	20.75	2	1.91	1.11	137	0.54	2.5	283.7	425.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.00	12.00	17.91	2	1.92	1.15	141	0.57	2.6	298.5	447.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.20	11.00	20.75	2	1.91	1.19	137	0.54	2.3	290.7	436.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.40	13.00	14.94	2	1.93	1.23	145	0.60	2.6	316.9	475.4	46.5	--	--	--	--	--	--	--	--	--	--	--	--
6.60	15.00	28.30	2	1.95	1.27	154	0.67	2.8	338.7	508.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
6.80	10.00	13.70	2	1.90	1.31	132	0.50	1.9	282.8	424.3	40.0	--	--	--	--	--	--	--	--	--	--	--	--
7.00	16.00	17.20	2	1.96	1.35	157	0.70	2.8	356.4	534.6	51.8	--	--	--	--	--	--	--	--	--	--	--	--
7.20	14.00	15.05	2	1.94	1.38	150	0.64	2.4	342.4	513.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
7.40	16.00	18.39	2	1.96	1.42	157	0.70	2.6	365.6	548.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
7.60	15.00	15.00	2	1.95	1.46	154	0.67	2.4	359.7	539.6	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.80	14.00	13.08	2	1.94	1.50	150	0.64	2.1	351.2	526.8	48.2	--	--	--	--	--	--	--	--	--	--	--	--
8.00	16.00	16.00	2	1.96	1.54	157	0.70	2.3	376.6	564.8	51.8	--	--	--	--	--	--	--	--	--	--	--	--
8.20	15.00	10.20	2	1.95	1.58	154	0.67	2.1	368.3	552.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
8.40	22.00	18.33	4	1.93	1.62	177	0.85	2.8	431.0	646.6	66.0	8	32	23	19	18	26	28	--	--	36.7	55.0	66.0
8.60	18.00	15.93	2	1.98	1.66	164	0.75	2.3	405.7	608.6	56.2	--	--	--	--	--	--	--	--	--	--	--	--
8.80	21.00	39.62	3	1.85	1.69	174	--	--	--	--	--	5	32	22	19	18	25	27	--	--	35.0	52.5	63.0
9.00	16.00	26.67	2	1.96	1.73	157	0.70	2.0	389.4	584.1	51.8	--	--	--	--	--	--	--	--	--	--	--	--
9.20	11.00	18.33	2	1.91	1.77	137	0.54	1.4	314.9	472.3	42.5	--	--	--	--	--	--	--	--	--	--	--	--
9.40	9.00	15.00	2	1.88	1.81	127	0.45	1.1	268.7	403.1	37.8	--	--	--	--	--	--	--	--	--	--	--	--
9.60	11.00	33.33	4	1.87	1.85	137	0.54	1.3	316.3	474.4	42.5	--	31	19	15	14	25	26	--	--	18.3	27.5	33.0
9.80	12.00	25.53	2	1.92	1.89	141	0.57	1.4	335.3	502.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
10.00	9.00	13.43	2	1.88	1.92	127	0.45	1.0	269.7	404.6	37.8	--	--	--	--	--	--	--	--	--	--	--	--
10.20	8.00	29.63	2	1.86	1.96	121	0.40	0.9	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
10.40	14.00	107.69	4	1.89	2.00	150	0.64	1.5	371.2	556.7	48.2	--	31	19	16	15	25	26	--	--	23.3	35.0	42.0
10.60	13.00	24.53	2	1.93	2.04	145	0.60	1.4	355.6	533.4	46.5	--	--	--	--	--	--	--	--	--	--	--	--
10.80	9.00	16.98	2	1.88	2.07	127	0.45	0.9	270.0	405.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
11.00	8.00	8.00	2	1.86	2.11	121	0.40	0.8	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
11.20	18.00	15.93	2	1.98	2.15	164	0.75	1.7	431.7	647.6	56.2	--	--	--	--	--	--	--	--	--	--	--	--
11.40	14.00	20.90	2	1.94	2.19	150	0.64	1.3	375.1	562.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
11.60	20.00	33.33	4	1.93	2.23	171	0.80	1.7	458.2	687.3	60.0	--	31	21	17	16	25	27	--	--	33.3	50.0	60.0
11.80	18.00	22.50	2	1.98	2.27	164	0.75	1.6	435.2	652.8	56.2	--	--	--	--	--	--	--	--	--	--	--	--
12.00	19.00	--	3	1.85	2.30	168	--	--	--	--	--	--	31	20	17	16	25	27	--	--	31.7	47.5	57.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	12
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	13.00	9.29	2	1.93	0.04	145	0.60	99.9	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
0.40	9.00	9.00	2	1.88	0.08	127	0.45	57.8	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
0.60	10.00	8.85	2	1.90	0.11	132	0.50	39.8	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
0.80	16.00	12.03	2	1.96	0.15	157	0.70	41.5	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.00	17.00	9.83	2	1.97	0.19	161	0.72	32.8	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
1.20	16.00	14.95	2	1.96	0.23	157	0.70	24.8	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.40	23.00	13.29	4	1.94	0.27	180	0.87	26.9	147.5	221.3	69.0	53	38	32	29	27	36	28	--	--	38.3	57.5	69.0
1.60	19.00	10.98	2	1.99	0.31	168	0.78	19.7	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
1.80	23.00	13.77	4	1.94	0.35	180	0.87	19.6	147.5	221.3	69.0	47	37	31	28	26	35	28	--	--	38.3	57.5	69.0
2.00	22.00	13.75	4	1.93	0.39	177	0.85	16.6	143.8	215.8	66.0	43	36	30	27	25	34	28	--	--	36.7	55.0	66.0
2.20	22.00	14.38	4	1.93	0.43	177	0.85	14.8	143.8	215.8	66.0	41	36	29	26	25	33	28	--	--	36.7	55.0	66.0
2.40	22.00	15.71	4	1.93	0.47	177	0.85	13.3	143.8	215.8	66.0	39	36	29	26	24	33	28	--	--	36.7	55.0	66.0
2.60	17.00	12.14	2	1.97	0.50	161	0.72	9.8	123.3	184.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.80	18.00	15.93	2	1.98	0.54	164	0.75	9.4	130.1	195.1	56.2	--	--	--	--	--	--	--	--	--	--	--	--
3.00	17.00	17.00	2	1.97	0.58	161	0.72	8.2	139.3	209.0	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.20	17.00	23.29	2	1.97	0.62	161	0.72	7.6	152.1	228.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.40	14.00	15.05	2	1.94	0.66	150	0.64	6.0	175.4	263.1	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.60	12.00	12.90	2	1.92	0.70	141	0.57	4.9	194.0	290.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.80	19.00	14.29	2	1.99	0.74	168	0.78	6.7	189.2	283.7	58.1	--	--	--	--	--	--	--	--	--	--	--	--
4.00	22.00	19.47	4	1.93	0.78	177	0.85	7.0	195.8	293.7	66.0	26	34	26	23	22	30	28	--	--	36.7	55.0	66.0
4.20	19.00	23.75	2	1.99	0.82	168	0.78	5.9	218.1	327.1	58.1	--	--	--	--	--	--	--	--	--	--	--	--
4.40	9.00	11.25	2	1.88	0.86	127	0.45	2.8	228.6	343.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
4.60	8.00	15.09	2	1.86	0.89	121	0.40	2.3	217.1	325.7	35.2	--	--	--	--	--	--	--	--	--	--	--	--
4.80	20.00	37.74	4	1.93	0.93	171	0.80	5.2	255.6	383.4	60.0	18	33	25	22	20	28	27	--	--	33.3	50.0	60.0
5.00	19.00	28.36	2	1.99	0.97	168	0.78	4.7	270.0	404.9	58.1	--	--	--	--	--	--	--	--	--	--	--	--
5.20	25.00	41.67	3	1.86	1.01	186	--	--	--	--	--	24	34	26	22	21	29	28	--	--	41.7	62.5	75.0
5.40	22.00	46.81	3	1.86	1.05	177	--	--	--	--	--	19	34	25	22	20	28	28	--	--	36.7	55.0	66.0
5.60	26.00	55.32	3	1.87	1.08	189	--	--	--	--	--	24	34	26	22	21	29	28	--	--	43.3	65.0	78.0
5.80	25.00	34.25	3	1.86	1.12	186	--	--	--	--	--	22	34	25	22	21	29	28	--	--	41.7	62.5	75.0
6.00	23.00	43.40	3	1.86	1.16	180	--	--	--	--	--	18	33	25	21	20	28	28	--	--	38.3	57.5	69.0
6.20	22.00	55.00	3	1.86	1.19	177	--	--	--	--	--	16	33	24	21	20	28	28	--	--	36.7	55.0	66.0
6.40	33.00	35.48	3	1.88	1.23	207	--	--	--	--	--	29	35	26	23	22	30	29	--	--	55.0	82.5	99.0
6.60	20.00	37.74	4	1.93	1.27	171	0.80	3.5	358.5	537.8	60.0	11	33	23	20	19	27	27	--	--	33.3	50.0	60.0
6.80	11.00	23.40	2	1.91	1.31	137	0.54	2.1	298.8	448.2	42.5	--	--	--	--	--	--	--	--	--	--	--	--
7.00	17.00	19.54	2	1.97	1.35	161	0.72	2.9	363.6	545.4	54.1	--	--	--	--	--	--	--	--	--	--	--	--
7.20	22.00	27.50	4	1.93	1.39	177	0.85	3.4	389.8	584.7	66.0	12	33	24	20	19	27	28	--	--	36.7	55.0	66.0
7.40	20.00	22.99	4	1.93	1.43	171	0.80	3.0	391.5	587.3	60.0	8	32	23	20	18	26	27	--	--	33.3	50.0	60.0
7.60	13.00	19.40	2	1.93	1.46	145	0.60	2.1	336.0	504.1	46.5	--	--	--	--	--	--	--	--	--	--	--	--
7.80	13.00	21.67	2	1.93	1.50	145	0.60	2.0	338.2	507.3	46.5	--	--	--	--	--	--	--	--	--	--	--	--
8.00	15.00	28.30	2	1.95	1.54	154	0.67	2.2	365.8	548.7	49.5	--	--	--	--	--	--	--	--	--	--	--	--
8.20	15.00	25.00	2	1.95	1.58	154	0.67	2.1	368.4	552.7	49.5	--	--	--	--	--	--	--	--	--	--	--	--
8.40	17.00	28.33	2	1.97	1.62	161	0.72	2.3	393.1	589.6	54.1	--	--	--	--	--	--	--	--	--	--	--	--
8.60	16.00	20.00	2	1.96	1.66	157	0.70	2.1	385.1	577.6	51.8	--	--	--	--	--	--	--	--	--	--	--	--
8.80	25.00	47.17	3	1.86	1.70	186	--	--	--	--	--	11	33	23	20	19	26	28	--	--	41.7	62.5	75.0
9.00	20.00	27.40	4	1.93	1.74	171	0.80	2.4	430.0	645.0	60.0	3	32	22	19	18	25	27	--	--	33.3	50.0	60.0
9.20	15.00	20.55	2	1.95	1.77	154	0.67	1.8	378.6	567.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
9.40	14.00	26.42	2	1.94	1.81	150	0.64	1.7	365.9	548.8	48.2	--	--	--	--	--	--	--	--	--	--	--	--
9.60	13.00	21.67	2	1.93	1.85	145	0.60	1.5	351.5	527.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
9.80	14.00	26.42	2	1.94	1.89	150	0.64	1.6	368.3	552.5	48.2	--	--	--	--	--	--	--	--	--	--	--	--
10.00	13.00	27.66	2	1.93	1.93	145	0.60	1.5	353.4	530.1	46.5	--	--	--	--	--	--	--	--	--	--	--	--
10.20	12.00	30.00	4	1.88	1.97	141	0.57	1.3	336.8	505.2	44.6	--	31	19	15	15	25	26	--	--	20.0	30.0	36.0
10.40	11.00	23.40	2	1.91	2.00	137	0.54	1.2	318.7	478.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
10.60	9.00	19.15	2	1.88	2.04	127	0.45	0.9	270.0	405.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
10.80	8.00	17.02	2	1.86	2.08	121	0.40	0.8	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
11.00	11.00	11.83	2	1.91	2.12	137	0.54	1.1	320.0	480.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
11.20	21.00	44.68	3	1.85	2.15	174	--	--	--	--	--	--	31	21	18	17	25	27	--	--	35.0	52.5	63.0
11.40	16.00	30.19	4	1.90	2.19	157	0.70	1.5	405.9	608.9	51.8	--	31	20	16	15	25	27	--	--	26.7	40.0	48.0
11.60	10.00	--	3	1.83	2.23	132	--	--	--	--	--	--	31	17	14	13	25	26	--	--	16.7	25.0	30.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT 13
riferimento **78-2024**

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	4.00	8.51	1	1.46	0.03	93	0.20	69.6	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	4.00	10.00	1	1.46	0.06	93	0.20	29.2	8.0	12.0	6.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	5.00	6.85	1	1.46	0.09	101	0.25	23.3	10.0	15.0	7.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	10.00	13.70	2	1.90	0.13	132	0.50	35.3	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
1.00	11.00	11.83	2	1.91	0.16	137	0.54	27.7	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.20	16.00	14.95	2	1.96	0.20	157	0.70	29.3	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.40	16.00	14.16	2	1.96	0.24	157	0.70	23.5	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.60	16.00	12.03	2	1.96	0.28	157	0.70	19.5	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.80	15.00	10.71	2	1.95	0.32	154	0.67	15.7	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.00	14.00	11.67	2	1.94	0.36	150	0.64	12.8	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.20	17.00	15.04	2	1.97	0.40	161	0.72	13.2	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.40	17.00	15.04	2	1.97	0.44	161	0.72	11.8	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.60	17.00	11.56	2	1.97	0.48	161	0.72	10.6	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.80	18.00	13.53	2	1.98	0.52	164	0.75	10.0	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
3.00	22.00	13.17	4	1.93	0.56	177	0.85	10.6	143.8	215.8	66.0	34	35	28	25	23	32	28	--	--	36.7	55.0	66.0
3.20	19.00	13.57	2	1.99	0.60	168	0.78	8.7	141.1	211.6	58.1	--	--	--	--	--	--	--	--	--	--	--	--
3.40	18.00	18.00	2	1.98	0.64	164	0.75	7.7	154.0	231.0	56.2	--	--	--	--	--	--	--	--	--	--	--	--
3.60	17.00	18.28	2	1.97	0.67	161	0.72	6.9	170.6	255.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.80	17.00	15.04	2	1.97	0.71	161	0.72	6.4	185.2	277.8	54.1	--	--	--	--	--	--	--	--	--	--	--	--
4.00	19.00	26.03	2	1.99	0.75	168	0.78	6.5	194.2	291.3	58.1	--	--	--	--	--	--	--	--	--	--	--	--
4.20	17.00	21.25	2	1.97	0.79	161	0.72	5.6	214.0	321.0	54.1	--	--	--	--	--	--	--	--	--	--	--	--
4.40	18.00	30.00	4	1.91	0.83	164	0.75	5.5	225.1	337.6	56.2	18	33	25	22	21	28	27	--	--	30.0	45.0	54.0
4.60	18.00	22.50	2	1.98	0.87	164	0.75	5.2	238.7	358.1	56.2	--	--	--	--	--	--	--	--	--	--	--	--
4.80	17.00	17.00	2	1.97	0.91	161	0.72	4.7	253.0	379.6	54.1	--	--	--	--	--	--	--	--	--	--	--	--
5.00	16.00	23.88	2	1.96	0.95	157	0.70	4.3	265.2	397.8	51.8	--	--	--	--	--	--	--	--	--	--	--	--
5.20	18.00	26.87	2	1.98	0.99	164	0.75	4.4	276.0	414.0	56.2	--	--	--	--	--	--	--	--	--	--	--	--
5.40	14.00	20.90	2	1.94	1.03	150	0.64	3.4	289.4	434.2	48.2	--	--	--	--	--	--	--	--	--	--	--	--
5.60	15.00	14.02	2	1.95	1.07	154	0.67	3.5	300.7	451.1	49.5	--	--	--	--	--	--	--	--	--	--	--	--
5.80	17.00	23.29	2	1.97	1.11	161	0.72	3.7	312.2	468.4	54.1	--	--	--	--	--	--	--	--	--	--	--	--
6.00	17.00	18.28	2	1.97	1.15	161	0.72	3.5	323.2	484.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
6.20	18.00	26.87	2	1.98	1.19	164	0.75	3.5	334.5	501.7	56.2	--	--	--	--	--	--	--	--	--	--	--	--
6.40	30.00	28.04	4	1.96	1.22	199	1.00	4.9	339.1	508.7	90.0	26	34	26	22	21	29	29	--	--	50.0	75.0	90.0
6.60	12.00	15.00	2	1.92	1.26	141	0.57	2.3	309.1	463.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
6.80	19.00	20.43	2	1.99	1.30	168	0.78	3.3	364.2	546.3	58.1	--	--	--	--	--	--	--	--	--	--	--	--
7.00	17.00	12.14	2	1.97	1.34	161	0.72	2.9	362.6	543.9	54.1	--	--	--	--	--	--	--	--	--	--	--	--
7.20	13.00	13.98	2	1.93	1.38	145	0.60	2.2	330.5	495.8	46.5	--	--	--	--	--	--	--	--	--	--	--	--
7.40	15.00	12.50	2	1.95	1.42	154	0.67	2.4	355.9	533.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.60	18.00	15.00	2	1.98	1.46	164	0.75	2.7	385.4	578.0	56.2	--	--	--	--	--	--	--	--	--	--	--	--
7.80	24.00	16.33	4	1.94	1.50	183	0.89	3.3	418.5	627.7	72.0	13	33	24	20	19	27	28	--	--	40.0	60.0	72.0
8.00	18.00	14.17	2	1.98	1.54	164	0.75	2.6	394.5	591.8	56.2	--	--	--	--	--	--	--	--	--	--	--	--
8.20	10.00	13.70	2	1.90	1.58	132	0.50	1.5	291.8	437.6	40.0	--	--	--	--	--	--	--	--	--	--	--	--
8.40	12.00	16.44	2	1.92	1.61	141	0.57	1.7	328.1	492.1	44.6	--	--	--	--	--	--	--	--	--	--	--	--
8.60	9.00	16.98	2	1.88	1.65	127	0.45	1.2	266.8	400.3	37.8	--	--	--	--	--	--	--	--	--	--	--	--
8.80	9.00	19.15	2	1.88	1.69	127	0.45	1.2	267.3	401.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
9.00	8.00	24.24	2	1.86	1.73	121	0.40	1.0	239.9	359.9	35.2	--	--	--	--	--	--	--	--	--	--	--	--
9.20	7.00	25.93	2	1.84	1.76	115	0.35	0.8	210.0	315.0	32.2	--	--	--	--	--	--	--	--	--	--	--	--
9.40	11.00	13.75	2	1.91	1.80	137	0.54	1.4	315.5	473.2	42.5	--	--	--	--	--	--	--	--	--	--	--	--
9.60	9.00	15.00	2	1.88	1.84	127	0.45	1.1	269.0	403.5	37.8	--	--	--	--	--	--	--	--	--	--	--	--
9.80	21.00	35.00	3	1.85	1.88	174	--	--	--	--	--	3	32	22	18	17	25	27	--	--	35.0	52.5	63.0
10.00	23.00	34.33	3	1.86	1.91	180	--	--	--	--	--	6	32	22	19	18	25	28	--	--	38.3	57.5	69.0
10.20	16.00	21.92	2	1.96	1.95	157	0.70	1.7	399.0	598.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
10.40	24.00	35.82	3	1.86	1.99	183	--	--	--	--	--	6	32	22	19	18	25	28	--	--	40.0	60.0	72.0
10.60	22.00	46.81	3	1.86	2.03	177	--	--	--	--	--	3	32	22	18	17	25	28	--	--	36.7	55.0	66.0
10.80	23.00	38.33	3	1.86	2.06	180	--	--	--	--	--	4	32	22	18	17	25	28	--	--	38.3	57.5	69.0
11.00	13.00	16.25	2	1.93	2.10	145	0.60	1.3	356.8	535.1	46.5	--	--	--	--	--	--	--	--	--	--	--	--
11.20	11.00	11.83	2	1.91	2.14	137	0.54	1.1	320.2	480.4	42.5	--	--	--	--	--	--	--	--	--	--	--	--
11.40	14.00	17.50	2	1.94	2.18	150	0.64	1.3	374.9	562.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
11.60	12.00	12.00	2	1.92	2.22	141	0.57	1.2	340.4	510.5	44.6	--	--	--	--	--	--	--	--	--	--	--	--
11.80	11.00	11.00	2	1.91	2.26	137	0.54	1.0	321.3	482.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
12.00	13.00	--	3	1.83	2.29	145	--	--	--	--	--	--	31	18	15	14	25	26	--	--	21.7	32.5	39.0

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Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	14
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	6.00	8.22	1	1.46	0.03	109	0.30	99.9	12.0	18.0	9.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	6.00	7.50	1	1.46	0.06	109	0.30	48.6	12.0	18.0	9.0	--	--	--	--	--	--	--	--	--	--	--	--
0.60	9.00	7.50	2	1.88	0.10	127	0.45	43.3	76.5	114.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
0.80	11.00	9.73	2	1.91	0.13	137	0.54	35.5	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
1.00	10.00	5.35	2	1.90	0.17	132	0.50	23.8	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
1.20	10.00	25.00	2	1.90	0.21	132	0.50	18.5	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
1.40	15.00	11.81	2	1.95	0.25	154	0.67	21.5	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.60	15.00	11.28	2	1.95	0.29	154	0.67	17.9	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
1.80	22.00	13.75	4	1.93	0.33	177	0.85	20.6	143.8	215.8	66.0	47	37	31	28	26	35	28	--	--	36.7	55.0	66.0
2.00	19.00	12.93	2	1.99	0.37	168	0.78	16.0	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.20	15.00	8.33	2	1.95	0.41	154	0.67	11.7	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.40	11.00	11.83	2	1.91	0.44	137	0.54	8.0	106.7	160.1	42.5	--	--	--	--	--	--	--	--	--	--	--	--
2.60	15.00	16.13	2	1.95	0.48	154	0.67	9.4	115.5	173.2	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.80	16.00	14.95	2	1.96	0.52	157	0.70	9.0	123.8	185.7	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.00	14.00	11.67	2	1.94	0.56	150	0.64	7.4	138.3	207.4	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.20	12.00	12.90	2	1.92	0.60	141	0.57	5.9	159.3	238.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
3.40	18.00	13.53	2	1.98	0.64	164	0.75	7.7	155.3	232.9	56.2	--	--	--	--	--	--	--	--	--	--	--	--
3.60	16.00	17.20	2	1.96	0.68	157	0.70	6.5	175.0	262.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.80	11.00	20.75	2	1.91	0.72	137	0.54	4.4	200.0	300.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
4.00	12.00	25.53	2	1.92	0.75	141	0.57	4.4	210.6	315.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
4.20	9.00	19.15	2	1.88	0.79	127	0.45	3.1	218.5	327.8	37.8	--	--	--	--	--	--	--	--	--	--	--	--
4.40	7.00	21.21	2	1.84	0.83	115	0.35	2.1	193.4	290.1	32.2	--	--	--	--	--	--	--	--	--	--	--	--
4.60	8.00	15.09	2	1.86	0.87	121	0.40	2.4	214.9	322.3	35.2	--	--	--	--	--	--	--	--	--	--	--	--
4.80	19.00	57.58	4	1.92	0.90	168	0.78	5.2	248.2	372.4	58.1	17	33	25	22	20	28	27	--	--	31.7	47.5	57.0
5.00	28.00	41.79	3	1.87	0.94	194	--	--	--	--	--	30	35	27	23	22	30	28	--	--	46.7	70.0	84.0
5.20	20.00	29.85	4	1.93	0.98	171	0.80	4.9	271.6	407.4	60.0	17	33	25	21	20	28	27	--	--	33.3	50.0	60.0
5.40	28.00	38.36	3	1.87	1.02	194	--	--	--	--	--	28	35	26	23	22	30	28	--	--	46.7	70.0	84.0
5.60	22.00	36.67	3	1.86	1.06	177	--	--	--	--	--	19	33	25	22	20	28	28	--	--	36.7	55.0	66.0
5.80	21.00	31.34	3	1.85	1.09	174	--	--	--	--	--	16	33	24	21	20	28	27	--	--	35.0	52.5	63.0
6.00	10.00	21.28	2	1.90	1.13	132	0.50	2.3	272.5	408.7	40.0	--	--	--	--	--	--	--	--	--	--	--	--
6.20	15.00	37.50	4	1.89	1.17	154	0.67	3.1	322.7	484.0	49.5	3	32	22	19	18	26	27	--	--	25.0	37.5	45.0
6.40	16.00	23.88	2	1.96	1.21	157	0.70	3.2	334.5	501.8	51.8	--	--	--	--	--	--	--	--	--	--	--	--
6.60	16.00	20.00	2	1.96	1.25	157	0.70	3.0	341.6	512.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
6.80	20.00	21.51	4	1.93	1.28	171	0.80	3.5	362.1	543.1	60.0	11	33	23	20	19	27	27	--	--	33.3	50.0	60.0
7.00	19.00	20.43	2	1.99	1.32	168	0.78	3.2	368.8	553.2	58.1	--	--	--	--	--	--	--	--	--	--	--	--
7.20	15.00	17.24	2	1.95	1.36	154	0.67	2.6	350.3	525.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.40	13.00	13.00	2	1.93	1.40	145	0.60	2.2	332.1	498.1	46.5	--	--	--	--	--	--	--	--	--	--	--	--
7.60	15.00	16.13	2	1.95	1.44	154	0.67	2.4	357.9	536.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.80	18.00	12.24	2	1.98	1.48	164	0.75	2.7	388.1	582.1	56.2	--	--	--	--	--	--	--	--	--	--	--	--
8.00	17.00	15.89	2	1.97	1.52	161	0.72	2.5	384.3	576.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
8.20	24.00	15.00	4	1.94	1.56	183	0.89	3.1	430.5	645.8	72.0	12	33	23	20	19	27	28	--	--	40.0	60.0	72.0
8.40	22.00	14.97	4	1.93	1.60	177	0.85	2.8	428.2	642.3	66.0	9	32	23	19	18	26	28	--	--	36.7	55.0	66.0
8.60	17.00	21.25	2	1.97	1.64	161	0.72	2.3	394.3	591.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
8.80	16.00	17.20	2	1.96	1.68	157	0.70	2.1	386.1	579.2	51.8	--	--	--	--	--	--	--	--	--	--	--	--
9.00	12.00	36.36	4	1.88	1.71	141	0.57	1.6	331.2	496.8	44.6	--	31	19	16	15	25	26	--	--	20.0	30.0	36.0
9.20	9.00	22.50	2	1.88	1.75	127	0.45	1.1	268.1	402.1	37.8	--	--	--	--	--	--	--	--	--	--	--	--
9.40	8.00	24.24	2	1.86	1.79	121	0.40	1.0	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
9.60	8.00	24.24	2	1.86	1.83	121	0.40	0.9	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
9.80	11.00	27.50	2	1.91	1.86	137	0.54	1.3	316.6	474.9	42.5	--	--	--	--	--	--	--	--	--	--	--	--
10.00	10.00	10.00	2	1.90	1.90	132	0.50	1.2	297.4	446.0	40.0	--	--	--	--	--	--	--	--	--	--	--	--
10.20	23.00	48.94	3	1.86	1.94	180	--	--	--	--	--	5	32	22	19	18	25	28	--	--	38.3	57.5	69.0
10.40	26.00	35.62	3	1.87	1.98	189	--	--	--	--	--	9	32	23	19	18	26	28	--	--	43.3	65.0	78.0
10.60	11.00	13.75	2	1.91	2.01	137	0.54	1.2	318.8	478.2	42.5	--	--	--	--	--	--	--	--	--	--	--	--
10.80	12.00	12.90	2	1.92	2.05	141	0.57	1.3	338.2	507.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
11.00	14.00	19.18	2	1.94	2.09	150	0.64	1.4	373.2	559.9	48.2	--	--	--	--	--	--	--	--	--	--	--	--
11.20	10.00	16.67	2	1.90	2.13	132	0.50	1.0	299.7	449.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
11.40	11.00	18.33	2	1.91	2.17	137	0.54	1.1	320.5	480.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
11.60	9.00	12.33	2	1.88	2.21	127	0.45	0.9	270.0	405.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
11.80	11.00	13.75	2	1.91	2.24	137	0.54	1.0	321.2	481.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
12.00	13.00	--	3	1.83	2.28	145	--	--	--	--	--	--	31	18	15	14	25	26	--	--	21.7	32.5	39.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT 15
riferimento **78-2024**

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 08/06/2007
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	12.00	15.00	2	1.92	0.04	141	0.57	99.9	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
0.40	11.00	7.48	2	1.91	0.08	137	0.54	71.5	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	11.00	8.66	2	1.91	0.11	137	0.54	43.1	91.2	136.8	42.5	--	--	--	--	--	--	--	--	--	--	--	--
0.80	10.00	7.87	2	1.90	0.15	132	0.50	27.6	85.0	127.5	40.0	--	--	--	--	--	--	--	--	--	--	--	--
1.00	12.00	8.16	2	1.92	0.19	141	0.57	24.7	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.20	12.00	9.02	2	1.92	0.23	141	0.57	19.6	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.40	12.00	10.00	2	1.92	0.27	141	0.57	16.2	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.60	12.00	10.62	2	1.92	0.31	141	0.57	13.7	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.80	12.00	12.90	2	1.92	0.34	141	0.57	11.8	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
2.00	15.00	14.02	2	1.95	0.38	154	0.67	12.5	113.3	170.0	49.5	--	--	--	--	--	--	--	--	--	--	--	--
2.20	14.00	13.08	2	1.94	0.42	150	0.64	10.5	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
2.40	17.00	14.17	2	1.97	0.46	161	0.72	11.0	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.60	16.00	12.60	2	1.96	0.50	157	0.70	9.5	120.1	180.2	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.80	15.00	14.02	2	1.95	0.54	154	0.67	8.2	129.1	193.6	49.5	--	--	--	--	--	--	--	--	--	--	--	--
3.00	17.00	14.17	2	1.97	0.58	161	0.72	8.3	138.1	207.1	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.20	17.00	14.17	2	1.97	0.62	161	0.72	7.6	150.7	226.0	54.1	--	--	--	--	--	--	--	--	--	--	--	--
3.40	14.00	12.39	2	1.94	0.66	150	0.64	6.0	173.9	260.8	48.2	--	--	--	--	--	--	--	--	--	--	--	--
3.60	15.00	17.24	2	1.95	0.70	154	0.67	5.9	185.0	277.5	49.5	--	--	--	--	--	--	--	--	--	--	--	--
3.80	17.00	15.04	2	1.97	0.74	161	0.72	6.1	193.4	290.1	54.1	--	--	--	--	--	--	--	--	--	--	--	--
4.00	15.00	15.00	2	1.95	0.78	154	0.67	5.2	212.6	318.8	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.20	12.00	22.64	2	1.92	0.81	141	0.57	4.0	227.0	340.5	44.6	--	--	--	--	--	--	--	--	--	--	--	--
4.40	16.00	18.39	2	1.96	0.85	157	0.70	4.9	236.2	354.3	51.8	--	--	--	--	--	--	--	--	--	--	--	--
4.60	12.00	20.00	2	1.92	0.89	141	0.57	3.6	251.6	377.4	44.6	--	--	--	--	--	--	--	--	--	--	--	--
4.80	11.00	16.42	2	1.91	0.93	137	0.54	3.2	257.7	386.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
5.00	12.00	36.36	4	1.88	0.97	141	0.57	3.3	269.8	404.8	44.6	--	31	22	19	18	25	26	--	--	20.0	30.0	36.0
5.20	17.00	25.37	2	1.97	1.01	161	0.72	4.2	281.0	421.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
5.40	12.00	25.53	2	1.92	1.04	141	0.57	3.0	284.0	426.0	44.6	--	--	--	--	--	--	--	--	--	--	--	--
5.60	12.00	30.00	4	1.88	1.08	141	0.57	2.8	289.6	434.4	44.6	--	31	22	18	17	25	26	--	--	20.0	30.0	36.0
5.80	24.00	25.81	4	1.94	1.12	183	0.89	4.7	311.7	467.5	72.0	20	34	25	22	20	28	28	--	--	40.0	60.0	72.0
6.00	13.00	27.66	2	1.93	1.16	145	0.60	2.8	308.5	462.7	46.5	--	--	--	--	--	--	--	--	--	--	--	--
6.20	22.00	30.14	3	1.86	1.20	177	--	--	--	--	--	16	33	24	21	20	28	28	--	--	36.7	55.0	66.0
6.40	14.00	20.90	2	1.94	1.24	150	0.64	2.7	326.6	489.9	48.2	--	--	--	--	--	--	--	--	--	--	--	--
6.60	11.00	20.75	2	1.91	1.27	137	0.54	2.1	296.6	444.9	42.5	--	--	--	--	--	--	--	--	--	--	--	--
6.80	19.00	14.96	2	1.99	1.31	168	0.78	3.2	366.5	549.7	58.1	--	--	--	--	--	--	--	--	--	--	--	--
7.00	16.00	16.00	2	1.96	1.35	157	0.70	2.7	357.3	536.0	51.8	--	--	--	--	--	--	--	--	--	--	--	--
7.20	15.00	16.13	2	1.95	1.39	154	0.67	2.5	353.2	529.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
7.40	23.00	18.11	4	1.94	1.43	180	0.87	3.4	401.5	602.3	69.0	13	33	24	20	19	27	28	--	--	38.3	57.5	69.0
7.60	25.00	17.86	4	1.94	1.47	186	0.91	3.4	413.7	620.6	75.0	15	33	24	21	19	27	28	--	--	41.7	62.5	75.0
7.80	22.00	23.66	4	1.93	1.51	177	0.85	3.0	414.1	621.1	66.0	10	32	23	20	19	26	28	--	--	36.7	55.0	66.0
8.00	12.00	13.79	2	1.92	1.55	141	0.57	1.8	325.5	488.3	44.6	--	--	--	--	--	--	--	--	--	--	--	--
8.20	10.00	14.93	2	1.90	1.58	132	0.50	1.5	292.0	437.9	40.0	--	--	--	--	--	--	--	--	--	--	--	--
8.40	8.00	29.63	2	1.86	1.62	121	0.40	1.1	239.0	358.5	35.2	--	--	--	--	--	--	--	--	--	--	--	--
8.60	11.00	27.50	2	1.91	1.66	137	0.54	1.5	312.3	468.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
8.80	8.00	17.02	2	1.86	1.70	121	0.40	1.0	239.7	359.5	35.2	--	--	--	--	--	--	--	--	--	--	--	--
9.00	8.00	20.00	2	1.86	1.73	121	0.40	1.0	240.0	359.9	35.2	--	--	--	--	--	--	--	--	--	--	--	--
9.20	8.00	20.00	2	1.86	1.77	121	0.40	1.0	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
9.40	9.00	15.00	2	1.88	1.81	127	0.45	1.1	268.7	403.1	37.8	--	--	--	--	--	--	--	--	--	--	--	--
9.60	20.00	27.40	4	1.93	1.85	171	0.80	2.2	438.8	658.2	60.0	2	31	22	18	17	25	27	--	--	33.3	50.0	60.0
9.80	9.00	16.98	2	1.88	1.89	127	0.45	1.0	269.4	404.1	37.8	--	--	--	--	--	--	--	--	--	--	--	--
10.00	16.00	23.88	2	1.96	1.92	157	0.70	1.8	397.9	596.9	51.8	--	--	--	--	--	--	--	--	--	--	--	--
10.20	12.00	17.91	2	1.92	1.96	141	0.57	1.3	336.7	505.1	44.6	--	--	--	--	--	--	--	--	--	--	--	--
10.40	27.00	40.30	3	1.87	2.00	192	--	--	--	--	--	10	32	23	19	18	26	28	--	--	45.0	67.5	81.0
10.60	29.00	39.73	3	1.87	2.04	197	--	--	--	--	--	12	33	23	20	19	26	29	--	--	48.3	72.5	87.0
10.80	25.00	23.36	4	1.94	2.08	186	0.91	2.2	497.0	745.5	75.0	7	32	22	19	18	25	28	--	--	41.7	62.5	75.0
11.00	16.00	14.16	2	1.96	2.12	157	0.70	1.6	404.0	606.0	51.8	--	--	--	--	--	--	--	--	--	--	--	--
11.20	19.00	12.42	2	1.99	2.16	168	0.78	1.7	444.0	666.0	58.1	--	--	--	--	--	--	--	--	--	--	--	--
11.40	25.00	17.86	4	1.94	2.19	186	0.91	2.1	504.8	757.2	75.0	5	32	22	18	17	25	28	--	--	41.7	62.5	75.0
11.60	31.00	38.75	3	1.88	2.23	202	--	--	--	--	--	12	33	23	19	18	26	29	--	--	51.7	77.5	93.0
11.80	26.00	17.69	4	1.95	2.27	189	0.93	2.1	517.3	776.0	78.0	6	32	22	18	18	25	28	--	--	43.3	65.0	78.0
12.00	22.00	--	3	1.86	2.31	177	--	--	--	--	--	--	31	21	18	17	25	28	--	--	36.7	55.0	66.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

Dott. Geol. Maurizio Zamboni
Via dei Giardini, 11
40036 Monzuno (BO)

PROVA PENETROMETRICA STATICA MECCANICA
PARAMETRI GEOTECNICI

CPT	16
riferimento	78-2024

Committente:	**GreenGo s.r.l.**	U.M.: **kg/cm²**	Data esec.: 25/11/2024
Cantiere:	**Realizzazione di un Campo agrivoltaico - progetto ´´Pratello´´**	Pagina: 1	
Località:	**Sala Bolognese (BO)**	Elaborato:	Falda: Non rilevata

							NATURA COESIVA					NATURA GRANULARE											
Prof.	qc	qc/fs	zone	γ'	σ'vo	Vs	Cu	OCR	Eu50	Eu25	Mo	Dr	Sc	Ca	Ko	DB	DM	Me	FLs	FLl	E'50	E'25	Mo
m	U.M.			t/m³	U.M.	m/s	U.M.	%	U.M.	U.M.	U.M.	%	(°)	(°)	(°)	(°)	(°)	(°)			U.M.	U.M.	U.M.
0.20	6.00	10.00	1	1.46	0.03	109	0.30	99.9	12.0	18.0	9.0	--	--	--	--	--	--	--	--	--	--	--	--
0.40	7.00	8.75	1	1.46	0.06	115	0.35	58.9	14.0	21.0	10.5	--	--	--	--	--	--	--	--	--	--	--	--
0.60	8.00	7.48	2	1.86	0.10	121	0.40	37.6	68.0	102.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
0.80	14.00	10.53	2	1.94	0.13	150	0.64	43.9	108.2	162.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
1.00	13.00	10.24	2	1.93	0.17	145	0.60	30.0	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.20	13.00	12.15	2	1.93	0.21	145	0.60	23.3	102.8	154.2	46.5	--	--	--	--	--	--	--	--	--	--	--	--
1.40	12.00	12.90	2	1.92	0.25	141	0.57	17.6	97.1	145.7	44.6	--	--	--	--	--	--	--	--	--	--	--	--
1.60	16.00	13.33	2	1.96	0.29	157	0.70	18.8	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
1.80	17.00	12.78	2	1.97	0.33	161	0.72	16.8	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.00	18.00	14.17	2	1.98	0.37	164	0.75	15.3	127.5	191.3	56.2	--	--	--	--	--	--	--	--	--	--	--	--
2.20	16.00	13.33	2	1.96	0.41	157	0.70	12.3	118.3	177.4	51.8	--	--	--	--	--	--	--	--	--	--	--	--
2.40	19.00	15.83	2	1.99	0.45	168	0.78	12.5	131.8	197.8	58.1	--	--	--	--	--	--	--	--	--	--	--	--
2.60	17.00	15.04	2	1.97	0.49	161	0.72	10.3	123.0	184.5	54.1	--	--	--	--	--	--	--	--	--	--	--	--
2.80	13.00	12.15	2	1.93	0.53	145	0.60	7.5	128.7	193.0	46.5	--	--	--	--	--	--	--	--	--	--	--	--
3.00	16.00	20.00	2	1.96	0.56	157	0.70	8.2	134.9	202.3	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.20	19.00	17.76	2	1.99	0.60	168	0.78	8.6	143.3	214.9	58.1	--	--	--	--	--	--	--	--	--	--	--	--
3.40	16.00	20.00	2	1.96	0.64	157	0.70	6.9	162.1	243.2	51.8	--	--	--	--	--	--	--	--	--	--	--	--
3.60	12.00	36.36	4	1.88	0.68	141	0.57	5.0	187.7	281.5	44.6	9	32	24	21	20	27	26	--	--	20.0	30.0	36.0
3.80	25.00	37.31	3	1.86	0.72	186	--	--	--	--	--	32	35	27	24	23	31	28	--	--	41.7	62.5	75.0
4.00	15.00	22.39	2	1.95	0.76	154	0.67	5.4	206.4	309.6	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.20	14.00	23.33	2	1.94	0.80	150	0.64	4.7	221.1	331.6	48.2	--	--	--	--	--	--	--	--	--	--	--	--
4.40	15.00	28.30	2	1.95	0.83	154	0.67	4.7	231.9	347.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
4.60	14.00	35.00	4	1.89	0.87	150	0.64	4.2	243.7	365.6	48.2	8	32	24	20	19	27	26	--	--	23.3	35.0	42.0
4.80	23.00	24.73	4	1.94	0.91	180	0.87	5.9	242.3	363.5	69.0	24	34	26	23	21	29	28	--	--	38.3	57.5	69.0
5.00	14.00	20.90	2	1.94	0.95	150	0.64	3.8	267.5	401.3	48.2	--	--	--	--	--	--	--	--	--	--	--	--
5.20	16.00	23.88	2	1.96	0.99	157	0.70	4.0	276.0	414.1	51.8	--	--	--	--	--	--	--	--	--	--	--	--
5.40	13.00	17.81	2	1.93	1.03	145	0.60	3.2	286.5	429.8	46.5	--	--	--	--	--	--	--	--	--	--	--	--
5.60	11.00	20.75	2	1.91	1.07	137	0.54	2.7	278.4	417.6	42.5	--	--	--	--	--	--	--	--	--	--	--	--
5.80	12.00	44.44	4	1.88	1.10	141	0.57	2.8	292.5	438.8	44.6	--	31	22	18	17	25	26	--	--	20.0	30.0	36.0
6.00	26.00	78.79	3	1.87	1.14	189	--	--	--	--	--	22	34	25	22	21	29	28	--	--	43.3	65.0	78.0
6.20	35.00	29.17	4	1.98	1.18	211	1.17	6.2	309.4	464.2	105.0	32	35	27	23	22	30	29	--	--	58.3	87.5	105.0
6.40	17.00	17.00	2	1.97	1.22	161	0.72	3.3	340.7	511.1	54.1	--	--	--	--	--	--	--	--	--	--	--	--
6.60	20.00	17.70	4	1.93	1.26	171	0.80	3.6	355.2	532.8	60.0	11	33	24	20	19	27	27	--	--	33.3	50.0	60.0
6.80	17.00	17.00	2	1.97	1.30	161	0.72	3.0	355.5	533.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
7.00	14.00	17.50	2	1.94	1.34	150	0.64	2.5	338.0	507.0	48.2	--	--	--	--	--	--	--	--	--	--	--	--
7.20	17.00	25.37	2	1.97	1.38	161	0.72	2.8	367.5	551.2	54.1	--	--	--	--	--	--	--	--	--	--	--	--
7.40	34.00	72.34	3	1.89	1.41	209	--	--	--	--	--	26	34	26	22	21	29	29	--	--	56.7	85.0	102.0
7.60	38.00	28.57	4	1.99	1.45	218	1.27	5.3	397.3	595.9	114.0	30	35	26	23	21	29	30	--	--	63.3	95.0	114.0
7.80	22.00	16.54	4	1.93	1.49	177	0.85	3.1	411.3	616.9	66.0	10	32	23	20	19	26	28	--	--	36.7	55.0	66.0
8.00	24.00	14.37	4	1.94	1.53	183	0.89	3.2	425.2	637.8	72.0	13	33	23	20	19	27	28	--	--	40.0	60.0	72.0
8.20	22.00	14.38	4	1.93	1.57	177	0.85	2.9	424.1	636.1	66.0	9	32	23	20	18	26	28	--	--	36.7	55.0	66.0
8.40	21.00	18.58	4	1.93	1.61	174	0.82	2.7	423.9	635.8	63.0	7	32	23	19	18	26	27	--	--	35.0	52.5	63.0
8.60	26.00	15.03	4	1.95	1.65	189	0.93	3.1	453.1	679.6	78.0	14	33	23	20	19	27	28	--	--	43.3	65.0	78.0
8.80	23.00	16.43	4	1.94	1.69	180	0.87	2.7	445.6	668.4	69.0	9	32	23	19	18	26	28	--	--	38.3	57.5	69.0
9.00	19.00	35.85	4	1.92	1.72	168	0.78	2.3	420.4	630.5	58.1	2	31	22	18	17	25	27	--	--	31.7	47.5	57.0
9.20	11.00	23.40	2	1.91	1.76	137	0.54	1.4	314.7	472.0	42.5	--	--	--	--	--	--	--	--	--	--	--	--
9.40	11.00	23.40	2	1.91	1.80	137	0.54	1.4	315.4	473.2	42.5	--	--	--	--	--	--	--	--	--	--	--	--
9.60	13.00	24.53	2	1.93	1.84	145	0.60	1.6	351.2	526.7	46.5	--	--	--	--	--	--	--	--	--	--	--	--
9.80	15.00	20.55	2	1.95	1.88	154	0.67	1.7	382.6	573.9	49.5	--	--	--	--	--	--	--	--	--	--	--	--
10.00	12.00	20.00	2	1.92	1.92	141	0.57	1.4	335.9	503.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
10.20	9.00	33.33	4	1.85	1.95	127	0.45	1.0	270.0	405.0	37.8	--	31	17	14	13	25	26	--	--	15.0	22.5	27.0
10.40	9.00	27.27	2	1.88	1.99	127	0.45	1.0	270.0	405.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
10.60	11.00	40.74	4	1.87	2.03	137	0.54	1.2	319.0	478.4	42.5	--	31	18	15	14	25	26	--	--	18.3	27.5	33.0
10.80	10.00	16.67	2	1.90	2.07	132	0.50	1.1	299.1	448.7	40.0	--	--	--	--	--	--	--	--	--	--	--	--
11.00	8.00	17.02	2	1.86	2.10	121	0.40	0.8	240.0	360.0	35.2	--	--	--	--	--	--	--	--	--	--	--	--
11.20	11.00	33.33	4	1.87	2.14	137	0.54	1.1	320.2	480.4	42.5	--	31	18	14	14	25	26	--	--	18.3	27.5	33.0
11.40	12.00	25.53	2	1.92	2.18	141	0.57	1.2	339.9	509.9	44.6	--	--	--	--	--	--	--	--	--	--	--	--
11.60	9.00	15.00	2	1.88	2.22	127	0.45	0.9	270.0	405.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
11.80	9.00	16.98	2	1.88	2.25	127	0.45	0.8	270.0	405.0	37.8	--	--	--	--	--	--	--	--	--	--	--	--
12.00	11.00	20.75	2	1.91	2.29	137	0.54	1.0	321.6	482.5	42.5	--	--	--	--	--	--	--	--	--	--	--	--
12.20	11.00	--	3	1.83	2.33	137	--	--	--	--	--	--	31	17	14	13	25	26	--	--	18.3	27.5	33.0

FON053

Software by dott. Geol. Diego Merlin 0425-840820

ALLEGATO II

- PROVE PENETROMETRICHE STATICHE ELETTRICHE
CON PIEZOCONO-

DIAGRAMMI DI RESISTENZA
--
VALUTAZIONI LITOLOGICHE
--
PARAMETRI GEOTECNICI

Dott. geol. Maurizio Zamboni
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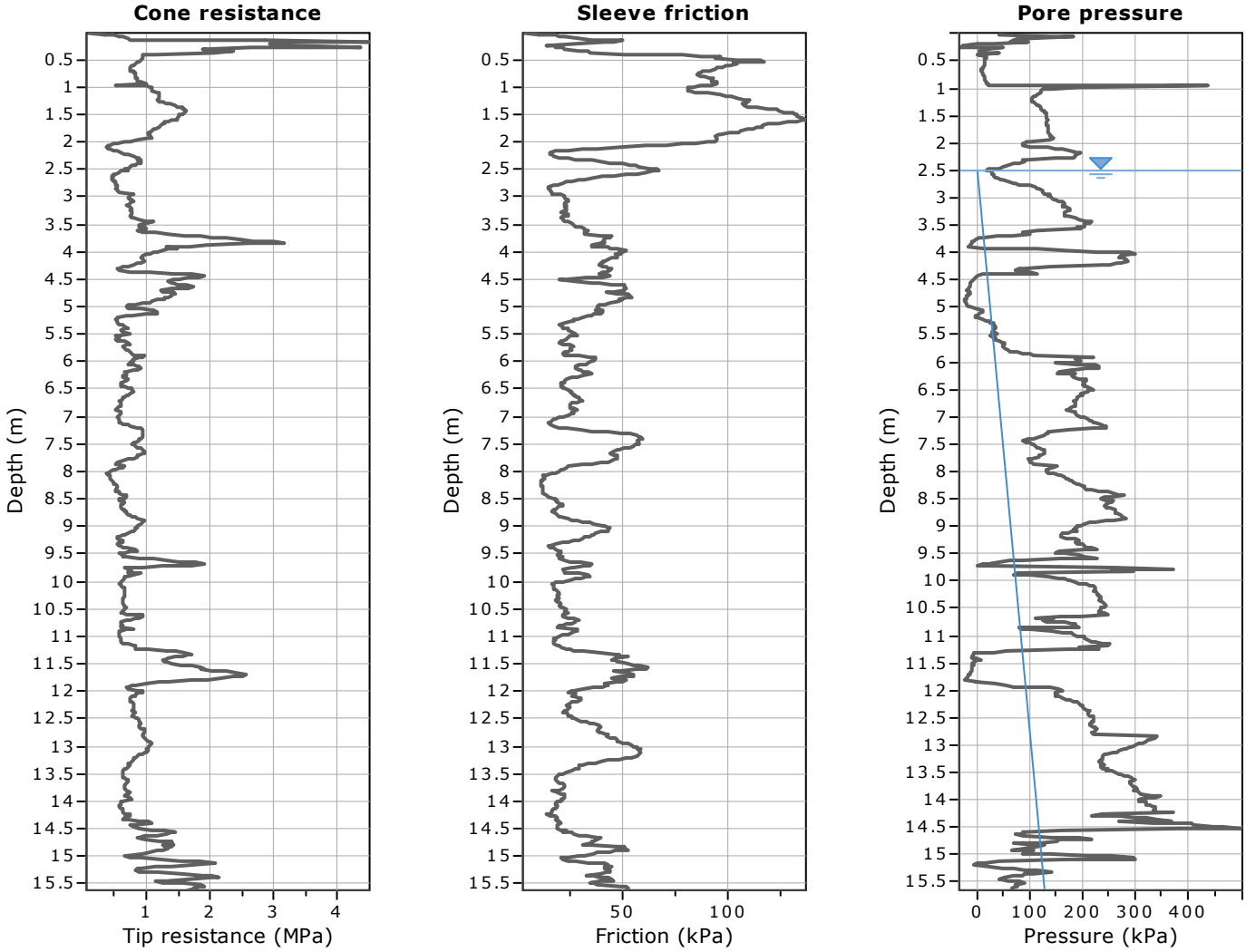
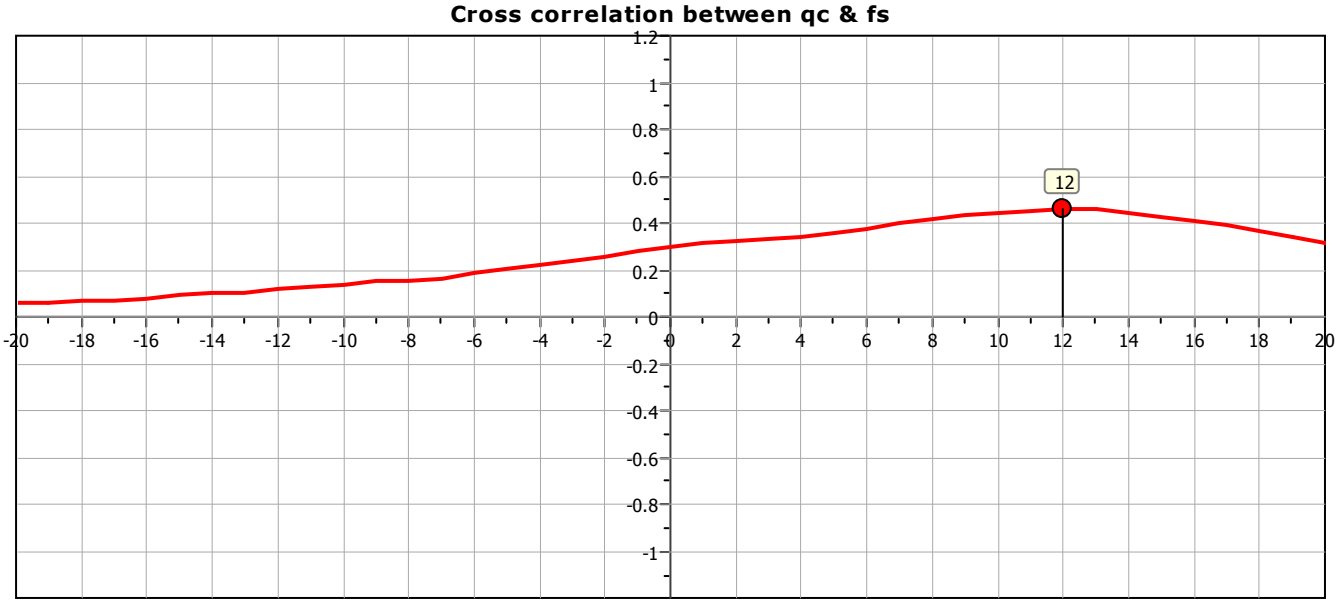
CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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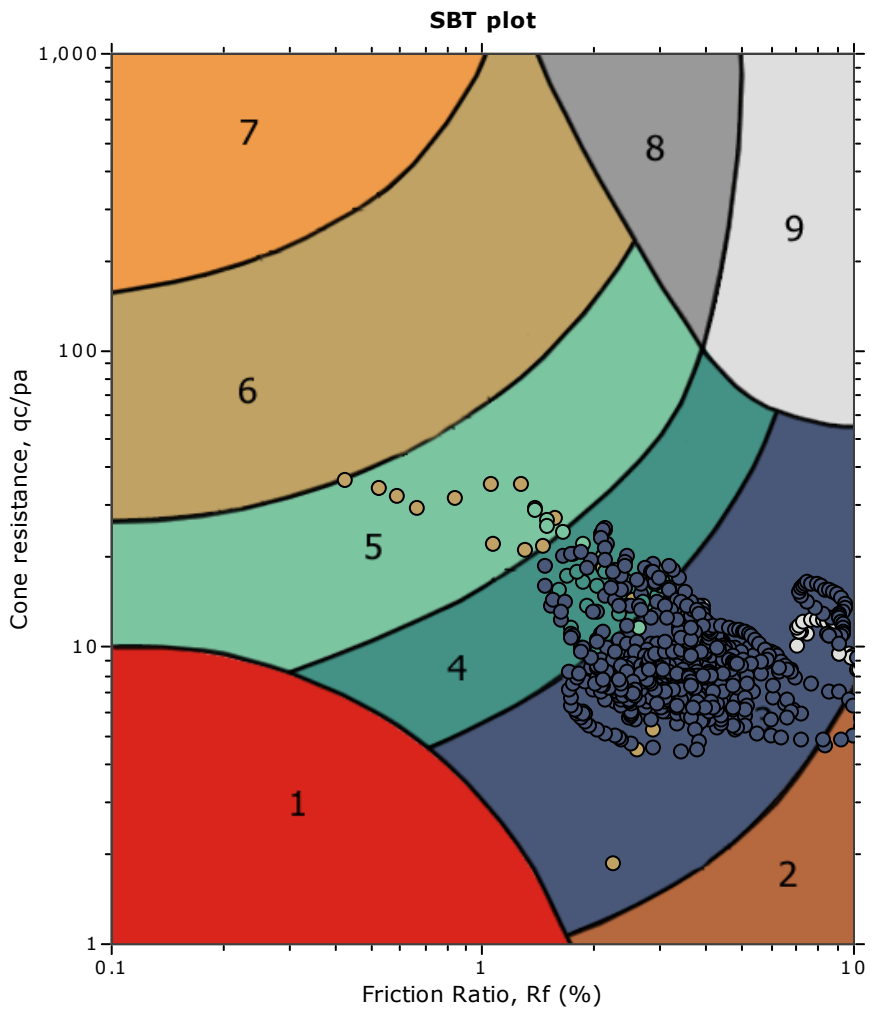
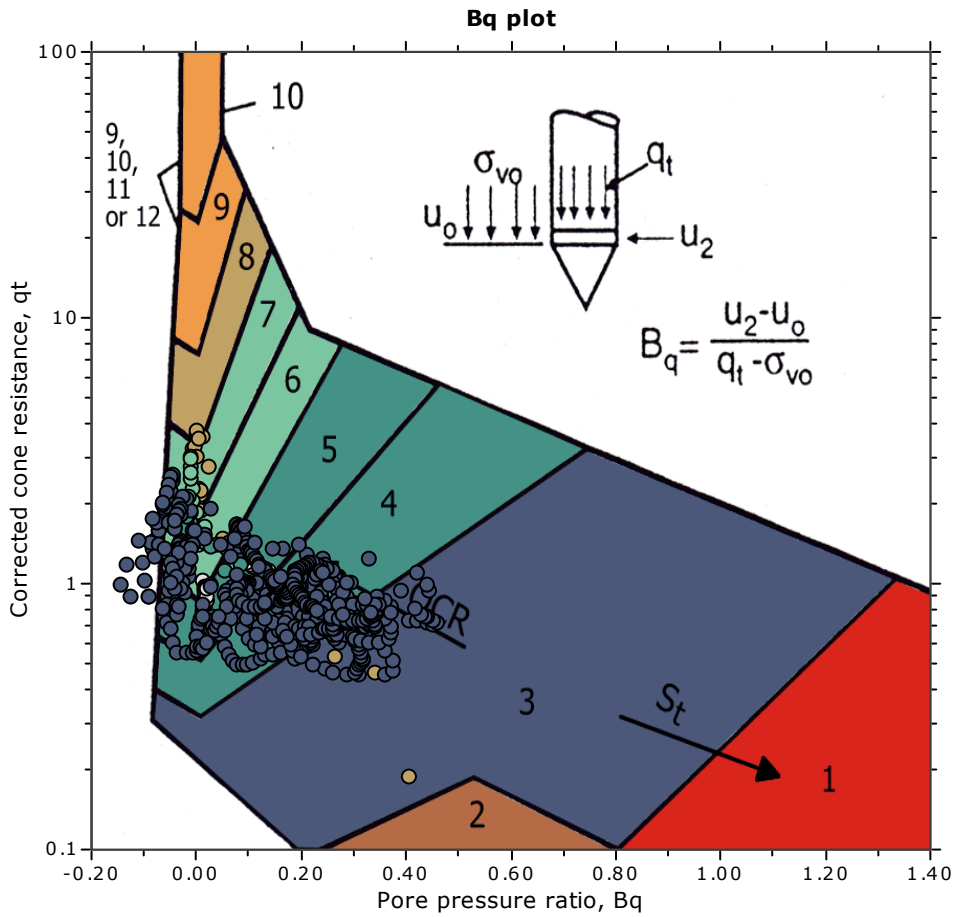
Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots





SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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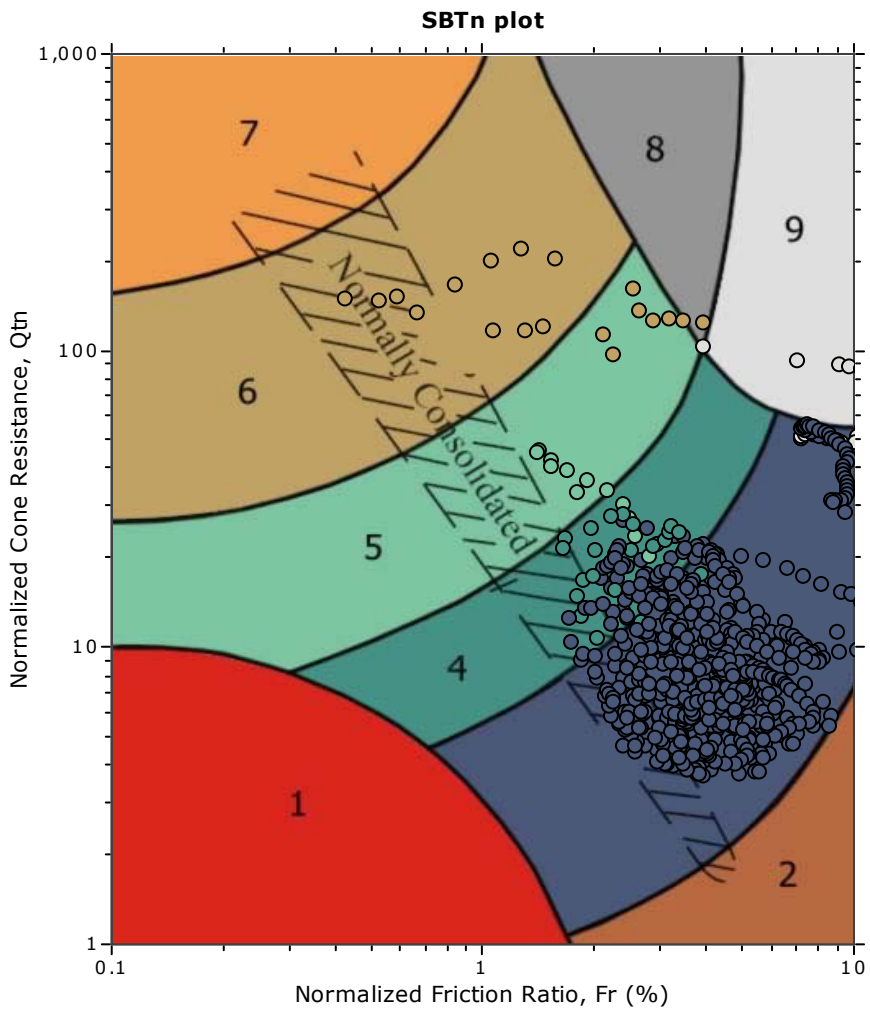
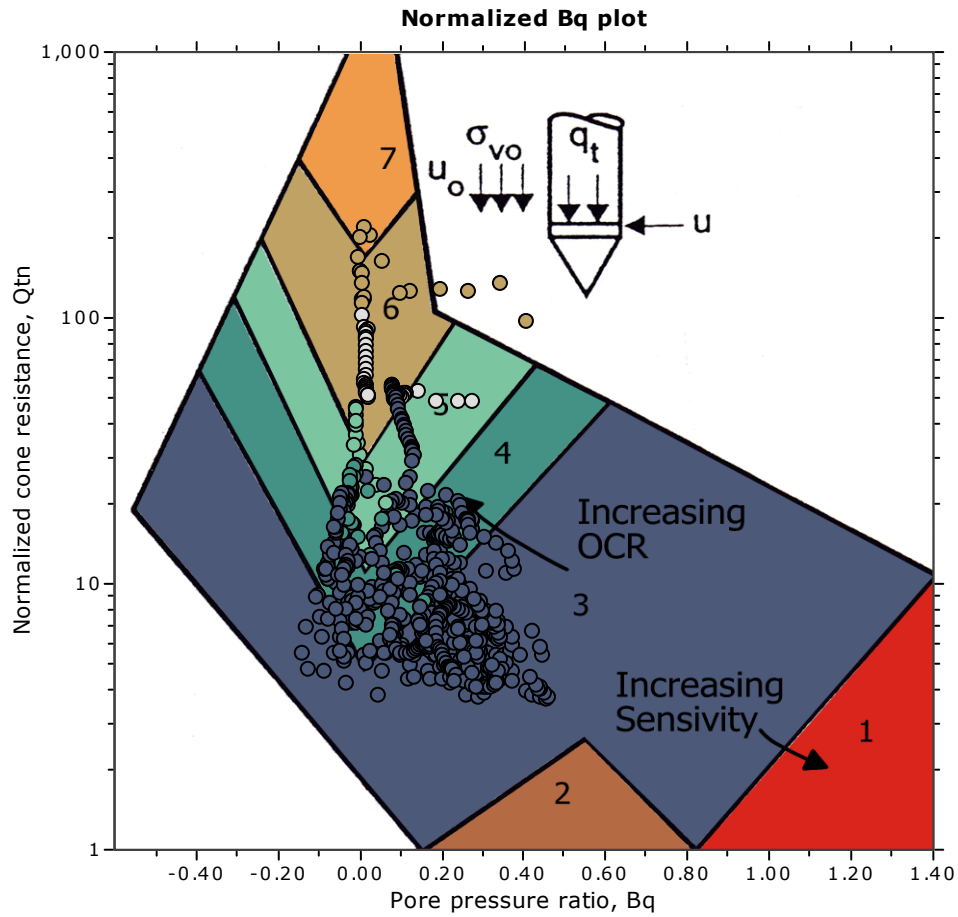
Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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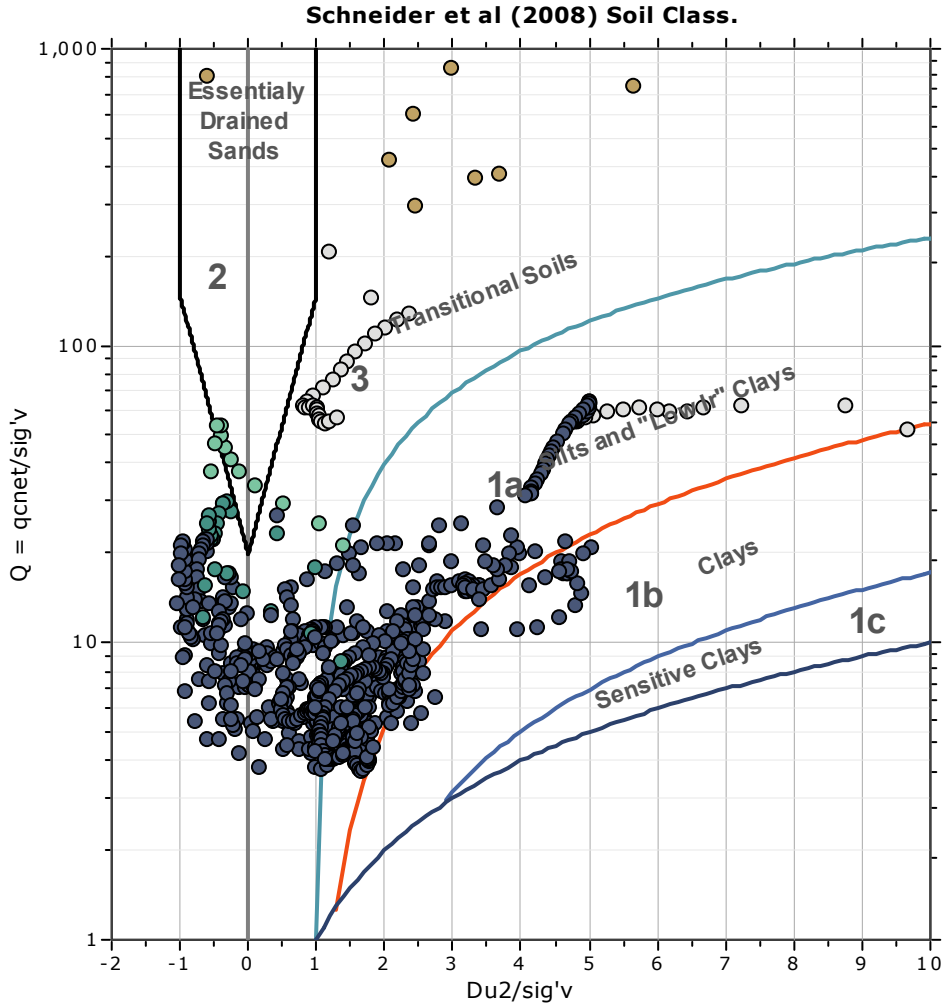
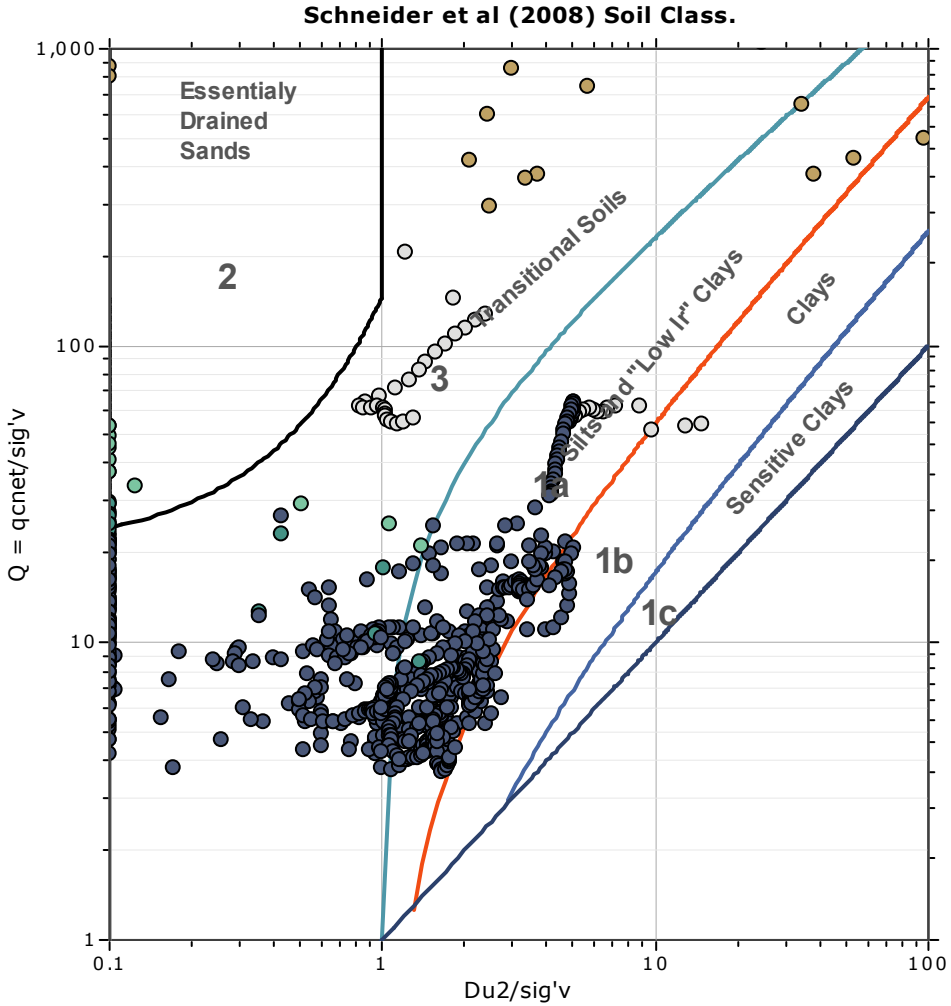
Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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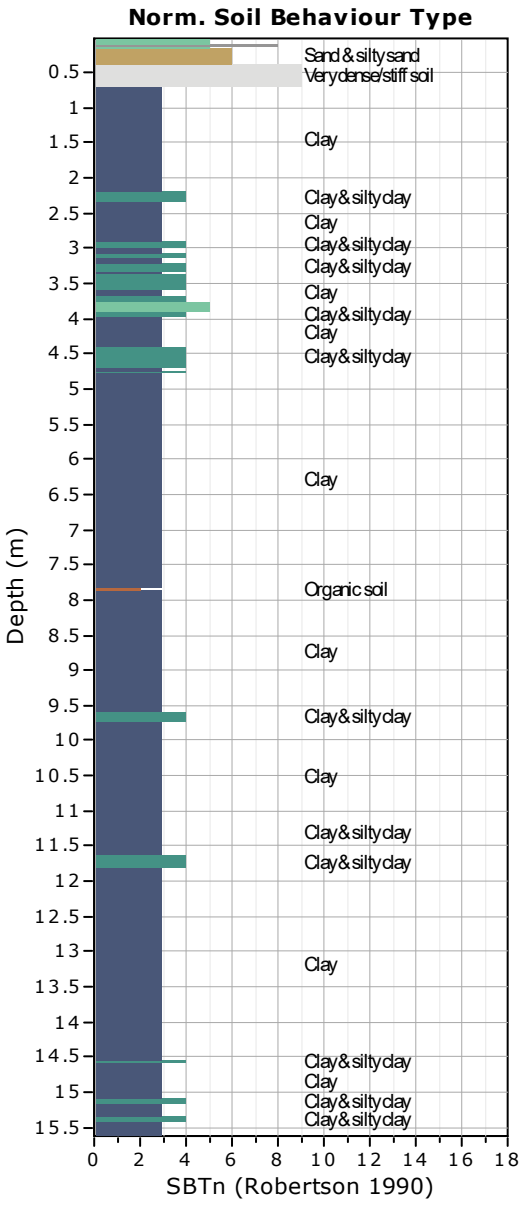
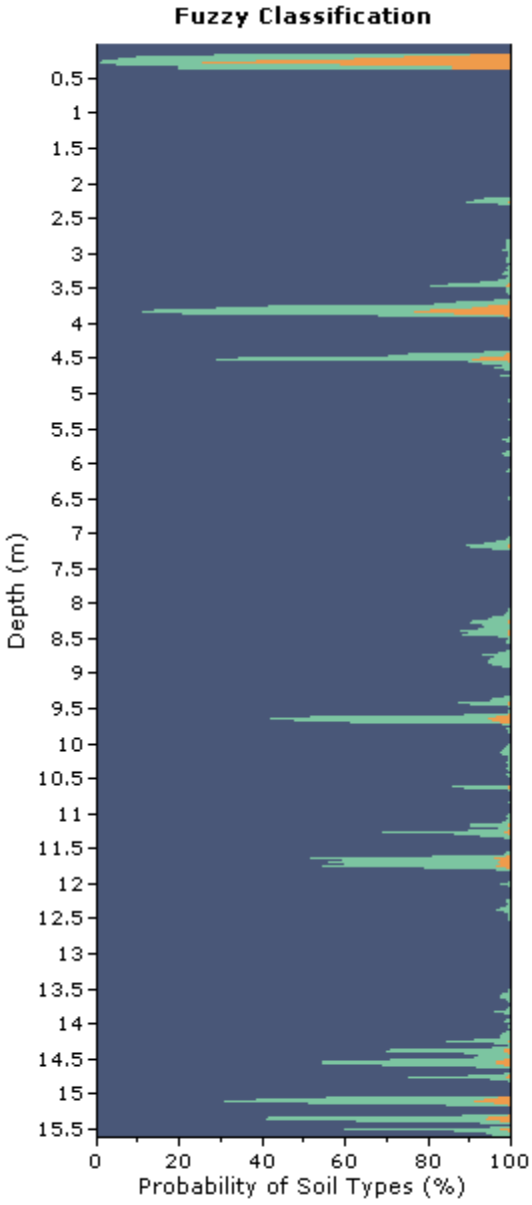
CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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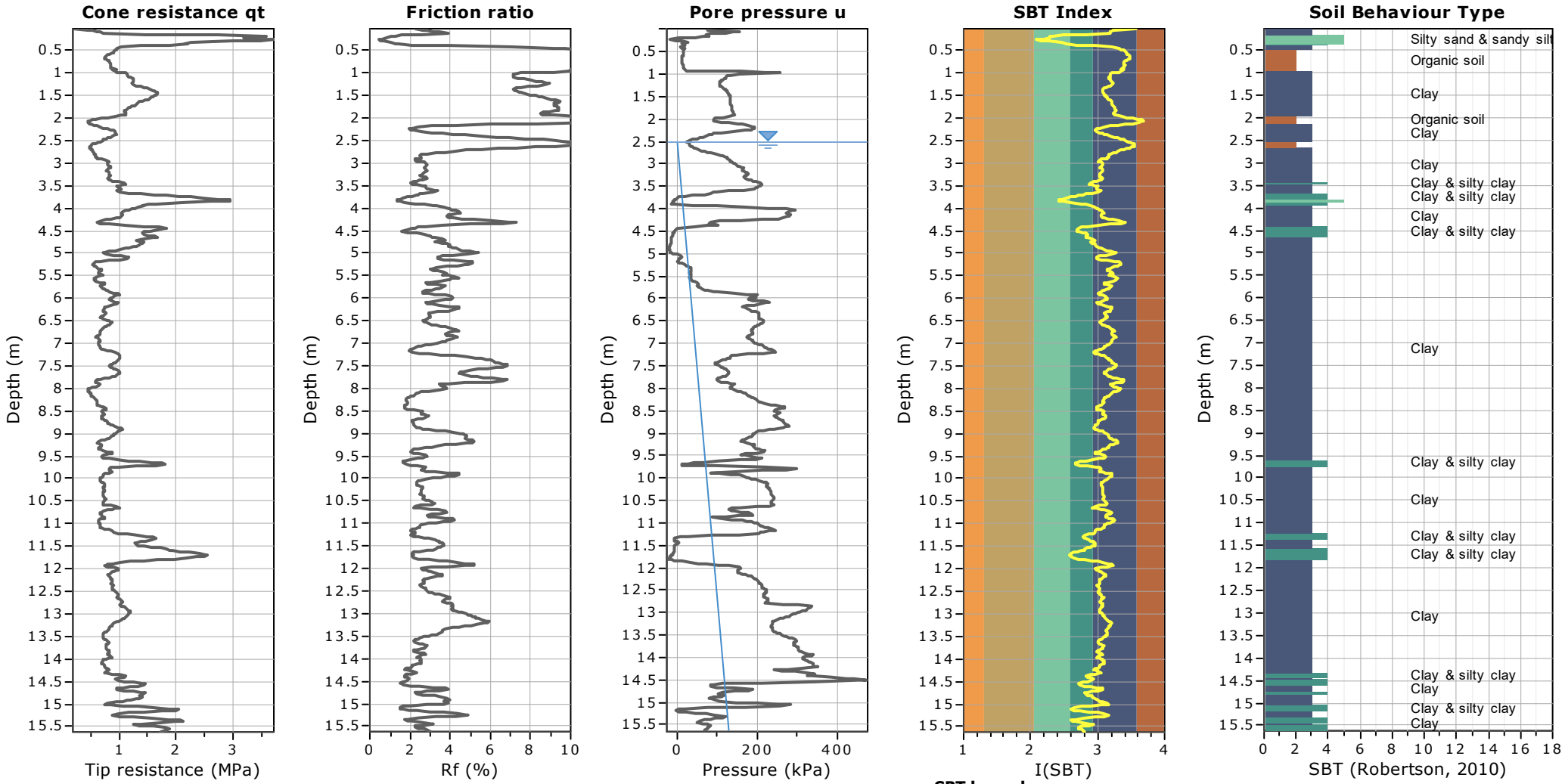
Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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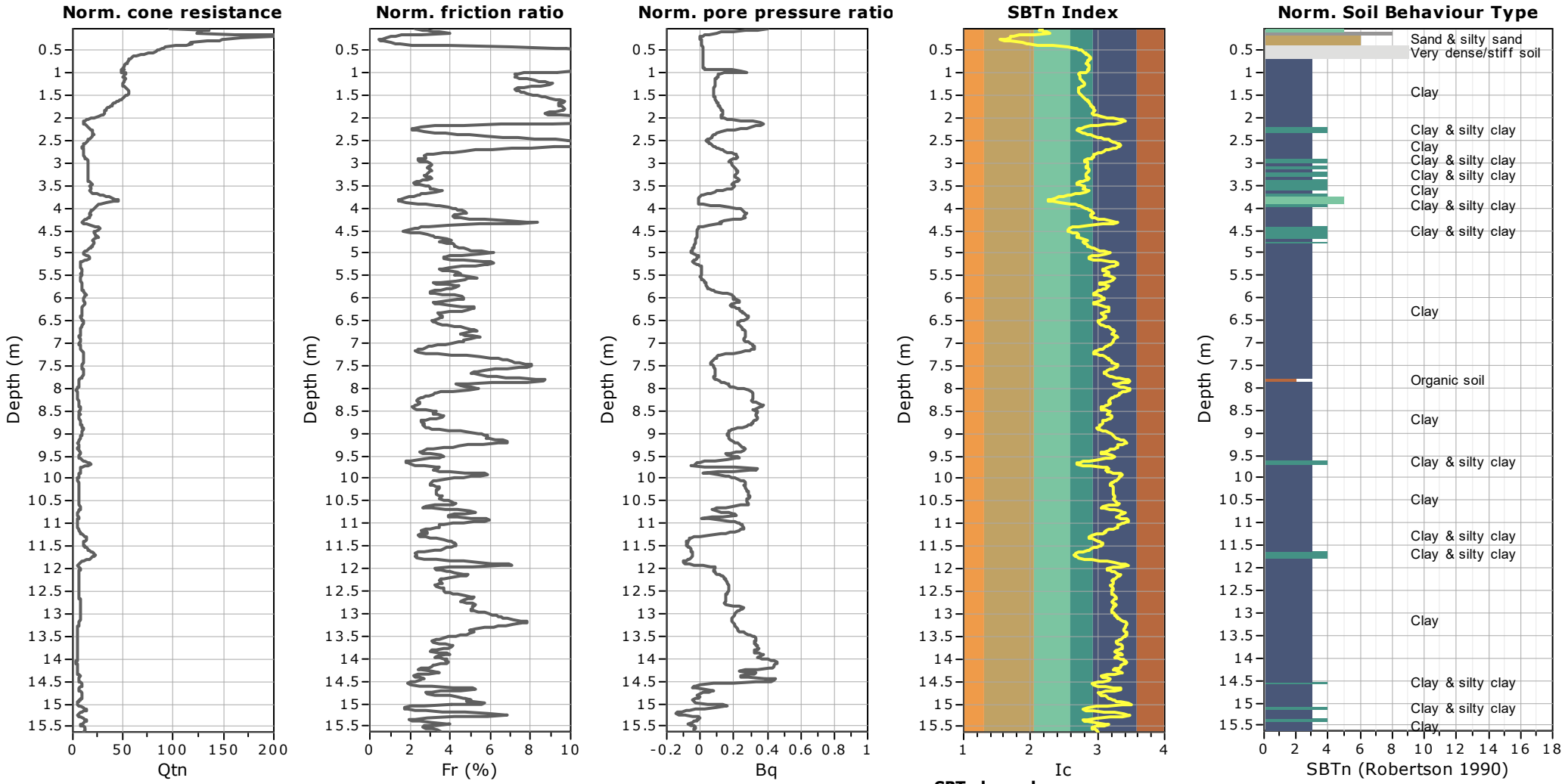
Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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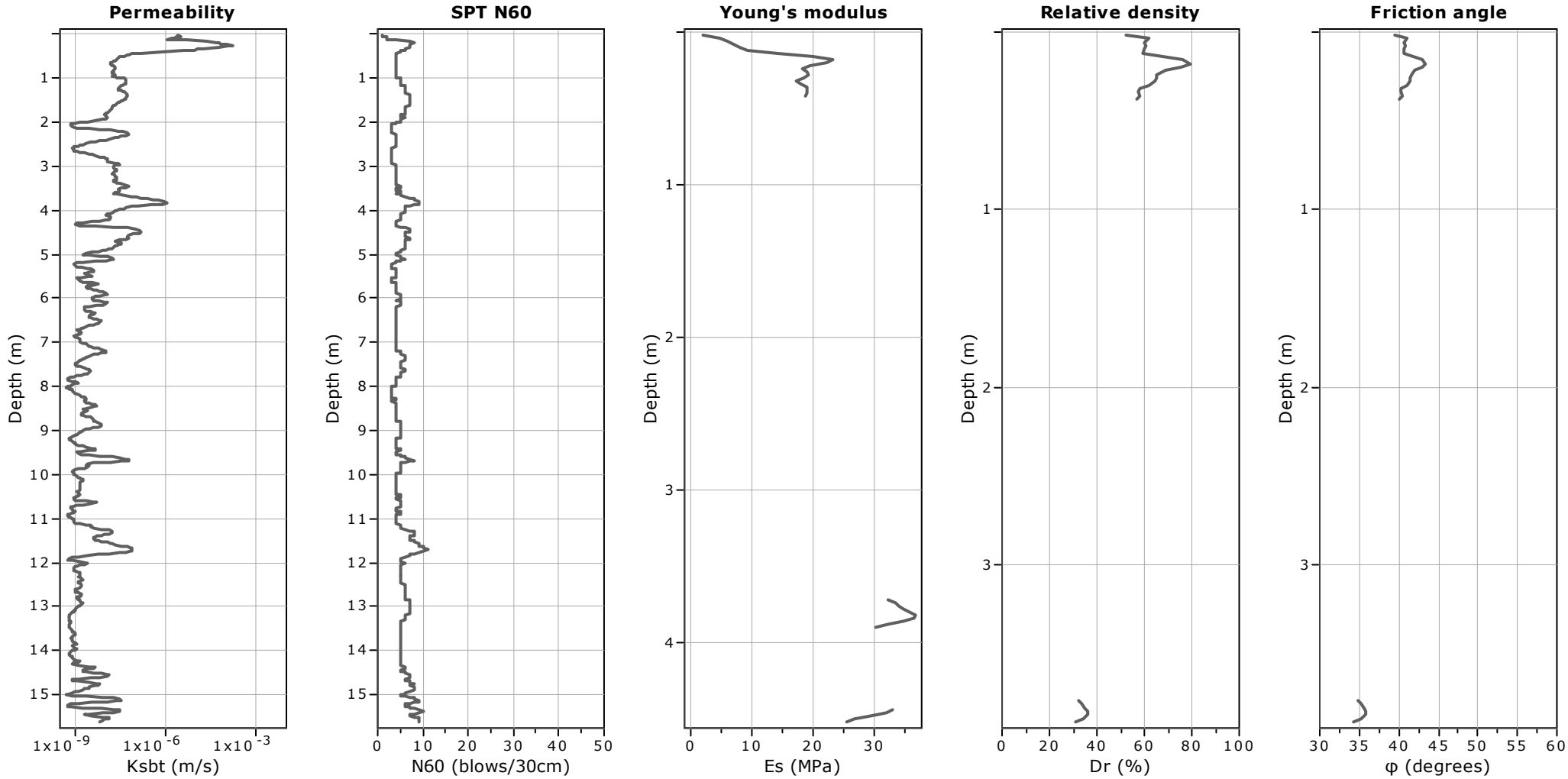
Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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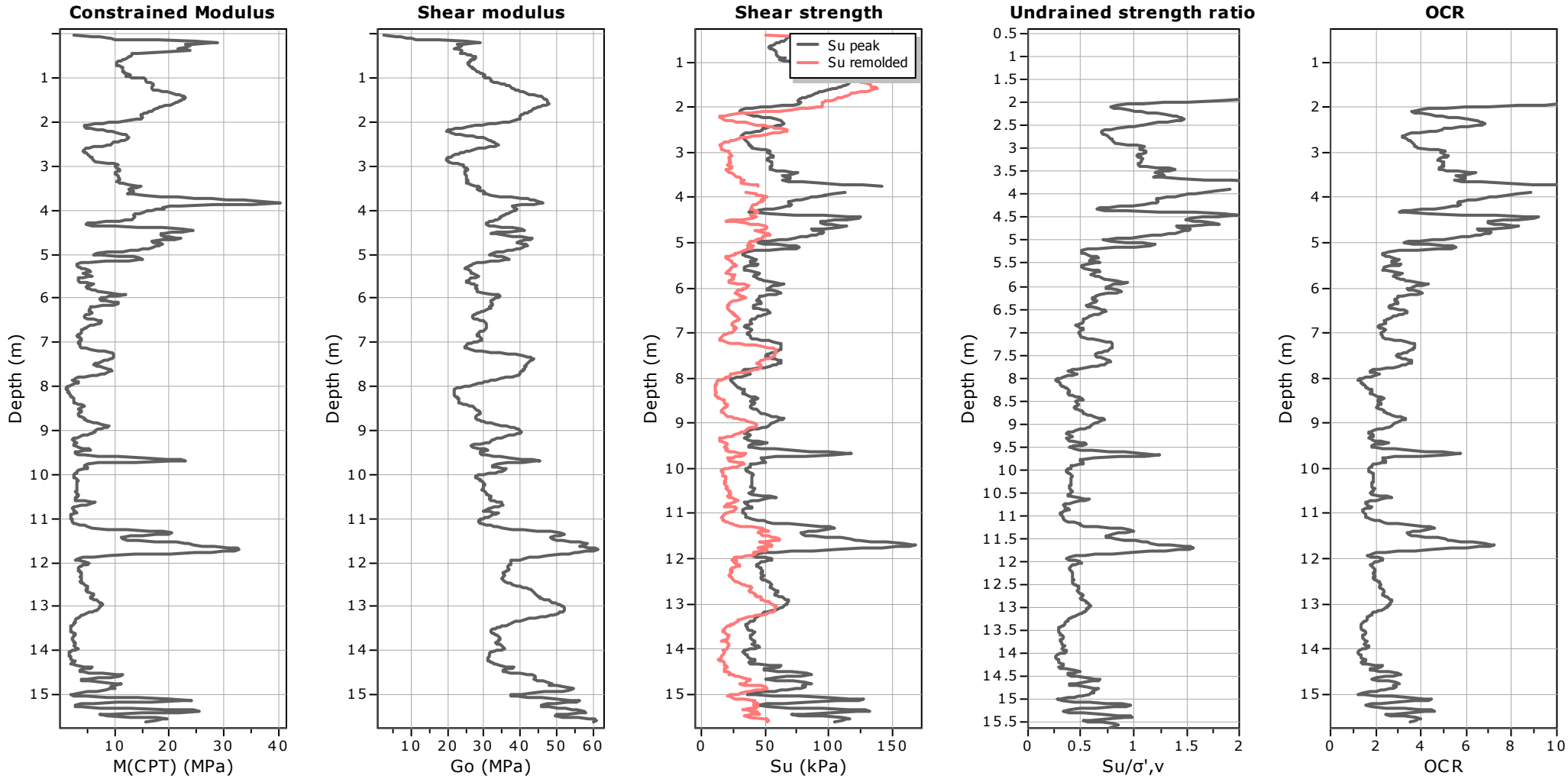
Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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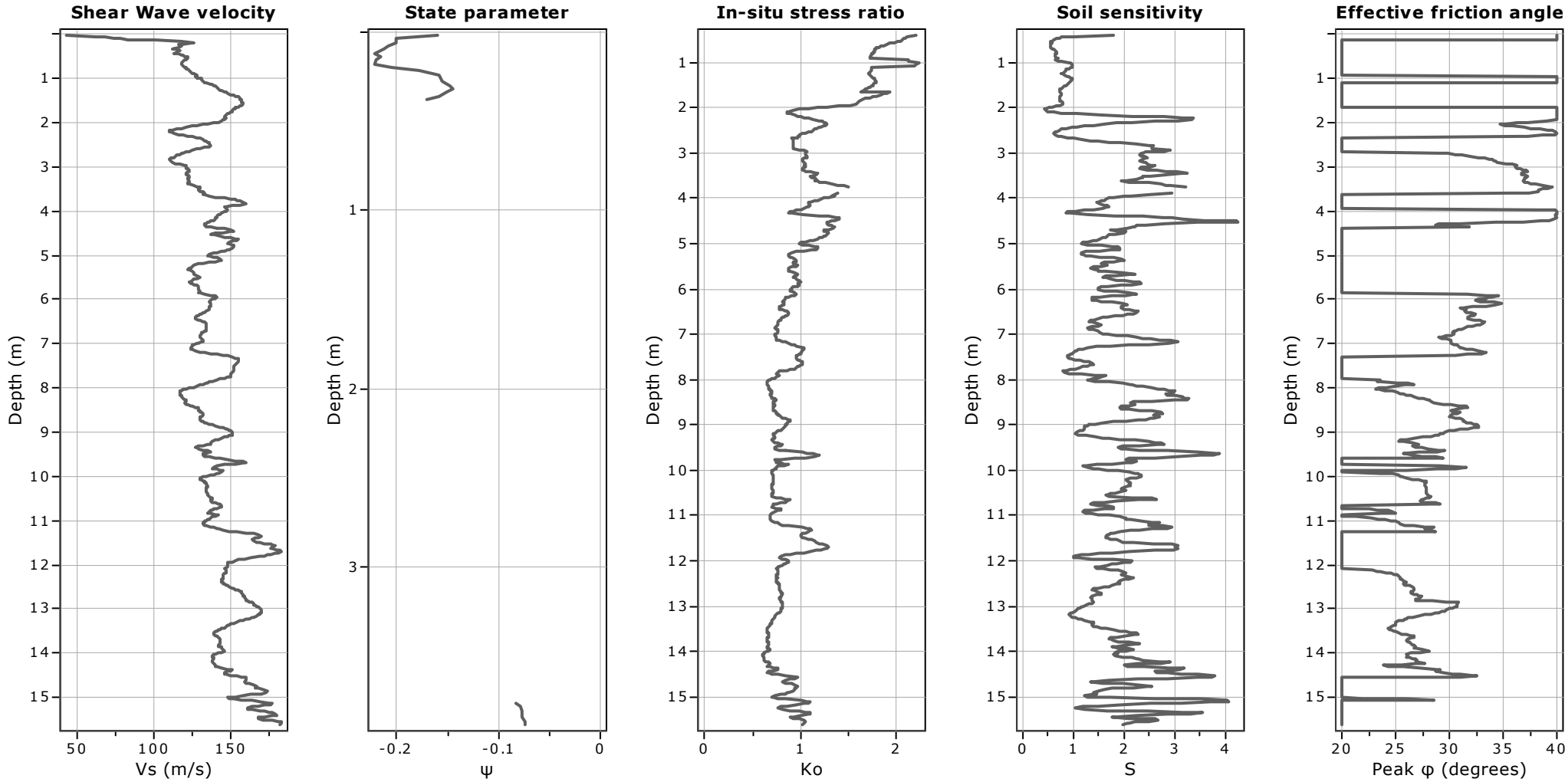
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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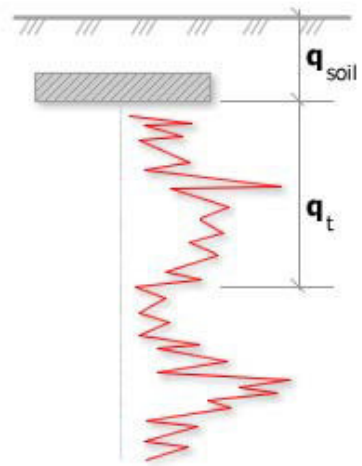
CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

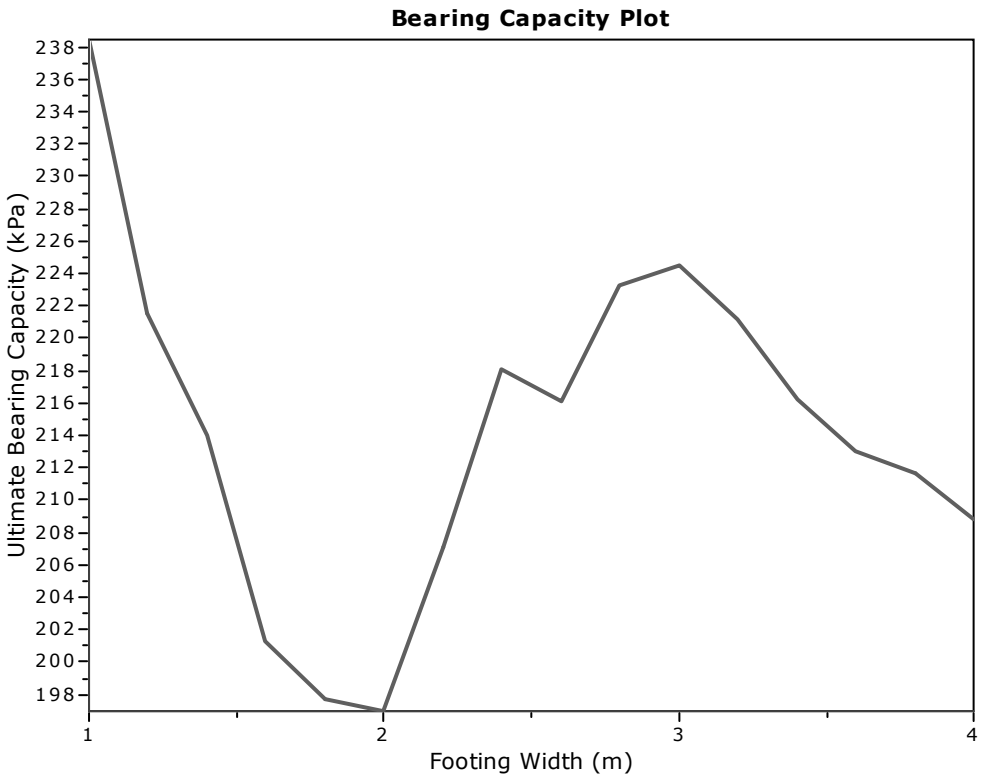
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.14	0.20	9.50	238.46
2	1.20	0.50	2.30	1.06	0.20	9.50	221.56
3	1.40	0.50	2.60	1.02	0.20	9.50	213.99
4	1.60	0.50	2.90	0.96	0.20	9.50	201.33
5	1.80	0.50	3.20	0.94	0.20	9.50	197.71
6	2.00	0.50	3.50	0.94	0.20	9.50	196.96
7	2.20	0.50	3.80	0.99	0.20	9.50	207.06
8	2.40	0.50	4.10	1.04	0.20	9.50	218.05
9	2.60	0.50	4.40	1.03	0.20	9.50	216.05
10	2.80	0.50	4.70	1.07	0.20	9.50	223.23
11	3.00	0.50	5.00	1.08	0.20	9.50	224.55
12	3.20	0.50	5.30	1.06	0.20	9.50	221.15
13	3.40	0.50	5.60	1.03	0.20	9.50	216.21
14	3.60	0.50	5.90	1.02	0.20	9.50	213.01
15	3.80	0.50	6.20	1.01	0.20	9.50	211.61
16	4.00	0.50	6.50	1.00	0.20	9.50	208.85

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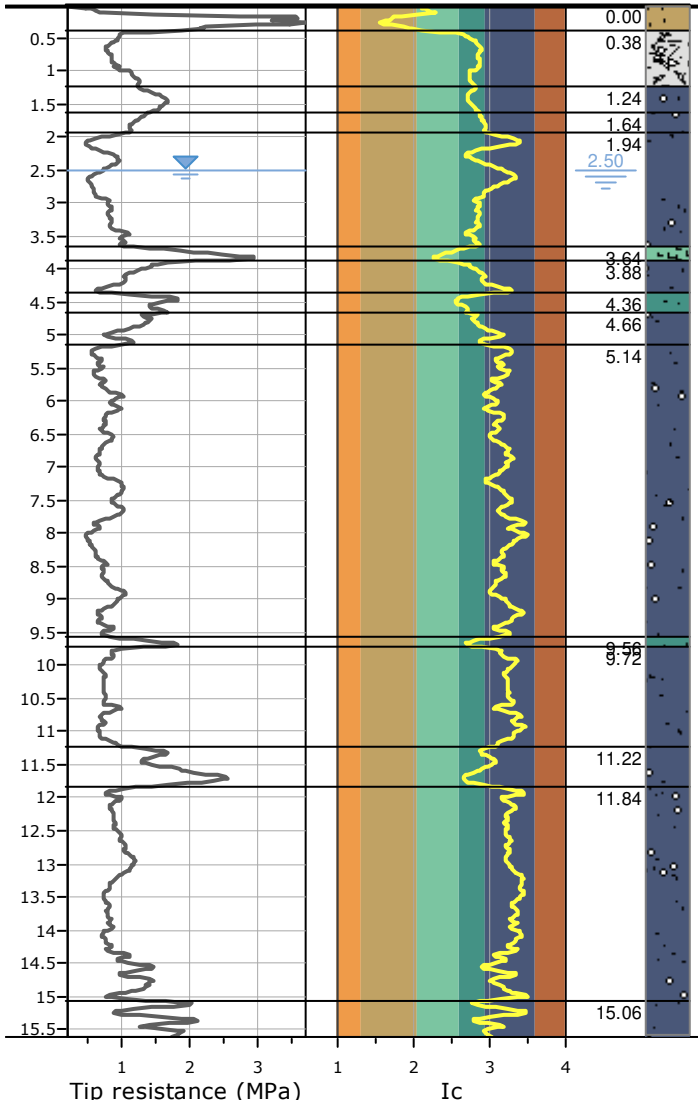
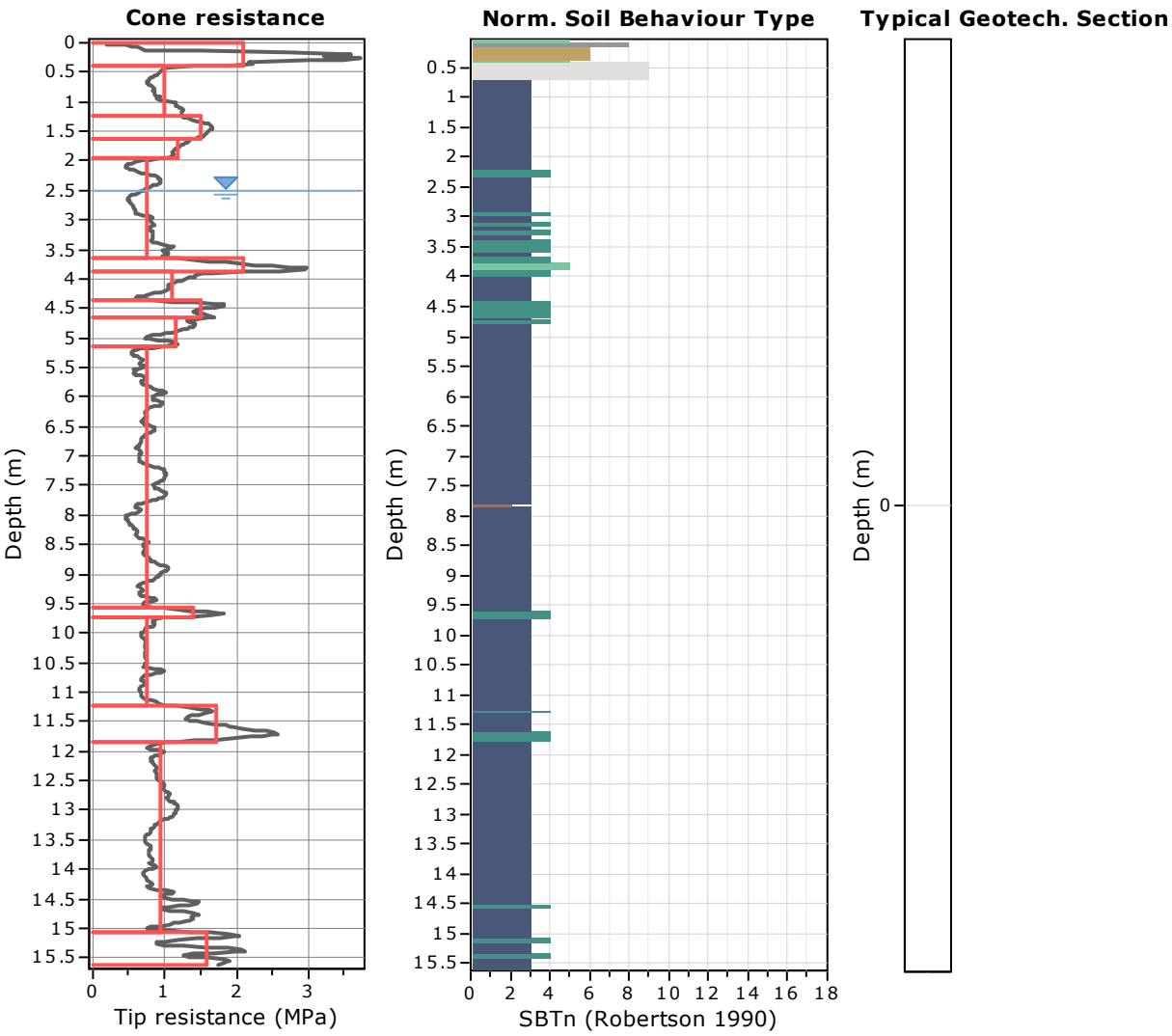
CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:

Depth (m) Elevation: 0.00 (m)



Depth (m)	Description	qt (MPa)	Ksbt (m/s)	N60	Es (MPa)	Dr	Phi (°)	M (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
0.00	Sand & silty sand	2.1	3.66E-5	5.0	15.0	63.6	41.2	18.7	18.8	-	-	-	16.8
0.38	Very dense/stiff soil	1.0	1.32E-7	4.4	18.8	-	-	13.7	29.3	68.7	4.3	19.9	18.2
1.24	Clay	1.5	3.57E-8	6.7	-	-	-	20.6	44.3	105.4	3.7	16.9	18.7
1.64	Clay	1.2	1.22E-8	5.7	-	-	-	16.2	41.8	82.4	2.5	11.6	18.4
1.94	Clay	0.8	1.70E-8	3.8	-	-	-	9.5	26.6	50.4	1.1	5.0	16.8
3.64	Silty sand & sandy silt	2.1	4.35E-7	7.5	35.0	33.9	35.2	28.2	40.3	-	-	-	17.4
3.88	Clay	1.1	3.32E-8	5.2	30.3	-	-	13.9	35.2	70.3	1.2	5.7	17.3
4.36	Clay & silty clay	1.5	7.95E-8	6.3	29.3	-	-	19.8	37.8	101.2	1.6	7.5	17.3
4.66	Clay	1.2	1.66E-8	5.4	-	-	-	14.5	37.5	76.1	1.2	5.6	17.4
5.14	Clay	0.7	2.88E-9	4.2	-	-	-	5.2	30.5	44.3	0.6	2.6	16.6
9.50	Clay & silty clay	1.4	2.88E-8	6.3	-	-	-	15.2	38.7	86.5	0.9	4.2	16.8
9.72	Clay	0.8	1.64E-9	4.5	-	-	-	3.5	31.6	41.4	0.4	1.9	16.4
11.22	Clay	1.7	2.26E-8	8.1	-	-	-	19.6	52.1	108.4	1.0	4.7	17.6
11.84	Clay	0.9	1.60E-9	5.7	-	-	-	4.5	39.8	51.2	0.4	2.0	16.8
15.06	Clay	1.6	1.10E-8	8.1	-	-	-	14.1	52.7	94.3	0.7	3.3	17.4



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.38 (m)

Description: Sand & silty sand

Basic results	Estimation results	
Total cone resistance: 2.08 ±1.25 MPa	Permeability: 3.66E-05 ±4.78E-05 m/s	Constrained Mod.: 18.66 ±8.30 MPa
Sleeve friction: 25.36 ±12.31 kPa	N60: 5.00 ±2.52 blows	Go: 18.78 ±8.17 MPa
SBT_n: 6	Es: 14.99 ±6.52 MPa	Su: 0.00 ±0.00 kPa
SBTn description: Sand & silty sand	Dr (%): 63.64 ±7.20	Su ratio: 0.00 ±0.00
	ö (degrees): 41.21 ±1.05 °	O.C.R.: 0.00 ±0.00
	Unit weight: 16.76 ±0.90 kN/m³	

.:: Layer No: 2 ::.

Code: A1 **Start depth:** 0.38 (m), **End depth:** 1.24 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 1.00 ±0.22 MPa	Permeability: 1.32E-07 ±5.66E-07 m/s	Constrained Mod.: 13.70 ±2.90 MPa
Sleeve friction: 91.83 ±14.37 kPa	N60: 4.43 ±0.66 blows	Go: 29.25 ±4.06 MPa
SBT_n: 9	Es: 18.82 ±0.18 MPa	Su: 68.67 ±12.56 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 4.32 ±1.06
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 19.95 ±4.89
	Unit weight: 18.16 ±0.18 kN/m³	

.:: Layer No: 3 ::.

Code: B1 **Start depth:** 1.24 (m), **End depth:** 1.64 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.50 ±0.14 MPa	Permeability: 3.57E-08 ±1.18E-08 m/s	Constrained Mod.: 20.65 ±1.88 MPa
Sleeve friction: 122.78 ±11.37 kPa	N60: 6.67 ±0.48 blows	Go: 44.31 ±3.31 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 105.36 ±9.59 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 3.67 ±0.25
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 16.95 ±1.18
	Unit weight: 18.67 ±0.13 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 1.64 (m), **End depth:** 1.94 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.19 ±0.10 MPa	Permeability: 1.22E-08 ±2.76E-09 m/s	Constrained Mod.: 16.16 ±1.42 MPa
Sleeve friction: 108.55 ±11.35 kPa	N60: 5.69 ±0.48 blows	Go: 41.83 ±2.00 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 82.44 ±7.25 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 2.51 ±0.32
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 11.58 ±1.47
	Unit weight: 18.44 ±0.15 kN/m³	

.:: Layer No: 5 ::.

Code: D1 **Start depth:** 1.94 (m), **End depth:** 3.64 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.75 ±0.18 MPa	Permeability: 1.70E-08 ±1.51E-08 m/s	Constrained Mod.: 9.46 ±2.99 MPa
Sleeve friction: 34.24 ±21.19 kPa	N60: 3.77 ±0.64 blows	Go: 26.59 ±4.57 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 50.39 ±12.36 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.08 ±0.25
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.99 ±1.16
	Unit weight: 16.76 ±0.59 kN/m³	

.:: Layer No: 6 ::.

Code: B2 **Start depth:** 3.64 (m), **End depth:** 3.88 (m)

Description: Silty sand & sandy silt

Basic results	Estimation results	
Total cone resistance: 2.08 ±0.65 MPa	Permeability: 4.35E-07 ±3.93E-07 m/s	Constrained Mod.: 28.24 ±9.07 MPa
Sleeve friction: 38.52 ±4.73 kPa	N60: 7.46 ±1.51 blows	Go: 40.29 ±5.15 MPa
SBT_n: 5	Es: 34.98 ±1.59 MPa	Su: 0.00 ±0.00 kPa
SBTn description: Silty sand & sandy silt	Dr (%): 33.94 ±1.96	Su ratio: 0.00 ±0.00
	ö (degrees): 35.25 ±0.56 °	O.C.R.: 0.00 ±0.00
	Unit weight: 17.45 ±0.24 kN/m³	

.:: Layer No: 7 ::.

Code: D2 **Start depth:** 3.88 (m), **End depth:** 4.36 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.10 ±0.35 MPa	Permeability: 3.32E-08 ±6.71E-08 m/s	Constrained Mod.: 13.91 ±5.54 MPa
Sleeve friction: 43.30 ±4.26 kPa	N60: 5.20 ±1.04 blows	Go: 35.25 ±2.97 MPa
SBT_n: 3	Es: 30.30 ±30.30 MPa	Su: 70.33 ±20.61 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.23 ±0.35
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.70 ±1.64
	Unit weight: 17.34 ±0.16 kN/m³	

.:: Layer No: 8 ::.

Code: B3 **Start depth:** 4.36 (m), **End depth:** 4.66 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 1.50 ±0.25 MPa	Permeability: 7.95E-08 ±4.72E-08 m/s	Constrained Mod.: 19.80 ±3.64 MPa
Sleeve friction: 38.42 ±9.69 kPa	N60: 6.25 ±0.86 blows	Go: 37.80 ±3.75 MPa
SBT_n: 4	Es: 29.31 ±3.20 MPa	Su: 101.24 ±17.93 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.63 ±0.26
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 7.51 ±1.21
	Unit weight: 17.30 ±0.30 kN/m³	

.:: Layer No: 9 ::.

Code: A3 **Start depth:** 4.66 (m), **End depth:** 5.14 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.15 ±0.24 MPa	Permeability: 1.66E-08 ±1.13E-08 m/s	Constrained Mod.: 14.53 ±4.06 MPa
Sleeve friction: 44.66 ±5.99 kPa	N60: 5.44 ±0.77 blows	Go: 37.52 ±3.42 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 76.09 ±17.40 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.22 ±0.28
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.62 ±1.30
	Unit weight: 17.39 ±0.22 kN/m³	

.:: Layer No: 10 ::.

Code: D3 **Start depth:** 5.14 (m), **End depth:** 9.56 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.75 ±0.14 MPa	Permeability: 2.88E-09 ±2.29E-09 m/s	Constrained Mod.: 5.22 ±2.43 MPa
Sleeve friction: 26.90 ±11.74 kPa	N60: 4.23 ±0.72 blows	Go: 30.49 ±5.42 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 44.26 ±10.16 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.57 ±0.15
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.64 ±0.68
	Unit weight: 16.56 ±0.53 kN/m³	

.:: Layer No: 11 ::.

Code: B4 **Start depth:** 9.56 (m), **End depth:** 9.72 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 1.38 ±0.35 MPa	Permeability: 2.88E-08 ±2.07E-08 m/s	Constrained Mod.: 15.19 ±6.73 MPa
Sleeve friction: 26.25 ±6.28 kPa	N60: 6.33 ±1.00 blows	Go: 38.72 ±5.22 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 86.54 ±24.73 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 0.92 ±0.26
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.24 ±1.20
	Unit weight: 16.82 ±0.35 kN/m³	

.:: Layer No: 12 ::.

Code: D4 **Start depth:** 9.72 (m), **End depth:** 11.22 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.76 ±0.11 MPa	Permeability: 1.64E-09 ±1.66E-09 m/s	Constrained Mod.: 3.51 ±1.65 MPa
Sleeve friction: 21.66 ±4.46 kPa	N60: 4.47 ±0.53 blows	Go: 31.60 ±2.42 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 41.41 ±7.94 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.42 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.93 ±0.39
	Unit weight: 16.40 ±0.23 kN/m³	

.:: Layer No: 13 ::.

Code: B5 **Start depth:** 11.22 (m), **End depth:** 11.84 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.71 ±0.44 MPa	Permeability: 2.26E-08 ±2.36E-08 m/s	Constrained Mod.: 19.58 ±7.77 MPa
Sleeve friction: 47.31 ±9.67 kPa	N60: 8.13 ±1.39 blows	Go: 52.06 ±6.36 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 108.39 ±31.30 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.01 ±0.29
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.69 ±1.33
	Unit weight: 17.59 ±0.34 kN/m³	

.:: Layer No: 14 ::.

Code: A4 **Start depth:** 11.84 (m), **End depth:** 15.06 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.95 ±0.19 MPa	Permeability: 1.60E-09 ±1.87E-09 m/s	Constrained Mod.: 4.53 ±2.33 MPa
Sleeve friction: 30.38 ±12.35 kPa	N60: 5.73 ±0.88 blows	Go: 39.85 ±6.51 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 51.21 ±13.23 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.43 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.96 ±0.49
	Unit weight: 16.80 ±0.49 kN/m³	

.:: Layer No: 15 ::.

Code: B6 **Start depth:** 15.06 (m), **End depth:** 15.62 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.58 ±0.38 MPa	Permeability: 1.10E-08 ±1.01E-08 m/s	Constrained Mod.: 14.05 ±7.04 MPa
Sleeve friction: 39.87 ±7.76 kPa	N60: 8.07 ±1.12 blows	Go: 52.68 ±5.01 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 94.29 ±26.85 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.71 ±0.20
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.26 ±0.93
	Unit weight: 17.37 ±0.25 kN/m³	

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Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.38	3.66E-05	5.0	15.0	63.6	41.2	18.7	18.8	0.0	0.0	0.0	16.8
0.38		(±4.78E-05)	(±2.5)	(±6.5)	(±7.2)	(±1.0)	(±8.3)	(±8.2)	(±0.0)	(±0.0)	(±0.0)	(±0.9)
0.38	0.86	1.32E-07	4.4	18.8	0.0	0.0	13.7	29.3	68.7	4.3	19.9	18.2
1.24		(±5.66E-07)	(±0.7)	(±0.2)	(±0.0)	(±0.0)	(±2.9)	(±4.1)	(±12.6)	(±1.1)	(±4.9)	(±0.2)
1.24	0.40	3.57E-08	6.7	0.0	0.0	0.0	20.6	44.3	105.4	3.7	16.9	18.7
1.64		(±1.18E-08)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.9)	(±3.3)	(±9.6)	(±0.3)	(±1.2)	(±0.1)
1.64	0.30	1.22E-08	5.7	0.0	0.0	0.0	16.2	41.8	82.4	2.5	11.6	18.4
1.94		(±2.76E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.4)	(±2.0)	(±7.2)	(±0.3)	(±1.5)	(±0.1)
1.94	1.70	1.70E-08	3.8	0.0	0.0	0.0	9.5	26.6	50.4	1.1	5.0	16.8
3.64		(±1.51E-08)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±4.6)	(±12.4)	(±0.3)	(±1.2)	(±0.6)
3.64	0.24	4.35E-07	7.5	35.0	33.9	35.2	28.2	40.3	0.0	0.0	0.0	17.4
3.88		(±3.93E-07)	(±1.5)	(±1.6)	(±2.0)	(±0.6)	(±9.1)	(±5.2)	(±0.0)	(±0.0)	(±0.0)	(±0.2)
3.88	0.48	3.32E-08	5.2	30.3	0.0	0.0	13.9	35.2	70.3	1.2	5.7	17.3
4.36		(±6.71E-08)	(±1.0)	(±30.3)	(±0.0)	(±0.0)	(±5.5)	(±3.0)	(±20.6)	(±0.4)	(±1.6)	(±0.2)
4.36	0.30	7.95E-08	6.3	29.3	0.0	0.0	19.8	37.8	101.2	1.6	7.5	17.3
4.66		(±4.72E-08)	(±0.9)	(±3.2)	(±0.0)	(±0.0)	(±3.6)	(±3.8)	(±17.9)	(±0.3)	(±1.2)	(±0.3)
4.66	0.48	1.66E-08	5.4	0.0	0.0	0.0	14.5	37.5	76.1	1.2	5.6	17.4
5.14		(±1.13E-08)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±4.1)	(±3.4)	(±17.4)	(±0.3)	(±1.3)	(±0.2)
5.14	4.42	2.88E-09	4.2	0.0	0.0	0.0	5.2	30.5	44.3	0.6	2.6	16.6
9.56		(±2.29E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±2.4)	(±5.4)	(±10.2)	(±0.1)	(±0.7)	(±0.5)
9.56	0.16	2.88E-08	6.3	0.0	0.0	0.0	15.2	38.7	86.5	0.9	4.2	16.8
9.72		(±2.07E-08)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±6.7)	(±5.2)	(±24.7)	(±0.3)	(±1.2)	(±0.3)

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Project:
Location:

CPT: CPTu-01
Total depth: 15.62 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
9.72	1.50	1.64E-09	4.5	0.0	0.0	0.0	3.5	31.6	41.4	0.4	1.9	16.4
11.22		(±1.66E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.6)	(±2.4)	(±7.9)	(±0.1)	(±0.4)	(±0.2)
11.22	0.62	2.26E-08	8.1	0.0	0.0	0.0	19.6	52.1	108.4	1.0	4.7	17.6
11.84		(±2.36E-08)	(±1.4)	(±0.0)	(±0.0)	(±0.0)	(±7.8)	(±6.4)	(±31.3)	(±0.3)	(±1.3)	(±0.3)
11.84	3.22	1.60E-09	5.7	0.0	0.0	0.0	4.5	39.8	51.2	0.4	2.0	16.8
15.06		(±1.87E-09)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±2.3)	(±6.5)	(±13.2)	(±0.1)	(±0.5)	(±0.5)
15.06	0.56	1.10E-08	8.1	0.0	0.0	0.0	14.1	52.7	94.3	0.7	3.3	17.4
15.62		(±1.01E-08)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±7.0)	(±5.0)	(±26.8)	(±0.2)	(±0.9)	(±0.2)

Depth values presented in this table are measured from free ground surface

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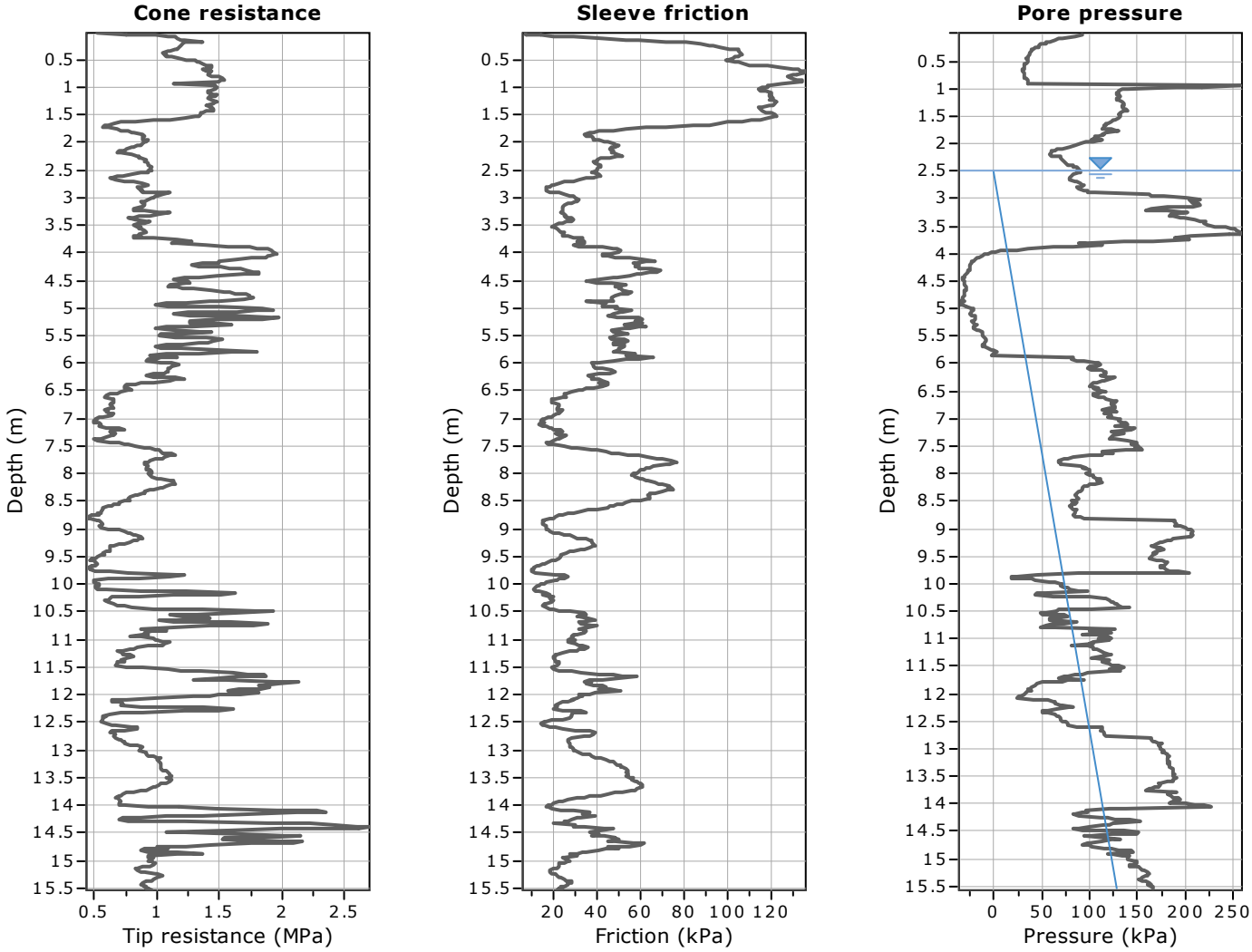
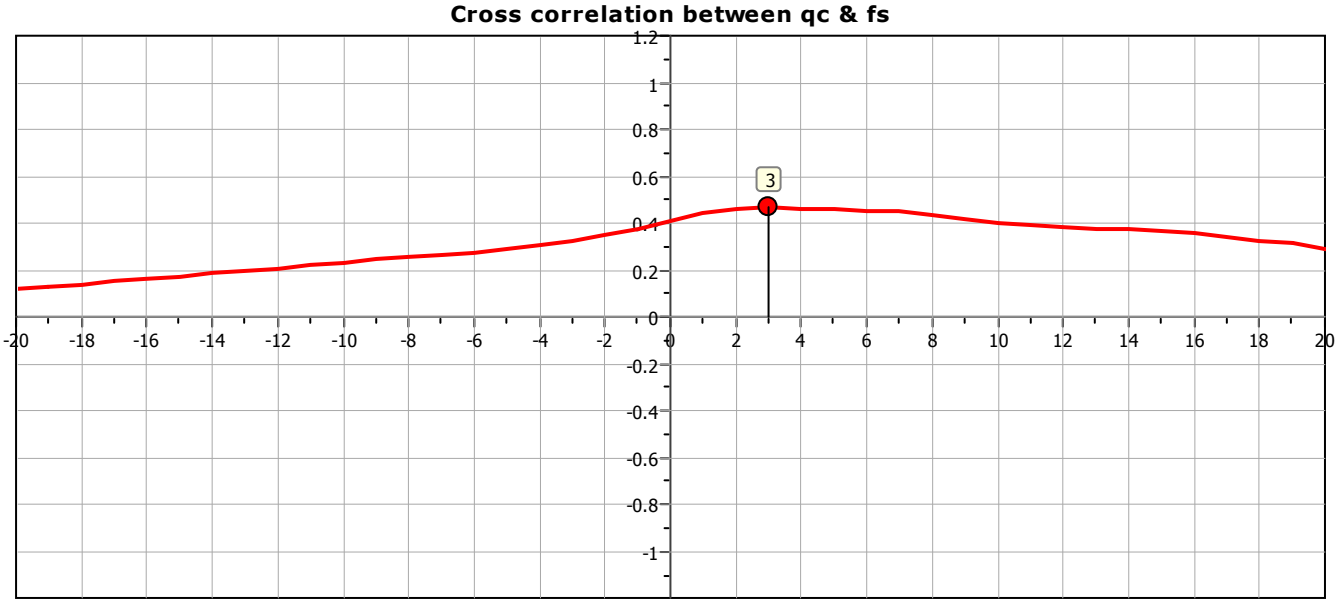
CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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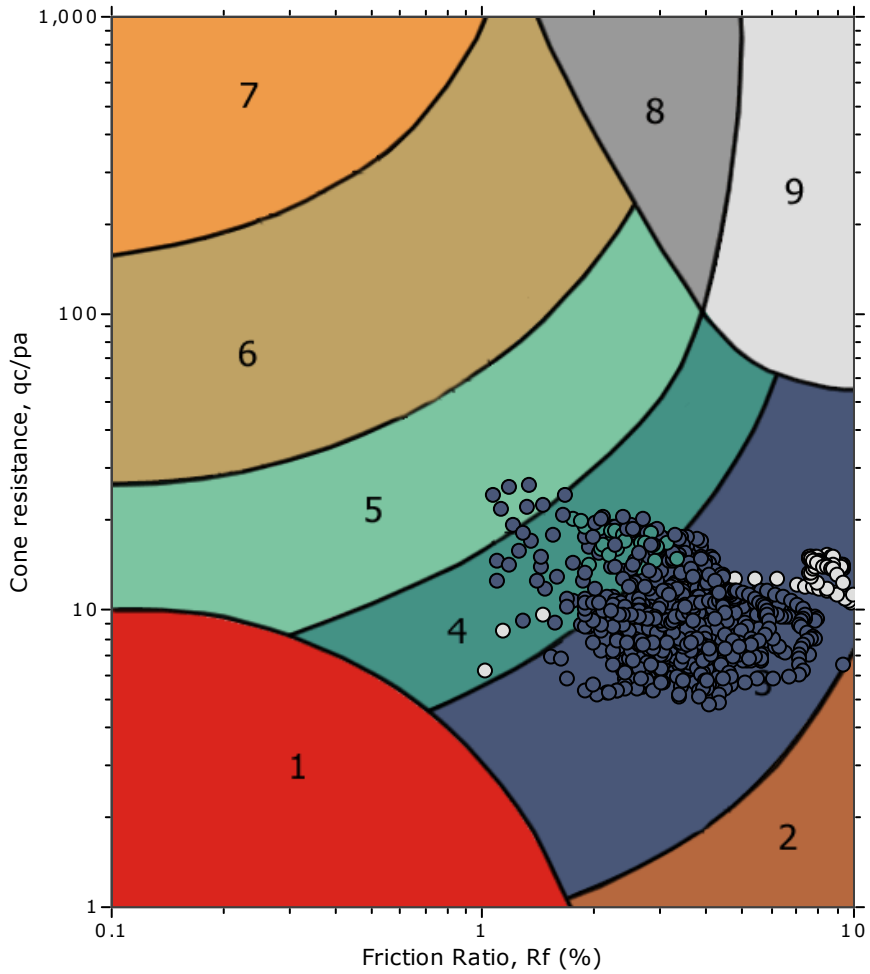
Project:
Location:

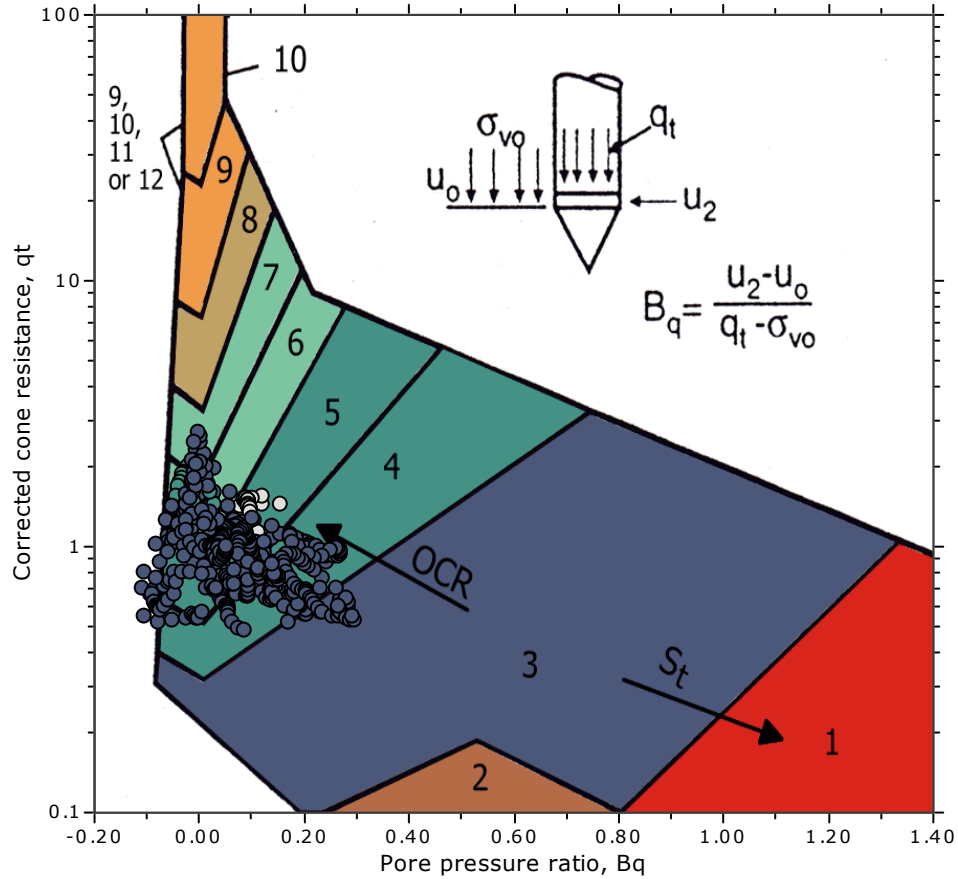
CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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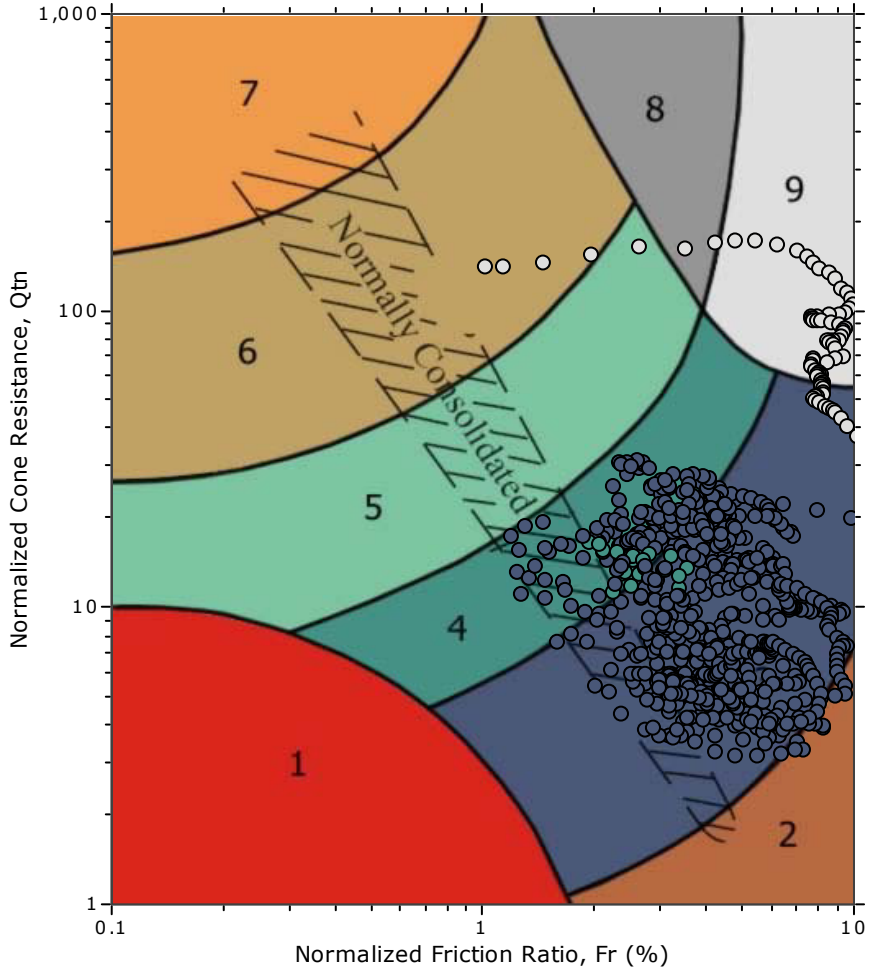
Project:
Location:

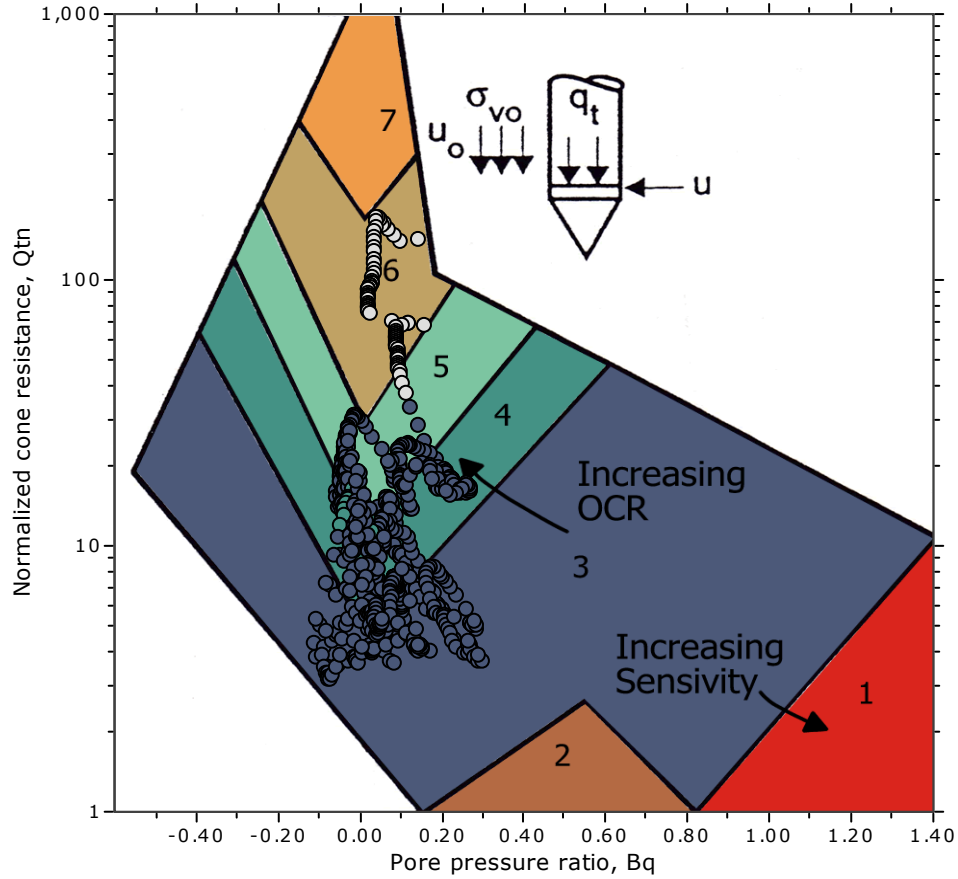
CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)

SBTn plot



Normalized Bq plot



SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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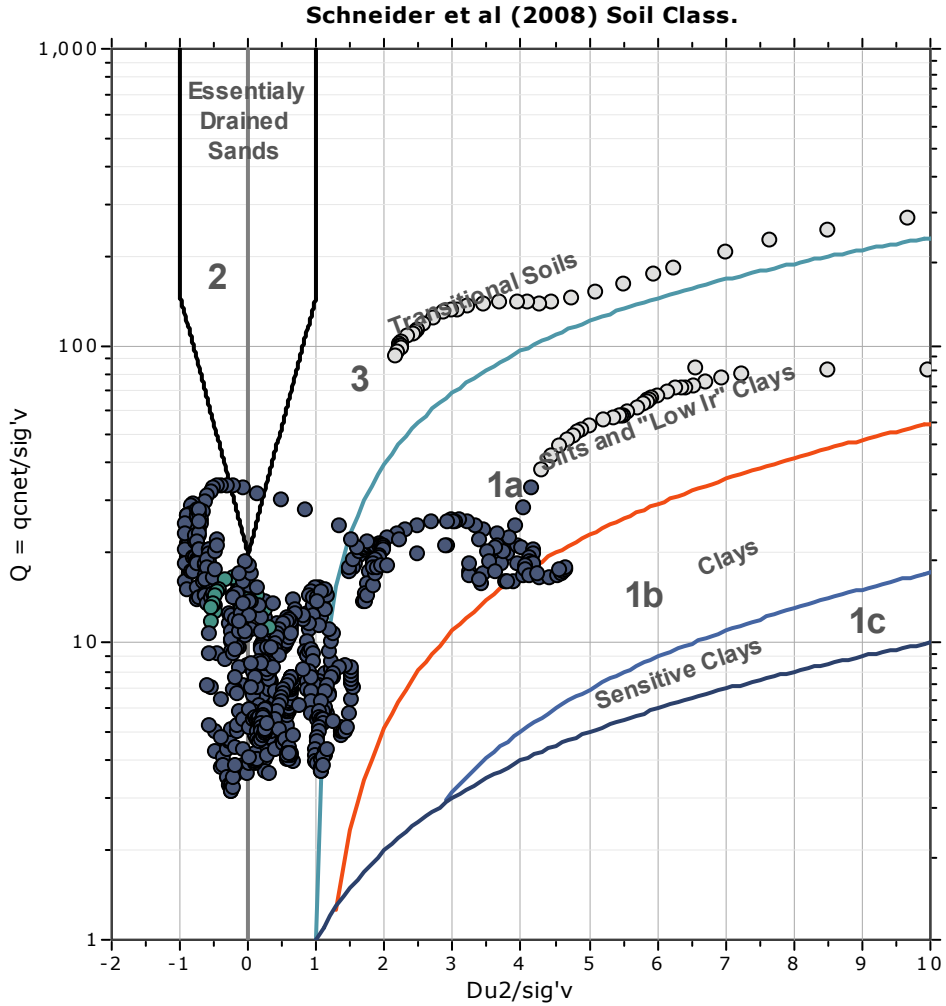
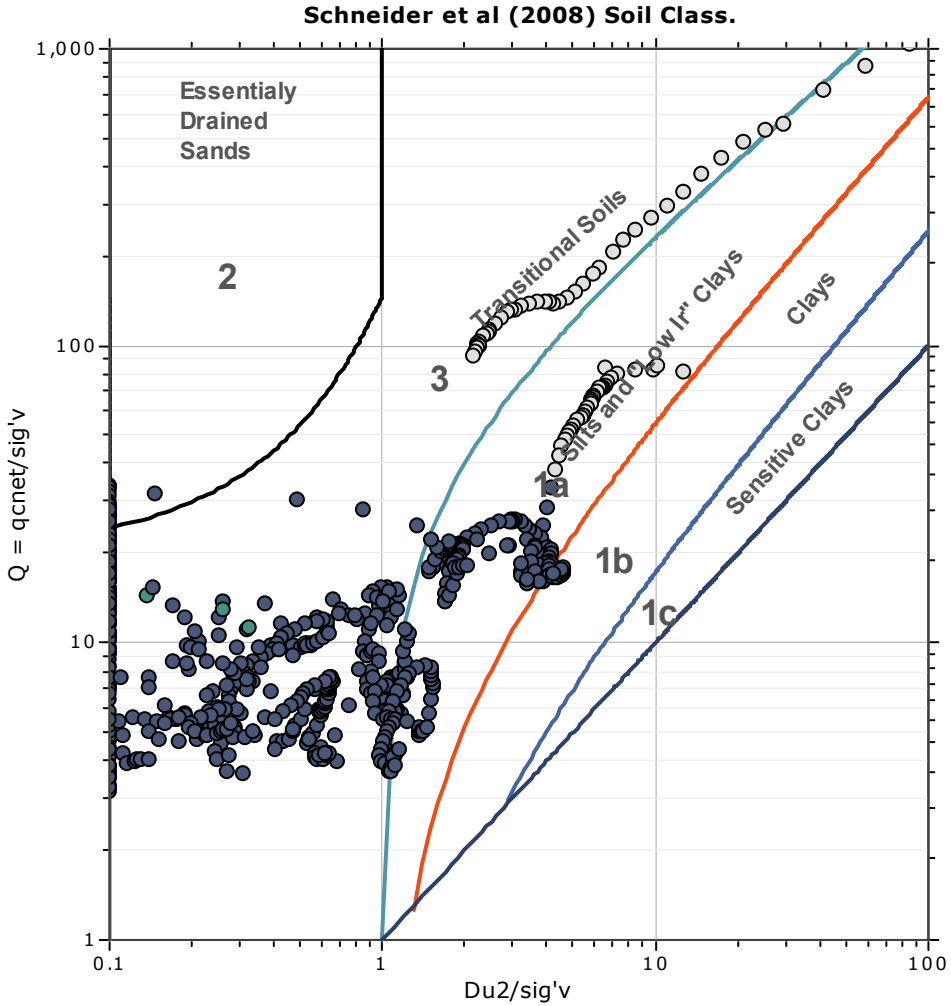
Project:
Location:

CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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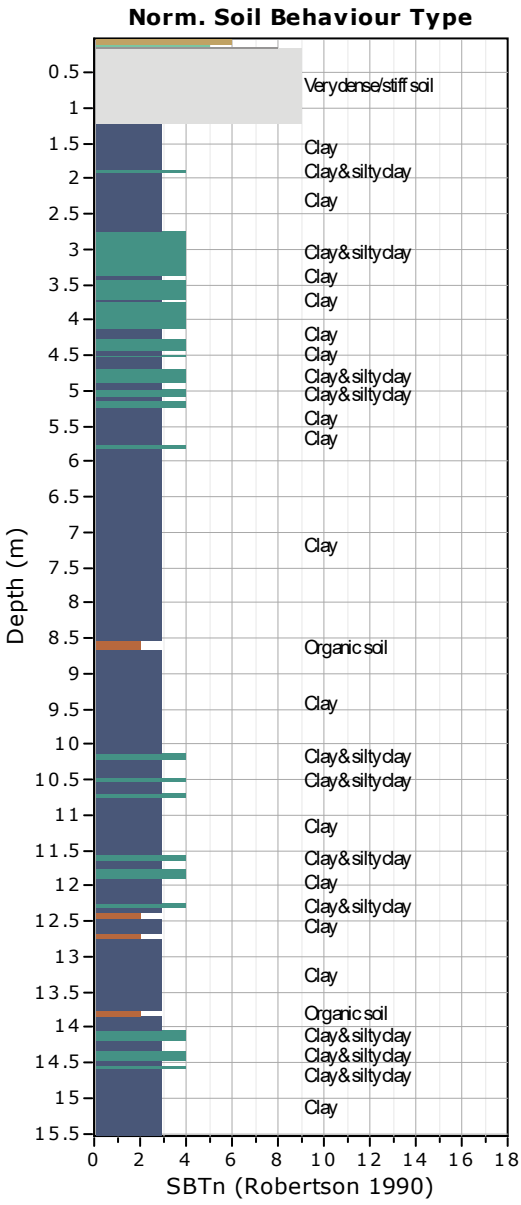
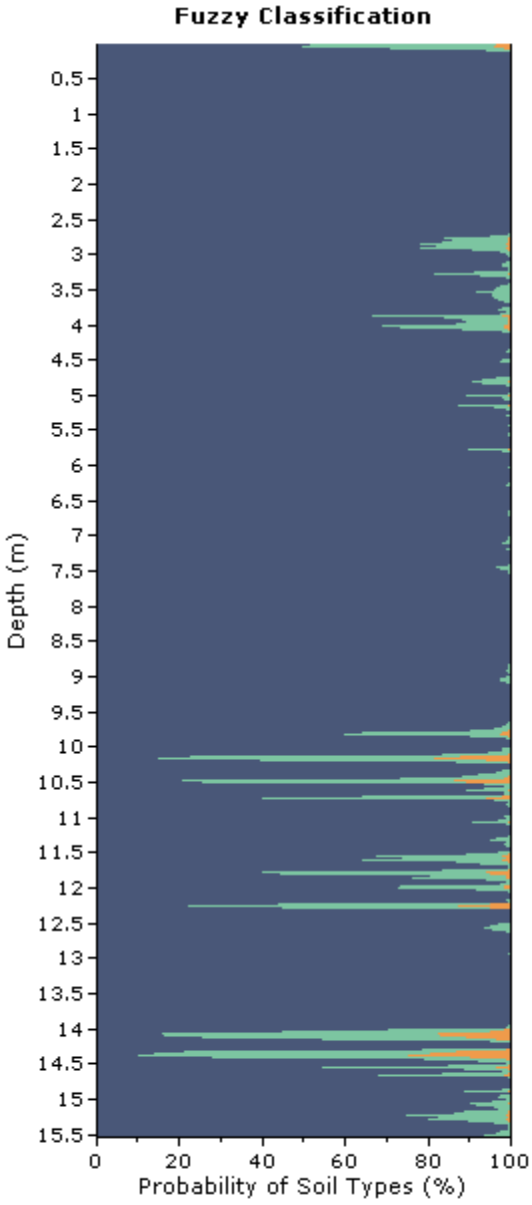
CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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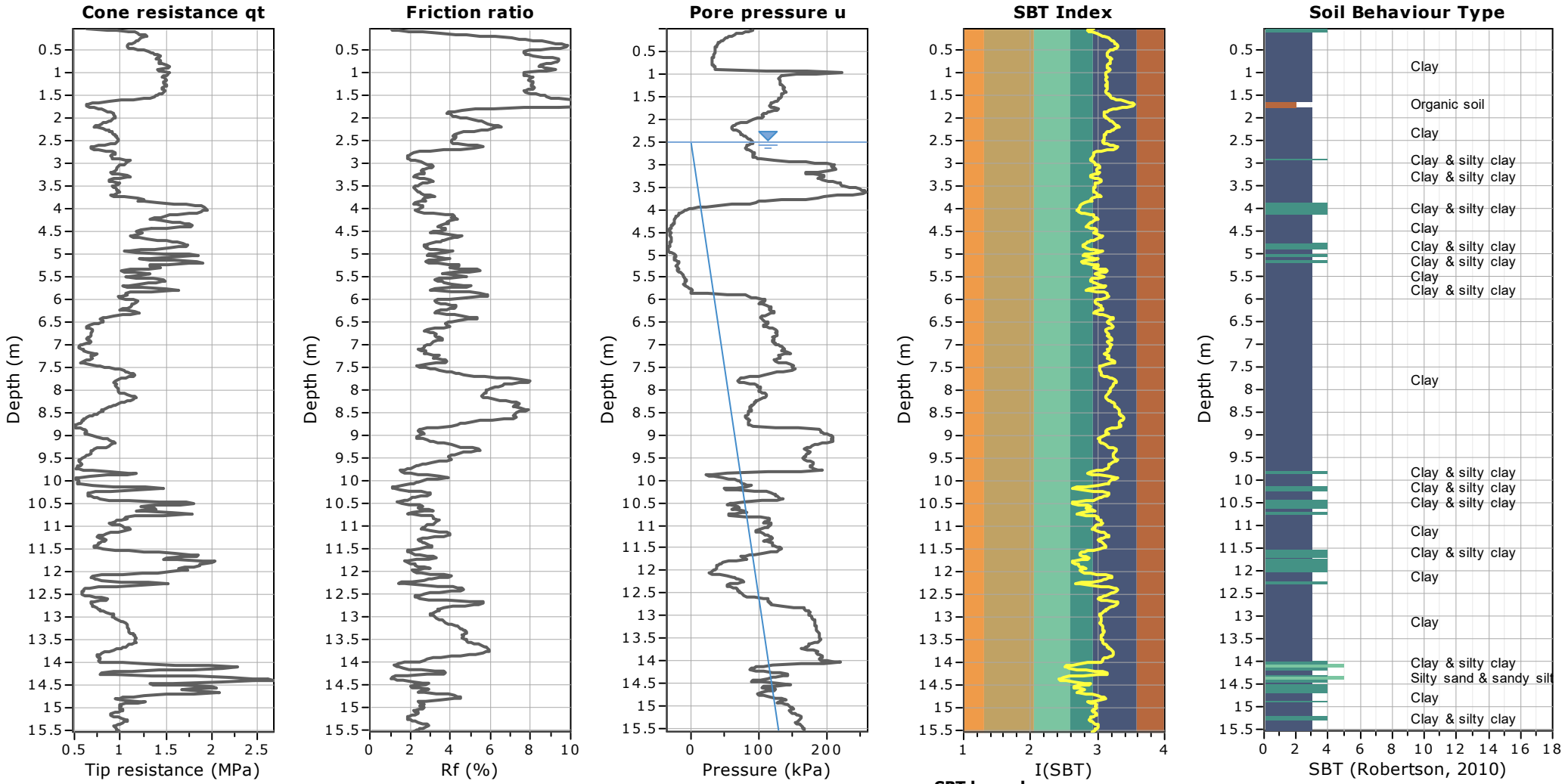
Project:
Location:

CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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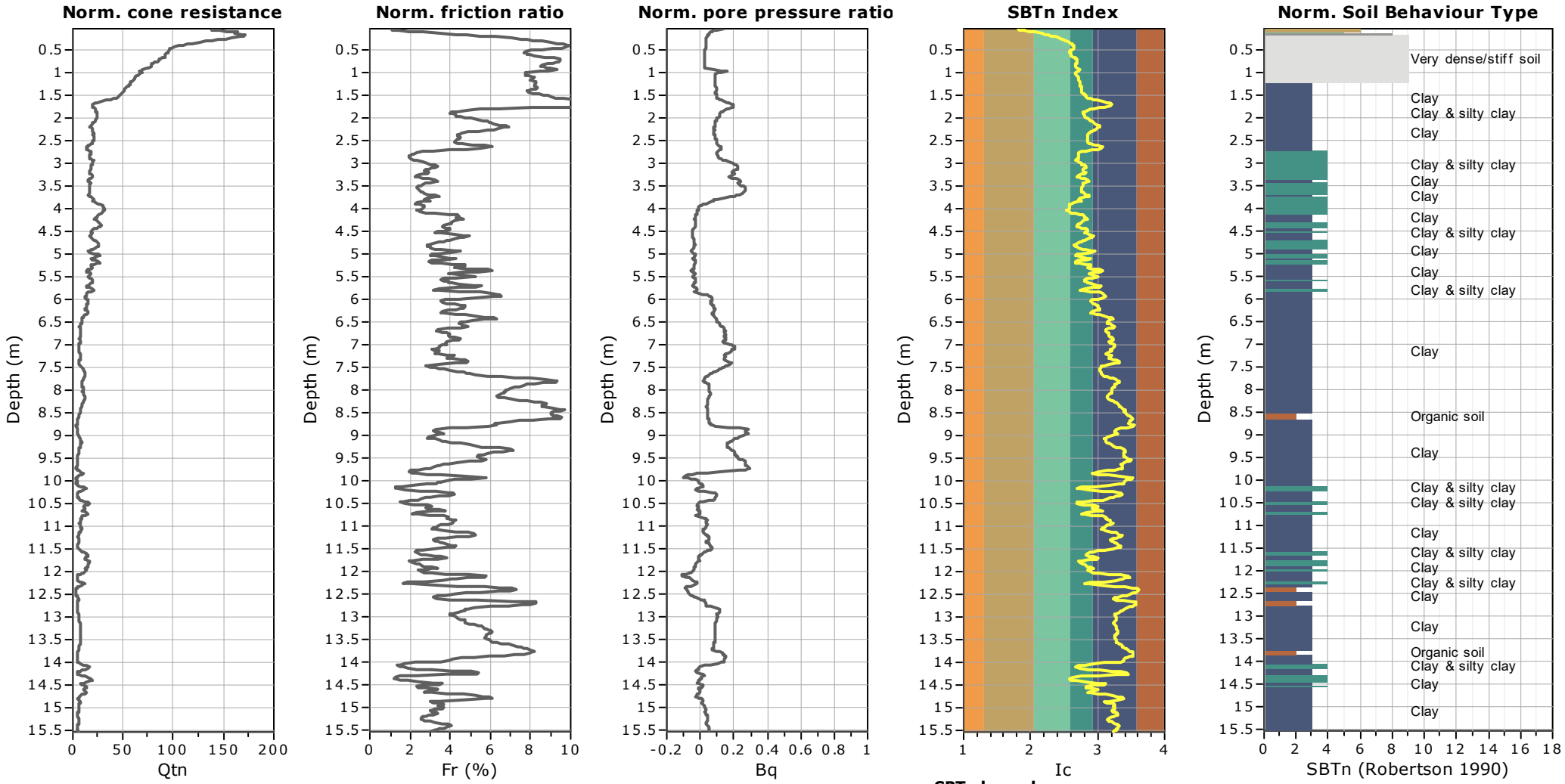
Project:
Location:

CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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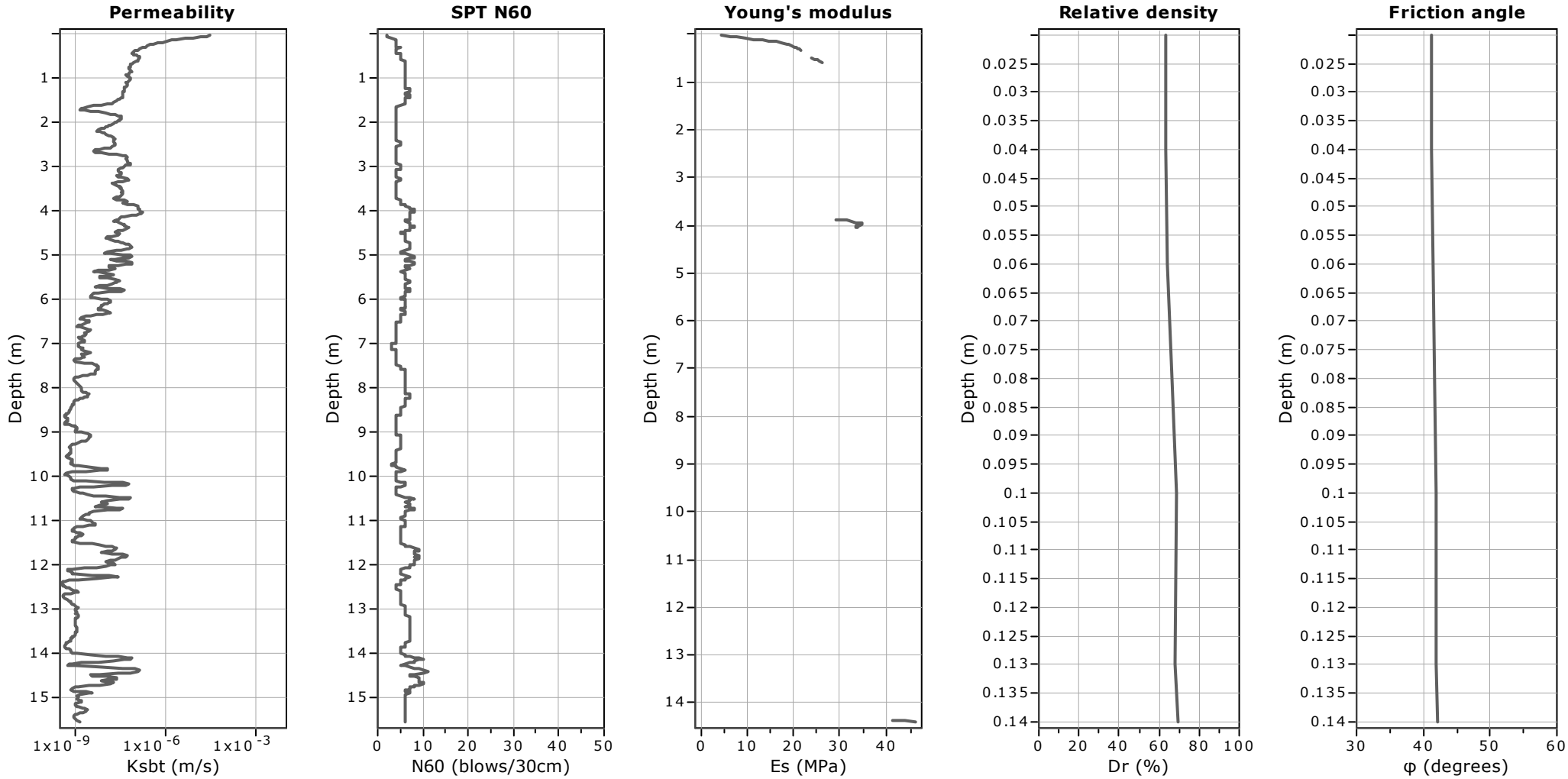
Project:
Location:

CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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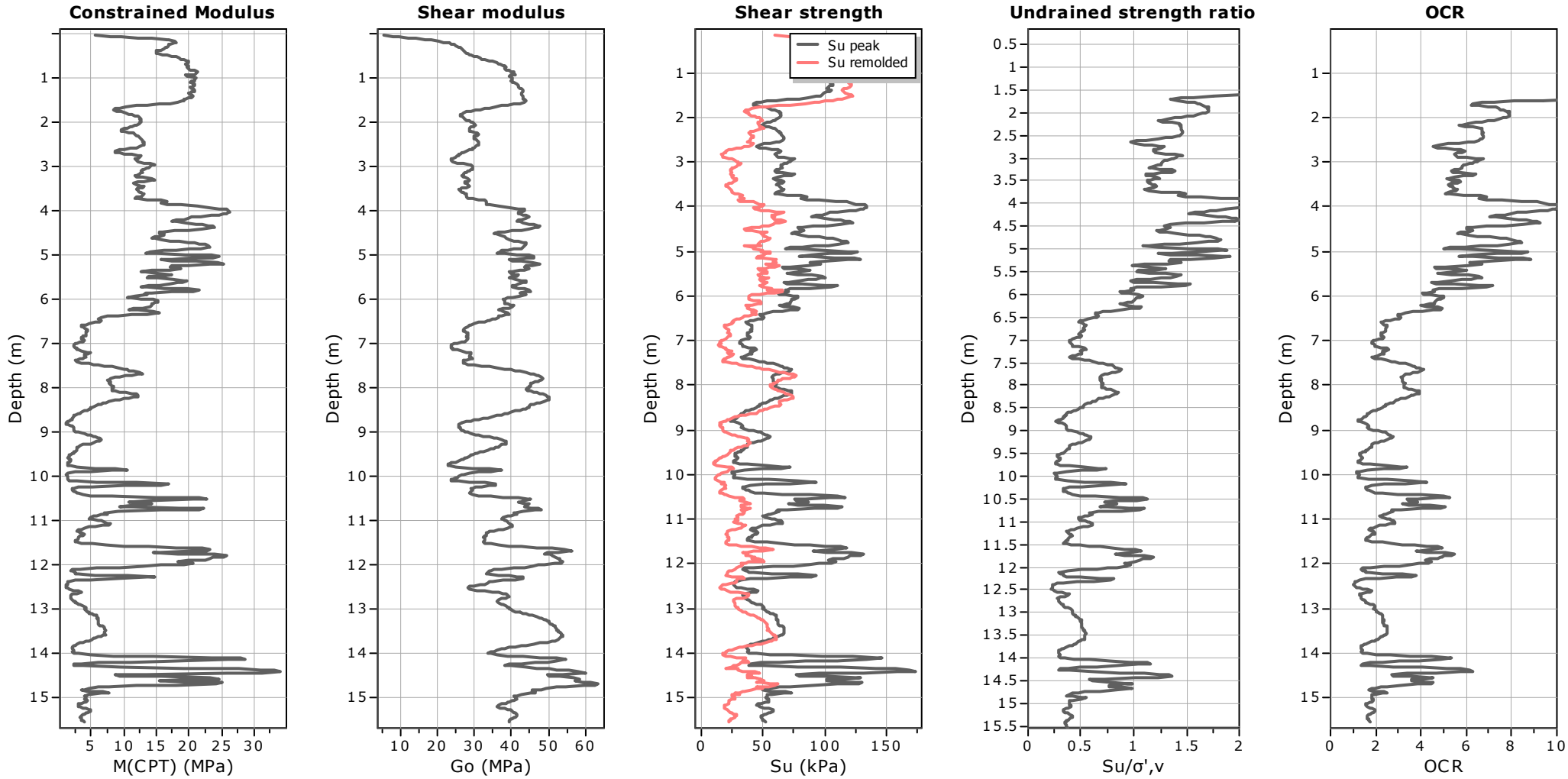
Project:
Location:

CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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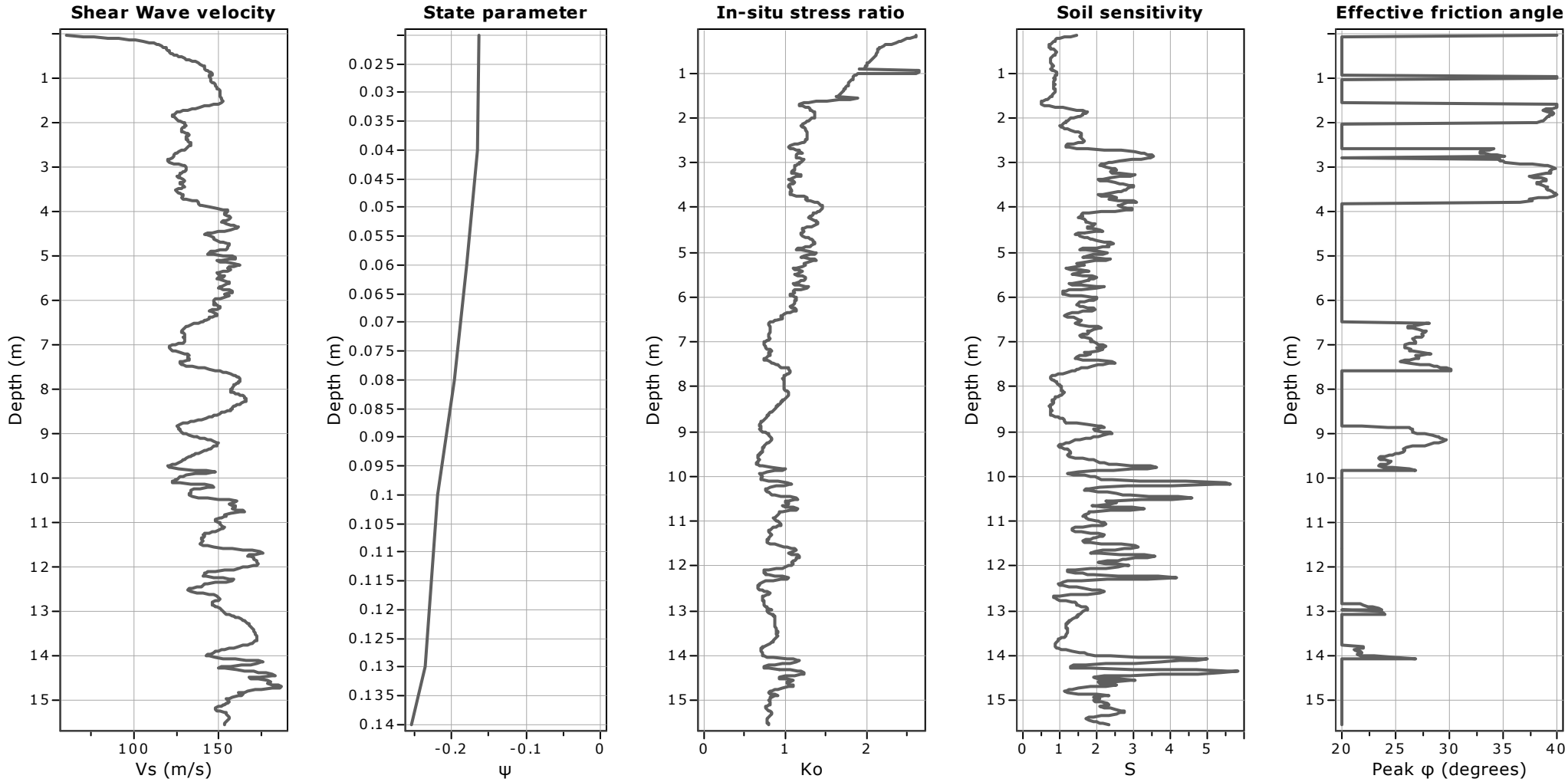
Project:
Location:

CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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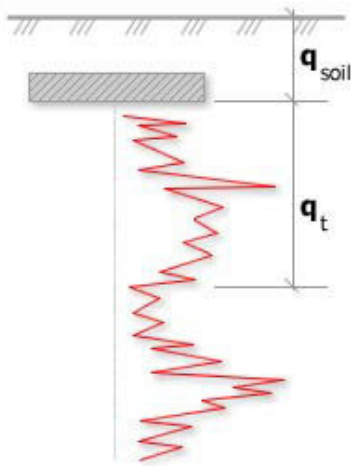
CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

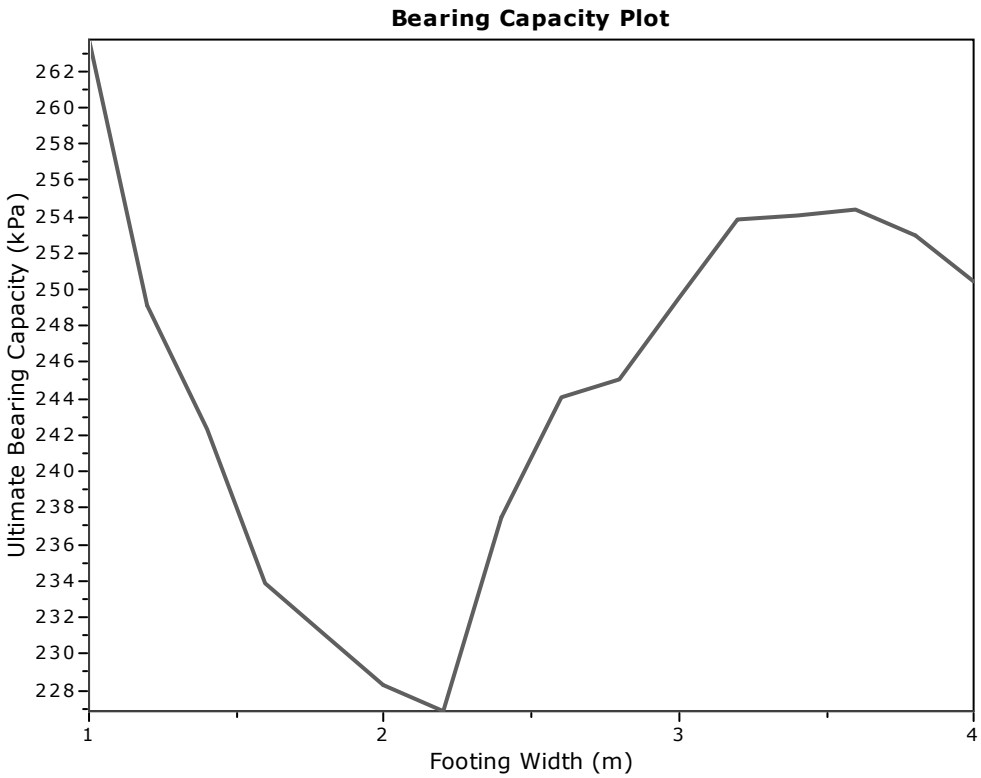
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.27	0.20	9.50	263.70
2	1.20	0.50	2.30	1.20	0.20	9.50	249.12
3	1.40	0.50	2.60	1.16	0.20	9.50	242.34
4	1.60	0.50	2.90	1.12	0.20	9.50	233.84
5	1.80	0.50	3.20	1.11	0.20	9.50	231.06
6	2.00	0.50	3.50	1.09	0.20	9.50	228.32
7	2.20	0.50	3.80	1.09	0.20	9.50	226.86
8	2.40	0.50	4.10	1.14	0.20	9.50	237.55
9	2.60	0.50	4.40	1.17	0.20	9.50	244.12
10	2.80	0.50	4.70	1.18	0.20	9.50	245.04
11	3.00	0.50	5.00	1.20	0.20	9.50	249.52
12	3.20	0.50	5.30	1.22	0.20	9.50	253.82
13	3.40	0.50	5.60	1.22	0.20	9.50	254.04
14	3.60	0.50	5.90	1.22	0.20	9.50	254.35
15	3.80	0.50	6.20	1.22	0.20	9.50	253.01
16	4.00	0.50	6.50	1.20	0.20	9.50	250.39

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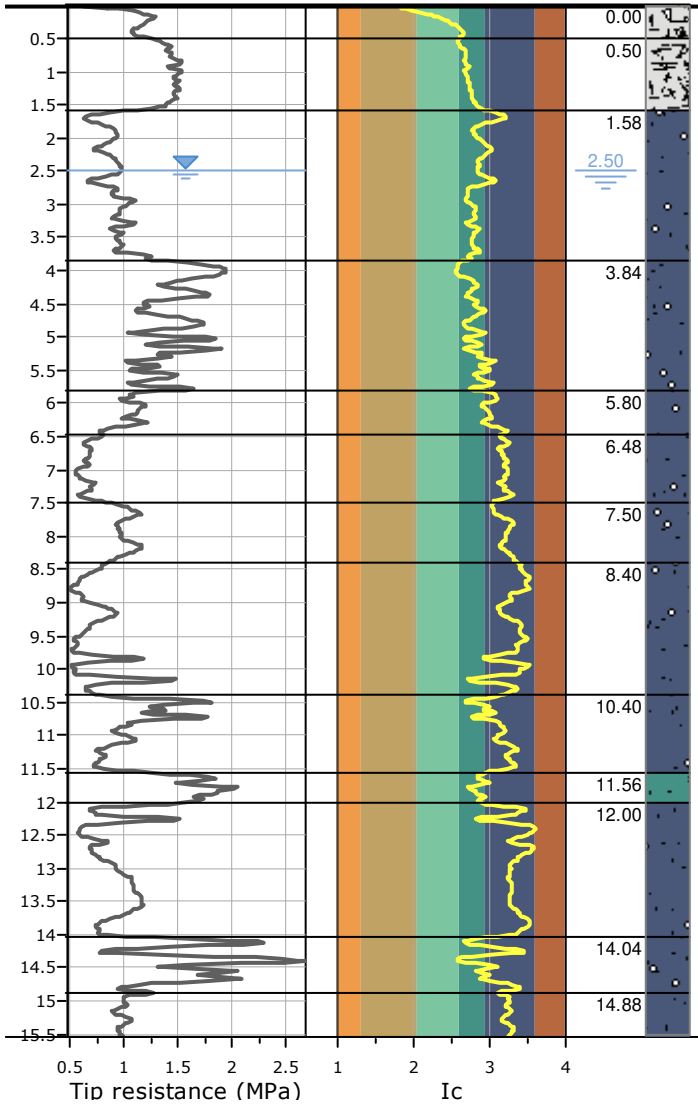
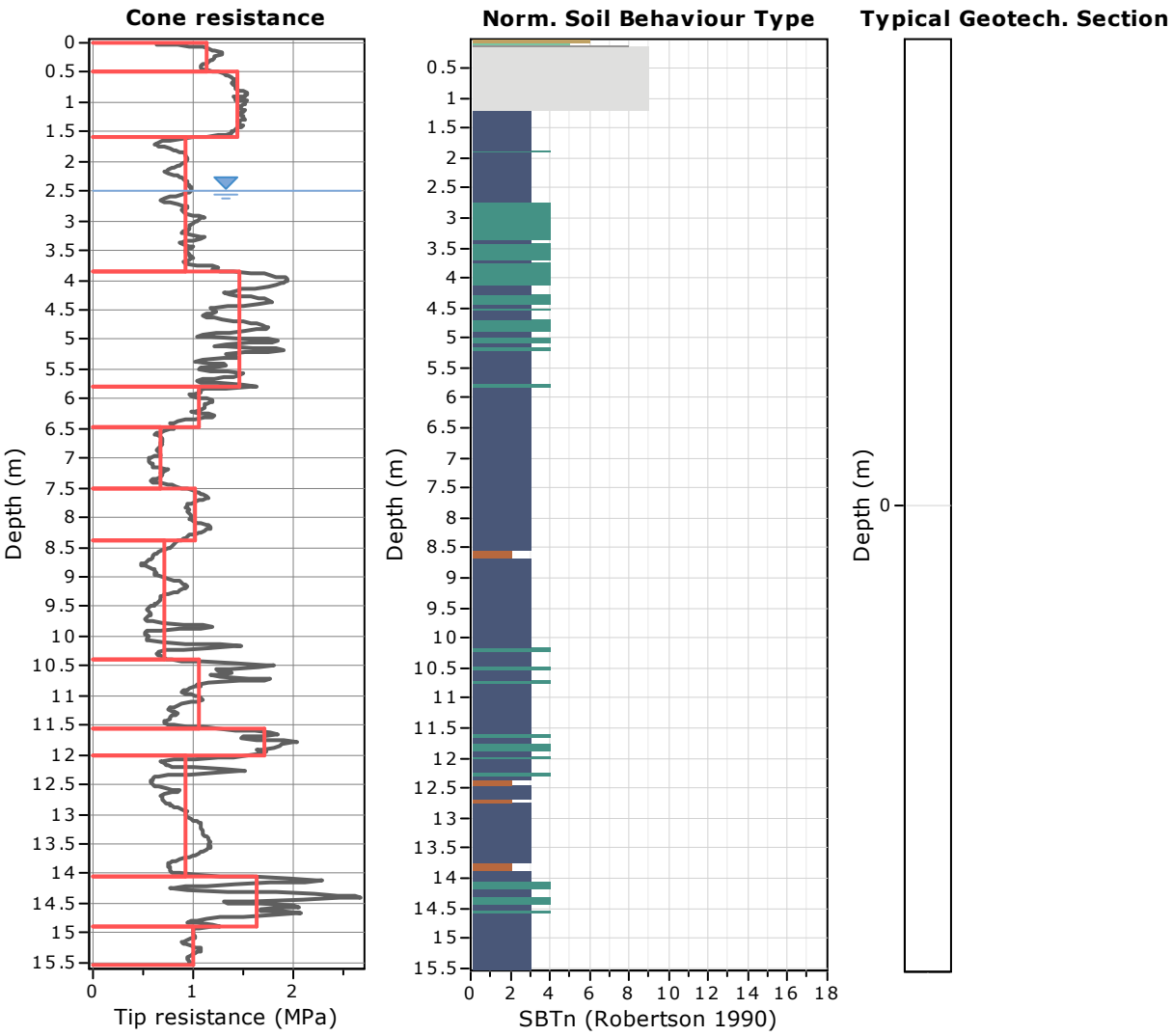
CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:

Depth (m) Elevation: 0.00 (m)



Depth (m)	Description	qt (MPa)	Ksbt (m/s)	N60	Es (MPa)	Dr	Phi (°)	M (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
0.00	Very dense/stiff soil	1.1	3.48E-6	3.9	19.9	-	-	15.1	22.2	83.6	9.1	42.0	17.8
0.50	Very dense/stiff soil	1.4	5.71E-8	6.0	25.1	-	-	19.9	39.8	101.6	4.8	22.2	18.6
1.58	Clay	0.9	2.48E-8	4.2	-	-	-	12.2	28.9	62.2	1.4	6.3	17.0
3.84	Clay	1.5	4.16E-8	6.6	33.2	-	-	19.2	41.9	98.2	1.5	7.2	17.6
5.80	Clay	1.1	7.60E-9	5.6	-	-	-	12.4	39.0	68.3	0.9	4.4	17.4
6.48	Clay	0.7	2.00E-9	3.9	-	-	-	3.9	27.8	39.1	0.5	2.3	16.3
7.50	Clay	1.0	2.13E-9	6.0	-	-	-	9.2	45.5	62.8	0.7	3.4	17.7
8.40	Clay	0.7	2.92E-9	4.4	-	-	-	3.5	31.4	39.3	0.4	1.9	16.4
10.40	Clay	1.1	7.60E-9	5.8	-	-	-	8.0	38.5	62.5	0.6	2.7	16.8
11.56	Clay & silty clay	1.7	2.04E-8	8.1	-	-	-	20.0	50.8	108.1	1.0	4.5	17.4
12.00	Clay	0.9	1.73E-9	5.8	-	-	-	4.5	41.7	50.2	0.4	1.9	17.0
14.04	Clay	1.6	2.45E-8	8.0	44.1	-	-	15.8	51.5	99.2	0.8	3.5	17.3
14.88	Clay	1.0	1.41E-9	6.1	-	-	-	4.1	40.2	53.0	0.4	1.8	16.6



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.50 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 1.13 ±0.14 MPa	Permeability: 3.48E-06 ±7.46E-06 m/s	Constrained Mod.: 15.13 ±3.12 MPa
Sleeve friction: 75.75 ±35.47 kPa	N60: 3.88 ±0.88 blows	Go: 22.19 ±7.17 MPa
SBT_n: 9	Es: 19.91 ±2.14 MPa	Su: 83.56 ±5.31 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 9.10 ±1.95
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 42.05 ±9.01
	Unit weight: 17.76 ±0.99 kN/m³	

.:: Layer No: 2 ::.

Code: H **Start depth:** 0.50 (m), **End depth:** 1.58 (m)

Description: Very dense/stiff soil

Basic results	**Estimation results**	
Total cone resistance: 1.44 ±0.08 MPa	Permeability: 5.71E-08 ±2.79E-08 m/s	Constrained Mod.: 19.91 ±1.09 MPa
Sleeve friction: 120.27 ±8.54 kPa	N60: 6.04 ±0.47 blows	Go: 39.84 ±3.54 MPa
SBT_n: 9	Es: 25.11 ±0.92 MPa	Su: 101.57 ±5.58 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 4.80 ±1.20
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 22.17 ±5.52
	Unit weight: 18.63 ±0.09 kN/m³	

.:: Layer No: 3 ::.

Code: A1 **Start depth:** 1.58 (m), **End depth:** 3.84 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.92 ±0.13 MPa	Permeability: 2.48E-08 ±1.55E-08 m/s	Constrained Mod.: 12.18 ±1.68 MPa
Sleeve friction: 37.60 ±19.34 kPa	N60: 4.22 ±0.44 blows	Go: 28.93 ±2.79 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 62.18 ±8.55 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.37 ±0.25
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.35 ±1.14
	Unit weight: 17.01 ±0.46 kN/m³	

.:: Layer No: 4 ::.

Code: B2 **Start depth:** 3.84 (m), **End depth:** 5.80 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.46 ±0.26 MPa	Permeability: 4.16E-08 ±3.83E-08 m/s	Constrained Mod.: 19.24 ±3.76 MPa
Sleeve friction: 50.78 ±7.62 kPa	N60: 6.56 ±0.77 blows	Go: 41.91 ±3.08 MPa
SBT_n: 3	Es: 33.25 ±1.75 MPa	Su: 98.20 ±19.12 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.55 ±0.33
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 7.15 ±1.54
	Unit weight: 17.63 ±0.19 kN/m³	

.:: Layer No: 5 ::.

Code: A2 **Start depth:** 5.80 (m), **End depth:** 6.48 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.06 ±0.16 MPa	Permeability: 7.60E-09 ±5.87E-09 m/s	Constrained Mod.: 12.42 ±3.42 MPa
Sleeve friction: 44.78 ±8.31 kPa	N60: 5.63 ±0.55 blows	Go: 38.96 ±2.78 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 68.26 ±11.83 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.95 ±0.17
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.37 ±0.81
	Unit weight: 17.36 ±0.21 kN/m³	

.:: Layer No: 6 ::.

Code: D1 **Start depth:** 6.48 (m), **End depth:** 7.50 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.67 ±0.07 MPa	Permeability: 2.00E-09 ±9.54E-10 m/s	Constrained Mod.: 3.92 ±1.07 MPa
Sleeve friction: 21.25 ±4.15 kPa	N60: 3.92 ±0.44 blows	Go: 27.81 ±2.16 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 39.15 ±5.22 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.50 ±0.07
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.32 ±0.32
	Unit weight: 16.33 ±0.24 kN/m³	

.:: Layer No: 7 ::.

Code: A3 **Start depth:** 7.50 (m), **End depth:** 8.40 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.02 ±0.09 MPa	Permeability: 2.13E-09 ±1.49E-09 m/s	Constrained Mod.: 9.19 ±1.87 MPa
Sleeve friction: 60.66 ±12.59 kPa	N60: 6.02 ±0.45 blows	Go: 45.50 ±4.06 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 62.75 ±6.24 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.74 ±0.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.42 ±0.36
	Unit weight: 17.68 ±0.30 kN/m³	

.:: Layer No: 8 ::.

Code: D2 **Start depth:** 8.40 (m), **End depth:** 10.40 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.71 ±0.19 MPa	Permeability: 2.92E-09 ±8.05E-09 m/s	Constrained Mod.: 3.54 ±2.80 MPa
Sleeve friction: 25.46 ±13.66 kPa	N60: 4.43 ±0.67 blows	Go: 31.44 ±5.62 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 39.25 ±13.71 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.41 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.90 ±0.65
	Unit weight: 16.43 ±0.57 kN/m³	

.:: Layer No: 9 ::.

Code: A4 **Start depth:** 10.40 (m), **End depth:** 11.56 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.06 ±0.30 MPa	Permeability: 7.60E-09 ±1.27E-08 m/s	Constrained Mod.: 8.02 ±5.65 MPa
Sleeve friction: 27.97 ±6.44 kPa	N60: 5.80 ±0.91 blows	Go: 38.50 ±4.65 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 62.55 ±21.44 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.59 ±0.21
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.75 ±0.99
	Unit weight: 16.80 ±0.33 kN/m³	

.:: Layer No: 10 ::.

Code: B3 **Start depth:** 11.56 (m), **End depth:** 12.00 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 1.72 ±0.19 MPa	Permeability: 2.04E-08 ±1.15E-08 m/s	Constrained Mod.: 20.00 ±4.00 MPa
Sleeve friction: 40.76 ±8.42 kPa	N60: 8.09 ±0.73 blows	Go: 50.81 ±3.87 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 108.06 ±13.55 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 0.97 ±0.12
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.48 ±0.56
	Unit weight: 17.44 ±0.25 kN/m³	

.:: Layer No: 11 ::.

Code: A5 **Start depth:** 12.00 (m), **End depth:** 14.04 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.93 ±0.22 MPa	Permeability: 1.73E-09 ±3.55E-09 m/s	Constrained Mod.: 4.51 ±2.91 MPa
Sleeve friction: 35.77 ±13.61 kPa	N60: 5.84 ±0.96 blows	Go: 41.71 ±7.37 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 50.25 ±15.65 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.42 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.93 ±0.61
	Unit weight: 16.98 ±0.50 kN/m³	

.:: Layer No: 12 ::.

Code: B4 **Start depth:** 14.04 (m), **End depth:** 14.88 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.64 ±0.52 MPa	Permeability: 2.45E-08 ±3.57E-08 m/s	Constrained Mod.: 15.77 ±9.77 MPa
Sleeve friction: 37.92 ±10.78 kPa	N60: 8.05 ±1.46 blows	Go: 51.48 ±6.77 MPa
SBT_n: 3	Es: 44.05 ±2.45 MPa	Su: 99.20 ±37.27 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.76 ±0.30
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.53 ±1.37
	Unit weight: 17.29 ±0.36 kN/m³	

.:: Layer No: 13 ::.

Code: A6 **Start depth:** 14.88 (m), **End depth:** 15.54 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.00 ±0.08 MPa	Permeability: 1.41E-09 ±6.10E-10 m/s	Constrained Mod.: 4.09 ±0.98 MPa
Sleeve friction: 24.11 ±3.40 kPa	N60: 6.06 ±0.24 blows	Go: 40.17 ±2.18 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 53.00 ±5.72 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.39 ±0.04
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.80 ±0.20
	Unit weight: 16.64 ±0.17 kN/m³	

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Project:
Location:

CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.50	3.48E-06	3.9	19.9	0.0	0.0	15.1	22.2	83.6	9.1	42.0	17.8
0.50		(±7.46E-06)	(±0.9)	(±2.1)	(±0.0)	(±0.0)	(±3.1)	(±7.2)	(±5.3)	(±2.0)	(±9.0)	(±1.0)
0.50	1.08	5.71E-08	6.0	25.1	0.0	0.0	19.9	39.8	101.6	4.8	22.2	18.6
1.58		(±2.79E-08)	(±0.5)	(±0.9)	(±0.0)	(±0.0)	(±1.1)	(±3.5)	(±5.6)	(±1.2)	(±5.5)	(±0.1)
1.58	2.26	2.48E-08	4.2	0.0	0.0	0.0	12.2	28.9	62.2	1.4	6.3	17.0
3.84		(±1.55E-08)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±1.7)	(±2.8)	(±8.6)	(±0.2)	(±1.1)	(±0.5)
3.84	1.96	4.16E-08	6.6	33.2	0.0	0.0	19.2	41.9	98.2	1.5	7.2	17.6
5.80		(±3.83E-08)	(±0.8)	(±1.7)	(±0.0)	(±0.0)	(±3.8)	(±3.1)	(±19.1)	(±0.3)	(±1.5)	(±0.2)
5.80	0.68	7.60E-09	5.6	0.0	0.0	0.0	12.4	39.0	68.3	0.9	4.4	17.4
6.48		(±5.87E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±3.4)	(±2.8)	(±11.8)	(±0.2)	(±0.8)	(±0.2)
6.48	1.02	2.00E-09	3.9	0.0	0.0	0.0	3.9	27.8	39.1	0.5	2.3	16.3
7.50		(±9.54E-10)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±1.1)	(±2.2)	(±5.2)	(±0.1)	(±0.3)	(±0.2)
7.50	0.90	2.13E-09	6.0	0.0	0.0	0.0	9.2	45.5	62.8	0.7	3.4	17.7
8.40		(±1.49E-09)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±1.9)	(±4.1)	(±6.2)	(±0.1)	(±0.4)	(±0.3)
8.40	2.00	2.92E-09	4.4	0.0	0.0	0.0	3.5	31.4	39.3	0.4	1.9	16.4
10.40		(±8.05E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±2.8)	(±5.6)	(±13.7)	(±0.1)	(±0.6)	(±0.6)
10.40	1.16	7.60E-09	5.8	0.0	0.0	0.0	8.0	38.5	62.5	0.6	2.7	16.8
11.56		(±1.27E-08)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±5.7)	(±4.7)	(±21.4)	(±0.2)	(±1.0)	(±0.3)
11.56	0.44	2.04E-08	8.1	0.0	0.0	0.0	20.0	50.8	108.1	1.0	4.5	17.4
12.00		(±1.15E-08)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±4.0)	(±3.9)	(±13.6)	(±0.1)	(±0.6)	(±0.2)
12.00	2.04	1.73E-09	5.8	0.0	0.0	0.0	4.5	41.7	50.2	0.4	1.9	17.0
14.04		(±3.55E-09)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±2.9)	(±7.4)	(±15.7)	(±0.1)	(±0.6)	(±0.5)

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Project:
Location:

CPT: CPTu-02
Total depth: 15.54 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
14.04	0.84	2.45E-08	8.0	44.1	0.0	0.0	15.8	51.5	99.2	0.8	3.5	17.3
14.88		(±3.57E-08)	(±1.5)	(±2.5)	(±0.0)	(±0.0)	(±9.8)	(±6.8)	(±37.3)	(±0.3)	(±1.4)	(±0.4)
14.88	0.66	1.41E-09	6.1	0.0	0.0	0.0	4.1	40.2	53.0	0.4	1.8	16.6
15.54		(±6.10E-10)	(±0.2)	(±0.0)	(±0.0)	(±0.0)	(±1.0)	(±2.2)	(±5.7)	(±0.0)	(±0.2)	(±0.2)

Depth values presented in this table are measured from free ground surface

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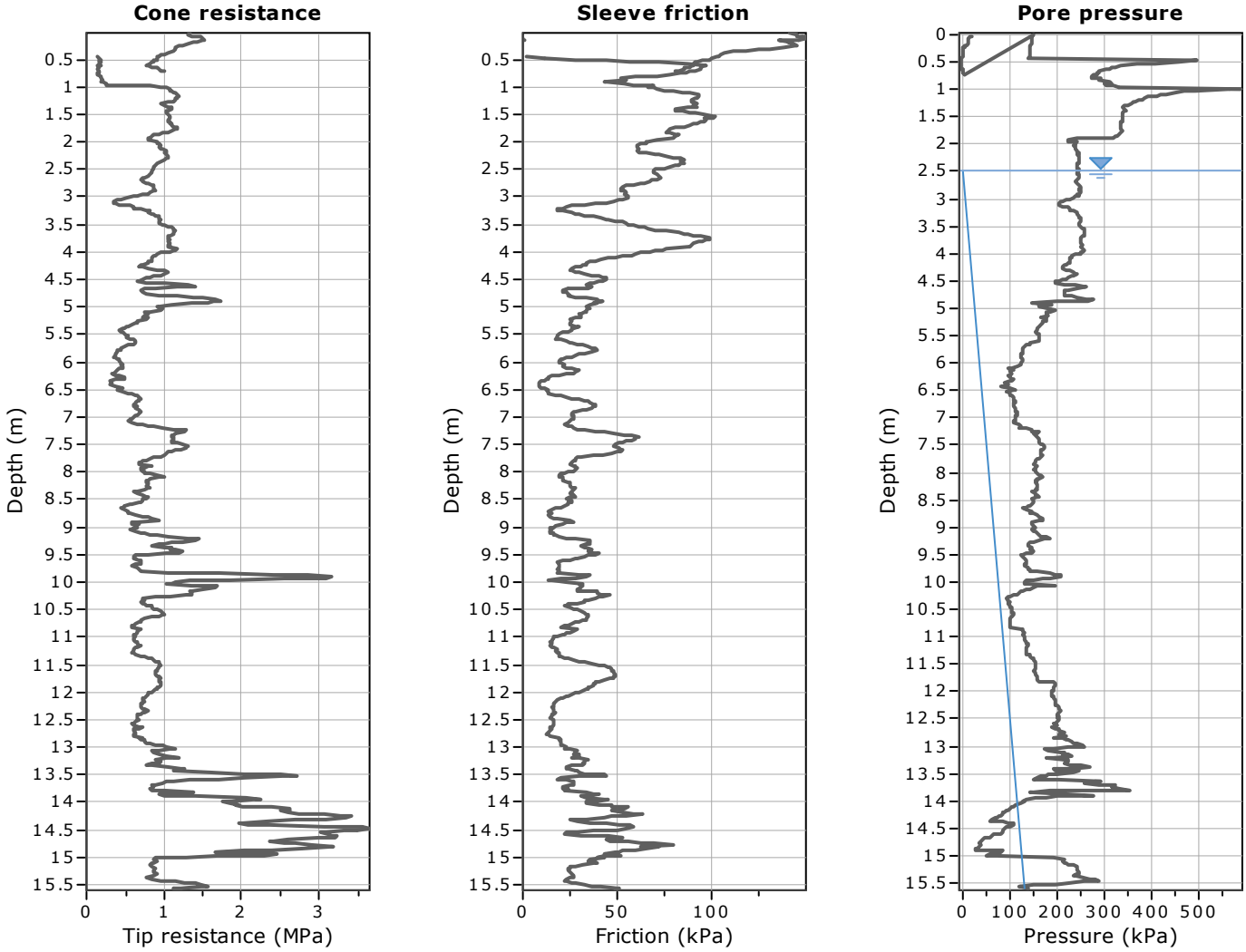
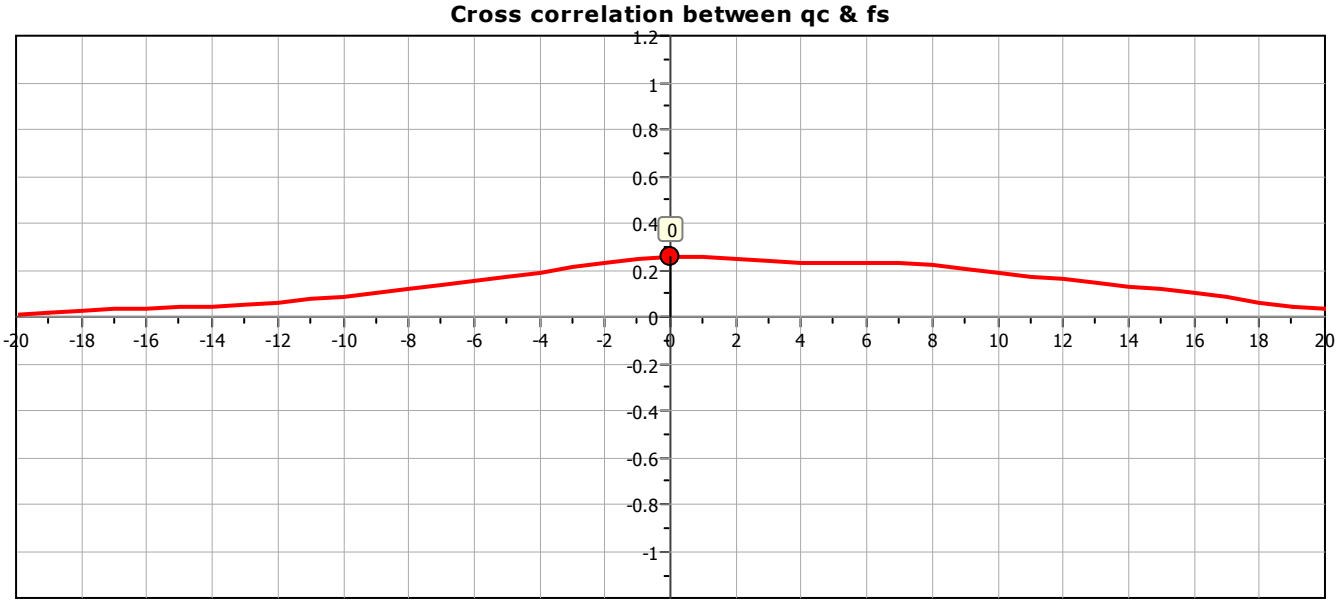
CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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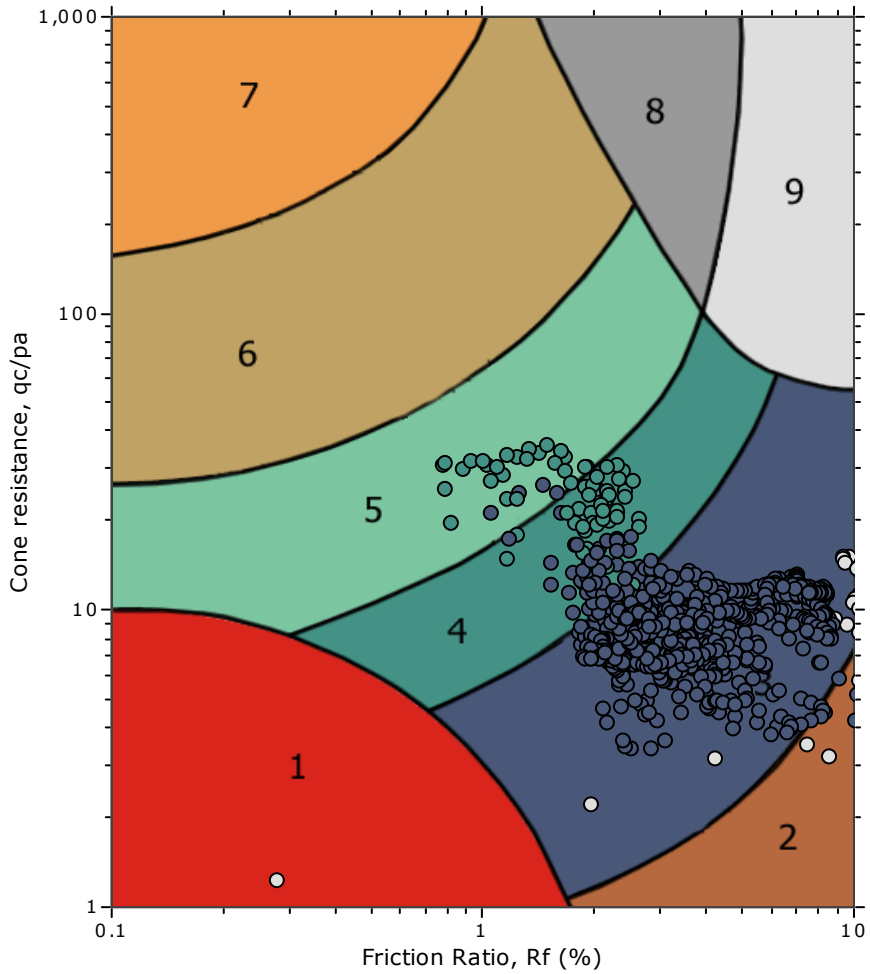
Project:
Location:

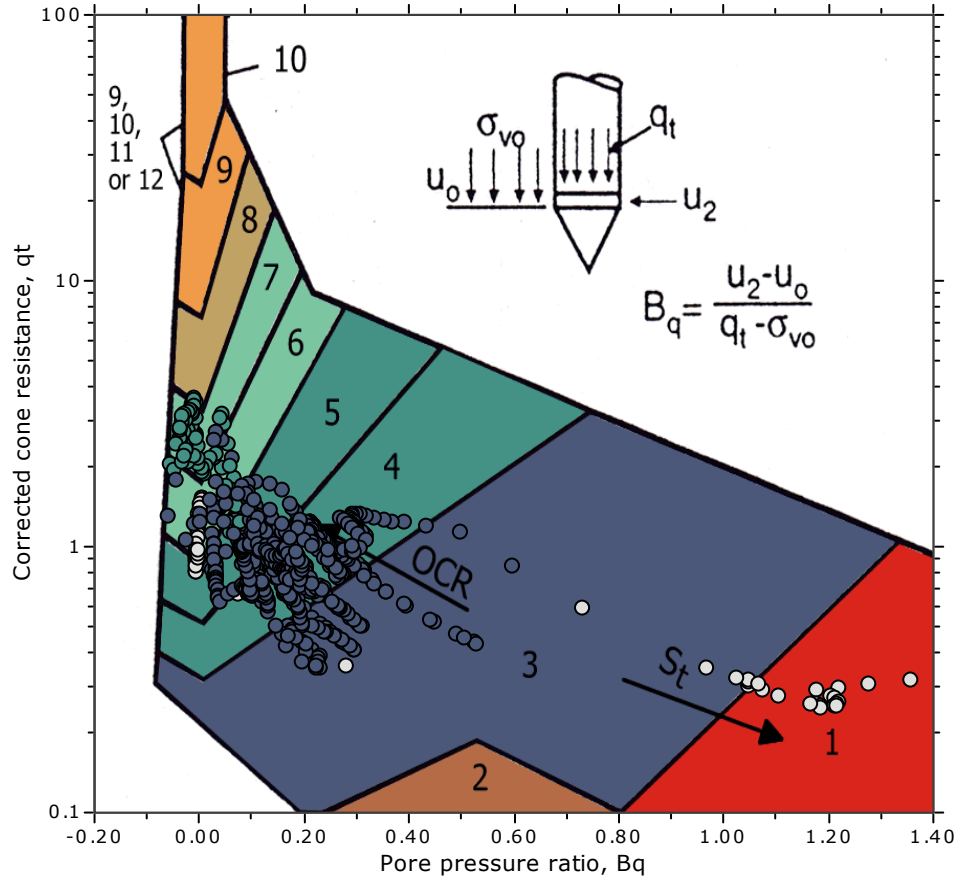
CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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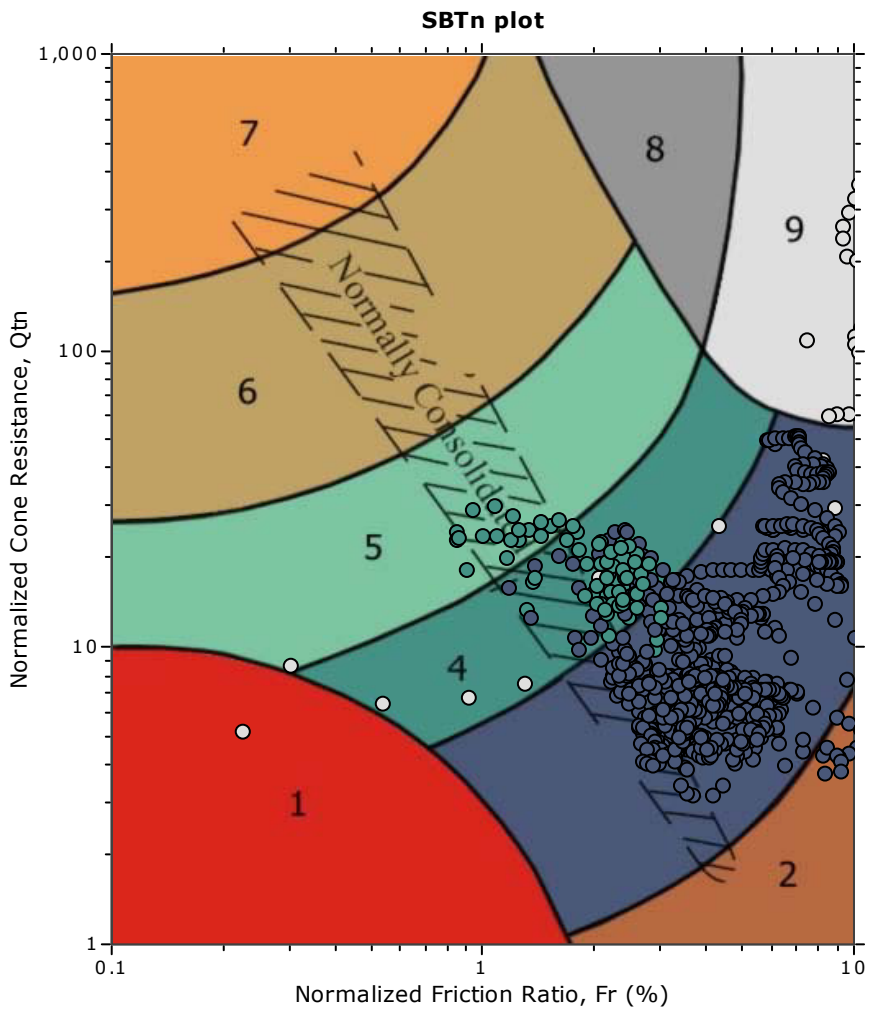
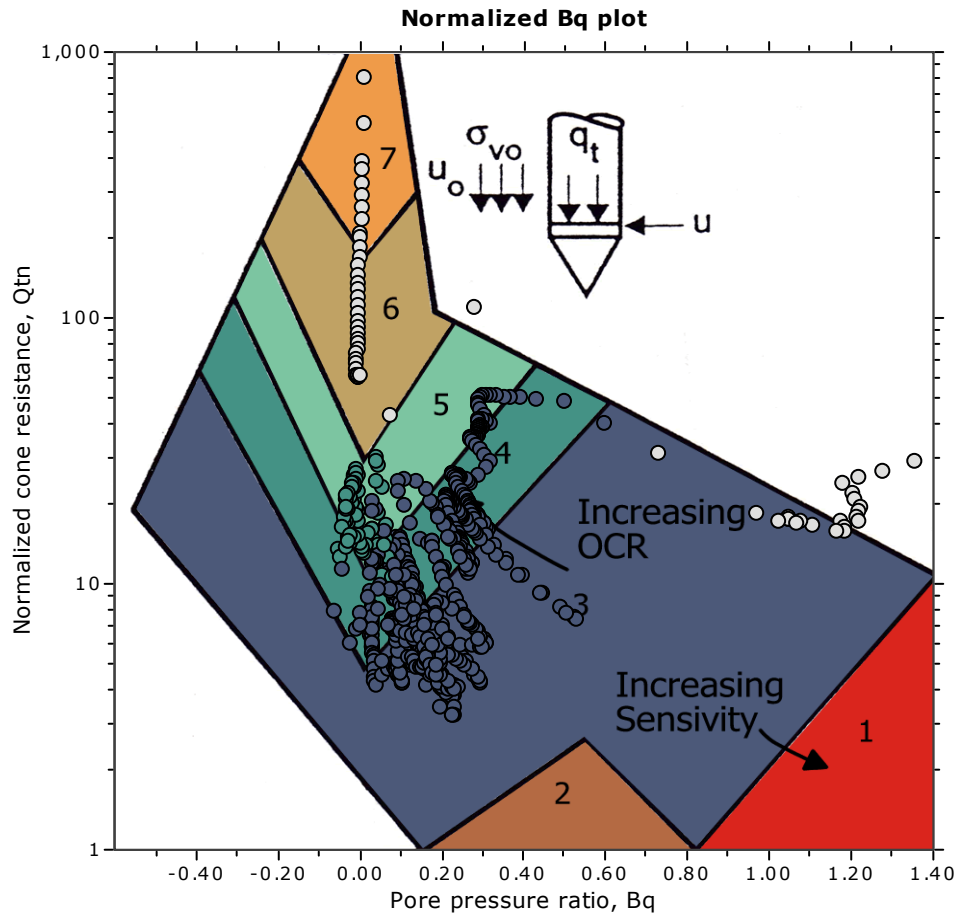
Project:
Location:

CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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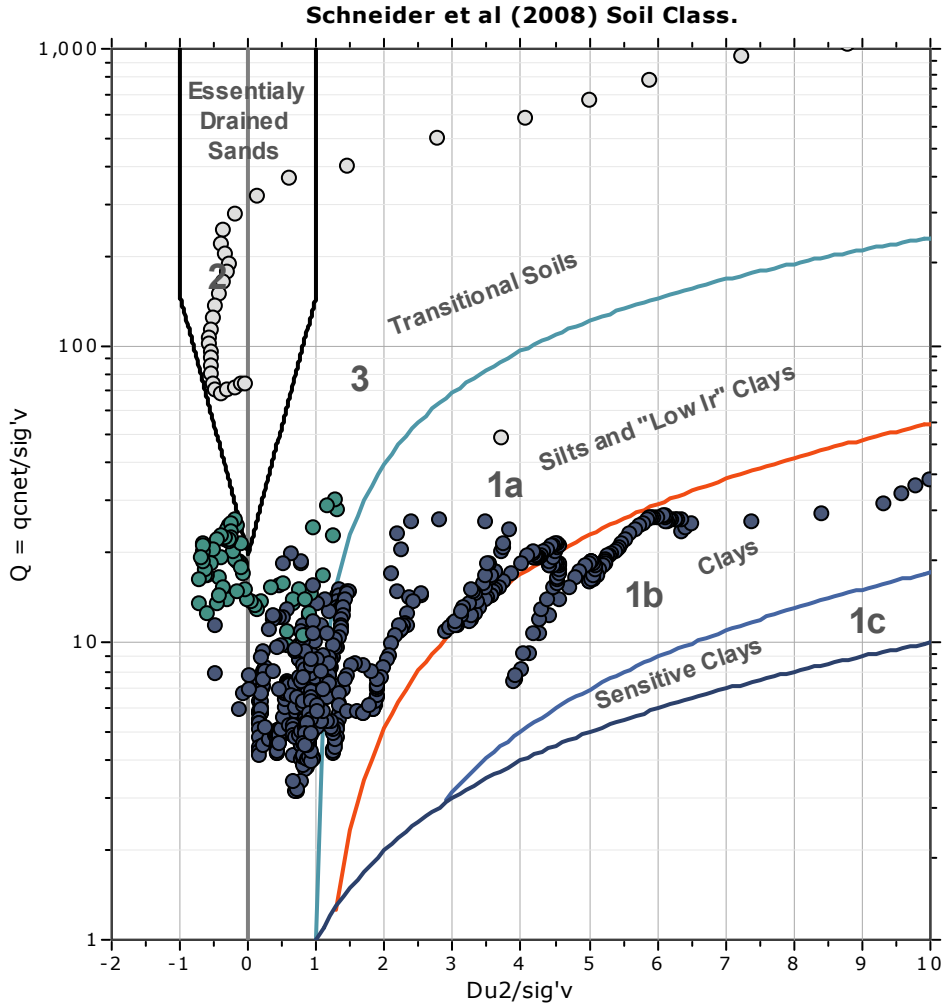
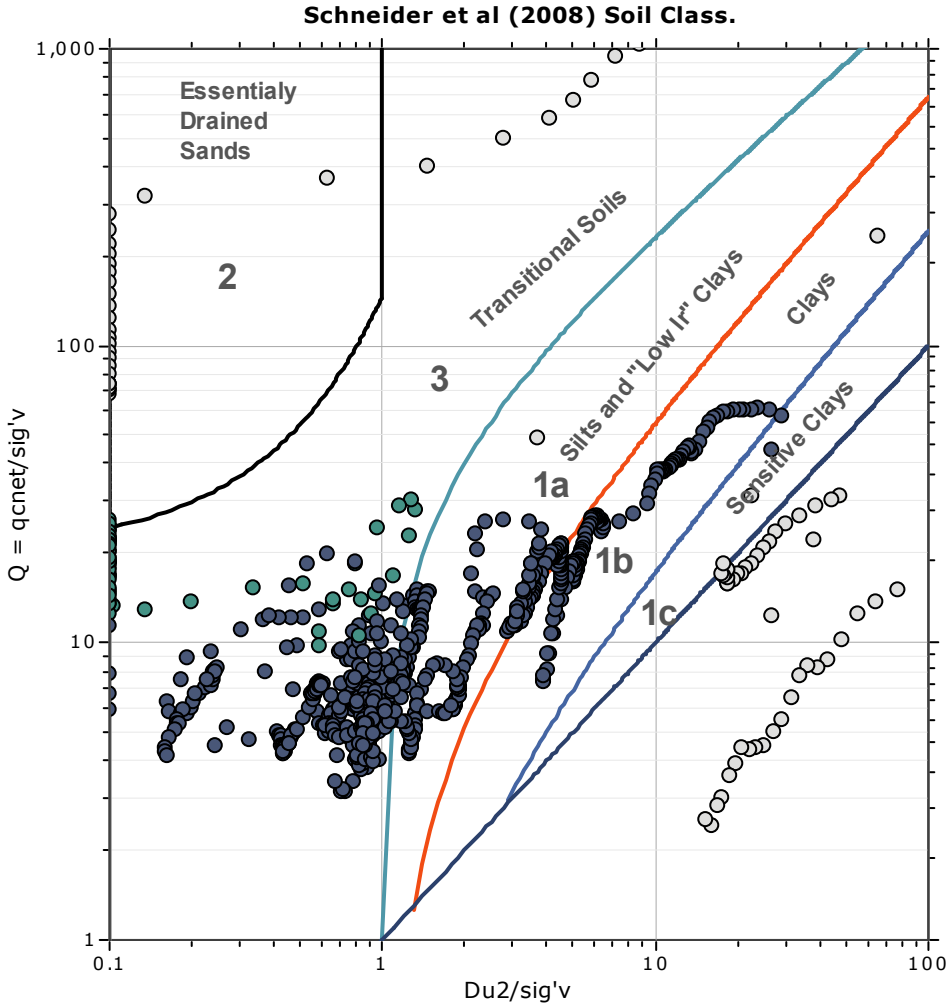
Project:
Location:

CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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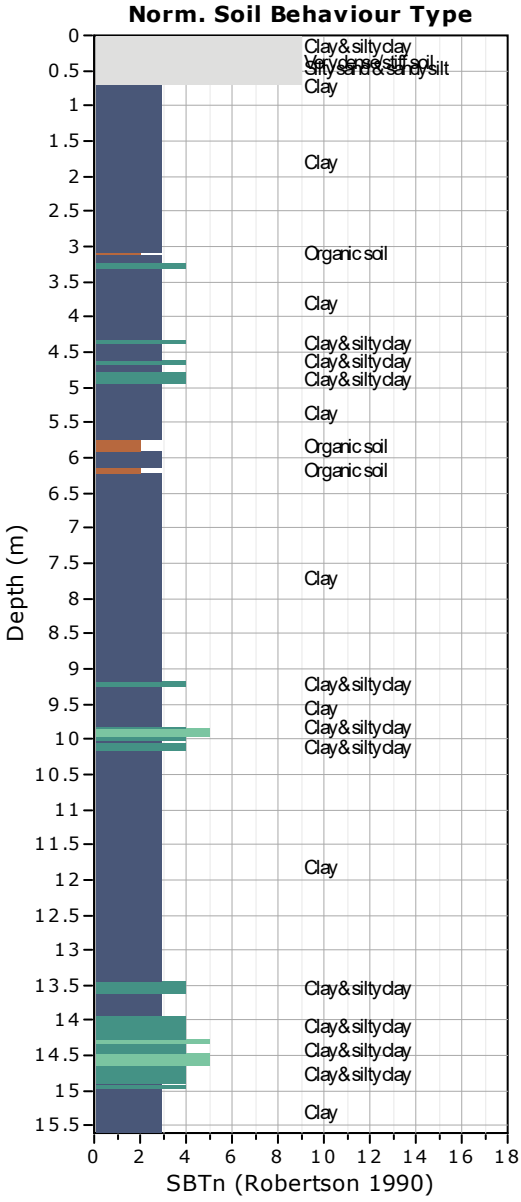
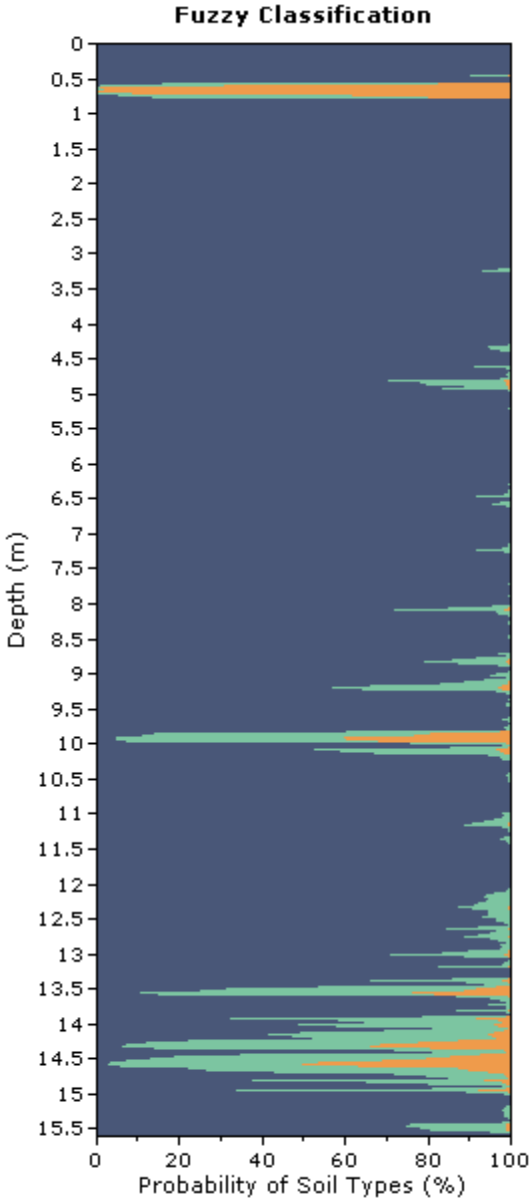
CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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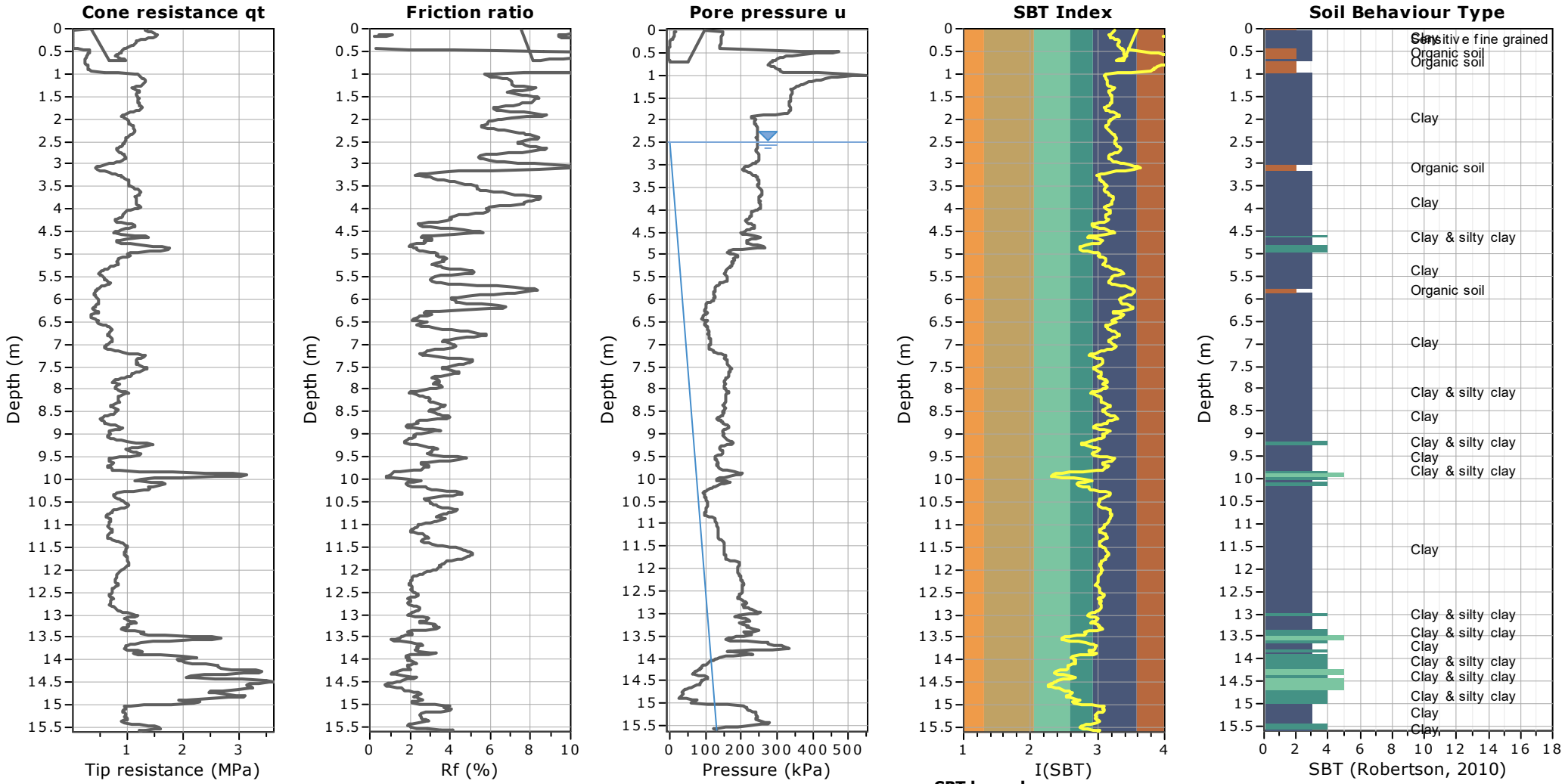
Project:
Location:

CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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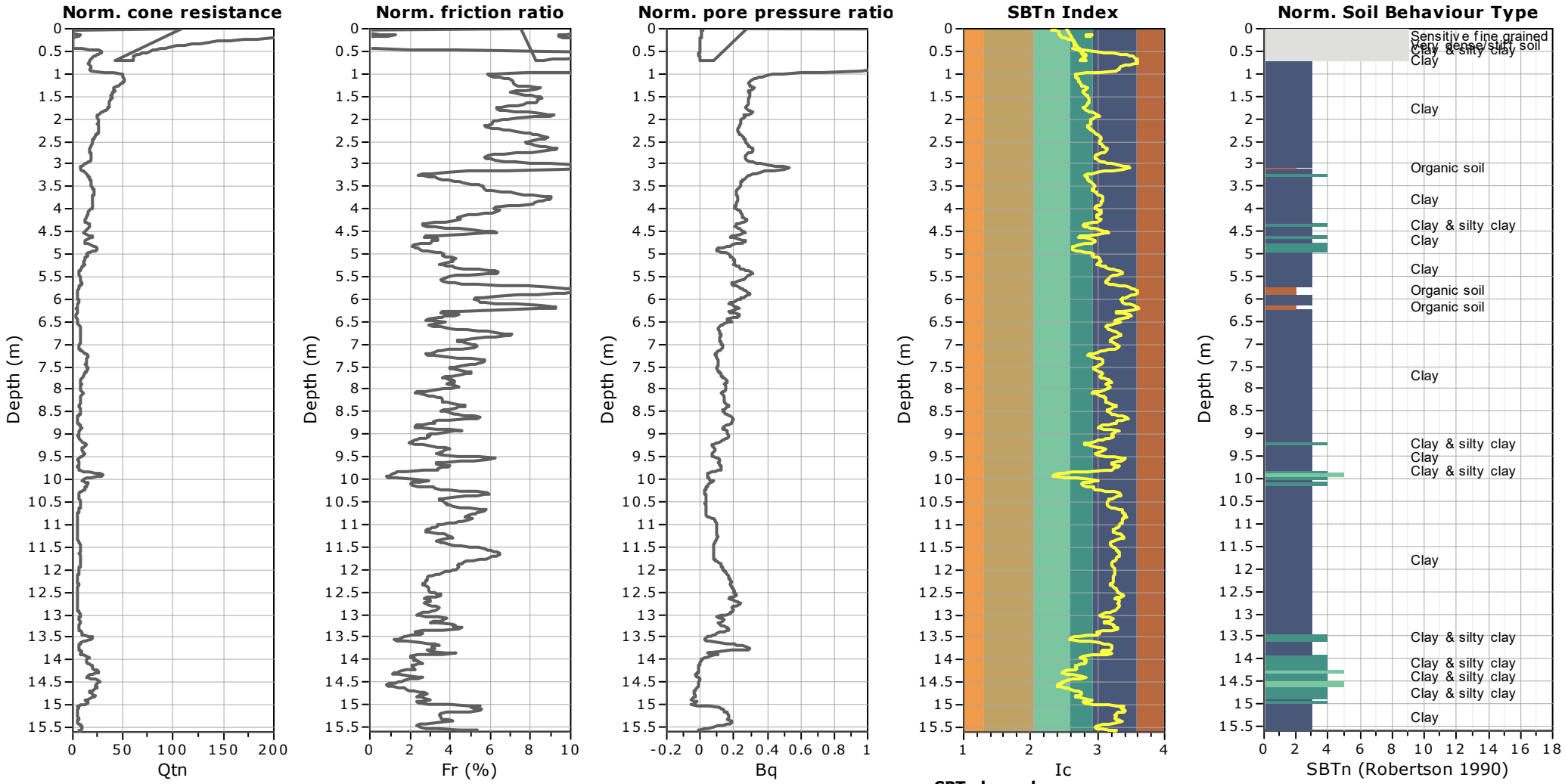
Project:
Location:

CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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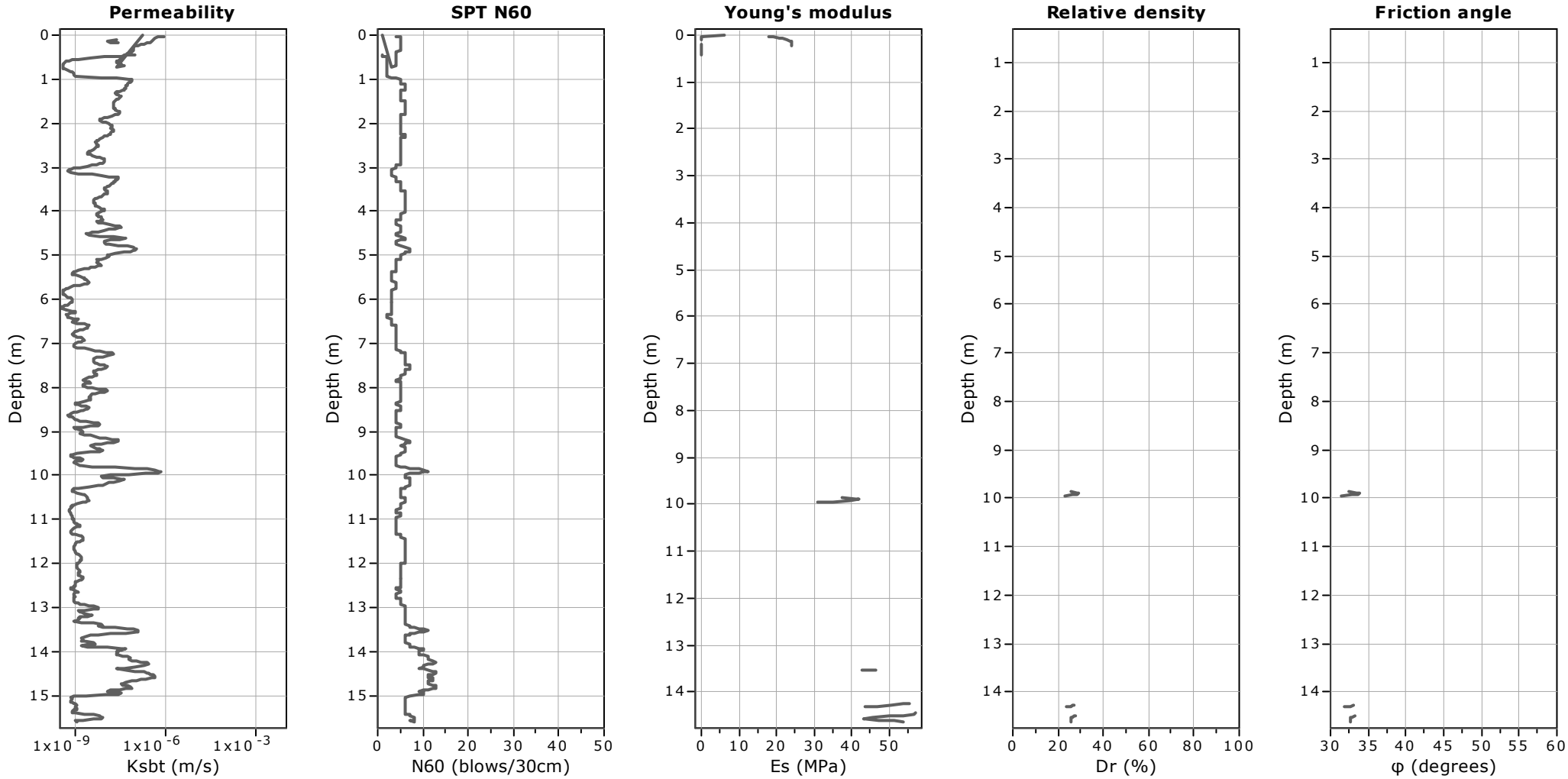
Project:
Location:

CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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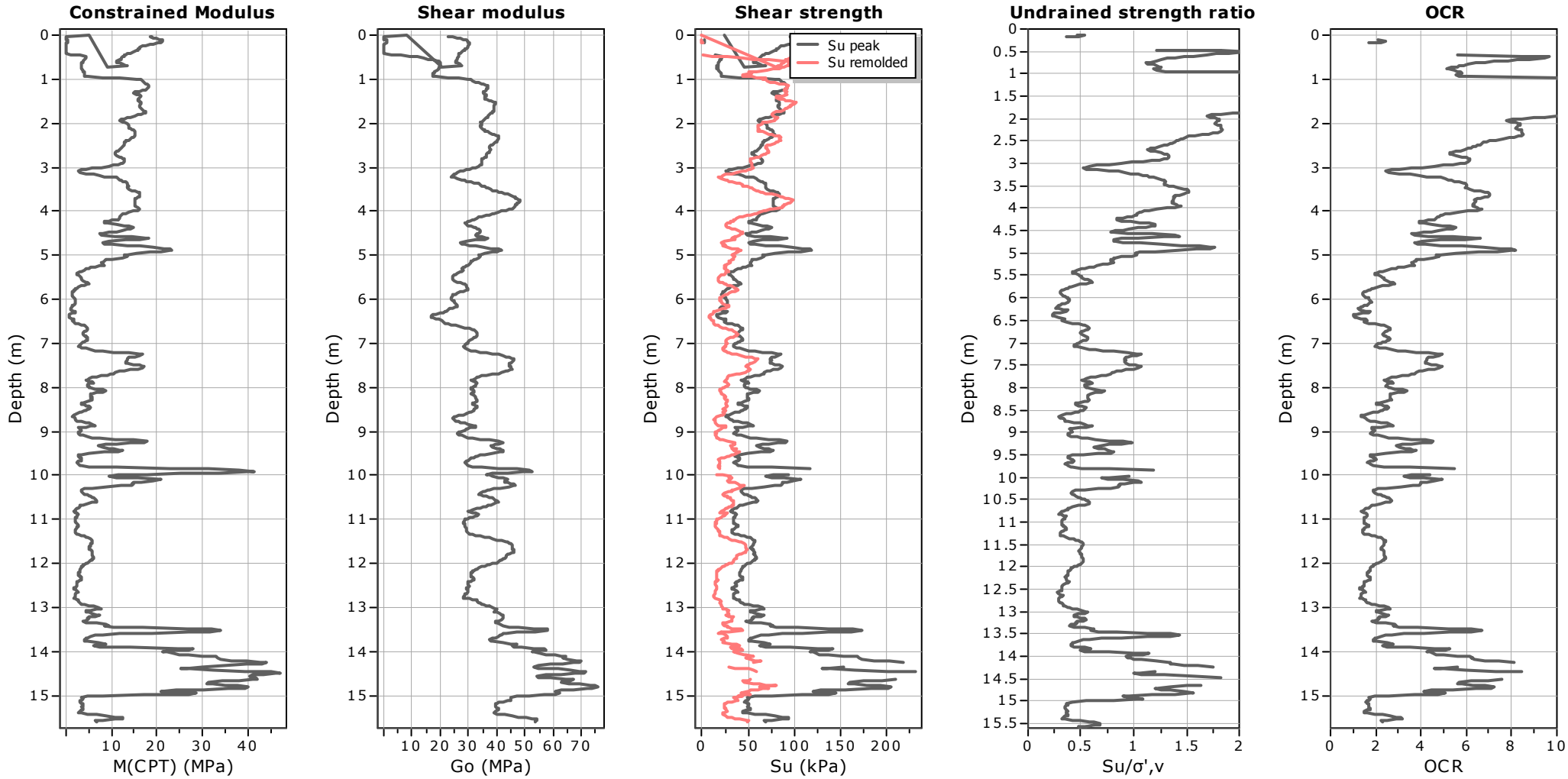
Project:
Location:

CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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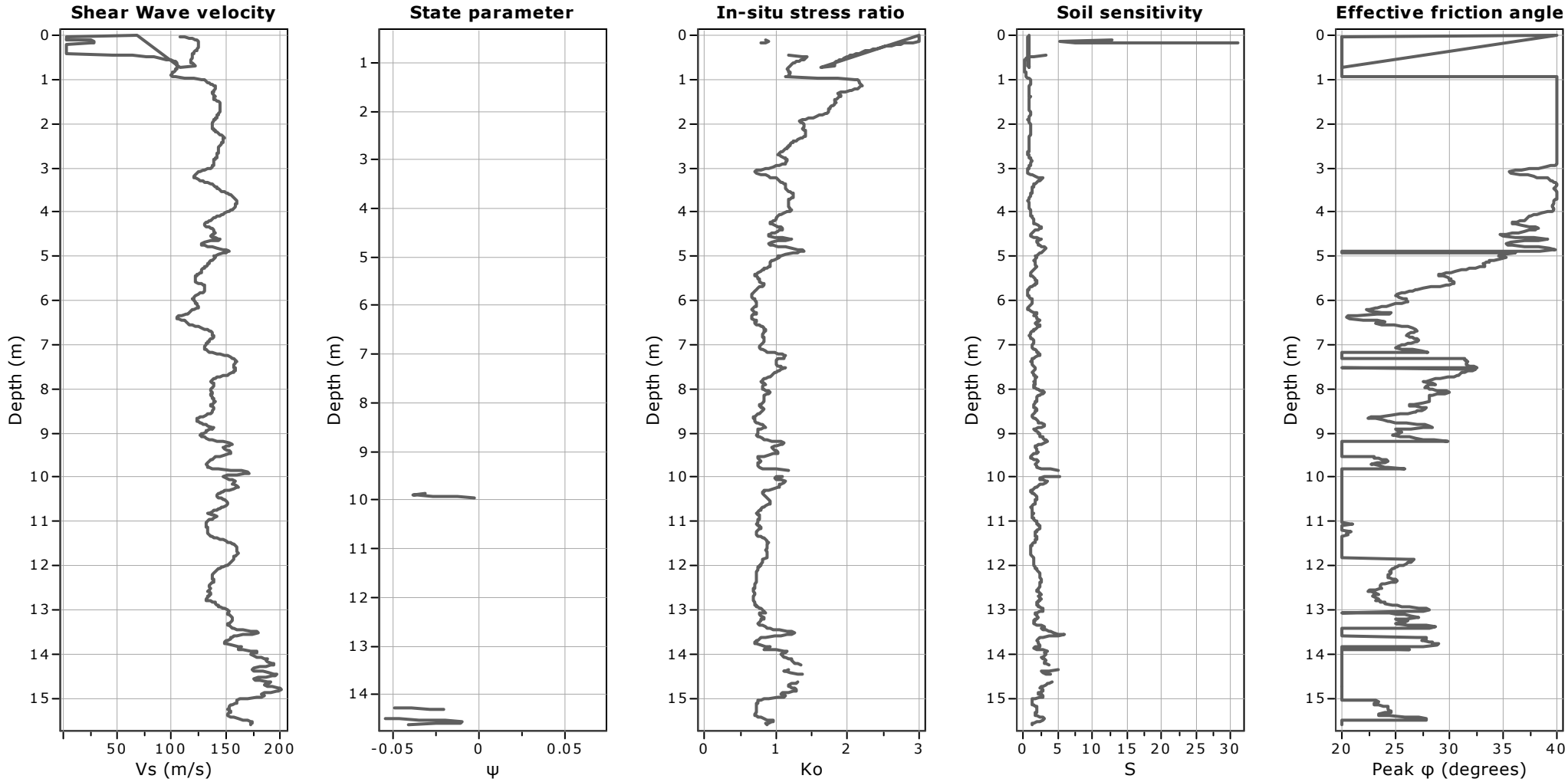
Project:
Location:

CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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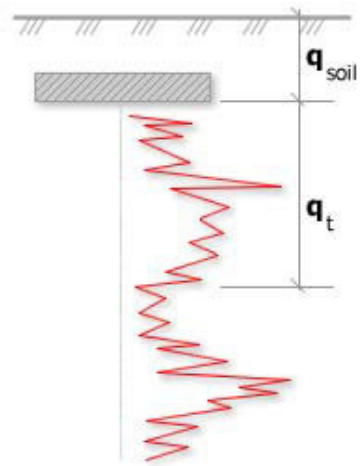
CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

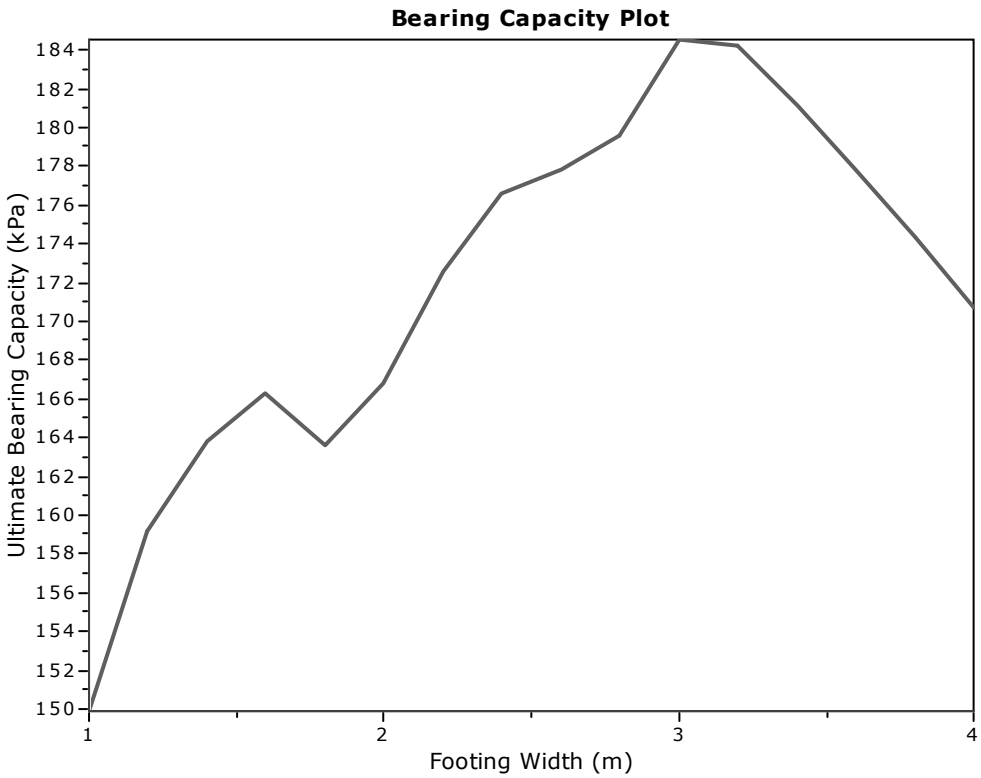
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	0.70	0.20	9.50	149.91
2	1.20	0.50	2.30	0.75	0.20	9.50	159.20
3	1.40	0.50	2.60	0.77	0.20	9.50	163.83
4	1.60	0.50	2.90	0.78	0.20	9.50	166.29
5	1.80	0.50	3.20	0.77	0.20	9.50	163.66
6	2.00	0.50	3.50	0.79	0.20	9.50	166.76
7	2.20	0.50	3.80	0.82	0.20	9.50	172.55
8	2.40	0.50	4.10	0.84	0.20	9.50	176.62
9	2.60	0.50	4.40	0.84	0.20	9.50	177.88
10	2.80	0.50	4.70	0.85	0.20	9.50	179.59
11	3.00	0.50	5.00	0.88	0.20	9.50	184.53
12	3.20	0.50	5.30	0.87	0.20	9.50	184.25
13	3.40	0.50	5.60	0.86	0.20	9.50	181.15
14	3.60	0.50	5.90	0.84	0.20	9.50	177.87
15	3.80	0.50	6.20	0.82	0.20	9.50	174.30
16	4.00	0.50	6.50	0.81	0.20	9.50	170.68

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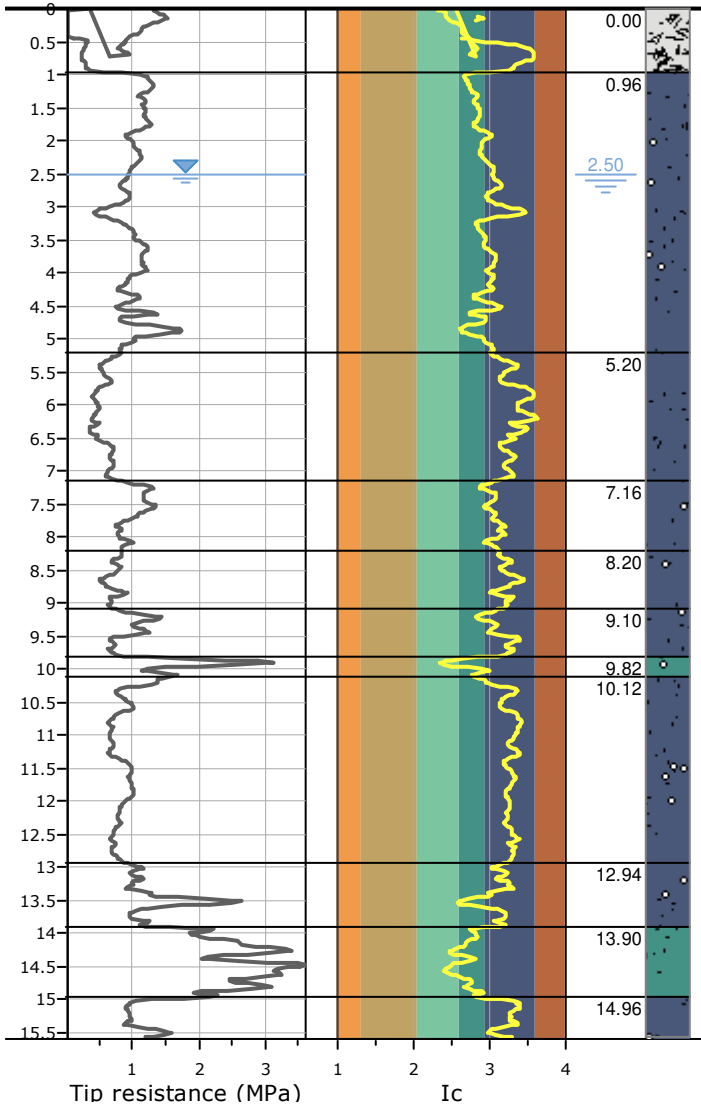
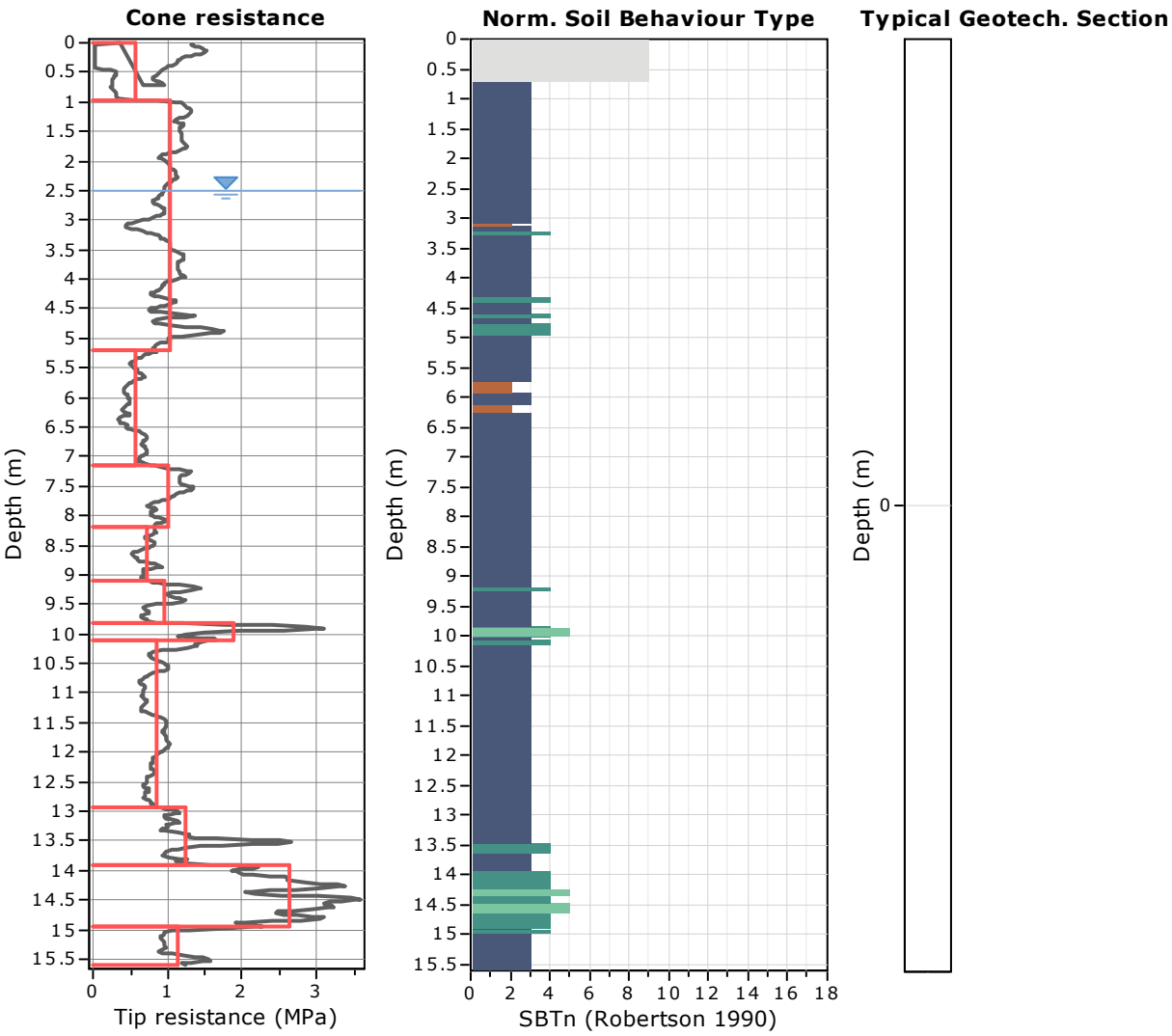
CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



Depth (m)	Description	qt (MPa)	Ksbt (m/s)	N60	Es (MPa)	Dr	Phi (°)	M (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
0.00	Very dense/stiff soil	0.6	8.73E-8	3.3	9.2	-	-	7.8	17.2	50.5	7.1	32.9	17.9
0.96	Clay	1.0	1.67E-8	5.1	-	-	-	13.4	35.9	70.0	1.6	7.5	17.6
5.20	Clay	0.6	1.39E-9	3.4	-	-	-	3.1	26.6	32.8	0.5	2.1	16.3
7.16	Clay	1.0	5.80E-9	5.5	-	-	-	10.0	37.6	63.6	0.8	3.6	17.0
8.20	Clay	0.7	2.00E-9	4.4	-	-	-	3.8	29.7	41.0	0.5	2.1	16.3
9.10	Clay	1.0	5.87E-9	5.1	-	-	-	7.2	35.1	56.2	0.6	2.7	16.7
9.82	Clay & silty clay	1.9	1.88E-7	7.6	-	-	-	23.1	42.8	90.5	0.9	4.2	16.9
10.12	Clay	0.8	1.76E-9	5.1	-	-	-	4.2	35.5	46.3	0.4	2.0	16.6
12.94	Clay	1.3	1.40E-8	6.7	44.7	-	-	9.3	42.6	73.3	0.6	2.8	16.9
13.90	Clay & silty clay	2.6	1.07E-7	10.9	55.5	-	-	33.3	62.8	158.7	1.2	5.7	17.8
14.96	Clay	1.1	3.00E-9	6.7	-	-	-	6.4	45.2	62.9	0.5	2.1	17.0



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.96 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 0.57 ±0.50 MPa	Permeability: 8.73E-08 ±1.51E-07 m/s	Constrained Mod.: 7.80 ±7.10 MPa
Sleeve friction: 68.93 ±52.18 kPa	N60: 3.33 ±1.37 blows	Go: 17.17 ±11.22 MPa
SBT_n: 9	Es: 9.23 ±11.18 MPa	Su: 50.46 ±33.53 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 7.13 ±9.66
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 32.93 ±44.64
	Unit weight: 17.86 ±1.36 kN/m³	

.:: Layer No: 2 ::.

Code: A1 **Start depth:** 0.96 (m), **End depth:** 5.20 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.04 ±0.21 MPa	Permeability: 1.67E-08 ±1.80E-08 m/s	Constrained Mod.: 13.45 ±3.51 MPa
Sleeve friction: 60.61 ±23.55 kPa	N60: 5.08 ±0.83 blows	Go: 35.87 ±5.14 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 70.00 ±15.56 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.62 ±0.77
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 7.47 ±3.56
	Unit weight: 17.61 ±0.55 kN/m³	

.:: Layer No: 3 ::.

Code: D1 **Start depth:** 5.20 (m), **End depth:** 7.16 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.57 ±0.13 MPa	Permeability: 1.39E-09 ±1.24E-09 m/s	Constrained Mod.: 3.11 ±1.66 MPa
Sleeve friction: 23.96 ±7.85 kPa	N60: 3.44 ±0.59 blows	Go: 26.57 ±4.03 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 32.75 ±9.01 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.45 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.08 ±0.58
	Unit weight: 16.35 ±0.48 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 7.16 (m), **End depth:** 8.20 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.02 ±0.19 MPa	Permeability: 5.80E-09 ±3.91E-09 m/s	Constrained Mod.: 9.98 ±4.36 MPa
Sleeve friction: 36.27 ±13.54 kPa	N60: 5.51 ±0.75 blows	Go: 37.65 ±5.97 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 63.59 ±14.13 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.77 ±0.19
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.55 ±0.86
	Unit weight: 17.04 ±0.48 kN/m³	

.:: Layer No: 5 ::.

Code: D2 **Start depth:** 8.20 (m), **End depth:** 9.10 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.72 ±0.11 MPa	Permeability: 2.00E-09 ±1.34E-09 m/s	Constrained Mod.: 3.81 ±1.38 MPa
Sleeve friction: 20.97 ±5.05 kPa	N60: 4.37 ±0.49 blows	Go: 29.73 ±2.88 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 41.01 ±7.65 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.46 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.11 ±0.41
	Unit weight: 16.33 ±0.31 kN/m³	

.:: Layer No: 6 ::.

Code: A3 **Start depth:** 9.10 (m), **End depth:** 9.82 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.95 ±0.25 MPa	Permeability: 5.87E-09 ±6.85E-09 m/s	Constrained Mod.: 7.18 ±4.51 MPa
Sleeve friction: 26.55 ±8.12 kPa	N60: 5.08 ±0.98 blows	Go: 35.14 ±5.06 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 56.19 ±17.89 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.59 ±0.19
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.74 ±0.89
	Unit weight: 16.68 ±0.41 kN/m³	

.:: Layer No: 7 ::.

Code: B1 **Start depth:** 9.82 (m), **End depth:** 10.12 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 1.90 ±0.68 MPa	Permeability: 1.88E-07 ±2.37E-07 m/s	Constrained Mod.: 23.06 ±10.72 MPa
Sleeve friction: 26.10 ±6.88 kPa	N60: 7.56 ±1.67 blows	Go: 42.84 ±5.28 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 90.48 ±16.20 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 0.91 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.22 ±0.76
	Unit weight: 16.94 ±0.32 kN/m³	

.:: Layer No: 8 ::.

Code: D3 **Start depth:** 10.12 (m), **End depth:** 12.94 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.85 ±0.18 MPa	Permeability: 1.76E-09 ±3.17E-09 m/s	Constrained Mod.: 4.20 ±2.96 MPa
Sleeve friction: 26.10 ±10.64 kPa	N60: 5.12 ±0.82 blows	Go: 35.49 ±5.85 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 46.26 ±12.98 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.43 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.97 ±0.62
	Unit weight: 16.58 ±0.51 kN/m³	

.:: Layer No: 9 ::.

Code: A4 **Start depth:** 12.94 (m), **End depth:** 13.90 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.26 ±0.43 MPa	Permeability: 1.40E-08 ±2.99E-08 m/s	Constrained Mod.: 9.28 ±7.84 MPa
Sleeve friction: 27.84 ±5.80 kPa	N60: 6.67 ±1.25 blows	Go: 42.58 ±4.99 MPa
SBT_n: 3	Es: 44.70 ±2.54 MPa	Su: 73.35 ±30.89 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.60 ±0.26
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.78 ±1.18
	Unit weight: 16.87 ±0.26 kN/m³	

.:: Layer No: 10 ::.

Code: C **Start depth:** 13.90 (m), **End depth:** 14.96 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 2.64 ±0.52 MPa	Permeability: 1.07E-07 ±1.14E-07 m/s	Constrained Mod.: 33.28 ±7.72 MPa
Sleeve friction: 47.49 ±12.58 kPa	N60: 10.93 ±1.36 blows	Go: 62.81 ±6.56 MPa
SBT_n: 4	Es: 55.46 ±1.66 MPa	Su: 158.69 ±32.20 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.24 ±0.26
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.72 ±1.18
	Unit weight: 17.76 ±0.32 kN/m³	

.:: Layer No: 11 ::.

Code: A5 **Start depth:** 14.96 (m), **End depth:** 15.60 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.14 ±0.31 MPa	Permeability: 3.00E-09 ±4.83E-09 m/s	Constrained Mod.: 6.36 ±5.19 MPa
Sleeve friction: 32.21 ±8.89 kPa	N60: 6.69 ±1.06 blows	Go: 45.15 ±6.09 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 62.90 ±22.14 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.46 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.13 ±0.76
	Unit weight: 16.98 ±0.34 kN/m³	

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geologozamboni@gmail.com

Project:
Location:

CPT: CPTu-03
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.96	8.73E-08	3.3	9.2	0.0	0.0	7.8	17.2	50.5	7.1	32.9	17.9
0.96		(±1.51E-07)	(±1.4)	(±11.2)	(±0.0)	(±0.0)	(±7.1)	(±11.2)	(±33.5)	(±9.7)	(±44.6)	(±1.4)
0.96	4.24	1.67E-08	5.1	0.0	0.0	0.0	13.4	35.9	70.0	1.6	7.5	17.6
5.20		(±1.80E-08)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±3.5)	(±5.1)	(±15.6)	(±0.8)	(±3.6)	(±0.5)
5.20	1.96	1.39E-09	3.4	0.0	0.0	0.0	3.1	26.6	32.8	0.5	2.1	16.3
7.16		(±1.24E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±1.7)	(±4.0)	(±9.0)	(±0.1)	(±0.6)	(±0.5)
7.16	1.04	5.80E-09	5.5	0.0	0.0	0.0	10.0	37.6	63.6	0.8	3.6	17.0
8.20		(±3.91E-09)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±4.4)	(±6.0)	(±14.1)	(±0.2)	(±0.9)	(±0.5)
8.20	0.90	2.00E-09	4.4	0.0	0.0	0.0	3.8	29.7	41.0	0.5	2.1	16.3
9.10		(±1.34E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.4)	(±2.9)	(±7.7)	(±0.1)	(±0.4)	(±0.3)
9.10	0.72	5.87E-09	5.1	0.0	0.0	0.0	7.2	35.1	56.2	0.6	2.7	16.7
9.82		(±6.85E-09)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±4.5)	(±5.1)	(±17.9)	(±0.2)	(±0.9)	(±0.4)
9.82	0.30	1.88E-07	7.6	0.0	0.0	0.0	23.1	42.8	90.5	0.9	4.2	16.9
10.12		(±2.37E-07)	(±1.7)	(±0.0)	(±0.0)	(±0.0)	(±10.7)	(±5.3)	(±16.2)	(±0.2)	(±0.8)	(±0.3)
10.12	2.82	1.76E-09	5.1	0.0	0.0	0.0	4.2	35.5	46.3	0.4	2.0	16.6
12.94		(±3.17E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±5.8)	(±13.0)	(±0.1)	(±0.6)	(±0.5)
12.94	0.96	1.40E-08	6.7	44.7	0.0	0.0	9.3	42.6	73.3	0.6	2.8	16.9
13.90		(±2.99E-08)	(±1.2)	(±2.5)	(±0.0)	(±0.0)	(±7.8)	(±5.0)	(±30.9)	(±0.3)	(±1.2)	(±0.3)
13.90	1.06	1.07E-07	10.9	55.5	0.0	0.0	33.3	62.8	158.7	1.2	5.7	17.8
14.96		(±1.14E-07)	(±1.4)	(±1.7)	(±0.0)	(±0.0)	(±7.7)	(±6.6)	(±32.2)	(±0.3)	(±1.2)	(±0.3)
14.96	0.64	3.00E-09	6.7	0.0	0.0	0.0	6.4	45.2	62.9	0.5	2.1	17.0
15.60		(±4.83E-09)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±5.2)	(±6.1)	(±22.1)	(±0.2)	(±0.8)	(±0.3)

Depth values presented in this table are measured from free ground surface

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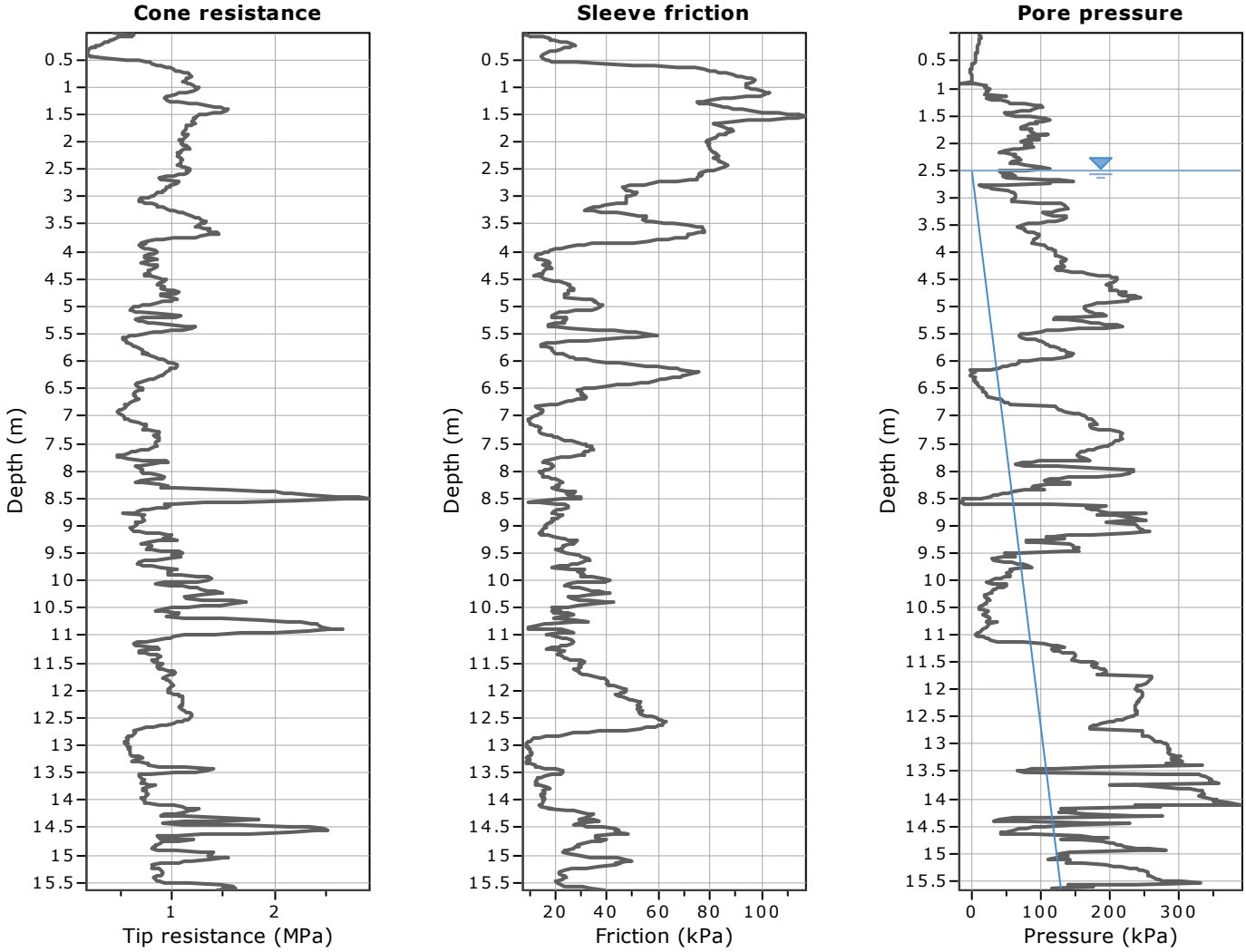
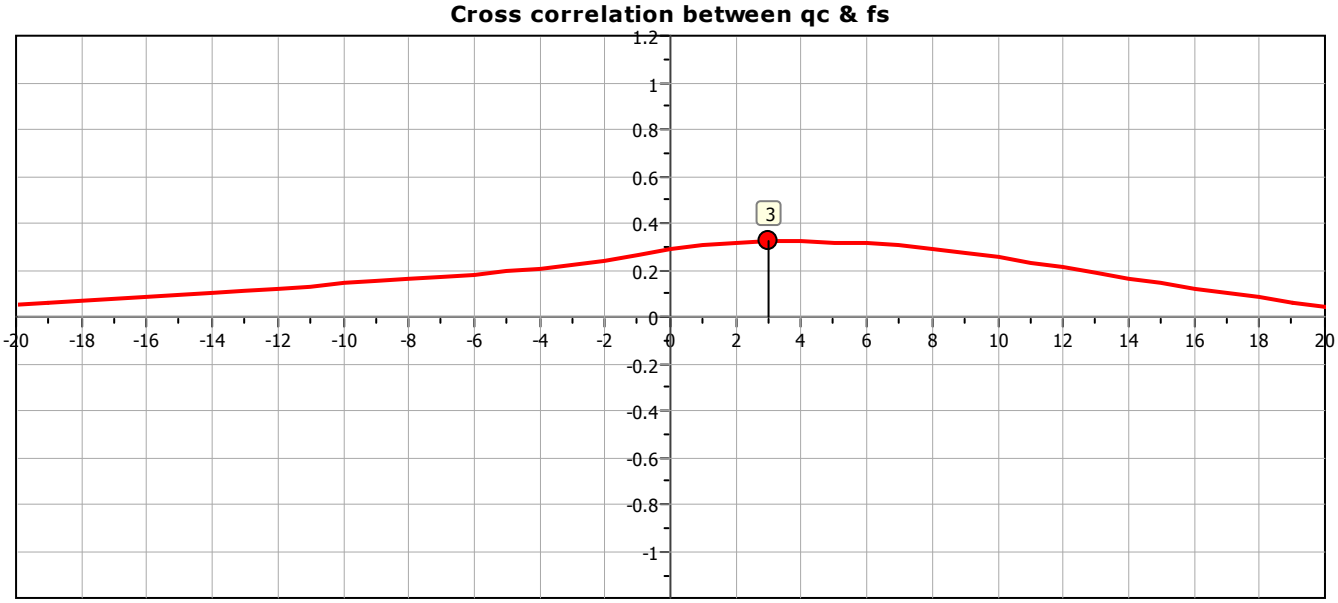
CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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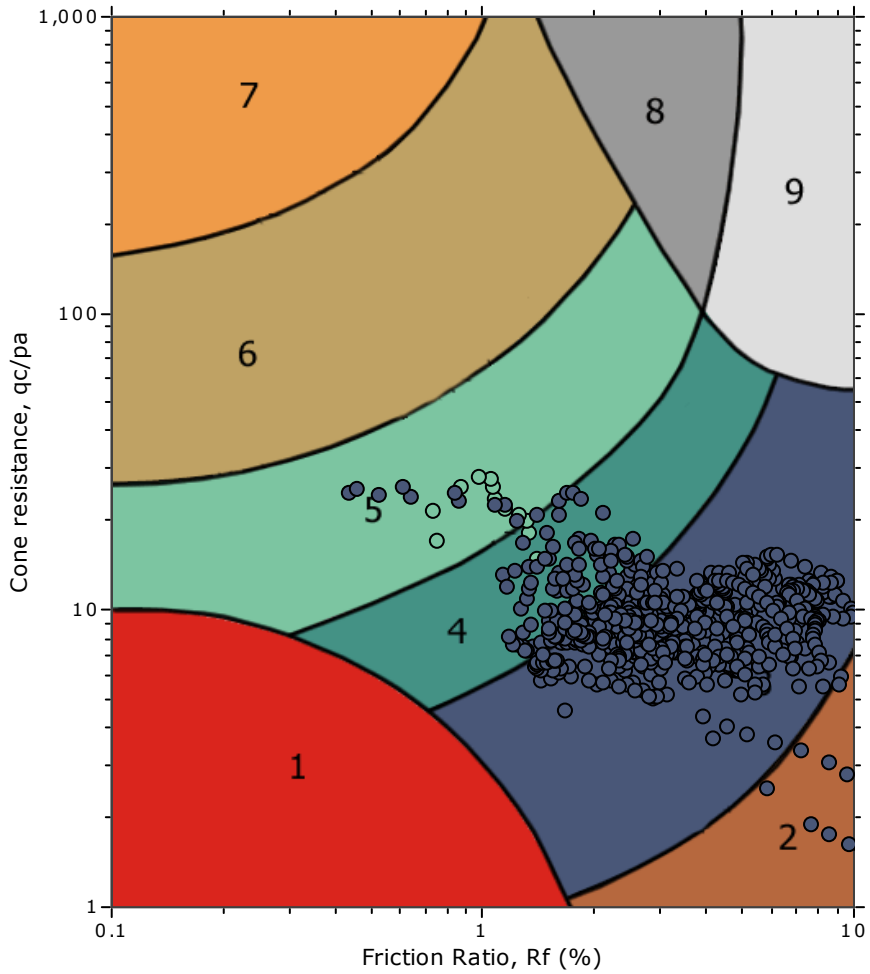
Project:
Location:

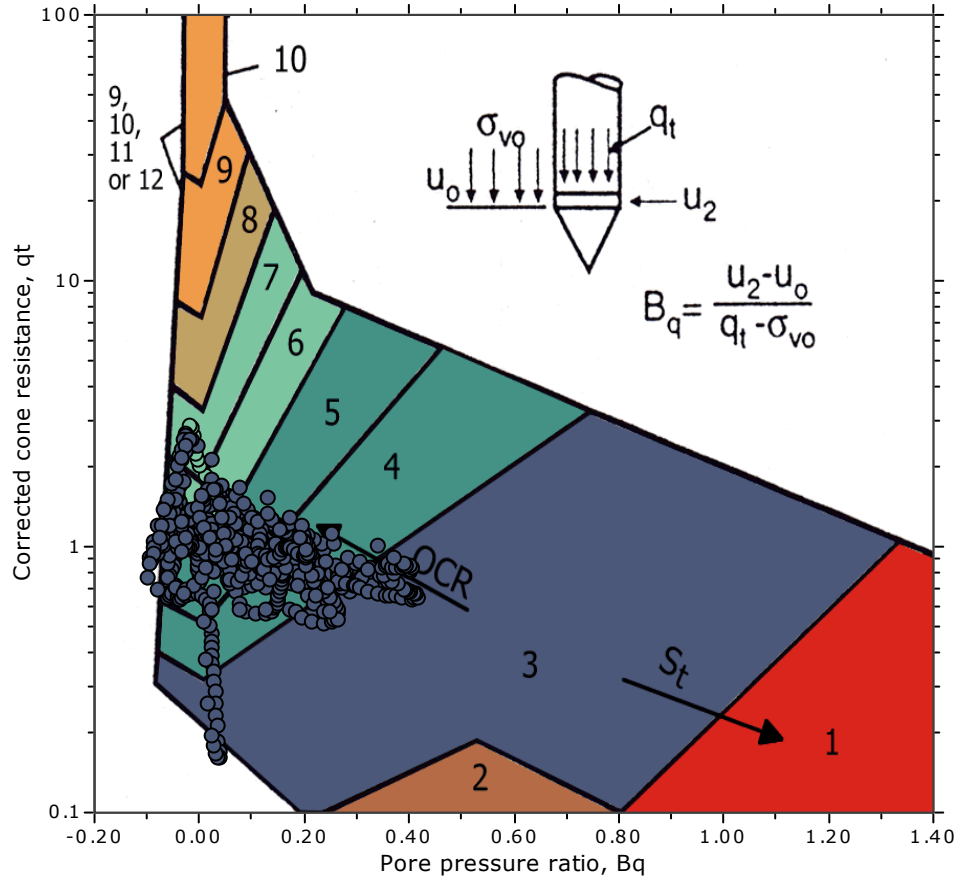
CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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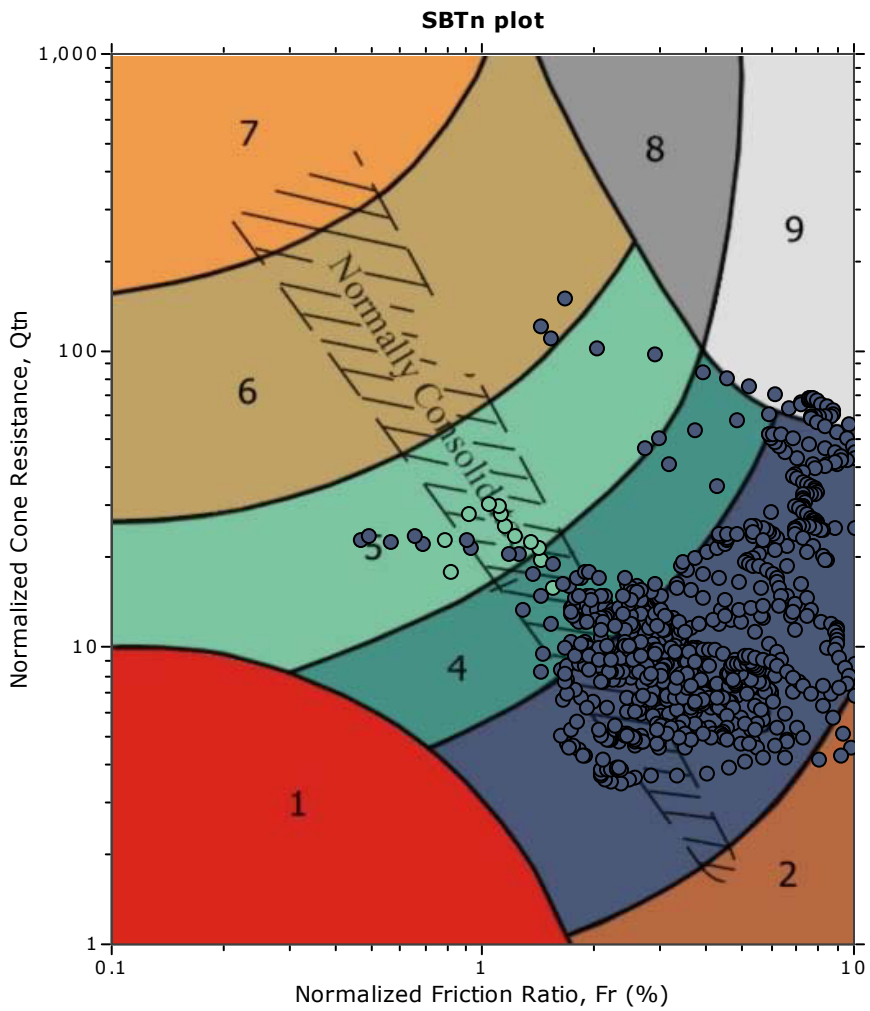
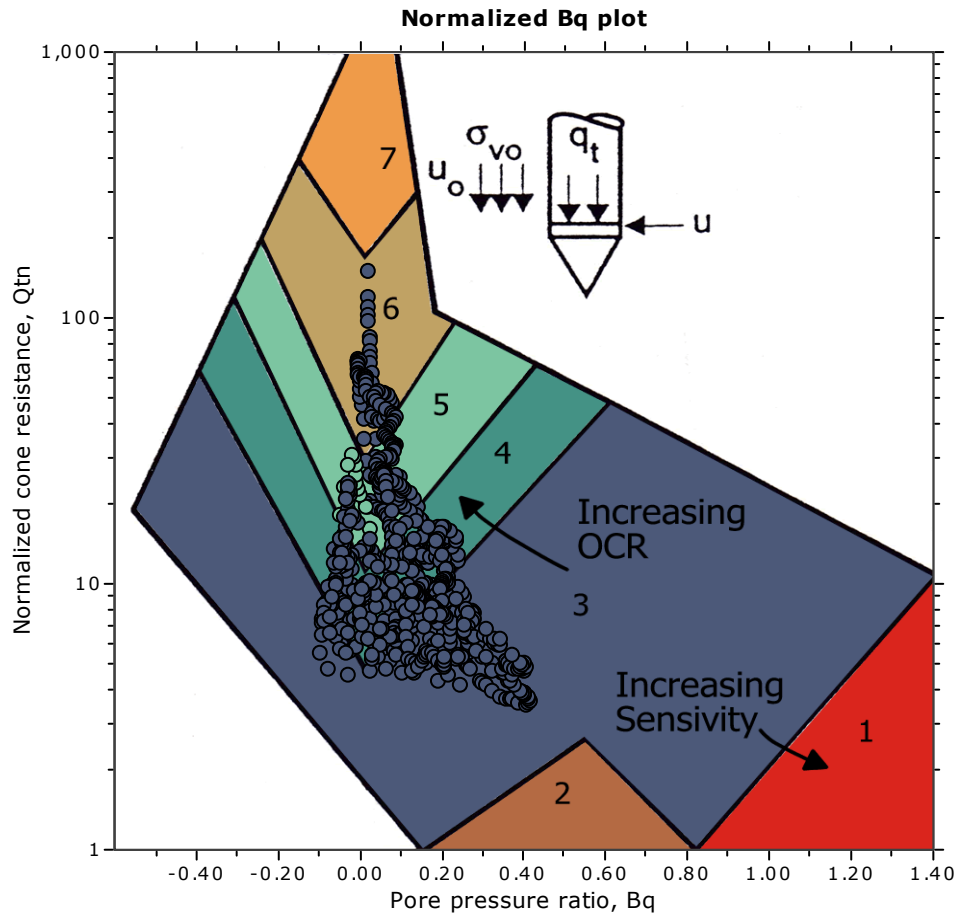
Project:
Location:

CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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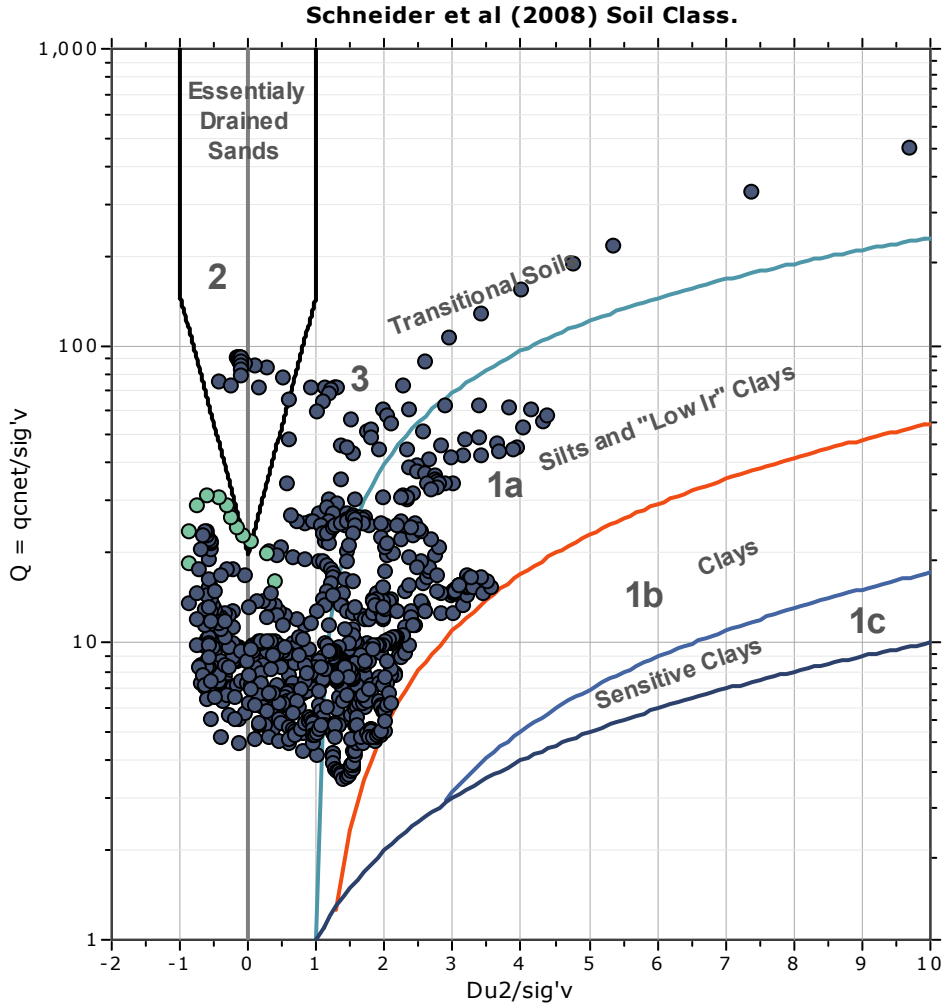
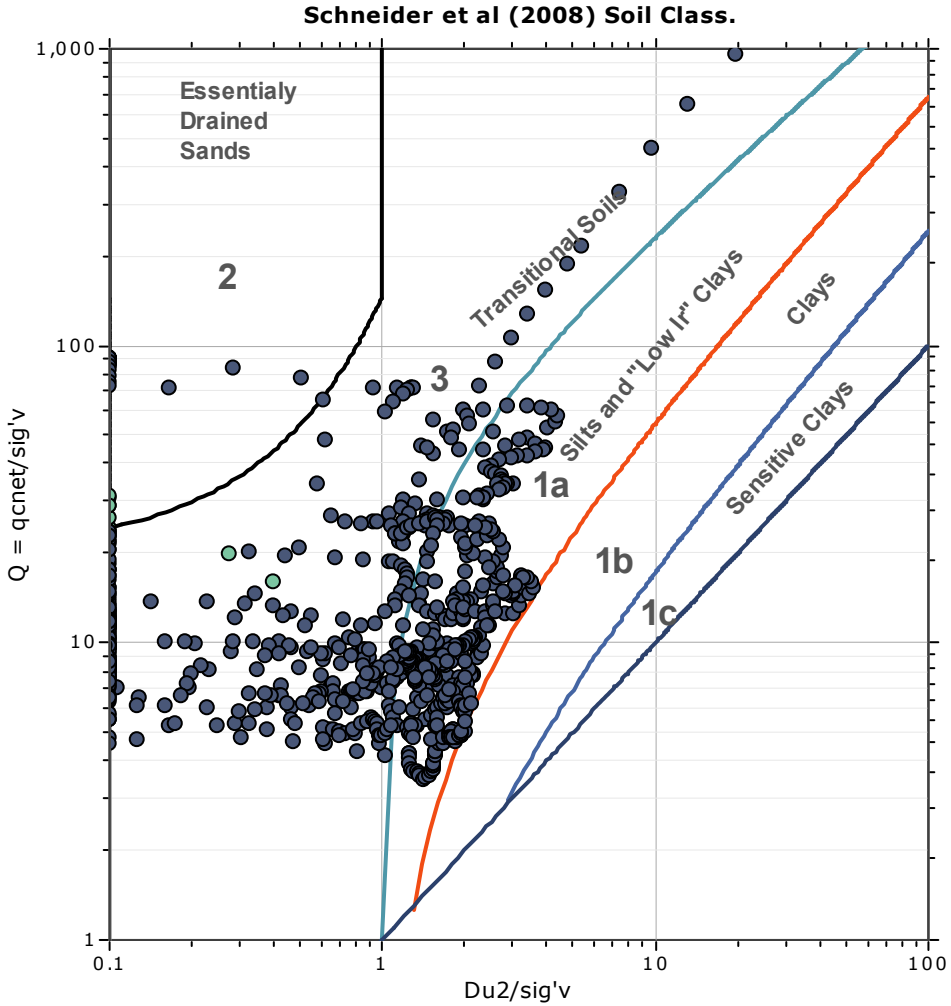
Project:
Location:

CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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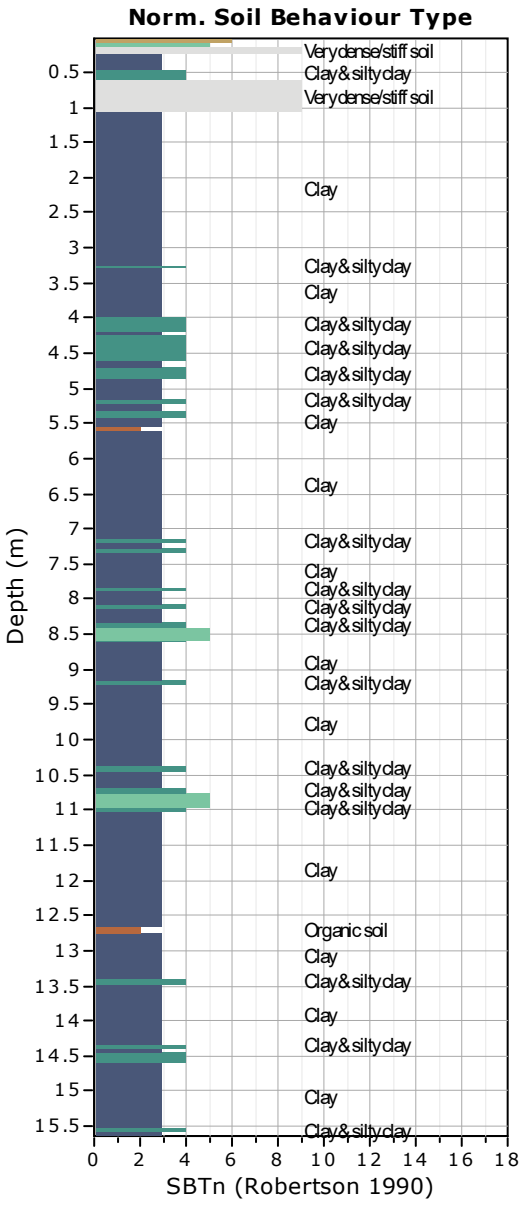
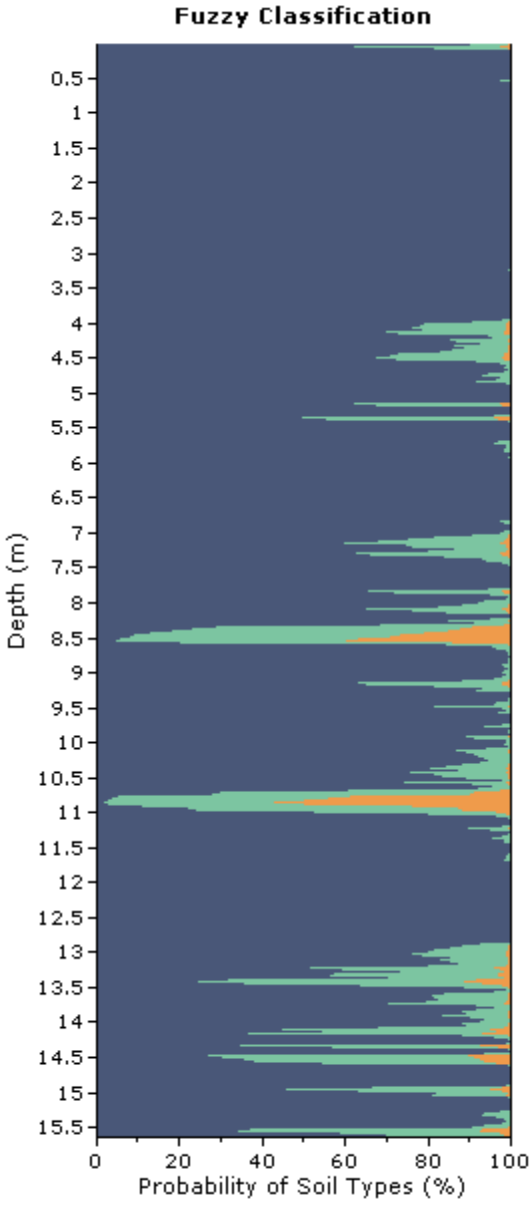
CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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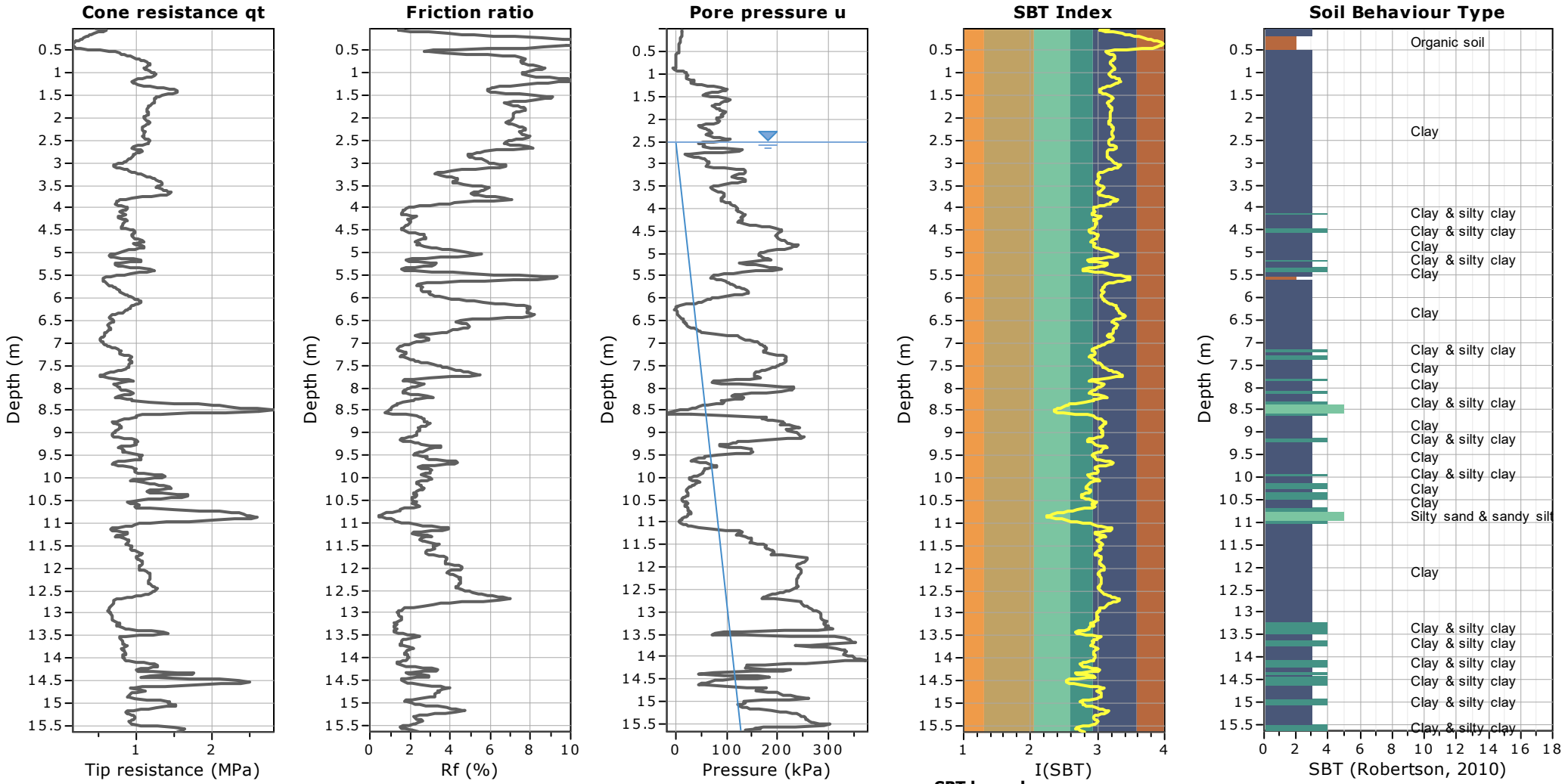
Project:
Location:

CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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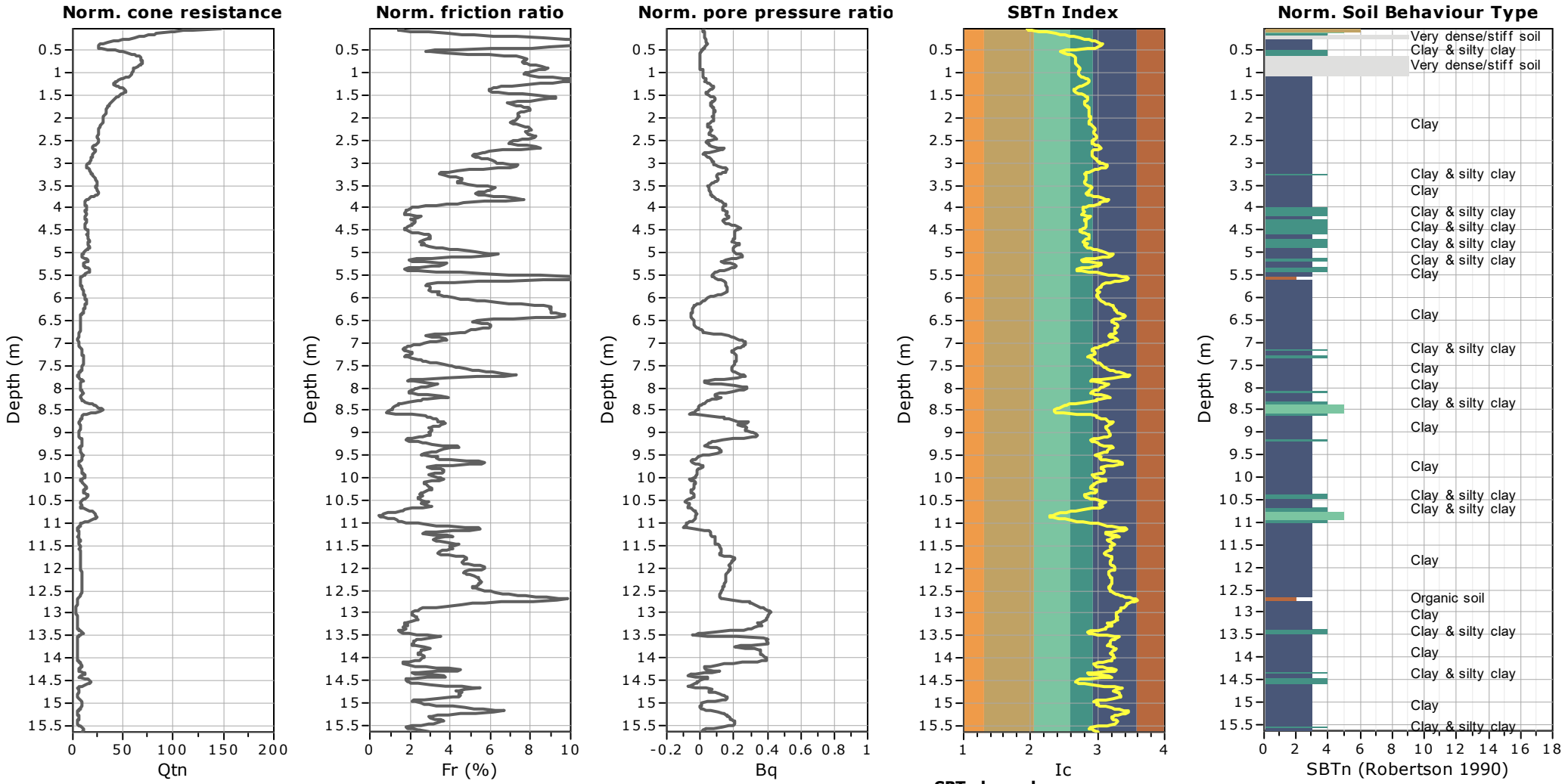
Project:
Location:

CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
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4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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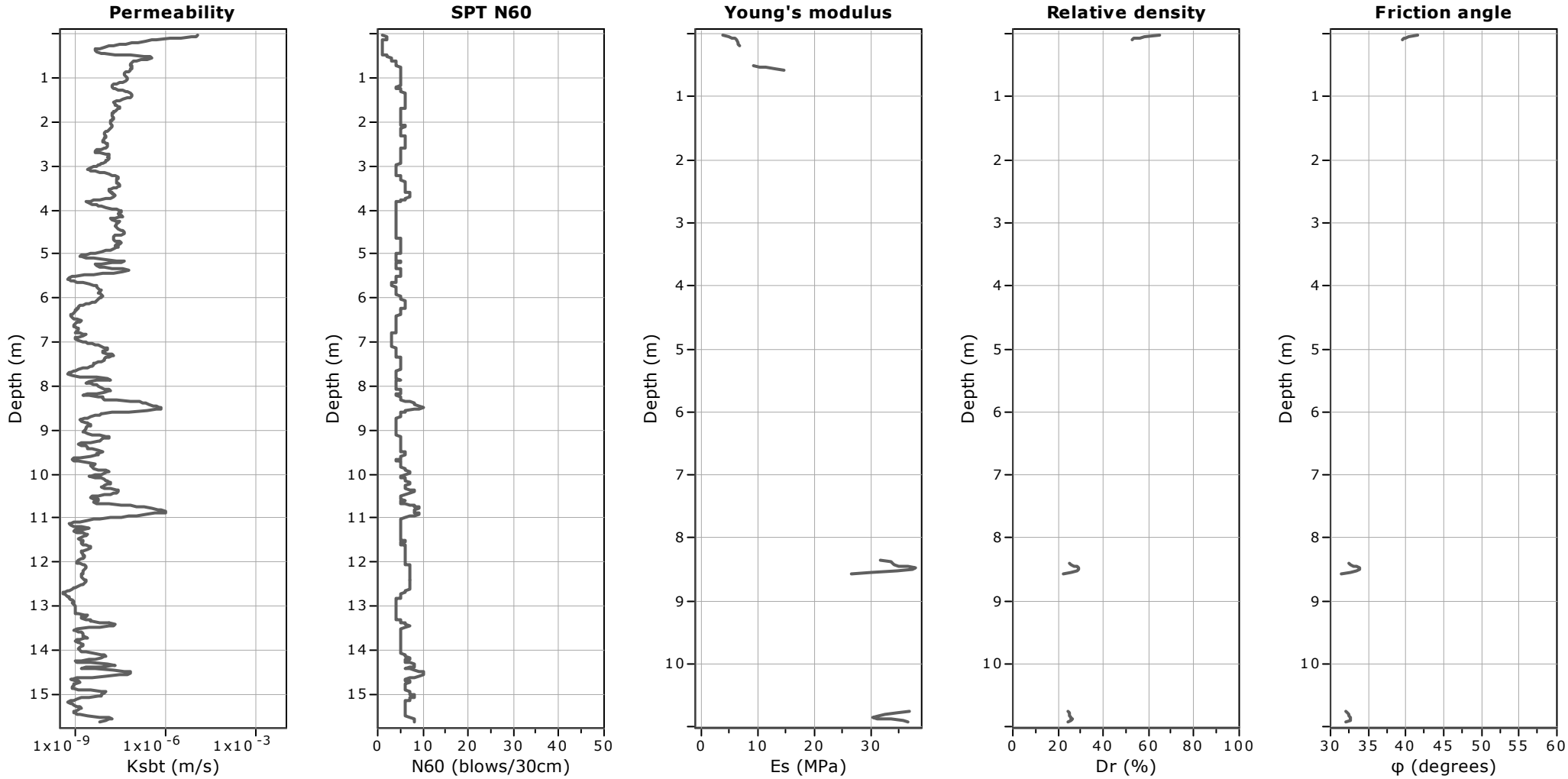
Project:
Location:

CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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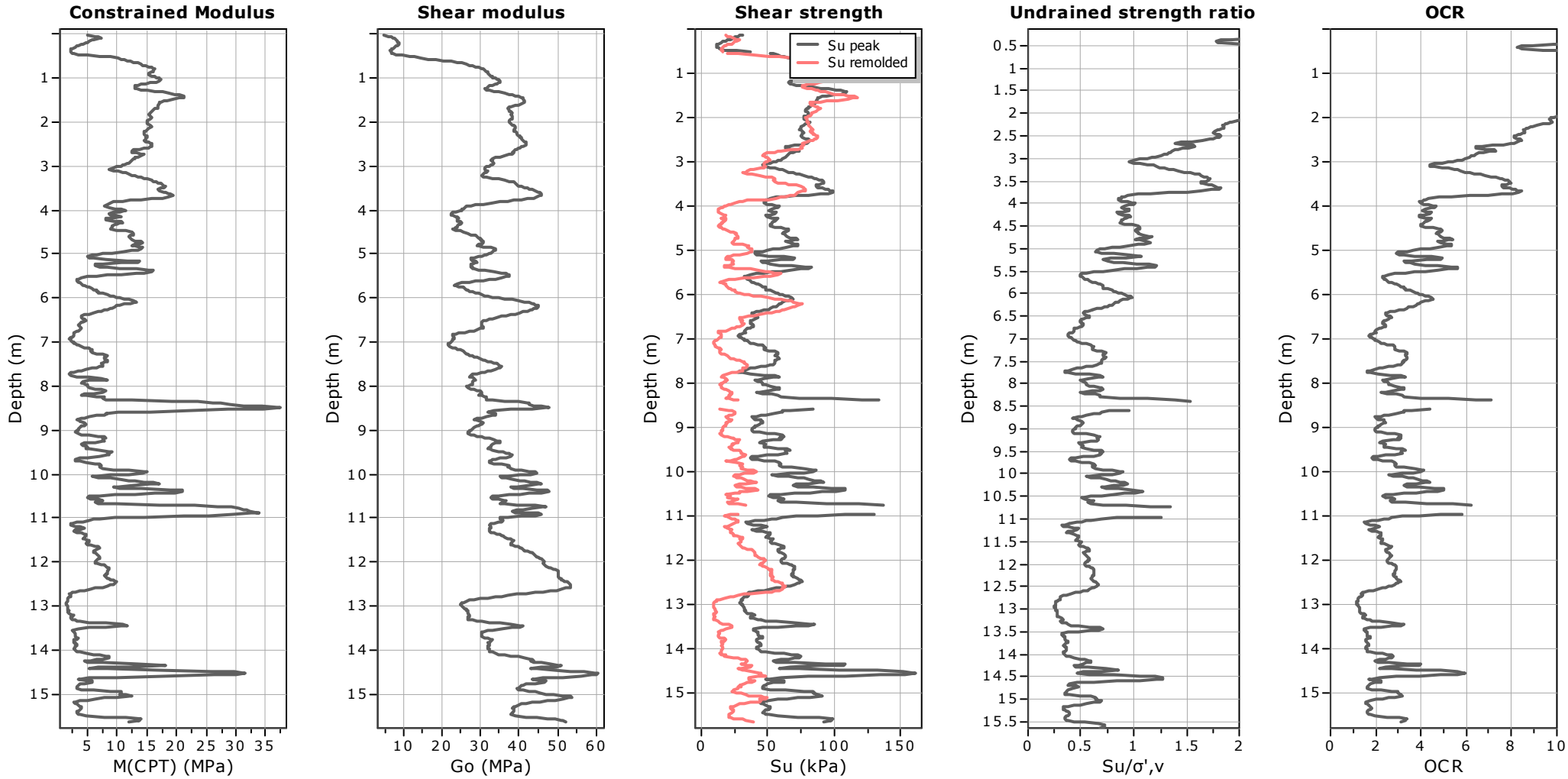
Project:
Location:

CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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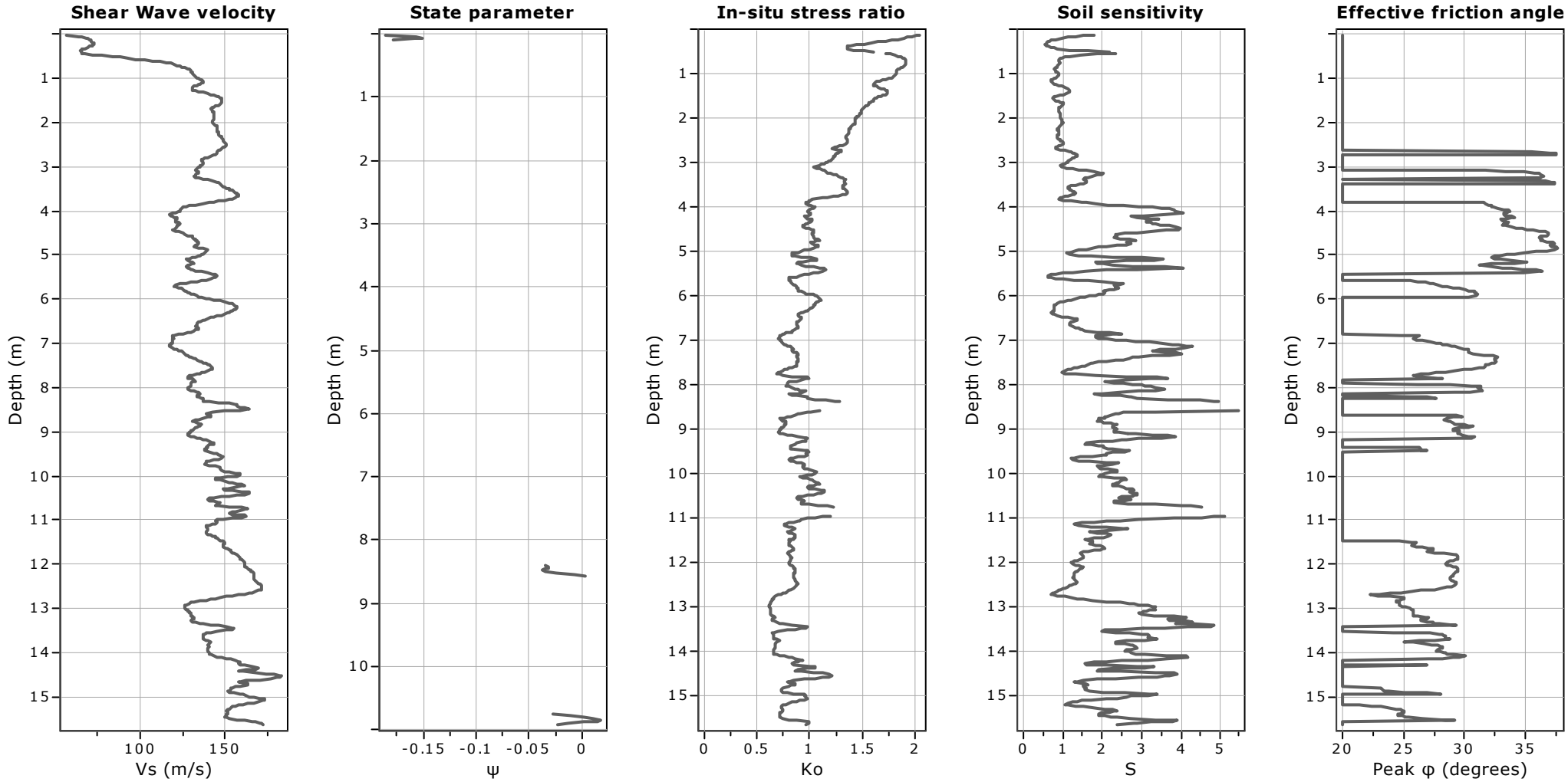
Project:
Location:

CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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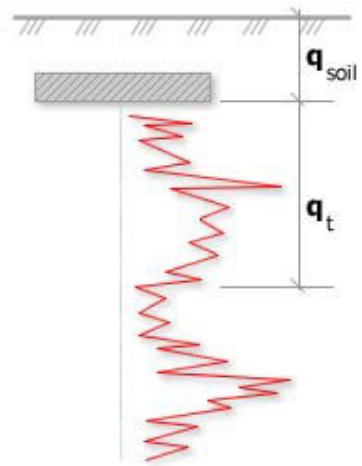
CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

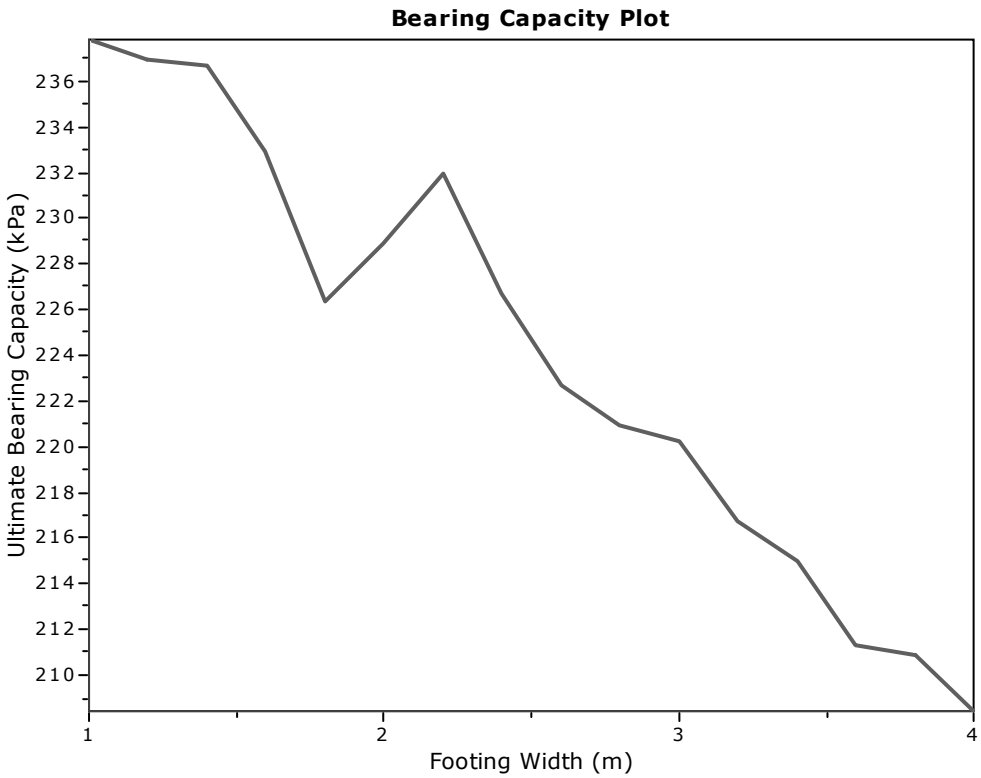
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.14	0.20	9.50	237.83
2	1.20	0.50	2.30	1.14	0.20	9.50	236.92
3	1.40	0.50	2.60	1.14	0.20	9.50	236.73
4	1.60	0.50	2.90	1.12	0.20	9.50	232.92
5	1.80	0.50	3.20	1.08	0.20	9.50	226.35
6	2.00	0.50	3.50	1.10	0.20	9.50	228.86
7	2.20	0.50	3.80	1.11	0.20	9.50	231.98
8	2.40	0.50	4.10	1.09	0.20	9.50	226.71
9	2.60	0.50	4.40	1.07	0.20	9.50	222.73
10	2.80	0.50	4.70	1.06	0.20	9.50	220.93
11	3.00	0.50	5.00	1.05	0.20	9.50	220.23
12	3.20	0.50	5.30	1.04	0.20	9.50	216.78
13	3.40	0.50	5.60	1.03	0.20	9.50	214.99
14	3.60	0.50	5.90	1.01	0.20	9.50	211.29
15	3.80	0.50	6.20	1.01	0.20	9.50	210.90
16	4.00	0.50	6.50	0.99	0.20	9.50	208.42

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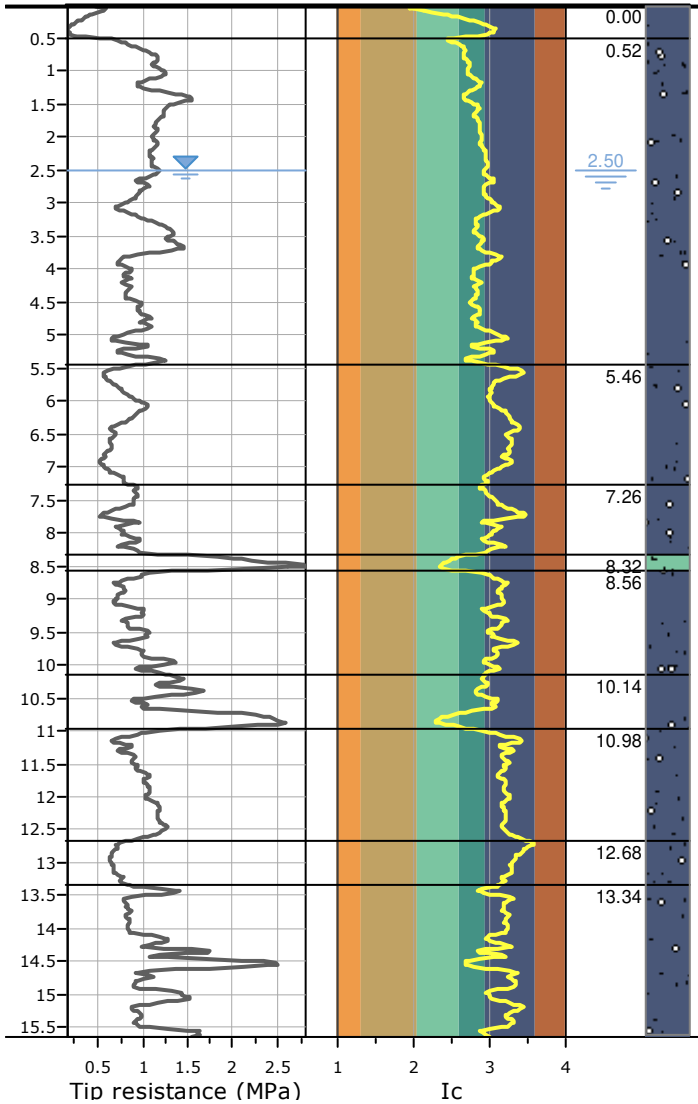
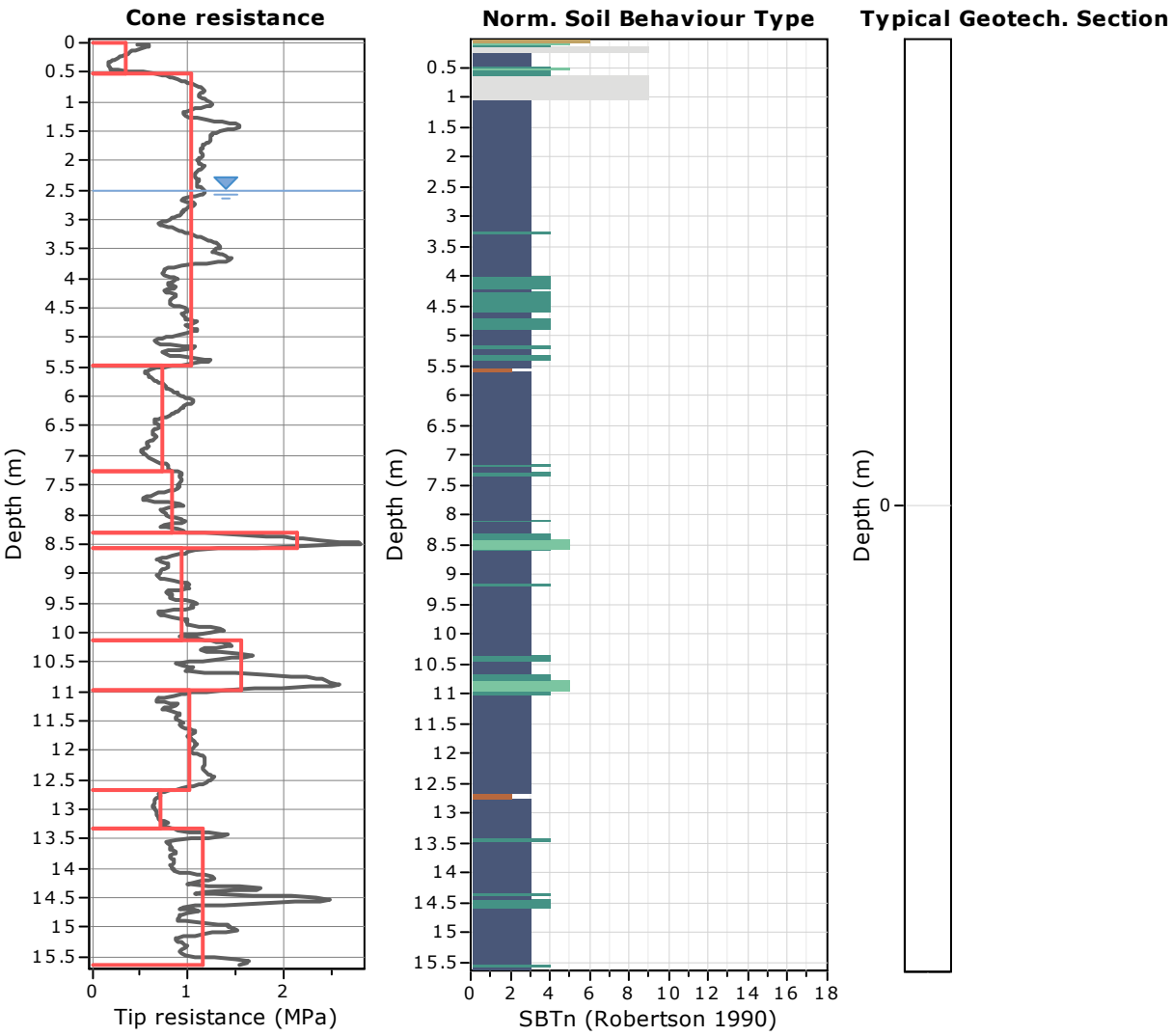
CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:

Depth (m) Elevation: 0.00 (m)



Depth (m)	Description	qt (MPa)	Ksbt (m/s)	N60	Es (MPa)	Dr	Phi (°)	M (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
0.00	Clay	0.3	1.33E-6	1.3	7.1	-	-	4.5	8.0	19.5	3.3	15.3	15.8
0.52	Clay	1.0	2.68E-8	4.9	13.1	-	-	13.6	33.4	70.7	1.9	9.0	17.5
5.46	Clay	0.7	3.25E-9	4.2	-	-	-	5.7	30.8	44.1	0.6	2.9	16.7
7.26	Clay	0.8	6.61E-9	4.5	-	-	-	6.2	30.0	49.8	0.6	2.8	16.4
8.32	Silty sand & sandy silt	2.2	3.36E-7	7.9	34.1	26.8	33.0	28.0	41.2	-	-	-	16.9
8.56	Clay	0.9	8.14E-9	5.0	-	-	-	6.8	33.6	54.3	0.6	2.7	16.6
10.14	Clay	1.6	1.33E-7	6.8	-	-	-	17.3	40.6	82.5	0.8	3.8	16.8
10.98	Clay	1.0	2.23E-9	6.0	-	-	-	6.4	42.8	58.8	0.5	2.5	17.1
12.68	Clay	0.7	1.10E-9	4.4	-	-	-	2.0	29.5	34.4	0.3	1.4	15.9
13.34	Clay	1.2	6.55E-9	6.4	-	-	-	7.3	41.1	64.8	0.5	2.4	16.7



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.52 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.34 ±0.16 MPa	Permeability: 1.33E-06 ±3.08E-06 m/s	Constrained Mod.: 4.54 ±1.97 MPa
Sleeve friction: 18.14 ±5.78 kPa	N60: 1.31 ±0.47 blows	Go: 7.96 ±1.60 MPa
SBT_n: 3	Es: 7.09 ±1.15 MPa	Su: 19.55 ±7.76 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 3.31 ±1.44
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 15.30 ±6.67
	Unit weight: 15.81 ±0.35 kN/m³	

.:: Layer No: 2 ::.

Code: A1 **Start depth:** 0.52 (m), **End depth:** 5.46 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.04 ±0.20 MPa	Permeability: 2.68E-08 ±3.54E-08 m/s	Constrained Mod.: 13.56 ±3.35 MPa
Sleeve friction: 57.73 ±29.49 kPa	N60: 4.90 ±0.84 blows	Go: 33.36 ±6.35 MPa
SBT_n: 3	Es: 13.07 ±1.60 MPa	Su: 70.67 ±14.87 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.95 ±1.18
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 8.99 ±5.44
	Unit weight: 17.46 ±0.78 kN/m³	

.:: Layer No: 3 ::.

Code: D1 **Start depth:** 5.46 (m), **End depth:** 7.26 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.73 ±0.15 MPa	Permeability: 3.25E-09 ±2.99E-09 m/s	Constrained Mod.: 5.68 ±2.93 MPa
Sleeve friction: 33.06 ±19.74 kPa	N60: 4.16 ±0.89 blows	Go: 30.85 ±7.08 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 44.11 ±10.71 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.62 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.86 ±0.76
	Unit weight: 16.67 ±0.75 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 7.26 (m), **End depth:** 8.32 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.83 ±0.13 MPa	Permeability: 6.61E-09 ±5.19E-09 m/s	Constrained Mod.: 6.18 ±2.14 MPa
Sleeve friction: 21.86 ±6.61 kPa	N60: 4.46 ±0.50 blows	Go: 30.02 ±2.57 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 49.77 ±9.34 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.61 ±0.12
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.83 ±0.54
	Unit weight: 16.41 ±0.31 kN/m³	

.:: Layer No: 5 ::.

Code: B1 **Start depth:** 8.32 (m), **End depth:** 8.56 (m)

Description: Silty sand & sandy silt

Basic results	Estimation results	
Total cone resistance: 2.15 ±0.50 MPa	Permeability: 3.36E-07 ±2.22E-07 m/s	Constrained Mod.: 28.01 ±7.34 MPa
Sleeve friction: 23.49 ±5.96 kPa	N60: 7.92 ±1.55 blows	Go: 41.19 ±4.78 MPa
SBT_n: 5	Es: 34.06 ±3.60 MPa	Su: 0.00 ±0.00 kPa
SBTn description: Silty sand & sandy silt	Dr (%): 26.83 ±2.18	Su ratio: 0.00 ±0.00
	ö (degrees): 32.99 ±0.80 °	O.C.R.: 0.00 ±0.00
	Unit weight: 16.88 ±0.33 kN/m³	

.:: Layer No: 6 ::.

Code: A3 **Start depth:** 8.56 (m), **End depth:** 10.14 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.93 ±0.20 MPa	Permeability: 8.14E-09 ±2.70E-08 m/s	Constrained Mod.: 6.77 ±3.46 MPa
Sleeve friction: 24.13 ±6.40 kPa	N60: 4.97 ±0.80 blows	Go: 33.59 ±4.22 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 54.26 ±12.53 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.59 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.72 ±0.59
	Unit weight: 16.58 ±0.34 kN/m³	

.:: Layer No: 7 ::.

Code: B2 **Start depth:** 10.14 (m), **End depth:** 10.98 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.57 ±0.54 MPa	Permeability: 1.33E-07 ±2.58E-07 m/s	Constrained Mod.: 17.34 ±9.23 MPa
Sleeve friction: 25.93 ±8.17 kPa	N60: 6.79 ±1.30 blows	Go: 40.60 ±4.29 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 82.50 ±22.02 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 0.83 ±0.22
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.82 ±1.00
	Unit weight: 16.83 ±0.34 kN/m³	

.:: Layer No: 8 ::.

Code: A4 **Start depth:** 10.98 (m), **End depth:** 12.68 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.02 ±0.16 MPa	Permeability: 2.23E-09 ±3.61E-09 m/s	Constrained Mod.: 6.38 ±2.20 MPa
Sleeve friction: 39.08 ±13.95 kPa	N60: 6.00 ±0.81 blows	Go: 42.84 ±7.03 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 58.75 ±11.04 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.54 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.48 ±0.43
	Unit weight: 17.13 ±0.48 kN/m³	

.:: Layer No: 9 ::.

Code: D3 **Start depth:** 12.68 (m), **End depth:** 13.34 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.70 ±0.06 MPa	Permeability: 1.10E-09 ±7.02E-10 m/s	Constrained Mod.: 2.00 ±0.48 MPa
Sleeve friction: 16.76 ±13.22 kPa	N60: 4.35 ±0.60 blows	Go: 29.48 ±5.82 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 34.42 ±4.04 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.29 ±0.03
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.35 ±0.15
	Unit weight: 15.87 ±0.66 kN/m³	

.:: Layer No: 10 ::.

Code: A5 **Start depth:** 13.34 (m), **End depth:** 15.64 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.15 ±0.38 MPa	Permeability: 6.55E-09 ±1.21E-08 m/s	Constrained Mod.: 7.29 ±6.45 MPa
Sleeve friction: 26.17 ±10.28 kPa	N60: 6.36 ±1.29 blows	Go: 41.10 ±7.80 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 64.76 ±27.08 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.51 ±0.21
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.35 ±0.98
	Unit weight: 16.69 ±0.53 kN/m³	

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Project:
Location:

CPT: CPTu-04
Total depth: 15.64 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.52	1.33E-06	1.3	7.1	0.0	0.0	4.5	8.0	19.5	3.3	15.3	15.8
0.52		(±3.08E-06)	(±0.5)	(±1.2)	(±0.0)	(±0.0)	(±2.0)	(±1.6)	(±7.8)	(±1.4)	(±6.7)	(±0.4)
0.52	4.94	2.68E-08	4.9	13.1	0.0	0.0	13.6	33.4	70.7	1.9	9.0	17.5
5.46		(±3.54E-08)	(±0.8)	(±1.6)	(±0.0)	(±0.0)	(±3.4)	(±6.3)	(±14.9)	(±1.2)	(±5.4)	(±0.8)
5.46	1.80	3.25E-09	4.2	0.0	0.0	0.0	5.7	30.8	44.1	0.6	2.9	16.7
7.26		(±2.99E-09)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±2.9)	(±7.1)	(±10.7)	(±0.2)	(±0.8)	(±0.8)
7.26	1.06	6.61E-09	4.5	0.0	0.0	0.0	6.2	30.0	49.8	0.6	2.8	16.4
8.32		(±5.19E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±2.1)	(±2.6)	(±9.3)	(±0.1)	(±0.5)	(±0.3)
8.32	0.24	3.36E-07	7.9	34.1	26.8	33.0	28.0	41.2	0.0	0.0	0.0	16.9
8.56		(±2.22E-07)	(±1.6)	(±3.6)	(±2.2)	(±0.8)	(±7.3)	(±4.8)	(±0.0)	(±0.0)	(±0.0)	(±0.3)
8.56	1.58	8.14E-09	5.0	0.0	0.0	0.0	6.8	33.6	54.3	0.6	2.7	16.6
10.14		(±2.70E-08)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±3.5)	(±4.2)	(±12.5)	(±0.1)	(±0.6)	(±0.3)
10.14	0.84	1.33E-07	6.8	0.0	0.0	0.0	17.3	40.6	82.5	0.8	3.8	16.8
10.98		(±2.58E-07)	(±1.3)	(±0.0)	(±0.0)	(±0.0)	(±9.2)	(±4.3)	(±22.0)	(±0.2)	(±1.0)	(±0.3)
10.98	1.70	2.23E-09	6.0	0.0	0.0	0.0	6.4	42.8	58.8	0.5	2.5	17.1
12.68		(±3.61E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±7.0)	(±11.0)	(±0.1)	(±0.4)	(±0.5)
12.68	0.66	1.10E-09	4.4	0.0	0.0	0.0	2.0	29.5	34.4	0.3	1.4	15.9
13.34		(±7.02E-10)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±0.5)	(±5.8)	(±4.0)	(±0.0)	(±0.2)	(±0.7)
13.34	2.30	6.55E-09	6.4	0.0	0.0	0.0	7.3	41.1	64.8	0.5	2.4	16.7
15.64		(±1.21E-08)	(±1.3)	(±0.0)	(±0.0)	(±0.0)	(±6.5)	(±7.8)	(±27.1)	(±0.2)	(±1.0)	(±0.5)

Depth values presented in this table are measured from free ground surface

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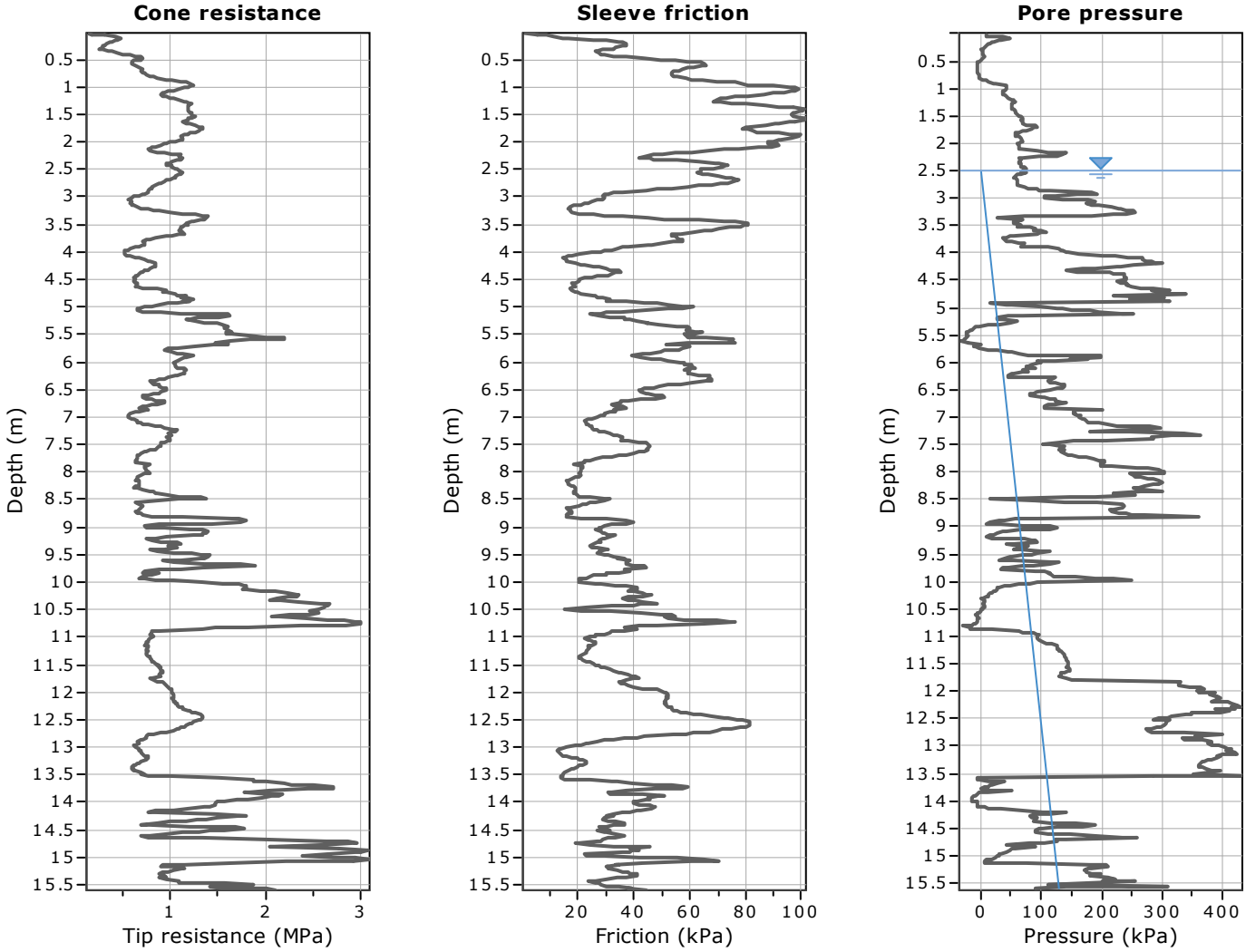
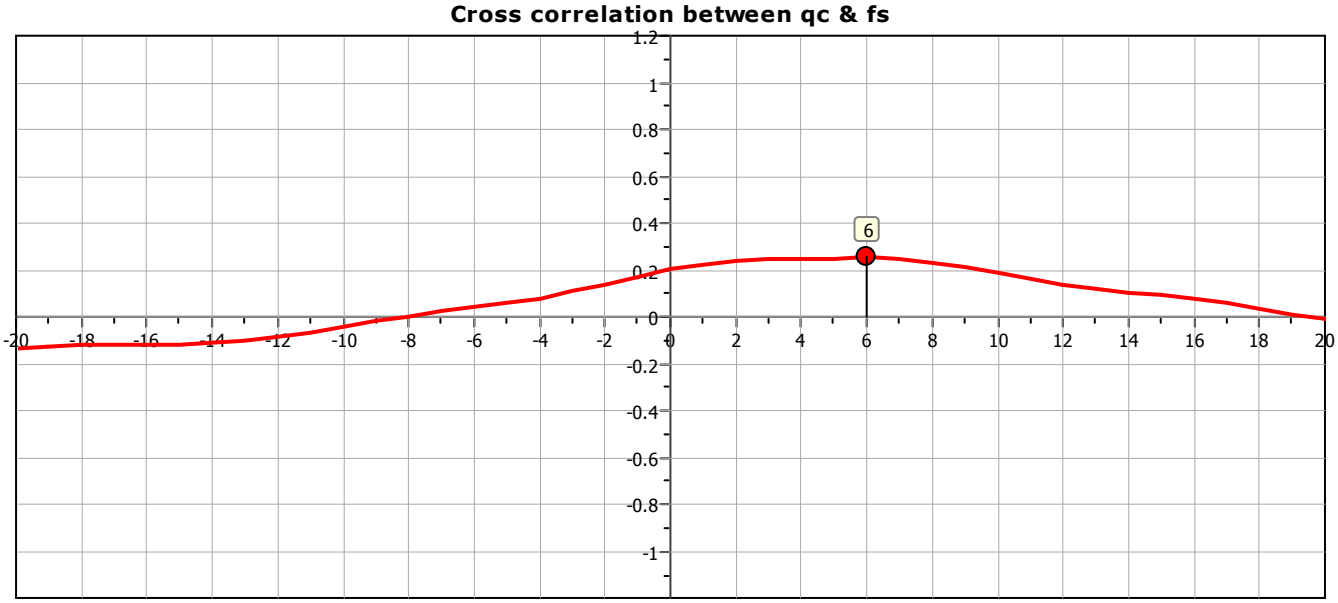
CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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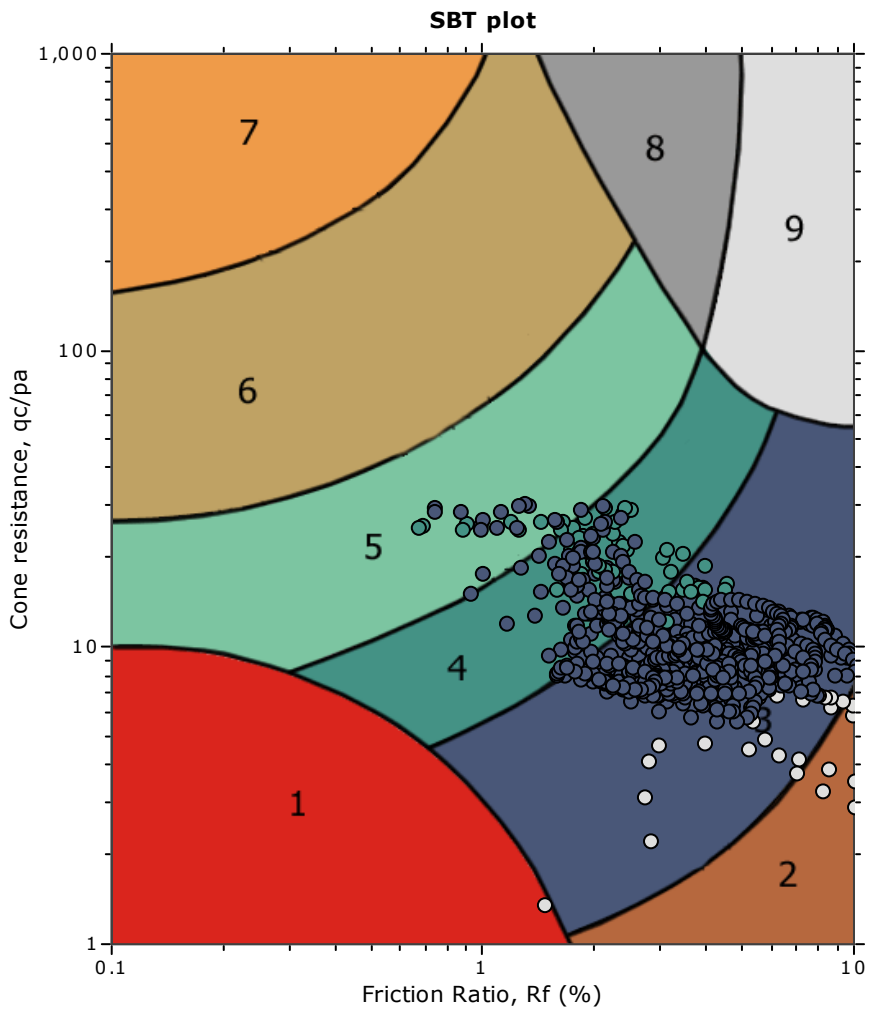
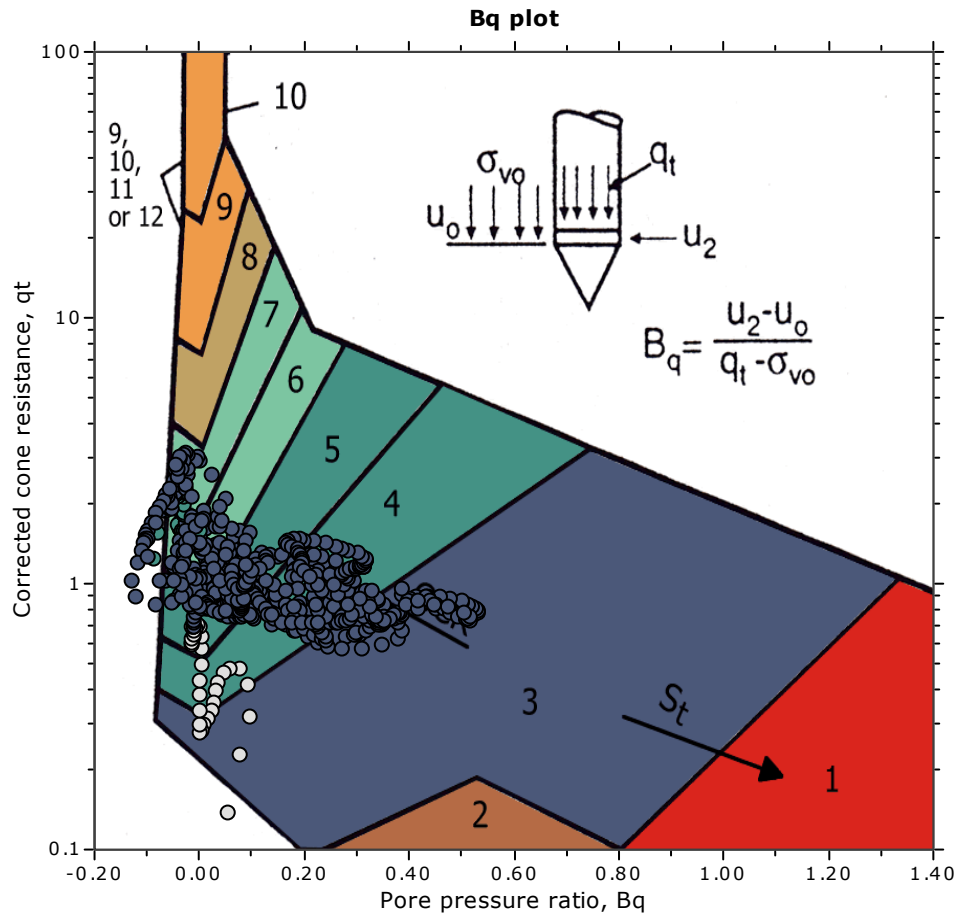
Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots





SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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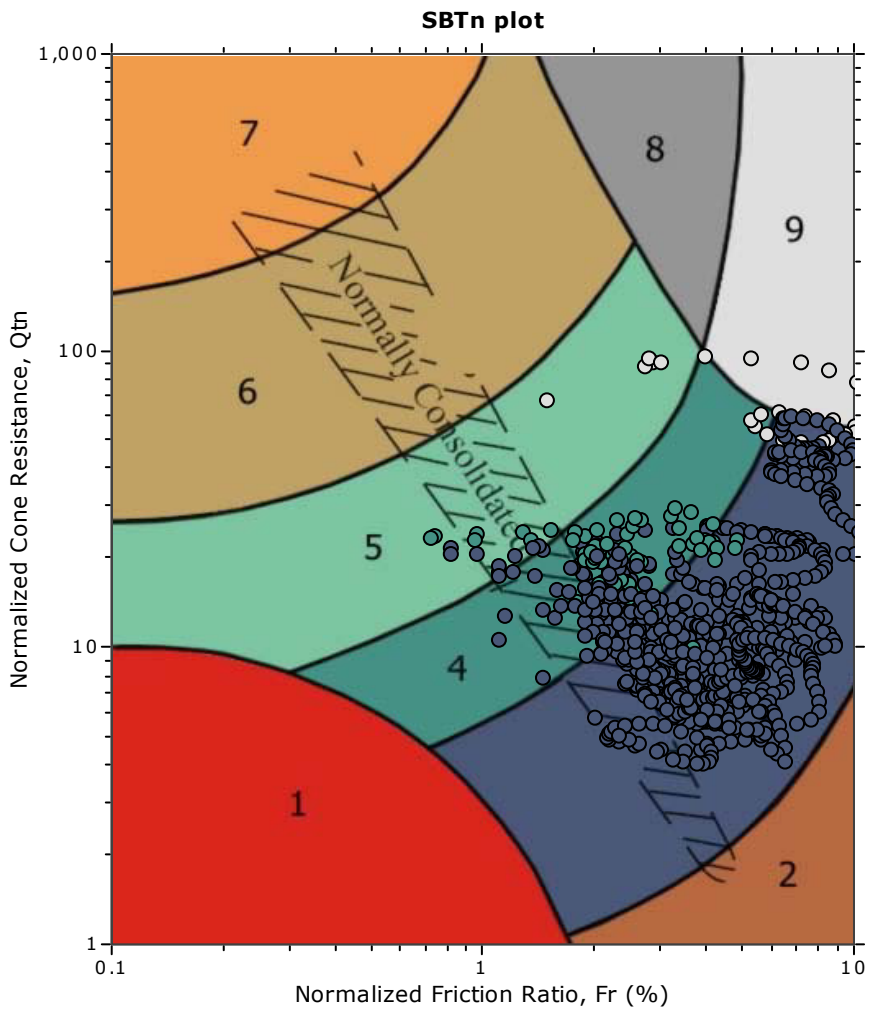
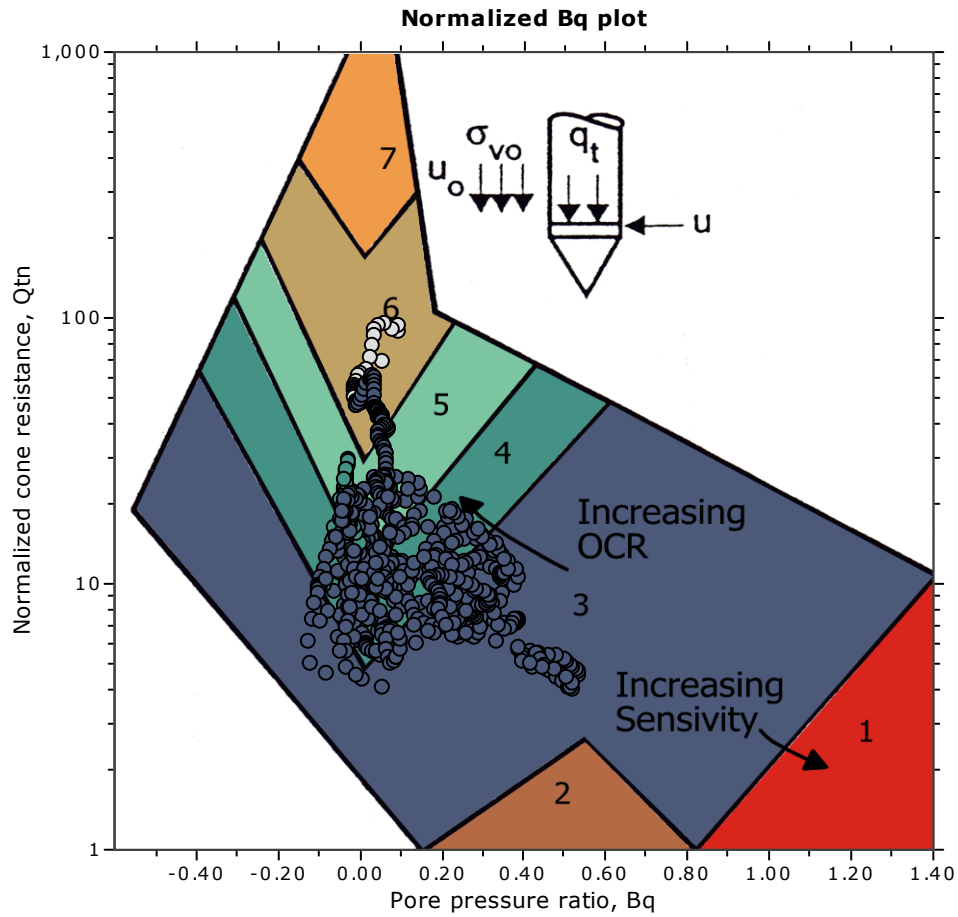
Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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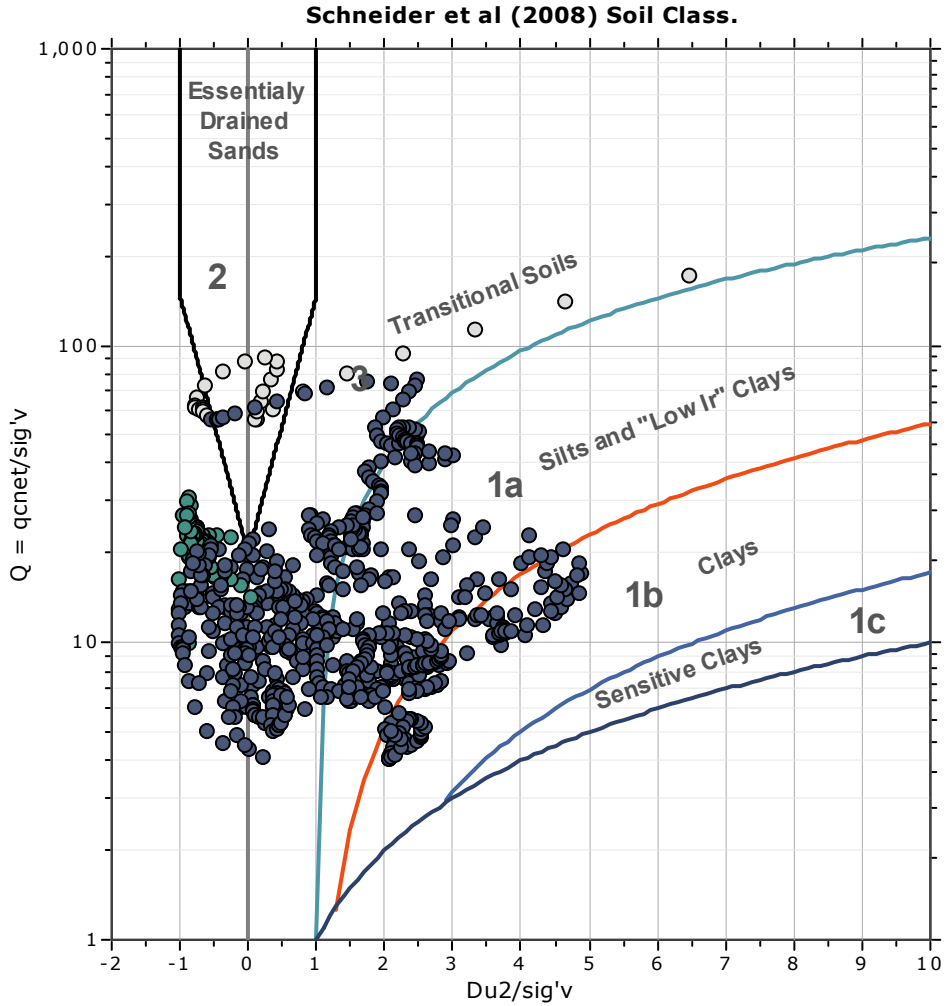
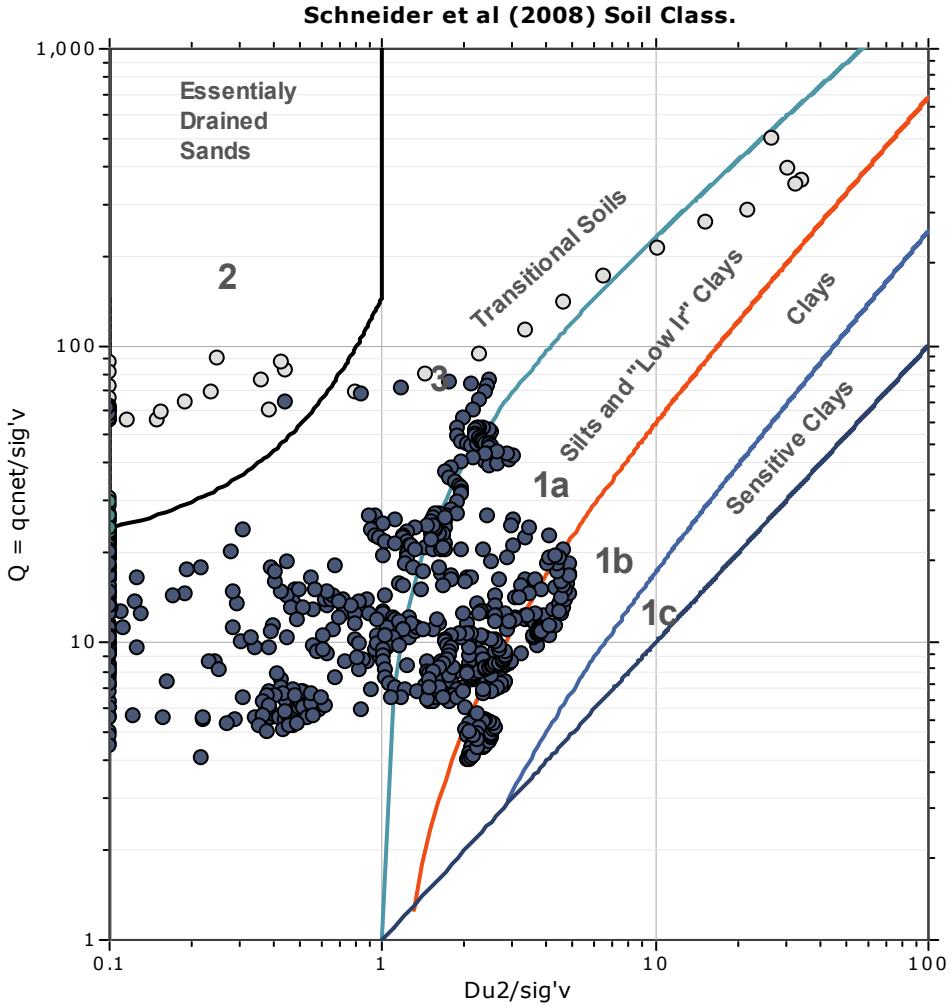
Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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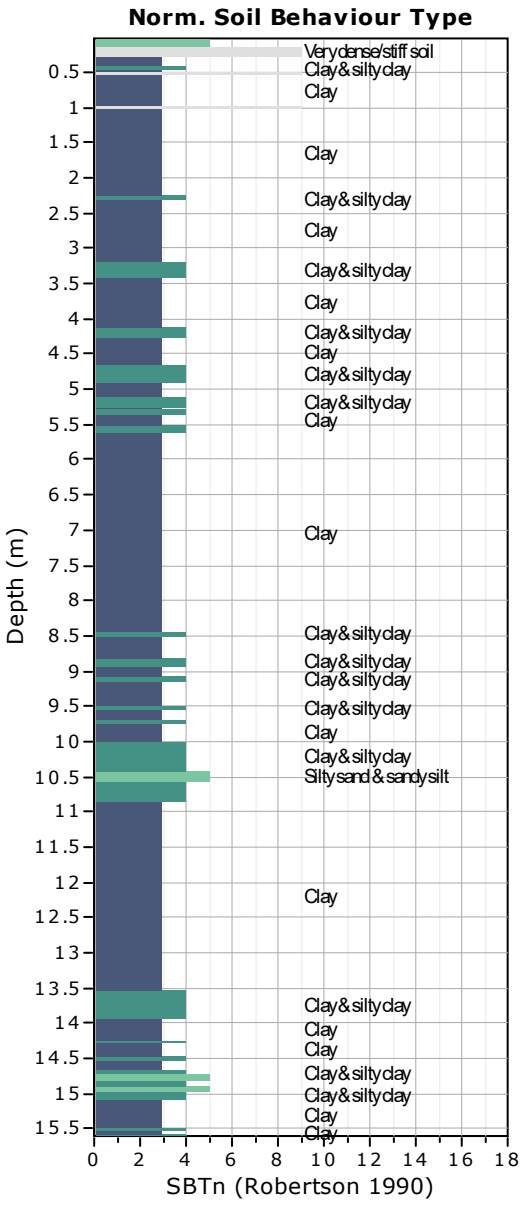
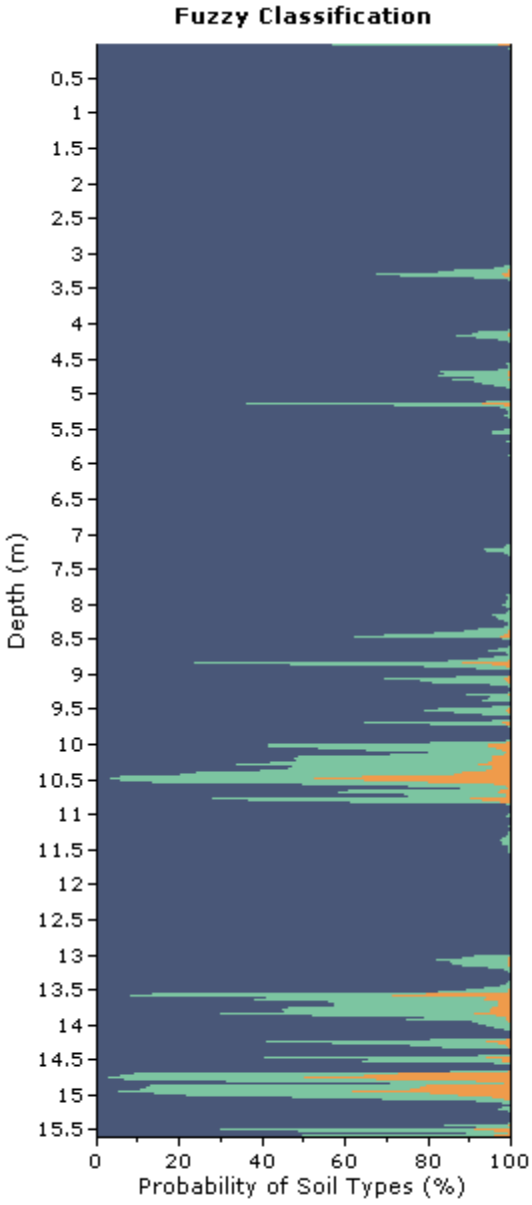
CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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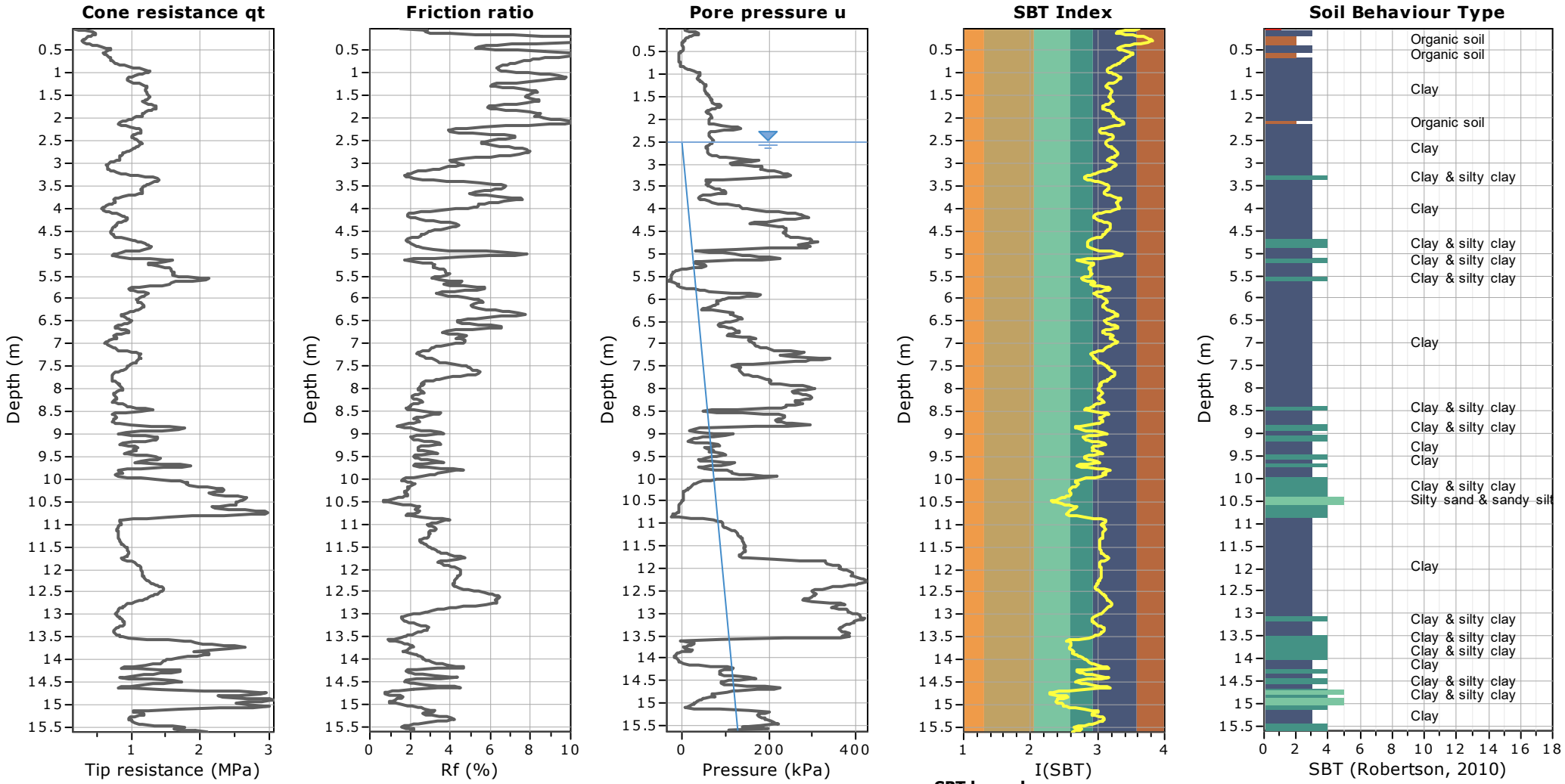
Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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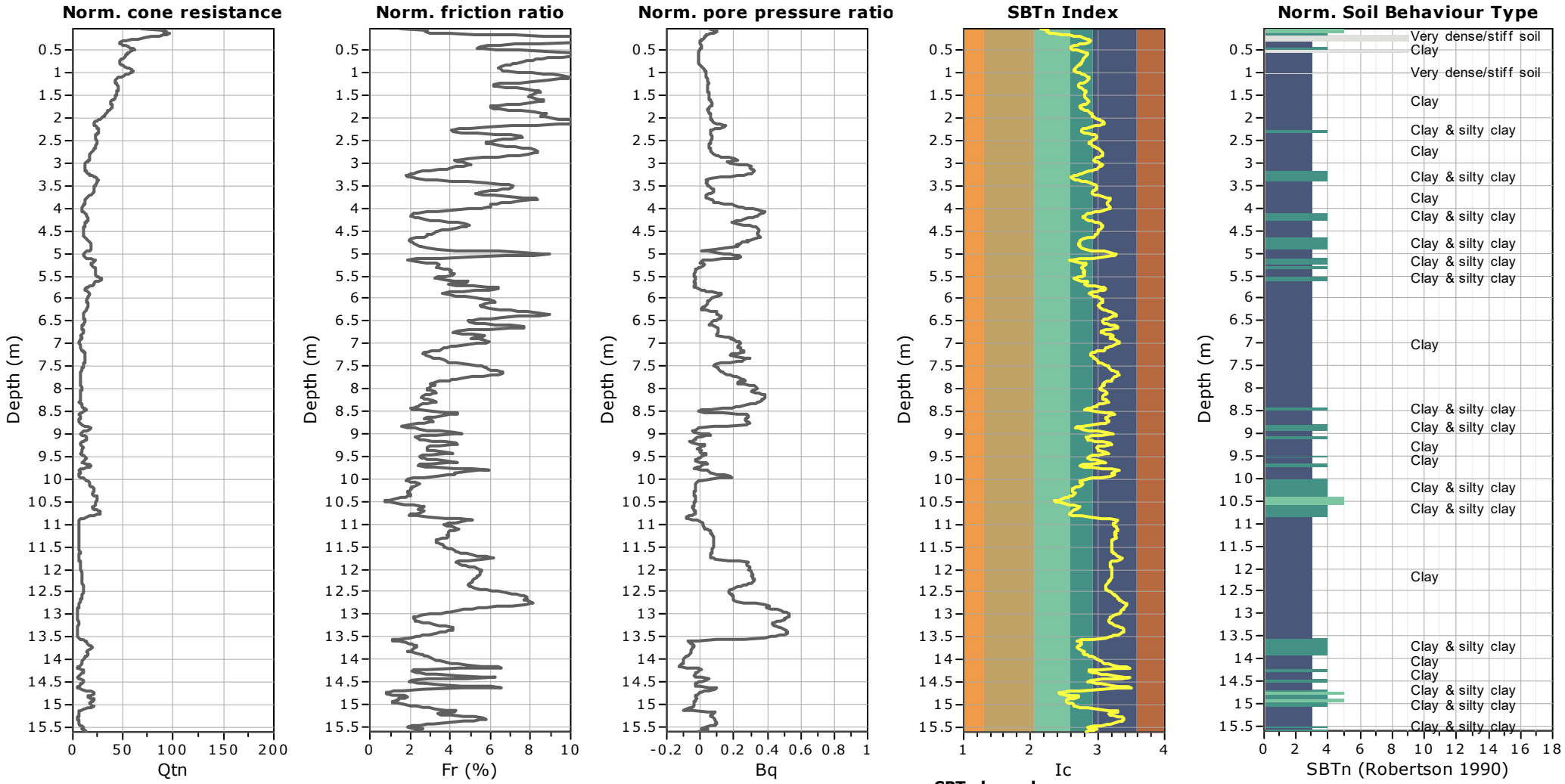
Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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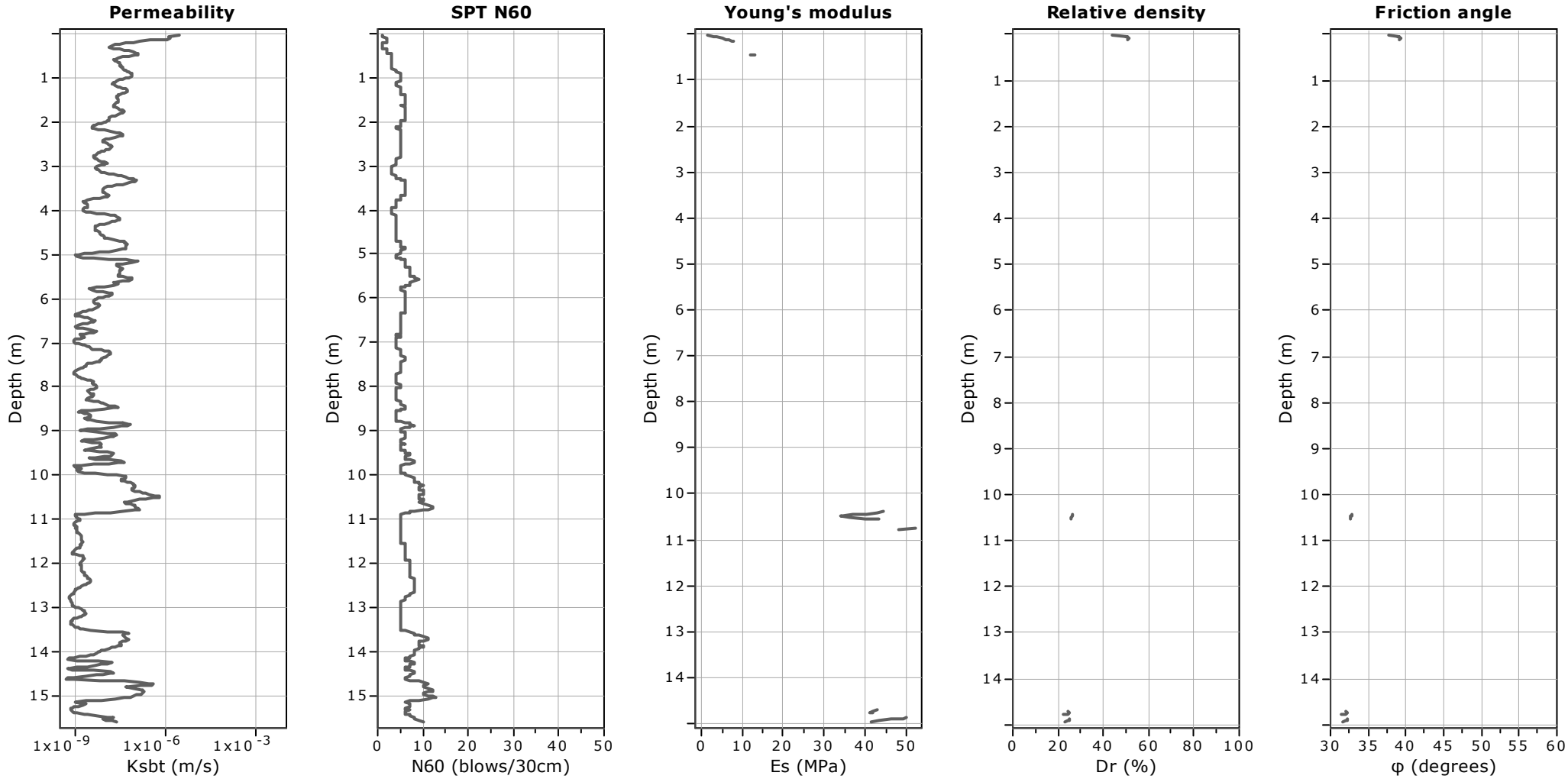
Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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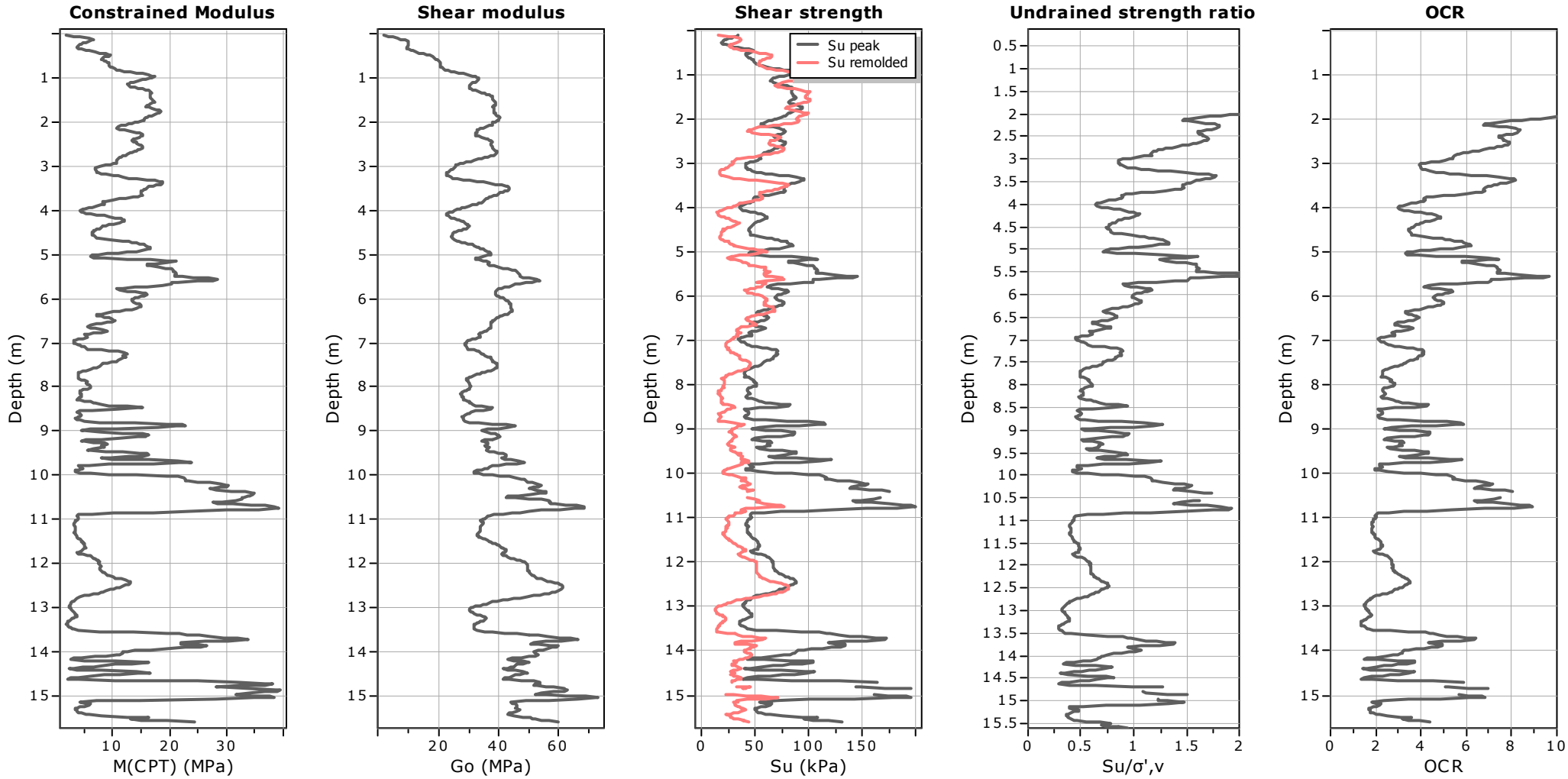
Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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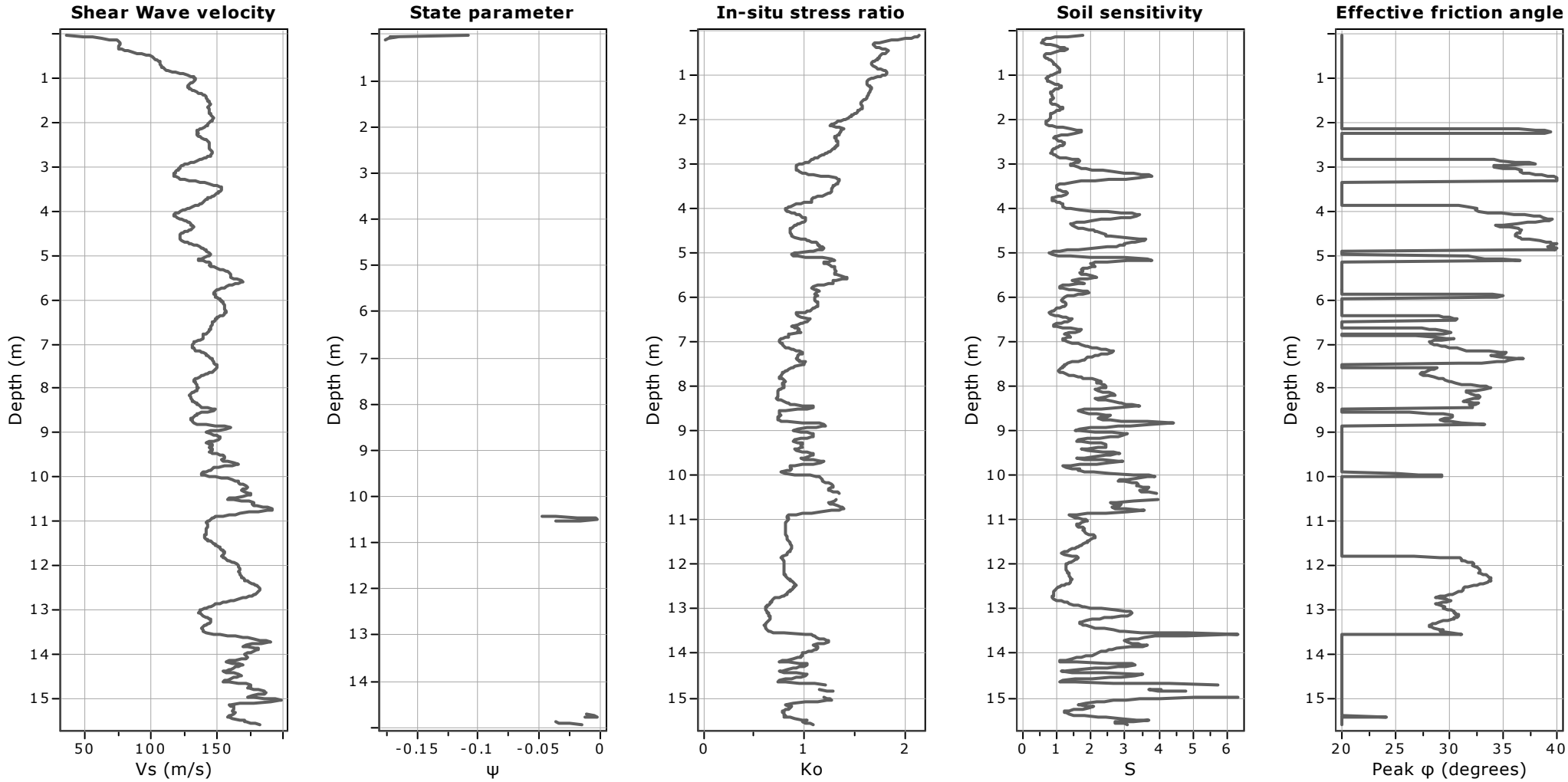
Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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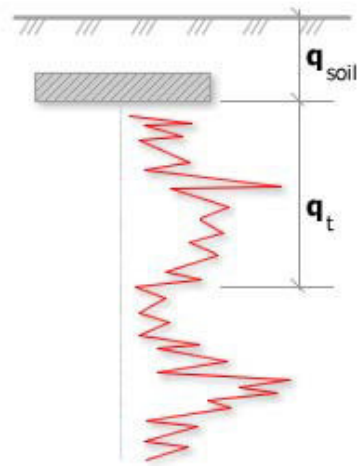
CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

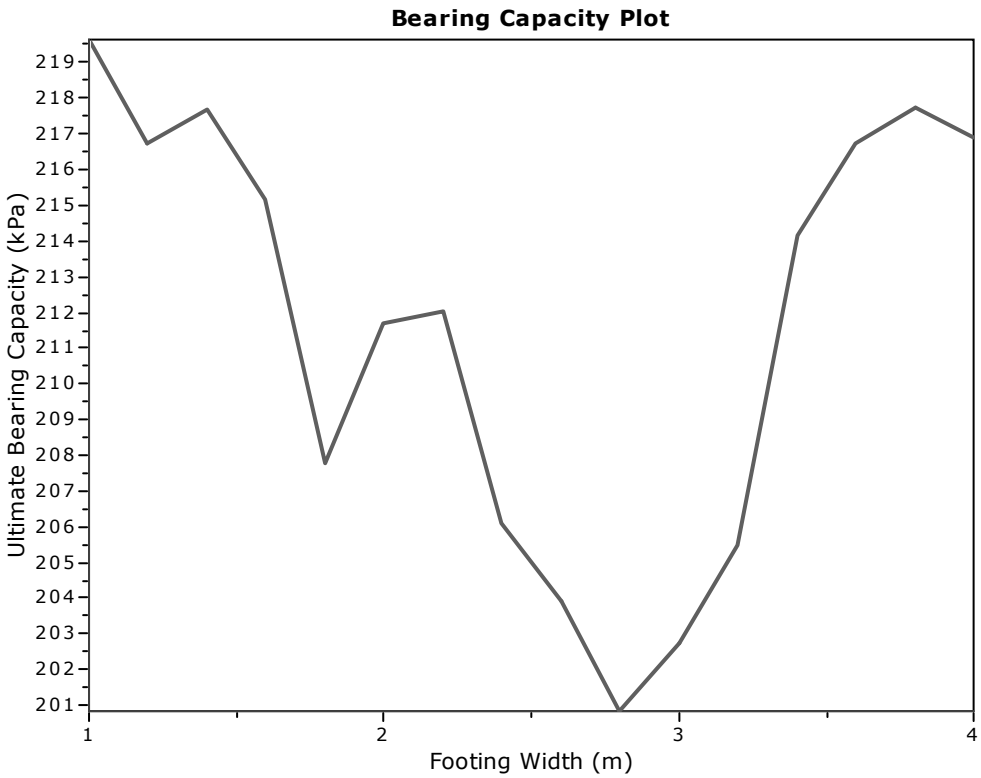
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.05	0.20	9.50	219.64
2	1.20	0.50	2.30	1.04	0.20	9.50	216.74
3	1.40	0.50	2.60	1.04	0.20	9.50	217.68
4	1.60	0.50	2.90	1.03	0.20	9.50	215.16
5	1.80	0.50	3.20	0.99	0.20	9.50	207.75
6	2.00	0.50	3.50	1.01	0.20	9.50	211.70
7	2.20	0.50	3.80	1.01	0.20	9.50	212.04
8	2.40	0.50	4.10	0.98	0.20	9.50	206.12
9	2.60	0.50	4.40	0.97	0.20	9.50	203.93
10	2.80	0.50	4.70	0.96	0.20	9.50	200.83
11	3.00	0.50	5.00	0.97	0.20	9.50	202.76
12	3.20	0.50	5.30	0.98	0.20	9.50	205.48
13	3.40	0.50	5.60	1.02	0.20	9.50	214.18
14	3.60	0.50	5.90	1.04	0.20	9.50	216.73
15	3.80	0.50	6.20	1.04	0.20	9.50	217.74
16	4.00	0.50	6.50	1.04	0.20	9.50	216.92

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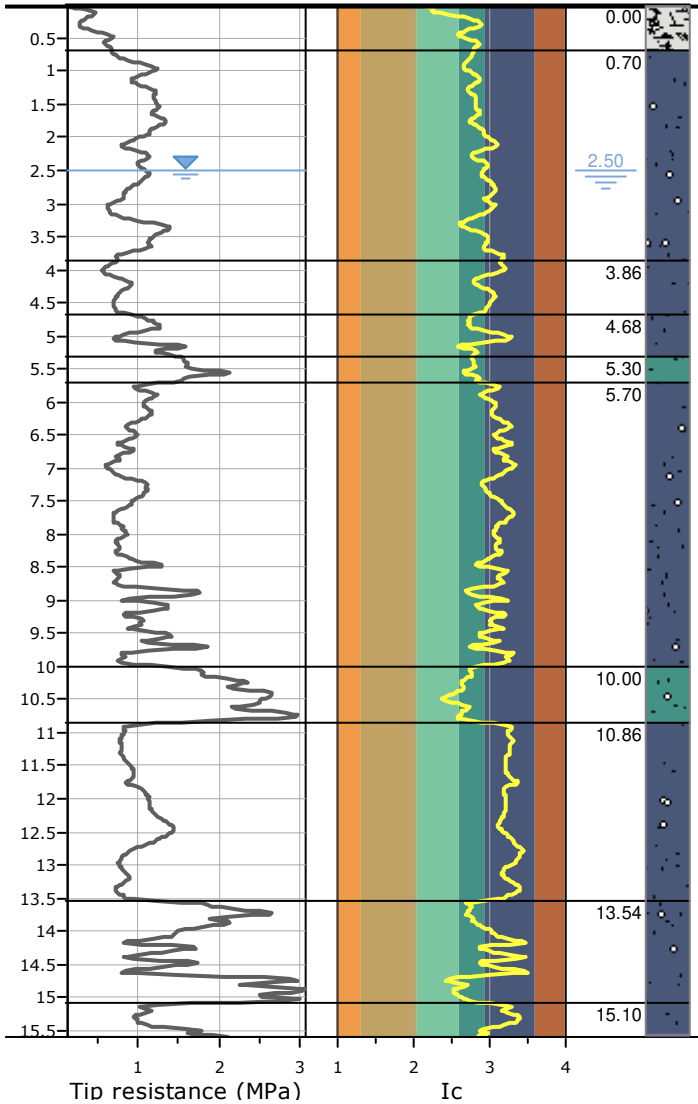
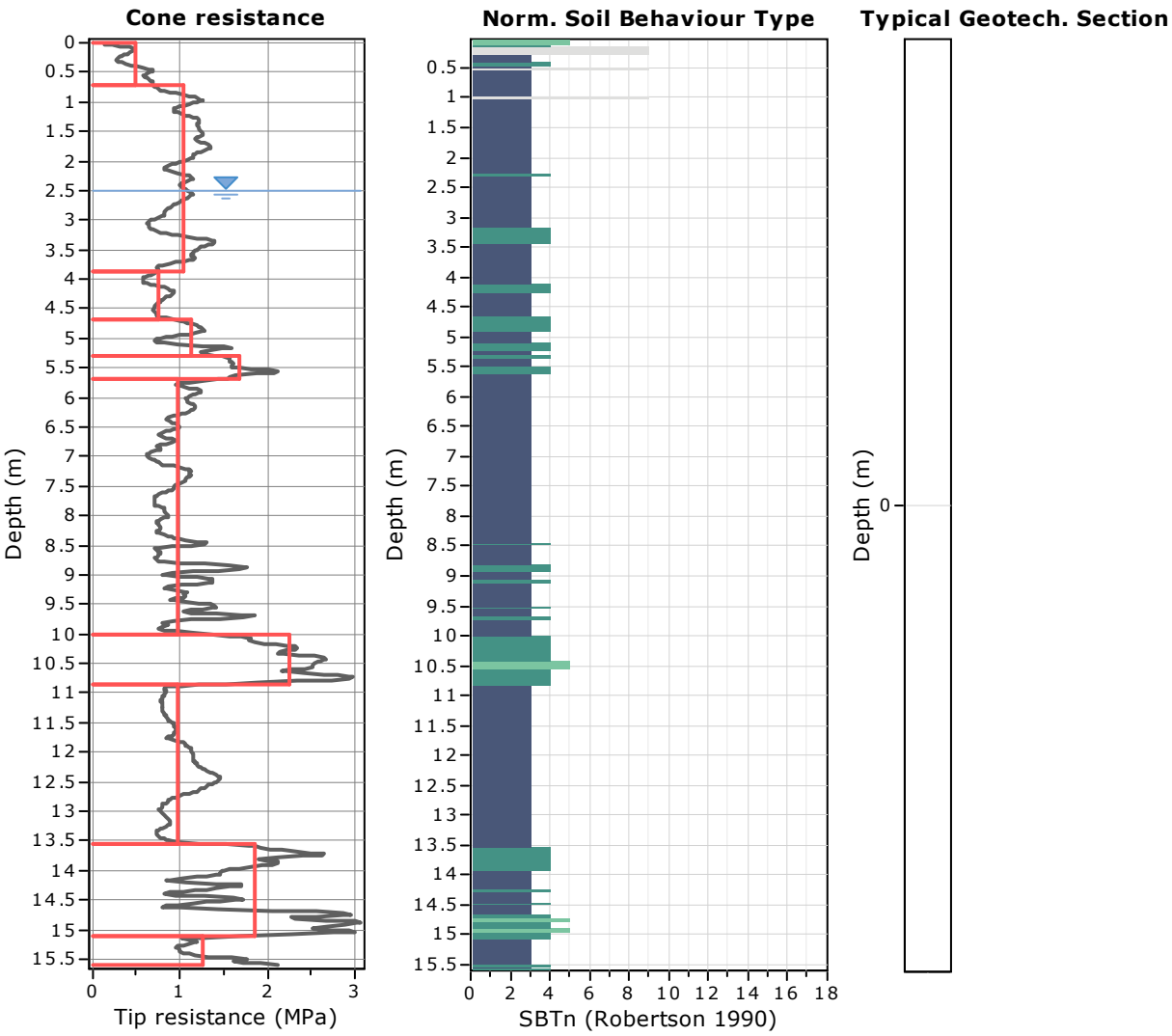
CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:

Depth (m) Elevation: 0.00 (m)



Depth (m)	Description	qt (MPa)	Ksbt (m/s)	N60	Es (MPa)	Dr	Phi (°)	M (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
0.00	Very dense/stiff soil	0.5	2.79E-7	2.1	9.3	-	-	6.6	13.0	35.5	4.3	19.8	16.6
0.70	Clay	1.0	2.29E-8	4.9	-	-	-	13.8	34.1	70.8	2.1	9.8	17.7
3.86	Clay	0.7	1.01E-8	3.8	-	-	-	7.9	26.6	47.9	0.8	3.8	16.5
4.68	Clay	1.1	3.25E-8	5.2	28.7	-	-	14.2	34.4	74.6	1.2	5.4	17.1
5.30	Clay & silty clay	1.7	3.50E-8	7.4	-	-	-	22.0	47.5	112.5	1.7	7.7	17.9
5.70	Clay	1.0	6.76E-9	5.2	-	-	-	8.9	36.2	59.8	0.7	3.4	16.9
10.00	Clay & silty clay	2.3	1.21E-7	9.2	46.6	-	-	28.9	52.6	143.9	1.4	6.6	17.5
10.86	Clay	1.0	1.47E-9	5.9	-	-	-	5.5	41.9	54.8	0.5	2.2	17.0
13.54	Clay	1.9	4.89E-8	8.6	44.9	-	-	19.8	52.6	107.5	0.8	3.9	17.3
15.10	Clay	1.3	4.41E-9	7.0	-	-	-	7.8	47.5	70.8	0.5	2.4	17.1



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.70 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 0.48 ±0.16 MPa	Permeability: 2.79E-07 ±5.62E-07 m/s	Constrained Mod.: 6.58 ±2.23 MPa
Sleeve friction: 37.14 ±18.33 kPa	N60: 2.09 ±0.83 blows	Go: 12.99 ±5.51 MPa
SBT_n: 9	Es: 9.34 ±2.87 MPa	Su: 35.50 ±10.62 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 4.30 ±1.01
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 19.85 ±4.68
	Unit weight: 16.65 ±0.89 kN/m³	

.:: Layer No: 2 ::.

Code: A1 **Start depth:** 0.70 (m), **End depth:** 3.86 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.03 ±0.20 MPa	Permeability: 2.29E-08 ±2.09E-08 m/s	Constrained Mod.: 13.79 ±3.04 MPa
Sleeve friction: 66.89 ±23.58 kPa	N60: 4.89 ±0.93 blows	Go: 34.14 ±5.83 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 70.82 ±14.55 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 2.11 ±0.94
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 9.75 ±4.36
	Unit weight: 17.73 ±0.57 kN/m³	

.:: Layer No: 3 ::.

Code: D1 **Start depth:** 3.86 (m), **End depth:** 4.68 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.75 ±0.10 MPa	Permeability: 1.01E-08 ±8.85E-09 m/s	Constrained Mod.: 7.93 ±2.24 MPa
Sleeve friction: 25.11 ±8.24 kPa	N60: 3.81 ±0.40 blows	Go: 26.62 ±2.62 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 47.92 ±7.32 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.83 ±0.12
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.84 ±0.54
	Unit weight: 16.53 ±0.35 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 4.68 (m), **End depth:** 5.30 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.13 ±0.24 MPa	Permeability: 3.25E-08 ±2.76E-08 m/s	Constrained Mod.: 14.21 ±4.06 MPa
Sleeve friction: 35.62 ±12.32 kPa	N60: 5.19 ±0.78 blows	Go: 34.43 ±3.70 MPa
SBT_n: 3	Es: 28.74 ±28.74 MPa	Su: 74.59 ±17.23 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.17 ±0.24
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.40 ±1.13
	Unit weight: 17.07 ±0.38 kN/m³	

.:: Layer No: 5 ::.

Code: B1 **Start depth:** 5.30 (m), **End depth:** 5.70 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 1.67 ±0.19 MPa	Permeability: 3.50E-08 ±1.63E-08 m/s	Constrained Mod.: 22.04 ±2.69 MPa
Sleeve friction: 61.44 ±8.44 kPa	N60: 7.38 ±0.67 blows	Go: 47.54 ±3.14 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 112.46 ±13.74 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.66 ±0.18
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 7.68 ±0.85
	Unit weight: 17.91 ±0.17 kN/m³	

.:: Layer No: 6 ::.

Code: A3 **Start depth:** 5.70 (m), **End depth:** 10.00 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.97 ±0.24 MPa	Permeability: 6.76E-09 ±9.06E-09 m/s	Constrained Mod.: 8.89 ±4.68 MPa
Sleeve friction: 34.16 ±13.53 kPa	N60: 5.17 ±0.92 blows	Go: 36.15 ±5.19 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 59.84 ±16.97 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.73 ±0.21
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.36 ±0.99
	Unit weight: 16.94 ±0.48 kN/m³	

.:: Layer No: 7 ::.

Code: B2 **Start depth:** 10.00 (m), **End depth:** 10.86 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 2.26 ±0.43 MPa	Permeability: 1.21E-07 ±1.32E-07 m/s	Constrained Mod.: 28.89 ±6.39 MPa
Sleeve friction: 41.87 ±13.70 kPa	N60: 9.20 ±1.37 blows	Go: 52.58 ±7.07 MPa
SBT_n: 4	Es: 46.62 ±3.67 MPa	Su: 143.92 ±31.12 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.42 ±0.29
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.55 ±1.36
	Unit weight: 17.53 ±0.41 kN/m³	

.:: Layer No: 8 ::.

Code: A4 **Start depth:** 10.86 (m), **End depth:** 13.54 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.98 ±0.20 MPa	Permeability: 1.47E-09 ±1.10E-09 m/s	Constrained Mod.: 5.52 ±3.00 MPa
Sleeve friction: 37.06 ±19.18 kPa	N60: 5.94 ±1.09 blows	Go: 41.88 ±9.30 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 54.85 ±14.62 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.48 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.22 ±0.59
	Unit weight: 16.98 ±0.65 kN/m³	

.:: Layer No: 9 ::.

Code: B3 **Start depth:** 13.54 (m), **End depth:** 15.10 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.86 ±0.67 MPa	Permeability: 4.89E-08 ±7.55E-08 m/s	Constrained Mod.: 19.77 ±11.82 MPa
Sleeve friction: 37.00 ±11.11 kPa	N60: 8.65 ±1.88 blows	Go: 52.55 ±7.84 MPa
SBT_n: 3	Es: 44.89 ±4.42 MPa	Su: 107.51 ±42.89 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.84 ±0.33
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.87 ±1.55
	Unit weight: 17.31 ±0.39 kN/m³	

.:: Layer No: 10 ::.

Code: A5 **Start depth:** 15.10 (m), **End depth:** 15.60 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.26 ±0.31 MPa	Permeability: 4.41E-09 ±5.36E-09 m/s	Constrained Mod.: 7.79 ±4.98 MPa
Sleeve friction: 33.65 ±5.24 kPa	N60: 7.04 ±1.02 blows	Go: 47.53 ±4.00 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 70.84 ±22.01 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.51 ±0.16
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.38 ±0.73
	Unit weight: 17.10 ±0.19 kN/m³	

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Project:
Location:

CPT: CPTu-05
Total depth: 15.60 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.70	2.79E-07	2.1	9.3	0.0	0.0	6.6	13.0	35.5	4.3	19.8	16.6
0.70		(±5.62E-07)	(±0.8)	(±2.9)	(±0.0)	(±0.0)	(±2.2)	(±5.5)	(±10.6)	(±1.0)	(±4.7)	(±0.9)
0.70	3.16	2.29E-08	4.9	0.0	0.0	0.0	13.8	34.1	70.8	2.1	9.8	17.7
3.86		(±2.09E-08)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±5.8)	(±14.6)	(±0.9)	(±4.4)	(±0.6)
3.86	0.82	1.01E-08	3.8	0.0	0.0	0.0	7.9	26.6	47.9	0.8	3.8	16.5
4.68		(±8.85E-09)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±2.6)	(±7.3)	(±0.1)	(±0.5)	(±0.3)
4.68	0.62	3.25E-08	5.2	28.7	0.0	0.0	14.2	34.4	74.6	1.2	5.4	17.1
5.30		(±2.76E-08)	(±0.8)	(±28.7)	(±0.0)	(±0.0)	(±4.1)	(±3.7)	(±17.2)	(±0.2)	(±1.1)	(±0.4)
5.30	0.40	3.50E-08	7.4	0.0	0.0	0.0	22.0	47.5	112.5	1.7	7.7	17.9
5.70		(±1.63E-08)	(±0.7)	(±0.0)	(±0.0)	(±0.0)	(±2.7)	(±3.1)	(±13.7)	(±0.2)	(±0.8)	(±0.2)
5.70	4.30	6.76E-09	5.2	0.0	0.0	0.0	8.9	36.2	59.8	0.7	3.4	16.9
10.00		(±9.06E-09)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±4.7)	(±5.2)	(±17.0)	(±0.2)	(±1.0)	(±0.5)
10.00	0.86	1.21E-07	9.2	46.6	0.0	0.0	28.9	52.6	143.9	1.4	6.6	17.5
10.86		(±1.32E-07)	(±1.4)	(±3.7)	(±0.0)	(±0.0)	(±6.4)	(±7.1)	(±31.1)	(±0.3)	(±1.4)	(±0.4)
10.86	2.68	1.47E-09	5.9	0.0	0.0	0.0	5.5	41.9	54.8	0.5	2.2	17.0
13.54		(±1.10E-09)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±9.3)	(±14.6)	(±0.1)	(±0.6)	(±0.7)
13.54	1.56	4.89E-08	8.6	44.9	0.0	0.0	19.8	52.6	107.5	0.8	3.9	17.3
15.10		(±7.55E-08)	(±1.9)	(±4.4)	(±0.0)	(±0.0)	(±11.8)	(±7.8)	(±42.9)	(±0.3)	(±1.5)	(±0.4)
15.10	0.50	4.41E-09	7.0	0.0	0.0	0.0	7.8	47.5	70.8	0.5	2.4	17.1
15.60		(±5.36E-09)	(±1.0)	(±0.0)	(±0.0)	(±0.0)	(±5.0)	(±4.0)	(±22.0)	(±0.2)	(±0.7)	(±0.2)

Depth values presented in this table are measured from free ground surface

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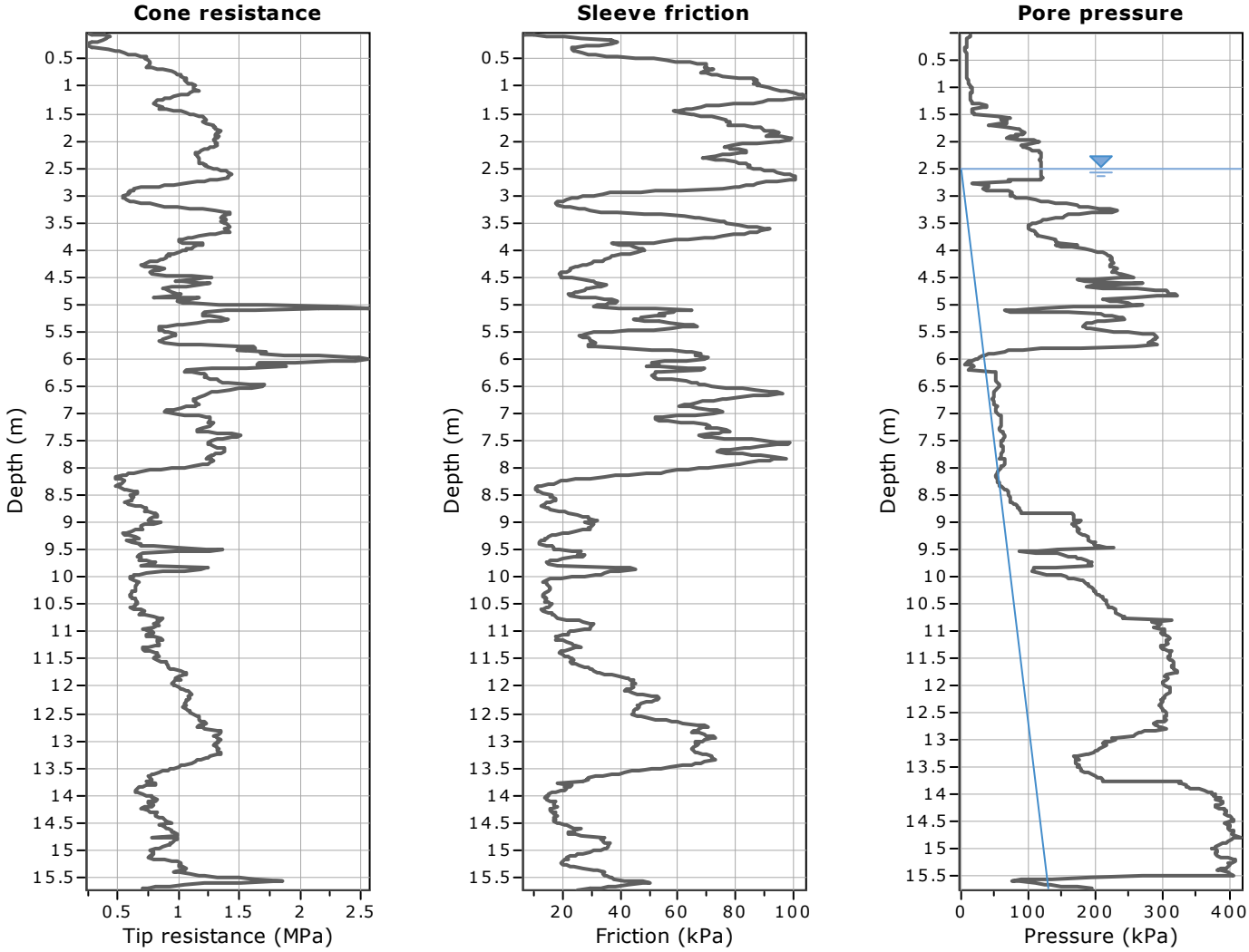
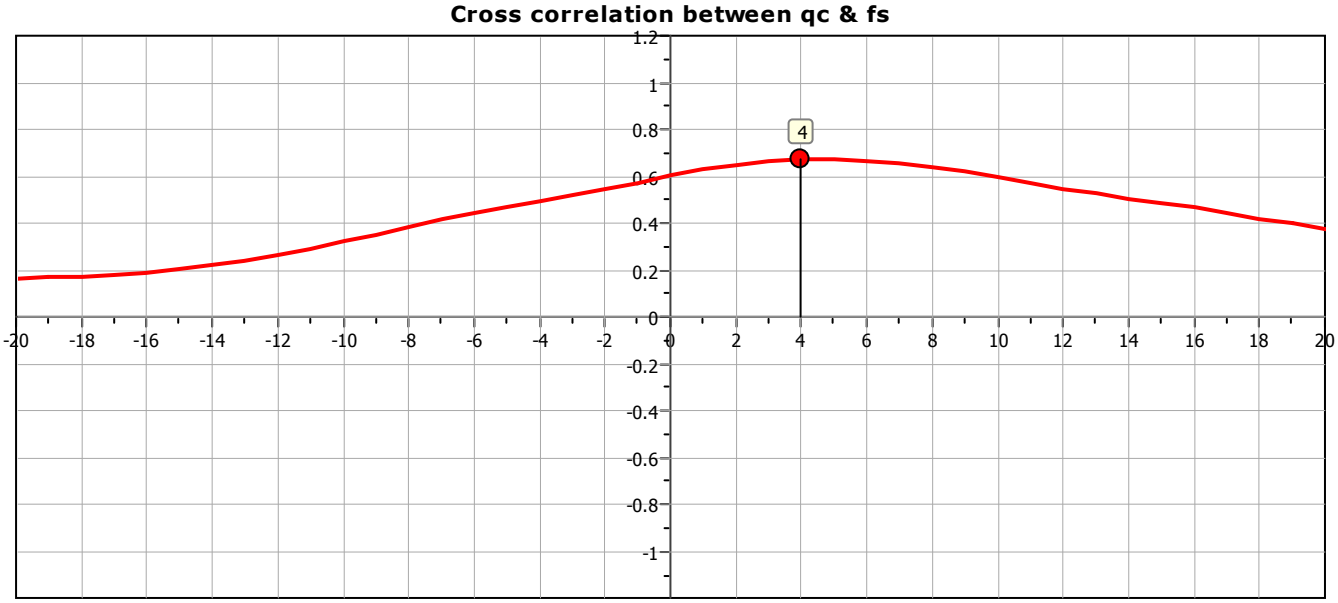
CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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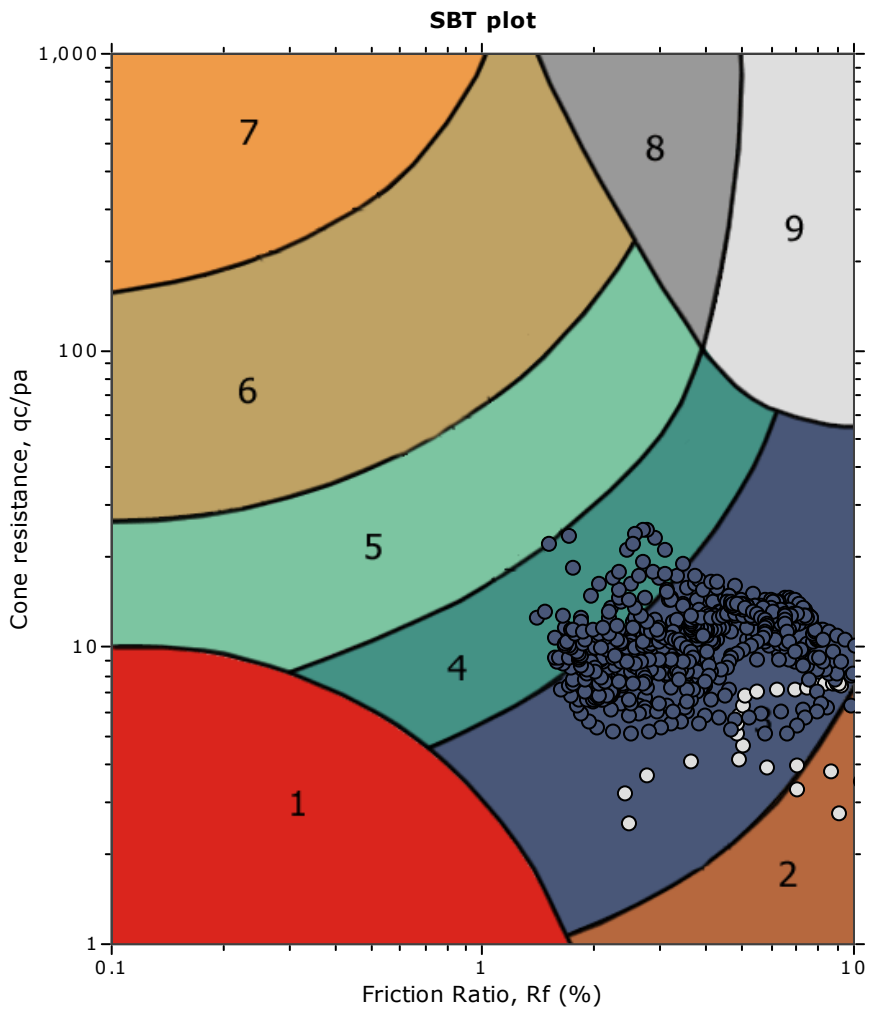
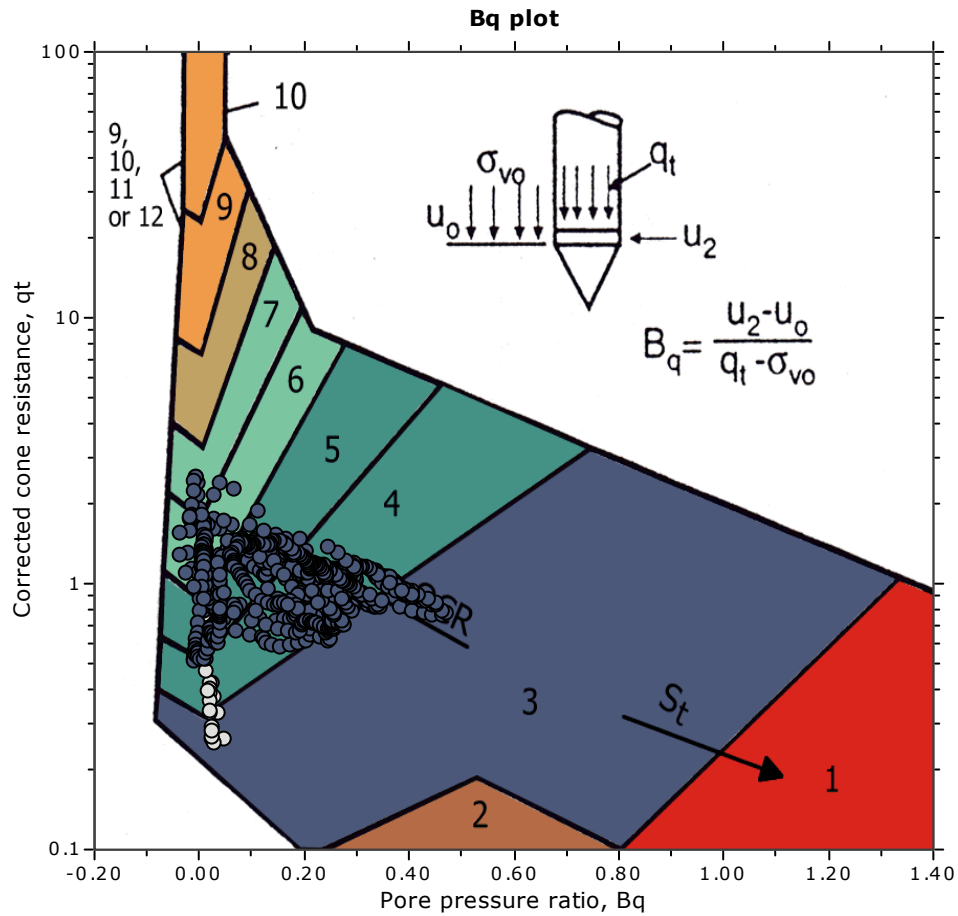
Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots





SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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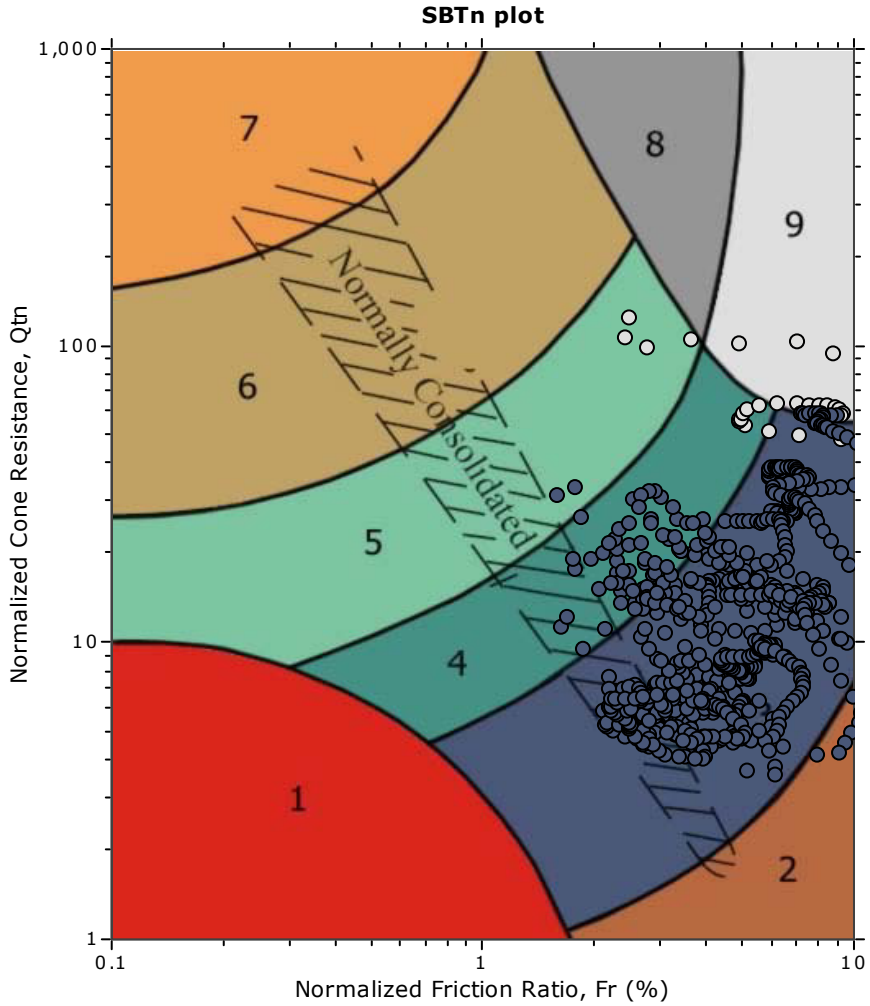
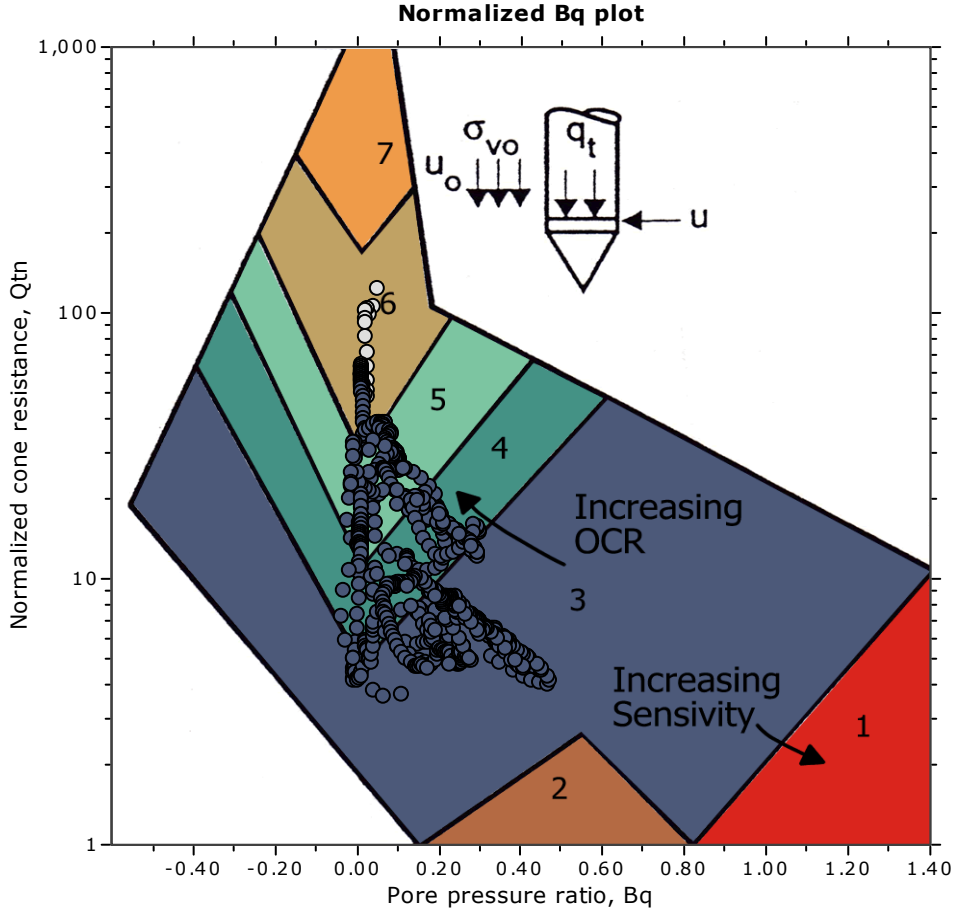
Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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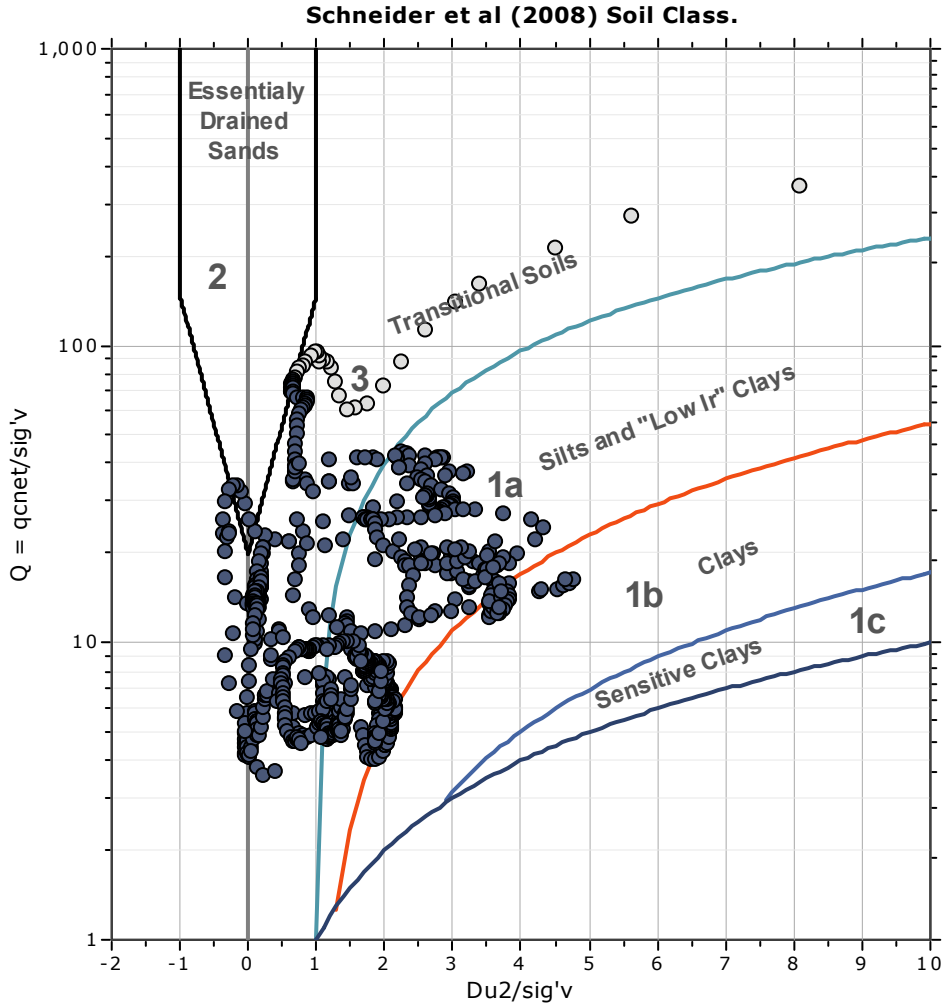
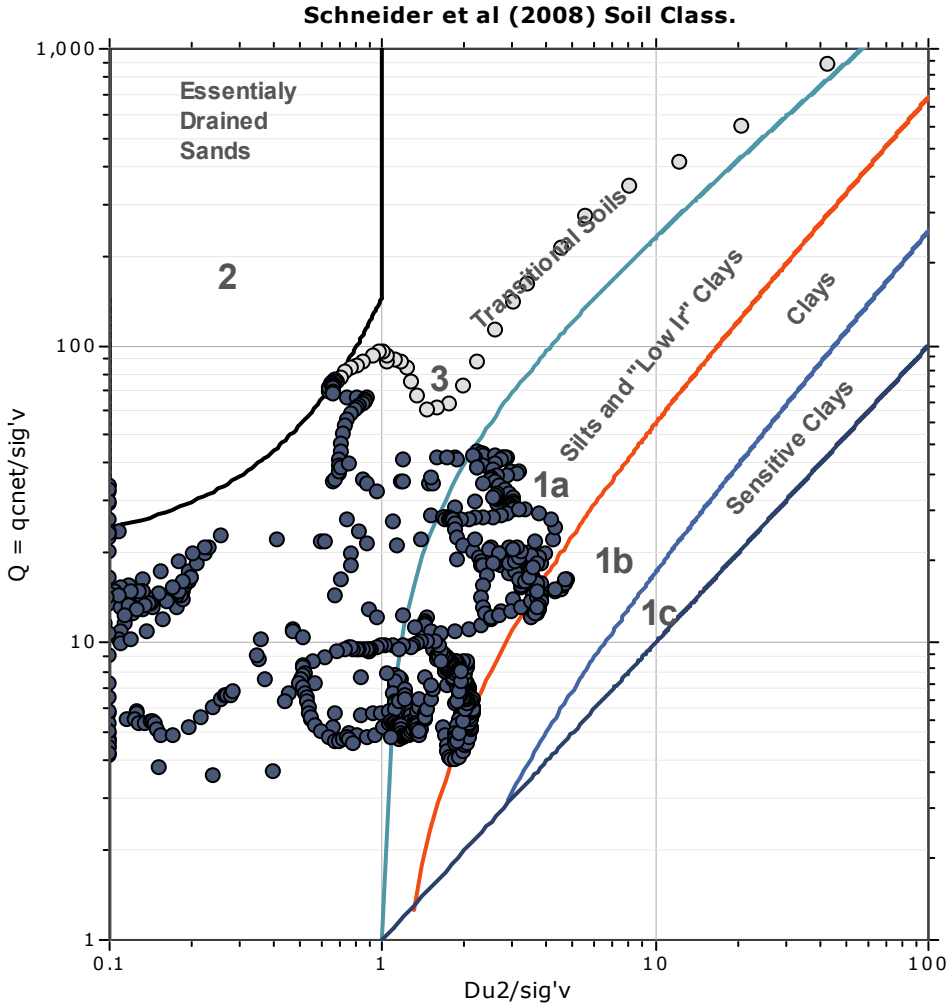
Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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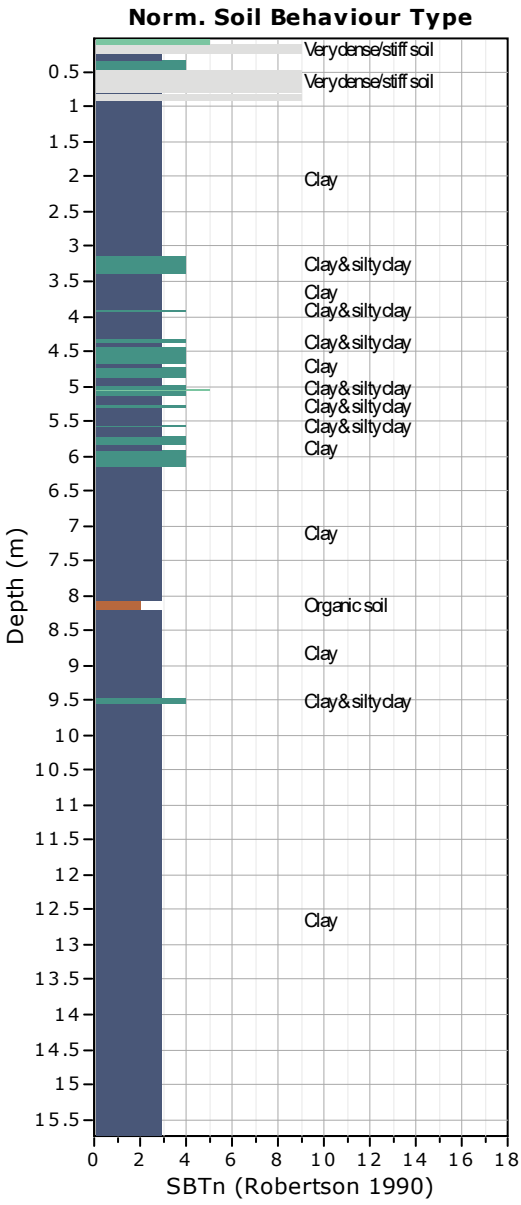
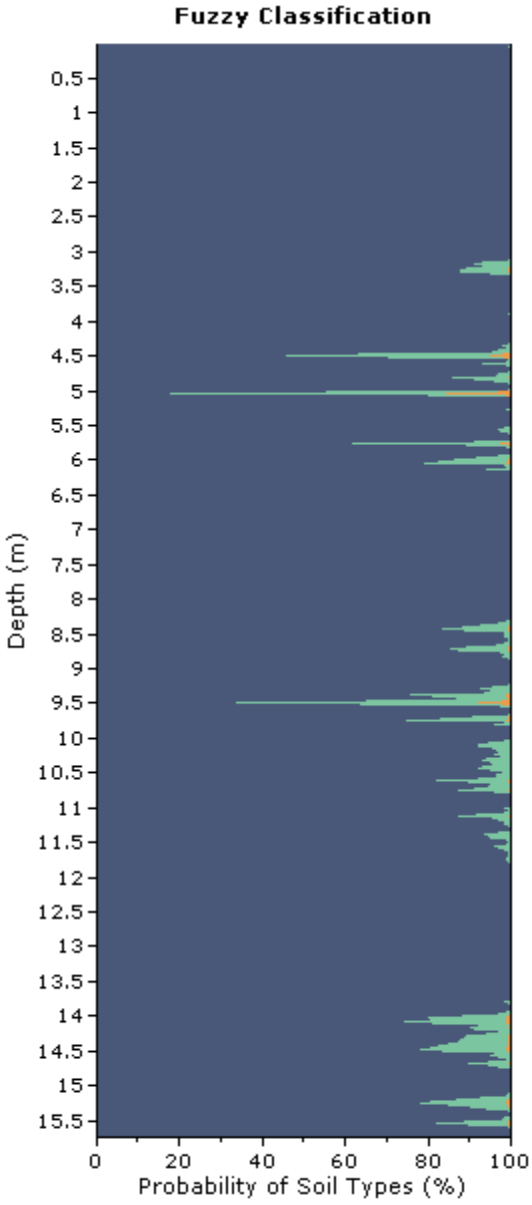
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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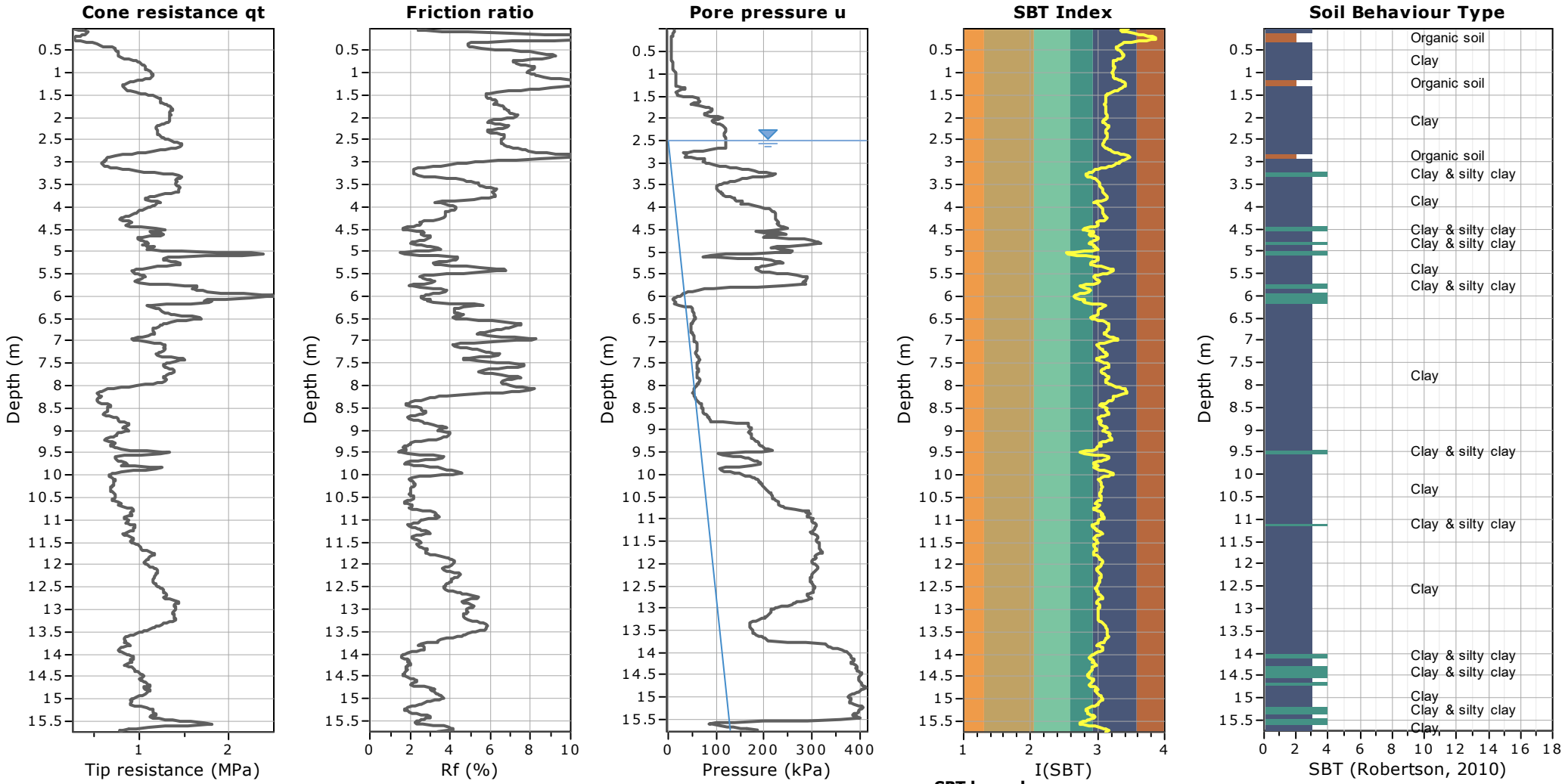
Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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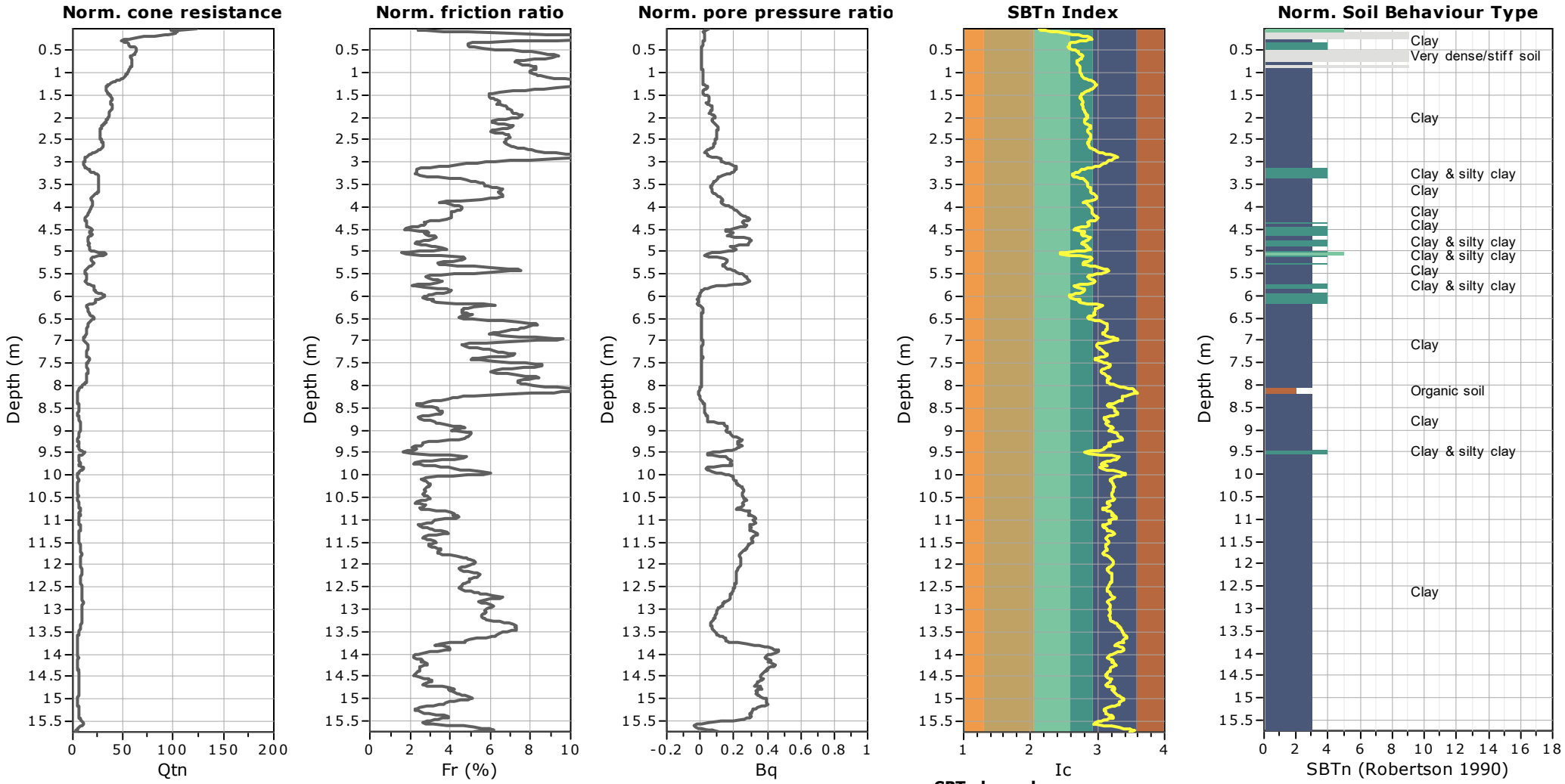
Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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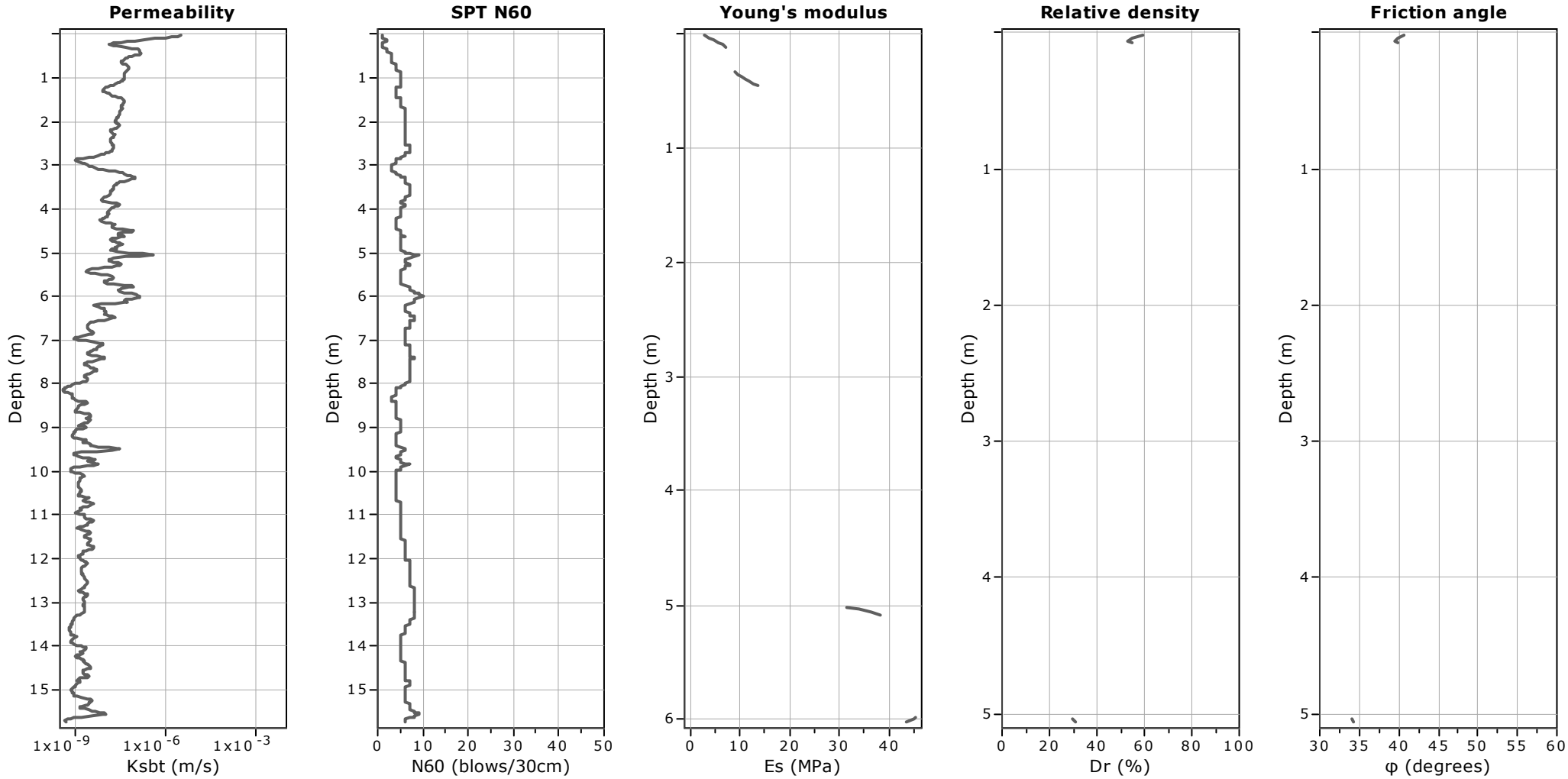
Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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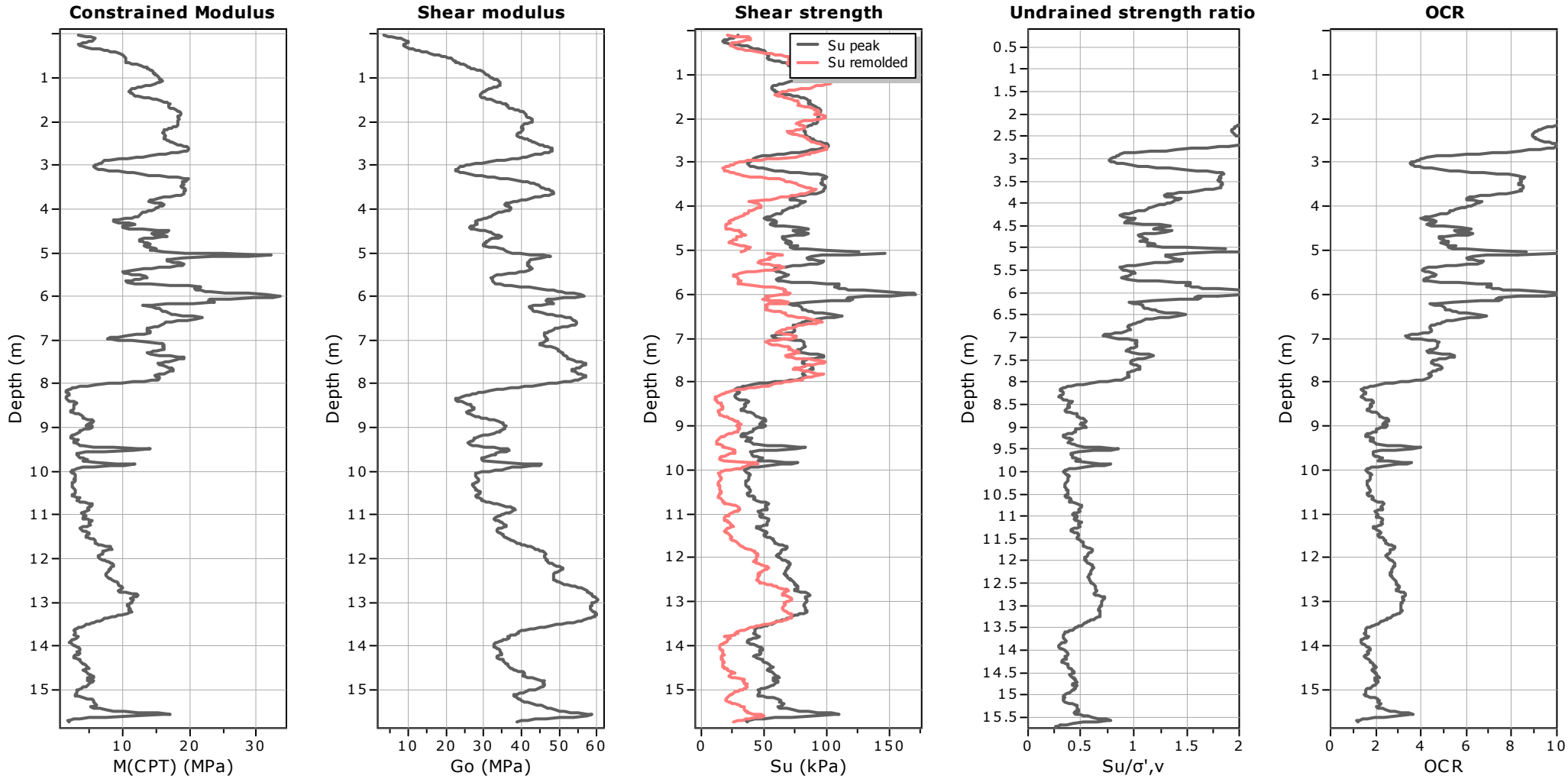
Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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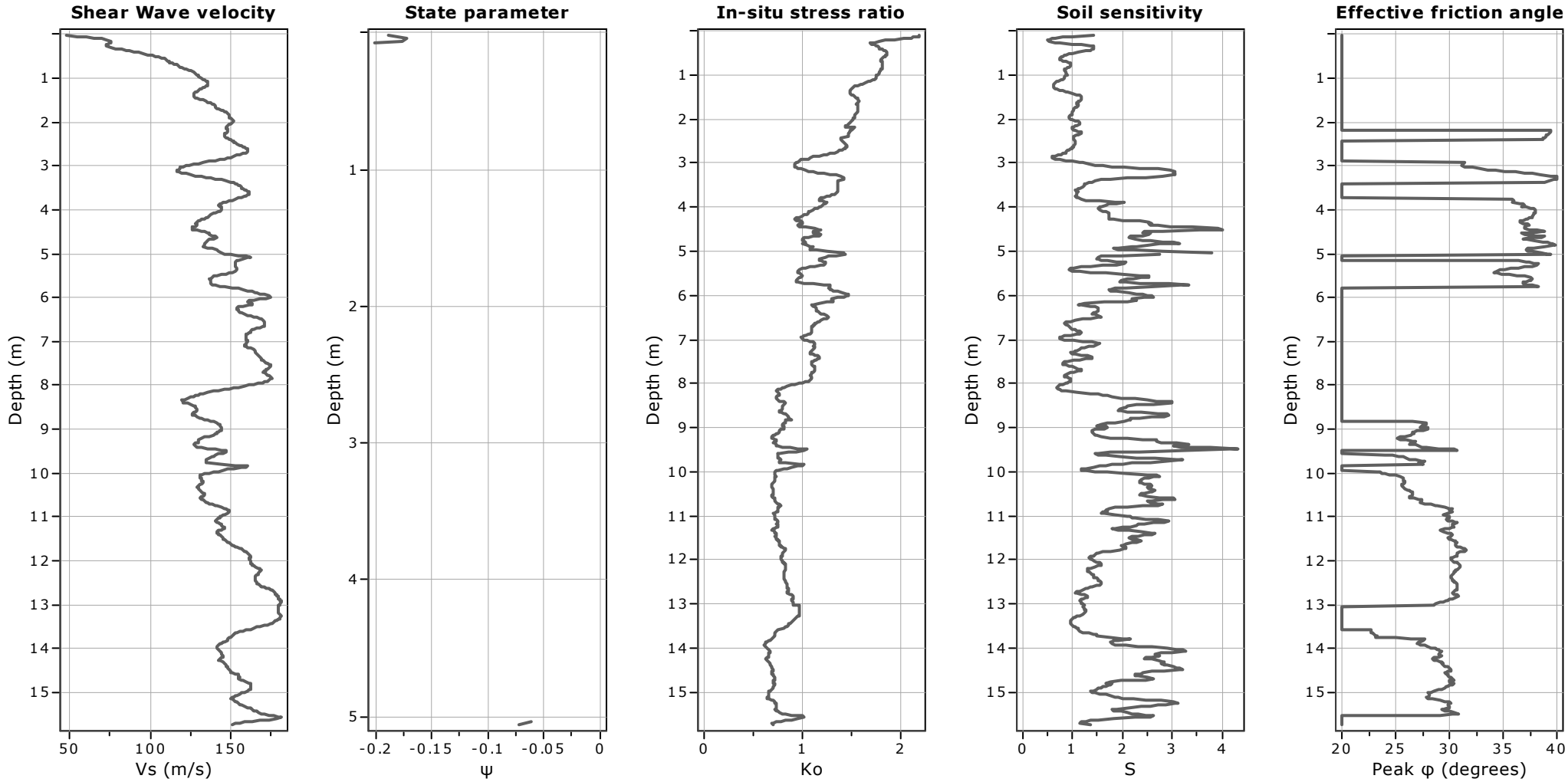
Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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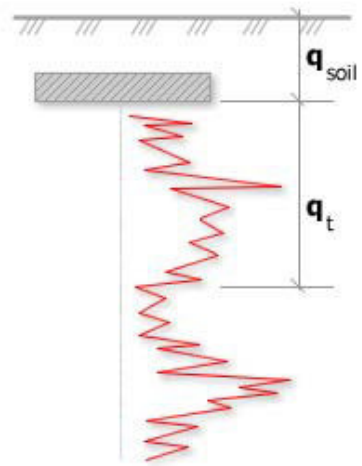
CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

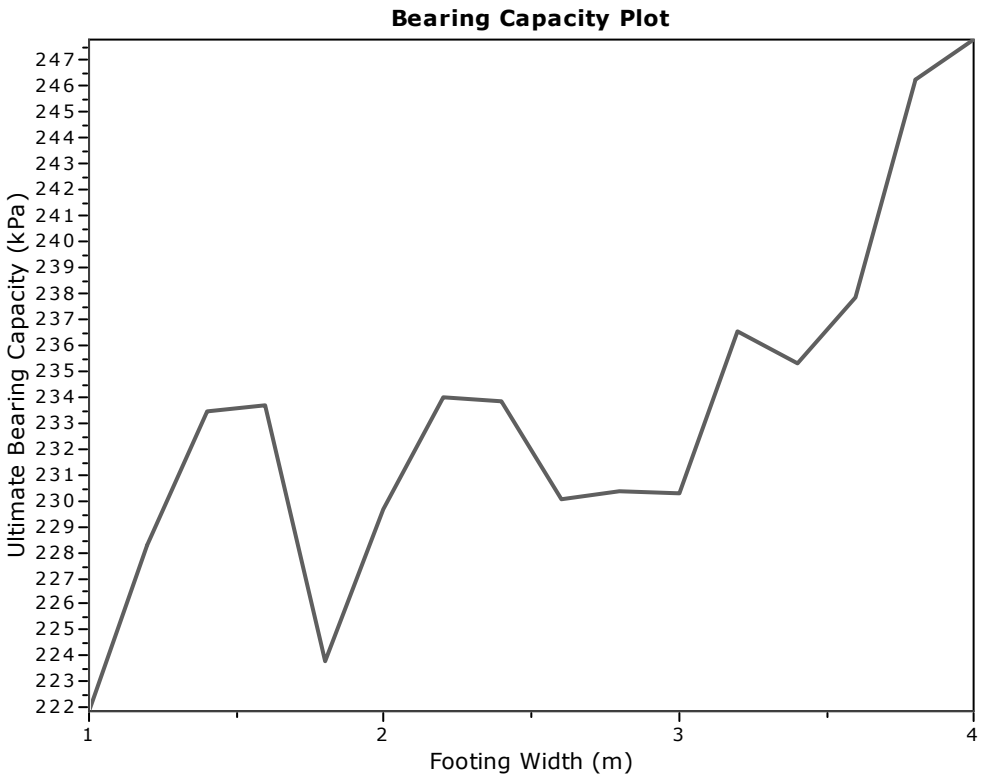
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.06	0.20	9.50	221.88
2	1.20	0.50	2.30	1.09	0.20	9.50	228.31
3	1.40	0.50	2.60	1.12	0.20	9.50	233.40
4	1.60	0.50	2.90	1.12	0.20	9.50	233.63
5	1.80	0.50	3.20	1.07	0.20	9.50	223.77
6	2.00	0.50	3.50	1.10	0.20	9.50	229.67
7	2.20	0.50	3.80	1.12	0.20	9.50	233.97
8	2.40	0.50	4.10	1.12	0.20	9.50	233.78
9	2.60	0.50	4.40	1.10	0.20	9.50	230.06
10	2.80	0.50	4.70	1.10	0.20	9.50	230.36
11	3.00	0.50	5.00	1.10	0.20	9.50	230.30
12	3.20	0.50	5.30	1.14	0.20	9.50	236.51
13	3.40	0.50	5.60	1.13	0.20	9.50	235.30
14	3.60	0.50	5.90	1.14	0.20	9.50	237.85
15	3.80	0.50	6.20	1.18	0.20	9.50	246.21
16	4.00	0.50	6.50	1.19	0.20	9.50	247.75

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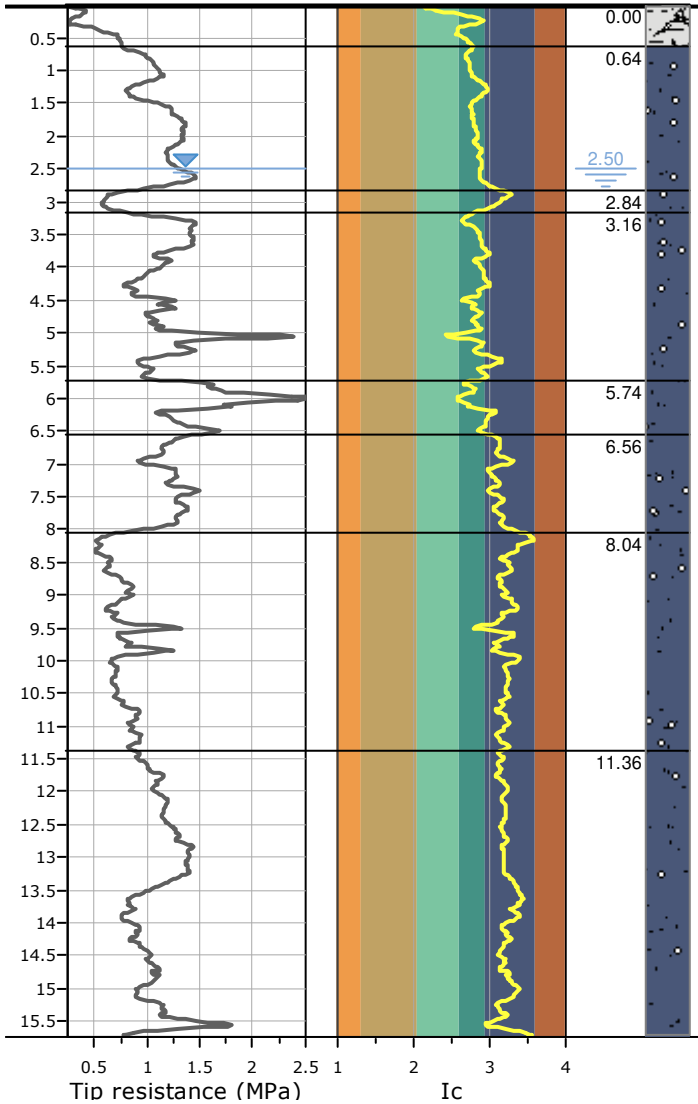
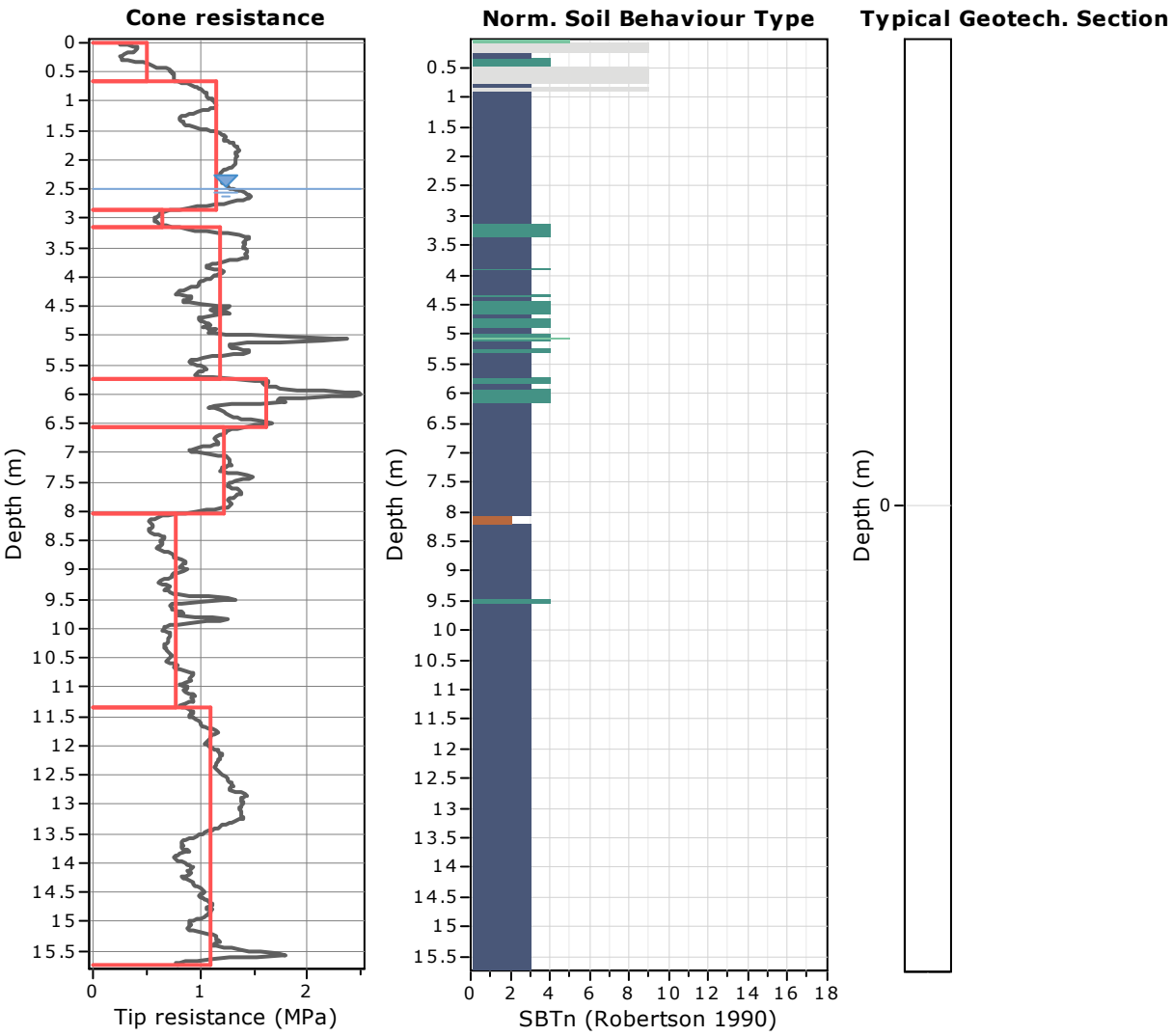
CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:

Depth (m) Elevation: 0.00 (m)



Depth (m)	Description	qt (MPa)	Ksbt (m/s)	N60	Es (MPa)	Dr	Phi (°)	M (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
0.00	Very dense/stiff soil	0.5	3.24E-7	2.0	10.1	-	-	7.0	13.0	37.5	4.6	21.4	16.7
0.64	Clay	1.2	2.55E-8	5.4	-	-	-	15.8	36.8	80.4	2.7	12.6	18.1
2.84	Clay	0.7	5.85E-9	3.5	-	-	-	7.4	27.7	42.9	0.9	4.1	16.9
3.16	Clay	1.2	2.97E-8	5.5	34.9	-	-	15.3	36.4	77.4	1.3	6.0	17.3
5.74	Clay	1.6	3.75E-8	7.4	44.5	-	-	21.2	47.7	108.1	1.5	6.8	17.8
6.56	Clay	1.2	3.43E-9	6.7	-	-	-	14.6	51.1	78.4	1.0	4.5	18.0
8.04	Clay	0.8	2.24E-9	4.5	-	-	-	3.8	31.3	42.8	0.4	2.0	16.3
11.36	Clay	1.1	1.86E-9	6.5	-	-	-	6.4	45.3	61.8	0.5	2.3	17.1



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.64 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 0.51 ±0.19 MPa	Permeability: 3.24E-07 ±7.12E-07 m/s	Constrained Mod.: 7.02 ±2.69 MPa
Sleeve friction: 36.52 ±18.52 kPa	N60: 1.97 ±0.86 blows	Go: 12.98 ±5.78 MPa
SBT_n: 9	Es: 10.09 ±2.38 MPa	Su: 37.49 ±13.80 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 4.64 ±1.08
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 21.43 ±5.00
	Unit weight: 16.67 ±0.79 kN/m³	

.:: Layer No: 2 ::.

Code: A1 **Start depth:** 0.64 (m), **End depth:** 2.84 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.16 ±0.19 MPa	Permeability: 2.55E-08 ±1.36E-08 m/s	Constrained Mod.: 15.76 ±2.50 MPa
Sleeve friction: 83.98 ±11.26 kPa	N60: 5.36 ±0.94 blows	Go: 36.80 ±6.44 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 80.39 ±12.78 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 2.72 ±0.80
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 12.58 ±3.68
	Unit weight: 18.12 ±0.19 kN/m³	

.:: Layer No: 3 ::.

Code: D1 **Start depth:** 2.84 (m), **End depth:** 3.16 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.65 ±0.08 MPa	Permeability: 5.85E-09 ±7.42E-09 m/s	Constrained Mod.: 7.38 ±1.69 MPa
Sleeve friction: 39.39 ±22.64 kPa	N60: 3.53 ±0.62 blows	Go: 27.74 ±5.62 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 42.87 ±5.55 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.88 ±0.11
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.07 ±0.51
	Unit weight: 16.89 ±0.63 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 3.16 (m), **End depth:** 5.74 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.18 ±0.27 MPa	Permeability: 2.97E-08 ±4.69E-08 m/s	Constrained Mod.: 15.25 ±3.95 MPa
Sleeve friction: 43.60 ±19.59 kPa	N60: 5.48 ±1.01 blows	Go: 36.38 ±6.33 MPa
SBT_n: 3	Es: 34.87 ±4.69 MPa	Su: 77.36 ±16.46 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.30 ±0.31
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.99 ±1.46
	Unit weight: 17.28 ±0.54 kN/m³	

.:: Layer No: 5 ::.

Code: B1 **Start depth:** 5.74 (m), **End depth:** 6.56 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.62 ±0.38 MPa	Permeability: 3.75E-08 ±3.73E-08 m/s	Constrained Mod.: 21.18 ±5.35 MPa
Sleeve friction: 59.06 ±12.57 kPa	N60: 7.38 ±1.13 blows	Go: 47.73 ±5.12 MPa
SBT_n: 3	Es: 44.54 ±1.02 MPa	Su: 108.14 ±27.20 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.48 ±0.37
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.83 ±1.70
	Unit weight: 17.83 ±0.30 kN/m³	

.:: Layer No: 6 ::.

Code: A3 **Start depth:** 6.56 (m), **End depth:** 8.04 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.23 ±0.14 MPa	Permeability: 3.43E-09 ±1.94E-09 m/s	Constrained Mod.: 14.58 ±3.04 MPa
Sleeve friction: 76.43 ±12.18 kPa	N60: 6.71 ±0.54 blows	Go: 51.15 ±3.98 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 78.40 ±10.25 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.96 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.46 ±0.59
	Unit weight: 18.04 ±0.20 kN/m³	

.:: Layer No: 7 ::.

Code: D2 **Start depth:** 8.04 (m), **End depth:** 11.36 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.77 ±0.15 MPa	Permeability: 2.24E-09 ±3.26E-09 m/s	Constrained Mod.: 3.82 ±1.97 MPa
Sleeve friction: 21.42 ±9.02 kPa	N60: 4.48 ±0.65 blows	Go: 31.27 ±4.58 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 42.77 ±10.06 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.43 ±0.10
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.01 ±0.45
	Unit weight: 16.33 ±0.44 kN/m³	

.:: Layer No: 8 ::.

Code: A4 **Start depth:** 11.36 (m), **End depth:** 15.74 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.10 ±0.20 MPa	Permeability: 1.86E-09 ±1.21E-09 m/s	Constrained Mod.: 6.36 ±3.02 MPa
Sleeve friction: 38.32 ±17.75 kPa	N60: 6.47 ±1.05 blows	Go: 45.33 ±8.44 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 61.75 ±14.44 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.50 ±0.13
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.30 ±0.58
	Unit weight: 17.09 ±0.60 kN/m³	

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Project:
Location:

CPT: CPTu-06
Total depth: 15.74 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.64	3.24E-07	2.0	10.1	0.0	0.0	7.0	13.0	37.5	4.6	21.4	16.7
0.64		(±7.12E-07)	(±0.9)	(±2.4)	(±0.0)	(±0.0)	(±2.7)	(±5.8)	(±13.8)	(±1.1)	(±5.0)	(±0.8)
0.64	2.20	2.55E-08	5.4	0.0	0.0	0.0	15.8	36.8	80.4	2.7	12.6	18.1
2.84		(±1.36E-08)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±2.5)	(±6.4)	(±12.8)	(±0.8)	(±3.7)	(±0.2)
2.84	0.32	5.85E-09	3.5	0.0	0.0	0.0	7.4	27.7	42.9	0.9	4.1	16.9
3.16		(±7.42E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±1.7)	(±5.6)	(±5.6)	(±0.1)	(±0.5)	(±0.6)
3.16	2.58	2.97E-08	5.5	34.9	0.0	0.0	15.3	36.4	77.4	1.3	6.0	17.3
5.74		(±4.69E-08)	(±1.0)	(±4.7)	(±0.0)	(±0.0)	(±4.0)	(±6.3)	(±16.5)	(±0.3)	(±1.5)	(±0.5)
5.74	0.82	3.75E-08	7.4	44.5	0.0	0.0	21.2	47.7	108.1	1.5	6.8	17.8
6.56		(±3.73E-08)	(±1.1)	(±1.0)	(±0.0)	(±0.0)	(±5.4)	(±5.1)	(±27.2)	(±0.4)	(±1.7)	(±0.3)
6.56	1.48	3.43E-09	6.7	0.0	0.0	0.0	14.6	51.1	78.4	1.0	4.5	18.0
8.04		(±1.94E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±4.0)	(±10.3)	(±0.1)	(±0.6)	(±0.2)
8.04	3.32	2.24E-09	4.5	0.0	0.0	0.0	3.8	31.3	42.8	0.4	2.0	16.3
11.36		(±3.26E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±2.0)	(±4.6)	(±10.1)	(±0.1)	(±0.4)	(±0.4)
11.36	4.38	1.86E-09	6.5	0.0	0.0	0.0	6.4	45.3	61.8	0.5	2.3	17.1
15.74		(±1.21E-09)	(±1.1)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±8.4)	(±14.4)	(±0.1)	(±0.6)	(±0.6)

Depth values presented in this table are measured from free ground surface

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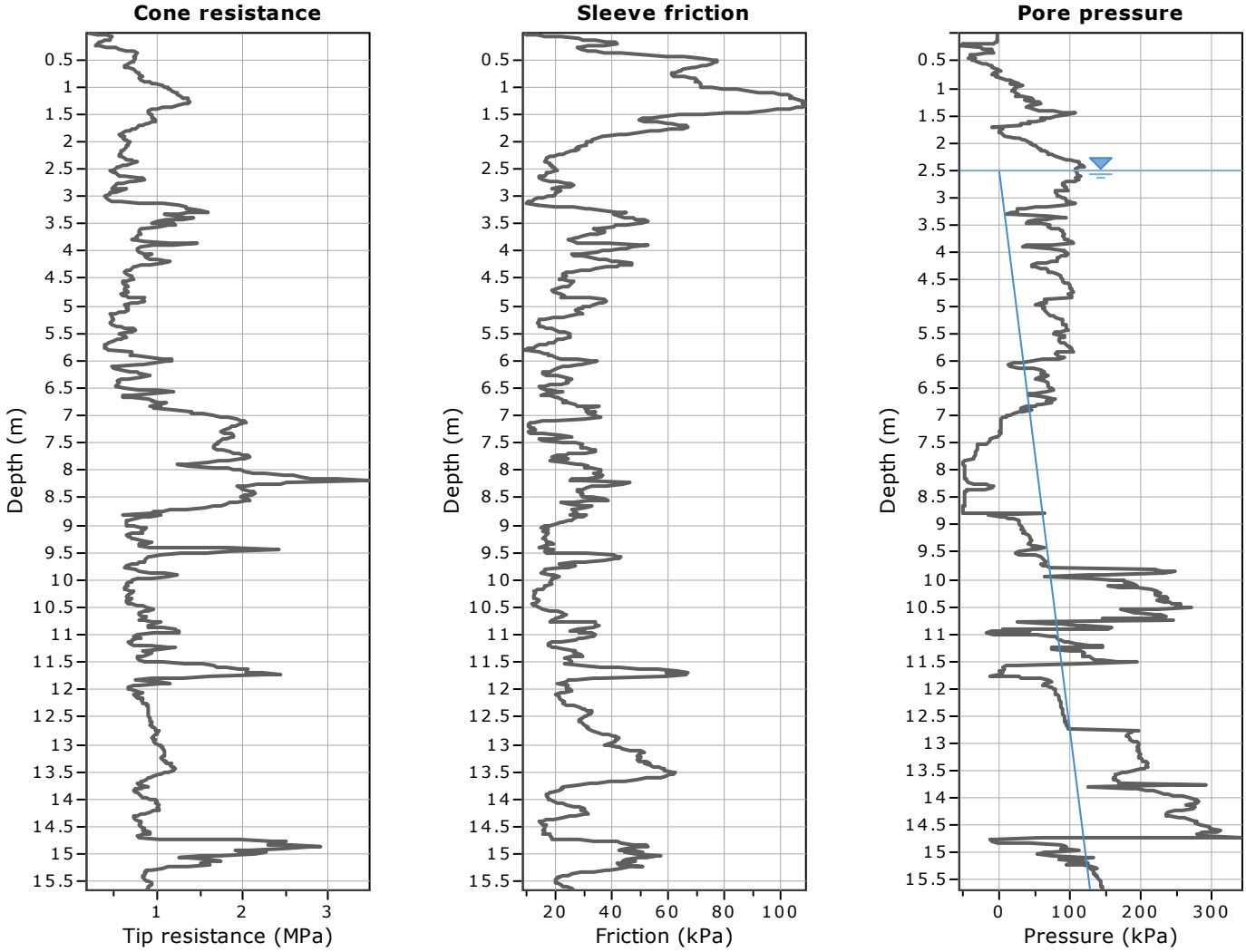
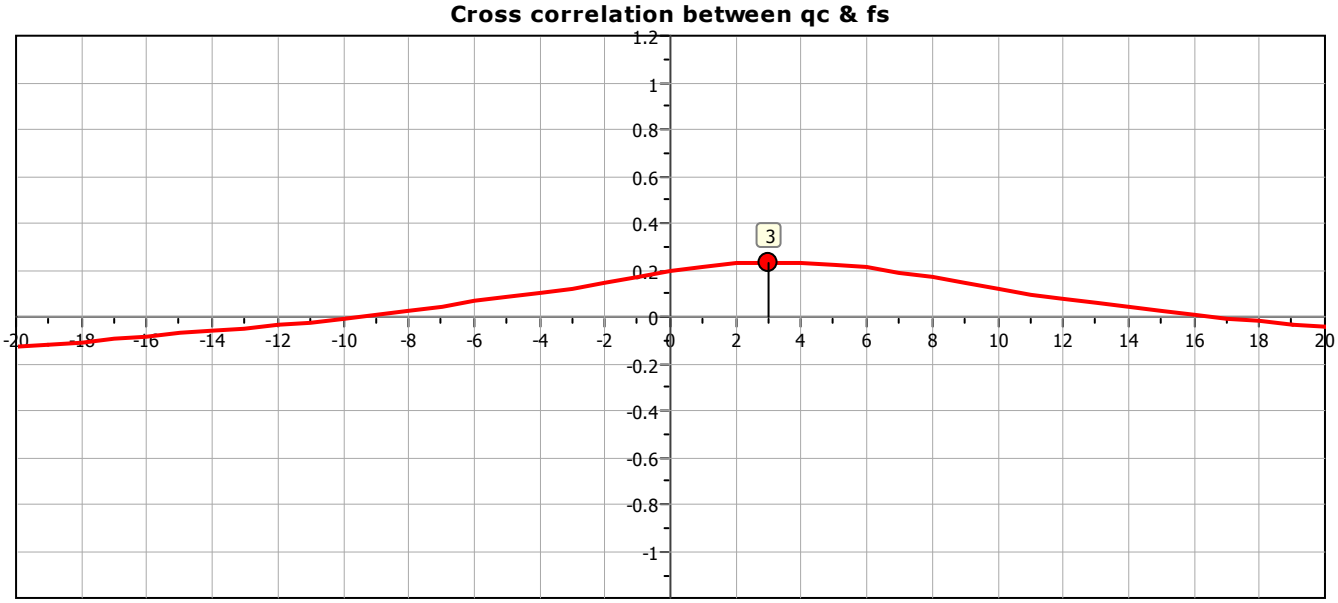
CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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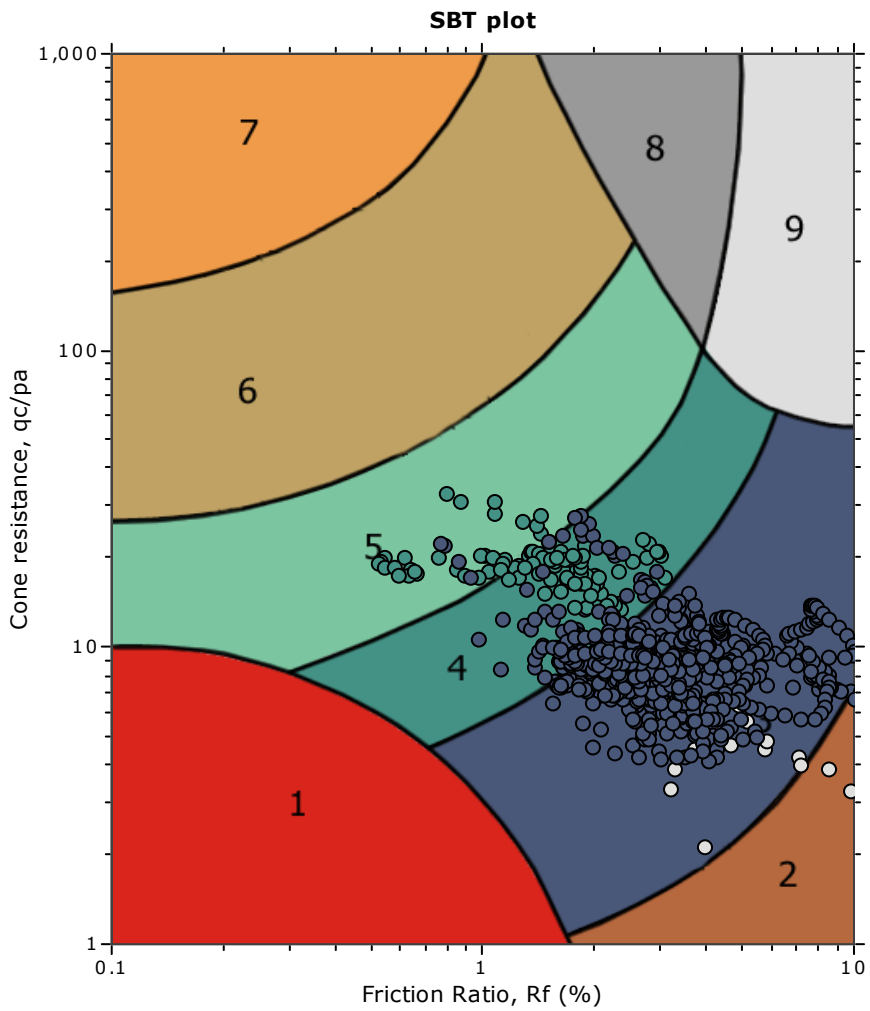
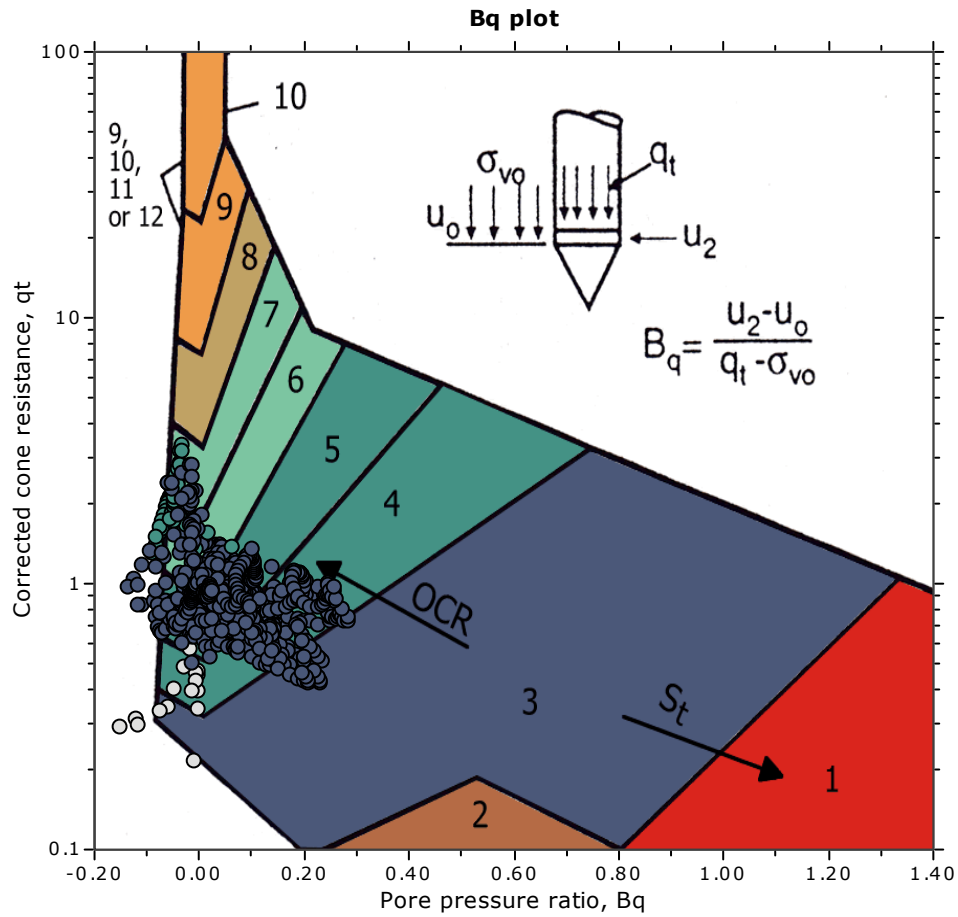
Project:
Location:

CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots





SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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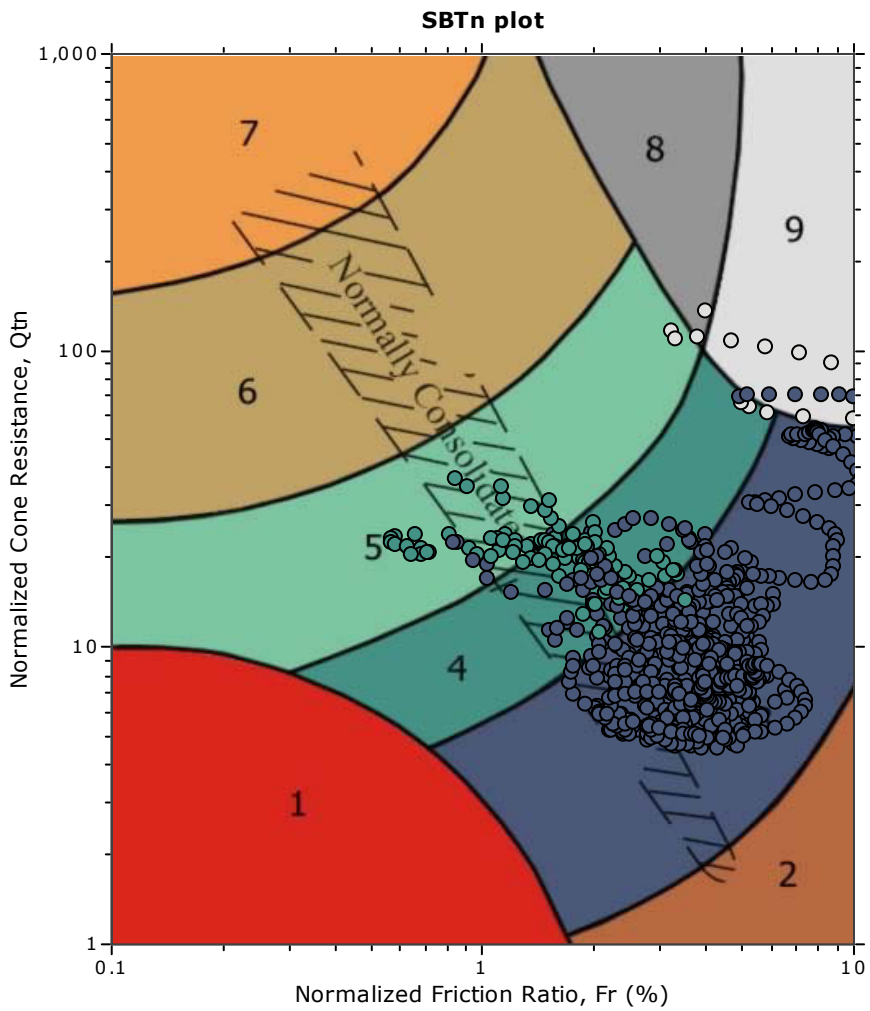
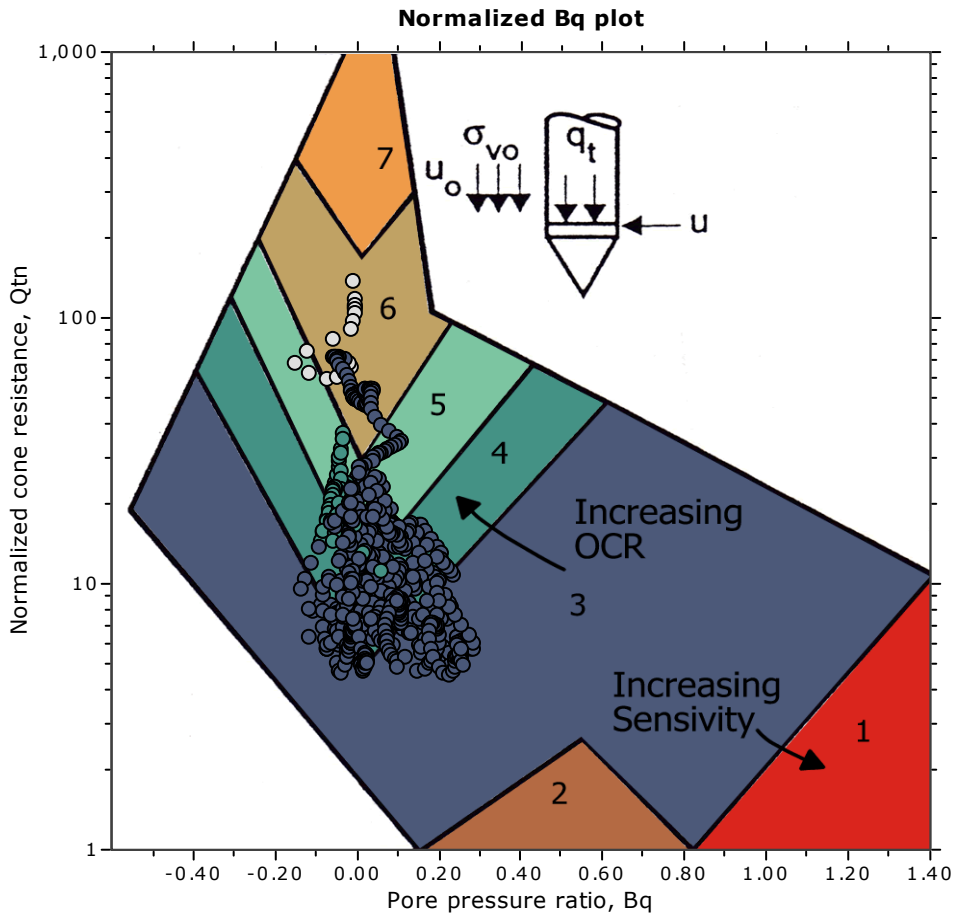
Project:
Location:

CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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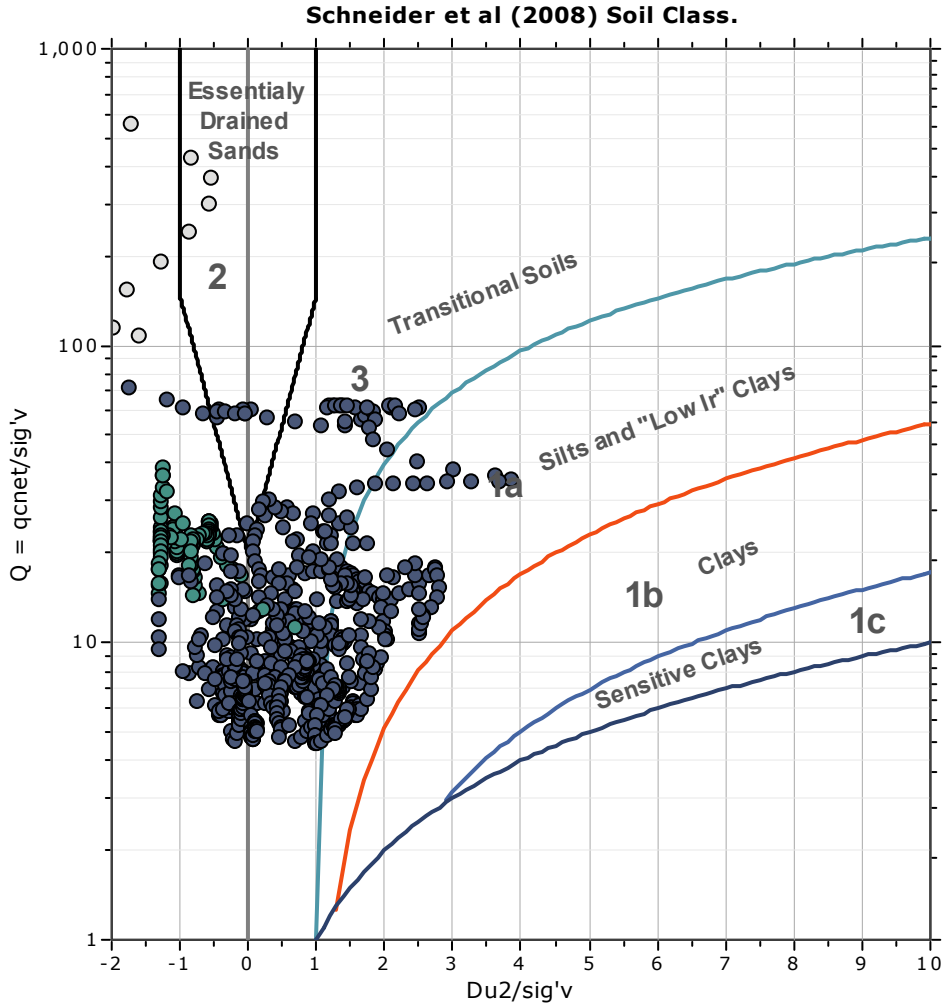
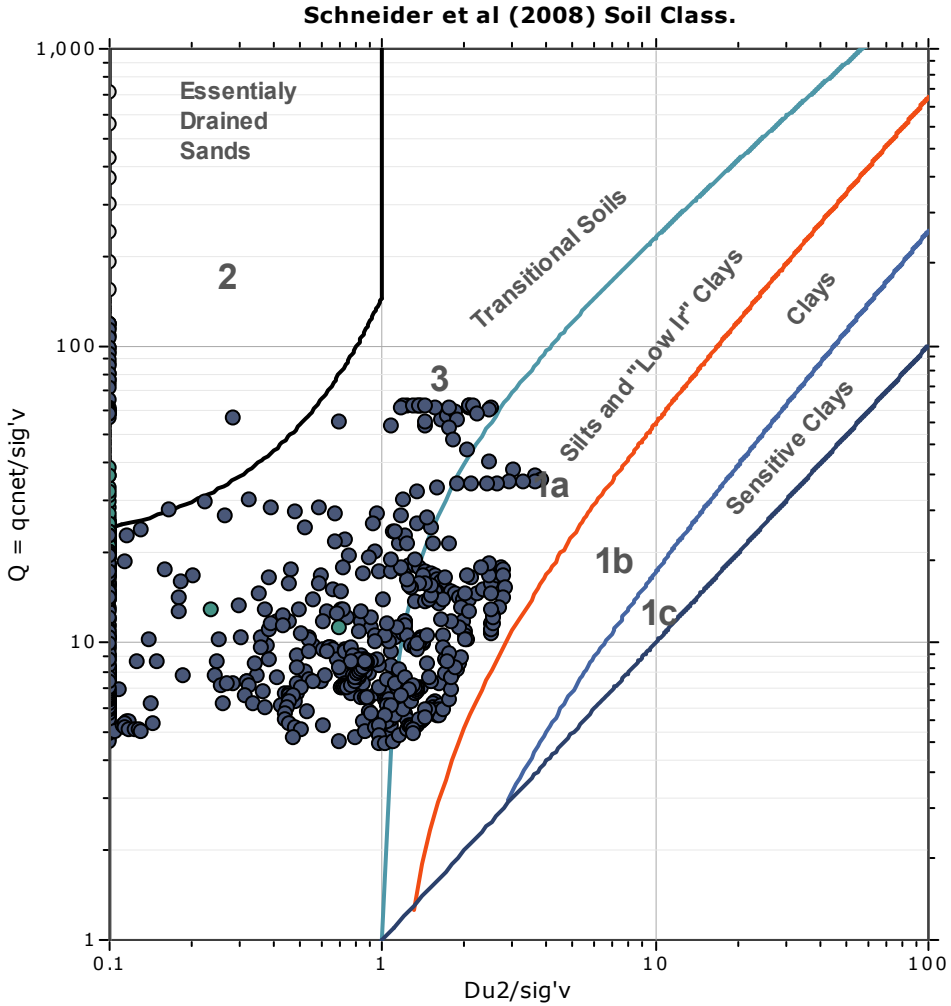
Project:
Location:

CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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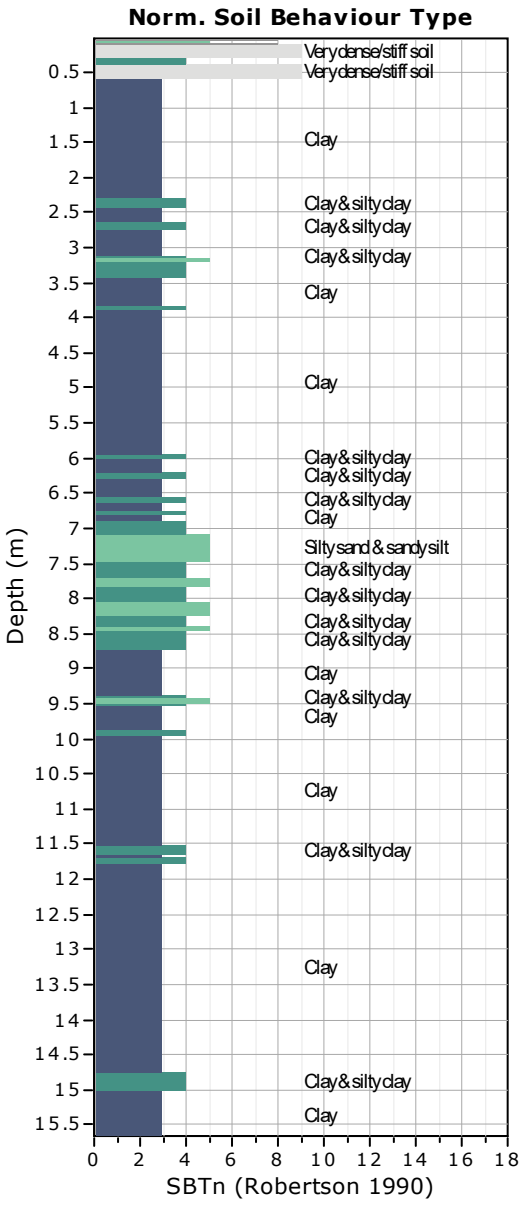
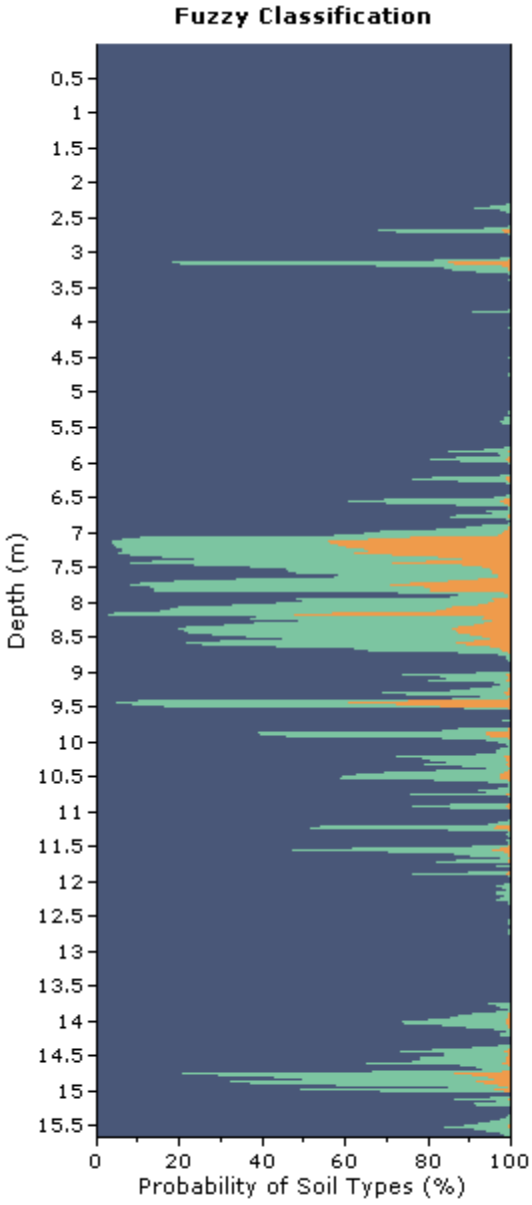
CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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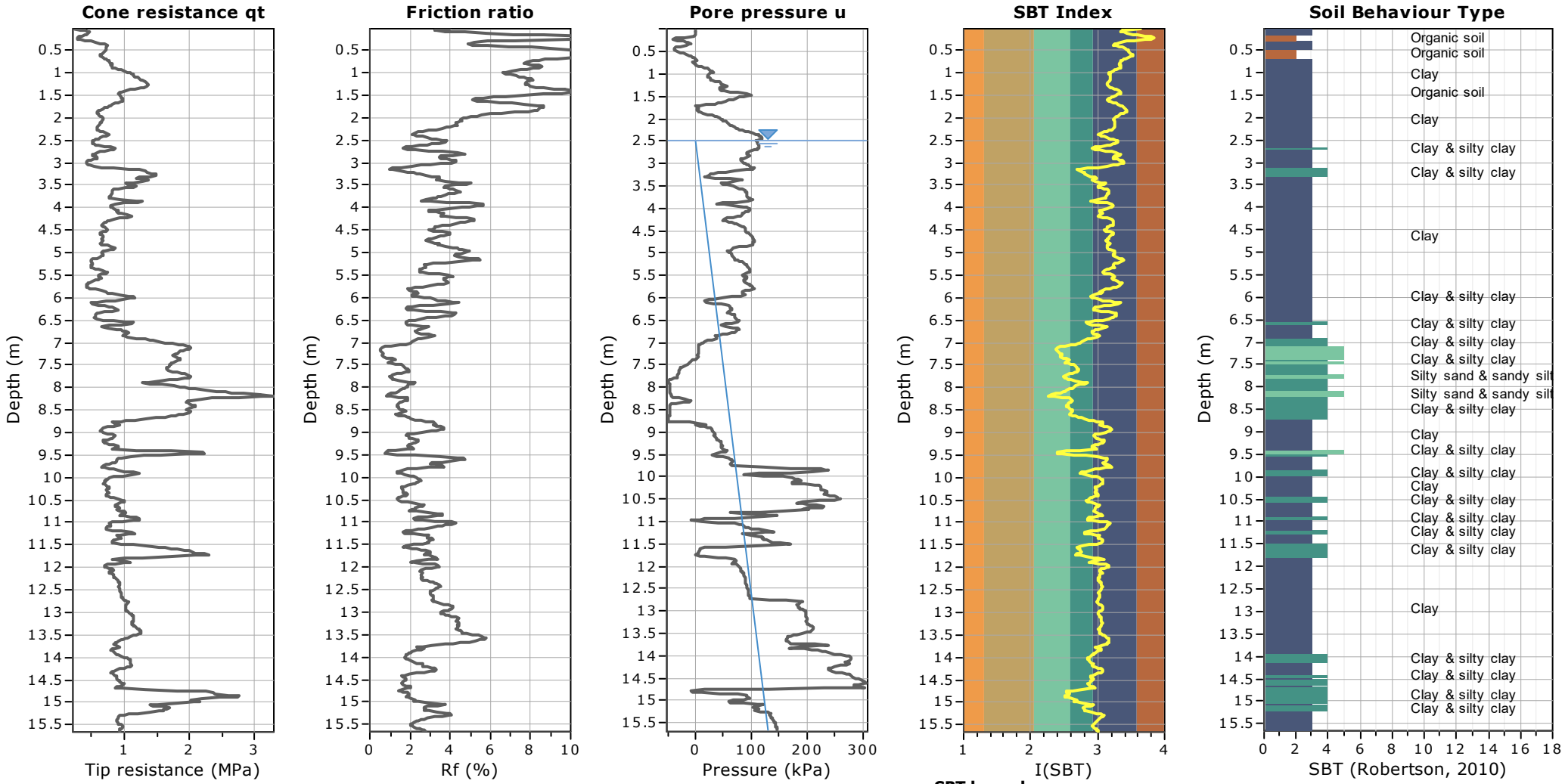
Project:
Location:

CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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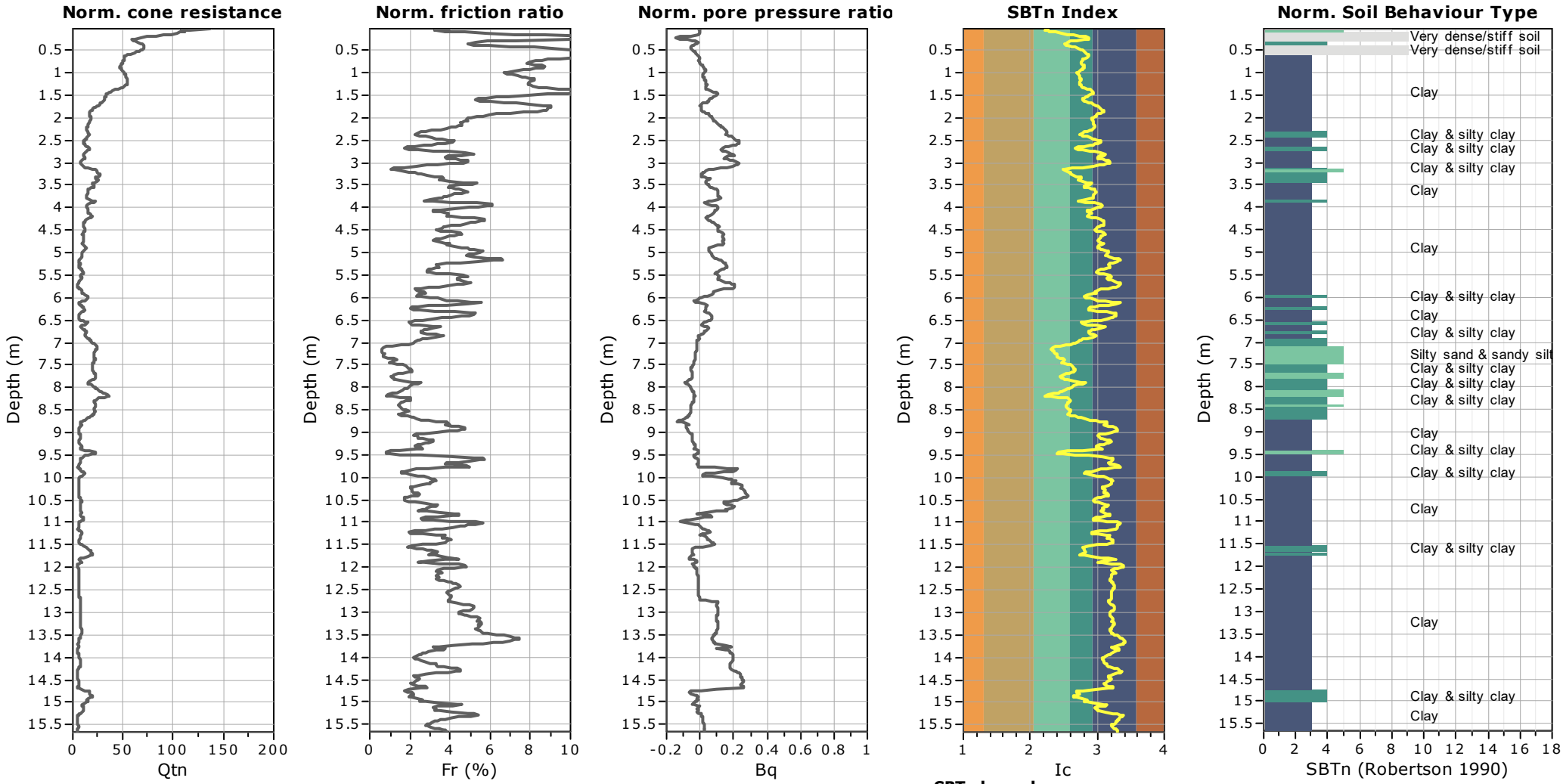
Project:
Location:

CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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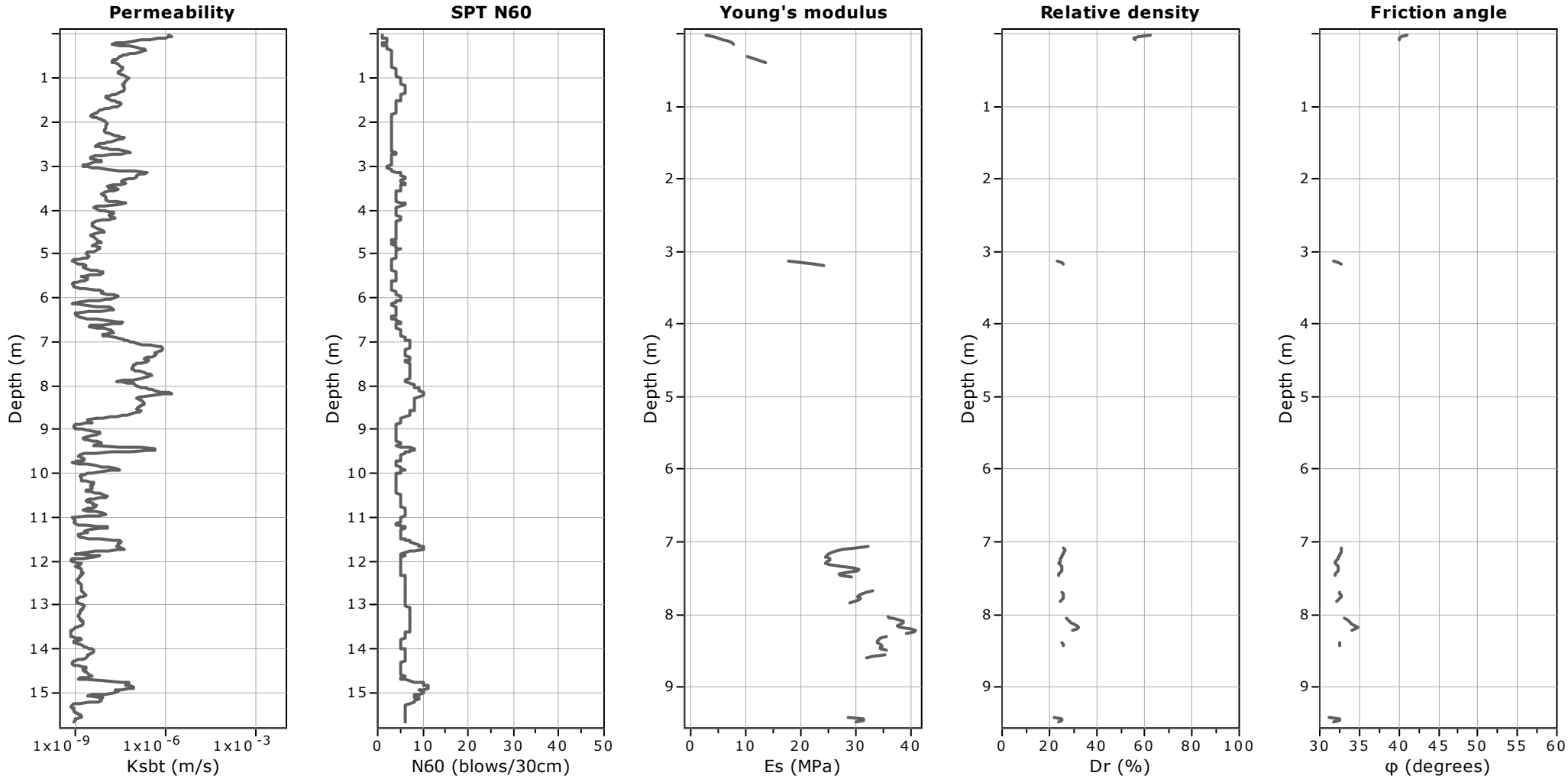
Project:
Location:

CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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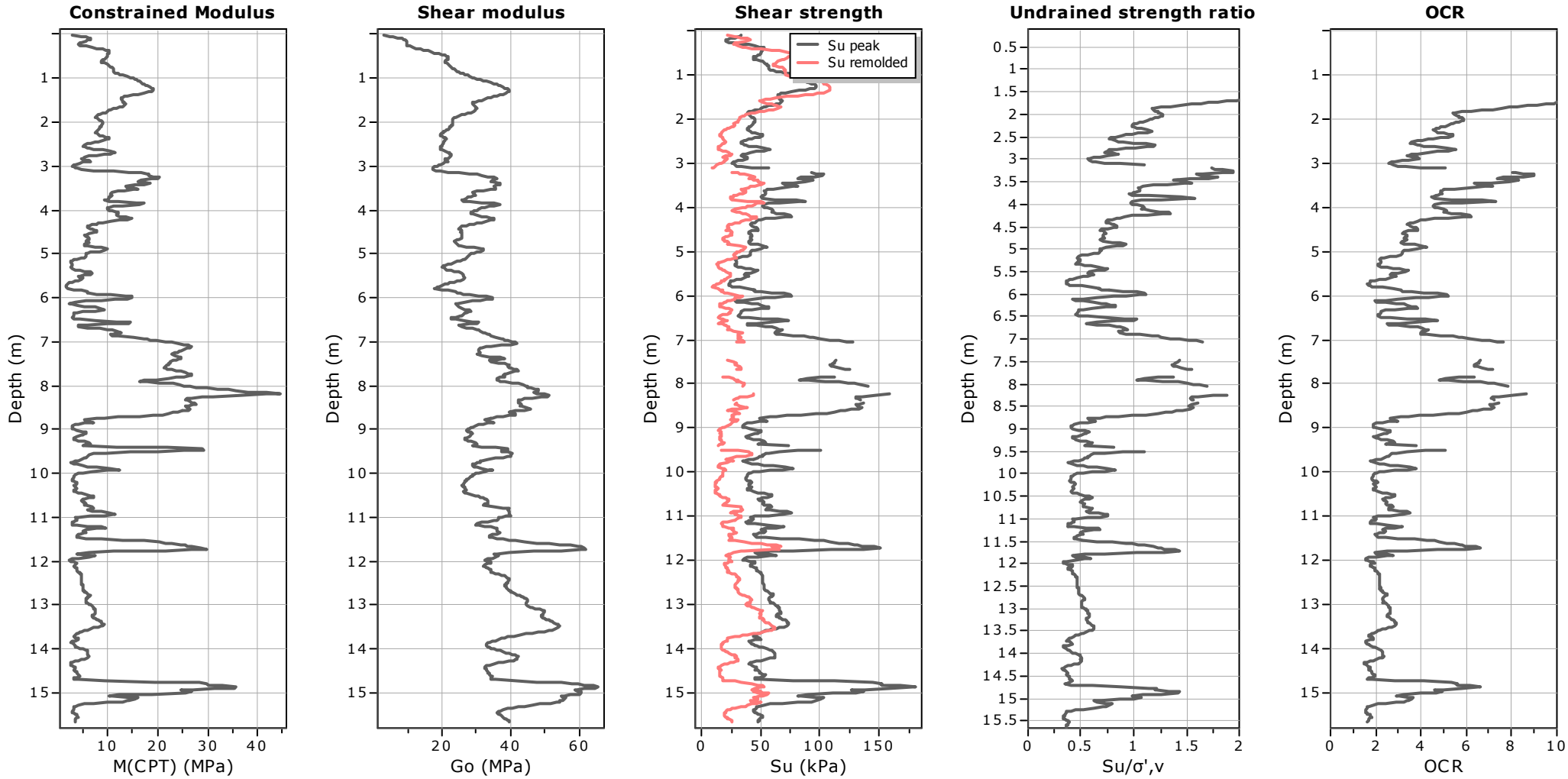
Project:
Location:

CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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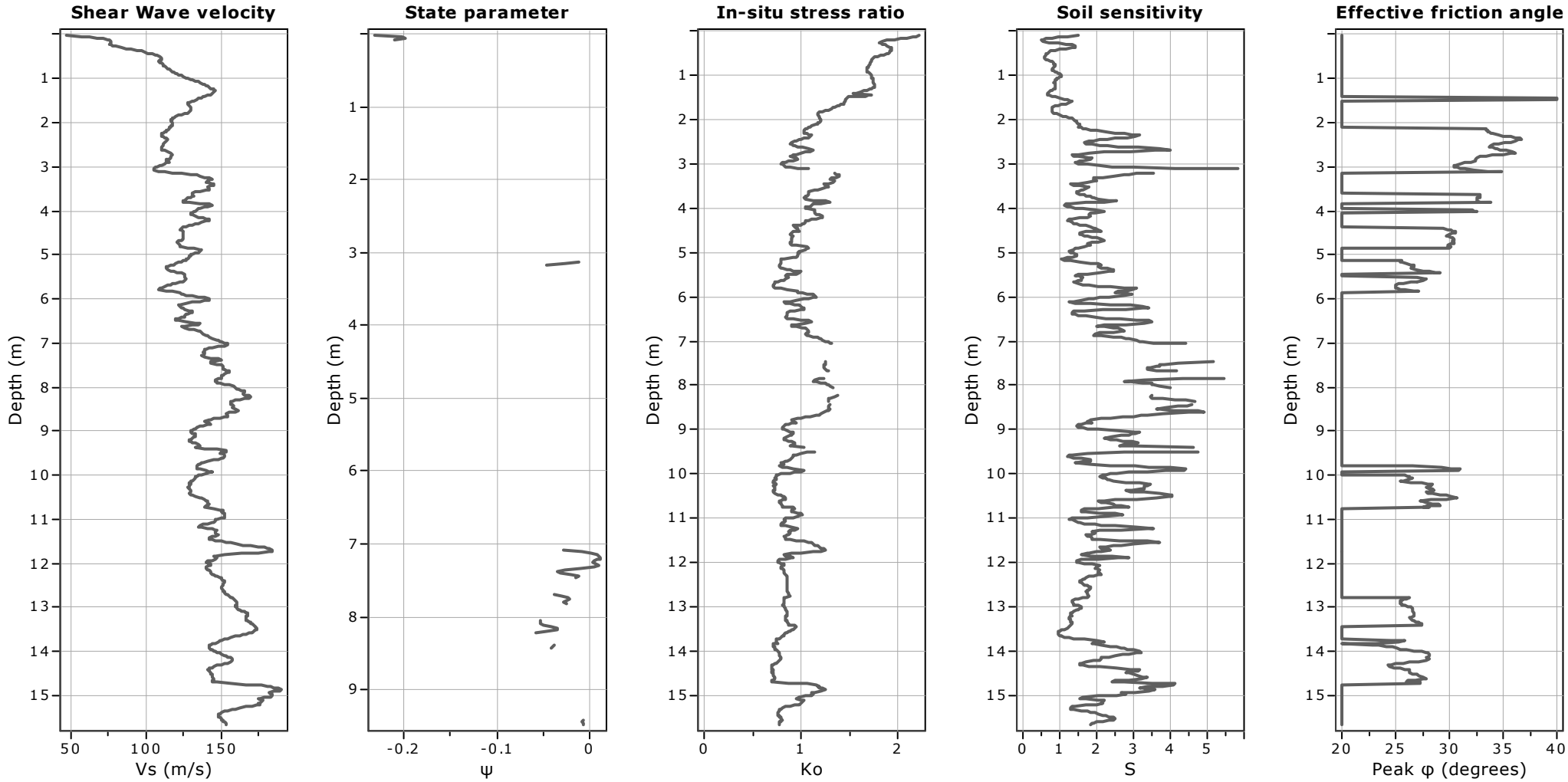
CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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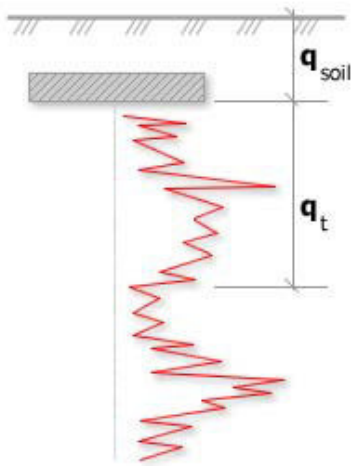
CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

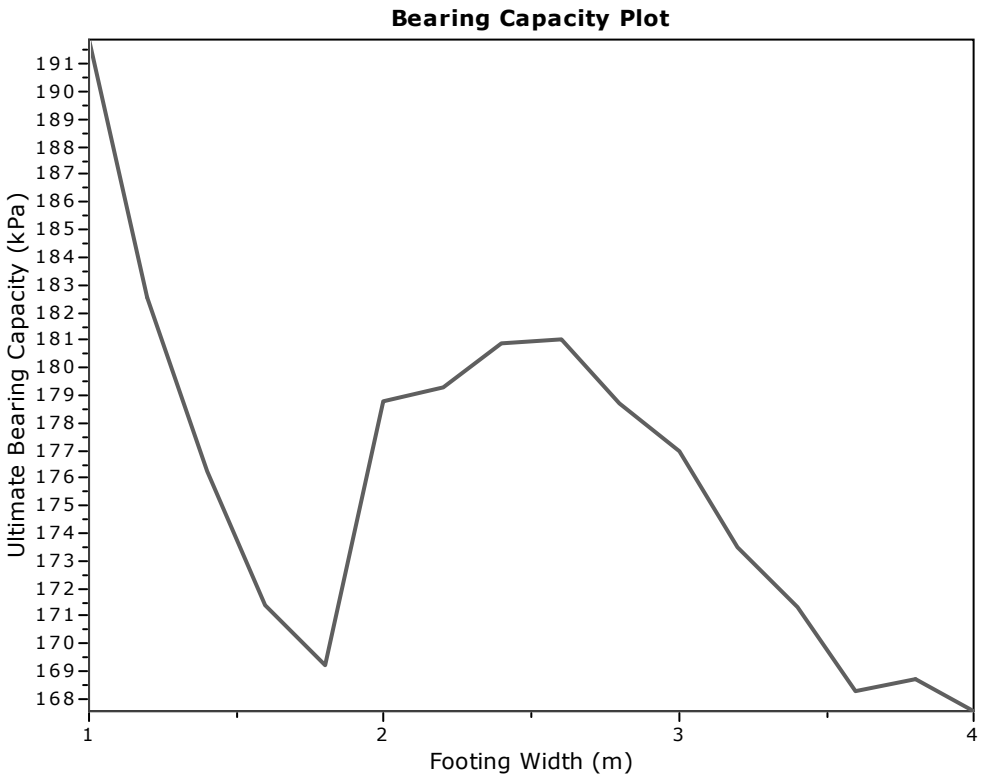
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	0.91	0.20	9.50	191.89
2	1.20	0.50	2.30	0.87	0.20	9.50	182.55
3	1.40	0.50	2.60	0.83	0.20	9.50	176.27
4	1.60	0.50	2.90	0.81	0.20	9.50	171.36
5	1.80	0.50	3.20	0.80	0.20	9.50	169.22
6	2.00	0.50	3.50	0.85	0.20	9.50	178.80
7	2.20	0.50	3.80	0.85	0.20	9.50	179.30
8	2.40	0.50	4.10	0.86	0.20	9.50	180.90
9	2.60	0.50	4.40	0.86	0.20	9.50	180.99
10	2.80	0.50	4.70	0.85	0.20	9.50	178.70
11	3.00	0.50	5.00	0.84	0.20	9.50	176.94
12	3.20	0.50	5.30	0.82	0.20	9.50	173.50
13	3.40	0.50	5.60	0.81	0.20	9.50	171.31
14	3.60	0.50	5.90	0.79	0.20	9.50	168.26
15	3.80	0.50	6.20	0.80	0.20	9.50	168.68
16	4.00	0.50	6.50	0.79	0.20	9.50	167.55

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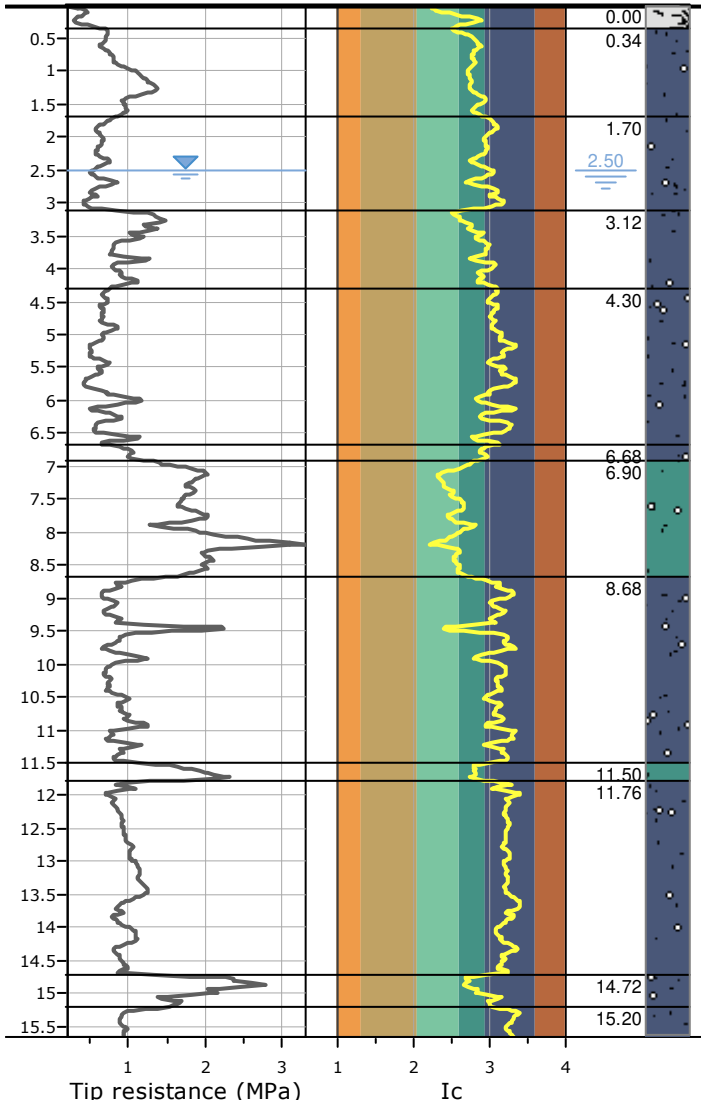
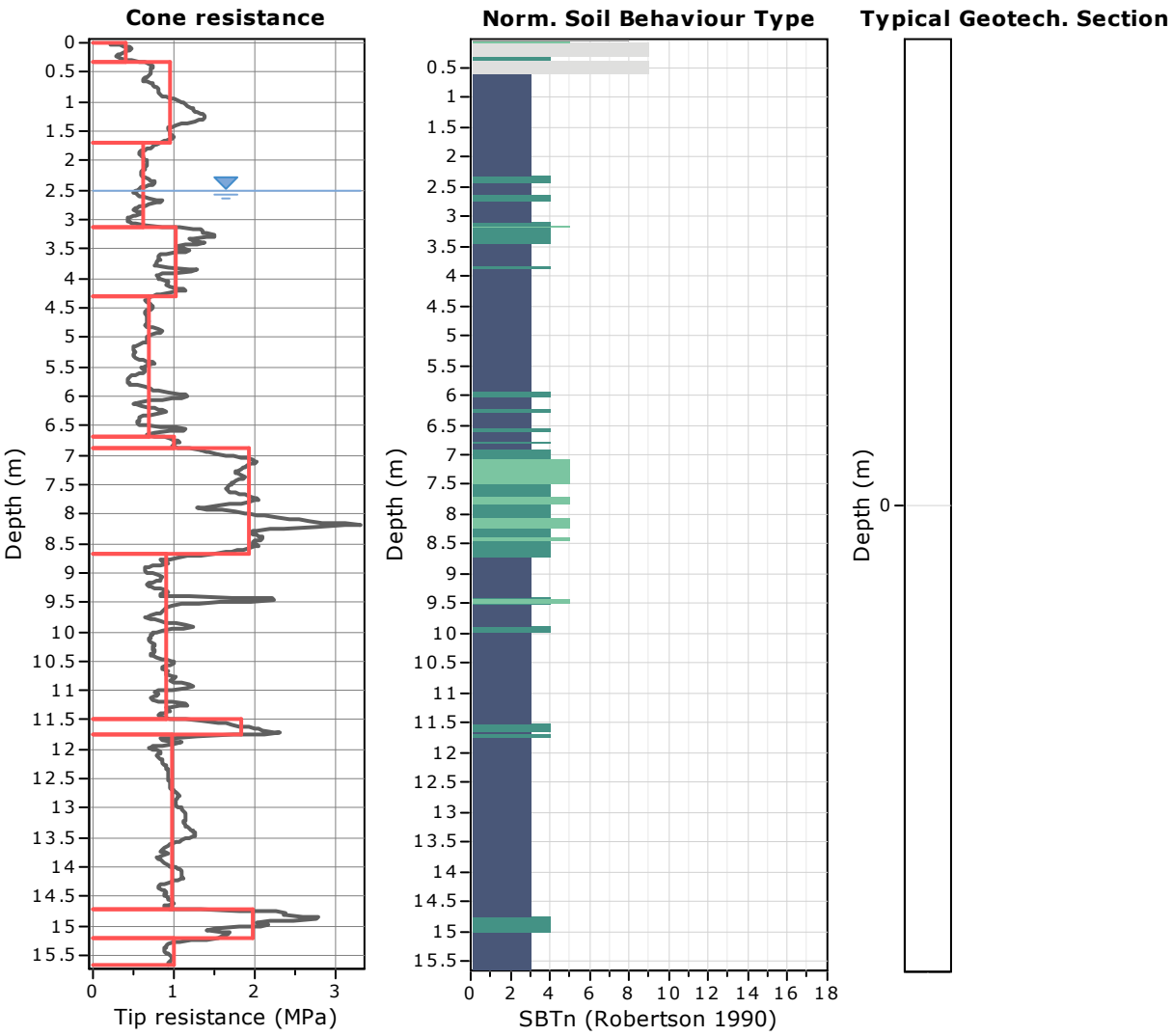
CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



Description	qt (MPa)	Ksbt (m/s)	N60	Es (MPa)	Dr	Phi (°)	M (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
Very dense/stiff soil	0.4	3.87E-7	1.5	8.6	-	-	5.5	9.3	29.4	5.5	25.3	16.3
Clay	0.9	4.02E-8	4.2	12.4	-	-	13.0	28.4	66.2	3.5	16.3	17.9
Clay	0.6	1.35E-8	3.1	-	-	-	7.6	22.1	41.6	1.0	4.8	16.4
Clay	1.0	3.61E-8	4.7	24.3	-	-	13.5	31.7	68.4	1.3	6.0	17.1
Clay	0.7	5.69E-9	3.8	-	-	-	5.8	25.9	42.1	0.7	3.1	16.3
Clay	1.0	1.22E-8	4.9	-	-	-	10.8	32.2	63.1	0.9	4.0	16.7
Clay & silty clay	1.9	2.48E-7	7.3	34.2	-	-	25.1	40.1	117.4	1.4	6.6	16.9
Clay	0.9	1.40E-8	4.9	-	-	-	6.2	32.5	51.0	0.5	2.5	16.4
Clay & silty clay	1.8	2.49E-8	8.4	-	-	-	22.3	52.4	117.2	1.1	5.2	17.6
Clay	1.0	1.78E-9	5.9	-	-	-	5.2	40.4	54.6	0.5	2.2	16.9
Clay	2.0	2.81E-8	9.2	-	-	-	22.0	57.5	123.9	1.0	4.5	17.6
Clay	1.0	1.31E-9	6.3	-	-	-	4.3	41.2	52.8	0.4	1.8	16.8



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.34 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 0.40 ±0.11 MPa	Permeability: 3.87E-07 ±5.03E-07 m/s	Constrained Mod.: 5.54 ±1.48 MPa
Sleeve friction: 27.38 ±10.39 kPa	N60: 1.53 ±0.51 blows	Go: 9.29 ±2.63 MPa
SBT_n: 9	Es: 8.64 ±1.88 MPa	Su: 29.35 ±7.58 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 5.47 ±1.25
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 25.26 ±5.78
	Unit weight: 16.33 ±0.57 kN/m³	

.:: Layer No: 2 ::.

Code: A1 **Start depth:** 0.34 (m), **End depth:** 1.70 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.94 ±0.23 MPa	Permeability: 4.02E-08 ±3.87E-08 m/s	Constrained Mod.: 12.98 ±3.12 MPa
Sleeve friction: 75.38 ±20.16 kPa	N60: 4.20 ±1.08 blows	Go: 28.37 ±6.98 MPa
SBT_n: 3	Es: 12.40 ±1.10 MPa	Su: 66.24 ±15.91 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 3.53 ±0.86
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 16.32 ±3.95
	Unit weight: 17.89 ±0.39 kN/m³	

.:: Layer No: 3 ::.

Code: D1 **Start depth:** 1.70 (m), **End depth:** 3.12 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.62 ±0.10 MPa	Permeability: 1.35E-08 ±1.55E-08 m/s	Constrained Mod.: 7.59 ±2.17 MPa
Sleeve friction: 26.06 ±14.28 kPa	N60: 3.07 ±0.42 blows	Go: 22.08 ±2.90 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 41.62 ±7.58 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.04 ±0.28
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.82 ±1.30
	Unit weight: 16.42 ±0.55 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 3.12 (m), **End depth:** 4.30 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.03 ±0.22 MPa	Permeability: 3.61E-08 ±5.03E-08 m/s	Constrained Mod.: 13.49 ±3.20 MPa
Sleeve friction: 36.49 ±10.10 kPa	N60: 4.67 ±0.75 blows	Go: 31.68 ±3.83 MPa
SBT_n: 3	Es: 24.26 ±24.26 MPa	Su: 68.43 ±15.92 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.29 ±0.31
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.98 ±1.42
	Unit weight: 17.07 ±0.41 kN/m³	

.:: Layer No: 5 ::.

Code: D2 **Start depth:** 4.30 (m), **End depth:** 6.68 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.68 ±0.16 MPa	Permeability: 5.69E-09 ±6.41E-09 m/s	Constrained Mod.: 5.79 ±2.98 MPa
Sleeve friction: 22.13 ±6.54 kPa	N60: 3.77 ±0.59 blows	Go: 25.91 ±3.29 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 42.09 ±11.31 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.66 ±0.17
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 3.06 ±0.79
	Unit weight: 16.35 ±0.38 kN/m³	

.:: Layer No: 6 ::.

Code: A3 **Start depth:** 6.68 (m), **End depth:** 6.90 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 1.00 ±0.11 MPa	Permeability: 1.22E-08 ±4.59E-09 m/s	Constrained Mod.: 10.85 ±2.31 MPa
Sleeve friction: 26.47 ±4.55 kPa	N60: 4.92 ±0.51 blows	Go: 32.19 ±2.44 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 63.05 ±7.62 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.87 ±0.10
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.03 ±0.46
	Unit weight: 16.74 ±0.22 kN/m³	

.:: Layer No: 7 ::.

Code: B1 **Start depth:** 6.90 (m), **End depth:** 8.68 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 1.92 ±0.37 MPa	Permeability: 2.48E-07 ±2.64E-07 m/s	Constrained Mod.: 25.08 ±5.14 MPa
Sleeve friction: 26.84 ±8.62 kPa	N60: 7.31 ±1.05 blows	Go: 40.09 ±5.08 MPa
SBT_n: 4	Es: 34.23 ±2.80 MPa	Su: 117.41 ±17.43 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.43 ±0.18
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.63 ±0.83
	Unit weight: 16.95 ±0.44 kN/m³	

.:: Layer No: 8 ::.

Code: A4 **Start depth:** 8.68 (m), **End depth:** 11.50 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.92 ±0.26 MPa	Permeability: 1.40E-08 ±5.56E-08 m/s	Constrained Mod.: 6.25 ±4.59 MPa
Sleeve friction: 21.72 ±7.39 kPa	N60: 4.87 ±0.88 blows	Go: 32.53 ±4.31 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 50.95 ±12.45 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.54 ±0.14
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.49 ±0.63
	Unit weight: 16.43 ±0.39 kN/m³	

.:: Layer No: 9 ::.

Code: B2 **Start depth:** 11.50 (m), **End depth:** 11.76 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 1.84 ±0.34 MPa	Permeability: 2.49E-08 ±8.34E-09 m/s	Constrained Mod.: 22.29 ±6.00 MPa
Sleeve friction: 47.32 ±16.88 kPa	N60: 8.36 ±1.45 blows	Go: 52.41 ±8.68 MPa
SBT_n: 4	Es: 0.00 ±0.00 MPa	Su: 117.24 ±24.15 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.12 ±0.23
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 5.15 ±1.04
	Unit weight: 17.56 ±0.51 kN/m³	

.:: Layer No: 10 ::.

Code: A5 **Start depth:** 11.76 (m), **End depth:** 14.72 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.99 ±0.15 MPa	Permeability: 1.78E-09 ±1.40E-09 m/s	Constrained Mod.: 5.20 ±2.22 MPa
Sleeve friction: 31.68 ±13.30 kPa	N60: 5.86 ±0.76 blows	Go: 40.42 ±6.48 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 54.60 ±10.40 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.47 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.17 ±0.44
	Unit weight: 16.86 ±0.50 kN/m³	

.:: Layer No: 11 ::.

Code: B3 **Start depth:** 14.72 (m), **End depth:** 15.20 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.99 ±0.44 MPa	Permeability: 2.81E-08 ±2.53E-08 m/s	Constrained Mod.: 21.99 ±8.57 MPa
Sleeve friction: 44.99 ±8.45 kPa	N60: 9.24 ±1.20 blows	Go: 57.46 ±5.13 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 123.91 ±31.60 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.97 ±0.26
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 4.48 ±1.20
	Unit weight: 17.60 ±0.27 kN/m³	

.:: Layer No: 12 ::.

Code: A6 **Start depth:** 15.20 (m), **End depth:** 15.66 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 1.00 ±0.17 MPa	Permeability: 1.31E-09 ±9.84E-10 m/s	Constrained Mod.: 4.34 ±2.44 MPa
Sleeve friction: 28.40 ±9.89 kPa	N60: 6.26 ±0.62 blows	Go: 41.24 ±5.72 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 52.78 ±12.15 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.40 ±0.09
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 1.84 ±0.44
	Unit weight: 16.77 ±0.40 kN/m³	

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Project:
Location:

CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.34	3.87E-07	1.5	8.6	0.0	0.0	5.5	9.3	29.4	5.5	25.3	16.3
0.34		(±5.03E-07)	(±0.5)	(±1.9)	(±0.0)	(±0.0)	(±1.5)	(±2.6)	(±7.6)	(±1.3)	(±5.8)	(±0.6)
0.34	1.36	4.02E-08	4.2	12.4	0.0	0.0	13.0	28.4	66.2	3.5	16.3	17.9
1.70		(±3.87E-08)	(±1.1)	(±1.1)	(±0.0)	(±0.0)	(±3.1)	(±7.0)	(±15.9)	(±0.9)	(±4.0)	(±0.4)
1.70	1.42	1.35E-08	3.1	0.0	0.0	0.0	7.6	22.1	41.6	1.0	4.8	16.4
3.12		(±1.55E-08)	(±0.4)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±2.9)	(±7.6)	(±0.3)	(±1.3)	(±0.5)
3.12	1.18	3.61E-08	4.7	24.3	0.0	0.0	13.5	31.7	68.4	1.3	6.0	17.1
4.30		(±5.03E-08)	(±0.8)	(±24.3)	(±0.0)	(±0.0)	(±3.2)	(±3.8)	(±15.9)	(±0.3)	(±1.4)	(±0.4)
4.30	2.38	5.69E-09	3.8	0.0	0.0	0.0	5.8	25.9	42.1	0.7	3.1	16.3
6.68		(±6.41E-09)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±3.0)	(±3.3)	(±11.3)	(±0.2)	(±0.8)	(±0.4)
6.68	0.22	1.22E-08	4.9	0.0	0.0	0.0	10.8	32.2	63.1	0.9	4.0	16.7
6.90		(±4.59E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±2.3)	(±2.4)	(±7.6)	(±0.1)	(±0.5)	(±0.2)
6.90	1.78	2.48E-07	7.3	34.2	0.0	0.0	25.1	40.1	117.4	1.4	6.6	16.9
8.68		(±2.64E-07)	(±1.0)	(±2.8)	(±0.0)	(±0.0)	(±5.1)	(±5.1)	(±17.4)	(±0.2)	(±0.8)	(±0.4)
8.68	2.82	1.40E-08	4.9	0.0	0.0	0.0	6.2	32.5	51.0	0.5	2.5	16.4
11.50		(±5.56E-08)	(±0.9)	(±0.0)	(±0.0)	(±0.0)	(±4.6)	(±4.3)	(±12.4)	(±0.1)	(±0.6)	(±0.4)
11.50	0.26	2.49E-08	8.4	0.0	0.0	0.0	22.3	52.4	117.2	1.1	5.2	17.6
11.76		(±8.34E-09)	(±1.4)	(±0.0)	(±0.0)	(±0.0)	(±6.0)	(±8.7)	(±24.2)	(±0.2)	(±1.0)	(±0.5)
11.76	2.96	1.78E-09	5.9	0.0	0.0	0.0	5.2	40.4	54.6	0.5	2.2	16.9
14.72		(±1.40E-09)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±2.2)	(±6.5)	(±10.4)	(±0.1)	(±0.4)	(±0.5)
14.72	0.48	2.81E-08	9.2	0.0	0.0	0.0	22.0	57.5	123.9	1.0	4.5	17.6
15.20		(±2.53E-08)	(±1.2)	(±0.0)	(±0.0)	(±0.0)	(±8.6)	(±5.1)	(±31.6)	(±0.3)	(±1.2)	(±0.3)

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CPT: CPTu-07
Total depth: 15.66 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
15.20	0.46	1.31E-09	6.3	0.0	0.0	0.0	4.3	41.2	52.8	0.4	1.8	16.8
15.66		(±9.84E-10)	(±0.6)	(±0.0)	(±0.0)	(±0.0)	(±2.4)	(±5.7)	(±12.2)	(±0.1)	(±0.4)	(±0.4)

Depth values presented in this table are measured from free ground surface

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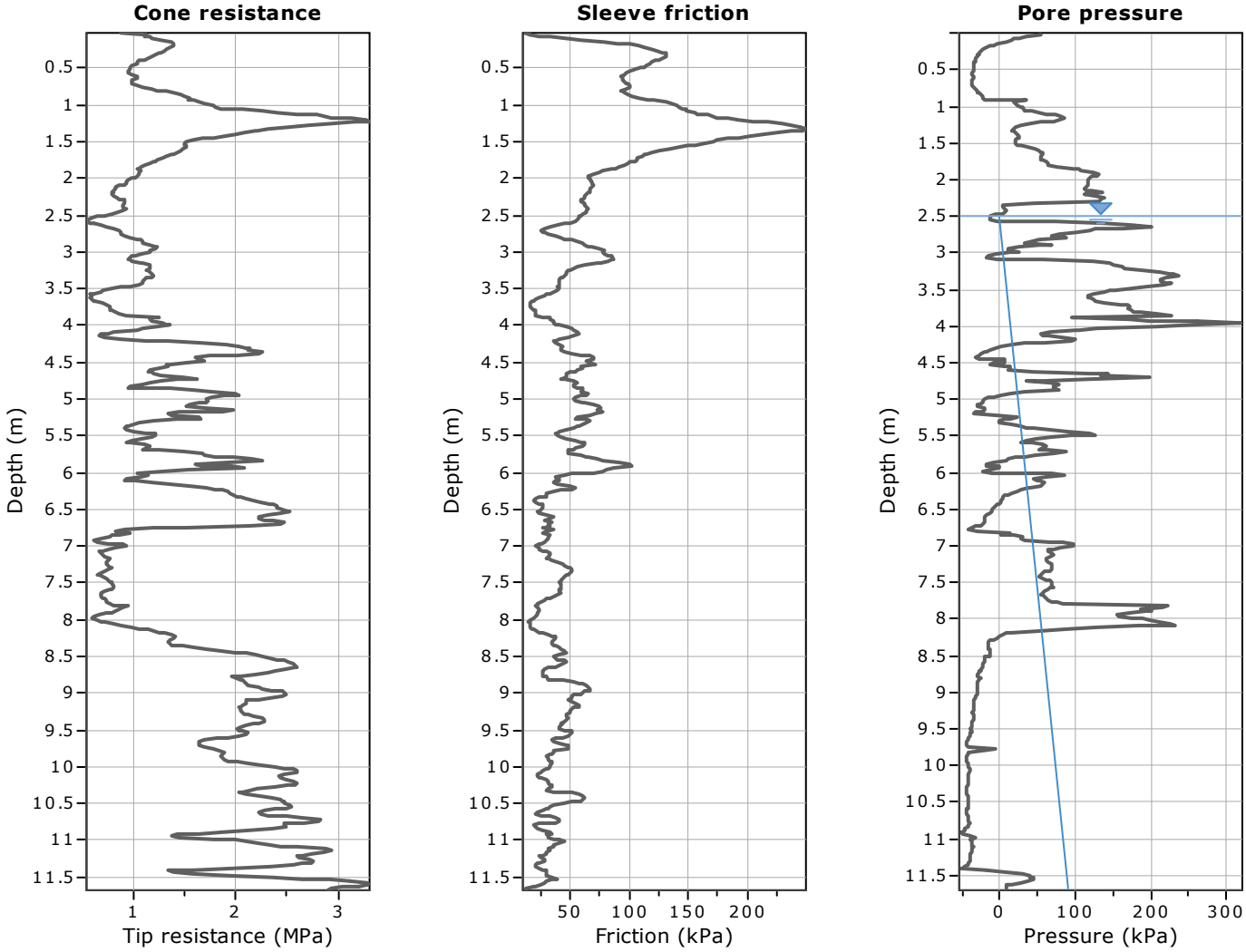
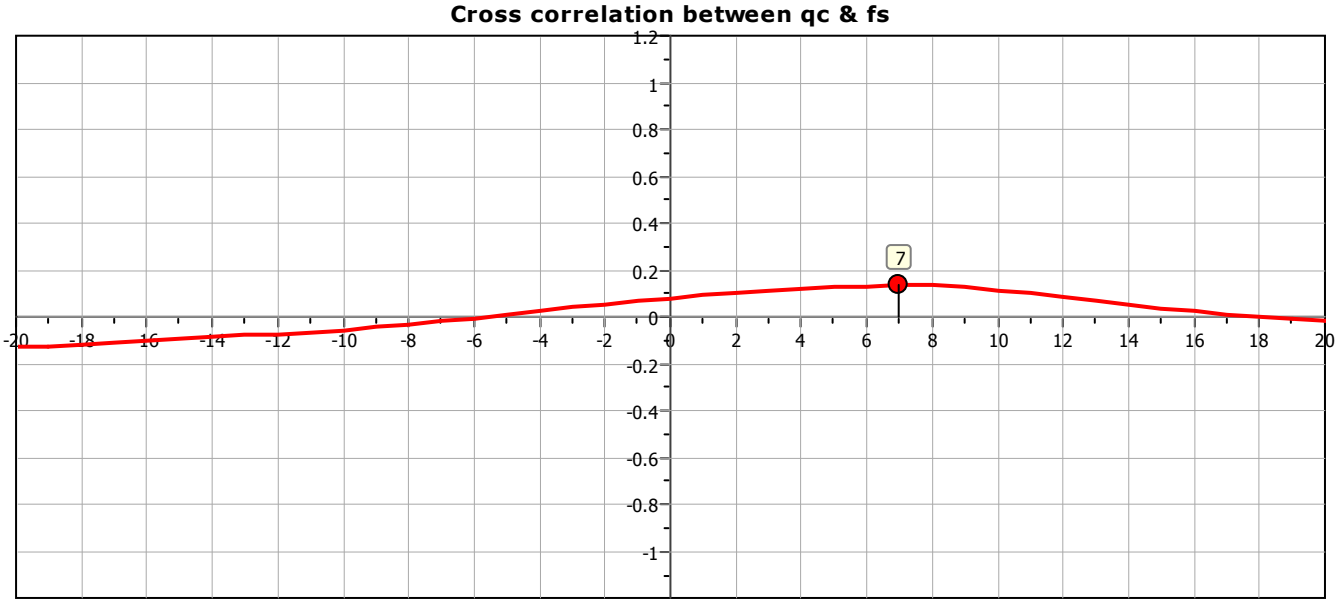
CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



The plot below presents the cross correlation coeficient between the raw qc and fs values (as measured on the field). X axes presents the lag distance (one lag is the distance between two sucessive CPT measurements).



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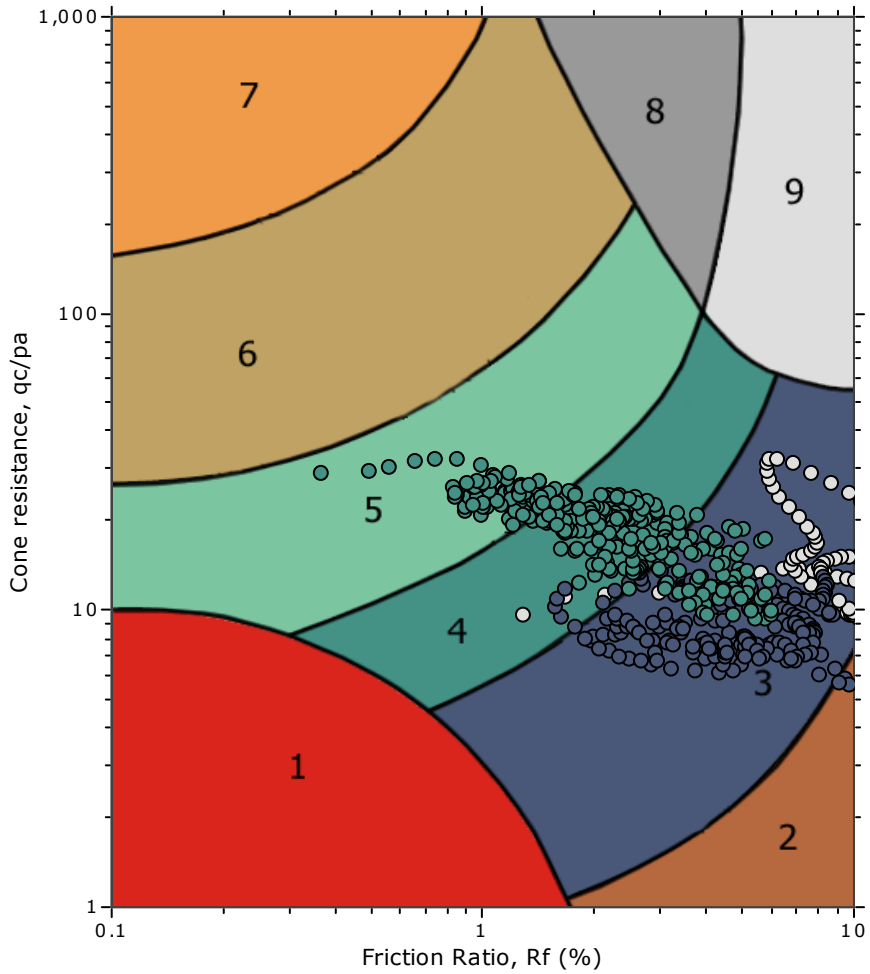
Project:
Location:

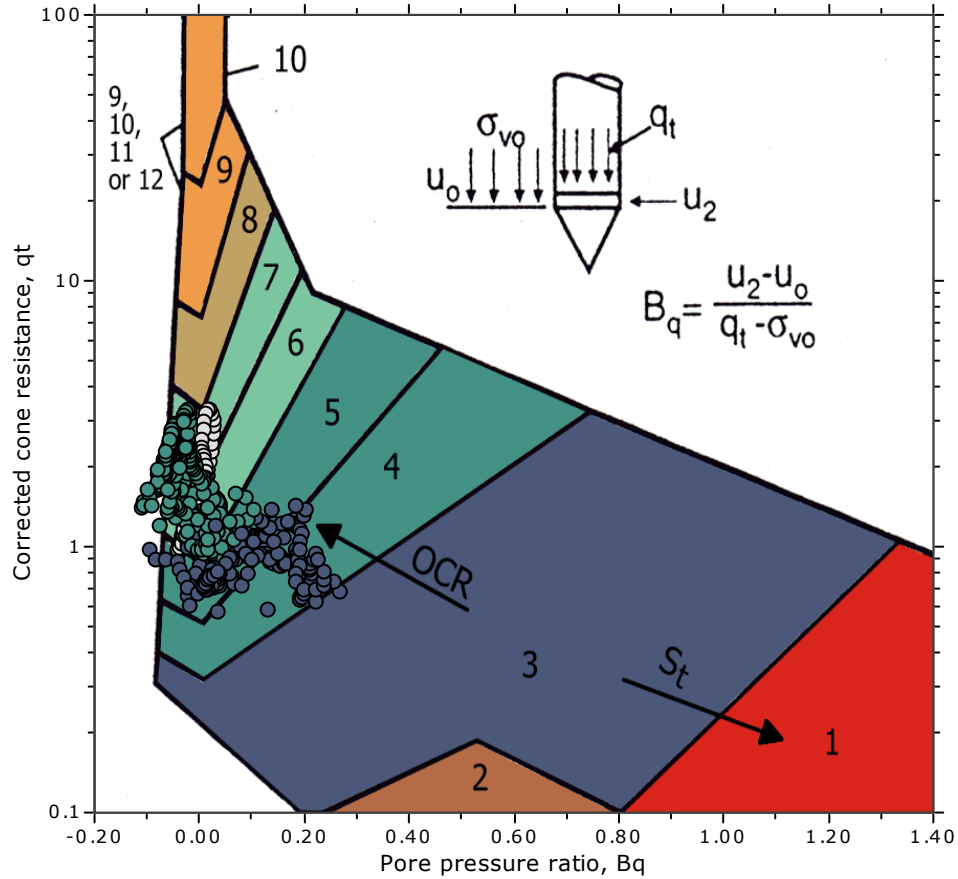
CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots

SBT plot



Bq plot



SBT legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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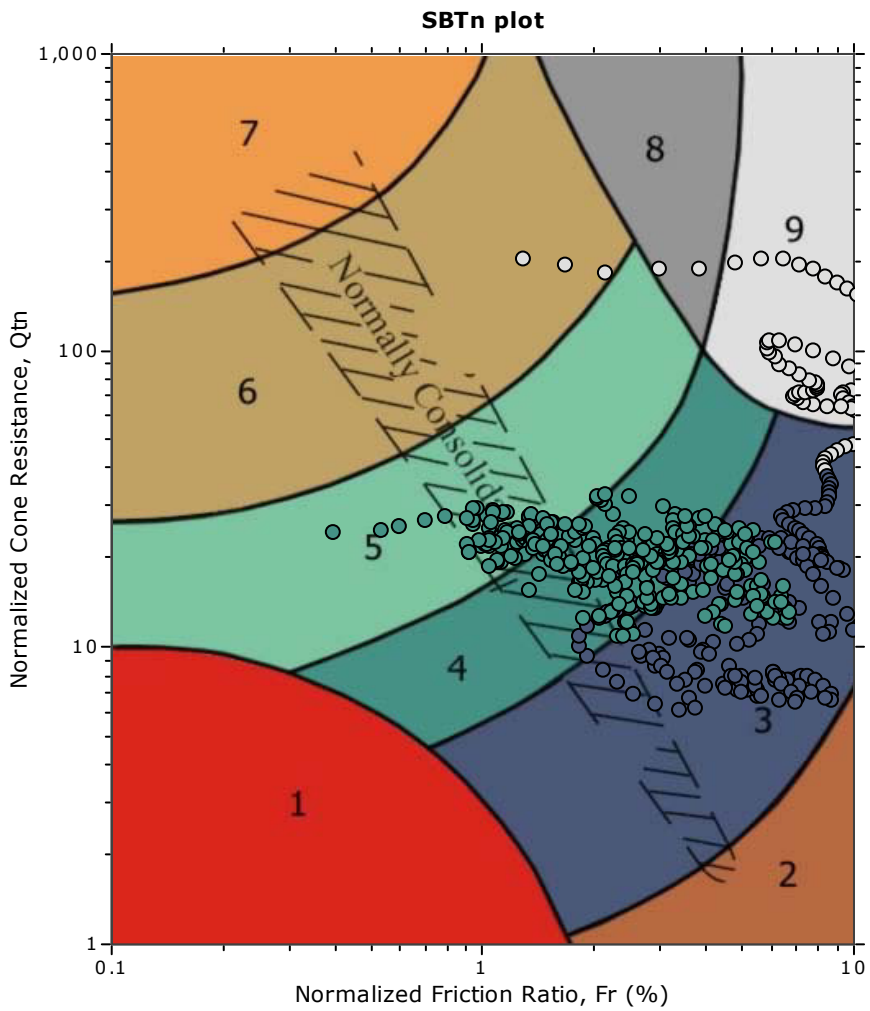
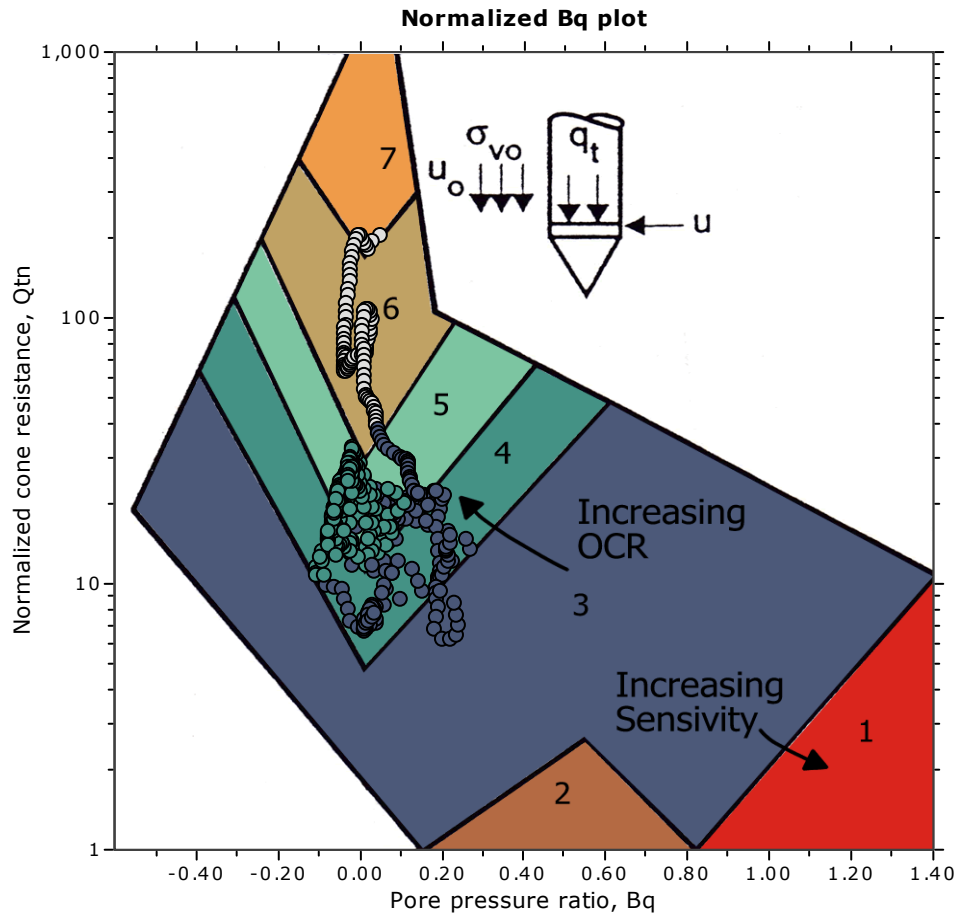
Project:
Location:

CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

SBT - Bq plots (normalized)





SBTn legend

- 1. Sensitive fine grained
- 2. Organic material
- 3. Clay to silty clay
- 4. Clayey silt to silty clay
- 5. Silty sand to sandy silt
- 6. Clean sand to silty sand
- 7. Gravely sand to sand
- 8. Very stiff sand to clayey sand
- 9. Very stiff fine grained

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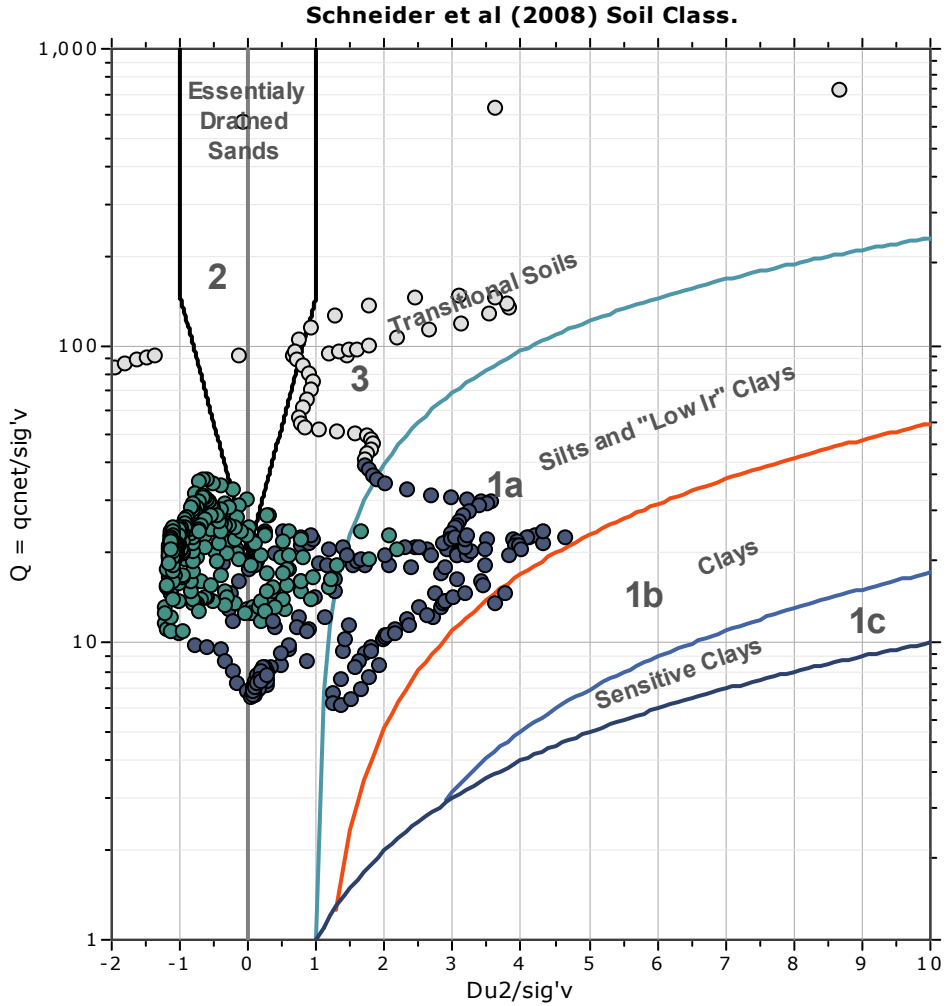
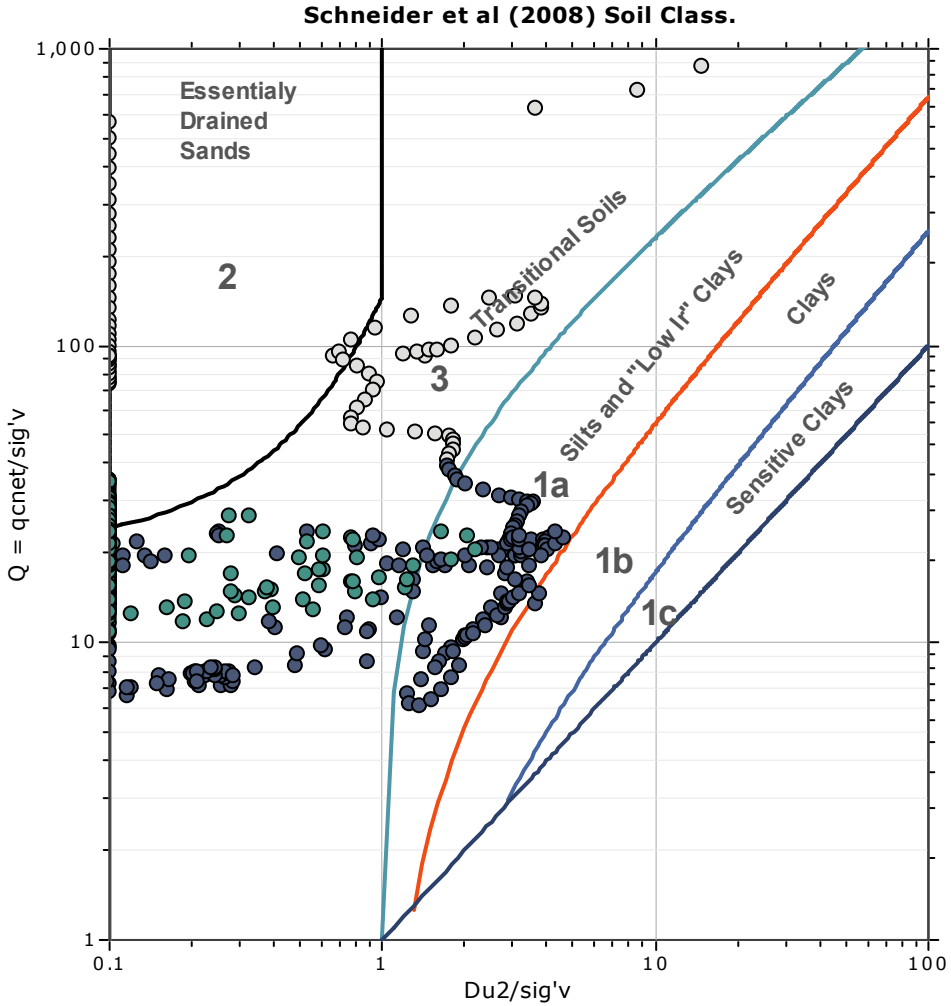
Project:
Location:

CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Bq plots (Schneider)





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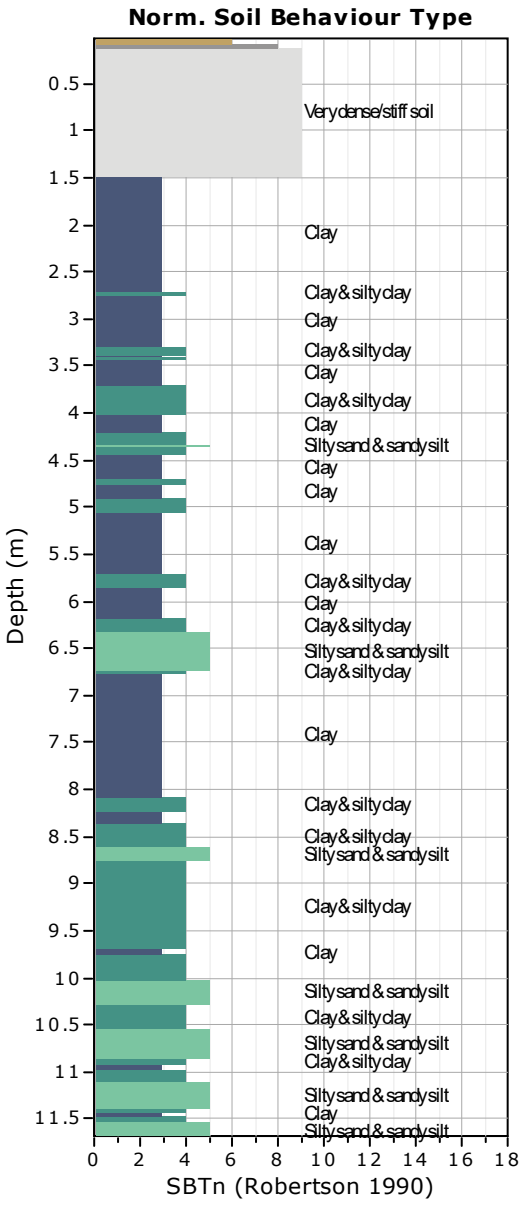
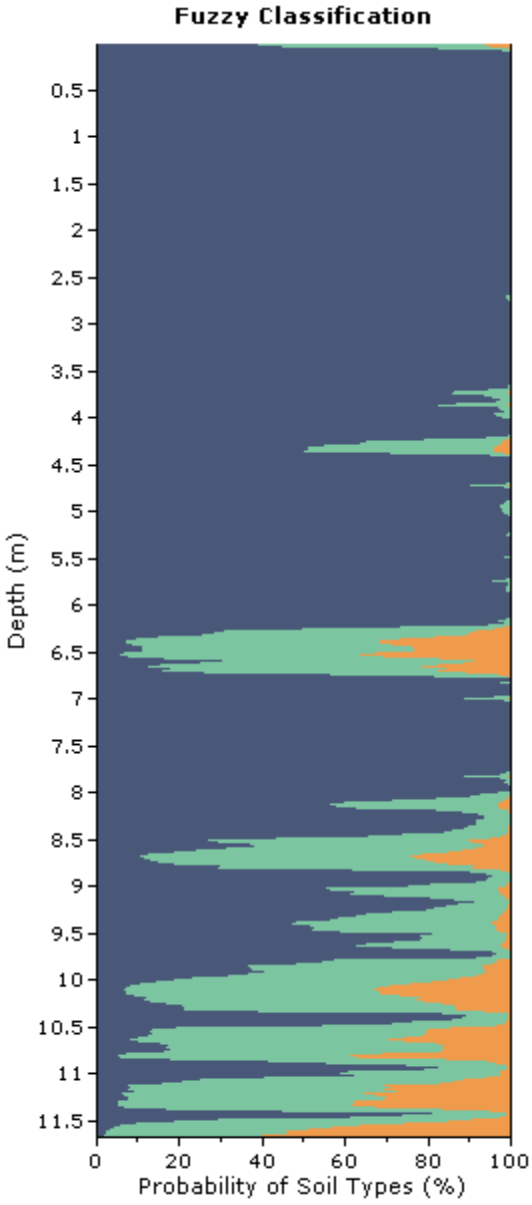
CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:





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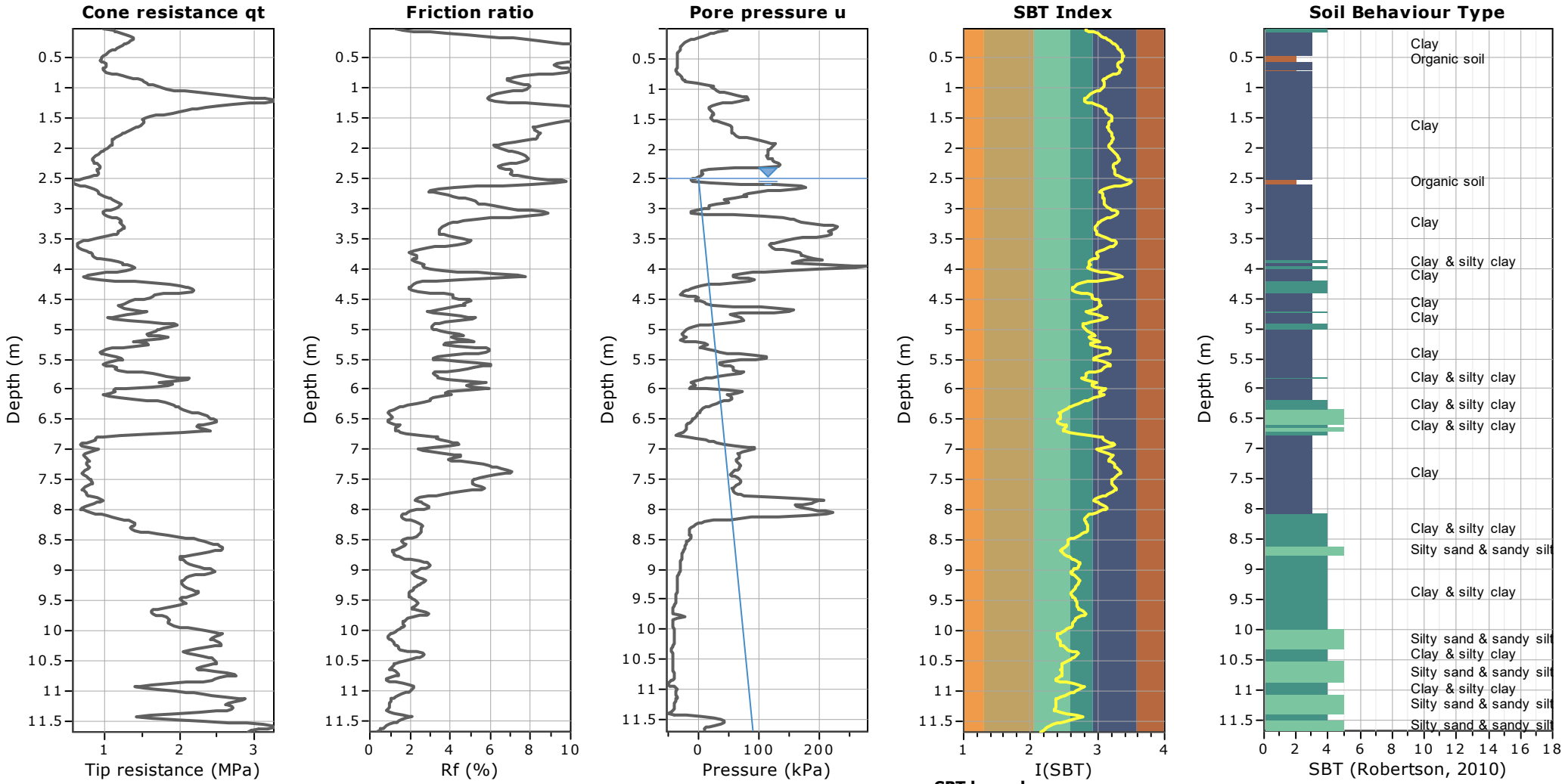
Project:
Location:

CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty clay
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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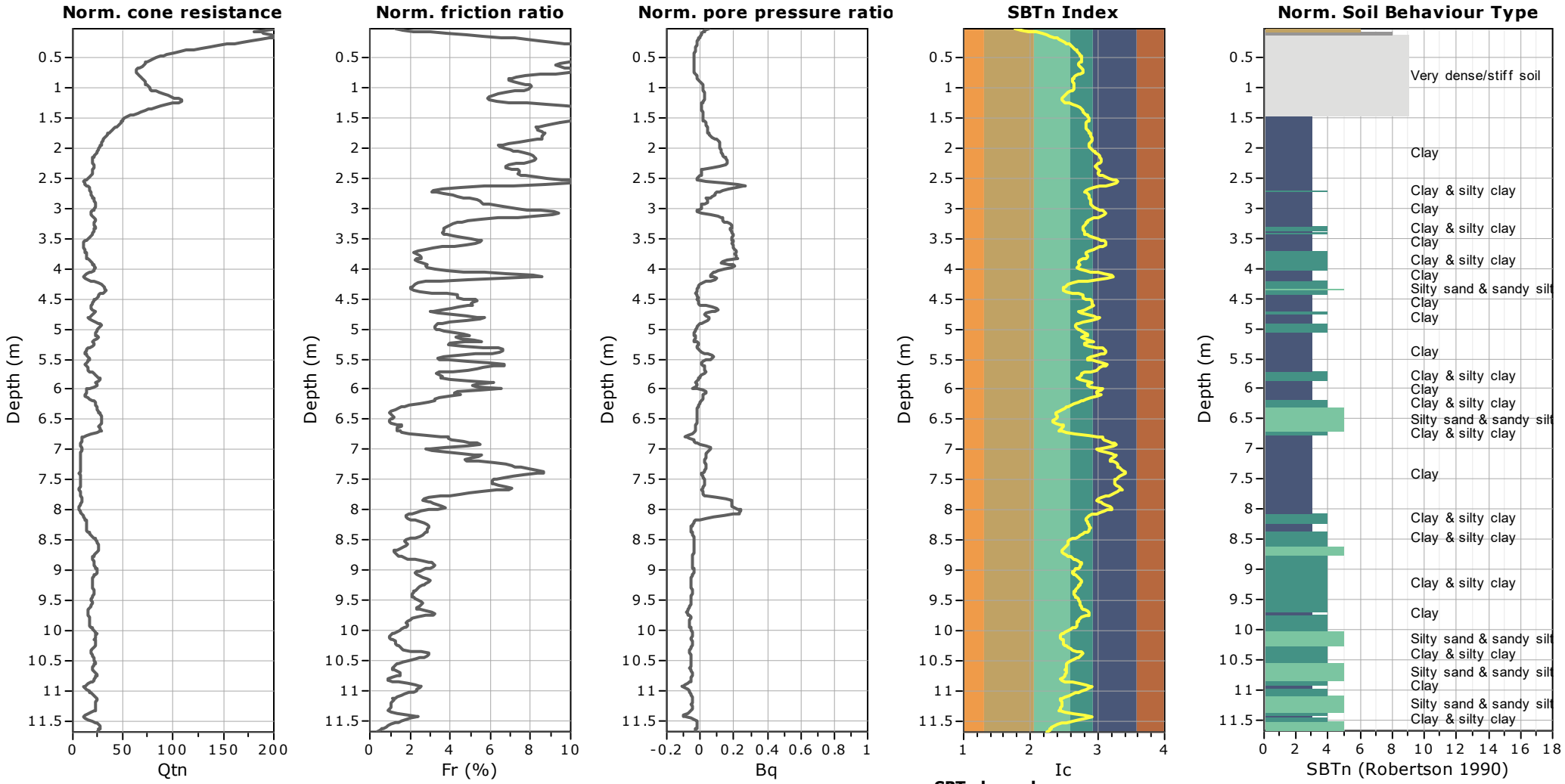
Project:
Location:

CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
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5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to clayey sand
9. Very stiff fine grained

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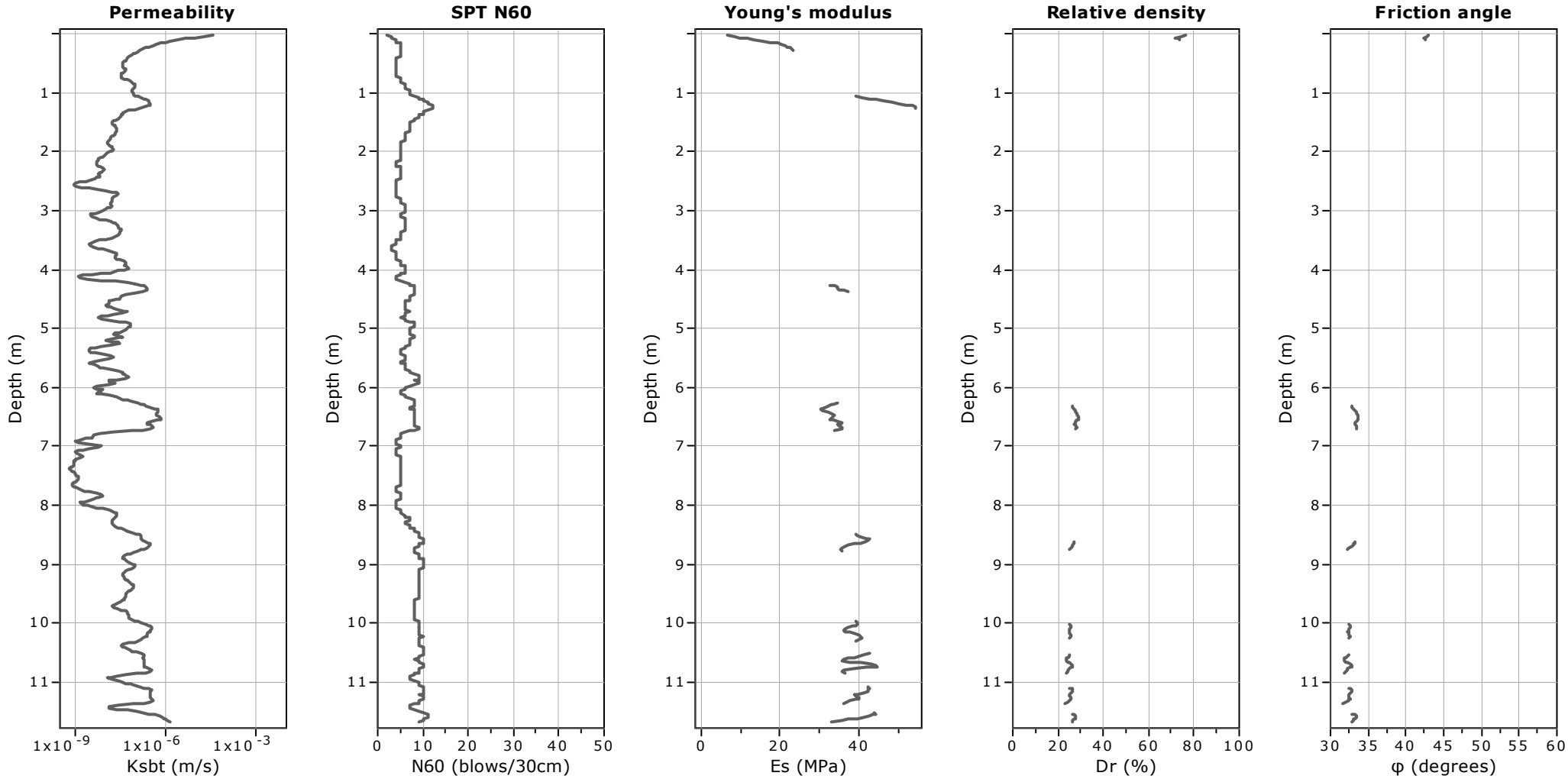
Project:
Location:

CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Permeability: Based on SBT_n
SPT N_{60}: Based on I_c and q_t
Young's modulus: Based on variable alpha using I_c (Robertson, 2009)
Relative desnisty constant, C_{Dr}: 350.0
Phi: Based on Kulhawy & Mayne (1990)
User defined estimation data

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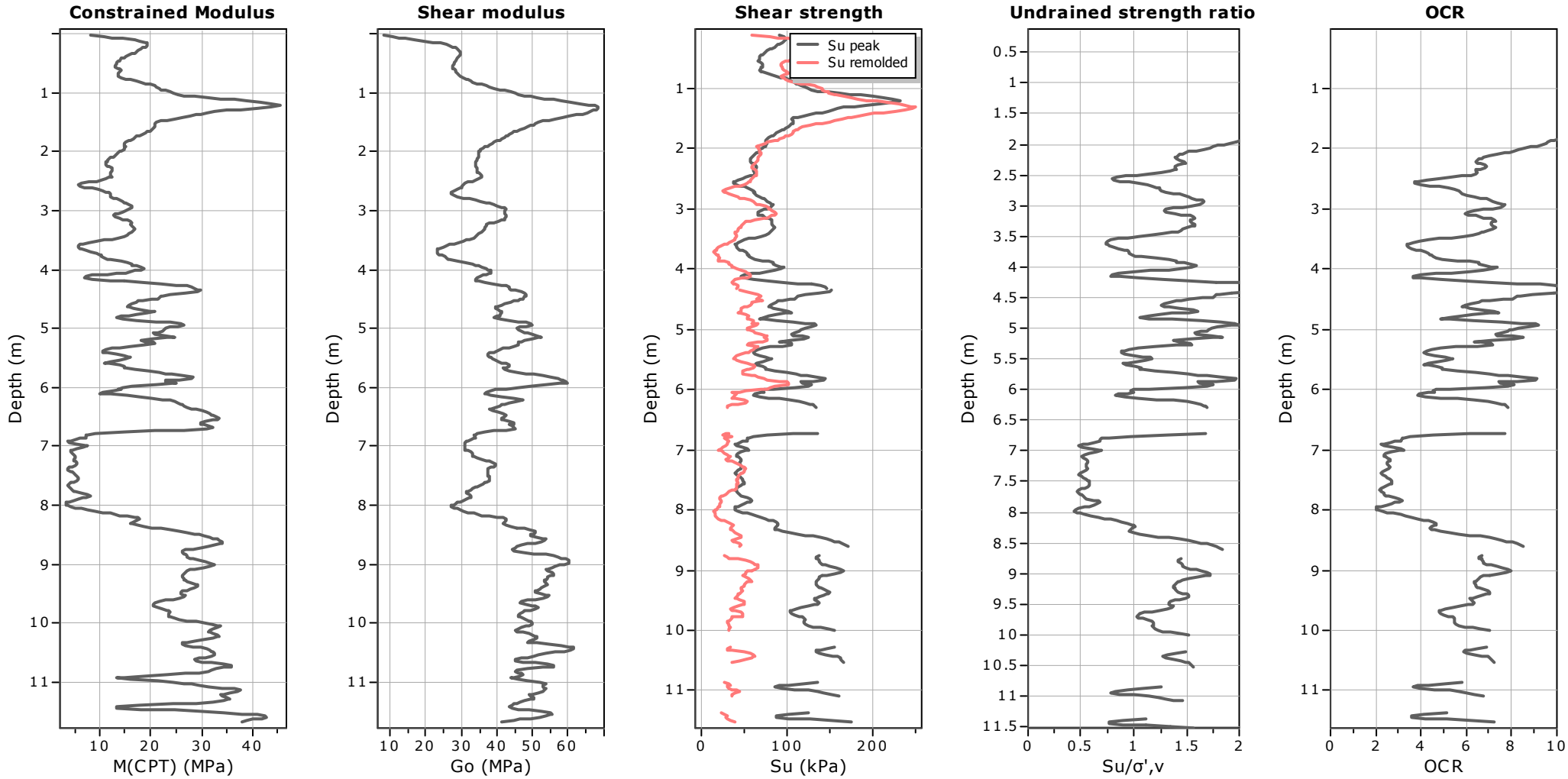
Project:
Location:

CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Constrained modulus: Based on variable *alpha* using I_c and Q_{tn} (Robertson, 2009)
Go: Based on variable *alpha* using I_c (Robertson, 2009)
Undrained shear strength cone factor for clays, N_{kt}: 14

OCR factor for clays, N_{kt}: 0.33
User defined estimation data

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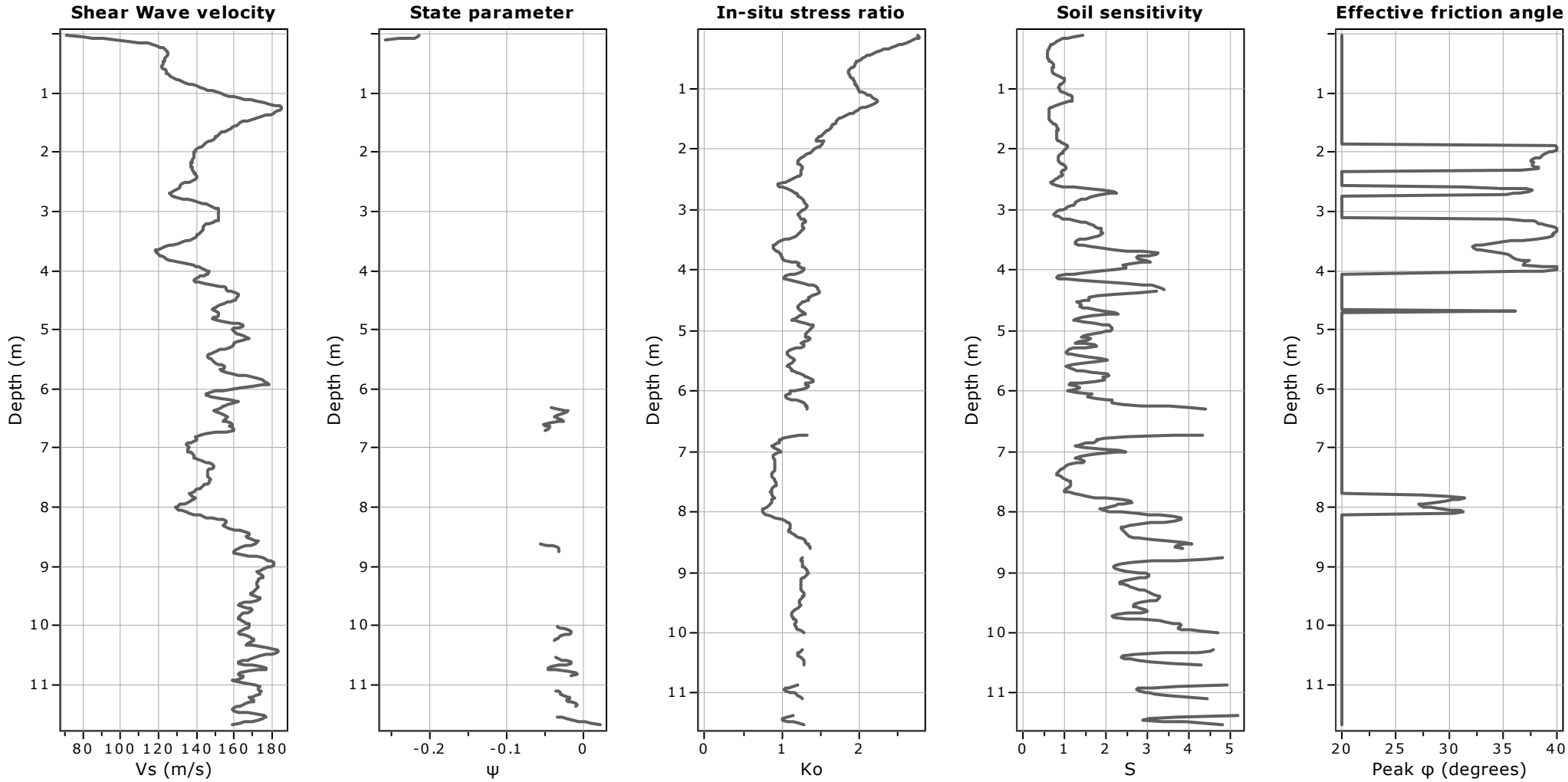
Project:
Location:

CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown



Calculation parameters

Soil Sensitivity factor, N_S: 7.00

User defined estimation data

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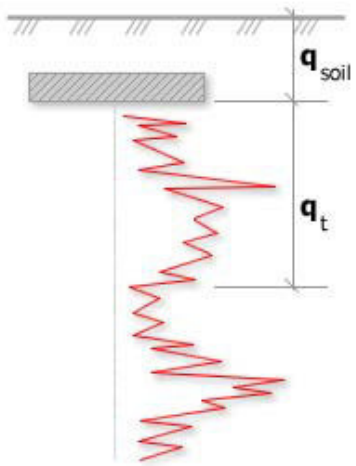
CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

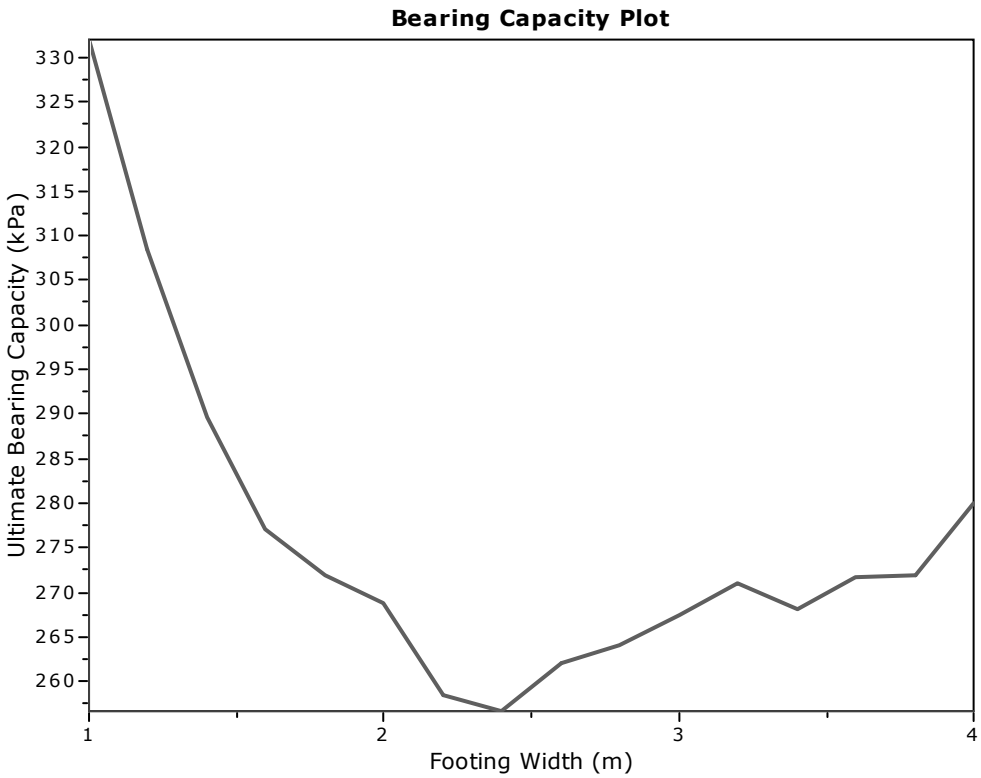
Project:
Location:



Bearing Capacity calculation is perfromed based on the formula:

$$Q_{ult} = R_k \times q_t + q_{soil}$$

where:
R_k: Bearing capacity factor
q_t: Average corrected cone resistance over calculation depth
q_{soil}: Pressure applied by soil above footing



:: Tabular results ::

No	B (m)	Start Depth (m)	End Depth (m)	Ave. q_t (MPa)	R_k	Soil Press. (kPa)	Ult. bearing cap. (kPa)
1	1.00	0.50	2.00	1.61	0.20	9.50	332.00
2	1.20	0.50	2.30	1.49	0.20	9.50	308.43
3	1.40	0.50	2.60	1.40	0.20	9.50	289.64
4	1.60	0.50	2.90	1.34	0.20	9.50	277.03
5	1.80	0.50	3.20	1.31	0.20	9.50	272.06
6	2.00	0.50	3.50	1.30	0.20	9.50	268.84
7	2.20	0.50	3.80	1.25	0.20	9.50	258.50
8	2.40	0.50	4.10	1.24	0.20	9.50	256.71
9	2.60	0.50	4.40	1.26	0.20	9.50	262.20
10	2.80	0.50	4.70	1.27	0.20	9.50	264.11
11	3.00	0.50	5.00	1.29	0.20	9.50	267.55
12	3.20	0.50	5.30	1.31	0.20	9.50	271.09
13	3.40	0.50	5.60	1.29	0.20	9.50	268.14
14	3.60	0.50	5.90	1.31	0.20	9.50	271.67
15	3.80	0.50	6.20	1.31	0.20	9.50	271.86
16	4.00	0.50	6.50	1.35	0.20	9.50	280.11

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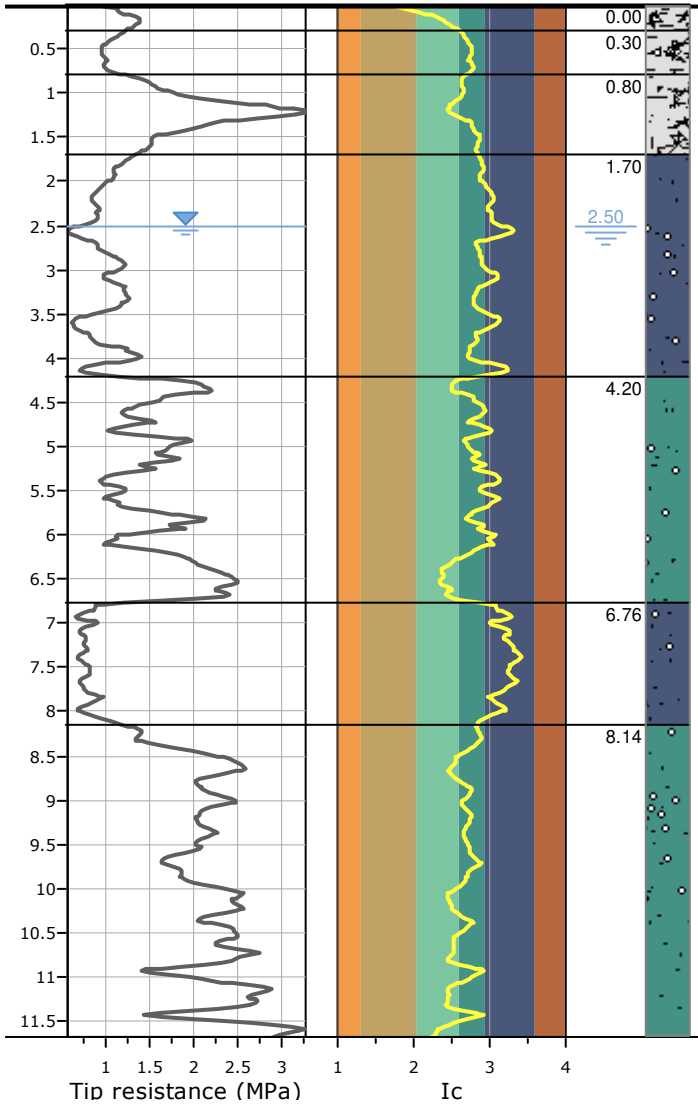
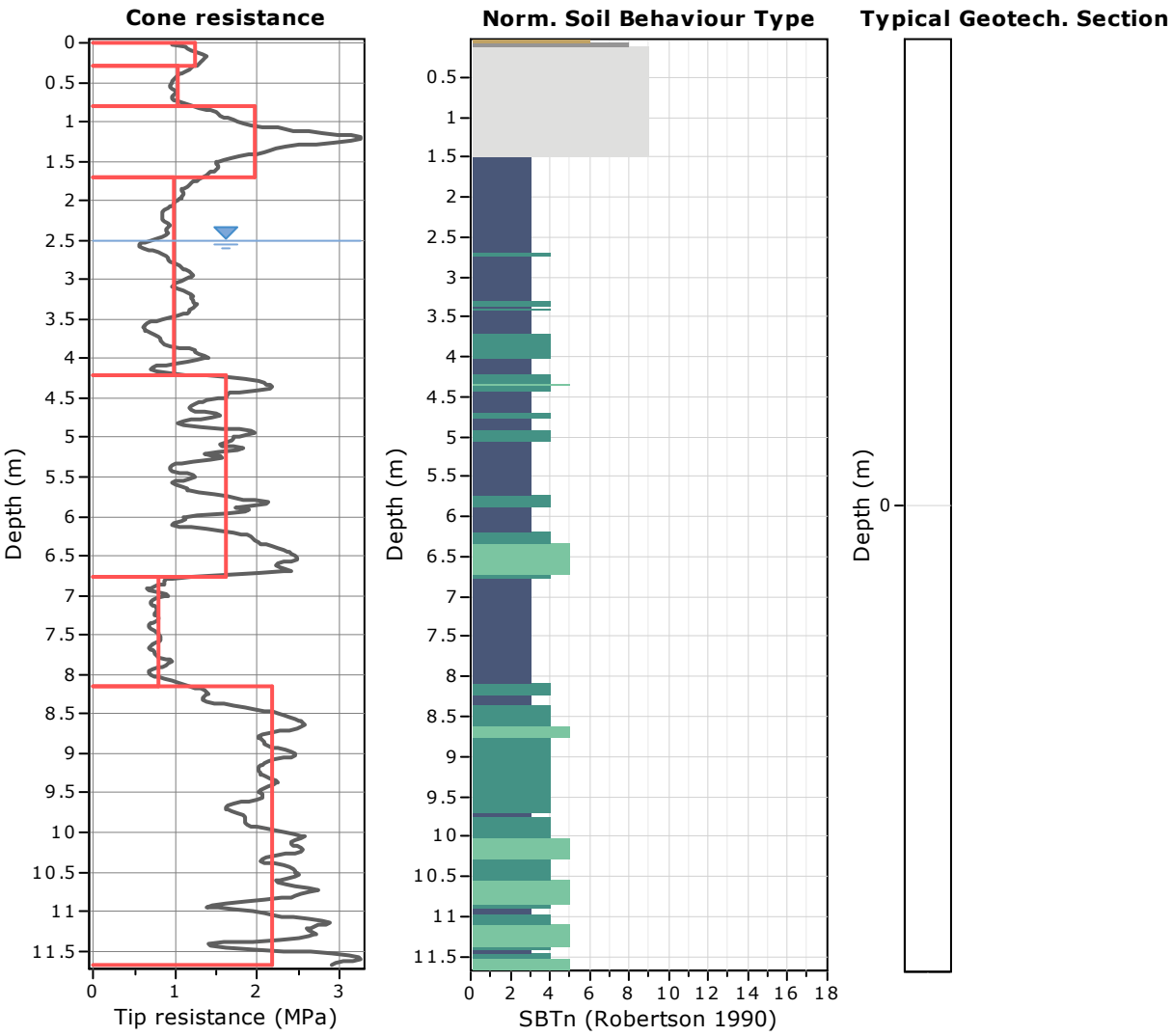
CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Project:
Location:



Depth (m)	Description	qt (MPa)	Ksbt (m/s)	N60	Es (MPa)	Dr	Phi (°)	M (MPa)	Go (MPa)	Su (kPa)	Su ratio	OCR	Gamma (kN/m³)
0.00	Very dense/stiff soil	1.3	5.17E-6	4.2	20.6	-	-	16.5	21.6	94.1	12.8	59.0	17.9
0.30	Very dense/stiff soil	1.0	4.97E-8	4.3	-	-	-	14.4	29.1	73.6	6.1	28.3	18.4
0.80	Very dense/stiff soil	2.0	8.93E-8	8.2	48.0	-	-	27.2	51.7	138.9	5.1	23.8	19.0
1.70	Clay	1.0	1.42E-8	4.9	-	-	-	12.8	34.4	66.4	1.4	6.5	17.5
4.20	Clay & silty clay	1.6	1.01E-7	7.0	34.5	-	-	21.2	44.1	99.4	1.5	6.7	17.6
6.76	Clay	0.8	3.41E-9	4.7	-	-	-	5.5	33.7	48.0	0.6	2.7	16.8
8.14	Clay & silty clay	2.2	1.40E-7	8.8	40.4	-	-	28.0	50.2	129.9	1.3	6.1	17.4



Tabular results

.:: Layer No: 1 ::.

Code: R **Start depth:** 0.00 (m), **End depth:** 0.30 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 1.25 ±0.12 MPa	Permeability: 5.17E-06 ±1.04E-05 m/s	Constrained Mod.: 16.47 ±3.45 MPa
Sleeve friction: 78.88 ±43.55 kPa	N60: 4.20 ±1.01 blows	Go: 21.62 ±7.40 MPa
SBT_n: 9	Es: 20.57 ±2.64 MPa	Su: 94.09 ±4.05 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 12.77 ±1.51
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 59.01 ±6.99
	Unit weight: 17.85 ±0.92 kN/m³	

.:: Layer No: 2 ::.

Code: A1 **Start depth:** 0.30 (m), **End depth:** 0.80 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 1.04 ±0.09 MPa	Permeability: 4.97E-08 ±1.99E-08 m/s	Constrained Mod.: 14.43 ±1.28 MPa
Sleeve friction: 107.44 ±13.67 kPa	N60: 4.35 ±0.49 blows	Go: 29.13 ±1.29 MPa
SBT_n: 9	Es: 0.00 ±0.00 MPa	Su: 73.60 ±6.52 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 6.14 ±1.77
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 28.35 ±8.20
	Unit weight: 18.37 ±0.16 kN/m³	

.:: Layer No: 3 ::.

Code: C1 **Start depth:** 0.80 (m), **End depth:** 1.70 (m)

Description: Very dense/stiff soil

Basic results	Estimation results	
Total cone resistance: 1.97 ±0.60 MPa	Permeability: 8.93E-08 ±8.29E-08 m/s	Constrained Mod.: 27.22 ±8.43 MPa
Sleeve friction: 160.79 ±46.41 kPa	N60: 8.20 ±2.02 blows	Go: 51.66 ±10.59 MPa
SBT_n: 9	Es: 48.02 ±5.58 MPa	Su: 138.89 ±43.01 kPa
SBTn description: Very dense/stiff soil	Dr (%): 0.00 ±0.00	Su ratio: 5.15 ±1.42
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 23.79 ±6.58
	Unit weight: 19.03 ±0.42 kN/m³	

.:: Layer No: 4 ::.

Code: A2 **Start depth:** 1.70 (m), **End depth:** 4.20 (m)

Description: Clay

Basic results	Estimation results	
Total cone resistance: 0.98 ±0.20 MPa	Permeability: 1.42E-08 ±1.16E-08 m/s	Constrained Mod.: 12.76 ±3.29 MPa
Sleeve friction: 54.21 ±22.24 kPa	N60: 4.89 ±0.83 blows	Go: 34.42 ±5.15 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 66.38 ±14.62 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 1.40 ±0.43
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.49 ±2.00
	Unit weight: 17.46 ±0.57 kN/m³	

.:: Layer No: 5 ::.

Code: B1 **Start depth:** 4.20 (m), **End depth:** 6.76 (m)

Description: Clay & silty clay

Basic results	Estimation results	
Total cone resistance: 1.62 ±0.44 MPa	Permeability: 1.01E-07 ±1.60E-07 m/s	Constrained Mod.: 21.17 ±6.34 MPa
Sleeve friction: 51.18 ±17.82 kPa	N60: 7.00 ±1.14 blows	Go: 44.13 ±5.16 MPa
SBT_n: 4	Es: 34.49 ±1.38 MPa	Su: 99.37 ±25.20 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.45 ±0.37
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.71 ±1.72
	Unit weight: 17.61 ±0.40 kN/m³	

.:: Layer No: 6 ::.

Code: D1 **Start depth:** 6.76 (m), **End depth:** 8.14 (m)

Description: Clay

Basic results	**Estimation results**	
Total cone resistance: 0.80 ±0.11 MPa	Permeability: 3.41E-09 ±4.47E-09 m/s	Constrained Mod.: 5.55 ±2.02 MPa
Sleeve friction: 31.40 ±10.42 kPa	N60: 4.66 ±0.51 blows	Go: 33.72 ±3.23 MPa
SBT_n: 3	Es: 0.00 ±0.00 MPa	Su: 47.97 ±7.93 kPa
SBTn description: Clay	Dr (%): 0.00 ±0.00	Su ratio: 0.57 ±0.10
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 2.66 ±0.44
	Unit weight: 16.80 ±0.38 kN/m³	

.:: Layer No: 7 ::.

Code: B2 **Start depth:** 8.14 (m), **End depth:** 11.68 (m)

Description: Clay & silty clay

Basic results	**Estimation results**	
Total cone resistance: 2.18 ±0.42 MPa	Permeability: 1.40E-07 ±1.62E-07 m/s	Constrained Mod.: 27.96 ±6.15 MPa
Sleeve friction: 37.33 ±11.39 kPa	N60: 8.82 ±1.09 blows	Go: 50.24 ±4.91 MPa
SBT_n: 4	Es: 40.42 ±2.50 MPa	Su: 129.89 ±24.02 kPa
SBTn description: Clay & silty clay	Dr (%): 0.00 ±0.00	Su ratio: 1.31 ±0.25
	ö (degrees): 0.00 ±0.00 °	O.C.R.: 6.06 ±1.15
	Unit weight: 17.39 ±0.34 kN/m³	

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Project:
Location:

CPT: CPTu-08
Total depth: 11.68 m, Date: 26/11/2024
Surface Elevation: 0.00 m
Coords: X:0.00, Y:0.00
Cone Type: Uknown
Cone Operator: Uknown

Summary table of mean values

From depth To depth (m)	Thickness (m)	Permeability (m/s)	SPT_{N60} (blows/30cm)	E_s (MPa)	D_r	Friction angle	Constrained modulus, M (MPa)	Shear modulus, G_O (MPa)	Undrained strength, S_U (kPa)	Undrained strength ratio	OCR	Unit weight (kN/m³)
0.00	0.30	5.17E-06	4.2	20.6	0.0	0.0	16.5	21.6	94.1	12.8	59.0	17.9
0.30		(±1.04E-05)	(±1.0)	(±2.6)	(±0.0)	(±0.0)	(±3.4)	(±7.4)	(±4.0)	(±1.5)	(±7.0)	(±0.9)
0.30	0.50	4.97E-08	4.3	0.0	0.0	0.0	14.4	29.1	73.6	6.1	28.3	18.4
0.80		(±1.99E-08)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±1.3)	(±1.3)	(±6.5)	(±1.8)	(±8.2)	(±0.2)
0.80	0.90	8.93E-08	8.2	48.0	0.0	0.0	27.2	51.7	138.9	5.1	23.8	19.0
1.70		(±8.29E-08)	(±2.0)	(±5.6)	(±0.0)	(±0.0)	(±8.4)	(±10.6)	(±43.0)	(±1.4)	(±6.6)	(±0.4)
1.70	2.50	1.42E-08	4.9	0.0	0.0	0.0	12.8	34.4	66.4	1.4	6.5	17.5
4.20		(±1.16E-08)	(±0.8)	(±0.0)	(±0.0)	(±0.0)	(±3.3)	(±5.1)	(±14.6)	(±0.4)	(±2.0)	(±0.6)
4.20	2.56	1.01E-07	7.0	34.5	0.0	0.0	21.2	44.1	99.4	1.5	6.7	17.6
6.76		(±1.60E-07)	(±1.1)	(±1.4)	(±0.0)	(±0.0)	(±6.3)	(±5.2)	(±25.2)	(±0.4)	(±1.7)	(±0.4)
6.76	1.38	3.41E-09	4.7	0.0	0.0	0.0	5.5	33.7	48.0	0.6	2.7	16.8
8.14		(±4.47E-09)	(±0.5)	(±0.0)	(±0.0)	(±0.0)	(±2.0)	(±3.2)	(±7.9)	(±0.1)	(±0.4)	(±0.4)
8.14	3.54	1.40E-07	8.8	40.4	0.0	0.0	28.0	50.2	129.9	1.3	6.1	17.4
11.68		(±1.62E-07)	(±1.1)	(±2.5)	(±0.0)	(±0.0)	(±6.1)	(±4.9)	(±24.0)	(±0.2)	(±1.2)	(±0.3)

Depth values presented in this table are measured from free ground surface

Presented below is a list of formulas used for the estimation of various soil properties. The formulas are presented in SI unit system and assume that all components are expressed in the same units.

:: Unit Weight, g (kN/m³) ::

$$g = g_w \cdot \left(0.27 \cdot \log(R_f) + 0.36 \cdot \log(\frac{q_t}{p_a}) + 1.236\right)$$

where g_w = water unit weight

:: Permeability, k (m/s) ::

$I_c < 3.27$ and $I_c > 1.00$ then $k = 10^{0.952-3.04 \cdot I_c}$

$I_c \leq 4.00$ and $I_c > 3.27$ then $k = 10^{-4.52-1.37 \cdot I_c}$

:: N_{SPT} (blows per 30 cm) ::

$$N_{60} = \left(\frac{q_c}{P_a}\right) \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

$$N_{1(60)} = Q_{tn} \cdot \frac{1}{10^{1.1268-0.2817 \cdot I_c}}$$

:: Young's Modulus, Es (MPa) ::

$$(q_t - \sigma_v) \cdot 0.015 \cdot 10^{0.55 \cdot I_c + 1.68}$$

(applicable only to $I_c < I_{c\_cutoff}$)

:: Relative Density, Dr (%) ::

$$100 \cdot \sqrt{\frac{Q_{tn}}{k_{DR}}}$$

(applicable only to SBT_n: 5, 6, 7 and 8 or $I_c < I_{c\_cutoff}$)

:: State Parameter, ψ ::

$$\psi = 0.56 - 0.33 \cdot \log(Q_{tn,cs})$$

:: Peak drained friction angle, φ (°) ::

$$\varphi = 17.60 + 11 \cdot \log(Q_{tn})$$

(applicable only to SBT_n: 5, 6, 7 and 8)

:: 1-D constrained modulus, M (MPa) ::

If $I_c > 2.20$

$\alpha = 14$ for $Q_{tn} > 14$

$\alpha = Q_{tn}$ for $Q_{tn} \leq 14$

$M_{CPT} = \alpha \cdot (q_t - \sigma_v)$

If $I_c \leq 2.20$

$M_{CPT} = (q_t - \sigma_v) \cdot 0.0188 \cdot 10^{0.55 \cdot I_c + 1.68}$

:: Small strain shear Modulus, Go (MPa) ::

$$G_0 = (q_t - \sigma_v) \cdot 0.0188 \cdot 10^{0.55 \cdot I_c + 1.68}$$

:: Shear Wave Velocity, Vs (m/s) ::

$$V_s = \left(\frac{G_0}{\rho}\right)^{0.50}$$

:: Undrained peak shear strength, Su (kPa) ::

$N_{kt} = 10.50 + 7 \cdot \log(F_r)$ or user defined

$$S_u = \frac{(q_t - \sigma_v)}{N_{kt}}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: Remolded undrained shear strength, Su(rem) (kPa) ::

$S_{u(rem)} = f_s$ (applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: Overconsolidation Ratio, OCR ::

$$k_{OCR} = \left[\frac{Q_{tn}^{0.20}}{0.25 \cdot (10.50 \cdot +7 \cdot \log(F_r))}\right]^{1.25}$$ or user defined

$OCR = k_{OCR} \cdot Q_{tn}$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: In situ Stress Ratio, Ko ::

$$K_O = (1 - \sin\varphi') \cdot OCR^{\sin\varphi'}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: Soil Sensitivity, S_t ::

$$S_t = \frac{N_S}{F_r}$$

(applicable only to SBT_n: 1, 2, 3, 4 and 9 or $I_c > I_{c\_cutoff}$)

:: Effective Stress Friction Angle, φ' (°) ::

$$\varphi' = 29.5° \cdot B_q^{0.121} \cdot (0.256 + 0.336 \cdot B_q + \log Q_t)$$

(applicable for $0.10 < B_q < 1.00$)

References

• Robertson, P.K., Cabal K.L., Guide to Cone Penetration Testing for Geotechnical Engineering, Gregg Drilling & Testing, Inc., 5th Edition, November 2012

• Robertson, P.K., Interpretation of Cone Penetration Tests - a unified approach., Can. Geotech. J. 46(11): 1337–1355 (2009)

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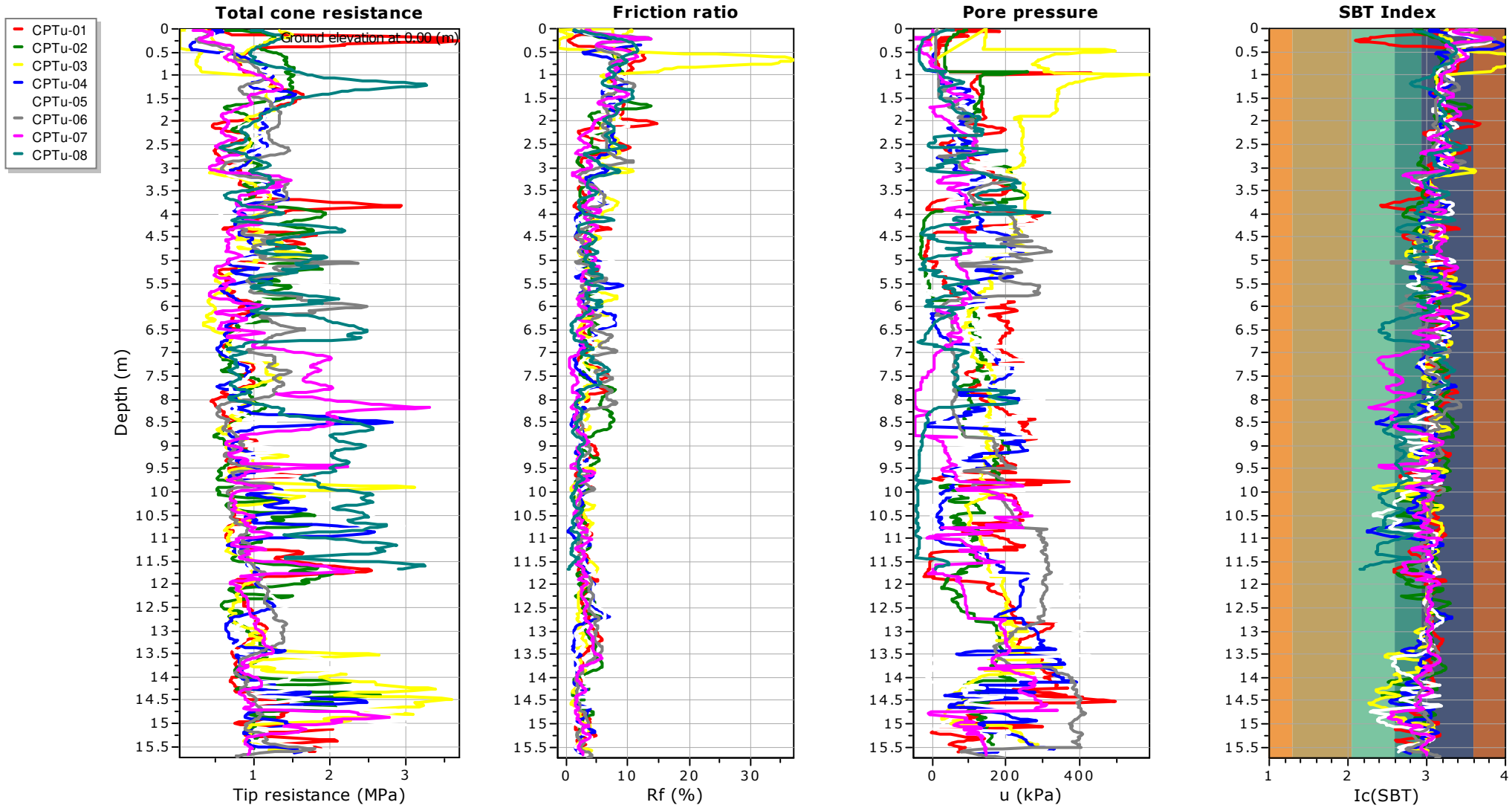
Project:
Location:

Overlay basic interpretation plots



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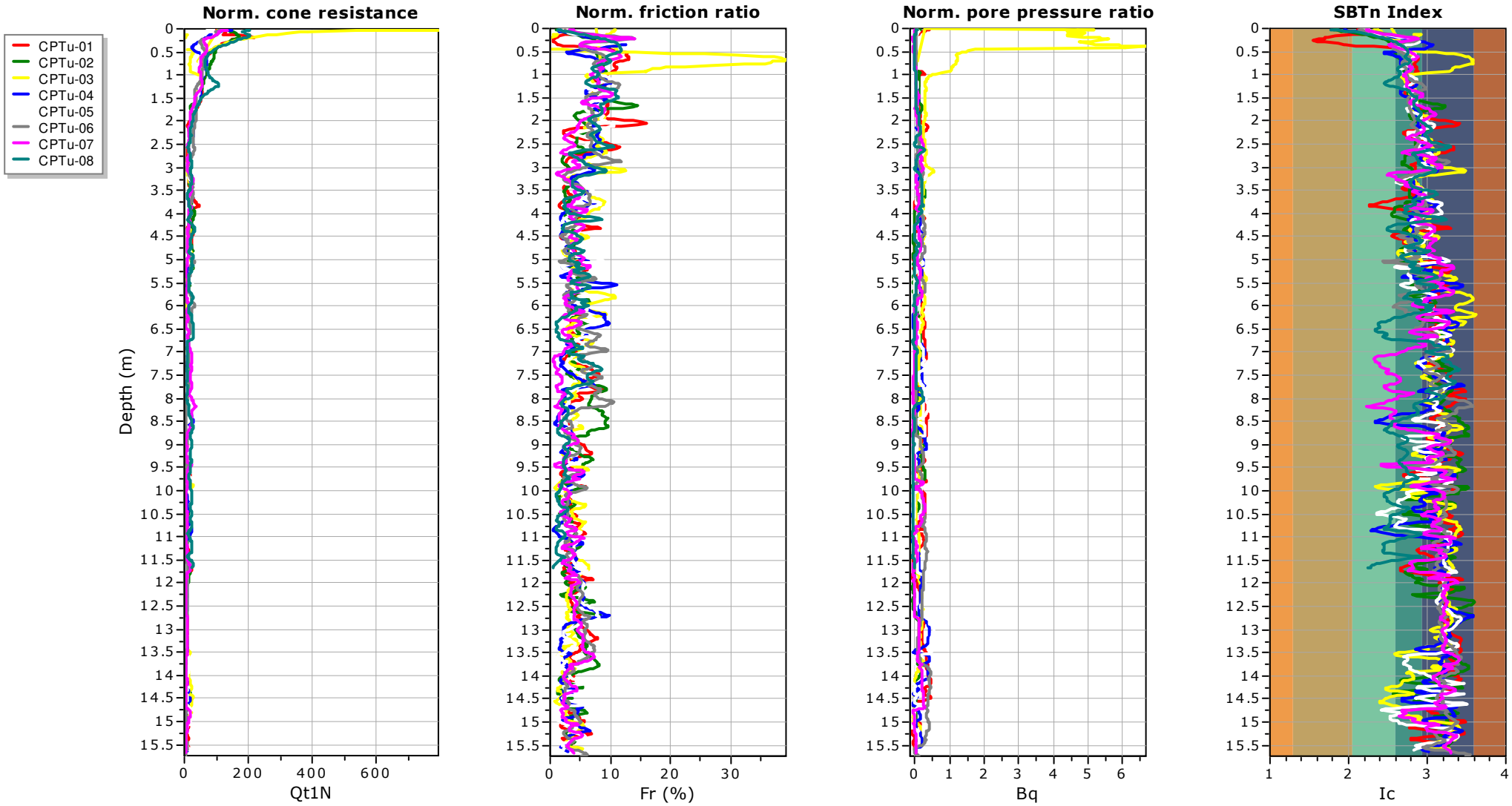
Project:
Location:

Normalized basic plots



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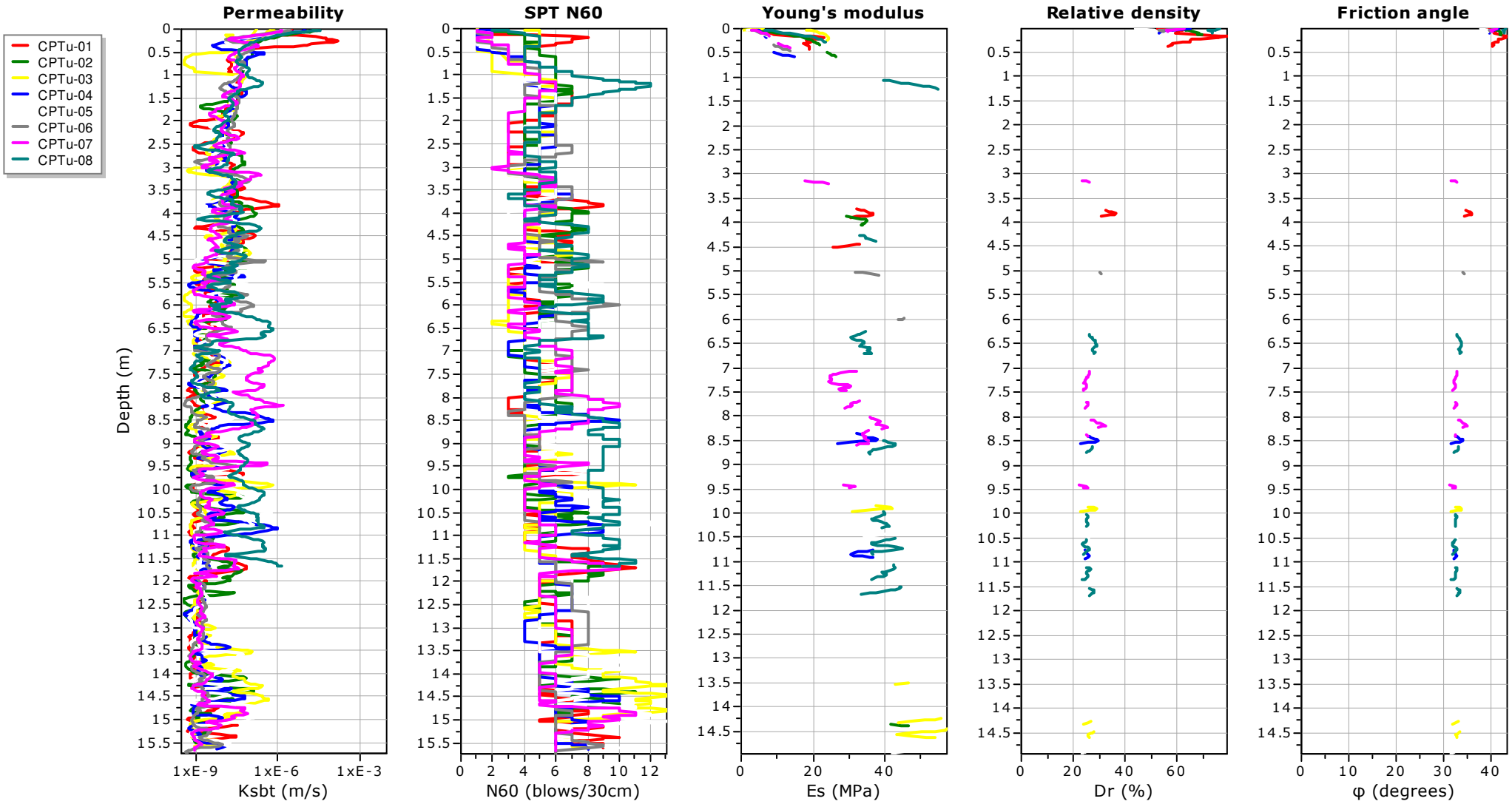
Project:
Location:

Overlay estimation plots (1)



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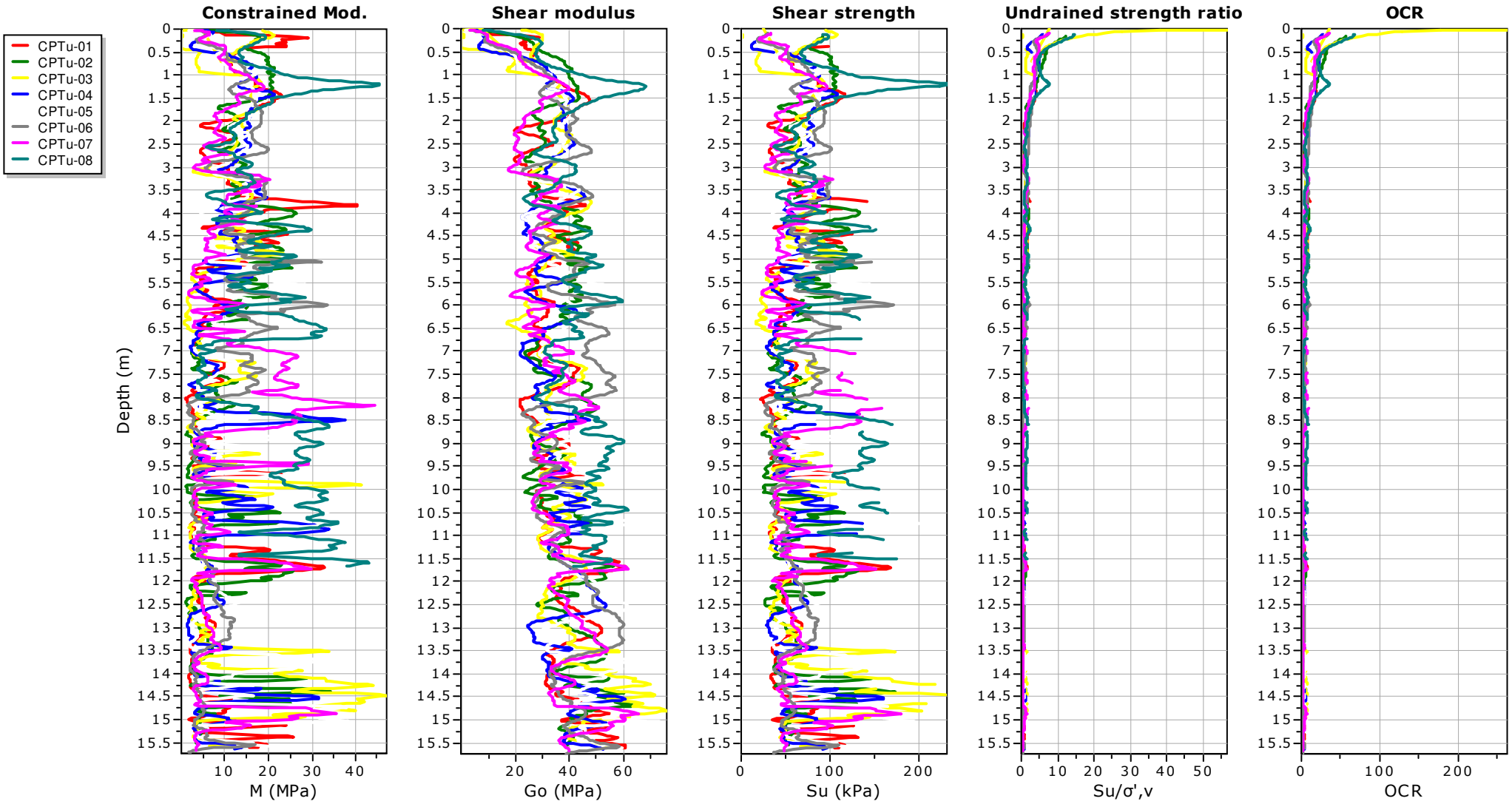
Project:
Location:

Overlay estimation plots (2)



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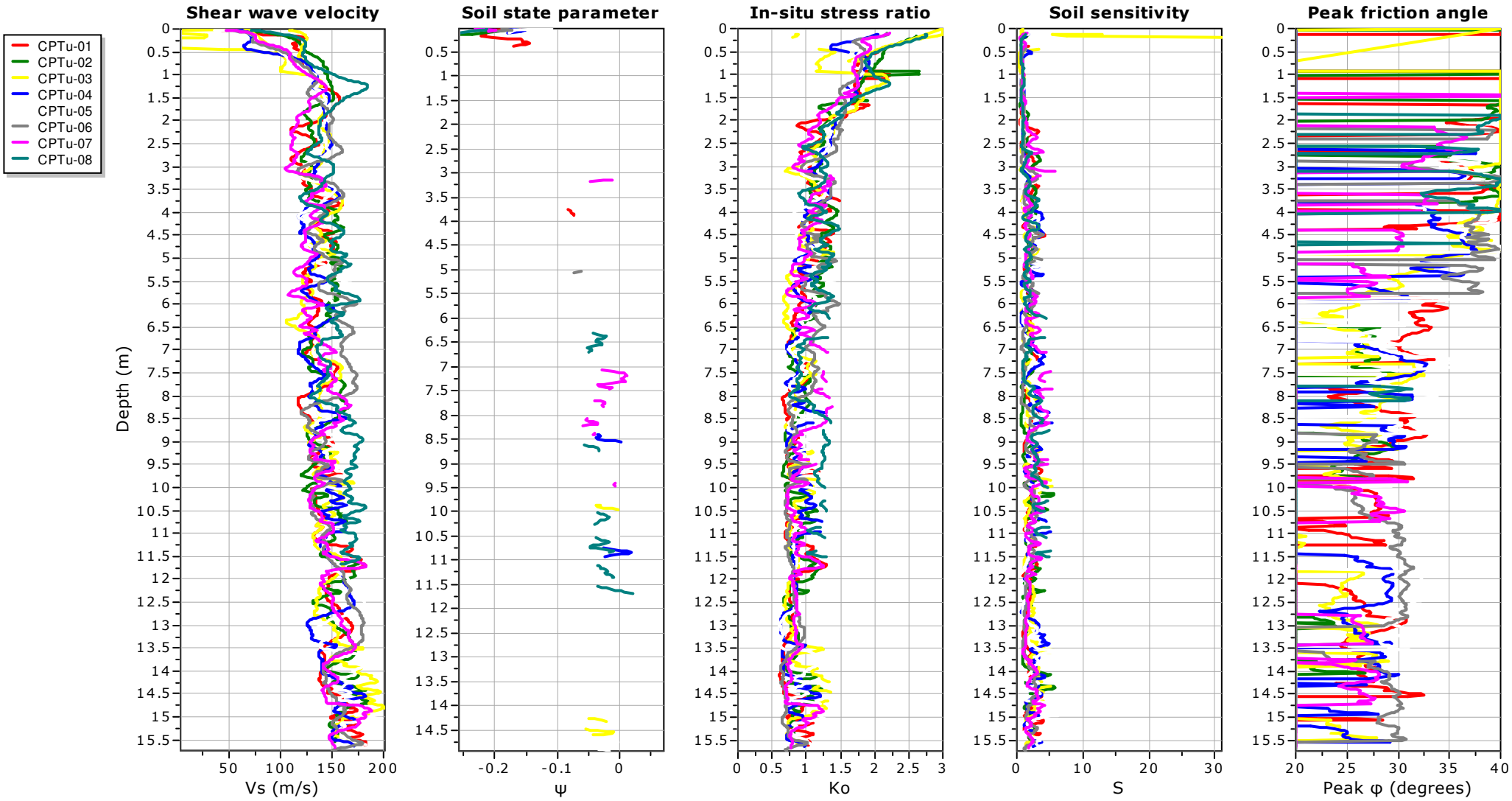
Project:
Location:

Overlay estimation plots (3)



ALLEGATO IV

- REPORT VERIFICA LIQUEFAZIONE -

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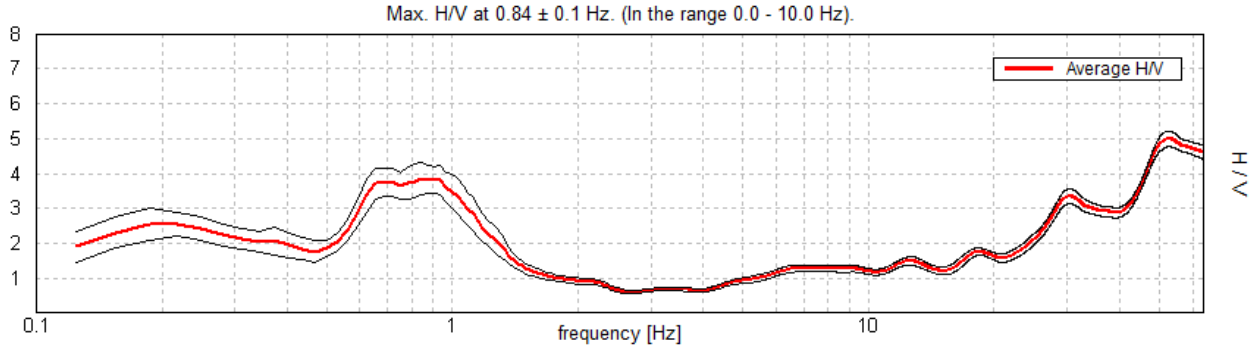
SALA_BOLOGNESE, SALAFOTOVOLT 1

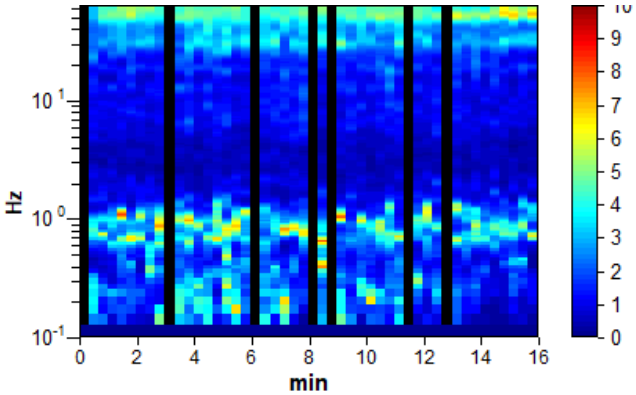
Strumento: TZB-0127/01-20
Formato dati: 32 bit
Fondo scala [mV]: 179
Inizio registrazione: 06/09/2023 14:03:12 Fine registrazione: 06/09/2023 14:19:12
Nomi canali: NORTH SOUTH; EAST WEST ; UP DOWN
Dato GPS non disponibile

Durata registrazione: 0h16'00". Analizzato 85% tracciato (selezione manuale)
Freq. campionamento: 128 Hz
Lunghezza finestre: 20 s
Tipo di lisciamento: Triangular window
Lisciamento: 13%

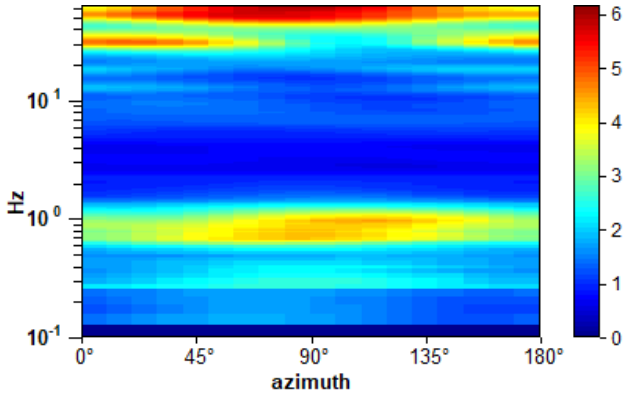
RAPPORTO SPETTRALE ORIZZONTALE SU VERTICALE



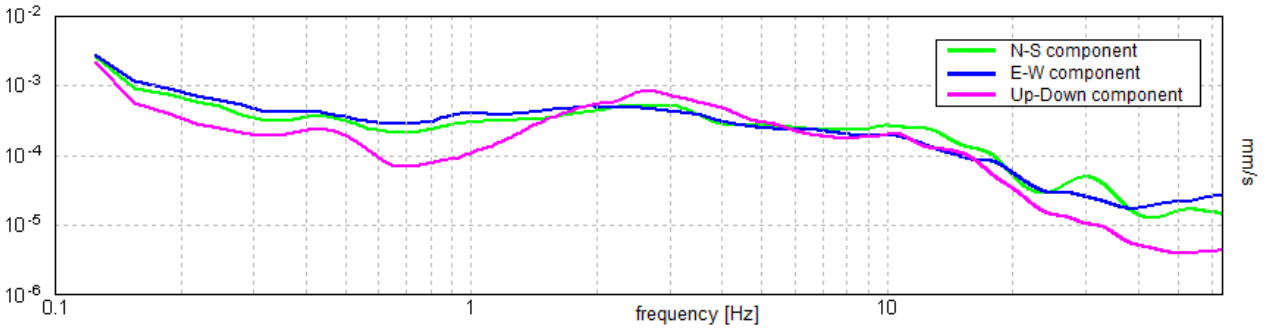
SERIE TEMPORALE H/V



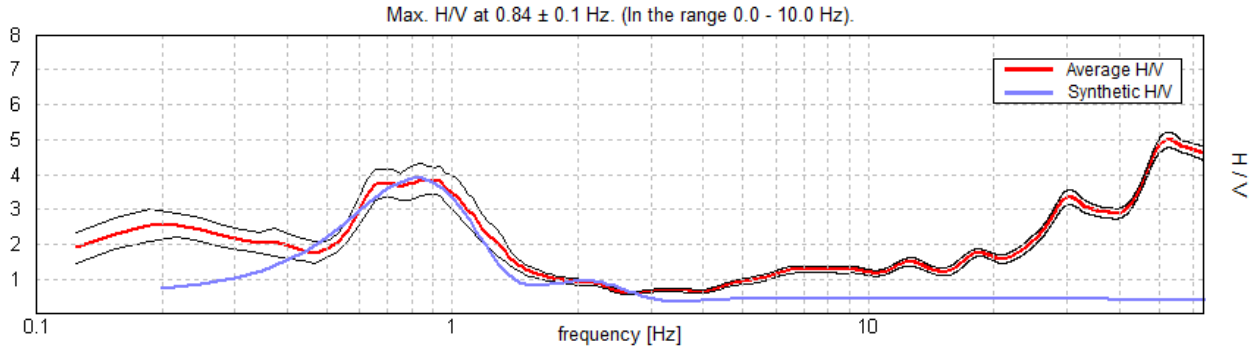
DIREZIONALITA' H/V



SPETTRI DELLE SINGOLE COMPONENTI

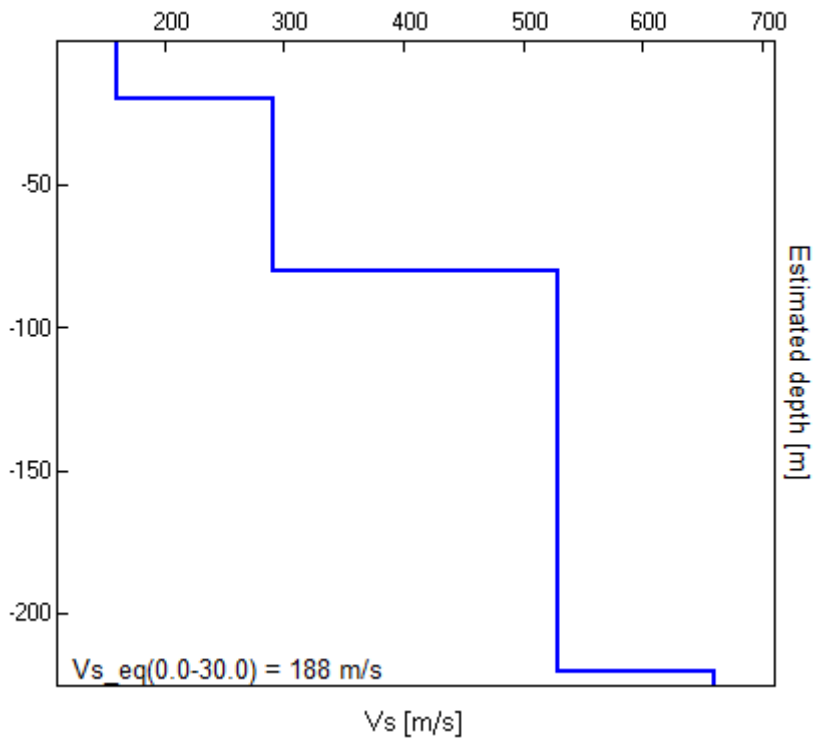


H/V SPERIMENTALE vs. H/V SINTETICO



Profondità alla base dello strato [m]	Spessore [m]	Vs [m/s]	Rapporto di Poisson
20.00	20.00	160	0.42
80.00	60.00	290	0.42
220.00	140.00	530	0.42
inf.	inf.	660	0.42

Vs_eq(0.0-30.0) = 188 m/s



[Secondo le linee guida SESAME, 2005. **Si raccomanda di leggere attentamente il manuale di** *Grilla* **prima di interpretare la tabella seguente**].

Picco H/V a 0.84 ± 0.1 Hz (nell'intervallo 0.0 - 10.0 Hz).

Criteri per una curva H/V affidabile [Tutti 3 dovrebbero risultare soddisfatti]			
$f_0 > 10 / L_w$	0.84 > 0.50	OK	
$n_c(f_0) > 200$	691.9 > 200	OK	
$\sigma_A(f) < 2$ per $0.5f_0 < f < 2f_0$ se $f_0 > 0.5$Hz **$\sigma_A(f) < 3$ per $0.5f_0 < f < 2f_0$ se $f_0 < 0.5$Hz**	Superato 0 volte su 41	OK	
Criteri per un picco H/V chiaro [Almeno 5 su 6 dovrebbero essere soddisfatti]			
Esiste f^- in $[f_0/4, f_0]$ | $A_{H/V}(f^-) < A_0 / 2$	0.5 Hz	OK	
Esiste f^+ in $[f_0, 4f_0]$ | $A_{H/V}(f^+) < A_0 / 2$	1.313 Hz	OK	
$A_0 > 2$	3.84 > 2	OK	
$f_{picco}[A_{H/V}(f) \pm \sigma_A(f)] = f_0 \pm 5\%$	|0.12147| < 0.05		NO
$\sigma_f < \varepsilon(f_0)$	0.10249 < 0.12656	OK	
$\sigma_A(f_0) < \theta(f_0)$	0.4672 < 2.0	OK	

L_w	lunghezza della finestra
n_w	numero di finestre usate nell'analisi
$n_c = L_w n_w f_0$	numero di cicli significativi
f	frequenza attuale
f_0	frequenza del picco H/V
σ_f	deviazione standard della frequenza del picco H/V
$\varepsilon(f_0)$	valore di soglia per la condizione di stabilità $\sigma_f < \varepsilon(f_0)$
A_0	ampiezza della curva H/V alla frequenza f_0
$A_{H/V}(f)$	ampiezza della curva H/V alla frequenza f
f^-	frequenza tra $f_0/4$ e f_0 alla quale $A_{H/V}(f^-) < A_0/2$
f^+	frequenza tra f_0 e $4f_0$ alla quale $A_{H/V}(f^+) < A_0/2$
$\sigma_A(f)$	deviazione standard di $A_{H/V}(f)$, $\sigma_A(f)$ è il fattore per il quale la curva $A_{H/V}(f)$ media deve essere moltiplicata o divisa
$\sigma_{logH/V}(f)$	deviazione standard della funzione log $A_{H/V}(f)$
$\theta(f_0)$	valore di soglia per la condizione di stabilità $\sigma_A(f) < \theta(f_0)$

Valori di soglia per σ_f e $\sigma_A(f_0)$					
Intervallo di freq. [Hz]	< 0.2	0.2 – 0.5	0.5 – 1.0	1.0 – 2.0	> 2.0
$\varepsilon(f_0)$ [Hz]	0.25 f_0	0.2 f_0	0.15 f_0	0.10 f_0	0.05 f_0
$\theta(f_0)$ per $\sigma_A(f_0)$	3.0	2.5	2.0	1.78	1.58
log $\theta(f_0)$ per $\sigma_{logH/V}(f_0)$	0.48	0.40	0.30	0.25	0.20

TROMINO
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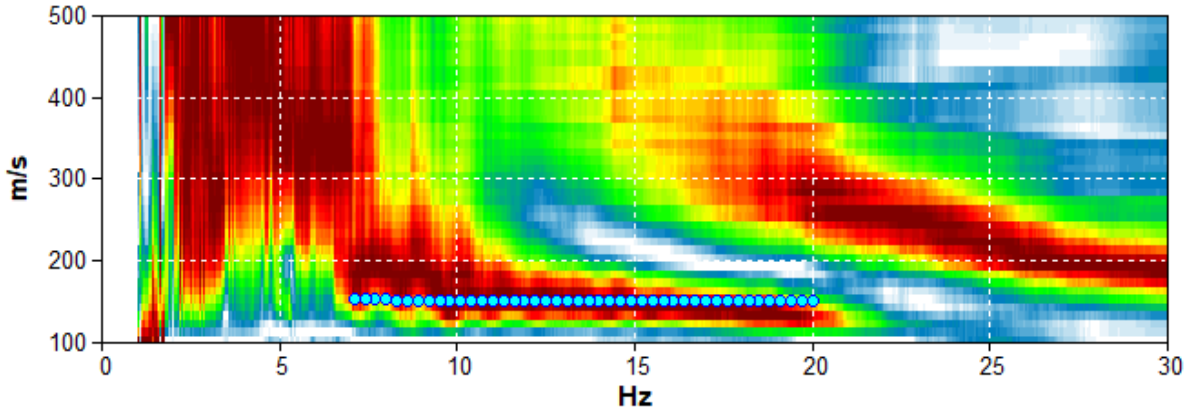
SALA_BOLOGNESE, SALA FOTOVOL T

Inizio registrazione: 06/09/2023 14:54:14 Fine registrazione: 06/09/2023 14:57:52
Durata registrazione: 0h03'37".
Freq. campionamento: 256 Hz

Nomi canali: TR1+ TR1- ; TR2+ TR2- ; TR3+ TR3- ; TR4+ TR4- ; TR5+ TR5- ; TR6+ TR6- ; TR7+ TR7- ; TR8+ TR8-

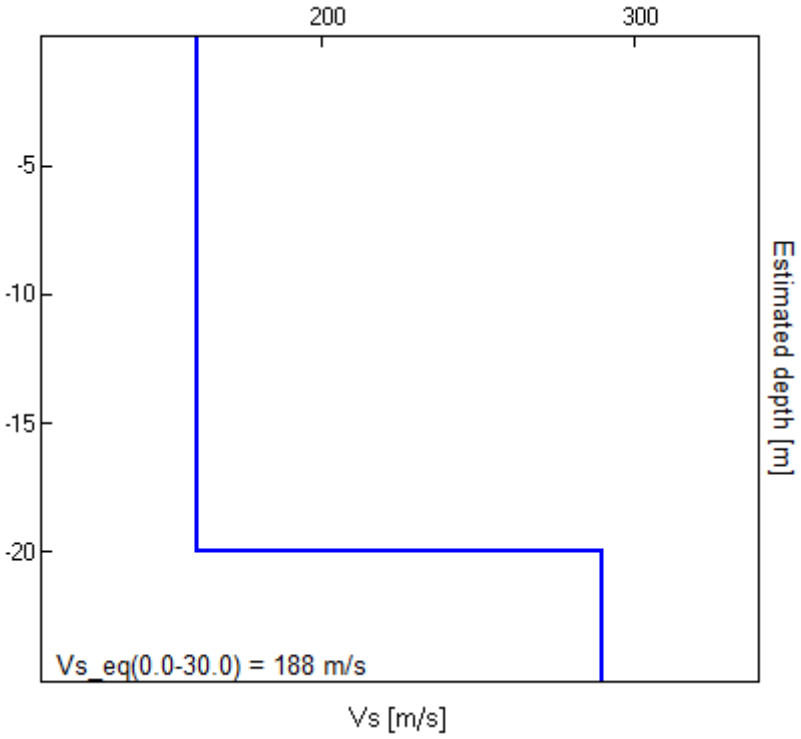
Array geometry (x): 0.0 3.0 6.0 9.0 12.0 15.0 18.0 21.0 m.

MODELLED RAYLEIGH WAVE PHASE VELOCITY DISPERSION CURVE



Depth at the bottom of the layer [m]	Thickness [m]	Vs [m/s]	Poisson ratio
20.00	20.00	160	0.42
inf.	inf.	290	0.42

Vs_eq(0.0-30.0) = 188 m/s


200
300
-5
-10
-15
-20
Estimated depth [m]
Vs_eq(0.0-30.0) = 188 m/s
Vs [m/s]

Parametri sismici

determinati con **GeoStru PS**

Le coordinate geografiche espresse in questo file sono in ED50

Tipo di elaborazione:Stabilità dei pendii

Sito in esame.

latitudine: 44,605351 [°]

longitudine: 11,278173 [°]

Classe d'uso: II. Costruzioni il cui uso preveda normali affollamenti, senza contenuti pericolosi per l'ambiente e senza funzioni pubbliche e sociali essenziali. Industrie con attività non pericolose per l'ambiente. Ponti, opere infrastrutturali, reti viarie non ricadenti in Classe d'uso III o in Classe d'uso IV, reti ferroviarie la cui interruzione non provochi situazioni di emergenza. Dighe il cui collasso non provochi conseguenze rilevanti.

Vita nominale: 50 [anni]

Tipo di interpolazione: Media ponderata

Siti di riferimento.

	ID	Latitudine [°]	Longitudine [°]	Distanza [m]
Sito 1	16285	44,613660	11,243670	2883,3
Sito 2	16286	44,614960	11,313840	3018,8
Sito 3	16508	44,564970	11,315690	5384,2
Sito 4	16507	44,563670	11,245570	5305,4

Parametri sismici

Categoria sottosuolo: C

Categoria topografica: T1

Periodo di riferimento: 50 anni

Coefficiente cu: 1

	Prob. superamento [%]	Tr [anni]	ag [g]	Fo [-]	Tc* [s]
Operatività (SLO)	81	30	0,049	2,479	0,258
Danno (SLD)	63	50	0,061	2,512	0,272
Salvaguardia della vita (SLV)	10	475	0,164	2,497	0,282
Prevenzione dal collasso (SLC)	5	975	0,215	2,485	0,286

Coefficienti Sismici Stabilità dei pendii

	Ss [-]	Cc [-]	St [-]	Kh [-]	Kv [-]	Amax [m/s²]	Beta [-]
SLO	1,500	1,640	1,000	0,015	0,007	0,726	0,200
SLD	1,500	1,610	1,000	0,018	0,009	0,894	0,200
SLV	1,450	1,590	1,000	0,057	0,029	2,333	0,240
SLC	1,380	1,590	1,000	0,083	0,042	2,915	0,280

Geostru

ALLEGATO III

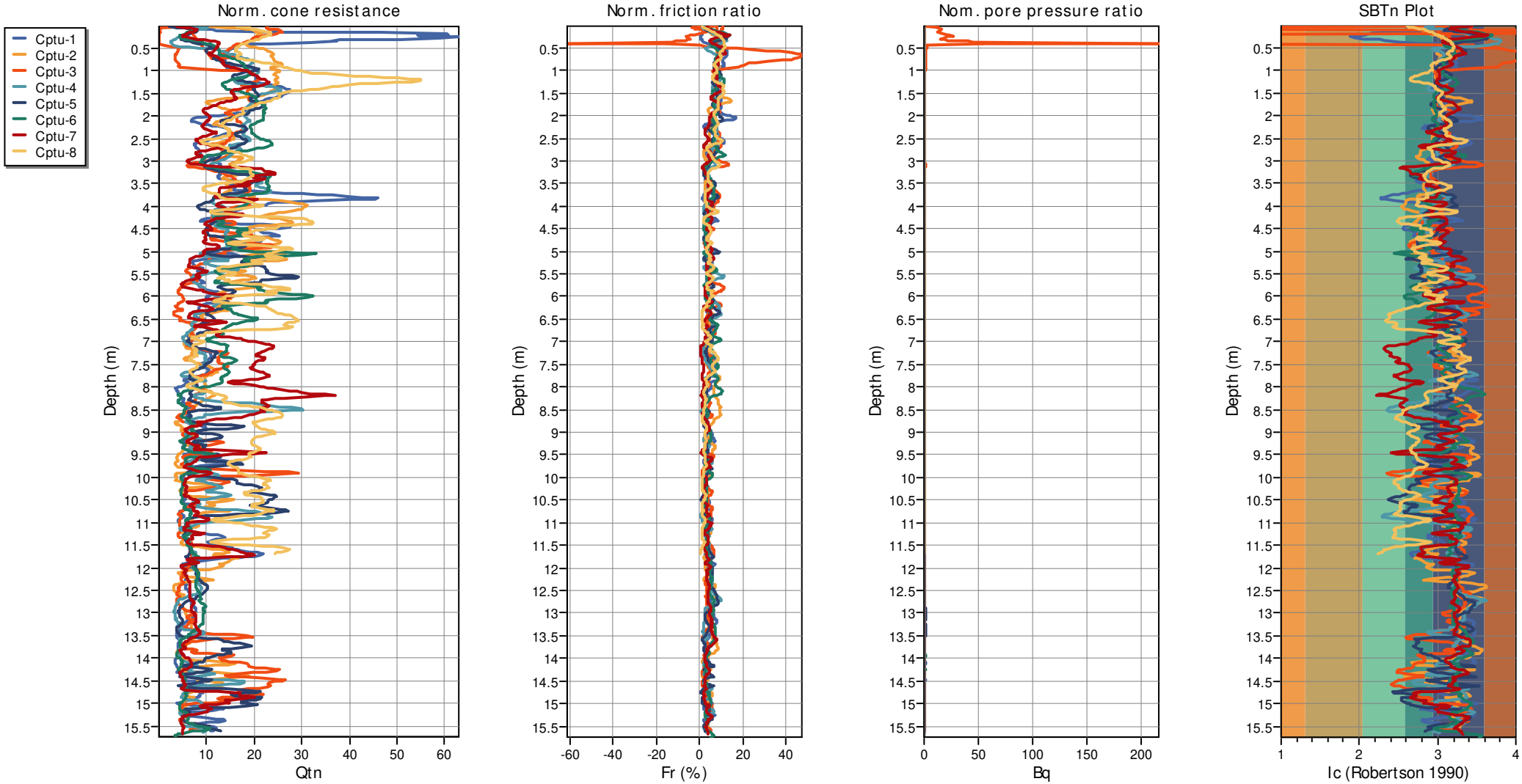
- SISMICA -

REPORT TOMOGRAFIA SISMICA
--
PARAMETRI SISMICI
--

Dott. geol. Maurizio Zamboni
Corso Esperanto, 3/h
40065 Pianoro (BO)
geologozamboni@gmail.com

Project:

Overlay Normalized Plots



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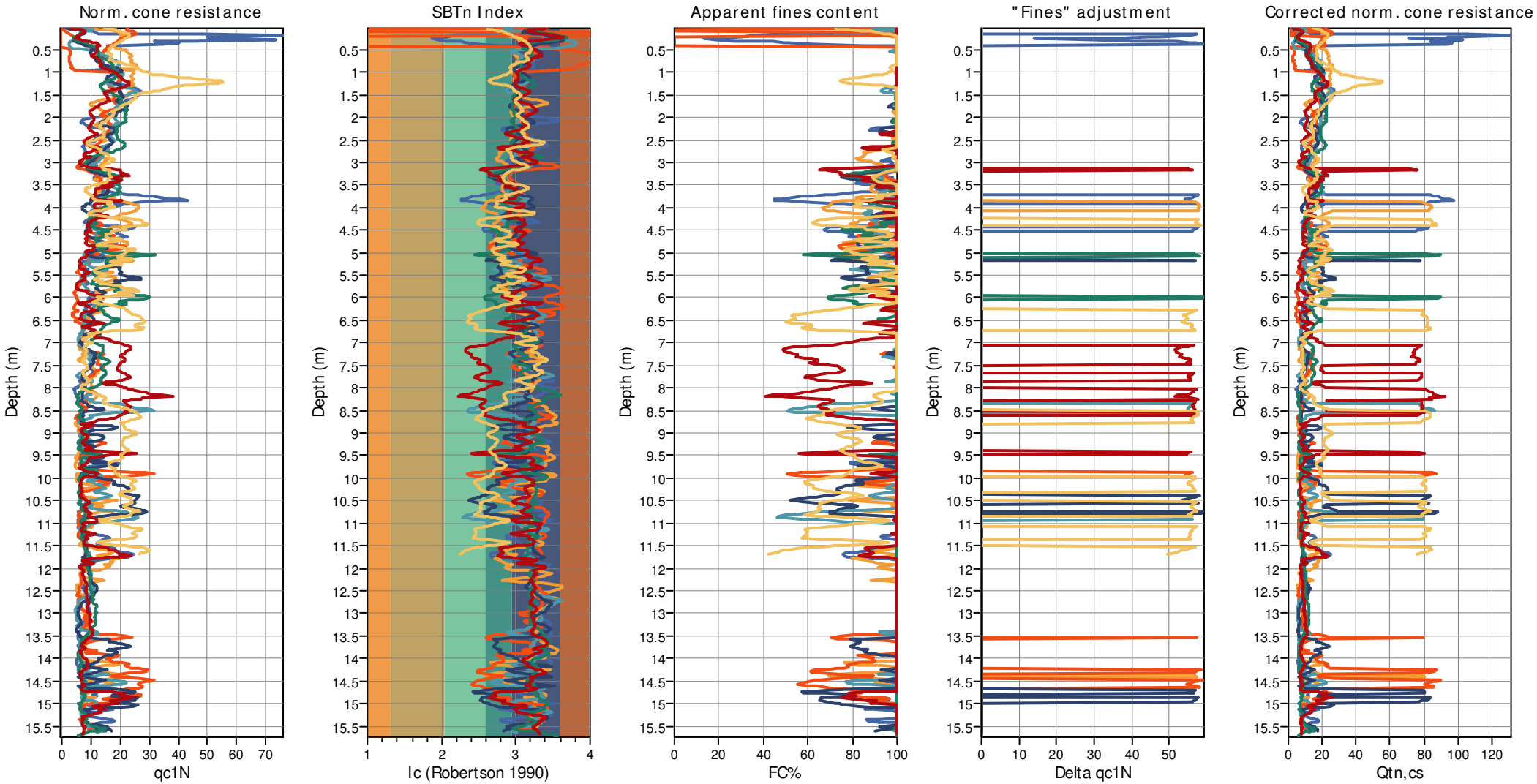
Project:

Overlay Intermediate Results



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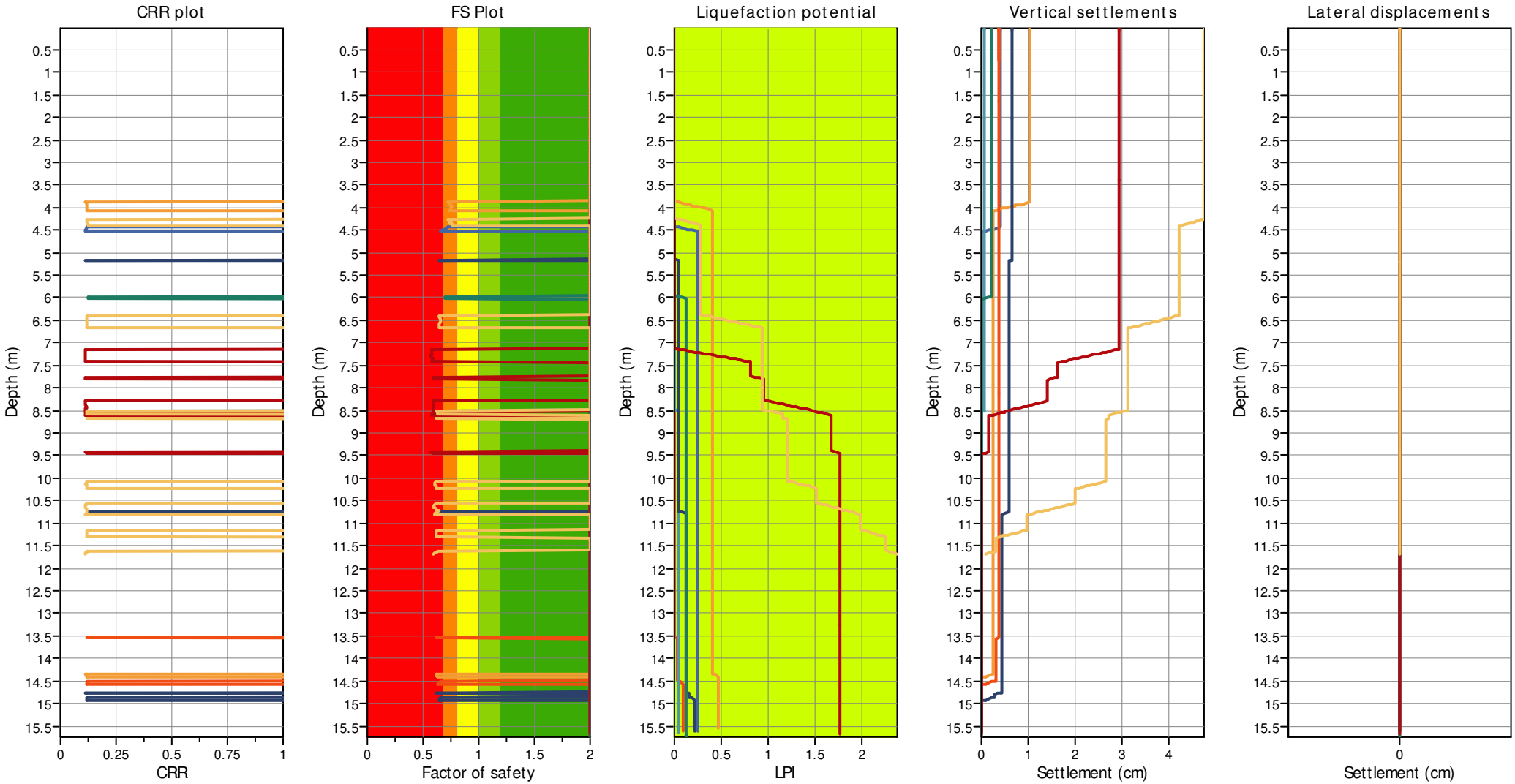
Project:

Overlay Cyclic Liquefaction Plots



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Project:

Overlay Strength Loss Plots

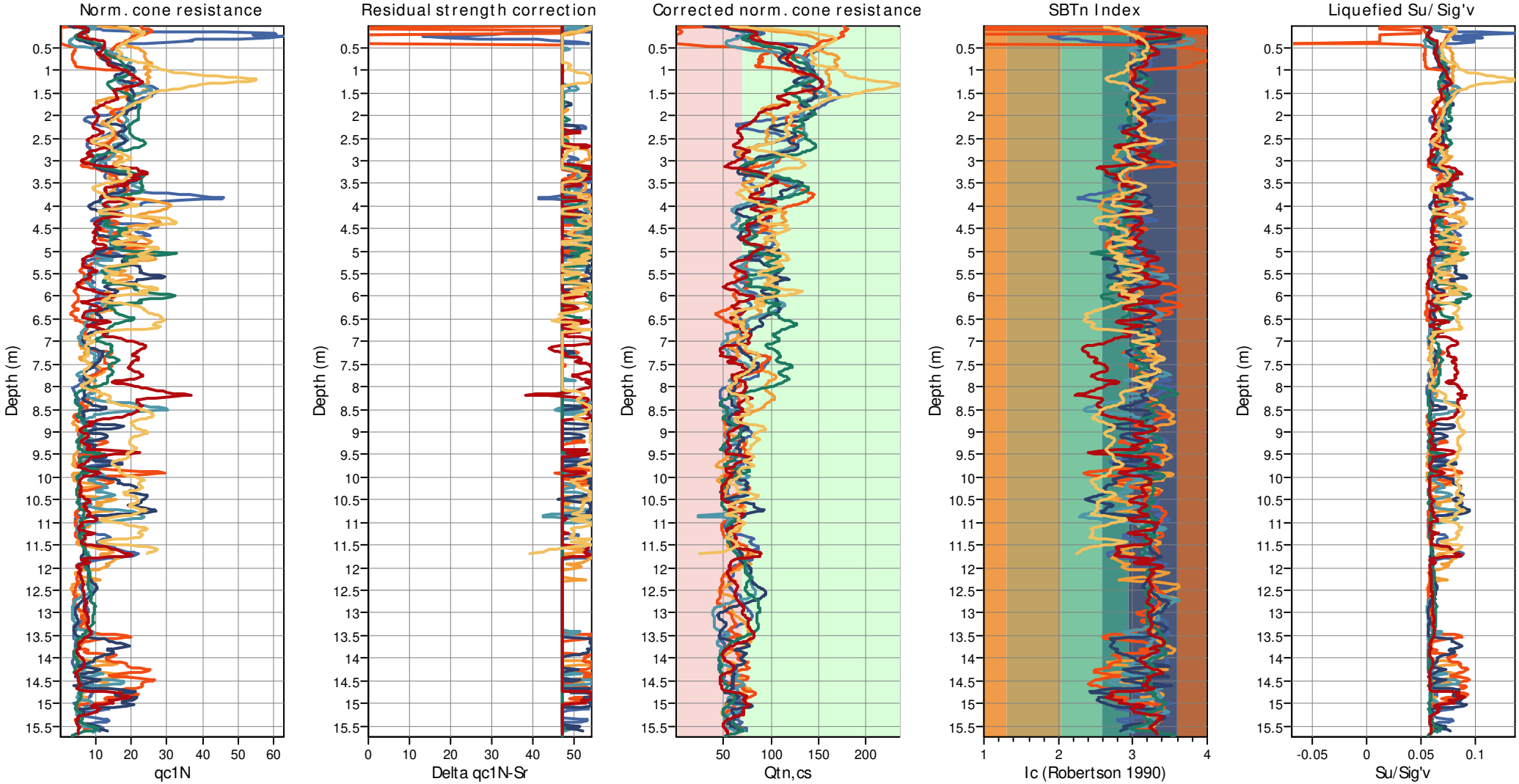

TABLE OF CONTENTS

Dott. geol. Maurizio Zamboni
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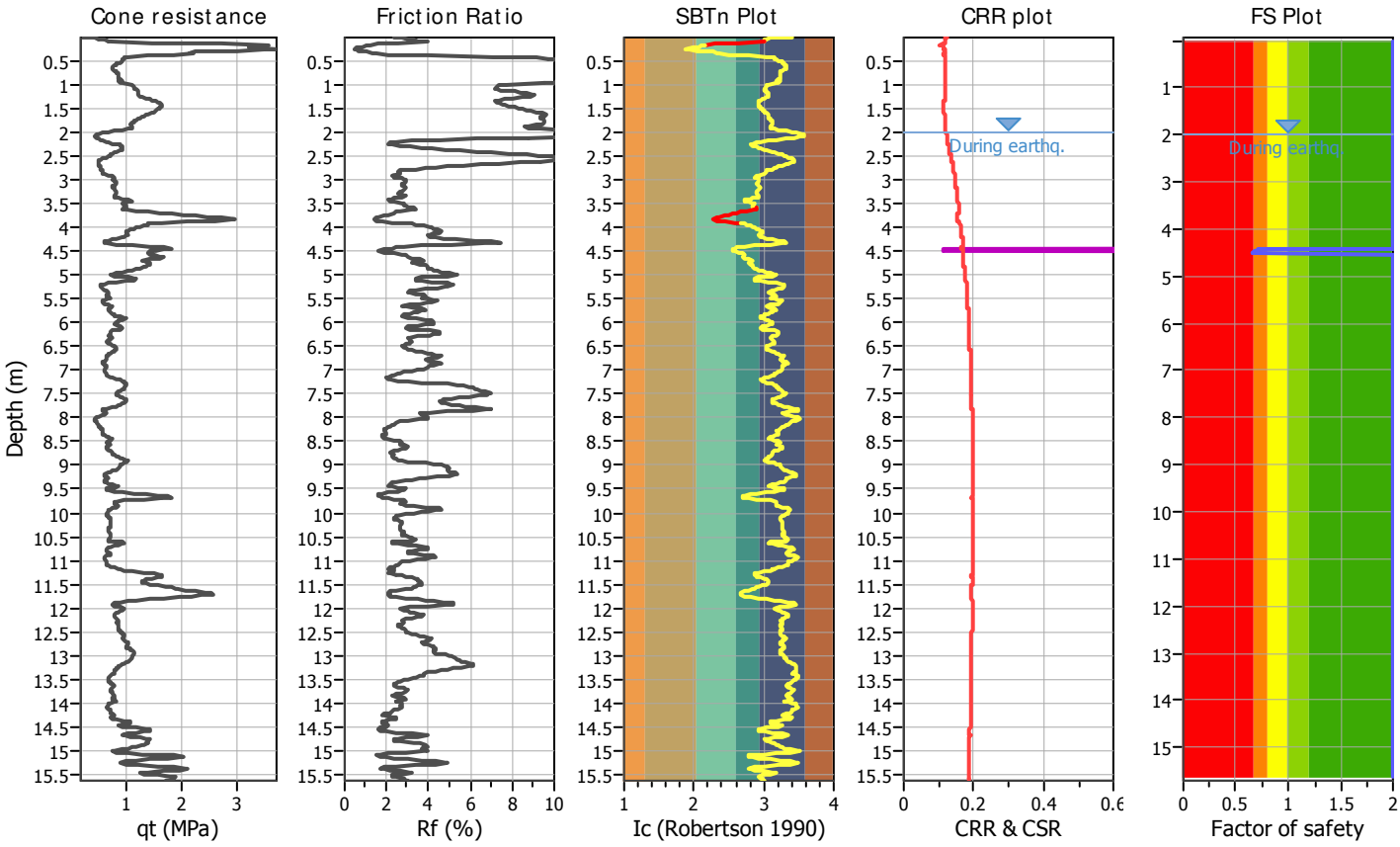
LIQUEFACTION ANALYSIS REPORT

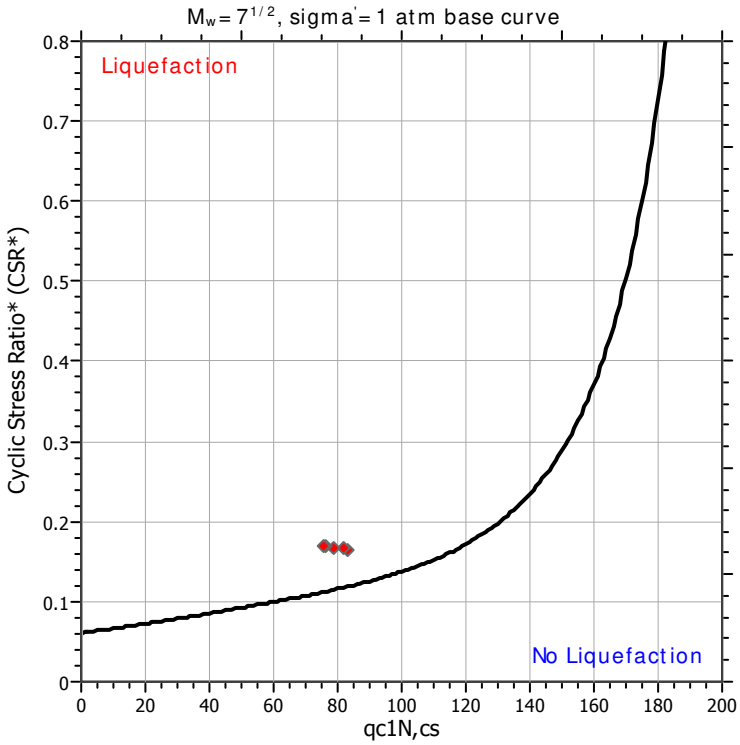
Project title : Location :

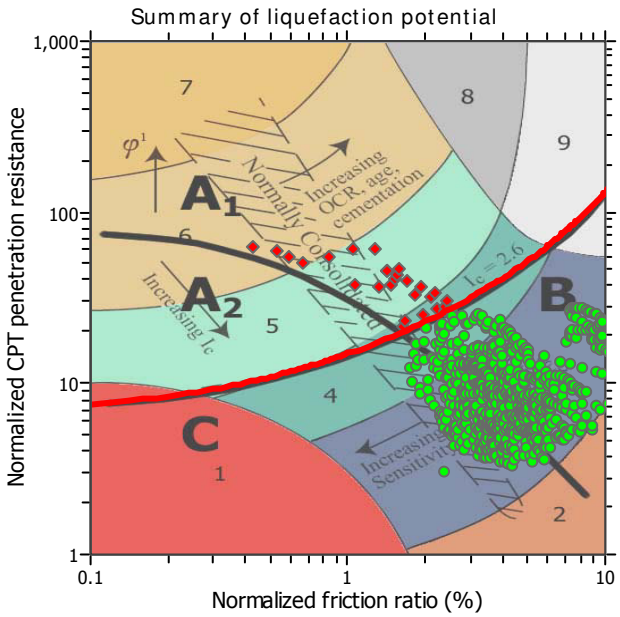
CPT file : Cptu-1

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.50 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.22	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

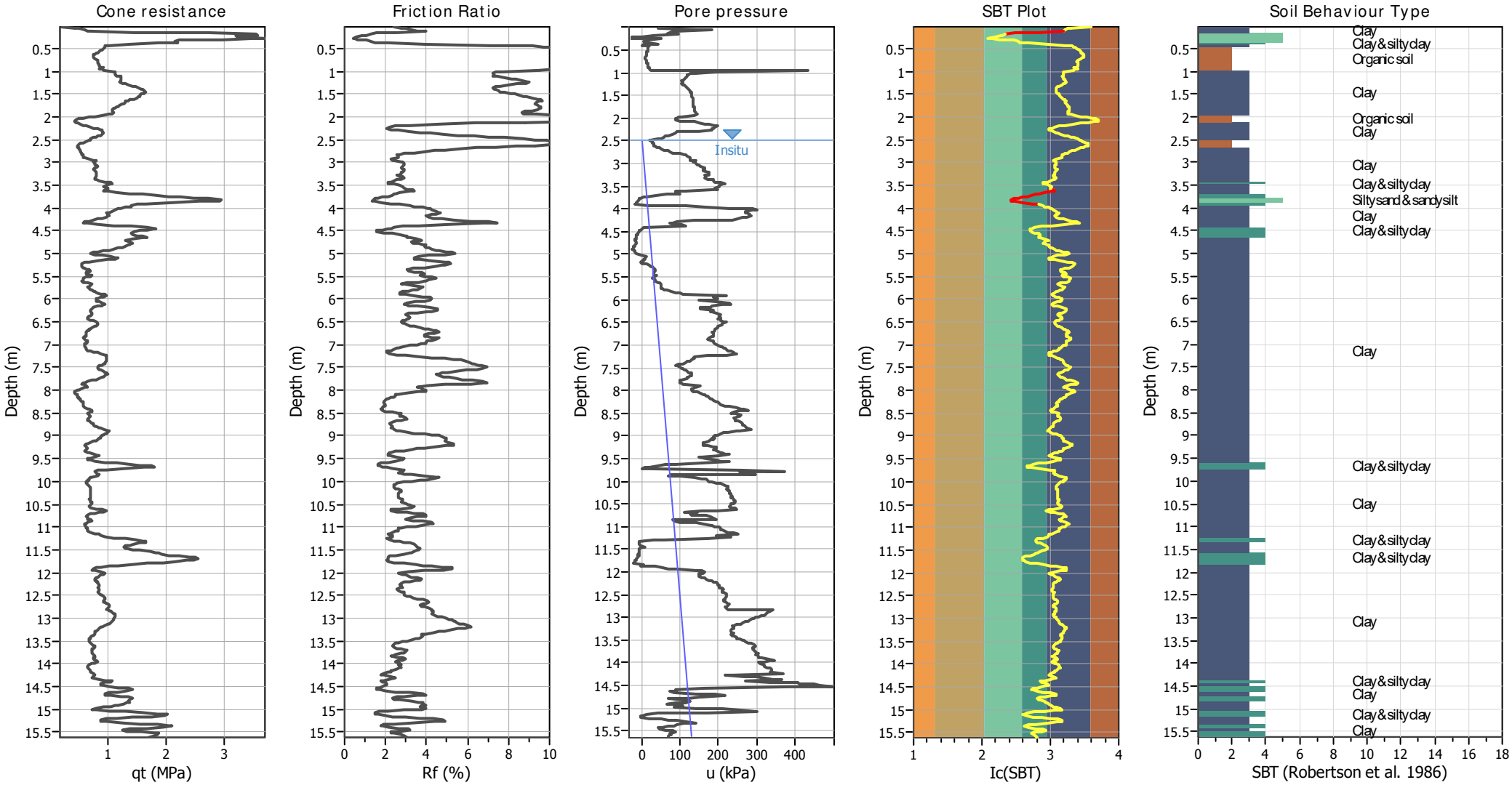






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



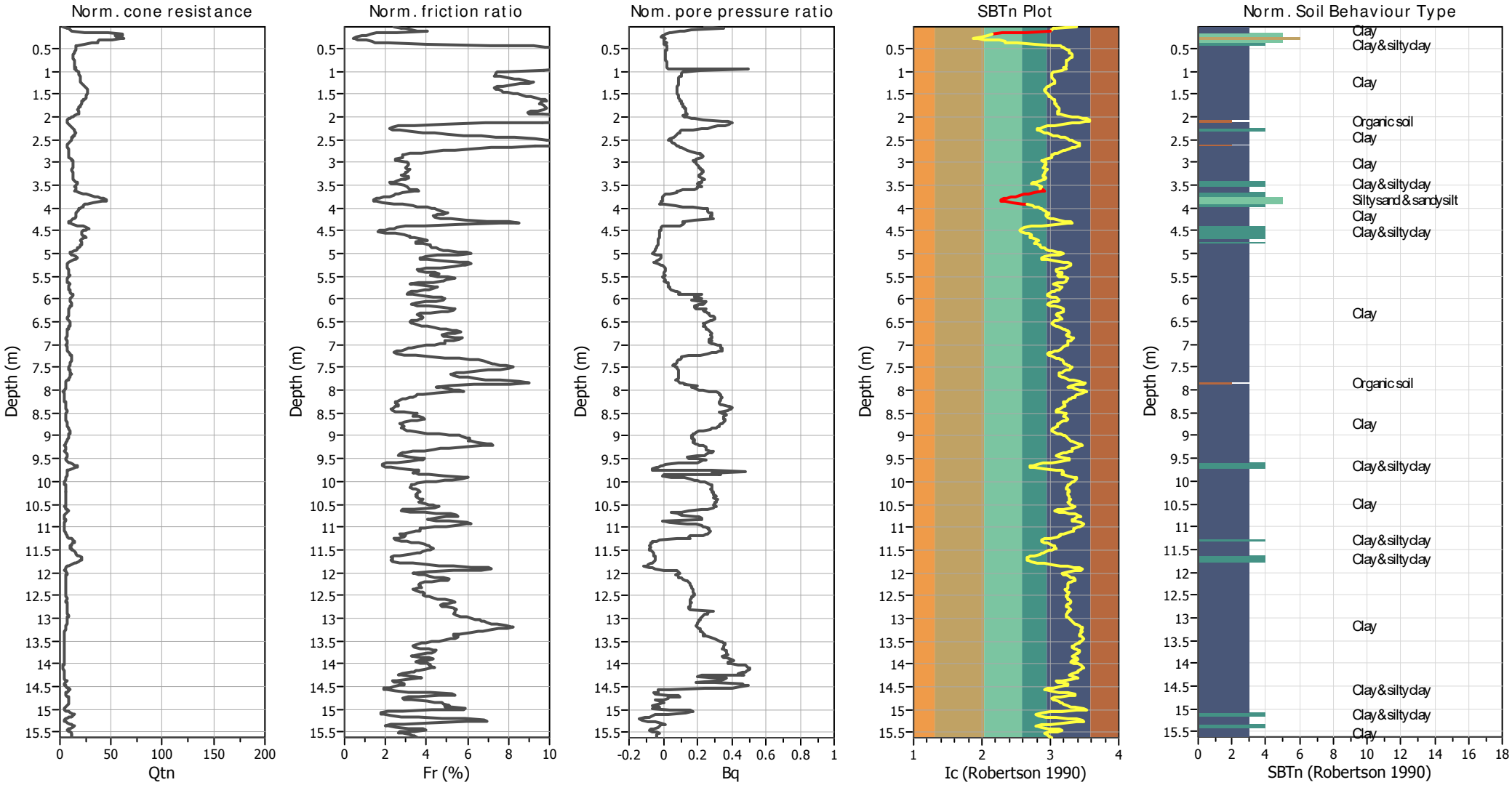
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



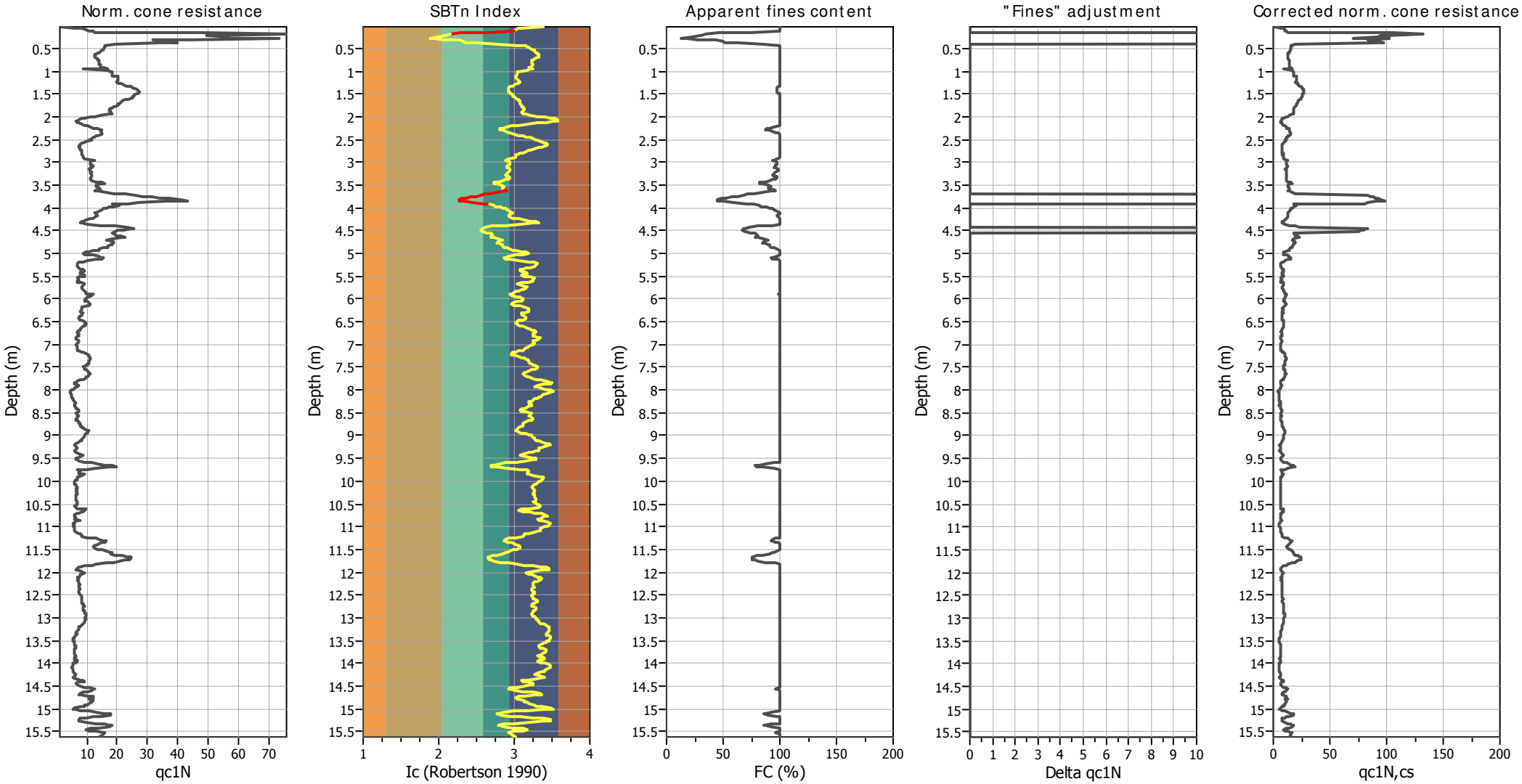
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

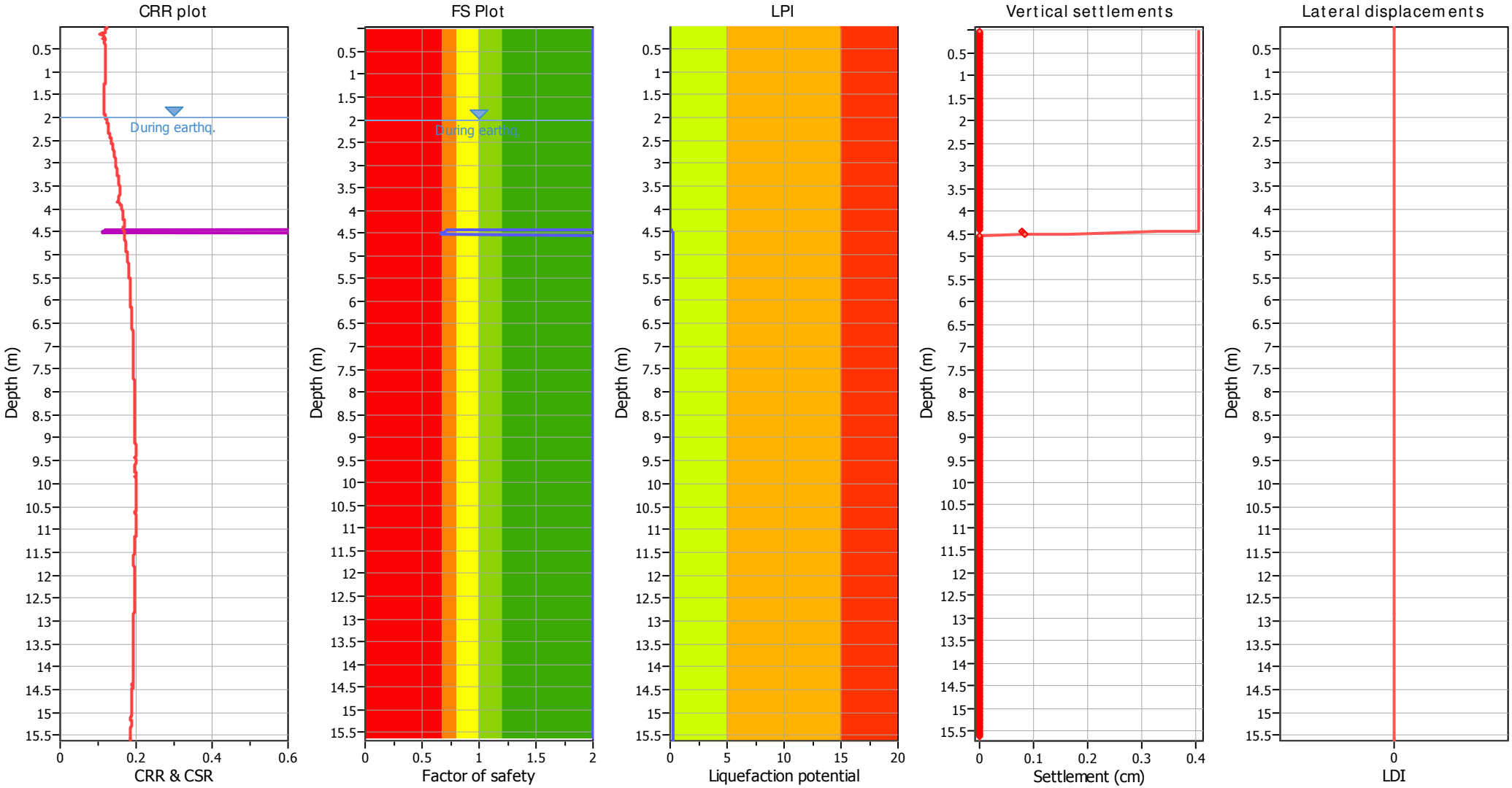
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

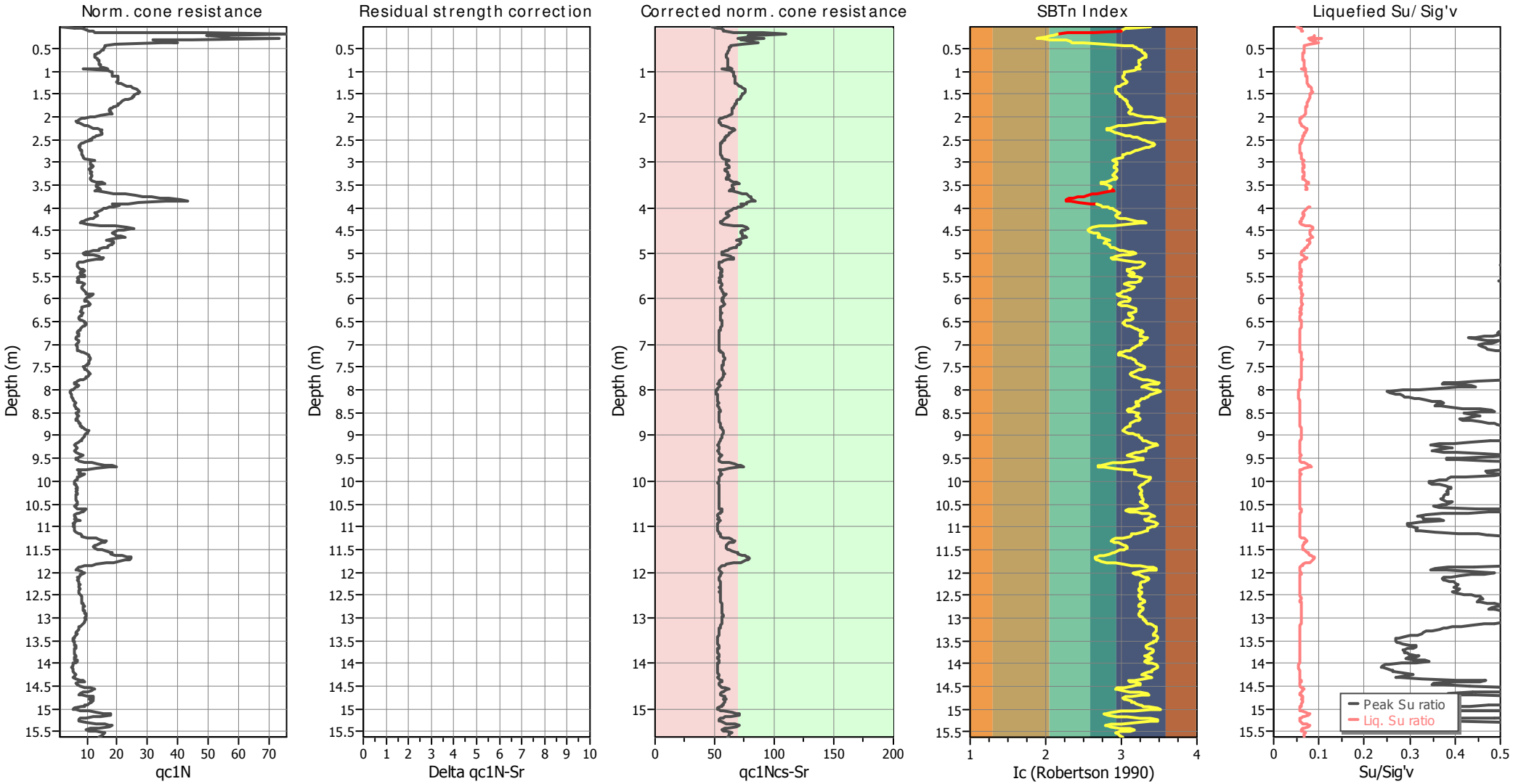
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

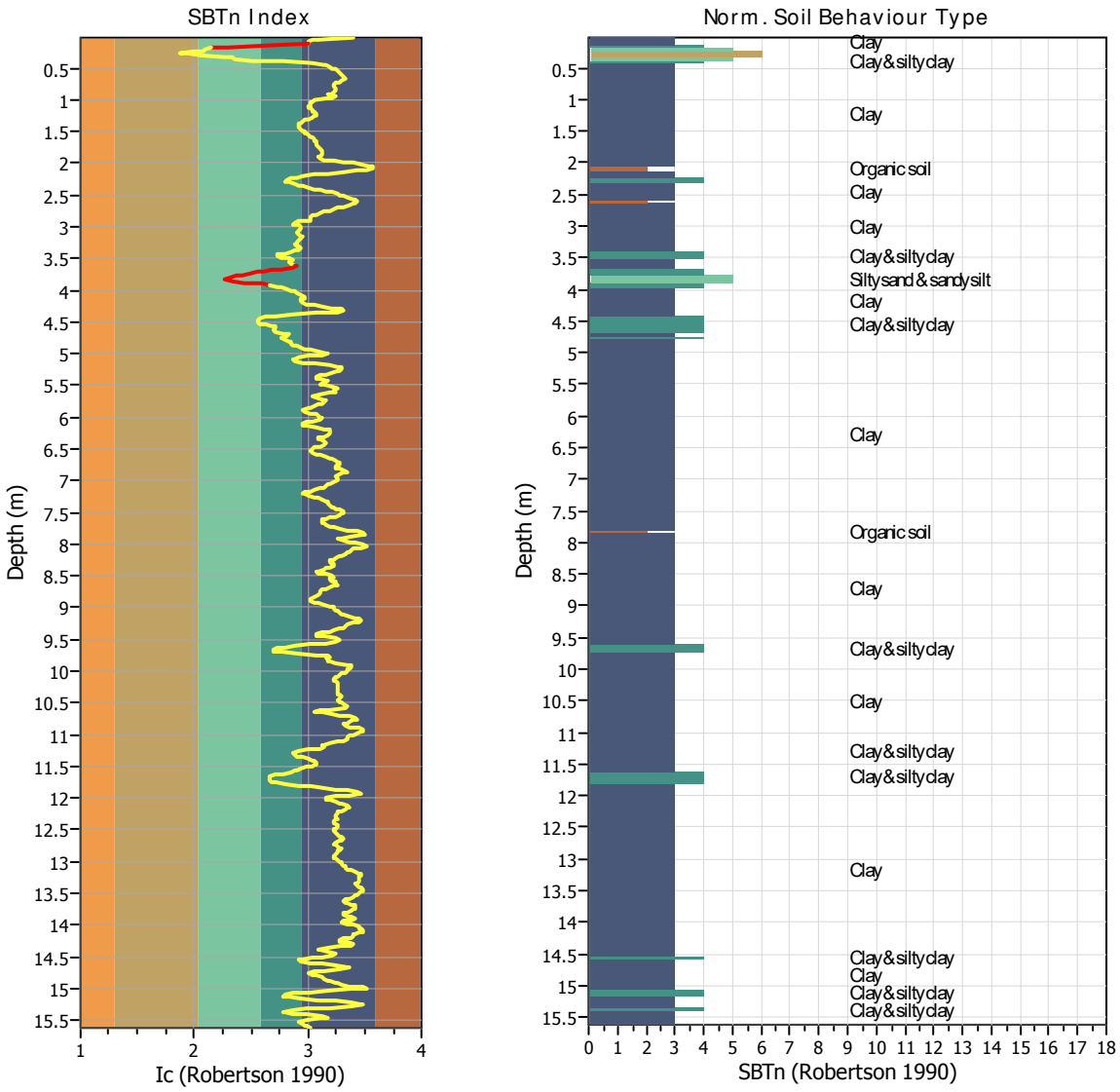
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	781
I_c maximum check value:	3.00	Total points excluded:	21
I_c change ratio value:	0.0100	Exclusion percentage:	2.69%
Minimum number of points in layer:	4	Number of layers detected:	3

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	4	Start depth: 0.14 (m)	4	Clay & silty clay
		End depth: 0.20 (m)	5	Silty sand & sandy silt
Transition layer 2	11	Start depth: 3.62 (m)	3	Clay
		End depth: 3.82 (m)	5	Silty sand & sandy silt
Transition layer 3	6	Start depth: 3.84 (m)	5	Silty sand & sandy silt
		End depth: 3.94 (m)	4	Clay & silty clay

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.06	1.68	42.34	89.12	13.98
2	0.04	0.36	9.33	143.09	64.53	15.53
3	0.06	0.50	17.47	181.90	61.81	15.87
4	0.08	0.59	19.11	96.40	59.41	16.20
5	0.10	0.63	21.78	80.84	58.36	16.44
6	0.12	0.71	28.58	71.79	58.96	16.70
7	0.14	0.74	34.44	64.17	37.46	17.30
8	0.16	2.86	49.32	96.47	22.42	17.70
9	0.18	4.52	45.75	32.61	17.26	17.86
10	0.20	3.26	40.59	2.85	15.66	17.65
11	0.22	2.96	26.79	-26.84	15.21	17.22
12	0.24	3.37	13.28	-29.08	12.78	16.83
13	0.26	3.37	17.15	48.92	5.00	16.67
14	0.28	4.36	16.97	18.85	11.45	16.81
15	0.30	2.67	20.75	11.41	14.40	16.85
16	0.32	1.89	21.89	6.14	21.26	16.95
17	0.34	2.15	28.98	15.69	23.70	17.12
18	0.36	2.39	33.55	41.04	24.43	17.29
19	0.38	2.07	34.37	3.72	30.84	17.45
20	0.40	1.14	50.31	2.23	44.64	17.71
21	0.42	0.95	78.85	18.41	61.70	17.92
22	0.44	0.96	86.93	17.98	68.89	18.12
23	0.46	0.95	97.27	16.74	70.29	18.18
24	0.48	0.94	93.99	16.43	72.37	18.25
25	0.50	0.93	105.09	16.06	74.37	18.31
26	0.52	0.92	116.05	15.44	77.19	18.39
27	0.54	0.88	117.86	14.38	78.41	18.37
28	0.56	0.85	102.68	13.89	79.16	18.32
29	0.58	0.84	104.34	13.76	79.61	18.25
30	0.60	0.80	101.35	13.33	80.97	18.22
31	0.62	0.78	99.73	12.03	82.20	18.19
32	0.64	0.76	97.74	10.73	82.97	18.15
33	0.66	0.74	95.39	9.61	83.37	18.12
34	0.68	0.74	93.86	9.55	83.06	18.10
35	0.70	0.75	91.86	10.29	81.16	18.08
36	0.72	0.80	88.25	11.47	79.10	18.06
37	0.74	0.81	87.31	12.46	76.78	18.05
38	0.76	0.84	86.77	13.45	75.86	18.05
39	0.78	0.83	85.71	14.20	75.18	18.05
40	0.80	0.84	87.26	14.69	75.46	18.06
41	0.82	0.83	89.19	14.57	75.95	18.09
42	0.84	0.84	91.85	15.38	76.30	18.12
43	0.86	0.85	93.04	16.49	76.19	18.13
44	0.88	0.85	92.30	17.48	75.88	18.14
45	0.90	0.86	92.88	18.78	74.50	18.16
46	0.92	0.93	95.05	20.83	71.86	18.20
47	0.94	1.02	95.54	23.81	76.30	18.16
48	0.96	0.53	92.37	434.66	73.59	18.14

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.01	86.98	194.92	71.15	18.10
50	1.00	1.07	83.79	142.96	62.40	18.12
51	1.02	1.10	81.59	125.98	60.87	18.10
52	1.04	1.10	81.59	121.20	60.45	18.10
53	1.06	1.10	81.50	120.46	60.62	18.10
54	1.09	1.09	81.64	120.58	60.00	18.12
55	1.10	1.18	84.69	115.75	59.45	18.17
56	1.12	1.20	90.69	113.83	59.33	18.25
57	1.14	1.20	96.46	111.47	60.11	18.31
58	1.16	1.21	99.71	108.00	61.09	18.36
59	1.18	1.20	102.35	104.90	61.69	18.39
60	1.20	1.21	104.89	105.46	62.53	18.42
61	1.23	1.19	108.64	105.52	63.34	18.45
62	1.24	1.18	110.66	104.84	63.62	18.47
63	1.26	1.21	109.60	106.26	62.70	18.48
64	1.28	1.27	109.42	109.80	60.79	18.49
65	1.30	1.33	108.86	114.26	58.69	18.50
66	1.32	1.39	107.65	117.23	56.68	18.51
67	1.34	1.46	107.82	120.21	55.15	18.53
68	1.36	1.50	109.81	121.57	53.99	18.57
69	1.38	1.57	114.14	123.00	53.64	18.62
70	1.40	1.58	119.94	124.55	53.52	18.67
71	1.42	1.61	123.83	127.03	53.57	18.71
72	1.44	1.63	124.59	128.77	53.73	18.73
73	1.46	1.61	127.34	130.07	54.26	18.76
74	1.48	1.60	131.49	130.75	55.24	18.78
75	1.50	1.56	132.83	130.87	56.24	18.79
76	1.52	1.53	133.19	131.00	57.04	18.79
77	1.54	1.52	133.67	130.81	57.76	18.79
78	1.56	1.50	136.14	132.11	58.47	18.80
79	1.59	1.48	137.94	133.54	59.55	18.80
80	1.60	1.42	136.59	133.04	60.82	18.78
81	1.62	1.36	133.62	132.11	62.22	18.74
82	1.64	1.30	129.22	131.99	62.97	18.69
83	1.66	1.29	125.26	132.55	63.28	18.64
84	1.68	1.26	119.90	133.54	63.16	18.60
85	1.70	1.25	117.08	134.22	63.55	18.57
86	1.72	1.21	116.84	134.78	64.04	18.54
87	1.74	1.19	114.20	135.71	65.01	18.52
88	1.76	1.15	112.93	136.14	65.69	18.48
89	1.78	1.13	109.79	136.52	66.46	18.45
90	1.80	1.10	106.80	136.64	67.05	18.41
91	1.82	1.07	105.27	136.76	67.64	18.37
92	1.84	1.04	101.40	137.38	67.83	18.33
93	1.86	1.04	97.26	138.75	67.08	18.29
94	1.88	1.07	96.18	140.92	66.07	18.27
95	1.90	1.08	94.56	142.78	65.28	18.27
96	1.92	1.08	94.82	143.71	65.93	18.26

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	1.02	95.34	137.88	69.08	18.23
98	1.96	0.88	95.15	101.80	74.61	18.19
99	1.99	0.76	94.24	94.36	82.07	18.11
100	2.00	0.65	90.73	90.82	89.27	18.01
101	2.02	0.56	84.25	88.28	96.44	17.88
102	2.04	0.48	78.21	87.60	100.00	17.73
103	2.06	0.43	70.36	99.63	100.00	17.57
104	2.08	0.41	60.69	136.14	100.00	17.38
105	2.10	0.39	48.88	149.29	100.00	17.15
106	2.12	0.41	37.80	163.17	92.45	16.90
107	2.14	0.44	30.80	175.02	81.91	16.65
108	2.16	0.49	23.50	189.46	71.79	16.40
109	2.18	0.54	17.56	196.84	62.46	16.15
110	2.20	0.60	14.89	189.21	55.92	15.98
111	2.22	0.65	14.65	186.17	51.76	15.96
112	2.24	0.71	15.53	185.00	48.60	16.05
113	2.26	0.81	16.70	181.34	46.63	16.19
114	2.28	0.87	19.34	147.30	46.37	16.38
115	2.30	0.90	23.68	93.86	48.16	16.58
116	2.32	0.88	27.43	87.48	50.92	16.81
117	2.34	0.91	34.96	89.40	53.24	17.00
118	2.36	0.92	38.86	79.60	55.23	17.18
119	2.38	0.92	43.28	70.99	58.30	17.30
120	2.40	0.85	49.37	61.19	61.92	17.40
121	2.42	0.83	52.80	58.28	66.31	17.47
122	2.44	0.77	55.59	49.47	69.69	17.52
123	2.46	0.74	57.72	42.90	73.52	17.56
124	2.48	0.72	62.56	23.25	77.56	17.61
125	2.50	0.67	66.66	19.47	79.36	17.66
126	2.52	0.72	67.16	29.45	82.48	17.66
127	2.54	0.61	64.99	28.33	84.65	17.61
128	2.56	0.57	61.03	30.01	89.38	17.50
129	2.58	0.53	56.67	32.05	91.84	17.38
130	2.60	0.49	51.07	32.49	92.86	17.25
131	2.62	0.47	45.21	35.83	91.81	17.10
132	2.64	0.48	40.28	40.92	89.57	16.96
133	2.66	0.47	35.83	44.82	86.34	16.82
134	2.68	0.48	31.14	50.59	82.72	16.70
135	2.70	0.50	28.80	59.27	78.60	16.58
136	2.72	0.51	25.69	68.51	74.60	16.48
137	2.74	0.53	22.79	71.92	72.05	16.36
138	2.76	0.51	21.23	81.96	69.17	16.24
139	2.78	0.52	18.39	100.00	66.50	16.12
140	2.80	0.54	16.25	110.54	63.21	15.97
141	2.82	0.54	14.11	113.70	61.38	15.87
142	2.84	0.53	14.26	119.53	60.44	15.85
143	2.86	0.56	15.17	124.55	60.40	15.87
144	2.88	0.55	15.05	124.92	59.94	15.90

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.56	15.11	125.11	59.47	15.93
146	2.92	0.59	15.93	126.91	53.65	16.00
147	2.94	0.82	15.91	139.80	51.58	16.16
148	2.96	0.75	20.19	133.54	50.46	16.30
149	2.98	0.74	21.36	137.45	53.46	16.40
150	3.00	0.74	21.98	142.59	54.16	16.42
151	3.02	0.73	21.80	144.58	54.27	16.45
152	3.04	0.75	22.88	147.86	54.09	16.49
153	3.06	0.77	23.70	154.00	53.08	16.53
154	3.08	0.81	23.38	163.73	52.41	16.53
155	3.10	0.78	22.44	164.48	52.12	16.49
156	3.12	0.75	21.39	164.79	53.08	16.44
157	3.14	0.73	21.54	161.50	54.45	16.42
158	3.16	0.70	22.27	161.56	55.04	16.44
159	3.18	0.74	22.59	170.30	54.68	16.46
160	3.20	0.75	22.06	176.26	53.23	16.47
161	3.22	0.78	22.24	175.70	52.90	16.47
162	3.24	0.75	22.50	174.27	52.39	16.46
163	3.26	0.78	21.42	164.85	52.12	16.43
164	3.28	0.77	20.27	166.77	51.21	16.41
165	3.30	0.79	21.06	167.20	51.90	16.44
166	3.32	0.77	23.56	165.16	53.43	16.50
167	3.34	0.74	23.91	172.72	54.19	16.50
168	3.36	0.75	21.30	187.72	53.17	16.43
169	3.38	0.77	19.75	187.41	51.20	16.39
170	3.40	0.80	20.77	191.75	48.84	16.40
171	3.42	0.89	20.89	207.01	45.84	16.47
172	3.44	1.01	21.74	217.11	42.56	16.56
173	3.46	1.11	23.14	212.71	42.10	16.65
174	3.48	1.02	25.60	203.72	44.42	16.71
175	3.50	0.88	26.28	202.73	47.92	16.73
176	3.52	0.88	26.31	202.60	49.79	16.73
177	3.54	0.91	27.13	188.96	49.07	16.79
178	3.56	0.98	29.47	197.95	48.41	16.87
179	3.58	1.00	30.96	186.24	48.84	16.92
180	3.60	0.94	31.02	114.63	51.44	16.95
181	3.62	0.86	33.25	88.16	52.57	16.94
182	3.64	0.94	30.96	88.72	49.72	16.97
183	3.66	1.15	31.20	99.38	43.95	17.00
184	3.68	1.34	31.43	65.59	39.26	17.17
185	3.70	1.60	39.55	37.82	35.97	17.37
186	3.72	1.85	44.47	12.40	33.31	17.54
187	3.74	2.03	44.03	5.33	30.37	17.59
188	3.76	2.25	41.04	-1.43	27.68	17.60
189	3.78	2.48	40.75	-5.46	25.21	17.60
190	3.80	2.69	40.54	-7.75	23.12	17.64
191	3.82	2.99	41.13	-8.62	21.43	17.67
192	3.84	3.18	41.04	-9.24	21.51	17.66

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	2.64	39.46	-12.65	23.75	17.55
194	3.88	1.96	35.18	-15.75	28.27	17.41
195	3.90	1.69	35.30	-16.37	34.93	17.36
196	3.92	1.31	42.94	14.69	38.74	17.40
197	3.94	1.51	43.35	113.70	42.60	17.48
198	3.96	1.34	47.22	165.53	43.61	17.55
199	3.98	1.26	51.26	227.59	47.13	17.58
200	4.00	1.17	50.15	288.16	49.15	17.57
201	4.02	1.12	48.22	299.32	50.76	17.53
202	4.04	1.07	48.83	290.82	52.09	17.48
203	4.06	1.02	46.28	271.92	54.26	17.45
204	4.09	0.95	47.42	269.13	56.22	17.42
205	4.10	0.92	46.81	273.71	57.06	17.39
206	4.12	0.94	44.11	280.97	56.38	17.35
207	4.14	0.95	43.03	282.58	54.84	17.31
208	4.16	0.97	41.09	284.62	53.89	17.27
209	4.18	0.97	39.72	272.85	53.87	17.24
210	4.20	0.92	39.74	264.23	55.24	17.21
211	4.22	0.86	39.51	252.51	57.79	17.17
212	4.24	0.80	38.43	237.32	62.01	17.14
213	4.26	0.71	40.07	139.49	67.40	17.12
214	4.28	0.65	41.47	92.06	74.19	17.12
215	4.30	0.58	42.97	80.16	80.14	17.12
216	4.32	0.55	44.11	75.02	82.76	17.13
217	4.34	0.58	43.70	87.72	77.42	17.15
218	4.36	0.74	41.65	102.05	64.22	17.20
219	4.38	1.06	39.71	115.87	50.48	17.26
220	4.40	1.44	38.45	11.66	41.46	17.36
221	4.42	1.72	41.15	3.41	36.42	17.46
222	4.44	1.91	43.67	1.30	34.41	17.51
223	4.46	1.83	39.95	-2.05	33.81	17.41
224	4.48	1.67	31.89	-4.90	33.58	17.15
225	4.50	1.52	22.22	-6.76	33.13	16.83
226	4.52	1.45	19.20	-7.38	34.21	16.71
227	4.54	1.36	26.09	-9.36	37.05	16.89
228	4.56	1.39	34.70	-10.60	39.76	17.14
229	4.58	1.44	38.22	-12.09	41.18	17.35
230	4.60	1.48	44.69	-13.08	41.30	17.51
231	4.62	1.62	50.85	-12.40	40.52	17.64
232	4.64	1.74	50.61	-13.27	40.09	17.71
233	4.66	1.65	51.67	-14.07	41.64	17.69
234	4.68	1.40	50.93	-16.24	45.46	17.65
235	4.70	1.23	50.29	-18.16	48.25	17.56
236	4.72	1.27	45.51	-12.65	46.99	17.49
237	4.74	1.44	42.09	-12.65	44.81	17.49
238	4.76	1.45	47.24	-14.76	44.40	17.56
239	4.78	1.41	52.08	-16.55	45.93	17.64
240	4.80	1.40	53.34	-17.92	47.53	17.68

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	1.35	54.13	-19.22	48.55	17.67
242	4.84	1.29	51.17	-20.33	49.14	17.61
243	4.86	1.28	47.95	-20.83	50.29	17.56
244	4.88	1.19	49.56	-22.19	52.27	17.52
245	4.90	1.08	48.30	-23.50	54.40	17.46
246	4.92	1.06	43.77	-18.29	57.10	17.38
247	4.94	0.94	43.89	-18.85	60.10	17.29
248	4.96	0.82	41.11	-17.11	65.23	17.19
249	4.98	0.73	38.38	-14.14	69.79	17.09
250	5.00	0.68	37.74	-13.08	71.86	17.05
251	5.02	0.72	38.59	-2.05	67.09	17.07
252	5.04	0.92	37.09	11.66	59.27	17.12
253	5.06	1.08	36.54	11.66	53.52	17.19
254	5.08	1.12	40.23	10.35	50.78	17.25
255	5.10	1.19	40.11	7.75	50.10	17.29
256	5.12	1.18	39.35	5.95	50.73	17.23
257	5.14	1.02	35.39	3.16	55.13	17.12
258	5.16	0.79	34.72	-0.43	62.54	16.99
259	5.18	0.68	33.25	-1.43	72.16	16.86
260	5.20	0.56	30.85	0.25	77.83	16.72
261	5.22	0.54	27.48	13.02	81.25	16.59
262	5.24	0.53	26.05	20.33	80.64	16.52
263	5.26	0.54	26.11	24.55	80.10	16.50
264	5.28	0.54	25.58	27.34	77.80	16.44
265	5.30	0.56	21.71	31.93	74.23	16.34
266	5.32	0.58	19.19	33.23	69.73	16.24
267	5.34	0.62	19.28	34.28	66.28	16.25
268	5.36	0.68	21.07	35.71	63.72	16.31
269	5.38	0.71	21.22	34.84	63.76	16.39
270	5.40	0.67	23.09	32.92	66.16	16.43
271	5.42	0.61	23.79	31.18	70.02	16.45
272	5.44	0.60	23.91	29.82	71.40	16.47
273	5.46	0.64	25.06	31.87	68.62	16.55
274	5.48	0.74	26.79	38.25	65.71	16.62
275	5.50	0.74	26.79	33.11	68.27	16.65
276	5.52	0.57	28.05	26.22	73.81	16.57
277	5.54	0.53	24.36	31.99	78.16	16.48
278	5.56	0.58	23.10	36.76	76.39	16.40
279	5.59	0.58	22.72	35.46	75.88	16.36
280	5.60	0.53	22.31	34.04	76.31	16.32
281	5.62	0.55	21.02	42.34	72.75	16.30
282	5.64	0.66	20.29	48.54	65.83	16.29
283	5.66	0.73	19.41	51.89	61.17	16.32
284	5.68	0.74	20.70	52.20	61.36	16.39
285	5.70	0.71	24.07	50.28	65.29	16.50
286	5.72	0.65	26.47	50.71	68.93	16.55
287	5.74	0.64	24.95	51.33	70.46	16.54
288	5.76	0.65	24.25	53.81	69.01	16.52

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	0.69	24.86	59.76	67.17	16.53
290	5.80	0.71	24.63	63.86	64.74	16.54
291	5.82	0.74	23.49	78.61	62.33	16.50
292	5.84	0.76	21.85	88.53	59.79	16.45
293	5.86	0.79	21.00	99.50	58.30	16.44
294	5.88	0.80	22.12	106.20	55.51	16.60
295	5.90	0.98	28.91	222.13	55.16	16.81
296	5.92	0.96	33.77	193.18	56.32	17.00
297	5.94	0.88	36.32	186.92	60.49	17.07
298	5.96	0.82	36.59	189.40	64.00	17.06
299	5.98	0.79	35.68	197.58	65.38	17.03
300	6.00	0.80	34.74	194.48	66.45	16.98
301	6.02	0.74	32.78	147.30	67.12	16.93
302	6.04	0.73	32.63	191.07	65.50	16.86
303	6.06	0.81	28.32	223.81	61.66	16.82
304	6.08	0.87	27.41	229.45	57.48	16.77
305	6.10	0.90	27.56	231.43	55.55	16.77
306	6.12	0.92	26.80	208.37	55.99	16.78
307	6.14	0.87	28.73	183.69	58.10	16.80
308	6.16	0.82	29.85	178.49	63.22	16.81
309	6.18	0.69	30.32	154.31	68.51	16.83
310	6.20	0.67	32.92	152.63	72.83	16.87
311	6.22	0.68	34.51	187.85	72.89	16.87
312	6.24	0.69	30.61	180.04	73.05	16.84
313	6.26	0.65	30.87	178.18	72.74	16.76
314	6.28	0.64	28.03	184.07	71.77	16.68
315	6.30	0.68	24.84	193.30	68.18	16.57
316	6.32	0.71	22.64	206.57	65.45	16.47
317	6.34	0.69	21.56	205.39	64.79	16.42
318	6.36	0.67	21.67	200.99	66.51	16.39
319	6.38	0.63	21.88	203.84	68.14	16.35
320	6.40	0.61	20.09	204.28	69.61	16.31
321	6.42	0.60	20.18	199.13	70.03	16.28
322	6.44	0.60	20.53	204.09	68.88	16.29
323	6.46	0.66	20.27	206.76	66.45	16.33
324	6.48	0.71	21.23	214.38	62.94	16.39
325	6.50	0.77	21.94	219.84	60.92	16.46
326	6.52	0.79	23.14	210.85	60.28	16.54
327	6.54	0.79	25.16	209.98	60.51	16.59
328	6.56	0.79	24.49	209.86	61.78	16.61
329	6.58	0.76	25.28	198.33	63.69	16.63
330	6.60	0.72	26.80	199.07	66.26	16.64
331	6.62	0.70	26.57	197.46	69.32	16.66
332	6.64	0.66	27.92	189.09	72.05	16.68
333	6.66	0.64	28.65	189.65	74.12	16.69
334	6.68	0.65	28.39	189.58	76.15	16.71
335	6.70	0.61	30.15	185.18	78.04	16.71
336	6.72	0.59	29.30	183.14	79.77	16.69

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	0.59	28.16	187.54	78.99	16.63
338	6.76	0.60	25.67	187.97	77.35	16.57
339	6.78	0.60	24.49	186.98	76.25	16.51
340	6.80	0.60	24.29	185.99	77.09	16.48
341	6.82	0.57	24.47	181.40	79.10	16.47
342	6.84	0.54	24.52	176.07	81.99	16.49
343	6.86	0.54	26.34	173.09	84.56	16.53
344	6.88	0.53	27.63	170.61	82.69	16.56
345	6.90	0.60	25.57	183.01	80.02	16.57
346	6.92	0.61	25.83	185.06	77.06	16.56
347	6.94	0.61	26.16	185.31	77.23	16.55
348	6.96	0.59	25.07	190.02	77.66	16.51
349	6.98	0.58	23.55	190.14	77.94	16.42
350	7.00	0.55	21.21	196.71	77.38	16.31
351	7.02	0.56	19.07	205.15	75.41	16.20
352	7.04	0.58	17.45	210.17	72.89	16.10
353	7.06	0.58	16.37	214.51	70.83	16.03
354	7.08	0.58	15.70	216.99	70.03	15.98
355	7.10	0.58	15.08	219.78	68.70	15.93
356	7.12	0.60	14.29	225.36	66.45	15.91
357	7.14	0.64	14.44	233.11	62.87	15.93
358	7.16	0.71	14.94	241.17	59.80	16.01
359	7.18	0.76	16.25	245.44	57.13	16.15
360	7.20	0.85	19.01	245.82	56.00	16.36
361	7.22	0.91	23.05	221.33	56.50	16.61
362	7.24	0.94	29.50	171.54	58.71	16.85
363	7.26	0.94	34.92	139.12	61.85	17.09
364	7.28	0.95	42.36	134.84	64.91	17.28
365	7.30	0.95	48.43	136.02	67.45	17.43
366	7.32	0.96	53.23	130.01	69.32	17.54
367	7.34	0.96	56.28	126.84	70.75	17.61
368	7.36	0.95	57.83	117.73	71.81	17.64
369	7.38	0.95	58.77	116.49	73.03	17.65
370	7.41	0.92	59.06	107.56	74.30	17.65
371	7.42	0.90	58.71	97.27	75.40	17.63
372	7.44	0.89	56.98	88.84	77.26	17.61
373	7.46	0.83	57.98	93.49	79.24	17.59
374	7.48	0.81	58.01	100.99	81.59	17.58
375	7.50	0.79	57.27	104.03	82.01	17.56
376	7.52	0.80	55.54	107.25	81.20	17.54
377	7.54	0.83	54.96	110.91	79.12	17.53
378	7.56	0.85	53.14	115.44	76.19	17.51
379	7.58	0.91	50.85	118.91	72.82	17.47
380	7.60	0.94	47.75	124.24	69.93	17.44
381	7.62	0.96	46.87	128.33	67.90	17.40
382	7.64	0.98	45.23	129.01	66.99	17.37
383	7.66	0.96	44.02	129.26	66.83	17.34
384	7.68	0.94	43.35	127.53	68.14	17.33

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	0.91	44.99	121.82	70.31	17.34
386	7.72	0.88	46.69	119.22	72.82	17.36
387	7.74	0.85	47.24	118.60	75.52	17.36
388	7.76	0.80	46.83	102.73	79.44	17.33
389	7.78	0.71	45.90	98.70	85.07	17.26
390	7.80	0.63	44.20	100.06	92.03	17.18
391	7.82	0.56	42.41	99.57	97.10	17.09
392	7.84	0.54	38.84	103.47	100.00	16.97
393	7.86	0.53	34.73	107.56	97.14	16.85
394	7.88	0.55	30.48	111.90	88.30	16.69
395	7.90	0.66	23.65	152.63	81.52	16.55
396	7.92	0.63	22.92	140.61	78.11	16.44
397	7.94	0.58	22.92	137.01	81.96	16.37
398	7.96	0.53	21.13	134.04	86.38	16.28
399	7.98	0.49	19.78	130.25	91.90	16.17
400	8.00	0.43	18.76	131.93	97.12	16.07
401	8.02	0.40	17.55	134.41	100.00	15.95
402	8.04	0.39	15.56	143.96	100.00	15.81
403	8.06	0.41	13.07	153.94	95.50	15.65
404	8.08	0.43	11.40	158.96	90.40	15.55
405	8.10	0.44	11.76	164.91	87.71	15.52
406	8.12	0.44	11.79	168.20	86.81	15.53
407	8.14	0.44	11.61	171.67	85.57	15.52
408	8.16	0.45	11.08	175.57	83.41	15.48
409	8.18	0.47	10.61	179.17	80.92	15.46
410	8.20	0.49	10.65	182.58	78.79	15.46
411	8.22	0.50	10.76	188.65	76.87	15.47
412	8.24	0.52	10.65	193.99	74.85	15.49
413	8.26	0.54	10.79	198.76	72.80	15.52
414	8.28	0.56	11.20	201.98	72.44	15.56
415	8.30	0.54	11.50	202.91	73.41	15.58
416	8.32	0.52	11.47	205.52	74.67	15.57
417	8.34	0.52	11.09	217.05	74.66	15.55
418	8.36	0.53	10.97	229.76	72.67	15.55
419	8.38	0.56	11.12	248.61	70.38	15.58
420	8.40	0.59	11.47	257.22	68.14	15.66
421	8.42	0.63	12.79	267.70	65.44	15.75
422	8.44	0.69	13.09	279.29	64.01	15.84
423	8.46	0.69	14.14	256.42	64.81	15.95
424	8.48	0.66	16.43	241.48	69.37	16.05
425	8.50	0.59	17.78	234.16	74.10	16.12
426	8.52	0.58	18.24	242.96	75.16	16.15
427	8.54	0.64	17.78	257.22	73.19	16.17
428	8.56	0.66	18.25	256.29	72.04	16.21
429	8.58	0.64	19.62	250.15	73.67	16.26
430	8.60	0.62	20.62	243.83	75.95	16.30
431	8.62	0.61	20.50	239.86	77.31	16.28
432	8.64	0.60	19.13	242.96	77.39	16.22

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	0.59	18.10	245.26	75.55	16.16
434	8.68	0.64	17.31	252.88	72.64	16.12
435	8.70	0.66	16.40	260.32	69.33	16.07
436	8.72	0.68	15.47	262.37	67.11	16.05
437	8.74	0.70	15.99	263.24	66.37	16.08
438	8.76	0.70	17.20	262.00	66.63	16.16
439	8.78	0.71	18.54	265.96	66.23	16.21
440	8.80	0.75	18.19	271.61	64.78	16.27
441	8.82	0.79	18.98	275.45	62.79	16.31
442	8.84	0.83	19.95	274.21	62.08	16.44
443	8.86	0.87	23.82	283.76	60.56	16.57
444	8.88	0.96	24.97	256.73	59.75	16.71
445	8.90	0.98	27.46	246.06	59.96	16.81
446	8.92	0.96	30.63	223.62	62.39	16.93
447	8.94	0.94	34.02	213.64	65.36	17.02
448	8.96	0.92	35.78	204.03	69.09	17.11
449	8.98	0.86	40.50	197.40	72.07	17.17
450	9.00	0.86	40.94	189.83	74.75	17.23
451	9.02	0.85	42.61	187.97	75.74	17.25
452	9.04	0.84	43.37	190.14	76.87	17.26
453	9.06	0.82	42.87	183.94	77.99	17.25
454	9.08	0.80	42.34	188.78	79.02	17.20
455	9.10	0.77	38.89	180.47	80.28	17.13
456	9.12	0.73	36.54	174.15	82.78	17.04
457	9.14	0.67	36.07	163.92	86.63	16.97
458	9.16	0.62	34.81	160.63	91.20	16.91
459	9.18	0.59	33.70	160.07	94.47	16.84
460	9.20	0.56	31.32	158.77	96.60	16.77
461	9.22	0.55	30.33	169.87	94.43	16.71
462	9.24	0.60	28.33	186.36	90.06	16.65
463	9.26	0.63	25.78	194.61	84.67	16.57
464	9.28	0.64	23.47	193.55	83.12	16.45
465	9.30	0.59	20.71	186.11	83.33	16.28
466	9.32	0.55	16.99	189.21	82.71	16.09
467	9.34	0.57	14.83	198.57	79.40	15.93
468	9.36	0.60	13.80	204.34	75.49	15.89
469	9.38	0.63	14.65	208.18	72.46	15.94
470	9.40	0.69	16.11	216.24	67.54	16.08
471	9.42	0.83	17.61	228.39	64.02	16.22
472	9.44	0.85	19.19	203.60	64.10	16.31
473	9.46	0.75	20.04	157.10	69.17	16.33
474	9.48	0.65	20.07	147.43	76.54	16.29
475	9.50	0.59	19.48	166.46	79.93	16.23
476	9.52	0.62	18.08	194.61	79.49	16.20
477	9.54	0.65	18.87	194.67	76.59	16.25
478	9.56	0.69	20.77	204.40	69.68	16.33
479	9.58	0.89	19.63	227.34	60.12	16.41
480	9.60	1.13	19.28	158.65	51.52	16.51

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	1.32	22.12	88.03	45.94	16.66
482	9.64	1.53	24.61	62.37	42.41	16.88
483	9.66	1.78	29.42	43.27	40.23	17.10
484	9.68	1.91	34.99	21.88	40.44	17.23
485	9.70	1.71	34.05	10.60	44.48	17.21
486	9.72	1.25	31.35	0.99	52.12	17.03
487	9.74	0.95	26.49	18.10	64.23	16.79
488	9.76	0.67	24.85	262.31	70.59	16.57
489	9.78	0.74	20.72	371.85	72.42	16.47
490	9.80	0.77	21.39	253.25	70.44	16.43
491	9.82	0.72	21.92	263.11	71.55	16.44
492	9.84	0.73	21.60	296.34	70.74	16.58
493	9.86	0.92	28.58	76.38	72.64	16.74
494	9.88	0.80	32.86	70.92	77.16	16.89
495	9.90	0.69	33.68	100.12	85.31	16.89
496	9.92	0.65	32.62	135.83	88.44	16.83
497	9.94	0.66	29.46	155.24	87.73	16.75
498	9.96	0.66	27.26	167.45	86.12	16.64
499	9.98	0.63	24.65	171.61	85.93	16.50
500	10.00	0.60	20.87	175.64	85.04	16.33
501	10.02	0.60	17.80	185.00	83.56	16.15
502	10.04	0.59	16.10	194.48	81.25	16.03
503	10.06	0.60	15.39	205.27	79.75	16.00
504	10.08	0.62	16.36	214.63	78.03	16.04
505	10.10	0.65	16.86	221.14	76.61	16.08
506	10.12	0.66	16.74	224.49	75.42	16.10
507	10.14	0.67	16.86	225.60	75.15	16.11
508	10.16	0.66	17.30	225.05	76.21	16.15
509	10.18	0.65	18.70	219.90	77.49	16.20
510	10.20	0.65	19.35	225.29	78.48	16.24
511	10.22	0.65	19.26	228.95	78.67	16.25
512	10.24	0.65	19.23	227.77	78.18	16.24
513	10.26	0.66	18.41	229.63	77.71	16.22
514	10.28	0.66	18.18	231.99	77.70	16.21
515	10.30	0.65	18.91	233.35	78.22	16.20
516	10.32	0.64	18.24	235.77	78.51	16.19
517	10.34	0.65	17.83	233.23	78.36	16.18
518	10.36	0.65	18.27	230.50	78.63	16.19
519	10.38	0.64	18.82	236.33	79.71	16.23
520	10.40	0.64	20.02	238.19	80.77	16.26
521	10.42	0.63	19.88	240.36	79.88	16.28
522	10.44	0.68	19.17	243.65	78.86	16.28
523	10.46	0.67	20.02	242.84	77.73	16.31
524	10.48	0.68	20.64	239.99	79.45	16.37
525	10.50	0.66	22.93	233.73	80.95	16.41
526	10.52	0.65	22.46	233.60	82.80	16.43
527	10.54	0.64	21.84	232.73	84.67	16.42
528	10.56	0.61	23.25	229.76	85.68	16.43

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	0.63	23.19	232.11	83.55	16.43
530	10.60	0.69	21.17	242.10	72.78	16.44
531	10.62	0.96	20.61	246.37	65.53	16.45
532	10.64	0.94	21.14	196.65	62.96	16.52
533	10.66	0.88	23.42	157.66	67.24	16.59
534	10.68	0.84	26.15	110.54	73.58	16.67
535	10.70	0.75	28.35	143.96	79.08	16.69
536	10.72	0.71	26.74	125.91	86.44	16.66
537	10.74	0.60	26.74	131.80	90.80	16.58
538	10.76	0.60	25.04	167.20	93.11	16.51
539	10.78	0.61	23.07	178.80	89.91	16.42
540	10.80	0.62	20.73	185.99	87.08	16.33
541	10.82	0.62	19.47	187.91	85.48	16.24
542	10.84	0.61	18.24	193.55	81.99	16.37
543	10.86	0.80	26.01	80.97	83.18	16.52
544	10.88	0.69	28.15	83.14	86.21	16.67
545	10.90	0.62	27.88	100.93	94.05	16.64
546	10.92	0.58	26.77	141.72	97.62	16.58
547	10.94	0.57	25.42	162.18	97.30	16.52
548	10.96	0.58	23.81	178.05	95.46	16.42
549	10.98	0.57	20.91	183.45	92.71	16.33
550	11.00	0.58	19.48	190.76	89.24	16.21
551	11.02	0.61	17.54	203.41	86.11	16.13
552	11.04	0.60	16.34	204.65	84.56	16.08
553	11.06	0.60	17.07	204.59	84.75	16.06
554	11.08	0.60	16.72	211.28	84.74	16.05
555	11.10	0.60	16.11	215.62	82.67	16.05
556	11.12	0.65	16.60	223.19	78.07	16.08
557	11.14	0.73	16.84	238.50	72.57	16.16
558	11.16	0.81	17.89	250.71	68.52	16.24
559	11.18	0.84	18.86	246.75	67.55	16.33
560	11.20	0.84	20.30	193.12	68.42	16.41
561	11.22	0.84	22.29	201.30	65.96	16.54
562	11.24	1.04	24.25	231.12	59.15	16.70
563	11.26	1.33	26.21	172.10	53.31	16.89
564	11.28	1.46	30.93	57.47	50.53	17.13
565	11.30	1.59	39.05	31.62	50.33	17.37
566	11.32	1.71	46.40	-4.59	50.94	17.55
567	11.34	1.66	48.07	-5.46	52.44	17.63
568	11.36	1.57	49.04	-6.45	55.46	17.66
569	11.38	1.46	52.70	-7.87	58.38	17.61
570	11.40	1.35	45.81	-7.69	60.95	17.55
571	11.42	1.29	44.20	-0.74	62.57	17.48
572	11.44	1.27	46.34	8.06	63.58	17.49
573	11.46	1.29	47.22	2.85	63.71	17.52
574	11.48	1.33	48.27	-6.14	62.83	17.58
575	11.50	1.40	52.46	-7.38	60.64	17.67
576	11.52	1.56	55.07	-6.39	57.49	17.77

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	1.72	57.27	-6.63	54.13	17.87
578	11.56	1.88	61.60	-7.07	51.93	17.93
579	11.58	1.91	61.31	-8.00	50.78	17.94
580	11.60	1.88	57.00	-9.18	48.58	17.87
581	11.62	2.02	49.15	-7.87	44.64	17.78
582	11.64	2.28	45.39	-7.44	41.12	17.76
583	11.66	2.40	51.46	-8.68	38.93	17.84
584	11.68	2.57	54.86	-10.91	38.38	17.93
585	11.70	2.58	55.21	-12.52	38.18	17.95
586	11.72	2.51	54.68	-13.83	38.60	17.90
587	11.74	2.37	48.82	-15.19	39.57	17.80
588	11.76	2.18	44.10	-16.99	41.63	17.71
589	11.78	1.99	47.12	-18.60	45.89	17.69
590	11.80	1.72	51.07	-20.71	52.87	17.67
591	11.82	1.35	49.81	-23.06	60.51	17.61
592	11.84	1.21	46.73	3.35	68.65	17.45
593	11.86	1.00	40.93	-1.92	76.64	17.33
594	11.88	0.83	42.87	37.01	85.15	17.23
595	11.90	0.79	41.64	55.80	92.35	17.18
596	11.93	0.73	39.88	68.51	95.53	17.10
597	11.94	0.68	36.01	93.43	94.66	16.98
598	11.96	0.73	30.91	139.99	86.41	16.85
599	11.98	0.87	26.08	155.42	76.83	16.75
600	12.00	0.94	25.49	164.04	70.12	16.68
601	12.02	0.96	23.76	158.59	70.18	16.69
602	12.04	0.88	27.07	147.74	72.78	16.70
603	12.06	0.84	27.13	148.42	76.12	16.71
604	12.08	0.83	25.29	151.83	78.79	16.68
605	12.10	0.77	26.11	147.92	81.43	16.69
606	12.12	0.75	28.86	155.05	84.79	16.74
607	12.14	0.76	29.89	162.37	86.07	16.79
608	12.16	0.75	29.62	169.31	85.72	16.78
609	12.18	0.76	27.95	175.82	83.74	16.72
610	12.20	0.78	25.37	184.25	81.17	16.65
611	12.22	0.79	24.26	188.59	78.60	16.58
612	12.24	0.80	22.77	192.75	77.39	16.54
613	12.26	0.80	22.71	197.21	76.64	16.53
614	12.28	0.81	23.44	198.88	76.85	16.55
615	12.30	0.81	24.11	200.19	77.24	16.56
616	12.32	0.79	23.18	201.30	78.03	16.55
617	12.34	0.78	23.00	202.60	77.02	16.51
618	12.36	0.82	21.57	210.60	75.62	16.48
619	12.38	0.83	21.27	212.28	74.76	16.47
620	12.40	0.81	22.50	210.85	75.81	16.51
621	12.42	0.80	23.53	208.99	77.69	16.54
622	12.44	0.78	23.71	209.18	78.59	16.58
623	12.46	0.80	25.03	214.76	78.21	16.62
624	12.48	0.84	25.64	219.22	76.78	16.67

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	0.87	26.29	222.19	75.68	16.73
626	12.52	0.88	28.02	220.40	75.52	16.80
627	12.54	0.89	30.01	220.58	76.01	16.87
628	12.56	0.90	31.83	220.77	76.62	16.95
629	12.58	0.91	33.61	218.16	77.52	17.02
630	12.60	0.91	35.78	215.87	79.31	17.08
631	12.62	0.88	38.16	213.14	80.96	17.14
632	12.64	0.89	39.15	214.32	81.74	17.17
633	12.66	0.90	38.65	219.34	80.88	17.18
634	12.68	0.93	38.80	222.50	79.02	17.18
635	12.70	0.96	38.04	225.36	77.14	17.17
636	12.72	0.98	37.16	226.84	75.78	17.18
637	12.74	0.99	38.36	224.61	76.00	17.19
638	12.76	0.97	39.59	221.76	77.32	17.23
639	12.78	0.95	41.55	218.16	79.36	17.27
640	12.80	0.94	42.93	220.21	80.32	17.29
641	12.82	0.95	41.88	226.66	79.61	17.31
642	12.84	0.98	43.73	340.67	78.62	17.35
643	12.86	0.99	46.46	335.28	77.65	17.41
644	12.89	1.02	46.72	328.33	77.18	17.44
645	12.90	1.04	46.87	328.33	76.12	17.46
646	12.92	1.06	47.57	322.13	75.50	17.49
647	12.95	1.08	49.91	318.35	75.61	17.54
648	12.96	1.08	52.26	312.96	76.49	17.58
649	12.98	1.06	53.90	305.33	78.01	17.62
650	13.00	1.04	55.33	298.02	79.40	17.64
651	13.02	1.05	56.65	293.55	80.25	17.66
652	13.04	1.05	57.12	288.28	81.31	17.68
653	13.06	1.02	58.47	283.38	81.96	17.69
654	13.08	1.03	57.59	278.92	83.05	17.69
655	13.10	1.01	58.08	269.56	83.89	17.68
656	13.12	0.98	58.03	264.04	85.65	17.67
657	13.14	0.95	57.64	257.59	88.13	17.65
658	13.16	0.90	57.41	246.06	91.05	17.63
659	13.18	0.86	56.76	240.05	93.99	17.58
660	13.20	0.82	53.72	236.39	95.53	17.53
661	13.22	0.82	51.16	239.24	95.84	17.45
662	13.24	0.80	47.56	239.24	95.00	17.36
663	13.26	0.79	42.87	236.45	94.59	17.25
664	13.28	0.77	39.65	233.91	94.55	17.14
665	13.30	0.74	36.72	232.11	94.93	17.04
666	13.32	0.72	33.49	233.35	94.12	16.93
667	13.34	0.73	30.21	236.27	92.21	16.83
668	13.36	0.74	28.57	240.67	91.19	16.77
669	13.38	0.72	28.45	234.10	92.22	16.74
670	13.40	0.69	28.83	234.41	94.60	16.71
671	13.42	0.66	26.99	239.18	96.50	16.65
672	13.44	0.64	24.91	246.62	97.08	16.55

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	0.63	22.94	245.94	96.95	16.48
674	13.48	0.63	22.88	254.25	96.03	16.41
675	13.50	0.63	20.83	262.12	94.43	16.35
676	13.52	0.64	19.37	267.20	92.56	16.26
677	13.54	0.64	18.08	270.74	91.11	16.19
678	13.56	0.64	17.58	278.55	89.20	16.15
679	13.58	0.66	17.11	287.17	87.01	16.14
680	13.60	0.69	17.41	292.75	84.13	16.15
681	13.62	0.71	17.35	297.21	82.83	16.19
682	13.64	0.72	18.40	298.33	83.17	16.24
683	13.66	0.70	19.43	292.19	85.60	16.30
684	13.68	0.68	20.93	287.91	88.75	16.36
685	13.70	0.66	21.72	287.48	90.98	16.40
686	13.72	0.66	21.89	291.32	91.83	16.41
687	13.74	0.67	21.72	293.61	91.23	16.40
688	13.76	0.67	20.99	295.97	90.34	16.37
689	13.78	0.67	20.49	299.57	88.78	16.34
690	13.80	0.69	19.58	304.34	85.84	16.24
691	13.82	0.71	15.73	296.78	82.82	16.21
692	13.84	0.75	18.43	301.80	81.86	16.23
693	13.86	0.73	20.04	305.52	84.74	16.35
694	13.88	0.68	22.09	304.53	88.79	16.40
695	13.90	0.66	21.97	310.35	90.62	16.43
696	13.92	0.69	21.89	330.44	87.48	16.43
697	13.94	0.76	21.42	345.88	82.90	16.42
698	13.96	0.79	20.42	335.90	80.98	16.41
699	13.98	0.75	20.51	319.78	84.84	16.36
700	14.00	0.63	20.22	304.90	90.23	16.29
701	14.02	0.62	18.43	306.39	94.51	16.21
702	14.04	0.61	17.34	319.71	94.78	16.15
703	14.06	0.60	17.61	318.60	96.24	16.14
704	14.08	0.58	18.28	320.52	97.82	16.15
705	14.10	0.58	18.16	325.67	96.85	16.14
706	14.12	0.61	17.14	334.78	93.80	16.11
707	14.14	0.63	16.23	336.70	90.58	16.06
708	14.16	0.64	15.76	338.07	89.41	16.03
709	14.18	0.63	15.67	336.95	89.27	16.02
710	14.20	0.63	15.70	334.47	87.45	15.99
711	14.22	0.67	14.36	339.12	82.28	15.95
712	14.24	0.74	13.33	370.12	78.81	15.94
713	14.26	0.75	14.74	236.33	79.78	16.01
714	14.28	0.70	16.96	218.23	85.37	16.11
715	14.30	0.65	18.20	266.96	90.05	16.18
716	14.32	0.65	18.49	297.89	88.50	16.20
717	14.34	0.73	17.73	319.40	80.29	16.25
718	14.36	0.90	18.46	341.17	70.79	16.33
719	14.38	1.03	19.25	366.09	65.00	16.42
720	14.40	1.09	20.28	268.75	66.08	16.41

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	0.84	18.40	333.48	71.14	16.36
722	14.44	0.75	18.14	407.01	76.68	16.28
723	14.46	0.79	18.17	410.42	77.04	16.27
724	14.48	0.80	18.14	447.99	73.62	16.28
725	14.50	0.88	17.85	463.73	67.90	16.37
726	14.52	1.08	20.42	497.64	60.93	16.51
727	14.54	1.30	22.42	385.18	55.03	16.63
728	14.56	1.46	21.30	159.45	53.28	16.73
729	14.58	1.41	24.85	87.66	54.43	16.79
730	14.60	1.33	26.34	91.20	59.53	16.87
731	14.62	1.17	28.83	87.35	67.09	16.94
732	14.64	0.99	32.58	72.10	77.08	17.02
733	14.66	0.90	37.10	85.74	85.71	17.09
734	14.68	0.87	38.97	141.35	86.28	17.14
735	14.70	0.98	37.07	191.69	78.81	17.17
736	14.72	1.19	35.46	218.04	68.70	17.18
737	14.74	1.40	34.81	156.42	62.72	17.20
738	14.76	1.39	34.72	151.70	59.35	17.16
739	14.78	1.43	30.33	122.50	61.07	17.13
740	14.80	1.26	33.64	70.12	63.02	17.27
741	14.82	1.41	47.17	107.19	67.86	17.45
742	14.84	1.29	50.87	127.09	68.68	17.60
743	14.87	1.36	50.60	113.39	71.39	17.62
744	14.88	1.27	52.16	89.52	72.78	17.58
745	14.91	1.17	46.38	65.84	76.94	17.49
746	14.92	1.06	43.42	79.79	78.17	17.34
747	14.94	1.08	37.36	107.07	80.75	17.21
748	14.96	0.95	35.66	90.58	86.65	17.04
749	14.98	0.70	31.06	86.24	97.03	16.87
750	15.00	0.66	28.39	139.62	100.00	16.68
751	15.02	0.74	23.11	209.98	88.84	16.56
752	15.04	0.92	20.10	253.38	71.45	16.52
753	15.06	1.24	21.06	295.97	58.46	16.63
754	15.08	1.54	23.90	298.82	50.19	16.82
755	15.10	1.84	26.89	170.30	45.76	17.06
756	15.12	2.09	33.22	41.54	44.77	17.30
757	15.14	2.10	40.75	14.26	47.81	17.46
758	15.16	1.73	42.42	2.05	54.18	17.49
759	15.18	1.41	41.10	-3.66	64.50	17.44
760	15.20	1.16	44.47	-3.60	76.62	17.36
761	15.22	0.92	42.51	20.64	88.20	17.30
762	15.24	0.85	40.98	49.41	96.35	17.25
763	15.26	0.84	43.89	70.12	97.35	17.26
764	15.28	0.88	43.80	90.33	88.26	17.31
765	15.30	1.17	41.51	114.14	73.02	17.35
766	15.32	1.55	38.87	141.17	58.23	17.33
767	15.34	1.89	32.54	109.42	49.81	17.34
768	15.36	2.04	35.77	91.69	45.50	17.37

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	2.16	38.70	85.55	45.92	17.49
770	15.40	2.04	43.12	68.88	49.76	17.55
771	15.42	1.65	44.85	53.44	57.57	17.56
772	15.44	1.33	45.73	43.21	67.29	17.44
773	15.46	1.14	39.04	46.87	71.36	17.30
774	15.48	1.26	33.89	60.01	66.04	17.22
775	15.50	1.57	35.35	81.90	57.26	17.27
776	15.52	1.85	37.14	89.40	53.28	17.47
777	15.54	1.92	49.09	77.50	53.24	17.63
778	15.56	1.82	51.26	73.22	55.68	17.74
779	15.58	1.76	52.17	75.26	57.14	17.76
780	15.60	1.79	52.46	72.97	57.51	17.77
781	15.62	1.65	51.70	67.70	59.71	17.74

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.28	0.00	0.28	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
2	0.04	0.59	0.00	0.59	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
3	0.06	0.91	0.00	0.91	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
4	0.08	1.23	0.00	1.23	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
5	0.10	1.56	0.00	1.56	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
6	0.12	1.89	0.00	1.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
7	0.14	2.24	0.00	2.24	1.00	0.143	1.43	0.100	1.10	1.00	2.000	Yes
8	0.16	2.59	0.00	2.59	1.00	0.143	1.43	0.100	1.10	1.00	2.000	Yes
9	0.18	2.95	0.00	2.95	1.00	0.143	1.43	0.100	1.10	1.00	2.000	Yes
10	0.20	3.30	0.00	3.30	1.00	0.143	1.43	0.100	1.10	1.00	2.000	Yes
11	0.22	3.65	0.00	3.65	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
12	0.24	3.99	0.00	3.99	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
13	0.26	4.32	0.00	4.32	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
14	0.28	4.66	0.00	4.66	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
15	0.30	4.99	0.00	4.99	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
16	0.32	5.33	0.00	5.33	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
17	0.34	5.67	0.00	5.67	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
18	0.36	6.02	0.00	6.02	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
19	0.38	6.37	0.00	6.37	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
20	0.40	6.72	0.00	6.72	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
21	0.42	7.08	0.00	7.08	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
22	0.44	7.44	0.00	7.44	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
23	0.46	7.81	0.00	7.81	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
24	0.48	8.17	0.00	8.17	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
25	0.50	8.54	0.00	8.54	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
26	0.52	8.91	0.00	8.91	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
27	0.54	9.27	0.00	9.27	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
28	0.56	9.64	0.00	9.64	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
29	0.58	10.00	0.00	10.00	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
30	0.60	10.37	0.00	10.37	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
31	0.62	10.73	0.00	10.73	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
32	0.64	11.10	0.00	11.10	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
33	0.66	11.46	0.00	11.46	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
34	0.68	11.82	0.00	11.82	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
35	0.70	12.18	0.00	12.18	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
36	0.72	12.54	0.00	12.54	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
37	0.74	12.90	0.00	12.90	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
38	0.76	13.27	0.00	13.27	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
39	0.78	13.63	0.00	13.63	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
40	0.80	13.99	0.00	13.99	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
41	0.82	14.35	0.00	14.35	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
42	0.84	14.71	0.00	14.71	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
43	0.86	15.07	0.00	15.07	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
44	0.88	15.44	0.00	15.44	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
45	0.90	15.80	0.00	15.80	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
46	0.92	16.16	0.00	16.16	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
47	0.94	16.53	0.00	16.53	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
48	0.96	16.89	0.00	16.89	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	17.25	0.00	17.25	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
50	1.00	17.61	0.00	17.61	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
51	1.02	17.98	0.00	17.98	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
52	1.04	18.34	0.00	18.34	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
53	1.06	18.70	0.00	18.70	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
54	1.09	19.24	0.00	19.24	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
55	1.10	19.43	0.00	19.43	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
56	1.12	19.79	0.00	19.79	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
57	1.14	20.16	0.00	20.16	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
58	1.16	20.52	0.00	20.52	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
59	1.18	20.89	0.00	20.89	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
60	1.20	21.26	0.00	21.26	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
61	1.23	21.81	0.00	21.81	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
62	1.24	22.00	0.00	22.00	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
63	1.26	22.37	0.00	22.37	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
64	1.28	22.74	0.00	22.74	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
65	1.30	23.11	0.00	23.11	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
66	1.32	23.48	0.00	23.48	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
67	1.34	23.85	0.00	23.85	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
68	1.36	24.22	0.00	24.22	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
69	1.38	24.59	0.00	24.59	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
70	1.40	24.97	0.00	24.97	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
71	1.42	25.34	0.00	25.34	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
72	1.44	25.71	0.00	25.71	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
73	1.46	26.09	0.00	26.09	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
74	1.48	26.46	0.00	26.46	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
75	1.50	26.84	0.00	26.84	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
76	1.52	27.22	0.00	27.22	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
77	1.54	27.59	0.00	27.59	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
78	1.56	27.97	0.00	27.97	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
79	1.59	28.53	0.00	28.53	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
80	1.60	28.72	0.00	28.72	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
81	1.62	29.09	0.00	29.09	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
82	1.64	29.47	0.00	29.47	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
83	1.66	29.84	0.00	29.84	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
84	1.68	30.21	0.00	30.21	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
85	1.70	30.58	0.00	30.58	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
86	1.72	30.96	0.00	30.96	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
87	1.74	31.33	0.00	31.33	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
88	1.76	31.70	0.00	31.70	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
89	1.78	32.06	0.00	32.06	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
90	1.80	32.43	0.00	32.43	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
91	1.82	32.80	0.00	32.80	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
92	1.84	33.17	0.00	33.17	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
93	1.86	33.53	0.00	33.53	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
94	1.88	33.90	0.00	33.90	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
95	1.90	34.26	0.00	34.26	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
96	1.92	34.63	0.00	34.63	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	34.99	0.00	34.99	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
98	1.96	35.36	0.00	35.36	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
99	1.99	35.90	0.00	35.90	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
100	2.00	36.08	0.00	36.08	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
101	2.02	36.44	0.20	36.24	0.98	0.141	1.43	0.098	1.08	1.00	0.121	No
102	2.04	36.79	0.39	36.40	0.98	0.141	1.43	0.099	1.08	1.00	0.122	No
103	2.06	37.14	0.59	36.56	0.98	0.142	1.43	0.099	1.08	1.00	0.123	No
104	2.08	37.49	0.78	36.71	0.98	0.143	1.43	0.100	1.08	1.00	0.123	No
105	2.10	37.83	0.98	36.85	0.98	0.143	1.43	0.100	1.08	1.00	0.124	No
106	2.12	38.17	1.18	37.00	0.98	0.144	1.43	0.101	1.08	1.00	0.125	No
107	2.14	38.51	1.37	37.13	0.98	0.145	1.43	0.101	1.08	1.00	0.125	No
108	2.16	38.83	1.57	37.26	0.98	0.145	1.43	0.102	1.08	1.00	0.125	No
109	2.18	39.16	1.77	37.39	0.98	0.146	1.43	0.102	1.08	1.00	0.126	No
110	2.20	39.48	1.96	37.51	0.98	0.147	1.43	0.103	1.08	1.00	0.126	No
111	2.22	39.80	2.16	37.64	0.98	0.147	1.43	0.103	1.08	1.00	0.127	No
112	2.24	40.12	2.35	37.76	0.97	0.148	1.43	0.104	1.08	1.00	0.127	No
113	2.26	40.44	2.55	37.89	0.97	0.149	1.43	0.104	1.08	1.00	0.127	No
114	2.28	40.77	2.75	38.02	0.97	0.149	1.43	0.105	1.08	1.00	0.127	No
115	2.30	41.10	2.94	38.16	0.97	0.150	1.43	0.105	1.08	1.00	0.128	No
116	2.32	41.44	3.14	38.30	0.97	0.151	1.43	0.105	1.08	1.00	0.128	No
117	2.34	41.78	3.34	38.44	0.97	0.151	1.43	0.106	1.08	1.00	0.129	No
118	2.36	42.12	3.53	38.59	0.97	0.152	1.43	0.106	1.08	1.00	0.129	No
119	2.38	42.47	3.73	38.74	0.97	0.152	1.43	0.107	1.08	1.00	0.130	No
120	2.40	42.81	3.92	38.89	0.97	0.153	1.43	0.107	1.08	1.00	0.131	No
121	2.42	43.16	4.12	39.04	0.97	0.154	1.43	0.108	1.08	1.00	0.131	No
122	2.44	43.51	4.32	39.20	0.97	0.154	1.43	0.108	1.08	1.00	0.132	No
123	2.46	43.86	4.51	39.35	0.97	0.155	1.43	0.108	1.08	1.00	0.133	No
124	2.48	44.22	4.71	39.51	0.97	0.155	1.43	0.109	1.08	1.00	0.134	No
125	2.50	44.57	4.91	39.66	0.97	0.156	1.43	0.109	1.08	1.00	0.134	No
126	2.52	44.92	5.10	39.82	0.97	0.156	1.43	0.110	1.08	1.00	0.135	No
127	2.54	45.28	5.30	39.98	0.97	0.157	1.43	0.110	1.08	1.00	0.136	No
128	2.56	45.63	5.49	40.13	0.97	0.158	1.43	0.110	1.08	1.00	0.136	No
129	2.58	45.97	5.69	40.28	0.97	0.158	1.43	0.111	1.07	1.00	0.137	No
130	2.60	46.32	5.89	40.43	0.97	0.159	1.43	0.111	1.07	1.00	0.138	No
131	2.62	46.66	6.08	40.58	0.97	0.159	1.43	0.111	1.07	1.00	0.138	No
132	2.64	47.00	6.28	40.72	0.97	0.160	1.43	0.112	1.07	1.00	0.139	No
133	2.66	47.34	6.47	40.86	0.97	0.160	1.43	0.112	1.07	1.00	0.139	No
134	2.68	47.67	6.67	41.00	0.97	0.161	1.43	0.113	1.07	1.00	0.140	No
135	2.70	48.00	6.87	41.13	0.97	0.161	1.43	0.113	1.07	1.00	0.140	No
136	2.72	48.33	7.06	41.27	0.97	0.162	1.43	0.113	1.07	1.00	0.141	No
137	2.74	48.66	7.26	41.40	0.97	0.162	1.43	0.114	1.07	1.00	0.141	No
138	2.76	48.98	7.46	41.53	0.97	0.163	1.43	0.114	1.07	1.00	0.142	No
139	2.78	49.31	7.65	41.65	0.97	0.163	1.43	0.114	1.07	1.00	0.142	No
140	2.80	49.62	7.85	41.78	0.97	0.164	1.43	0.115	1.07	1.00	0.143	No
141	2.82	49.94	8.04	41.90	0.96	0.164	1.43	0.115	1.07	1.00	0.143	No
142	2.84	50.26	8.24	42.02	0.96	0.165	1.43	0.115	1.07	1.00	0.144	No
143	2.86	50.58	8.44	42.14	0.96	0.165	1.43	0.116	1.07	1.00	0.144	No
144	2.88	50.89	8.63	42.26	0.96	0.166	1.43	0.116	1.07	1.00	0.144	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	51.21	8.83	42.38	0.96	0.166	1.43	0.117	1.07	1.00	0.145	No
146	2.92	51.53	9.03	42.51	0.96	0.167	1.43	0.117	1.07	1.00	0.145	No
147	2.94	51.86	9.22	42.64	0.96	0.167	1.43	0.117	1.07	1.00	0.145	No
148	2.96	52.18	9.42	42.76	0.96	0.168	1.43	0.118	1.07	1.00	0.145	No
149	2.98	52.51	9.61	42.90	0.96	0.168	1.43	0.118	1.07	1.00	0.146	No
150	3.00	52.84	9.81	43.03	0.96	0.169	1.43	0.118	1.07	1.00	0.146	No
151	3.02	53.17	10.01	43.16	0.96	0.169	1.43	0.119	1.07	1.00	0.147	No
152	3.04	53.50	10.20	43.30	0.96	0.170	1.43	0.119	1.07	1.00	0.147	No
153	3.06	53.83	10.40	43.43	0.96	0.170	1.43	0.119	1.07	1.00	0.147	No
154	3.08	54.16	10.59	43.56	0.96	0.171	1.43	0.119	1.07	1.00	0.148	No
155	3.10	54.49	10.79	43.70	0.96	0.171	1.43	0.120	1.07	1.00	0.148	No
156	3.12	54.82	10.99	43.83	0.96	0.172	1.43	0.120	1.07	1.00	0.149	No
157	3.14	55.15	11.18	43.96	0.96	0.172	1.43	0.120	1.07	1.00	0.149	No
158	3.16	55.47	11.38	44.10	0.96	0.172	1.43	0.121	1.07	1.00	0.150	No
159	3.18	55.80	11.58	44.23	0.96	0.173	1.43	0.121	1.07	1.00	0.150	No
160	3.20	56.13	11.77	44.36	0.96	0.173	1.43	0.121	1.07	1.00	0.151	No
161	3.22	56.46	11.97	44.49	0.96	0.174	1.43	0.122	1.07	1.00	0.151	No
162	3.24	56.79	12.16	44.63	0.96	0.174	1.43	0.122	1.07	1.00	0.151	No
163	3.26	57.12	12.36	44.76	0.96	0.175	1.43	0.122	1.07	1.00	0.152	No
164	3.28	57.45	12.56	44.89	0.96	0.175	1.43	0.123	1.07	1.00	0.152	No
165	3.30	57.78	12.75	45.02	0.96	0.175	1.43	0.123	1.07	1.00	0.152	No
166	3.32	58.11	12.95	45.16	0.96	0.176	1.43	0.123	1.07	1.00	0.153	No
167	3.34	58.44	13.15	45.29	0.96	0.176	1.43	0.123	1.07	1.00	0.153	No
168	3.36	58.77	13.34	45.42	0.95	0.177	1.43	0.124	1.07	1.00	0.154	No
169	3.38	59.09	13.54	45.56	0.95	0.177	1.43	0.124	1.07	1.00	0.154	No
170	3.40	59.42	13.73	45.69	0.95	0.177	1.43	0.124	1.07	1.00	0.154	No
171	3.42	59.75	13.93	45.82	0.95	0.178	1.43	0.124	1.07	1.00	0.154	No
172	3.44	60.08	14.13	45.96	0.95	0.178	1.43	0.125	1.07	1.00	0.154	No
173	3.46	60.42	14.32	46.09	0.95	0.179	1.43	0.125	1.07	1.00	0.154	No
174	3.48	60.75	14.52	46.23	0.95	0.179	1.43	0.125	1.07	1.00	0.155	No
175	3.50	61.08	14.72	46.37	0.95	0.179	1.43	0.126	1.07	1.00	0.156	No
176	3.52	61.42	14.91	46.51	0.95	0.180	1.43	0.126	1.07	1.00	0.156	No
177	3.54	61.75	15.11	46.65	0.95	0.180	1.43	0.126	1.07	1.00	0.156	No
178	3.56	62.09	15.30	46.79	0.95	0.180	1.43	0.126	1.07	1.00	0.156	No
179	3.58	62.43	15.50	46.93	0.95	0.181	1.43	0.127	1.07	1.00	0.157	No
180	3.60	62.77	15.70	47.07	0.95	0.181	1.43	0.127	1.07	1.00	0.157	No
181	3.62	63.11	15.89	47.22	0.95	0.182	1.43	0.127	1.06	1.00	2.000	Yes
182	3.64	63.45	16.09	47.36	0.95	0.182	1.43	0.127	1.06	1.00	2.000	Yes
183	3.66	63.79	16.28	47.50	0.95	0.182	1.43	0.128	1.07	1.00	2.000	Yes
184	3.68	64.13	16.48	47.65	0.95	0.183	1.43	0.128	1.07	1.00	2.000	Yes
185	3.70	64.48	16.68	47.80	0.95	0.183	1.43	0.128	1.07	1.00	2.000	Yes
186	3.72	64.83	16.87	47.96	0.95	0.183	1.43	0.128	1.07	1.00	2.000	Yes
187	3.74	65.18	17.07	48.11	0.95	0.184	1.43	0.129	1.07	1.00	2.000	Yes
188	3.76	65.53	17.27	48.27	0.95	0.184	1.43	0.129	1.07	1.00	2.000	Yes
189	3.78	65.89	17.46	48.42	0.95	0.184	1.43	0.129	1.07	1.00	2.000	Yes
190	3.80	66.24	17.66	48.58	0.95	0.185	1.43	0.129	1.07	1.00	2.000	Yes
191	3.82	66.59	17.85	48.74	0.95	0.185	1.43	0.129	1.07	1.00	2.000	Yes
192	3.84	66.94	18.05	48.89	0.95	0.185	1.43	0.130	1.08	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	67.30	18.25	49.05	0.95	0.185	1.43	0.130	1.07	1.00	2.000	Yes
194	3.88	67.64	18.44	49.20	0.94	0.186	1.43	0.130	1.07	1.00	2.000	Yes
195	3.90	67.99	18.64	49.35	0.94	0.186	1.43	0.130	1.07	1.00	2.000	Yes
196	3.92	68.34	18.84	49.50	0.94	0.186	1.43	0.130	1.06	1.00	2.000	Yes
197	3.94	68.69	19.03	49.66	0.94	0.187	1.43	0.131	1.06	1.00	2.000	Yes
198	3.96	69.04	19.23	49.81	0.94	0.187	1.43	0.131	1.06	1.00	0.161	No
199	3.98	69.39	19.42	49.97	0.94	0.187	1.43	0.131	1.06	1.00	0.162	No
200	4.00	69.74	19.62	50.12	0.94	0.188	1.43	0.131	1.06	1.00	0.163	No
201	4.02	70.09	19.82	50.28	0.94	0.188	1.43	0.131	1.06	1.00	0.163	No
202	4.04	70.44	20.01	50.43	0.94	0.188	1.43	0.132	1.06	1.00	0.164	No
203	4.06	70.79	20.21	50.58	0.94	0.188	1.43	0.132	1.06	1.00	0.164	No
204	4.09	71.31	20.50	50.81	0.94	0.189	1.43	0.132	1.06	1.00	0.165	No
205	4.10	71.49	20.60	50.89	0.94	0.189	1.43	0.132	1.06	1.00	0.165	No
206	4.12	71.84	20.80	51.04	0.94	0.189	1.43	0.132	1.06	1.00	0.165	No
207	4.14	72.18	20.99	51.19	0.94	0.190	1.43	0.133	1.06	1.00	0.166	No
208	4.16	72.53	21.19	51.34	0.94	0.190	1.43	0.133	1.06	1.00	0.166	No
209	4.18	72.87	21.39	51.49	0.94	0.190	1.43	0.133	1.06	1.00	0.166	No
210	4.20	73.22	21.58	51.63	0.94	0.190	1.43	0.133	1.06	1.00	0.167	No
211	4.22	73.56	21.78	51.78	0.94	0.191	1.43	0.133	1.06	1.00	0.167	No
212	4.24	73.90	21.97	51.93	0.94	0.191	1.43	0.134	1.06	1.00	0.168	No
213	4.26	74.25	22.17	52.07	0.94	0.191	1.43	0.134	1.05	1.00	0.168	No
214	4.28	74.59	22.37	52.22	0.94	0.191	1.43	0.134	1.05	1.00	0.169	No
215	4.30	74.93	22.56	52.37	0.94	0.192	1.43	0.134	1.05	1.00	0.170	No
216	4.32	75.27	22.76	52.51	0.94	0.192	1.43	0.134	1.05	1.00	0.170	No
217	4.34	75.62	22.96	52.66	0.94	0.192	1.43	0.134	1.05	1.00	0.170	No
218	4.36	75.96	23.15	52.81	0.94	0.192	1.43	0.135	1.05	1.00	0.170	No
219	4.38	76.30	23.35	52.96	0.93	0.193	1.43	0.135	1.06	1.00	0.169	No
220	4.40	76.65	23.54	53.11	0.93	0.193	1.43	0.135	1.06	1.00	0.167	No
221	4.42	77.00	23.74	53.26	0.93	0.193	1.43	0.135	1.06	1.00	0.166	No
222	4.44	77.35	23.94	53.41	0.93	0.193	1.43	0.135	1.06	1.00	0.166	No
223	4.46	77.70	24.13	53.57	0.93	0.194	1.43	0.136	1.06	1.00	0.166	No
224	4.48	78.04	24.33	53.71	0.93	0.194	1.43	0.136	1.06	1.00	0.168	No
225	4.50	78.38	24.53	53.85	0.93	0.194	1.43	0.136	1.06	1.00	0.169	No
226	4.52	78.71	24.72	53.99	0.93	0.194	1.43	0.136	1.06	1.00	0.169	No
227	4.54	79.05	24.92	54.13	0.93	0.195	1.43	0.136	1.05	1.00	0.170	No
228	4.56	79.39	25.11	54.28	0.93	0.195	1.43	0.136	1.05	1.00	0.170	No
229	4.58	79.74	25.31	54.43	0.93	0.195	1.43	0.137	1.06	1.00	0.170	No
230	4.60	80.09	25.51	54.59	0.93	0.195	1.43	0.137	1.06	1.00	0.170	No
231	4.62	80.44	25.70	54.74	0.93	0.195	1.43	0.137	1.06	1.00	0.169	No
232	4.64	80.80	25.90	54.90	0.93	0.196	1.43	0.137	1.06	1.00	0.169	No
233	4.66	81.15	26.09	55.06	0.93	0.196	1.43	0.137	1.06	1.00	0.169	No
234	4.68	81.50	26.29	55.21	0.93	0.196	1.43	0.137	1.05	1.00	0.171	No
235	4.70	81.86	26.49	55.37	0.93	0.196	1.43	0.137	1.05	1.00	0.172	No
236	4.72	82.21	26.68	55.52	0.93	0.196	1.43	0.138	1.05	1.00	0.172	No
237	4.74	82.56	26.88	55.68	0.93	0.197	1.43	0.138	1.05	1.00	0.171	No
238	4.76	82.91	27.08	55.83	0.93	0.197	1.43	0.138	1.05	1.00	0.171	No
239	4.78	83.26	27.27	55.99	0.93	0.197	1.43	0.138	1.05	1.00	0.172	No
240	4.80	83.61	27.47	56.15	0.93	0.197	1.43	0.138	1.05	1.00	0.172	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	83.97	27.66	56.30	0.93	0.197	1.43	0.138	1.05	1.00	0.172	No
242	4.84	84.32	27.86	56.46	0.93	0.198	1.43	0.138	1.05	1.00	0.173	No
243	4.86	84.67	28.06	56.61	0.93	0.198	1.43	0.138	1.05	1.00	0.173	No
244	4.88	85.02	28.25	56.77	0.92	0.198	1.43	0.139	1.05	1.00	0.174	No
245	4.90	85.37	28.45	56.92	0.92	0.198	1.43	0.139	1.05	1.00	0.174	No
246	4.92	85.72	28.65	57.07	0.92	0.198	1.43	0.139	1.05	1.00	0.175	No
247	4.94	86.06	28.84	57.22	0.92	0.199	1.43	0.139	1.05	1.00	0.176	No
248	4.96	86.41	29.04	57.37	0.92	0.199	1.43	0.139	1.05	1.00	0.176	No
249	4.98	86.75	29.23	57.52	0.92	0.199	1.43	0.139	1.05	1.00	0.177	No
250	5.00	87.09	29.43	57.66	0.92	0.199	1.43	0.139	1.05	1.00	0.177	No
251	5.02	87.43	29.63	57.80	0.92	0.199	1.43	0.140	1.05	1.00	0.177	No
252	5.04	87.77	29.82	57.95	0.92	0.200	1.43	0.140	1.05	1.00	0.177	No
253	5.06	88.12	30.02	58.10	0.92	0.200	1.43	0.140	1.05	1.00	0.176	No
254	5.08	88.46	30.21	58.25	0.92	0.200	1.43	0.140	1.05	1.00	0.176	No
255	5.10	88.81	30.41	58.40	0.92	0.200	1.43	0.140	1.05	1.00	0.176	No
256	5.12	89.15	30.61	58.55	0.92	0.200	1.43	0.140	1.05	1.00	0.176	No
257	5.14	89.49	30.80	58.69	0.92	0.200	1.43	0.140	1.05	1.00	0.177	No
258	5.16	89.83	31.00	58.84	0.92	0.201	1.43	0.140	1.04	1.00	0.178	No
259	5.18	90.17	31.20	58.98	0.92	0.201	1.43	0.141	1.04	1.00	0.179	No
260	5.20	90.51	31.39	59.11	0.92	0.201	1.43	0.141	1.04	1.00	0.180	No
261	5.22	90.84	31.59	59.25	0.92	0.201	1.43	0.141	1.04	1.00	0.180	No
262	5.24	91.17	31.78	59.38	0.92	0.201	1.43	0.141	1.04	1.00	0.180	No
263	5.26	91.50	31.98	59.52	0.92	0.202	1.43	0.141	1.04	1.00	0.180	No
264	5.28	91.83	32.18	59.65	0.92	0.202	1.43	0.141	1.04	1.00	0.181	No
265	5.30	92.15	32.37	59.78	0.92	0.202	1.43	0.141	1.04	1.00	0.181	No
266	5.32	92.48	32.57	59.91	0.92	0.202	1.43	0.141	1.04	1.00	0.181	No
267	5.34	92.80	32.77	60.04	0.92	0.202	1.43	0.142	1.04	1.00	0.181	No
268	5.36	93.13	32.96	60.17	0.91	0.202	1.43	0.142	1.04	1.00	0.181	No
269	5.38	93.46	33.16	60.30	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
270	5.40	93.79	33.35	60.43	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
271	5.42	94.12	33.55	60.57	0.91	0.203	1.43	0.142	1.04	1.00	0.182	No
272	5.44	94.44	33.75	60.70	0.91	0.203	1.43	0.142	1.04	1.00	0.182	No
273	5.46	94.78	33.94	60.83	0.91	0.203	1.43	0.142	1.04	1.00	0.182	No
274	5.48	95.11	34.14	60.97	0.91	0.203	1.43	0.142	1.04	1.00	0.182	No
275	5.50	95.44	34.34	61.11	0.91	0.204	1.43	0.143	1.04	1.00	0.182	No
276	5.52	95.77	34.53	61.24	0.91	0.204	1.43	0.143	1.04	1.00	0.183	No
277	5.54	96.10	34.73	61.37	0.91	0.204	1.43	0.143	1.04	1.00	0.183	No
278	5.56	96.43	34.92	61.51	0.91	0.204	1.43	0.143	1.04	1.00	0.183	No
279	5.59	96.92	35.22	61.70	0.91	0.204	1.43	0.143	1.04	1.00	0.183	No
280	5.60	97.08	35.32	61.77	0.91	0.204	1.43	0.143	1.04	1.00	0.184	No
281	5.62	97.41	35.51	61.90	0.91	0.205	1.43	0.143	1.04	1.00	0.184	No
282	5.64	97.74	35.71	62.03	0.91	0.205	1.43	0.143	1.04	1.00	0.183	No
283	5.66	98.06	35.90	62.16	0.91	0.205	1.43	0.143	1.04	1.00	0.183	No
284	5.68	98.39	36.10	62.29	0.91	0.205	1.43	0.144	1.04	1.00	0.183	No
285	5.70	98.72	36.30	62.42	0.91	0.205	1.43	0.144	1.04	1.00	0.184	No
286	5.72	99.05	36.49	62.56	0.91	0.205	1.43	0.144	1.04	1.00	0.184	No
287	5.74	99.38	36.69	62.69	0.91	0.205	1.43	0.144	1.04	1.00	0.184	No
288	5.76	99.71	36.89	62.83	0.91	0.206	1.43	0.144	1.04	1.00	0.185	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	100.04	37.08	62.96	0.91	0.206	1.43	0.144	1.04	1.00	0.185	No
290	5.80	100.37	37.28	63.10	0.91	0.206	1.43	0.144	1.04	1.00	0.185	No
291	5.82	100.70	37.47	63.23	0.90	0.206	1.43	0.144	1.04	1.00	0.185	No
292	5.84	101.03	37.67	63.36	0.90	0.206	1.43	0.144	1.04	1.00	0.185	No
293	5.86	101.36	37.87	63.50	0.90	0.206	1.43	0.144	1.04	1.00	0.185	No
294	5.88	101.69	38.06	63.63	0.90	0.206	1.43	0.145	1.04	1.00	0.185	No
295	5.90	102.03	38.26	63.77	0.90	0.207	1.43	0.145	1.04	1.00	0.184	No
296	5.92	102.37	38.46	63.91	0.90	0.207	1.43	0.145	1.04	1.00	0.184	No
297	5.94	102.71	38.65	64.06	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
298	5.96	103.05	38.85	64.20	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
299	5.98	103.39	39.04	64.35	0.90	0.207	1.43	0.145	1.04	1.00	0.186	No
300	6.00	103.73	39.24	64.49	0.90	0.207	1.43	0.145	1.04	1.00	0.186	No
301	6.02	104.07	39.44	64.64	0.90	0.207	1.43	0.145	1.04	1.00	0.186	No
302	6.04	104.41	39.63	64.78	0.90	0.207	1.43	0.145	1.04	1.00	0.186	No
303	6.06	104.74	39.83	64.92	0.90	0.208	1.43	0.145	1.04	1.00	0.186	No
304	6.08	105.08	40.02	65.06	0.90	0.208	1.43	0.145	1.04	1.00	0.186	No
305	6.10	105.42	40.22	65.19	0.90	0.208	1.43	0.145	1.04	1.00	0.186	No
306	6.12	105.75	40.42	65.33	0.90	0.208	1.43	0.146	1.04	1.00	0.186	No
307	6.14	106.09	40.61	65.47	0.90	0.208	1.43	0.146	1.04	1.00	0.186	No
308	6.16	106.42	40.81	65.61	0.90	0.208	1.43	0.146	1.04	1.00	0.187	No
309	6.18	106.76	41.01	65.75	0.90	0.208	1.43	0.146	1.03	1.00	0.187	No
310	6.20	107.10	41.20	65.90	0.90	0.208	1.43	0.146	1.03	1.00	0.188	No
311	6.22	107.44	41.40	66.04	0.90	0.208	1.43	0.146	1.03	1.00	0.188	No
312	6.24	107.77	41.59	66.18	0.90	0.209	1.43	0.146	1.03	1.00	0.188	No
313	6.26	108.11	41.79	66.32	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
314	6.28	108.44	41.99	66.45	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
315	6.30	108.77	42.18	66.59	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
316	6.32	109.10	42.38	66.72	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
317	6.34	109.43	42.58	66.85	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
318	6.36	109.76	42.77	66.99	0.89	0.209	1.43	0.146	1.03	1.00	0.189	No
319	6.38	110.08	42.97	67.12	0.89	0.209	1.43	0.146	1.03	1.00	0.189	No
320	6.40	110.41	43.16	67.25	0.89	0.209	1.43	0.147	1.03	1.00	0.189	No
321	6.42	110.74	43.36	67.38	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
322	6.44	111.06	43.56	67.51	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
323	6.46	111.39	43.75	67.64	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
324	6.48	111.72	43.95	67.77	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
325	6.50	112.05	44.15	67.90	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
326	6.52	112.38	44.34	68.04	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
327	6.54	112.71	44.54	68.17	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
328	6.56	113.04	44.73	68.31	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
329	6.58	113.37	44.93	68.44	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
330	6.60	113.71	45.13	68.58	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
331	6.62	114.04	45.32	68.72	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
332	6.64	114.37	45.52	68.86	0.89	0.211	1.43	0.147	1.03	1.00	0.190	No
333	6.66	114.71	45.71	68.99	0.89	0.211	1.43	0.147	1.03	1.00	0.191	No
334	6.68	115.04	45.91	69.13	0.89	0.211	1.43	0.148	1.03	1.00	0.191	No
335	6.70	115.38	46.11	69.27	0.89	0.211	1.43	0.148	1.03	1.00	0.191	No
336	6.72	115.71	46.30	69.41	0.88	0.211	1.43	0.148	1.03	1.00	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	116.04	46.50	69.54	0.88	0.211	1.43	0.148	1.03	1.00	0.191	No
338	6.76	116.37	46.70	69.68	0.88	0.211	1.43	0.148	1.03	1.00	0.191	No
339	6.78	116.70	46.89	69.81	0.88	0.211	1.43	0.148	1.03	1.00	0.191	No
340	6.80	117.03	47.09	69.95	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
341	6.82	117.36	47.28	70.08	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
342	6.84	117.69	47.48	70.21	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
343	6.86	118.02	47.68	70.35	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
344	6.88	118.35	47.87	70.48	0.88	0.212	1.43	0.148	1.03	1.00	0.192	No
345	6.90	118.69	48.07	70.62	0.88	0.212	1.43	0.148	1.03	1.00	0.192	No
346	6.92	119.02	48.27	70.75	0.88	0.212	1.43	0.148	1.03	1.00	0.192	No
347	6.94	119.35	48.46	70.89	0.88	0.212	1.43	0.148	1.03	1.00	0.192	No
348	6.96	119.68	48.66	71.02	0.88	0.212	1.43	0.148	1.03	1.00	0.192	No
349	6.98	120.01	48.85	71.15	0.88	0.212	1.43	0.148	1.03	1.00	0.192	No
350	7.00	120.33	49.05	71.28	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
351	7.02	120.66	49.25	71.41	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
352	7.04	120.98	49.44	71.54	0.88	0.212	1.43	0.149	1.03	1.00	0.193	No
353	7.06	121.30	49.64	71.66	0.88	0.212	1.43	0.149	1.03	1.00	0.193	No
354	7.08	121.62	49.83	71.78	0.88	0.212	1.43	0.149	1.03	1.00	0.193	No
355	7.10	121.94	50.03	71.91	0.88	0.212	1.43	0.149	1.03	1.00	0.193	No
356	7.12	122.26	50.23	72.03	0.88	0.213	1.43	0.149	1.03	1.00	0.193	No
357	7.14	122.57	50.42	72.15	0.88	0.213	1.43	0.149	1.03	1.00	0.193	No
358	7.16	122.89	50.62	72.27	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
359	7.18	123.22	50.82	72.40	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
360	7.20	123.54	51.01	72.53	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
361	7.22	123.88	51.21	72.67	0.87	0.213	1.43	0.149	1.03	1.00	0.192	No
362	7.24	124.21	51.40	72.81	0.87	0.213	1.43	0.149	1.03	1.00	0.192	No
363	7.26	124.56	51.60	72.95	0.87	0.213	1.43	0.149	1.03	1.00	0.192	No
364	7.28	124.90	51.80	73.10	0.87	0.213	1.43	0.149	1.03	1.00	0.192	No
365	7.30	125.25	51.99	73.26	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
366	7.32	125.60	52.19	73.41	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
367	7.34	125.95	52.39	73.57	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
368	7.36	126.31	52.58	73.72	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
369	7.38	126.66	52.78	73.88	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
370	7.41	127.19	53.07	74.12	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
371	7.42	127.36	53.17	74.19	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
372	7.44	127.72	53.37	74.35	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
373	7.46	128.07	53.56	74.51	0.87	0.213	1.43	0.149	1.03	1.00	0.194	No
374	7.48	128.42	53.76	74.66	0.87	0.213	1.43	0.149	1.02	1.00	0.194	No
375	7.50	128.77	53.96	74.82	0.87	0.213	1.43	0.149	1.02	1.00	0.194	No
376	7.52	129.12	54.15	74.97	0.87	0.213	1.43	0.149	1.02	1.00	0.194	No
377	7.54	129.47	54.35	75.13	0.87	0.213	1.43	0.149	1.02	1.00	0.194	No
378	7.56	129.82	54.54	75.28	0.87	0.213	1.43	0.149	1.02	1.00	0.194	No
379	7.58	130.17	54.74	75.43	0.87	0.213	1.43	0.149	1.02	1.00	0.194	No
380	7.60	130.52	54.94	75.59	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
381	7.62	130.87	55.13	75.74	0.86	0.214	1.43	0.149	1.02	1.00	0.194	No
382	7.64	131.22	55.33	75.89	0.86	0.214	1.43	0.149	1.02	1.00	0.194	No
383	7.66	131.56	55.52	76.04	0.86	0.214	1.43	0.149	1.02	1.00	0.194	No
384	7.68	131.91	55.72	76.19	0.86	0.214	1.43	0.150	1.02	1.00	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	132.26	55.92	76.34	0.86	0.214	1.43	0.150	1.02	1.00	0.194	No
386	7.72	132.60	56.11	76.49	0.86	0.214	1.43	0.150	1.02	1.00	0.194	No
387	7.74	132.95	56.31	76.64	0.86	0.214	1.43	0.150	1.02	1.00	0.194	No
388	7.76	133.30	56.51	76.79	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
389	7.78	133.64	56.70	76.94	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
390	7.80	133.99	56.90	77.09	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
391	7.82	134.33	57.09	77.23	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
392	7.84	134.67	57.29	77.38	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
393	7.86	135.00	57.49	77.52	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
394	7.88	135.34	57.68	77.66	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
395	7.90	135.67	57.88	77.79	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
396	7.92	136.00	58.08	77.92	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
397	7.94	136.33	58.27	78.05	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
398	7.96	136.65	58.47	78.18	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
399	7.98	136.98	58.66	78.31	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
400	8.00	137.30	58.86	78.44	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
401	8.02	137.62	59.06	78.56	0.85	0.214	1.43	0.150	1.02	1.00	0.197	No
402	8.04	137.93	59.25	78.68	0.85	0.214	1.43	0.150	1.02	1.00	0.197	No
403	8.06	138.24	59.45	78.80	0.85	0.214	1.43	0.150	1.02	1.00	0.197	No
404	8.08	138.56	59.64	78.91	0.85	0.214	1.43	0.150	1.02	1.00	0.197	No
405	8.10	138.87	59.84	79.03	0.85	0.214	1.43	0.150	1.02	1.00	0.197	No
406	8.12	139.18	60.04	79.14	0.85	0.214	1.43	0.150	1.02	1.00	0.197	No
407	8.14	139.49	60.23	79.25	0.85	0.214	1.43	0.150	1.02	1.00	0.197	No
408	8.16	139.80	60.43	79.37	0.85	0.214	1.43	0.150	1.02	1.00	0.197	No
409	8.18	140.11	60.63	79.48	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
410	8.20	140.42	60.82	79.59	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
411	8.22	140.72	61.02	79.71	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
412	8.24	141.03	61.21	79.82	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
413	8.26	141.35	61.41	79.93	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
414	8.28	141.66	61.61	80.05	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
415	8.30	141.97	61.80	80.16	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
416	8.32	142.28	62.00	80.28	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
417	8.34	142.59	62.20	80.39	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
418	8.36	142.90	62.39	80.51	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
419	8.38	143.21	62.59	80.62	0.85	0.215	1.43	0.150	1.02	1.00	0.197	No
420	8.40	143.53	62.78	80.74	0.85	0.215	1.43	0.151	1.02	1.00	0.197	No
421	8.42	143.84	62.98	80.86	0.85	0.215	1.43	0.151	1.02	1.00	0.197	No
422	8.44	144.16	63.18	80.98	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No
423	8.46	144.48	63.37	81.10	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No
424	8.48	144.80	63.57	81.23	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No
425	8.50	145.12	63.77	81.35	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
426	8.52	145.44	63.96	81.48	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
427	8.54	145.77	64.16	81.61	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No
428	8.56	146.09	64.35	81.74	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No
429	8.58	146.42	64.55	81.87	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
430	8.60	146.74	64.75	82.00	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
431	8.62	147.07	64.94	82.12	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
432	8.64	147.39	65.14	82.25	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	147.71	65.33	82.38	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
434	8.68	148.04	65.53	82.51	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
435	8.70	148.36	65.73	82.63	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
436	8.72	148.68	65.92	82.76	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
437	8.74	149.00	66.12	82.88	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
438	8.76	149.32	66.32	83.01	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
439	8.78	149.65	66.51	83.14	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
440	8.80	149.97	66.71	83.27	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
441	8.82	150.30	66.90	83.40	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
442	8.84	150.63	67.10	83.53	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No
443	8.86	150.96	67.30	83.66	0.83	0.215	1.43	0.151	1.02	1.00	0.197	No
444	8.88	151.29	67.49	83.80	0.83	0.215	1.43	0.151	1.02	1.00	0.197	No
445	8.90	151.63	67.69	83.94	0.83	0.215	1.43	0.151	1.02	1.00	0.197	No
446	8.92	151.97	67.89	84.08	0.83	0.215	1.43	0.151	1.02	1.00	0.197	No
447	8.94	152.31	68.08	84.23	0.83	0.215	1.43	0.151	1.02	1.00	0.197	No
448	8.96	152.65	68.28	84.37	0.83	0.215	1.43	0.151	1.01	1.00	0.197	No
449	8.98	153.00	68.47	84.52	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
450	9.00	153.34	68.67	84.67	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
451	9.02	153.68	68.87	84.82	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
452	9.04	154.03	69.06	84.97	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
453	9.06	154.38	69.26	85.12	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
454	9.08	154.72	69.45	85.26	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
455	9.10	155.06	69.65	85.41	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
456	9.12	155.40	69.85	85.56	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
457	9.14	155.74	70.04	85.70	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
458	9.16	156.08	70.24	85.84	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
459	9.18	156.42	70.44	85.98	0.83	0.215	1.43	0.151	1.01	1.00	0.199	No
460	9.20	156.75	70.63	86.12	0.83	0.215	1.43	0.151	1.01	1.00	0.199	No
461	9.22	157.09	70.83	86.26	0.83	0.215	1.43	0.151	1.01	1.00	0.199	No
462	9.24	157.42	71.02	86.40	0.83	0.215	1.43	0.151	1.01	1.00	0.199	No
463	9.26	157.75	71.22	86.53	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
464	9.28	158.08	71.42	86.66	0.83	0.215	1.43	0.151	1.01	1.00	0.198	No
465	9.30	158.41	71.61	86.79	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
466	9.32	158.73	71.81	86.92	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
467	9.34	159.05	72.01	87.04	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
468	9.36	159.36	72.20	87.16	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
469	9.38	159.68	72.40	87.28	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
470	9.40	160.00	72.59	87.41	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
471	9.42	160.33	72.79	87.54	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
472	9.44	160.65	72.99	87.67	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
473	9.46	160.98	73.18	87.80	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
474	9.48	161.31	73.38	87.93	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
475	9.50	161.63	73.58	88.06	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
476	9.52	161.96	73.77	88.18	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
477	9.54	162.28	73.97	88.31	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
478	9.56	162.61	74.16	88.44	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
479	9.58	162.94	74.36	88.58	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
480	9.60	163.27	74.56	88.71	0.82	0.215	1.43	0.151	1.01	1.00	0.197	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	163.60	74.75	88.85	0.82	0.215	1.43	0.151	1.01	1.00	0.197	No
482	9.64	163.94	74.95	88.99	0.82	0.215	1.43	0.151	1.01	1.00	0.196	No
483	9.66	164.28	75.14	89.13	0.82	0.215	1.43	0.151	1.01	1.00	0.195	No
484	9.68	164.62	75.34	89.28	0.82	0.215	1.43	0.151	1.01	1.00	0.195	No
485	9.70	164.97	75.54	89.43	0.81	0.215	1.43	0.150	1.01	1.00	0.195	No
486	9.72	165.31	75.73	89.57	0.81	0.215	1.43	0.150	1.01	1.00	0.197	No
487	9.74	165.64	75.93	89.71	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
488	9.76	165.97	76.13	89.85	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
489	9.78	166.30	76.32	89.98	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
490	9.80	166.63	76.52	90.11	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
491	9.82	166.96	76.71	90.25	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
492	9.84	167.29	76.91	90.38	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
493	9.86	167.63	77.11	90.52	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
494	9.88	167.97	77.30	90.66	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
495	9.90	168.30	77.50	90.80	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
496	9.92	168.64	77.70	90.95	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
497	9.94	168.98	77.89	91.08	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
498	9.96	169.31	78.09	91.22	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
499	9.98	169.64	78.28	91.35	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
500	10.00	169.96	78.48	91.48	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
501	10.02	170.29	78.68	91.61	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
502	10.04	170.61	78.87	91.74	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
503	10.06	170.93	79.07	91.86	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
504	10.08	171.25	79.26	91.98	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
505	10.10	171.57	79.46	92.11	0.81	0.215	1.43	0.150	1.01	1.00	0.199	No
506	10.12	171.89	79.66	92.24	0.80	0.215	1.43	0.150	1.01	1.00	0.199	No
507	10.14	172.21	79.85	92.36	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
508	10.16	172.54	80.05	92.49	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
509	10.18	172.86	80.25	92.62	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
510	10.20	173.19	80.44	92.74	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
511	10.22	173.51	80.64	92.87	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
512	10.24	173.84	80.83	93.00	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
513	10.26	174.16	81.03	93.13	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
514	10.28	174.49	81.23	93.26	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
515	10.30	174.81	81.42	93.39	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
516	10.32	175.13	81.62	93.51	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
517	10.34	175.46	81.82	93.64	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
518	10.36	175.78	82.01	93.77	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
519	10.38	176.11	82.21	93.90	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
520	10.40	176.43	82.40	94.03	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
521	10.42	176.76	82.60	94.16	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
522	10.44	177.08	82.80	94.29	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
523	10.46	177.41	82.99	94.42	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
524	10.48	177.74	83.19	94.55	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
525	10.50	178.06	83.39	94.68	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
526	10.52	178.39	83.58	94.81	0.80	0.214	1.43	0.150	1.01	1.00	0.199	No
527	10.54	178.72	83.78	94.94	0.79	0.214	1.43	0.150	1.01	1.00	0.199	No
528	10.56	179.05	83.97	95.08	0.79	0.214	1.43	0.150	1.01	1.00	0.199	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	179.38	84.17	95.21	0.79	0.214	1.43	0.150	1.00	1.00	0.199	No
530	10.60	179.71	84.37	95.34	0.79	0.214	1.43	0.150	1.00	1.00	0.199	No
531	10.62	180.04	84.56	95.47	0.79	0.214	1.43	0.150	1.00	1.00	0.198	No
532	10.64	180.37	84.76	95.61	0.79	0.214	1.43	0.150	1.00	1.00	0.198	No
533	10.66	180.70	84.95	95.74	0.79	0.214	1.43	0.150	1.00	1.00	0.198	No
534	10.68	181.03	85.15	95.88	0.79	0.214	1.43	0.150	1.00	1.00	0.198	No
535	10.70	181.37	85.35	96.02	0.79	0.214	1.43	0.150	1.00	1.00	0.198	No
536	10.72	181.70	85.54	96.16	0.79	0.214	1.43	0.150	1.00	1.00	0.199	No
537	10.74	182.03	85.74	96.29	0.79	0.214	1.43	0.150	1.00	1.00	0.199	No
538	10.76	182.36	85.94	96.42	0.79	0.214	1.43	0.149	1.00	1.00	0.199	No
539	10.78	182.69	86.13	96.56	0.79	0.214	1.43	0.149	1.00	1.00	0.199	No
540	10.80	183.02	86.33	96.69	0.79	0.213	1.43	0.149	1.00	1.00	0.199	No
541	10.82	183.34	86.52	96.82	0.79	0.213	1.43	0.149	1.00	1.00	0.199	No
542	10.84	183.67	86.72	96.95	0.79	0.213	1.43	0.149	1.00	1.00	0.199	No
543	10.86	184.00	86.92	97.08	0.79	0.213	1.43	0.149	1.00	1.00	0.198	No
544	10.88	184.33	87.11	97.22	0.79	0.213	1.43	0.149	1.00	1.00	0.199	No
545	10.90	184.66	87.31	97.36	0.79	0.213	1.43	0.149	1.00	1.00	0.199	No
546	10.92	185.00	87.51	97.49	0.79	0.213	1.43	0.149	1.00	1.00	0.199	No
547	10.94	185.33	87.70	97.62	0.79	0.213	1.43	0.149	1.00	1.00	0.199	No
548	10.96	185.65	87.90	97.76	0.78	0.213	1.43	0.149	1.00	1.00	0.199	No
549	10.98	185.98	88.09	97.89	0.78	0.213	1.43	0.149	1.00	1.00	0.199	No
550	11.00	186.31	88.29	98.02	0.78	0.213	1.43	0.149	1.00	1.00	0.199	No
551	11.02	186.63	88.49	98.14	0.78	0.213	1.43	0.149	1.00	1.00	0.199	No
552	11.04	186.95	88.68	98.27	0.78	0.213	1.43	0.149	1.00	1.00	0.199	No
553	11.06	187.27	88.88	98.39	0.78	0.213	1.43	0.149	1.00	1.00	0.199	No
554	11.08	187.59	89.07	98.52	0.78	0.213	1.43	0.149	1.00	1.00	0.199	No
555	11.10	187.91	89.27	98.64	0.78	0.213	1.43	0.149	1.00	1.00	0.199	No
556	11.12	188.23	89.47	98.77	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
557	11.14	188.56	89.66	98.89	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
558	11.16	188.88	89.86	99.02	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
559	11.18	189.21	90.06	99.15	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
560	11.20	189.54	90.25	99.28	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
561	11.22	189.87	90.45	99.42	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
562	11.24	190.20	90.64	99.56	0.78	0.213	1.43	0.149	1.00	1.00	0.197	No
563	11.26	190.54	90.84	99.70	0.78	0.213	1.43	0.149	1.00	1.00	0.196	No
564	11.28	190.88	91.04	99.85	0.78	0.212	1.43	0.149	1.00	1.00	0.196	No
565	11.30	191.23	91.23	100.00	0.78	0.212	1.43	0.149	1.00	1.00	0.196	No
566	11.32	191.58	91.43	100.15	0.78	0.212	1.43	0.149	1.00	1.00	0.195	No
567	11.34	191.93	91.63	100.31	0.78	0.212	1.43	0.149	1.00	1.00	0.195	No
568	11.36	192.29	91.82	100.46	0.78	0.212	1.43	0.149	1.00	1.00	0.195	No
569	11.38	192.64	92.02	100.62	0.77	0.212	1.43	0.148	1.00	1.00	0.196	No
570	11.40	192.99	92.21	100.78	0.77	0.212	1.43	0.148	1.00	1.00	0.196	No
571	11.42	193.34	92.41	100.93	0.77	0.212	1.43	0.148	1.00	1.00	0.196	No
572	11.44	193.69	92.61	101.08	0.77	0.212	1.43	0.148	1.00	1.00	0.196	No
573	11.46	194.04	92.80	101.24	0.77	0.212	1.43	0.148	1.00	1.00	0.196	No
574	11.48	194.39	93.00	101.39	0.77	0.212	1.43	0.148	1.00	1.00	0.196	No
575	11.50	194.74	93.19	101.55	0.77	0.212	1.43	0.148	1.00	1.00	0.196	No
576	11.52	195.10	93.39	101.71	0.77	0.212	1.43	0.148	1.00	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	195.46	93.59	101.87	0.77	0.212	1.43	0.148	1.00	1.00	0.195	No
578	11.56	195.82	93.78	102.03	0.77	0.211	1.43	0.148	1.00	1.00	0.194	No
579	11.58	196.17	93.98	102.19	0.77	0.211	1.43	0.148	1.00	1.00	0.194	No
580	11.60	196.53	94.18	102.36	0.77	0.211	1.43	0.148	1.00	1.00	0.194	No
581	11.62	196.89	94.37	102.51	0.77	0.211	1.43	0.148	1.00	1.00	0.194	No
582	11.64	197.24	94.57	102.67	0.77	0.211	1.43	0.148	1.00	1.00	0.193	No
583	11.66	197.60	94.76	102.83	0.77	0.211	1.43	0.148	1.00	1.00	0.193	No
584	11.68	197.96	94.96	103.00	0.77	0.211	1.43	0.148	1.00	1.00	0.192	No
585	11.70	198.32	95.16	103.16	0.77	0.211	1.43	0.148	1.00	1.00	0.192	No
586	11.72	198.67	95.35	103.32	0.77	0.211	1.43	0.148	1.00	1.00	0.192	No
587	11.74	199.03	95.55	103.48	0.77	0.211	1.43	0.148	1.00	1.00	0.192	No
588	11.76	199.38	95.75	103.64	0.77	0.211	1.43	0.147	1.00	1.00	0.193	No
589	11.78	199.74	95.94	103.80	0.77	0.211	1.43	0.147	1.00	1.00	0.193	No
590	11.80	200.09	96.14	103.95	0.76	0.211	1.43	0.147	1.00	1.00	0.194	No
591	11.82	200.44	96.33	104.11	0.76	0.210	1.43	0.147	1.00	1.00	0.195	No
592	11.84	200.79	96.53	104.26	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
593	11.86	201.14	96.73	104.41	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
594	11.88	201.48	96.92	104.56	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
595	11.90	201.83	97.12	104.71	0.76	0.210	1.43	0.147	1.00	1.00	0.197	No
596	11.93	202.34	97.41	104.93	0.76	0.210	1.43	0.147	1.00	1.00	0.197	No
597	11.94	202.51	97.51	105.00	0.76	0.210	1.43	0.147	1.00	1.00	0.197	No
598	11.96	202.85	97.71	105.14	0.76	0.210	1.43	0.147	1.00	1.00	0.197	No
599	11.98	203.18	97.90	105.28	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
600	12.00	203.52	98.10	105.42	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
601	12.02	203.85	98.30	105.55	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
602	12.04	204.18	98.49	105.69	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
603	12.06	204.52	98.69	105.83	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
604	12.08	204.85	98.88	105.97	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
605	12.10	205.19	99.08	106.10	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
606	12.12	205.52	99.28	106.24	0.76	0.209	1.43	0.147	1.00	1.00	0.196	No
607	12.14	205.86	99.47	106.38	0.76	0.209	1.43	0.147	1.00	1.00	0.196	No
608	12.16	206.19	99.67	106.52	0.76	0.209	1.43	0.147	1.00	1.00	0.196	No
609	12.18	206.53	99.87	106.66	0.76	0.209	1.43	0.146	1.00	1.00	0.196	No
610	12.20	206.86	100.06	106.80	0.76	0.209	1.43	0.146	1.00	1.00	0.196	No
611	12.22	207.19	100.26	106.93	0.75	0.209	1.43	0.146	1.00	1.00	0.196	No
612	12.24	207.52	100.45	107.07	0.75	0.209	1.43	0.146	1.00	1.00	0.196	No
613	12.26	207.85	100.65	107.20	0.75	0.209	1.43	0.146	1.00	1.00	0.196	No
614	12.28	208.18	100.85	107.34	0.75	0.209	1.43	0.146	1.00	1.00	0.196	No
615	12.30	208.51	101.04	107.47	0.75	0.209	1.43	0.146	1.00	1.00	0.196	No
616	12.32	208.85	101.24	107.61	0.75	0.209	1.43	0.146	1.00	1.00	0.196	No
617	12.34	209.18	101.44	107.74	0.75	0.209	1.43	0.146	1.00	1.00	0.196	No
618	12.36	209.51	101.63	107.87	0.75	0.209	1.43	0.146	0.99	1.00	0.196	No
619	12.38	209.83	101.83	108.01	0.75	0.209	1.43	0.146	0.99	1.00	0.196	No
620	12.40	210.16	102.02	108.14	0.75	0.209	1.43	0.146	0.99	1.00	0.196	No
621	12.42	210.50	102.22	108.28	0.75	0.209	1.43	0.146	0.99	1.00	0.196	No
622	12.44	210.83	102.42	108.41	0.75	0.208	1.43	0.146	0.99	1.00	0.196	No
623	12.46	211.16	102.61	108.55	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
624	12.48	211.49	102.81	108.68	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	211.83	103.01	108.82	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
626	12.52	212.16	103.20	108.96	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
627	12.54	212.50	103.40	109.10	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
628	12.56	212.84	103.59	109.25	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
629	12.58	213.18	103.79	109.39	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
630	12.60	213.52	103.99	109.54	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
631	12.62	213.86	104.18	109.68	0.75	0.208	1.43	0.145	0.99	1.00	0.195	No
632	12.64	214.21	104.38	109.83	0.74	0.208	1.43	0.145	0.99	1.00	0.195	No
633	12.66	214.55	104.57	109.98	0.74	0.208	1.43	0.145	0.99	1.00	0.195	No
634	12.68	214.90	104.77	110.12	0.74	0.208	1.43	0.145	0.99	1.00	0.195	No
635	12.70	215.24	104.97	110.27	0.74	0.208	1.43	0.145	0.99	1.00	0.195	No
636	12.72	215.58	105.16	110.42	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
637	12.74	215.93	105.36	110.57	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
638	12.76	216.27	105.56	110.71	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
639	12.78	216.62	105.75	110.86	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
640	12.80	216.96	105.95	111.01	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
641	12.82	217.31	106.14	111.16	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
642	12.84	217.65	106.34	111.31	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
643	12.86	218.00	106.54	111.47	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
644	12.89	218.53	106.83	111.70	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
645	12.90	218.70	106.93	111.77	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
646	12.92	219.05	107.13	111.93	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
647	12.95	219.58	107.42	112.16	0.74	0.207	1.43	0.145	0.99	1.00	0.194	No
648	12.96	219.75	107.52	112.23	0.74	0.206	1.43	0.145	0.99	1.00	0.194	No
649	12.98	220.10	107.71	112.39	0.74	0.206	1.43	0.144	0.99	1.00	0.194	No
650	13.00	220.46	107.91	112.55	0.74	0.206	1.43	0.144	0.99	1.00	0.194	No
651	13.02	220.81	108.11	112.70	0.74	0.206	1.43	0.144	0.99	1.00	0.193	No
652	13.04	221.16	108.30	112.86	0.74	0.206	1.43	0.144	0.99	1.00	0.193	No
653	13.06	221.52	108.50	113.02	0.74	0.206	1.43	0.144	0.99	1.00	0.193	No
654	13.08	221.87	108.69	113.18	0.73	0.206	1.43	0.144	0.99	1.00	0.193	No
655	13.10	222.23	108.89	113.33	0.73	0.206	1.43	0.144	0.99	1.00	0.193	No
656	13.12	222.58	109.09	113.49	0.73	0.206	1.43	0.144	0.99	1.00	0.193	No
657	13.14	222.93	109.28	113.65	0.73	0.206	1.43	0.144	0.99	1.00	0.193	No
658	13.16	223.28	109.48	113.81	0.73	0.206	1.43	0.144	0.99	1.00	0.193	No
659	13.18	223.64	109.68	113.96	0.73	0.206	1.43	0.144	0.99	1.00	0.193	No
660	13.20	223.99	109.87	114.11	0.73	0.205	1.43	0.144	0.99	1.00	0.193	No
661	13.22	224.34	110.07	114.27	0.73	0.205	1.43	0.144	0.99	1.00	0.193	No
662	13.24	224.68	110.26	114.42	0.73	0.205	1.43	0.144	0.99	1.00	0.193	No
663	13.26	225.03	110.46	114.57	0.73	0.205	1.43	0.144	0.99	1.00	0.193	No
664	13.28	225.37	110.66	114.71	0.73	0.205	1.43	0.144	0.99	1.00	0.193	No
665	13.30	225.71	110.85	114.86	0.73	0.205	1.43	0.144	0.99	1.00	0.193	No
666	13.32	226.05	111.05	115.00	0.73	0.205	1.43	0.143	0.99	1.00	0.193	No
667	13.34	226.39	111.25	115.14	0.73	0.205	1.43	0.143	0.99	1.00	0.193	No
668	13.36	226.72	111.44	115.28	0.73	0.205	1.43	0.143	0.99	1.00	0.193	No
669	13.38	227.06	111.64	115.42	0.73	0.205	1.43	0.143	0.99	1.00	0.193	No
670	13.40	227.39	111.83	115.56	0.73	0.205	1.43	0.143	0.99	1.00	0.193	No
671	13.42	227.72	112.03	115.69	0.73	0.205	1.43	0.143	0.99	1.00	0.193	No
672	13.44	228.06	112.23	115.83	0.73	0.204	1.43	0.143	0.99	1.00	0.193	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	228.38	112.42	115.96	0.73	0.204	1.43	0.143	0.99	1.00	0.193	No
674	13.48	228.71	112.62	116.09	0.73	0.204	1.43	0.143	0.99	1.00	0.193	No
675	13.50	229.04	112.82	116.22	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
676	13.52	229.36	113.01	116.35	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
677	13.54	229.69	113.21	116.48	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
678	13.56	230.01	113.40	116.61	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
679	13.58	230.33	113.60	116.73	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
680	13.60	230.66	113.80	116.86	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
681	13.62	230.98	113.99	116.99	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
682	13.64	231.31	114.19	117.12	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
683	13.66	231.63	114.38	117.25	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
684	13.68	231.96	114.58	117.38	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
685	13.70	232.29	114.78	117.51	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
686	13.72	232.62	114.97	117.64	0.72	0.204	1.43	0.142	0.99	1.00	0.193	No
687	13.74	232.94	115.17	117.77	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
688	13.76	233.27	115.37	117.91	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
689	13.78	233.60	115.56	118.04	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
690	13.80	233.92	115.76	118.16	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
691	13.82	234.25	115.95	118.29	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
692	13.84	234.57	116.15	118.42	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
693	13.86	234.90	116.35	118.55	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
694	13.88	235.23	116.54	118.68	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
695	13.90	235.55	116.74	118.82	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
696	13.92	235.88	116.94	118.95	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
697	13.94	236.21	117.13	119.08	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
698	13.96	236.54	117.33	119.21	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
699	13.98	236.87	117.52	119.34	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
700	14.00	237.19	117.72	119.47	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
701	14.02	237.52	117.92	119.60	0.71	0.202	1.43	0.142	0.99	1.00	0.192	No
702	14.04	237.84	118.11	119.73	0.71	0.202	1.43	0.142	0.99	1.00	0.192	No
703	14.06	238.16	118.31	119.85	0.71	0.202	1.43	0.142	0.99	1.00	0.192	No
704	14.08	238.49	118.50	119.98	0.71	0.202	1.43	0.142	0.99	1.00	0.192	No
705	14.10	238.81	118.70	120.11	0.71	0.202	1.43	0.142	0.99	1.00	0.192	No
706	14.12	239.13	118.90	120.23	0.71	0.202	1.43	0.141	0.99	1.00	0.192	No
707	14.14	239.45	119.09	120.36	0.71	0.202	1.43	0.141	0.99	1.00	0.192	No
708	14.16	239.77	119.29	120.48	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
709	14.18	240.09	119.49	120.61	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
710	14.20	240.41	119.68	120.73	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
711	14.22	240.73	119.88	120.85	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
712	14.24	241.05	120.07	120.98	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
713	14.26	241.37	120.27	121.10	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
714	14.28	241.69	120.47	121.23	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
715	14.30	242.02	120.66	121.35	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
716	14.32	242.34	120.86	121.48	0.71	0.201	1.43	0.141	0.99	1.00	0.191	No
717	14.34	242.67	121.06	121.61	0.71	0.201	1.43	0.141	0.99	1.00	0.191	No
718	14.36	242.99	121.25	121.74	0.71	0.201	1.43	0.141	0.99	1.00	0.190	No
719	14.38	243.32	121.45	121.87	0.70	0.201	1.43	0.141	0.99	1.00	0.190	No
720	14.40	243.65	121.64	122.01	0.70	0.201	1.43	0.141	0.98	1.00	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	243.98	121.84	122.14	0.70	0.201	1.43	0.141	0.99	1.00	0.190	No
722	14.44	244.30	122.04	122.27	0.70	0.201	1.43	0.141	0.99	1.00	0.191	No
723	14.46	244.63	122.23	122.39	0.70	0.201	1.43	0.141	0.99	1.00	0.190	No
724	14.48	244.95	122.43	122.52	0.70	0.201	1.43	0.141	0.98	1.00	0.190	No
725	14.50	245.28	122.63	122.66	0.70	0.201	1.43	0.141	0.98	1.00	0.190	No
726	14.52	245.61	122.82	122.79	0.70	0.201	1.43	0.140	0.98	1.00	0.190	No
727	14.54	245.94	123.02	122.93	0.70	0.201	1.43	0.140	0.98	1.00	0.189	No
728	14.56	246.28	123.21	123.06	0.70	0.201	1.43	0.140	0.98	1.00	0.189	No
729	14.58	246.61	123.41	123.20	0.70	0.200	1.43	0.140	0.98	1.00	0.189	No
730	14.60	246.95	123.61	123.34	0.70	0.200	1.43	0.140	0.98	1.00	0.189	No
731	14.62	247.29	123.80	123.49	0.70	0.200	1.43	0.140	0.98	1.00	0.189	No
732	14.64	247.63	124.00	123.63	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
733	14.66	247.97	124.19	123.78	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
734	14.68	248.31	124.39	123.92	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
735	14.70	248.66	124.59	124.07	0.70	0.200	1.43	0.140	0.98	1.00	0.189	No
736	14.72	249.00	124.78	124.22	0.70	0.200	1.43	0.140	0.98	1.00	0.189	No
737	14.74	249.35	124.98	124.37	0.70	0.200	1.43	0.140	0.98	1.00	0.188	No
738	14.76	249.69	125.18	124.51	0.70	0.200	1.43	0.140	0.98	1.00	0.188	No
739	14.78	250.03	125.37	124.66	0.70	0.200	1.43	0.140	0.98	1.00	0.188	No
740	14.80	250.38	125.57	124.81	0.70	0.199	1.43	0.140	0.98	1.00	0.188	No
741	14.82	250.73	125.76	124.96	0.69	0.199	1.43	0.140	0.98	1.00	0.188	No
742	14.84	251.08	125.96	125.12	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
743	14.87	251.61	126.25	125.35	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
744	14.88	251.78	126.35	125.43	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
745	14.91	252.31	126.65	125.66	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
746	14.92	252.48	126.75	125.73	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
747	14.94	252.82	126.94	125.88	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
748	14.96	253.17	127.14	126.03	0.69	0.199	1.43	0.139	0.98	1.00	0.189	No
749	14.98	253.50	127.33	126.17	0.69	0.199	1.43	0.139	0.98	1.00	0.189	No
750	15.00	253.84	127.53	126.31	0.69	0.199	1.43	0.139	0.98	1.00	0.189	No
751	15.02	254.17	127.73	126.44	0.69	0.198	1.43	0.139	0.98	1.00	0.189	No
752	15.04	254.50	127.92	126.58	0.69	0.198	1.43	0.139	0.98	1.00	0.188	No
753	15.06	254.83	128.12	126.71	0.69	0.198	1.43	0.139	0.98	1.00	0.188	No
754	15.08	255.17	128.31	126.85	0.69	0.198	1.43	0.139	0.98	1.00	0.187	No
755	15.10	255.51	128.51	127.00	0.69	0.198	1.43	0.139	0.98	1.00	0.186	No
756	15.12	255.85	128.71	127.15	0.69	0.198	1.43	0.139	0.98	1.00	0.186	No
757	15.14	256.20	128.90	127.30	0.69	0.198	1.43	0.139	0.98	1.00	0.185	No
758	15.16	256.55	129.10	127.45	0.69	0.198	1.43	0.138	0.98	1.00	0.186	No
759	15.18	256.90	129.30	127.61	0.69	0.198	1.43	0.138	0.98	1.00	0.187	No
760	15.20	257.25	129.49	127.76	0.69	0.198	1.43	0.138	0.98	1.00	0.187	No
761	15.22	257.59	129.69	127.91	0.69	0.198	1.43	0.138	0.98	1.00	0.188	No
762	15.24	257.94	129.88	128.06	0.69	0.197	1.43	0.138	0.98	1.00	0.188	No
763	15.26	258.29	130.08	128.20	0.69	0.197	1.43	0.138	0.98	1.00	0.188	No
764	15.28	258.63	130.28	128.35	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
765	15.30	258.98	130.47	128.51	0.68	0.197	1.43	0.138	0.98	1.00	0.187	No
766	15.32	259.32	130.67	128.66	0.68	0.197	1.43	0.138	0.98	1.00	0.186	No
767	15.34	259.67	130.87	128.81	0.68	0.197	1.43	0.138	0.98	1.00	0.185	No
768	15.36	260.02	131.06	128.96	0.68	0.197	1.43	0.138	0.98	1.00	0.185	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	260.37	131.26	129.11	0.68	0.197	1.43	0.138	0.98	1.00	0.185	No
770	15.40	260.72	131.45	129.27	0.68	0.197	1.43	0.138	0.98	1.00	0.185	No
771	15.42	261.07	131.65	129.42	0.68	0.197	1.43	0.138	0.98	1.00	0.185	No
772	15.44	261.42	131.85	129.57	0.68	0.197	1.43	0.138	0.98	1.00	0.186	No
773	15.46	261.77	132.04	129.72	0.68	0.196	1.43	0.138	0.98	1.00	0.186	No
774	15.48	262.11	132.24	129.87	0.68	0.196	1.43	0.137	0.98	1.00	0.186	No
775	15.50	262.46	132.44	130.02	0.68	0.196	1.43	0.137	0.98	1.00	0.185	No
776	15.52	262.81	132.63	130.17	0.68	0.196	1.43	0.137	0.98	1.00	0.185	No
777	15.54	263.16	132.83	130.33	0.68	0.196	1.43	0.137	0.98	1.00	0.184	No
778	15.56	263.51	133.02	130.49	0.68	0.196	1.43	0.137	0.98	1.00	0.185	No
779	15.58	263.87	133.22	130.65	0.68	0.196	1.43	0.137	0.98	1.00	0.185	No
780	15.60	264.22	133.42	130.81	0.68	0.196	1.43	0.137	0.98	1.00	0.185	No
781	15.62	264.58	133.61	130.97	0.68	0.196	1.43	0.137	0.98	1.00	0.185	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.18	100.00	3.39	0.62	1.70	1.07	0.00	1.07	4.000	No	Yes	2.00
2	0.04	0.44	100.00	3.09	0.60	1.70	5.99	0.00	5.99	4.000	No	Yes	2.00
3	0.06	0.51	100.00	3.05	0.59	1.70	8.37	0.00	8.37	4.000	No	Yes	2.00
4	0.08	0.60	100.00	3.01	0.58	1.70	9.92	0.00	9.92	4.000	No	Yes	2.00
5	0.10	0.66	100.00	3.00	0.58	1.70	10.53	0.00	10.53	4.000	No	Yes	2.00
6	0.12	0.71	100.00	3.01	0.58	1.70	11.85	0.00	11.85	4.000	No	Yes	2.00
7	0.14	1.45	74.38	2.64	0.58	1.70	12.46	0.00	12.46	4.000	Yes	Yes	2.00
8	0.16	2.72	46.78	2.30	0.49	1.70	48.02	57.29	105.32	4.000	Yes	No	2.00
9	0.18	3.55	34.74	2.15	0.43	1.70	75.83	55.81	131.64	4.000	Yes	No	2.00
10	0.20	3.58	30.59	2.09	0.49	1.70	54.63	47.00	101.63	4.000	Yes	No	2.00
11	0.22	3.19	29.39	2.08	0.51	1.70	49.66	44.64	94.30	4.000	No	No	2.00
12	0.24	3.24	22.51	1.99	0.52	1.70	56.62	35.97	92.59	4.000	No	No	2.00
13	0.26	3.71	13.00	1.88	0.57	1.70	56.60	14.10	70.70	4.000	No	No	2.00
14	0.28	3.48	18.42	1.94	0.49	1.70	73.20	29.73	102.93	4.000	No	No	2.00
15	0.30	2.98	27.17	2.05	0.53	1.70	44.85	41.02	85.87	4.000	No	No	2.00
16	0.32	2.24	44.22	2.27	0.54	1.70	31.77	51.90	83.67	4.000	No	No	2.00
17	0.34	2.15	49.51	2.33	0.52	1.70	36.07	55.37	91.43	4.000	No	No	2.00
18	0.36	2.20	51.02	2.35	0.50	1.70	40.03	57.01	97.04	4.000	No	No	2.00
19	0.38	1.87	63.29	2.50	0.51	1.70	34.67	59.27	93.94	4.000	No	No	2.00
20	0.40	1.39	85.11	2.78	0.55	1.70	19.19	0.00	19.19	4.000	No	Yes	2.00
21	0.42	1.02	100.00	3.05	0.56	1.70	15.86	0.00	15.86	4.000	No	Yes	2.00
22	0.44	0.96	100.00	3.15	0.56	1.70	16.15	0.00	16.15	4.000	No	Yes	2.00
23	0.46	0.95	100.00	3.16	0.56	1.70	15.90	0.00	15.90	4.000	No	Yes	2.00
24	0.48	0.94	100.00	3.19	0.56	1.70	15.76	0.00	15.76	4.000	No	Yes	2.00
25	0.50	0.93	100.00	3.22	0.56	1.70	15.57	0.00	15.57	4.000	No	Yes	2.00
26	0.52	0.91	100.00	3.25	0.56	1.70	15.41	0.00	15.41	4.000	No	Yes	2.00
27	0.54	0.89	100.00	3.27	0.56	1.70	14.82	0.00	14.82	4.000	No	Yes	2.00
28	0.56	0.86	100.00	3.28	0.57	1.70	14.34	0.00	14.34	4.000	No	Yes	2.00
29	0.58	0.83	100.00	3.28	0.57	1.70	14.01	0.00	14.01	4.000	No	Yes	2.00
30	0.60	0.81	100.00	3.30	0.57	1.70	13.37	0.00	13.37	4.000	No	Yes	2.00
31	0.62	0.78	100.00	3.31	0.57	1.70	13.08	0.00	13.08	4.000	No	Yes	2.00
32	0.64	0.76	100.00	3.32	0.57	1.70	12.67	0.00	12.67	4.000	No	Yes	2.00
33	0.66	0.75	100.00	3.33	0.57	1.70	12.45	0.00	12.45	4.000	No	Yes	2.00
34	0.68	0.75	100.00	3.32	0.57	1.70	12.45	0.00	12.45	4.000	No	Yes	2.00
35	0.70	0.76	100.00	3.30	0.57	1.70	12.53	0.00	12.53	4.000	No	Yes	2.00
36	0.72	0.79	100.00	3.28	0.57	1.70	13.36	0.00	13.36	4.000	No	Yes	2.00
37	0.74	0.82	100.00	3.25	0.57	1.70	13.55	0.00	13.55	4.000	No	Yes	2.00
38	0.76	0.83	100.00	3.24	0.57	1.70	14.01	0.00	14.01	4.000	No	Yes	2.00
39	0.78	0.84	100.00	3.23	0.57	1.70	13.93	0.00	13.93	4.000	No	Yes	2.00
40	0.80	0.84	100.00	3.23	0.57	1.70	14.12	0.00	14.12	4.000	No	Yes	2.00
41	0.82	0.84	100.00	3.24	0.57	1.70	13.98	0.00	13.98	4.000	No	Yes	2.00
42	0.84	0.84	100.00	3.24	0.57	1.70	14.01	0.00	14.01	4.000	No	Yes	2.00
43	0.86	0.85	100.00	3.24	0.57	1.70	14.27	0.00	14.27	4.000	No	Yes	2.00
44	0.88	0.86	100.00	3.24	0.57	1.70	14.32	0.00	14.32	4.000	No	Yes	2.00
45	0.90	0.88	100.00	3.22	0.57	1.70	14.36	0.00	14.36	4.000	No	Yes	2.00
46	0.92	0.94	100.00	3.19	0.56	1.70	15.65	0.00	15.65	4.000	No	Yes	2.00
47	0.94	0.86	100.00	3.24	0.56	1.70	17.05	0.00	17.05	4.000	No	Yes	2.00
48	0.96	0.89	100.00	3.21	0.59	1.70	8.86	0.00	8.86	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	0.92	100.00	3.18	0.56	1.70	16.88	0.00	16.88	4.000	No	Yes	2.00
50	1.00	1.09	100.00	3.06	0.55	1.70	18.01	0.00	18.01	4.000	No	Yes	2.00
51	1.02	1.12	100.00	3.03	0.55	1.70	18.53	0.00	18.53	4.000	No	Yes	2.00
52	1.04	1.13	100.00	3.03	0.55	1.70	18.52	0.00	18.52	4.000	No	Yes	2.00
53	1.06	1.12	100.00	3.03	0.55	1.70	18.40	0.00	18.40	4.000	No	Yes	2.00
54	1.09	1.15	100.00	3.02	0.55	1.70	18.35	0.00	18.35	4.000	No	Yes	2.00
55	1.10	1.18	100.00	3.01	0.55	1.70	19.73	0.00	19.73	4.000	No	Yes	2.00
56	1.12	1.22	100.00	3.01	0.55	1.70	20.21	0.00	20.21	4.000	No	Yes	2.00
57	1.14	1.23	100.00	3.02	0.55	1.70	20.20	0.00	20.20	4.000	No	Yes	2.00
58	1.16	1.22	100.00	3.04	0.54	1.70	20.26	0.00	20.26	4.000	No	Yes	2.00
59	1.18	1.22	100.00	3.05	0.55	1.70	20.06	0.00	20.06	4.000	No	Yes	2.00
60	1.20	1.22	100.00	3.06	0.55	1.70	20.23	0.00	20.23	4.000	No	Yes	2.00
61	1.23	1.21	100.00	3.07	0.55	1.70	19.98	0.00	19.98	4.000	No	Yes	2.00
62	1.24	1.21	100.00	3.07	0.55	1.70	19.74	0.00	19.74	4.000	No	Yes	2.00
63	1.26	1.24	100.00	3.06	0.54	1.70	20.28	0.00	20.28	4.000	No	Yes	2.00
64	1.28	1.29	100.00	3.03	0.54	1.70	21.35	0.00	21.35	4.000	No	Yes	2.00
65	1.30	1.35	100.00	3.00	0.54	1.70	22.34	0.00	22.34	4.000	No	Yes	2.00
66	1.32	1.42	100.00	2.97	0.53	1.70	23.34	0.00	23.34	4.000	No	Yes	2.00
67	1.34	1.47	98.97	2.95	0.53	1.70	24.52	0.00	24.52	4.000	No	Yes	2.00
68	1.36	1.53	97.52	2.93	0.53	1.70	25.17	0.00	25.17	4.000	No	Yes	2.00
69	1.38	1.57	97.09	2.93	0.53	1.70	26.27	0.00	26.27	4.000	No	Yes	2.00
70	1.40	1.61	96.94	2.92	0.52	1.70	26.59	0.00	26.59	4.000	No	Yes	2.00
71	1.42	1.63	96.99	2.92	0.52	1.70	27.01	0.00	27.01	4.000	No	Yes	2.00
72	1.44	1.64	97.20	2.93	0.52	1.70	27.36	0.00	27.36	4.000	No	Yes	2.00
73	1.46	1.64	97.86	2.94	0.52	1.70	27.06	0.00	27.06	4.000	No	Yes	2.00
74	1.48	1.62	99.08	2.95	0.52	1.70	26.77	0.00	26.77	4.000	No	Yes	2.00
75	1.50	1.59	100.00	2.97	0.53	1.70	26.24	0.00	26.24	4.000	No	Yes	2.00
76	1.52	1.56	100.00	2.98	0.53	1.70	25.72	0.00	25.72	4.000	No	Yes	2.00
77	1.54	1.54	100.00	2.99	0.53	1.70	25.46	0.00	25.46	4.000	No	Yes	2.00
78	1.56	1.53	100.00	3.00	0.53	1.70	25.24	0.00	25.24	4.000	No	Yes	2.00
79	1.59	1.50	100.00	3.02	0.53	1.70	24.87	0.00	24.87	4.000	No	Yes	2.00
80	1.60	1.45	100.00	3.03	0.53	1.70	23.81	0.00	23.81	4.000	No	Yes	2.00
81	1.62	1.39	100.00	3.05	0.54	1.70	22.84	0.00	22.84	4.000	No	Yes	2.00
82	1.64	1.34	100.00	3.06	0.54	1.70	21.82	0.00	21.82	4.000	No	Yes	2.00
83	1.66	1.31	100.00	3.07	0.54	1.70	21.68	0.00	21.68	4.000	No	Yes	2.00
84	1.68	1.29	100.00	3.07	0.54	1.70	21.19	0.00	21.19	4.000	No	Yes	2.00
85	1.70	1.27	100.00	3.07	0.54	1.70	20.94	0.00	20.94	4.000	No	Yes	2.00
86	1.72	1.25	100.00	3.08	0.54	1.70	20.38	0.00	20.38	4.000	No	Yes	2.00
87	1.74	1.21	100.00	3.09	0.55	1.70	20.00	0.00	20.00	4.000	No	Yes	2.00
88	1.76	1.18	100.00	3.10	0.55	1.70	19.25	0.00	19.25	4.000	No	Yes	2.00
89	1.78	1.15	100.00	3.11	0.55	1.70	18.88	0.00	18.88	4.000	No	Yes	2.00
90	1.80	1.12	100.00	3.12	0.55	1.70	18.40	0.00	18.40	4.000	No	Yes	2.00
91	1.82	1.10	100.00	3.13	0.55	1.70	17.89	0.00	17.89	4.000	No	Yes	2.00
92	1.84	1.08	100.00	3.13	0.55	1.70	17.48	0.00	17.48	4.000	No	Yes	2.00
93	1.86	1.08	100.00	3.12	0.55	1.70	17.38	0.00	17.38	4.000	No	Yes	2.00
94	1.88	1.09	100.00	3.11	0.55	1.70	17.96	0.00	17.96	4.000	No	Yes	2.00
95	1.90	1.10	100.00	3.10	0.55	1.70	18.05	0.00	18.05	4.000	No	Yes	2.00
96	1.92	1.09	100.00	3.11	0.55	1.70	18.10	0.00	18.10	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	1.02	100.00	3.15	0.56	1.70	17.13	0.00	17.13	4.000	No	Yes	2.00
98	1.96	0.91	100.00	3.22	0.56	1.70	14.71	0.00	14.71	4.000	No	Yes	2.00
99	1.99	0.78	100.00	3.31	0.57	1.70	12.78	0.00	12.78	4.000	No	Yes	2.00
100	2.00	0.68	100.00	3.40	0.58	1.70	10.93	0.00	10.93	4.000	No	Yes	2.00
101	2.02	0.58	100.00	3.47	0.58	1.70	9.37	0.00	9.37	4.000	No	Yes	2.00
102	2.04	0.51	100.00	3.54	0.59	1.70	8.12	0.00	8.12	4.000	No	Yes	2.00
103	2.06	0.46	100.00	3.57	0.59	1.70	7.17	0.00	7.17	4.000	No	Yes	2.00
104	2.08	0.43	100.00	3.57	0.60	1.70	6.82	0.00	6.82	4.000	No	Yes	2.00
105	2.10	0.43	100.00	3.52	0.60	1.70	6.54	0.00	6.54	4.000	No	Yes	2.00
106	2.12	0.45	100.00	3.43	0.59	1.70	6.84	0.00	6.84	4.000	No	Yes	2.00
107	2.14	0.48	100.00	3.31	0.59	1.70	7.40	0.00	7.40	4.000	No	Yes	2.00
108	2.16	0.53	100.00	3.18	0.59	1.70	8.30	0.00	8.30	4.000	No	Yes	2.00
109	2.18	0.58	100.00	3.06	0.59	1.70	9.05	0.00	9.05	4.000	No	Yes	2.00
110	2.20	0.63	99.90	2.96	0.58	1.70	10.07	0.00	10.07	4.000	No	Yes	2.00
111	2.22	0.69	94.69	2.90	0.58	1.70	10.90	0.00	10.90	4.000	No	Yes	2.00
112	2.24	0.76	90.56	2.84	0.58	1.70	11.96	0.00	11.96	4.000	No	Yes	2.00
113	2.26	0.83	87.88	2.81	0.57	1.69	13.55	0.00	13.55	4.000	No	Yes	2.00
114	2.28	0.89	87.53	2.81	0.57	1.68	14.42	0.00	14.42	4.000	No	Yes	2.00
115	2.30	0.90	89.96	2.84	0.57	1.67	14.74	0.00	14.74	4.000	No	Yes	2.00
116	2.32	0.91	93.61	2.88	0.57	1.66	14.38	0.00	14.38	4.000	No	Yes	2.00
117	2.34	0.92	96.58	2.92	0.56	1.65	14.80	0.00	14.80	4.000	No	Yes	2.00
118	2.36	0.93	99.06	2.95	0.56	1.64	14.97	0.00	14.97	4.000	No	Yes	2.00
119	2.38	0.91	100.00	3.00	0.56	1.63	14.80	0.00	14.80	4.000	No	Yes	2.00
120	2.40	0.88	100.00	3.05	0.57	1.63	13.73	0.00	13.73	4.000	No	Yes	2.00
121	2.42	0.83	100.00	3.11	0.57	1.63	13.29	0.00	13.29	4.000	No	Yes	2.00
122	2.44	0.79	100.00	3.16	0.57	1.62	12.36	0.00	12.36	4.000	No	Yes	2.00
123	2.46	0.75	100.00	3.21	0.58	1.62	11.86	0.00	11.86	4.000	No	Yes	2.00
124	2.48	0.71	100.00	3.26	0.58	1.61	11.42	0.00	11.42	4.000	No	Yes	2.00
125	2.50	0.71	100.00	3.28	0.58	1.61	10.61	0.00	10.61	4.000	No	Yes	2.00
126	2.52	0.67	100.00	3.32	0.58	1.60	11.41	0.00	11.41	4.000	No	Yes	2.00
127	2.54	0.64	100.00	3.34	0.58	1.61	9.69	0.00	9.69	4.000	No	Yes	2.00
128	2.56	0.57	100.00	3.40	0.59	1.61	8.98	0.00	8.98	4.000	No	Yes	2.00
129	2.58	0.53	100.00	3.42	0.59	1.61	8.40	0.00	8.40	4.000	No	Yes	2.00
130	2.60	0.50	100.00	3.43	0.59	1.61	7.71	0.00	7.71	4.000	No	Yes	2.00
131	2.62	0.49	100.00	3.42	0.59	1.61	7.52	0.00	7.52	4.000	No	Yes	2.00
132	2.64	0.48	100.00	3.40	0.59	1.60	7.64	0.00	7.64	4.000	No	Yes	2.00
133	2.66	0.48	100.00	3.36	0.59	1.60	7.37	0.00	7.37	4.000	No	Yes	2.00
134	2.68	0.49	100.00	3.32	0.59	1.60	7.53	0.00	7.53	4.000	No	Yes	2.00
135	2.70	0.51	100.00	3.27	0.59	1.59	7.93	0.00	7.93	4.000	No	Yes	2.00
136	2.72	0.53	100.00	3.22	0.59	1.59	7.94	0.00	7.94	4.000	No	Yes	2.00
137	2.74	0.53	100.00	3.19	0.59	1.59	8.23	0.00	8.23	4.000	No	Yes	2.00
138	2.76	0.54	100.00	3.15	0.59	1.58	8.04	0.00	8.04	4.000	No	Yes	2.00
139	2.78	0.54	100.00	3.11	0.59	1.58	8.16	0.00	8.16	4.000	No	Yes	2.00
140	2.80	0.55	100.00	3.07	0.59	1.58	8.39	0.00	8.39	4.000	No	Yes	2.00
141	2.82	0.56	100.00	3.04	0.59	1.58	8.37	0.00	8.37	4.000	No	Yes	2.00
142	2.84	0.57	100.00	3.03	0.59	1.57	8.26	0.00	8.26	4.000	No	Yes	2.00
143	2.86	0.57	100.00	3.03	0.59	1.57	8.62	0.00	8.62	4.000	No	Yes	2.00
144	2.88	0.58	100.00	3.02	0.59	1.57	8.54	0.00	8.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.59	100.00	3.01	0.59	1.56	8.66	0.00	8.66	4.000	No	Yes	2.00
146	2.92	0.68	97.10	2.93	0.59	1.56	9.03	0.00	9.03	4.000	No	Yes	2.00
147	2.94	0.75	94.47	2.89	0.57	1.54	12.49	0.00	12.49	4.000	No	Yes	2.00
148	2.96	0.80	93.01	2.88	0.58	1.55	11.45	0.00	11.45	4.000	No	Yes	2.00
149	2.98	0.77	96.85	2.92	0.58	1.54	11.22	0.00	11.22	4.000	No	Yes	2.00
150	3.00	0.76	97.73	2.93	0.58	1.54	11.21	0.00	11.21	4.000	No	Yes	2.00
151	3.02	0.77	97.87	2.94	0.58	1.54	11.12	0.00	11.12	4.000	No	Yes	2.00
152	3.04	0.78	97.65	2.93	0.58	1.54	11.37	0.00	11.37	4.000	No	Yes	2.00
153	3.06	0.81	96.38	2.92	0.58	1.53	11.62	0.00	11.62	4.000	No	Yes	2.00
154	3.08	0.82	95.53	2.91	0.57	1.53	12.20	0.00	12.20	4.000	No	Yes	2.00
155	3.10	0.81	95.15	2.90	0.58	1.53	11.78	0.00	11.78	4.000	No	Yes	2.00
156	3.12	0.79	96.38	2.92	0.58	1.53	11.34	0.00	11.34	4.000	No	Yes	2.00
157	3.14	0.76	98.09	2.94	0.58	1.53	10.95	0.00	10.95	4.000	No	Yes	2.00
158	3.16	0.76	98.83	2.95	0.58	1.52	10.60	0.00	10.60	4.000	No	Yes	2.00
159	3.18	0.77	98.38	2.94	0.58	1.52	11.05	0.00	11.05	4.000	No	Yes	2.00
160	3.20	0.79	96.57	2.92	0.58	1.52	11.26	0.00	11.26	4.000	No	Yes	2.00
161	3.22	0.80	96.15	2.91	0.58	1.51	11.70	0.00	11.70	4.000	No	Yes	2.00
162	3.24	0.81	95.50	2.91	0.58	1.51	11.26	0.00	11.26	4.000	No	Yes	2.00
163	3.26	0.80	95.15	2.90	0.58	1.51	11.57	0.00	11.57	4.000	No	Yes	2.00
164	3.28	0.81	93.98	2.89	0.58	1.51	11.52	0.00	11.52	4.000	No	Yes	2.00
165	3.30	0.81	94.88	2.90	0.58	1.50	11.72	0.00	11.72	4.000	No	Yes	2.00
166	3.32	0.80	96.81	2.92	0.58	1.50	11.38	0.00	11.38	4.000	No	Yes	2.00
167	3.34	0.78	97.77	2.93	0.58	1.50	10.90	0.00	10.90	4.000	No	Yes	2.00
168	3.36	0.79	96.49	2.92	0.58	1.50	11.05	0.00	11.05	4.000	No	Yes	2.00
169	3.38	0.81	93.97	2.89	0.58	1.50	11.36	0.00	11.36	4.000	No	Yes	2.00
170	3.40	0.86	90.88	2.85	0.58	1.49	11.83	0.00	11.83	4.000	No	Yes	2.00
171	3.42	0.94	86.79	2.80	0.57	1.49	13.01	0.00	13.01	4.000	No	Yes	2.00
172	3.44	1.04	82.12	2.74	0.57	1.48	14.76	0.00	14.76	4.000	No	Yes	2.00
173	3.46	1.09	81.44	2.73	0.56	1.47	16.16	0.00	16.16	4.000	No	Yes	2.00
174	3.48	1.05	84.80	2.77	0.57	1.47	14.80	0.00	14.80	4.000	No	Yes	2.00
175	3.50	0.97	89.64	2.83	0.57	1.48	12.89	0.00	12.89	4.000	No	Yes	2.00
176	3.52	0.93	92.13	2.86	0.57	1.48	12.83	0.00	12.83	4.000	No	Yes	2.00
177	3.54	0.96	91.17	2.85	0.57	1.47	13.16	0.00	13.16	4.000	No	Yes	2.00
178	3.56	1.00	90.29	2.84	0.57	1.47	14.21	0.00	14.21	4.000	No	Yes	2.00
179	3.58	1.01	90.87	2.85	0.57	1.46	14.44	0.00	14.44	4.000	No	Yes	2.00
180	3.60	0.96	94.28	2.89	0.57	1.46	13.59	0.00	13.59	4.000	No	Yes	2.00
181	3.62	0.93	95.73	2.91	0.57	1.46	12.43	0.00	12.43	4.000	Yes	Yes	2.00
182	3.64	1.00	92.04	2.86	0.57	1.46	13.56	0.00	13.56	4.000	Yes	Yes	2.00
183	3.66	1.16	84.12	2.76	0.56	1.45	16.49	0.00	16.49	4.000	Yes	Yes	2.00
184	3.68	1.38	77.18	2.68	0.56	1.44	18.99	0.00	18.99	4.000	Yes	Yes	2.00
185	3.70	1.61	72.00	2.61	0.55	1.43	22.62	0.00	22.62	4.000	Yes	Yes	2.00
186	3.72	1.83	67.58	2.56	0.54	1.42	25.95	57.71	83.66	4.000	Yes	No	2.00
187	3.74	2.04	62.44	2.49	0.53	1.41	28.21	57.23	85.44	4.000	Yes	No	2.00
188	3.76	2.25	57.45	2.43	0.53	1.40	31.19	56.75	87.95	4.000	Yes	No	2.00
189	3.78	2.47	52.60	2.37	0.52	1.40	34.16	56.02	90.18	4.000	Yes	No	2.00
190	3.80	2.72	48.29	2.32	0.52	1.39	36.95	55.09	92.05	4.000	Yes	No	2.00
191	3.82	2.95	44.60	2.27	0.51	1.38	40.84	54.38	95.22	4.000	Yes	No	2.00
192	3.84	2.93	44.78	2.27	0.50	1.37	43.12	55.05	98.16	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	2.59	49.62	2.33	0.52	1.39	36.06	55.41	91.47	4.000	Yes	No	2.00
194	3.88	2.09	58.57	2.44	0.54	1.40	27.14	55.94	83.08	4.000	Yes	No	2.00
195	3.90	1.65	70.30	2.59	0.54	1.40	23.43	57.50	80.93	4.000	Yes	No	2.00
196	3.92	1.51	76.38	2.67	0.56	1.42	18.32	0.00	18.32	4.000	Yes	Yes	2.00
197	3.94	1.40	82.17	2.74	0.55	1.40	20.86	0.00	20.86	4.000	Yes	Yes	2.00
198	3.96	1.40	83.64	2.76	0.56	1.41	18.57	0.00	18.57	4.000	No	Yes	2.00
199	3.98	1.30	88.57	2.82	0.56	1.41	17.50	0.00	17.50	4.000	No	Yes	2.00
200	4.00	1.24	91.29	2.85	0.56	1.41	16.23	0.00	16.23	4.000	No	Yes	2.00
201	4.02	1.18	93.40	2.88	0.56	1.41	15.59	0.00	15.59	4.000	No	Yes	2.00
202	4.04	1.13	95.11	2.90	0.56	1.41	14.93	0.00	14.93	4.000	No	Yes	2.00
203	4.06	1.07	97.86	2.94	0.57	1.41	14.14	0.00	14.14	4.000	No	Yes	2.00
204	4.09	1.02	100.00	2.97	0.57	1.41	13.16	0.00	13.16	4.000	No	Yes	2.00
205	4.10	0.99	100.00	2.98	0.57	1.41	12.73	0.00	12.73	4.000	No	Yes	2.00
206	4.12	0.99	100.00	2.97	0.57	1.40	13.01	0.00	13.01	4.000	No	Yes	2.00
207	4.14	1.01	98.58	2.94	0.57	1.40	13.17	0.00	13.17	4.000	No	Yes	2.00
208	4.16	1.02	97.40	2.93	0.57	1.40	13.36	0.00	13.36	4.000	No	Yes	2.00
209	4.18	1.01	97.37	2.93	0.57	1.40	13.31	0.00	13.31	4.000	No	Yes	2.00
210	4.20	0.97	99.07	2.95	0.57	1.40	12.74	0.00	12.74	4.000	No	Yes	2.00
211	4.22	0.91	100.00	2.99	0.57	1.40	11.90	0.00	11.90	4.000	No	Yes	2.00
212	4.24	0.83	100.00	3.05	0.58	1.40	10.97	0.00	10.97	4.000	No	Yes	2.00
213	4.26	0.75	100.00	3.13	0.58	1.40	9.83	0.00	9.83	4.000	No	Yes	2.00
214	4.28	0.67	100.00	3.22	0.59	1.40	8.96	0.00	8.96	4.000	No	Yes	2.00
215	4.30	0.61	100.00	3.29	0.59	1.40	8.06	0.00	8.06	4.000	No	Yes	2.00
216	4.32	0.59	100.00	3.32	0.59	1.40	7.56	0.00	7.56	4.000	No	Yes	2.00
217	4.34	0.64	100.00	3.26	0.59	1.40	8.03	0.00	8.03	4.000	No	Yes	2.00
218	4.36	0.82	100.00	3.08	0.58	1.39	10.17	0.00	10.17	4.000	No	Yes	2.00
219	4.38	1.09	93.03	2.88	0.57	1.37	14.39	0.00	14.39	4.000	No	Yes	2.00
220	4.40	1.41	80.50	2.72	0.55	1.36	19.29	0.00	19.29	4.000	No	Yes	2.00
221	4.42	1.69	72.72	2.62	0.54	1.35	22.98	0.00	22.98	4.000	No	Yes	2.00
222	4.44	1.82	69.44	2.58	0.54	1.35	25.32	57.89	83.21	0.119	No	No	0.72
223	4.46	1.80	68.44	2.57	0.54	1.35	24.38	57.42	81.80	0.118	No	No	0.71
224	4.48	1.67	68.04	2.56	0.55	1.35	22.25	56.73	78.98	0.115	No	No	0.69
225	4.50	1.54	67.27	2.55	0.56	1.35	20.31	56.02	76.33	0.113	No	No	0.67
226	4.52	1.44	69.09	2.58	0.56	1.35	19.32	56.08	75.40	0.112	No	No	0.66
227	4.54	1.40	73.73	2.63	0.56	1.35	18.20	0.00	18.20	4.000	No	Yes	2.00
228	4.56	1.40	77.95	2.69	0.56	1.35	18.54	0.00	18.54	4.000	No	Yes	2.00
229	4.58	1.44	80.09	2.71	0.55	1.35	19.14	0.00	19.14	4.000	No	Yes	2.00
230	4.60	1.51	80.26	2.72	0.55	1.34	19.64	0.00	19.64	4.000	No	Yes	2.00
231	4.62	1.61	79.09	2.70	0.55	1.34	21.40	0.00	21.40	4.000	No	Yes	2.00
232	4.64	1.67	78.45	2.69	0.54	1.33	22.85	0.00	22.85	4.000	No	Yes	2.00
233	4.66	1.59	80.77	2.72	0.55	1.33	21.73	0.00	21.73	4.000	No	Yes	2.00
234	4.68	1.42	86.25	2.79	0.55	1.34	18.42	0.00	18.42	4.000	No	Yes	2.00
235	4.70	1.30	90.09	2.84	0.56	1.34	16.28	0.00	16.28	4.000	No	Yes	2.00
236	4.72	1.31	88.37	2.82	0.56	1.34	16.73	0.00	16.73	4.000	No	Yes	2.00
237	4.74	1.38	85.34	2.78	0.55	1.33	18.84	0.00	18.84	4.000	No	Yes	2.00
238	4.76	1.43	84.76	2.77	0.55	1.33	18.99	0.00	18.99	4.000	No	Yes	2.00
239	4.78	1.42	86.91	2.80	0.55	1.33	18.47	0.00	18.47	4.000	No	Yes	2.00
240	4.80	1.38	89.11	2.83	0.55	1.32	18.24	0.00	18.24	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	1.34	90.49	2.84	0.56	1.32	17.61	0.00	17.61	4.000	No	Yes	2.00
242	4.84	1.30	91.27	2.85	0.56	1.32	16.89	0.00	16.89	4.000	No	Yes	2.00
243	4.86	1.25	92.78	2.87	0.56	1.32	16.69	0.00	16.69	4.000	No	Yes	2.00
244	4.88	1.18	95.35	2.90	0.56	1.32	15.49	0.00	15.49	4.000	No	Yes	2.00
245	4.90	1.10	98.04	2.94	0.57	1.32	14.12	0.00	14.12	4.000	No	Yes	2.00
246	4.92	1.02	100.00	2.98	0.57	1.32	13.80	0.00	13.80	4.000	No	Yes	2.00
247	4.94	0.94	100.00	3.02	0.57	1.32	12.27	0.00	12.27	4.000	No	Yes	2.00
248	4.96	0.83	100.00	3.10	0.58	1.33	10.78	0.00	10.78	4.000	No	Yes	2.00
249	4.98	0.74	100.00	3.16	0.58	1.33	9.58	0.00	9.58	4.000	No	Yes	2.00
250	5.00	0.71	100.00	3.19	0.59	1.33	8.93	0.00	8.93	4.000	No	Yes	2.00
251	5.02	0.77	100.00	3.12	0.58	1.32	9.41	0.00	9.41	4.000	No	Yes	2.00
252	5.04	0.91	100.00	3.01	0.57	1.32	11.99	0.00	11.99	4.000	No	Yes	2.00
253	5.06	1.04	96.93	2.92	0.57	1.31	13.95	0.00	13.95	4.000	No	Yes	2.00
254	5.08	1.13	93.43	2.88	0.57	1.31	14.50	0.00	14.50	4.000	No	Yes	2.00
255	5.10	1.17	92.54	2.87	0.56	1.30	15.33	0.00	15.33	4.000	No	Yes	2.00
256	5.12	1.13	93.37	2.88	0.56	1.30	15.17	0.00	15.17	4.000	No	Yes	2.00
257	5.14	1.00	98.94	2.95	0.57	1.30	13.07	0.00	13.07	4.000	No	Yes	2.00
258	5.16	0.83	100.00	3.06	0.58	1.31	10.18	0.00	10.18	4.000	No	Yes	2.00
259	5.18	0.68	100.00	3.19	0.59	1.31	8.82	0.00	8.82	4.000	No	Yes	2.00
260	5.20	0.59	100.00	3.26	0.59	1.31	7.23	0.00	7.23	4.000	No	Yes	2.00
261	5.22	0.55	100.00	3.30	0.59	1.31	7.02	0.00	7.02	4.000	No	Yes	2.00
262	5.24	0.54	100.00	3.29	0.59	1.31	6.87	0.00	6.87	4.000	No	Yes	2.00
263	5.26	0.54	100.00	3.29	0.59	1.31	6.95	0.00	6.95	4.000	No	Yes	2.00
264	5.28	0.55	100.00	3.26	0.59	1.31	7.00	0.00	7.00	4.000	No	Yes	2.00
265	5.30	0.57	100.00	3.22	0.59	1.31	7.22	0.00	7.22	4.000	No	Yes	2.00
266	5.32	0.60	100.00	3.16	0.59	1.30	7.50	0.00	7.50	4.000	No	Yes	2.00
267	5.34	0.63	100.00	3.11	0.59	1.30	8.01	0.00	8.01	4.000	No	Yes	2.00
268	5.36	0.68	100.00	3.08	0.59	1.30	8.65	0.00	8.65	4.000	No	Yes	2.00
269	5.38	0.69	100.00	3.08	0.59	1.29	9.04	0.00	9.04	4.000	No	Yes	2.00
270	5.40	0.67	100.00	3.11	0.59	1.29	8.55	0.00	8.55	4.000	No	Yes	2.00
271	5.42	0.63	100.00	3.16	0.59	1.29	7.84	0.00	7.84	4.000	No	Yes	2.00
272	5.44	0.62	100.00	3.18	0.59	1.29	7.60	0.00	7.60	4.000	No	Yes	2.00
273	5.46	0.67	100.00	3.14	0.59	1.29	8.19	0.00	8.19	4.000	No	Yes	2.00
274	5.48	0.72	100.00	3.10	0.58	1.29	9.43	0.00	9.43	4.000	No	Yes	2.00
275	5.50	0.69	100.00	3.14	0.58	1.28	9.42	0.00	9.42	4.000	No	Yes	2.00
276	5.52	0.62	100.00	3.21	0.59	1.29	7.27	0.00	7.27	4.000	No	Yes	2.00
277	5.54	0.57	100.00	3.26	0.60	1.29	6.67	0.00	6.67	4.000	No	Yes	2.00
278	5.56	0.57	100.00	3.24	0.59	1.28	7.38	0.00	7.38	4.000	No	Yes	2.00
279	5.59	0.57	100.00	3.24	0.59	1.28	7.34	0.00	7.34	4.000	No	Yes	2.00
280	5.60	0.56	100.00	3.24	0.60	1.28	6.66	0.00	6.66	4.000	No	Yes	2.00
281	5.62	0.59	100.00	3.20	0.59	1.28	6.97	0.00	6.97	4.000	No	Yes	2.00
282	5.64	0.66	100.00	3.10	0.59	1.28	8.37	0.00	8.37	4.000	No	Yes	2.00
283	5.66	0.72	100.00	3.04	0.59	1.27	9.23	0.00	9.23	4.000	No	Yes	2.00
284	5.68	0.74	100.00	3.04	0.59	1.27	9.30	0.00	9.30	4.000	No	Yes	2.00
285	5.70	0.71	100.00	3.10	0.59	1.27	8.85	0.00	8.85	4.000	No	Yes	2.00
286	5.72	0.68	100.00	3.15	0.59	1.27	8.12	0.00	8.12	4.000	No	Yes	2.00
287	5.74	0.66	100.00	3.17	0.59	1.27	8.06	0.00	8.06	4.000	No	Yes	2.00
288	5.76	0.67	100.00	3.15	0.59	1.27	8.17	0.00	8.17	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	0.70	100.00	3.12	0.59	1.27	8.58	0.00	8.58	4.000	No	Yes	2.00
290	5.80	0.73	100.00	3.09	0.59	1.26	8.88	0.00	8.88	4.000	No	Yes	2.00
291	5.82	0.75	100.00	3.06	0.59	1.26	9.26	0.00	9.26	4.000	No	Yes	2.00
292	5.84	0.78	100.00	3.02	0.58	1.26	9.42	0.00	9.42	4.000	No	Yes	2.00
293	5.86	0.80	100.00	3.00	0.58	1.26	9.74	0.00	9.74	4.000	No	Yes	2.00
294	5.88	0.88	99.41	2.96	0.58	1.26	9.90	0.00	9.90	4.000	No	Yes	2.00
295	5.90	0.95	98.97	2.95	0.57	1.25	12.14	0.00	12.14	4.000	No	Yes	2.00
296	5.92	0.98	100.00	2.97	0.58	1.25	11.82	0.00	11.82	4.000	No	Yes	2.00
297	5.94	0.92	100.00	3.03	0.58	1.25	10.88	0.00	10.88	4.000	No	Yes	2.00
298	5.96	0.87	100.00	3.08	0.58	1.25	10.08	0.00	10.08	4.000	No	Yes	2.00
299	5.98	0.84	100.00	3.10	0.58	1.25	9.68	0.00	9.68	4.000	No	Yes	2.00
300	6.00	0.81	100.00	3.11	0.58	1.25	9.83	0.00	9.83	4.000	No	Yes	2.00
301	6.02	0.79	100.00	3.12	0.59	1.25	9.14	0.00	9.14	4.000	No	Yes	2.00
302	6.04	0.80	100.00	3.10	0.59	1.25	8.99	0.00	8.99	4.000	No	Yes	2.00
303	6.06	0.85	100.00	3.05	0.58	1.24	9.96	0.00	9.96	4.000	No	Yes	2.00
304	6.08	0.91	100.00	2.98	0.58	1.24	10.60	0.00	10.60	4.000	No	Yes	2.00
305	6.10	0.94	99.46	2.96	0.58	1.24	11.03	0.00	11.03	4.000	No	Yes	2.00
306	6.12	0.94	100.00	2.96	0.58	1.24	11.20	0.00	11.20	4.000	No	Yes	2.00
307	6.14	0.91	100.00	2.99	0.58	1.24	10.59	0.00	10.59	4.000	No	Yes	2.00
308	6.16	0.83	100.00	3.07	0.58	1.24	9.96	0.00	9.96	4.000	No	Yes	2.00
309	6.18	0.76	100.00	3.14	0.59	1.24	8.46	0.00	8.46	4.000	No	Yes	2.00
310	6.20	0.72	100.00	3.20	0.59	1.24	8.21	0.00	8.21	4.000	No	Yes	2.00
311	6.22	0.72	100.00	3.20	0.59	1.23	8.31	0.00	8.31	4.000	No	Yes	2.00
312	6.24	0.71	100.00	3.20	0.59	1.23	8.40	0.00	8.40	4.000	No	Yes	2.00
313	6.26	0.70	100.00	3.20	0.59	1.23	7.88	0.00	7.88	4.000	No	Yes	2.00
314	6.28	0.69	100.00	3.18	0.59	1.23	7.82	0.00	7.82	4.000	No	Yes	2.00
315	6.30	0.71	100.00	3.14	0.59	1.23	8.21	0.00	8.21	4.000	No	Yes	2.00
316	6.32	0.73	100.00	3.10	0.59	1.23	8.55	0.00	8.55	4.000	No	Yes	2.00
317	6.34	0.73	100.00	3.09	0.59	1.23	8.30	0.00	8.30	4.000	No	Yes	2.00
318	6.36	0.70	100.00	3.11	0.59	1.22	8.11	0.00	8.11	4.000	No	Yes	2.00
319	6.38	0.68	100.00	3.14	0.59	1.22	7.61	0.00	7.61	4.000	No	Yes	2.00
320	6.40	0.66	100.00	3.16	0.59	1.22	7.36	0.00	7.36	4.000	No	Yes	2.00
321	6.42	0.65	100.00	3.16	0.59	1.22	7.28	0.00	7.28	4.000	No	Yes	2.00
322	6.44	0.66	100.00	3.15	0.59	1.22	7.27	0.00	7.27	4.000	No	Yes	2.00
323	6.46	0.70	100.00	3.11	0.59	1.22	7.88	0.00	7.88	4.000	No	Yes	2.00
324	6.48	0.75	100.00	3.06	0.59	1.22	8.49	0.00	8.49	4.000	No	Yes	2.00
325	6.50	0.80	100.00	3.04	0.59	1.21	9.21	0.00	9.21	4.000	No	Yes	2.00
326	6.52	0.83	100.00	3.03	0.58	1.21	9.44	0.00	9.44	4.000	No	Yes	2.00
327	6.54	0.83	100.00	3.03	0.58	1.21	9.48	0.00	9.48	4.000	No	Yes	2.00
328	6.56	0.82	100.00	3.05	0.58	1.21	9.47	0.00	9.47	4.000	No	Yes	2.00
329	6.58	0.80	100.00	3.08	0.59	1.21	9.01	0.00	9.01	4.000	No	Yes	2.00
330	6.60	0.77	100.00	3.11	0.59	1.21	8.63	0.00	8.63	4.000	No	Yes	2.00
331	6.62	0.73	100.00	3.15	0.59	1.21	8.39	0.00	8.39	4.000	No	Yes	2.00
332	6.64	0.71	100.00	3.19	0.59	1.21	7.82	0.00	7.82	4.000	No	Yes	2.00
333	6.66	0.69	100.00	3.21	0.59	1.21	7.61	0.00	7.61	4.000	No	Yes	2.00
334	6.68	0.67	100.00	3.24	0.59	1.20	7.71	0.00	7.71	4.000	No	Yes	2.00
335	6.70	0.65	100.00	3.26	0.59	1.20	7.22	0.00	7.22	4.000	No	Yes	2.00
336	6.72	0.63	100.00	3.28	0.59	1.20	6.95	0.00	6.95	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	0.63	100.00	3.27	0.59	1.20	7.05	0.00	7.05	4.000	No	Yes	2.00
338	6.76	0.64	100.00	3.25	0.59	1.20	7.10	0.00	7.10	4.000	No	Yes	2.00
339	6.78	0.64	100.00	3.24	0.59	1.20	7.09	0.00	7.09	4.000	No	Yes	2.00
340	6.80	0.63	100.00	3.25	0.59	1.20	7.09	0.00	7.09	4.000	No	Yes	2.00
341	6.82	0.61	100.00	3.28	0.60	1.20	6.69	0.00	6.69	4.000	No	Yes	2.00
342	6.84	0.59	100.00	3.31	0.60	1.20	6.42	0.00	6.42	4.000	No	Yes	2.00
343	6.86	0.57	100.00	3.34	0.60	1.19	6.36	0.00	6.36	4.000	No	Yes	2.00
344	6.88	0.59	100.00	3.32	0.60	1.19	6.20	0.00	6.20	4.000	No	Yes	2.00
345	6.90	0.62	100.00	3.29	0.59	1.19	7.08	0.00	7.08	4.000	No	Yes	2.00
346	6.92	0.64	100.00	3.25	0.59	1.19	7.18	0.00	7.18	4.000	No	Yes	2.00
347	6.94	0.64	100.00	3.25	0.59	1.19	7.10	0.00	7.10	4.000	No	Yes	2.00
348	6.96	0.63	100.00	3.26	0.59	1.19	6.96	0.00	6.96	4.000	No	Yes	2.00
349	6.98	0.61	100.00	3.26	0.60	1.19	6.80	0.00	6.80	4.000	No	Yes	2.00
350	7.00	0.60	100.00	3.26	0.60	1.19	6.48	0.00	6.48	4.000	No	Yes	2.00
351	7.02	0.60	100.00	3.23	0.60	1.18	6.50	0.00	6.50	4.000	No	Yes	2.00
352	7.04	0.61	100.00	3.20	0.60	1.18	6.75	0.00	6.75	4.000	No	Yes	2.00
353	7.06	0.62	100.00	3.17	0.60	1.18	6.75	0.00	6.75	4.000	No	Yes	2.00
354	7.08	0.62	100.00	3.16	0.60	1.18	6.79	0.00	6.79	4.000	No	Yes	2.00
355	7.10	0.63	100.00	3.14	0.60	1.18	6.71	0.00	6.71	4.000	No	Yes	2.00
356	7.12	0.65	100.00	3.11	0.59	1.18	6.94	0.00	6.94	4.000	No	Yes	2.00
357	7.14	0.70	100.00	3.06	0.59	1.18	7.48	0.00	7.48	4.000	No	Yes	2.00
358	7.16	0.75	100.00	3.02	0.59	1.17	8.22	0.00	8.22	4.000	No	Yes	2.00
359	7.18	0.82	100.00	2.98	0.59	1.17	8.78	0.00	8.78	4.000	No	Yes	2.00
360	7.20	0.89	100.00	2.96	0.58	1.17	9.81	0.00	9.81	4.000	No	Yes	2.00
361	7.22	0.94	100.00	2.97	0.58	1.17	10.47	0.00	10.47	4.000	No	Yes	2.00
362	7.24	0.97	100.00	3.00	0.58	1.17	10.85	0.00	10.85	4.000	No	Yes	2.00
363	7.26	0.98	100.00	3.05	0.58	1.16	10.86	0.00	10.86	4.000	No	Yes	2.00
364	7.28	0.98	100.00	3.09	0.58	1.16	10.95	0.00	10.95	4.000	No	Yes	2.00
365	7.30	0.98	100.00	3.13	0.58	1.16	10.95	0.00	10.95	4.000	No	Yes	2.00
366	7.32	0.98	100.00	3.15	0.58	1.16	10.98	0.00	10.98	4.000	No	Yes	2.00
367	7.34	0.98	100.00	3.17	0.58	1.16	11.00	0.00	11.00	4.000	No	Yes	2.00
368	7.36	0.98	100.00	3.18	0.58	1.16	10.86	0.00	10.86	4.000	No	Yes	2.00
369	7.38	0.96	100.00	3.20	0.58	1.16	10.79	0.00	10.79	4.000	No	Yes	2.00
370	7.41	0.94	100.00	3.22	0.58	1.16	10.52	0.00	10.52	4.000	No	Yes	2.00
371	7.42	0.92	100.00	3.23	0.58	1.15	10.26	0.00	10.26	4.000	No	Yes	2.00
372	7.44	0.89	100.00	3.25	0.58	1.15	10.09	0.00	10.09	4.000	No	Yes	2.00
373	7.46	0.86	100.00	3.28	0.58	1.15	9.49	0.00	9.49	4.000	No	Yes	2.00
374	7.48	0.83	100.00	3.31	0.59	1.15	9.20	0.00	9.20	4.000	No	Yes	2.00
375	7.50	0.82	100.00	3.31	0.59	1.15	8.96	0.00	8.96	4.000	No	Yes	2.00
376	7.52	0.83	100.00	3.30	0.59	1.15	9.12	0.00	9.12	4.000	No	Yes	2.00
377	7.54	0.85	100.00	3.28	0.58	1.15	9.36	0.00	9.36	4.000	No	Yes	2.00
378	7.56	0.88	100.00	3.24	0.58	1.15	9.65	0.00	9.65	4.000	No	Yes	2.00
379	7.58	0.92	100.00	3.20	0.58	1.14	10.24	0.00	10.24	4.000	No	Yes	2.00
380	7.60	0.96	100.00	3.16	0.58	1.14	10.60	0.00	10.60	4.000	No	Yes	2.00
381	7.62	0.98	100.00	3.13	0.58	1.14	10.79	0.00	10.79	4.000	No	Yes	2.00
382	7.64	0.99	100.00	3.12	0.58	1.14	10.98	0.00	10.98	4.000	No	Yes	2.00
383	7.66	0.99	100.00	3.12	0.58	1.14	10.83	0.00	10.83	4.000	No	Yes	2.00
384	7.68	0.96	100.00	3.14	0.58	1.14	10.57	0.00	10.57	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	0.93	100.00	3.17	0.58	1.14	10.16	0.00	10.16	4.000	No	Yes	2.00
386	7.72	0.90	100.00	3.20	0.58	1.14	9.82	0.00	9.82	4.000	No	Yes	2.00
387	7.74	0.86	100.00	3.23	0.58	1.14	9.53	0.00	9.53	4.000	No	Yes	2.00
388	7.76	0.81	100.00	3.28	0.59	1.13	8.94	0.00	8.94	4.000	No	Yes	2.00
389	7.78	0.73	100.00	3.35	0.59	1.13	7.96	0.00	7.96	4.000	No	Yes	2.00
390	7.80	0.65	100.00	3.43	0.59	1.13	7.05	0.00	7.05	4.000	No	Yes	2.00
391	7.82	0.60	100.00	3.48	0.60	1.13	6.28	0.00	6.28	4.000	No	Yes	2.00
392	7.84	0.57	100.00	3.50	0.60	1.13	6.08	0.00	6.08	4.000	No	Yes	2.00
393	7.86	0.56	100.00	3.48	0.60	1.13	5.95	0.00	5.95	4.000	No	Yes	2.00
394	7.88	0.60	100.00	3.38	0.60	1.13	6.12	0.00	6.12	4.000	No	Yes	2.00
395	7.90	0.64	100.00	3.31	0.59	1.13	7.33	0.00	7.33	4.000	No	Yes	2.00
396	7.92	0.65	100.00	3.26	0.59	1.13	7.01	0.00	7.01	4.000	No	Yes	2.00
397	7.94	0.61	100.00	3.31	0.60	1.13	6.50	0.00	6.50	4.000	No	Yes	2.00
398	7.96	0.56	100.00	3.36	0.60	1.13	5.87	0.00	5.87	4.000	No	Yes	2.00
399	7.98	0.51	100.00	3.42	0.60	1.13	5.47	0.00	5.47	4.000	No	Yes	2.00
400	8.00	0.47	100.00	3.48	0.60	1.13	4.79	0.00	4.79	4.000	No	Yes	2.00
401	8.02	0.44	100.00	3.53	0.60	1.12	4.49	0.00	4.49	4.000	No	Yes	2.00
402	8.04	0.43	100.00	3.51	0.61	1.12	4.32	0.00	4.32	4.000	No	Yes	2.00
403	8.06	0.44	100.00	3.46	0.60	1.12	4.51	0.00	4.51	4.000	No	Yes	2.00
404	8.08	0.46	100.00	3.41	0.60	1.12	4.71	0.00	4.71	4.000	No	Yes	2.00
405	8.10	0.47	100.00	3.38	0.60	1.12	4.83	0.00	4.83	4.000	No	Yes	2.00
406	8.12	0.47	100.00	3.37	0.60	1.12	4.88	0.00	4.88	4.000	No	Yes	2.00
407	8.14	0.48	100.00	3.35	0.60	1.12	4.90	0.00	4.90	4.000	No	Yes	2.00
408	8.16	0.49	100.00	3.33	0.60	1.12	5.00	0.00	5.00	4.000	No	Yes	2.00
409	8.18	0.51	100.00	3.30	0.60	1.12	5.20	0.00	5.20	4.000	No	Yes	2.00
410	8.20	0.52	100.00	3.27	0.60	1.12	5.34	0.00	5.34	4.000	No	Yes	2.00
411	8.22	0.54	100.00	3.25	0.60	1.11	5.47	0.00	5.47	4.000	No	Yes	2.00
412	8.24	0.56	100.00	3.22	0.60	1.11	5.69	0.00	5.69	4.000	No	Yes	2.00
413	8.26	0.58	100.00	3.20	0.60	1.11	5.91	0.00	5.91	4.000	No	Yes	2.00
414	8.28	0.59	100.00	3.19	0.60	1.11	6.13	0.00	6.13	4.000	No	Yes	2.00
415	8.30	0.58	100.00	3.21	0.60	1.11	5.93	0.00	5.93	4.000	No	Yes	2.00
416	8.32	0.57	100.00	3.22	0.60	1.11	5.70	0.00	5.70	4.000	No	Yes	2.00
417	8.34	0.57	100.00	3.22	0.60	1.11	5.70	0.00	5.70	4.000	No	Yes	2.00
418	8.36	0.59	100.00	3.20	0.60	1.11	5.80	0.00	5.80	4.000	No	Yes	2.00
419	8.38	0.61	100.00	3.17	0.60	1.11	6.17	0.00	6.17	4.000	No	Yes	2.00
420	8.40	0.64	100.00	3.14	0.60	1.11	6.43	0.00	6.43	4.000	No	Yes	2.00
421	8.42	0.69	100.00	3.10	0.59	1.10	6.82	0.00	6.82	4.000	No	Yes	2.00
422	8.44	0.72	100.00	3.08	0.59	1.10	7.50	0.00	7.50	4.000	No	Yes	2.00
423	8.46	0.73	100.00	3.09	0.59	1.10	7.52	0.00	7.52	4.000	No	Yes	2.00
424	8.48	0.70	100.00	3.15	0.59	1.10	7.15	0.00	7.15	4.000	No	Yes	2.00
425	8.50	0.66	100.00	3.21	0.60	1.10	6.42	0.00	6.42	4.000	No	Yes	2.00
426	8.52	0.65	100.00	3.23	0.60	1.10	6.34	0.00	6.34	4.000	No	Yes	2.00
427	8.54	0.68	100.00	3.20	0.59	1.10	6.92	0.00	6.92	4.000	No	Yes	2.00
428	8.56	0.70	100.00	3.19	0.59	1.10	7.14	0.00	7.14	4.000	No	Yes	2.00
429	8.58	0.69	100.00	3.21	0.59	1.10	6.94	0.00	6.94	4.000	No	Yes	2.00
430	8.60	0.67	100.00	3.24	0.60	1.10	6.70	0.00	6.70	4.000	No	Yes	2.00
431	8.62	0.66	100.00	3.25	0.60	1.09	6.62	0.00	6.62	4.000	No	Yes	2.00
432	8.64	0.65	100.00	3.26	0.60	1.09	6.44	0.00	6.44	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	0.66	100.00	3.23	0.60	1.09	6.39	0.00	6.39	4.000	No	Yes	2.00
434	8.68	0.68	100.00	3.20	0.59	1.09	6.85	0.00	6.85	4.000	No	Yes	2.00
435	8.70	0.71	100.00	3.15	0.59	1.09	7.11	0.00	7.11	4.000	No	Yes	2.00
436	8.72	0.73	100.00	3.12	0.59	1.09	7.27	0.00	7.27	4.000	No	Yes	2.00
437	8.74	0.75	100.00	3.11	0.59	1.09	7.56	0.00	7.56	4.000	No	Yes	2.00
438	8.76	0.76	100.00	3.12	0.59	1.09	7.55	0.00	7.55	4.000	No	Yes	2.00
439	8.78	0.78	100.00	3.11	0.59	1.09	7.62	0.00	7.62	4.000	No	Yes	2.00
440	8.80	0.81	100.00	3.09	0.59	1.09	8.05	0.00	8.05	4.000	No	Yes	2.00
441	8.82	0.84	100.00	3.06	0.59	1.08	8.47	0.00	8.47	4.000	No	Yes	2.00
442	8.84	0.88	100.00	3.05	0.59	1.08	8.83	0.00	8.83	4.000	No	Yes	2.00
443	8.86	0.94	100.00	3.03	0.59	1.08	9.25	0.00	9.25	4.000	No	Yes	2.00
444	8.88	0.99	100.00	3.02	0.58	1.08	10.28	0.00	10.28	4.000	No	Yes	2.00
445	8.90	1.02	100.00	3.02	0.58	1.08	10.49	0.00	10.49	4.000	No	Yes	2.00
446	8.92	1.01	100.00	3.06	0.58	1.08	10.20	0.00	10.20	4.000	No	Yes	2.00
447	8.94	0.98	100.00	3.10	0.58	1.08	9.97	0.00	9.97	4.000	No	Yes	2.00
448	8.96	0.95	100.00	3.15	0.58	1.08	9.72	0.00	9.72	4.000	No	Yes	2.00
449	8.98	0.92	100.00	3.19	0.59	1.08	9.14	0.00	9.14	4.000	No	Yes	2.00
450	9.00	0.89	100.00	3.22	0.59	1.07	9.09	0.00	9.09	4.000	No	Yes	2.00
451	9.02	0.89	100.00	3.23	0.59	1.07	9.01	0.00	9.01	4.000	No	Yes	2.00
452	9.04	0.88	100.00	3.25	0.59	1.07	8.92	0.00	8.92	4.000	No	Yes	2.00
453	9.06	0.86	100.00	3.26	0.59	1.07	8.72	0.00	8.72	4.000	No	Yes	2.00
454	9.08	0.84	100.00	3.28	0.59	1.07	8.48	0.00	8.48	4.000	No	Yes	2.00
455	9.10	0.81	100.00	3.29	0.59	1.07	8.16	0.00	8.16	4.000	No	Yes	2.00
456	9.12	0.76	100.00	3.32	0.59	1.07	7.74	0.00	7.74	4.000	No	Yes	2.00
457	9.14	0.71	100.00	3.37	0.59	1.07	7.10	0.00	7.10	4.000	No	Yes	2.00
458	9.16	0.66	100.00	3.42	0.60	1.07	6.57	0.00	6.57	4.000	No	Yes	2.00
459	9.18	0.62	100.00	3.45	0.60	1.07	6.18	0.00	6.18	4.000	No	Yes	2.00
460	9.20	0.60	100.00	3.48	0.60	1.07	5.91	0.00	5.91	4.000	No	Yes	2.00
461	9.22	0.60	100.00	3.45	0.60	1.07	5.73	0.00	5.73	4.000	No	Yes	2.00
462	9.24	0.63	100.00	3.40	0.60	1.06	6.32	0.00	6.32	4.000	No	Yes	2.00
463	9.26	0.66	100.00	3.34	0.60	1.06	6.59	0.00	6.59	4.000	No	Yes	2.00
464	9.28	0.66	100.00	3.32	0.60	1.06	6.70	0.00	6.70	4.000	No	Yes	2.00
465	9.30	0.63	100.00	3.33	0.60	1.06	6.13	0.00	6.13	4.000	No	Yes	2.00
466	9.32	0.61	100.00	3.32	0.60	1.06	5.73	0.00	5.73	4.000	No	Yes	2.00
467	9.34	0.61	100.00	3.28	0.60	1.06	6.00	0.00	6.00	4.000	No	Yes	2.00
468	9.36	0.64	100.00	3.23	0.60	1.06	6.26	0.00	6.26	4.000	No	Yes	2.00
469	9.38	0.68	100.00	3.19	0.60	1.06	6.58	0.00	6.58	4.000	No	Yes	2.00
470	9.40	0.76	100.00	3.13	0.59	1.06	7.16	0.00	7.16	4.000	No	Yes	2.00
471	9.42	0.83	100.00	3.08	0.59	1.06	8.65	0.00	8.65	4.000	No	Yes	2.00
472	9.44	0.85	100.00	3.08	0.59	1.05	8.88	0.00	8.88	4.000	No	Yes	2.00
473	9.46	0.79	100.00	3.15	0.59	1.05	7.84	0.00	7.84	4.000	No	Yes	2.00
474	9.48	0.70	100.00	3.24	0.60	1.05	6.81	0.00	6.81	4.000	No	Yes	2.00
475	9.50	0.66	100.00	3.29	0.60	1.05	6.15	0.00	6.15	4.000	No	Yes	2.00
476	9.52	0.66	100.00	3.28	0.60	1.05	6.45	0.00	6.45	4.000	No	Yes	2.00
477	9.54	0.69	100.00	3.25	0.60	1.05	6.73	0.00	6.73	4.000	No	Yes	2.00
478	9.56	0.79	100.00	3.16	0.59	1.05	7.16	0.00	7.16	4.000	No	Yes	2.00
479	9.58	0.94	100.00	3.02	0.59	1.05	9.21	0.00	9.21	4.000	No	Yes	2.00
480	9.60	1.14	94.38	2.89	0.58	1.05	11.64	0.00	11.64	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	1.35	86.93	2.80	0.57	1.05	13.61	0.00	13.61	4.000	No	Yes	2.00
482	9.64	1.56	81.90	2.74	0.57	1.04	15.80	0.00	15.80	4.000	No	Yes	2.00
483	9.66	1.75	78.67	2.70	0.56	1.04	18.28	0.00	18.28	4.000	No	Yes	2.00
484	9.68	1.81	78.97	2.70	0.55	1.04	19.67	0.00	19.67	4.000	No	Yes	2.00
485	9.70	1.63	84.87	2.77	0.56	1.04	17.60	0.00	17.60	4.000	No	Yes	2.00
486	9.72	1.31	95.16	2.90	0.57	1.04	12.88	0.00	12.88	4.000	No	Yes	2.00
487	9.74	0.98	100.00	3.08	0.58	1.04	9.71	0.00	9.71	4.000	No	Yes	2.00
488	9.76	0.83	100.00	3.17	0.59	1.04	6.93	0.00	6.93	4.000	No	Yes	2.00
489	9.78	0.79	100.00	3.19	0.59	1.04	7.64	0.00	7.64	4.000	No	Yes	2.00
490	9.80	0.80	100.00	3.17	0.59	1.04	7.87	0.00	7.87	4.000	No	Yes	2.00
491	9.82	0.79	100.00	3.18	0.59	1.04	7.42	0.00	7.42	4.000	No	Yes	2.00
492	9.84	0.83	100.00	3.17	0.59	1.04	7.44	0.00	7.44	4.000	No	Yes	2.00
493	9.86	0.85	100.00	3.20	0.58	1.04	9.41	0.00	9.41	4.000	No	Yes	2.00
494	9.88	0.82	100.00	3.25	0.59	1.04	8.16	0.00	8.16	4.000	No	Yes	2.00
495	9.90	0.73	100.00	3.35	0.59	1.03	7.08	0.00	7.08	4.000	No	Yes	2.00
496	9.92	0.70	100.00	3.39	0.60	1.03	6.64	0.00	6.64	4.000	No	Yes	2.00
497	9.94	0.69	100.00	3.38	0.60	1.03	6.77	0.00	6.77	4.000	No	Yes	2.00
498	9.96	0.68	100.00	3.36	0.60	1.03	6.69	0.00	6.69	4.000	No	Yes	2.00
499	9.98	0.66	100.00	3.36	0.60	1.03	6.43	0.00	6.43	4.000	No	Yes	2.00
500	10.00	0.64	100.00	3.35	0.60	1.03	6.08	0.00	6.08	4.000	No	Yes	2.00
501	10.02	0.63	100.00	3.33	0.60	1.03	6.08	0.00	6.08	4.000	No	Yes	2.00
502	10.04	0.63	100.00	3.30	0.60	1.03	5.98	0.00	5.98	4.000	No	Yes	2.00
503	10.06	0.64	100.00	3.28	0.60	1.03	6.09	0.00	6.09	4.000	No	Yes	2.00
504	10.08	0.66	100.00	3.26	0.60	1.03	6.29	0.00	6.29	4.000	No	Yes	2.00
505	10.10	0.69	100.00	3.25	0.60	1.03	6.54	0.00	6.54	4.000	No	Yes	2.00
506	10.12	0.70	100.00	3.23	0.60	1.03	6.67	0.00	6.67	4.000	No	Yes	2.00
507	10.14	0.71	100.00	3.23	0.60	1.02	6.73	0.00	6.73	4.000	No	Yes	2.00
508	10.16	0.70	100.00	3.24	0.60	1.02	6.68	0.00	6.68	4.000	No	Yes	2.00
509	10.18	0.70	100.00	3.26	0.60	1.02	6.56	0.00	6.56	4.000	No	Yes	2.00
510	10.20	0.70	100.00	3.27	0.60	1.02	6.60	0.00	6.60	4.000	No	Yes	2.00
511	10.22	0.70	100.00	3.27	0.60	1.02	6.58	0.00	6.58	4.000	No	Yes	2.00
512	10.24	0.70	100.00	3.27	0.60	1.02	6.55	0.00	6.55	4.000	No	Yes	2.00
513	10.26	0.70	100.00	3.26	0.60	1.02	6.66	0.00	6.66	4.000	No	Yes	2.00
514	10.28	0.70	100.00	3.26	0.60	1.02	6.61	0.00	6.61	4.000	No	Yes	2.00
515	10.30	0.70	100.00	3.27	0.60	1.02	6.51	0.00	6.51	4.000	No	Yes	2.00
516	10.32	0.69	100.00	3.27	0.60	1.02	6.46	0.00	6.46	4.000	No	Yes	2.00
517	10.34	0.69	100.00	3.27	0.60	1.02	6.48	0.00	6.48	4.000	No	Yes	2.00
518	10.36	0.69	100.00	3.27	0.60	1.02	6.50	0.00	6.50	4.000	No	Yes	2.00
519	10.38	0.69	100.00	3.28	0.60	1.02	6.45	0.00	6.45	4.000	No	Yes	2.00
520	10.40	0.69	100.00	3.30	0.60	1.01	6.38	0.00	6.38	4.000	No	Yes	2.00
521	10.42	0.70	100.00	3.29	0.60	1.01	6.33	0.00	6.33	4.000	No	Yes	2.00
522	10.44	0.71	100.00	3.27	0.60	1.01	6.75	0.00	6.75	4.000	No	Yes	2.00
523	10.46	0.72	100.00	3.26	0.60	1.01	6.70	0.00	6.70	4.000	No	Yes	2.00
524	10.48	0.72	100.00	3.28	0.60	1.01	6.79	0.00	6.79	4.000	No	Yes	2.00
525	10.50	0.71	100.00	3.30	0.60	1.01	6.60	0.00	6.60	4.000	No	Yes	2.00
526	10.52	0.70	100.00	3.32	0.60	1.01	6.49	0.00	6.49	4.000	No	Yes	2.00
527	10.54	0.68	100.00	3.34	0.60	1.01	6.35	0.00	6.35	4.000	No	Yes	2.00
528	10.56	0.67	100.00	3.35	0.60	1.01	6.10	0.00	6.10	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	0.69	100.00	3.33	0.60	1.01	6.27	0.00	6.27	4.000	No	Yes	2.00
530	10.60	0.81	100.00	3.20	0.59	1.01	6.89	0.00	6.89	4.000	No	Yes	2.00
531	10.62	0.91	100.00	3.10	0.58	1.01	9.53	0.00	9.53	4.000	No	Yes	2.00
532	10.64	0.97	100.00	3.06	0.58	1.00	9.34	0.00	9.34	4.000	No	Yes	2.00
533	10.66	0.92	100.00	3.12	0.59	1.00	8.73	0.00	8.73	4.000	No	Yes	2.00
534	10.68	0.85	100.00	3.21	0.59	1.00	8.30	0.00	8.30	4.000	No	Yes	2.00
535	10.70	0.79	100.00	3.28	0.59	1.00	7.38	0.00	7.38	4.000	No	Yes	2.00
536	10.72	0.71	100.00	3.36	0.59	1.00	6.97	0.00	6.97	4.000	No	Yes	2.00
537	10.74	0.66	100.00	3.41	0.60	1.00	5.90	0.00	5.90	4.000	No	Yes	2.00
538	10.76	0.63	100.00	3.44	0.60	1.00	5.87	0.00	5.87	4.000	No	Yes	2.00
539	10.78	0.64	100.00	3.40	0.60	1.00	6.02	0.00	6.02	4.000	No	Yes	2.00
540	10.80	0.65	100.00	3.37	0.60	1.00	6.13	0.00	6.13	4.000	No	Yes	2.00
541	10.82	0.65	100.00	3.35	0.60	1.00	6.10	0.00	6.10	4.000	No	Yes	2.00
542	10.84	0.71	100.00	3.31	0.60	1.00	5.99	0.00	5.99	4.000	No	Yes	2.00
543	10.86	0.72	100.00	3.33	0.59	1.00	7.84	0.00	7.84	4.000	No	Yes	2.00
544	10.88	0.72	100.00	3.36	0.60	1.00	6.75	0.00	6.75	4.000	No	Yes	2.00
545	10.90	0.65	100.00	3.45	0.60	0.99	6.06	0.00	6.06	4.000	No	Yes	2.00
546	10.92	0.62	100.00	3.49	0.60	0.99	5.66	0.00	5.66	4.000	No	Yes	2.00
547	10.94	0.61	100.00	3.48	0.60	0.99	5.59	0.00	5.59	4.000	No	Yes	2.00
548	10.96	0.61	100.00	3.46	0.60	0.99	5.72	0.00	5.72	4.000	No	Yes	2.00
549	10.98	0.62	100.00	3.43	0.60	0.99	5.58	0.00	5.58	4.000	No	Yes	2.00
550	11.00	0.63	100.00	3.39	0.60	0.99	5.71	0.00	5.71	4.000	No	Yes	2.00
551	11.02	0.64	100.00	3.36	0.60	0.99	5.97	0.00	5.97	4.000	No	Yes	2.00
552	11.04	0.65	100.00	3.34	0.60	0.99	5.90	0.00	5.90	4.000	No	Yes	2.00
553	11.06	0.64	100.00	3.34	0.60	0.99	5.85	0.00	5.85	4.000	No	Yes	2.00
554	11.08	0.64	100.00	3.34	0.60	0.99	5.82	0.00	5.82	4.000	No	Yes	2.00
555	11.10	0.66	100.00	3.32	0.60	0.99	5.86	0.00	5.86	4.000	No	Yes	2.00
556	11.12	0.71	100.00	3.26	0.60	0.99	6.32	0.00	6.32	4.000	No	Yes	2.00
557	11.14	0.78	100.00	3.19	0.59	0.99	7.13	0.00	7.13	4.000	No	Yes	2.00
558	11.16	0.84	100.00	3.14	0.59	0.99	7.89	0.00	7.89	4.000	No	Yes	2.00
559	11.18	0.88	100.00	3.13	0.59	0.98	8.19	0.00	8.19	4.000	No	Yes	2.00
560	11.20	0.88	100.00	3.14	0.59	0.98	8.12	0.00	8.12	4.000	No	Yes	2.00
561	11.22	0.95	100.00	3.11	0.59	0.98	8.18	0.00	8.18	4.000	No	Yes	2.00
562	11.24	1.11	100.00	3.01	0.58	0.98	10.10	0.00	10.10	4.000	No	Yes	2.00
563	11.26	1.31	96.67	2.92	0.57	0.98	12.91	0.00	12.91	4.000	No	Yes	2.00
564	11.28	1.48	93.10	2.88	0.57	0.98	14.17	0.00	14.17	4.000	No	Yes	2.00
565	11.30	1.59	92.84	2.87	0.56	0.98	15.43	0.00	15.43	4.000	No	Yes	2.00
566	11.32	1.65	93.64	2.88	0.56	0.98	16.53	0.00	16.53	4.000	No	Yes	2.00
567	11.34	1.64	95.57	2.91	0.56	0.98	16.01	0.00	16.01	4.000	No	Yes	2.00
568	11.36	1.56	99.35	2.95	0.56	0.98	15.13	0.00	15.13	4.000	No	Yes	2.00
569	11.38	1.46	100.00	3.00	0.57	0.98	14.11	0.00	14.11	4.000	No	Yes	2.00
570	11.40	1.37	100.00	3.04	0.57	0.98	13.01	0.00	13.01	4.000	No	Yes	2.00
571	11.42	1.30	100.00	3.06	0.57	0.98	12.43	0.00	12.43	4.000	No	Yes	2.00
572	11.44	1.28	100.00	3.07	0.57	0.97	12.18	0.00	12.18	4.000	No	Yes	2.00
573	11.46	1.29	100.00	3.08	0.57	0.97	12.38	0.00	12.38	4.000	No	Yes	2.00
574	11.48	1.34	100.00	3.06	0.57	0.97	12.74	0.00	12.74	4.000	No	Yes	2.00
575	11.50	1.43	100.00	3.03	0.57	0.97	13.47	0.00	13.47	4.000	No	Yes	2.00
576	11.52	1.56	100.00	2.99	0.56	0.97	14.95	0.00	14.95	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	1.72	97.70	2.93	0.56	0.97	16.51	0.00	16.51	4.000	No	Yes	2.00
578	11.56	1.83	94.92	2.90	0.55	0.97	17.97	0.00	17.97	4.000	No	Yes	2.00
579	11.58	1.89	93.43	2.88	0.55	0.97	18.25	0.00	18.25	4.000	No	Yes	2.00
580	11.60	1.93	90.53	2.84	0.56	0.97	17.95	0.00	17.95	4.000	No	Yes	2.00
581	11.62	2.06	85.10	2.78	0.55	0.97	19.35	0.00	19.35	4.000	No	Yes	2.00
582	11.64	2.23	80.00	2.71	0.55	0.97	21.75	0.00	21.75	4.000	No	Yes	2.00
583	11.66	2.41	76.67	2.67	0.54	0.97	22.89	0.00	22.89	4.000	No	Yes	2.00
584	11.68	2.51	75.82	2.66	0.54	0.97	24.49	0.00	24.49	4.000	No	Yes	2.00
585	11.70	2.55	75.51	2.66	0.54	0.97	24.63	0.00	24.63	4.000	No	Yes	2.00
586	11.72	2.49	76.16	2.66	0.54	0.97	23.90	0.00	23.90	4.000	No	Yes	2.00
587	11.74	2.35	77.66	2.68	0.54	0.96	22.56	0.00	22.56	4.000	No	Yes	2.00
588	11.76	2.18	80.75	2.72	0.55	0.96	20.76	0.00	20.76	4.000	No	Yes	2.00
589	11.78	1.96	86.86	2.80	0.55	0.96	18.88	0.00	18.88	4.000	No	Yes	2.00
590	11.80	1.68	96.11	2.91	0.56	0.96	16.29	0.00	16.29	4.000	No	Yes	2.00
591	11.82	1.43	100.00	3.03	0.57	0.96	12.82	0.00	12.82	4.000	No	Yes	2.00
592	11.84	1.19	100.00	3.14	0.58	0.96	11.46	0.00	11.46	4.000	No	Yes	2.00
593	11.86	1.02	100.00	3.25	0.58	0.96	9.45	0.00	9.45	4.000	No	Yes	2.00
594	11.88	0.88	100.00	3.35	0.59	0.96	7.82	0.00	7.82	4.000	No	Yes	2.00
595	11.90	0.79	100.00	3.43	0.59	0.95	7.45	0.00	7.45	4.000	No	Yes	2.00
596	11.93	0.75	100.00	3.46	0.59	0.95	6.85	0.00	6.85	4.000	No	Yes	2.00
597	11.94	0.74	100.00	3.45	0.60	0.95	6.42	0.00	6.42	4.000	No	Yes	2.00
598	11.96	0.79	100.00	3.36	0.59	0.95	6.90	0.00	6.90	4.000	No	Yes	2.00
599	11.98	0.88	100.00	3.25	0.59	0.95	8.17	0.00	8.17	4.000	No	Yes	2.00
600	12.00	0.95	100.00	3.16	0.59	0.95	8.78	0.00	8.78	4.000	No	Yes	2.00
601	12.02	0.96	100.00	3.16	0.59	0.95	9.00	0.00	9.00	4.000	No	Yes	2.00
602	12.04	0.92	100.00	3.20	0.59	0.95	8.28	0.00	8.28	4.000	No	Yes	2.00
603	12.06	0.88	100.00	3.24	0.59	0.95	7.82	0.00	7.82	4.000	No	Yes	2.00
604	12.08	0.84	100.00	3.27	0.59	0.95	7.80	0.00	7.80	4.000	No	Yes	2.00
605	12.10	0.82	100.00	3.30	0.59	0.95	7.18	0.00	7.18	4.000	No	Yes	2.00
606	12.12	0.79	100.00	3.34	0.59	0.95	7.05	0.00	7.05	4.000	No	Yes	2.00
607	12.14	0.79	100.00	3.36	0.59	0.95	7.06	0.00	7.06	4.000	No	Yes	2.00
608	12.16	0.79	100.00	3.35	0.59	0.95	7.01	0.00	7.01	4.000	No	Yes	2.00
609	12.18	0.80	100.00	3.33	0.59	0.94	7.05	0.00	7.05	4.000	No	Yes	2.00
610	12.20	0.81	100.00	3.30	0.59	0.94	7.30	0.00	7.30	4.000	No	Yes	2.00
611	12.22	0.83	100.00	3.27	0.59	0.94	7.38	0.00	7.38	4.000	No	Yes	2.00
612	12.24	0.84	100.00	3.26	0.59	0.94	7.44	0.00	7.44	4.000	No	Yes	2.00
613	12.26	0.84	100.00	3.25	0.59	0.94	7.45	0.00	7.45	4.000	No	Yes	2.00
614	12.28	0.85	100.00	3.25	0.59	0.94	7.55	0.00	7.55	4.000	No	Yes	2.00
615	12.30	0.84	100.00	3.25	0.59	0.94	7.49	0.00	7.49	4.000	No	Yes	2.00
616	12.32	0.83	100.00	3.26	0.59	0.94	7.36	0.00	7.36	4.000	No	Yes	2.00
617	12.34	0.84	100.00	3.25	0.59	0.94	7.23	0.00	7.23	4.000	No	Yes	2.00
618	12.36	0.85	100.00	3.23	0.59	0.94	7.58	0.00	7.58	4.000	No	Yes	2.00
619	12.38	0.86	100.00	3.22	0.59	0.94	7.66	0.00	7.66	4.000	No	Yes	2.00
620	12.40	0.85	100.00	3.24	0.59	0.94	7.49	0.00	7.49	4.000	No	Yes	2.00
621	12.42	0.84	100.00	3.26	0.59	0.94	7.40	0.00	7.40	4.000	No	Yes	2.00
622	12.44	0.84	100.00	3.27	0.59	0.94	7.23	0.00	7.23	4.000	No	Yes	2.00
623	12.46	0.85	100.00	3.27	0.59	0.94	7.41	0.00	7.41	4.000	No	Yes	2.00
624	12.48	0.88	100.00	3.25	0.59	0.93	7.72	0.00	7.72	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	0.91	100.00	3.23	0.59	0.93	7.99	0.00	7.99	4.000	No	Yes	2.00
626	12.52	0.92	100.00	3.23	0.59	0.93	8.13	0.00	8.13	4.000	No	Yes	2.00
627	12.54	0.94	100.00	3.24	0.59	0.93	8.21	0.00	8.21	4.000	No	Yes	2.00
628	12.56	0.95	100.00	3.25	0.59	0.93	8.31	0.00	8.31	4.000	No	Yes	2.00
629	12.58	0.95	100.00	3.26	0.59	0.93	8.39	0.00	8.39	4.000	No	Yes	2.00
630	12.60	0.94	100.00	3.28	0.59	0.93	8.34	0.00	8.34	4.000	No	Yes	2.00
631	12.62	0.94	100.00	3.30	0.59	0.93	8.11	0.00	8.11	4.000	No	Yes	2.00
632	12.64	0.93	100.00	3.31	0.59	0.93	8.17	0.00	8.17	4.000	No	Yes	2.00
633	12.66	0.95	100.00	3.30	0.59	0.93	8.24	0.00	8.24	4.000	No	Yes	2.00
634	12.68	0.97	100.00	3.28	0.59	0.93	8.49	0.00	8.49	4.000	No	Yes	2.00
635	12.70	1.00	100.00	3.25	0.59	0.93	8.83	0.00	8.83	4.000	No	Yes	2.00
636	12.72	1.02	100.00	3.24	0.59	0.93	8.93	0.00	8.93	4.000	No	Yes	2.00
637	12.74	1.02	100.00	3.24	0.59	0.93	9.07	0.00	9.07	4.000	No	Yes	2.00
638	12.76	1.02	100.00	3.25	0.59	0.93	8.87	0.00	8.87	4.000	No	Yes	2.00
639	12.78	1.00	100.00	3.28	0.59	0.92	8.70	0.00	8.70	4.000	No	Yes	2.00
640	12.80	0.99	100.00	3.29	0.59	0.92	8.53	0.00	8.53	4.000	No	Yes	2.00
641	12.82	1.01	100.00	3.28	0.59	0.92	8.62	0.00	8.62	4.000	No	Yes	2.00
642	12.84	1.03	100.00	3.27	0.59	0.92	8.94	0.00	8.94	4.000	No	Yes	2.00
643	12.86	1.06	100.00	3.26	0.59	0.92	9.02	0.00	9.02	4.000	No	Yes	2.00
644	12.89	1.08	100.00	3.25	0.59	0.92	9.23	0.00	9.23	4.000	No	Yes	2.00
645	12.90	1.10	100.00	3.24	0.58	0.92	9.44	0.00	9.44	4.000	No	Yes	2.00
646	12.92	1.12	100.00	3.23	0.58	0.92	9.63	0.00	9.63	4.000	No	Yes	2.00
647	12.95	1.14	100.00	3.23	0.58	0.92	9.81	0.00	9.81	4.000	No	Yes	2.00
648	12.96	1.14	100.00	3.24	0.58	0.92	9.82	0.00	9.82	4.000	No	Yes	2.00
649	12.98	1.13	100.00	3.26	0.58	0.92	9.65	0.00	9.65	4.000	No	Yes	2.00
650	13.00	1.11	100.00	3.28	0.58	0.92	9.46	0.00	9.46	4.000	No	Yes	2.00
651	13.02	1.11	100.00	3.29	0.58	0.92	9.47	0.00	9.47	4.000	No	Yes	2.00
652	13.04	1.10	100.00	3.30	0.58	0.92	9.48	0.00	9.48	4.000	No	Yes	2.00
653	13.06	1.09	100.00	3.31	0.59	0.92	9.18	0.00	9.18	4.000	No	Yes	2.00
654	13.08	1.07	100.00	3.32	0.59	0.91	9.25	0.00	9.25	4.000	No	Yes	2.00
655	13.10	1.06	100.00	3.33	0.59	0.91	9.08	0.00	9.08	4.000	No	Yes	2.00
656	13.12	1.03	100.00	3.35	0.59	0.91	8.83	0.00	8.83	4.000	No	Yes	2.00
657	13.14	0.99	100.00	3.38	0.59	0.91	8.55	0.00	8.55	4.000	No	Yes	2.00
658	13.16	0.95	100.00	3.41	0.59	0.91	8.09	0.00	8.09	4.000	No	Yes	2.00
659	13.18	0.91	100.00	3.45	0.59	0.91	7.72	0.00	7.72	4.000	No	Yes	2.00
660	13.20	0.88	100.00	3.46	0.59	0.91	7.38	0.00	7.38	4.000	No	Yes	2.00
661	13.22	0.86	100.00	3.47	0.59	0.91	7.31	0.00	7.31	4.000	No	Yes	2.00
662	13.24	0.85	100.00	3.46	0.59	0.91	7.18	0.00	7.18	4.000	No	Yes	2.00
663	13.26	0.83	100.00	3.45	0.59	0.91	7.09	0.00	7.09	4.000	No	Yes	2.00
664	13.28	0.81	100.00	3.45	0.59	0.91	6.84	0.00	6.84	4.000	No	Yes	2.00
665	13.30	0.79	100.00	3.46	0.60	0.91	6.61	0.00	6.61	4.000	No	Yes	2.00
666	13.32	0.78	100.00	3.45	0.60	0.90	6.46	0.00	6.46	4.000	No	Yes	2.00
667	13.34	0.78	100.00	3.43	0.60	0.90	6.50	0.00	6.50	4.000	No	Yes	2.00
668	13.36	0.78	100.00	3.42	0.60	0.90	6.59	0.00	6.59	4.000	No	Yes	2.00
669	13.38	0.76	100.00	3.43	0.60	0.90	6.40	0.00	6.40	4.000	No	Yes	2.00
670	13.40	0.74	100.00	3.45	0.60	0.90	6.14	0.00	6.14	4.000	No	Yes	2.00
671	13.42	0.71	100.00	3.47	0.60	0.90	5.89	0.00	5.89	4.000	No	Yes	2.00
672	13.44	0.69	100.00	3.48	0.60	0.90	5.70	0.00	5.70	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	0.68	100.00	3.48	0.60	0.90	5.60	0.00	5.60	4.000	No	Yes	2.00
674	13.48	0.68	100.00	3.47	0.60	0.90	5.62	0.00	5.62	4.000	No	Yes	2.00
675	13.50	0.69	100.00	3.45	0.60	0.90	5.59	0.00	5.59	4.000	No	Yes	2.00
676	13.52	0.69	100.00	3.43	0.60	0.90	5.65	0.00	5.65	4.000	No	Yes	2.00
677	13.54	0.69	100.00	3.42	0.60	0.90	5.63	0.00	5.63	4.000	No	Yes	2.00
678	13.56	0.70	100.00	3.39	0.60	0.90	5.62	0.00	5.62	4.000	No	Yes	2.00
679	13.58	0.72	100.00	3.37	0.60	0.90	5.86	0.00	5.86	4.000	No	Yes	2.00
680	13.60	0.75	100.00	3.34	0.60	0.90	6.06	0.00	6.06	4.000	No	Yes	2.00
681	13.62	0.77	100.00	3.32	0.60	0.90	6.32	0.00	6.32	4.000	No	Yes	2.00
682	13.64	0.77	100.00	3.33	0.60	0.89	6.34	0.00	6.34	4.000	No	Yes	2.00
683	13.66	0.76	100.00	3.35	0.60	0.89	6.18	0.00	6.18	4.000	No	Yes	2.00
684	13.68	0.74	100.00	3.39	0.60	0.89	6.01	0.00	6.01	4.000	No	Yes	2.00
685	13.70	0.73	100.00	3.41	0.60	0.89	5.83	0.00	5.83	4.000	No	Yes	2.00
686	13.72	0.72	100.00	3.42	0.60	0.89	5.83	0.00	5.83	4.000	No	Yes	2.00
687	13.74	0.73	100.00	3.42	0.60	0.89	5.87	0.00	5.87	4.000	No	Yes	2.00
688	13.76	0.73	100.00	3.41	0.60	0.89	5.91	0.00	5.91	4.000	No	Yes	2.00
689	13.78	0.74	100.00	3.39	0.60	0.89	5.93	0.00	5.93	4.000	No	Yes	2.00
690	13.80	0.75	100.00	3.36	0.60	0.89	6.06	0.00	6.06	4.000	No	Yes	2.00
691	13.82	0.77	100.00	3.32	0.60	0.89	6.20	0.00	6.20	4.000	No	Yes	2.00
692	13.84	0.79	100.00	3.31	0.60	0.89	6.55	0.00	6.55	4.000	No	Yes	2.00
693	13.86	0.78	100.00	3.34	0.60	0.89	6.39	0.00	6.39	4.000	No	Yes	2.00
694	13.88	0.75	100.00	3.39	0.60	0.89	5.99	0.00	5.99	4.000	No	Yes	2.00
695	13.90	0.74	100.00	3.41	0.60	0.89	5.77	0.00	5.77	4.000	No	Yes	2.00
696	13.92	0.77	100.00	3.37	0.60	0.89	6.04	0.00	6.04	4.000	No	Yes	2.00
697	13.94	0.81	100.00	3.32	0.60	0.89	6.67	0.00	6.67	4.000	No	Yes	2.00
698	13.96	0.83	100.00	3.30	0.59	0.89	6.89	0.00	6.89	4.000	No	Yes	2.00
699	13.98	0.79	100.00	3.34	0.60	0.89	6.53	0.00	6.53	4.000	No	Yes	2.00
700	14.00	0.73	100.00	3.41	0.60	0.88	5.49	0.00	5.49	4.000	No	Yes	2.00
701	14.02	0.68	100.00	3.45	0.60	0.88	5.37	0.00	5.37	4.000	No	Yes	2.00
702	14.04	0.67	100.00	3.46	0.60	0.88	5.31	0.00	5.31	4.000	No	Yes	2.00
703	14.06	0.66	100.00	3.47	0.60	0.88	5.21	0.00	5.21	4.000	No	Yes	2.00
704	14.08	0.65	100.00	3.49	0.60	0.88	5.05	0.00	5.05	4.000	No	Yes	2.00
705	14.10	0.66	100.00	3.48	0.60	0.88	5.06	0.00	5.06	4.000	No	Yes	2.00
706	14.12	0.68	100.00	3.45	0.60	0.88	5.34	0.00	5.34	4.000	No	Yes	2.00
707	14.14	0.69	100.00	3.41	0.60	0.88	5.47	0.00	5.47	4.000	No	Yes	2.00
708	14.16	0.70	100.00	3.40	0.60	0.88	5.53	0.00	5.53	4.000	No	Yes	2.00
709	14.18	0.70	100.00	3.40	0.60	0.88	5.46	0.00	5.46	4.000	No	Yes	2.00
710	14.20	0.71	100.00	3.37	0.60	0.88	5.46	0.00	5.46	4.000	No	Yes	2.00
711	14.22	0.75	100.00	3.31	0.60	0.88	5.81	0.00	5.81	4.000	No	Yes	2.00
712	14.24	0.78	100.00	3.27	0.60	0.88	6.46	0.00	6.46	4.000	No	Yes	2.00
713	14.26	0.79	100.00	3.28	0.60	0.88	6.49	0.00	6.49	4.000	No	Yes	2.00
714	14.28	0.75	100.00	3.35	0.60	0.88	6.06	0.00	6.06	4.000	No	Yes	2.00
715	14.30	0.72	100.00	3.40	0.60	0.88	5.64	0.00	5.64	4.000	No	Yes	2.00
716	14.32	0.74	100.00	3.39	0.60	0.88	5.60	0.00	5.60	4.000	No	Yes	2.00
717	14.34	0.82	100.00	3.29	0.60	0.88	6.32	0.00	6.32	4.000	No	Yes	2.00
718	14.36	0.96	100.00	3.17	0.59	0.88	7.79	0.00	7.79	4.000	No	Yes	2.00
719	14.38	1.07	100.00	3.09	0.59	0.88	8.95	0.00	8.95	4.000	No	Yes	2.00
720	14.40	1.05	100.00	3.11	0.58	0.88	9.39	0.00	9.39	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	0.96	100.00	3.18	0.59	0.87	7.27	0.00	7.27	4.000	No	Yes	2.00
722	14.44	0.87	100.00	3.25	0.60	0.87	6.48	0.00	6.48	4.000	No	Yes	2.00
723	14.46	0.87	100.00	3.25	0.59	0.87	6.83	0.00	6.83	4.000	No	Yes	2.00
724	14.48	0.91	100.00	3.21	0.59	0.87	6.93	0.00	6.93	4.000	No	Yes	2.00
725	14.50	1.02	100.00	3.13	0.59	0.87	7.57	0.00	7.57	4.000	No	Yes	2.00
726	14.52	1.18	100.00	3.04	0.58	0.87	9.32	0.00	9.32	4.000	No	Yes	2.00
727	14.54	1.35	98.82	2.95	0.58	0.87	11.26	0.00	11.26	4.000	No	Yes	2.00
728	14.56	1.43	96.63	2.92	0.57	0.87	12.57	0.00	12.57	4.000	No	Yes	2.00
729	14.58	1.42	98.07	2.94	0.57	0.87	12.17	0.00	12.17	4.000	No	Yes	2.00
730	14.60	1.32	100.00	3.02	0.58	0.87	11.50	0.00	11.50	4.000	No	Yes	2.00
731	14.62	1.18	100.00	3.12	0.58	0.87	10.04	0.00	10.04	4.000	No	Yes	2.00
732	14.64	1.04	100.00	3.25	0.59	0.87	8.51	0.00	8.51	4.000	No	Yes	2.00
733	14.66	0.94	100.00	3.35	0.59	0.87	7.74	0.00	7.74	4.000	No	Yes	2.00
734	14.68	0.95	100.00	3.36	0.59	0.87	7.45	0.00	7.45	4.000	No	Yes	2.00
735	14.70	1.05	100.00	3.27	0.59	0.87	8.41	0.00	8.41	4.000	No	Yes	2.00
736	14.72	1.23	100.00	3.14	0.58	0.87	10.24	0.00	10.24	4.000	No	Yes	2.00
737	14.74	1.36	100.00	3.06	0.57	0.87	11.99	0.00	11.99	4.000	No	Yes	2.00
738	14.76	1.43	100.00	3.01	0.57	0.87	11.94	0.00	11.94	4.000	No	Yes	2.00
739	14.78	1.38	100.00	3.04	0.57	0.87	12.23	0.00	12.23	4.000	No	Yes	2.00
740	14.80	1.38	100.00	3.07	0.58	0.87	10.75	0.00	10.75	4.000	No	Yes	2.00
741	14.82	1.34	100.00	3.13	0.57	0.87	12.07	0.00	12.07	4.000	No	Yes	2.00
742	14.84	1.38	100.00	3.14	0.58	0.87	11.05	0.00	11.05	4.000	No	Yes	2.00
743	14.87	1.33	100.00	3.18	0.58	0.87	11.62	0.00	11.62	4.000	No	Yes	2.00
744	14.88	1.29	100.00	3.20	0.58	0.86	10.84	0.00	10.84	4.000	No	Yes	2.00
745	14.91	1.18	100.00	3.25	0.58	0.86	9.99	0.00	9.99	4.000	No	Yes	2.00
746	14.92	1.12	100.00	3.26	0.59	0.86	8.98	0.00	8.98	4.000	No	Yes	2.00
747	14.94	1.05	100.00	3.30	0.59	0.86	9.15	0.00	9.15	4.000	No	Yes	2.00
748	14.96	0.93	100.00	3.37	0.59	0.86	8.08	0.00	8.08	4.000	No	Yes	2.00
749	14.98	0.79	100.00	3.48	0.60	0.86	5.95	0.00	5.95	4.000	No	Yes	2.00
750	15.00	0.73	100.00	3.52	0.60	0.86	5.58	0.00	5.58	4.000	No	Yes	2.00
751	15.02	0.81	100.00	3.39	0.60	0.86	6.23	0.00	6.23	4.000	No	Yes	2.00
752	15.04	1.02	100.00	3.18	0.59	0.86	7.80	0.00	7.80	4.000	No	Yes	2.00
753	15.06	1.29	100.00	3.00	0.58	0.86	10.51	0.00	10.51	4.000	No	Yes	2.00
754	15.08	1.59	92.66	2.87	0.57	0.86	13.11	0.00	13.11	4.000	No	Yes	2.00
755	15.10	1.86	86.67	2.80	0.56	0.86	15.64	0.00	15.64	4.000	No	Yes	2.00
756	15.12	2.03	85.29	2.78	0.56	0.86	17.81	0.00	17.81	4.000	No	Yes	2.00
757	15.14	1.98	89.49	2.83	0.56	0.86	17.89	0.00	17.89	4.000	No	Yes	2.00
758	15.16	1.75	97.76	2.93	0.56	0.86	14.72	0.00	14.72	4.000	No	Yes	2.00
759	15.18	1.43	100.00	3.09	0.57	0.86	11.93	0.00	11.93	4.000	No	Yes	2.00
760	15.20	1.16	100.00	3.25	0.58	0.85	9.74	0.00	9.74	4.000	No	Yes	2.00
761	15.22	0.98	100.00	3.38	0.59	0.85	7.73	0.00	7.73	4.000	No	Yes	2.00
762	15.24	0.88	100.00	3.47	0.59	0.85	7.15	0.00	7.15	4.000	No	Yes	2.00
763	15.26	0.87	100.00	3.48	0.59	0.85	7.07	0.00	7.07	4.000	No	Yes	2.00
764	15.28	0.98	100.00	3.38	0.59	0.85	7.40	0.00	7.40	4.000	No	Yes	2.00
765	15.30	1.23	100.00	3.20	0.58	0.85	9.86	0.00	9.86	4.000	No	Yes	2.00
766	15.32	1.56	100.00	3.00	0.57	0.85	13.08	0.00	13.08	4.000	No	Yes	2.00
767	15.34	1.85	92.16	2.86	0.56	0.86	15.97	0.00	15.97	4.000	No	Yes	2.00
768	15.36	2.05	86.31	2.79	0.56	0.86	17.21	0.00	17.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	2.10	86.90	2.80	0.56	0.86	18.26	0.00	18.26	4.000	No	Yes	2.00
770	15.40	1.97	92.09	2.86	0.56	0.86	17.25	0.00	17.25	4.000	No	Yes	2.00
771	15.42	1.69	100.00	2.99	0.57	0.85	13.89	0.00	13.89	4.000	No	Yes	2.00
772	15.44	1.38	100.00	3.12	0.58	0.85	11.12	0.00	11.12	4.000	No	Yes	2.00
773	15.46	1.25	100.00	3.18	0.58	0.85	9.49	0.00	9.49	4.000	No	Yes	2.00
774	15.48	1.33	100.00	3.11	0.58	0.85	10.51	0.00	10.51	4.000	No	Yes	2.00
775	15.50	1.57	100.00	2.98	0.57	0.85	13.16	0.00	13.16	4.000	No	Yes	2.00
776	15.52	1.80	96.63	2.92	0.56	0.85	15.53	0.00	15.53	4.000	No	Yes	2.00
777	15.54	1.88	96.59	2.92	0.56	0.85	16.11	0.00	16.11	4.000	No	Yes	2.00
778	15.56	1.85	99.61	2.96	0.56	0.85	15.24	0.00	15.24	4.000	No	Yes	2.00
779	15.58	1.81	100.00	2.98	0.56	0.85	14.77	0.00	14.77	4.000	No	Yes	2.00
780	15.60	1.80	100.00	2.99	0.56	0.85	15.02	0.00	15.02	4.000	No	Yes	2.00
781	15.62	1.72	100.00	3.02	0.57	0.85	13.82	0.00	13.82	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.09	2.00	0.00	9.46	0.03	0.00
1.10	2.00	0.00	9.45	0.01	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.23	2.00	0.00	9.39	0.03	0.00	1.24	2.00	0.00	9.38	0.01	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.59	2.00	0.00	9.21	0.03	0.00	1.60	2.00	0.00	9.20	0.01	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.99	2.00	0.00	9.01	0.03	0.00	2.00	2.00	0.00	9.00	0.01	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.04	2.00	0.00	7.98	0.02	0.00
4.06	2.00	0.00	7.97	0.02	0.00	4.09	2.00	0.00	7.96	0.03	0.00
4.10	2.00	0.00	7.95	0.01	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	0.72	0.28	7.78	0.02	0.04
4.46	0.71	0.29	7.77	0.02	0.05	4.48	0.69	0.31	7.76	0.02	0.05
4.50	0.67	0.33	7.75	0.02	0.05	4.52	0.66	0.34	7.74	0.02	0.05
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.59	2.00	0.00	7.21	0.03	0.00	5.60	2.00	0.00	7.20	0.01	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.41	2.00	0.00	6.30	0.03	0.00
7.42	2.00	0.00	6.29	0.01	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.02	2.00	0.00	4.99	0.02	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.93	2.00	0.00	4.04	0.03	0.00
11.94	2.00	0.00	4.03	0.01	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.89	2.00	0.00	3.56	0.03	0.00
12.90	2.00	0.00	3.55	0.01	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.95	2.00	0.00	3.53	0.03	0.00	12.96	2.00	0.00	3.52	0.01	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.20	2.00	0.00	3.40	0.02	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.82	2.00	0.00	3.09	0.02	0.00	13.84	2.00	0.00	3.08	0.02	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.80	2.00	0.00	2.60	0.02	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.84	2.00	0.00	2.58	0.02	0.00
14.87	2.00	0.00	2.57	0.03	0.00	14.88	2.00	0.00	2.56	0.01	0.00
14.91	2.00	0.00	2.55	0.03	0.00	14.92	2.00	0.00	2.54	0.01	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.00	2.00	0.00	2.50	0.02	0.00
15.02	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00
15.62	2.00	0.00	2.19	0.02	0.00						

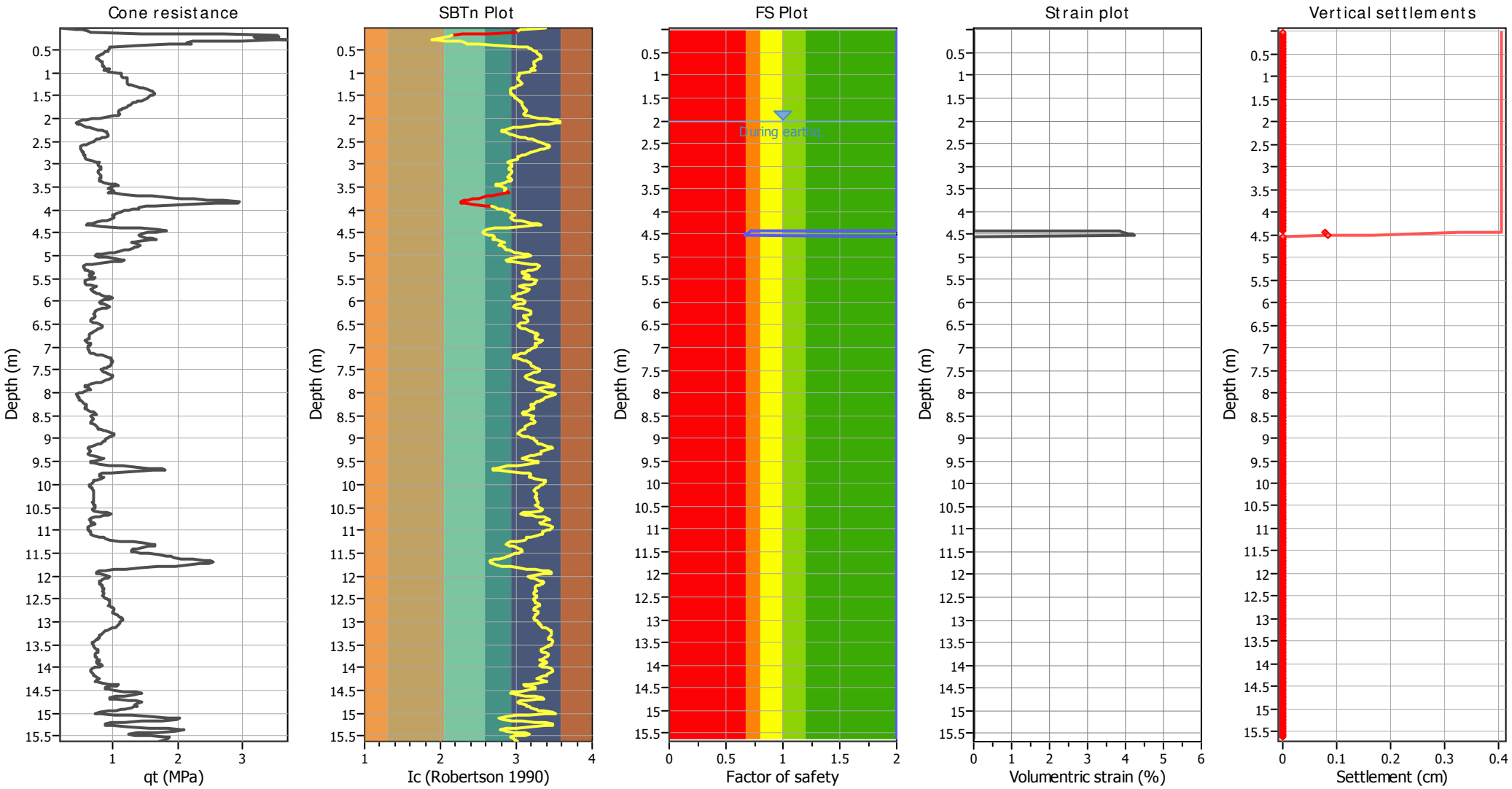
Overall liquefaction potential: 0.24

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.00	10.93	2.00	0.00	1.00	0.00	2.02	9.37	2.00	0.00	1.00	0.00
2.04	8.12	2.00	0.00	1.00	0.00	2.06	7.17	2.00	0.00	1.00	0.00
2.08	6.82	2.00	0.00	1.00	0.00	2.10	6.54	2.00	0.00	1.00	0.00
2.12	6.84	2.00	0.00	1.00	0.00	2.14	7.40	2.00	0.00	1.00	0.00
2.16	8.30	2.00	0.00	1.00	0.00	2.18	9.05	2.00	0.00	1.00	0.00
2.20	10.07	2.00	0.00	1.00	0.00	2.22	10.90	2.00	0.00	1.00	0.00
2.24	11.96	2.00	0.00	1.00	0.00	2.26	13.55	2.00	0.00	1.00	0.00
2.28	14.42	2.00	0.00	1.00	0.00	2.30	14.74	2.00	0.00	1.00	0.00
2.32	14.38	2.00	0.00	1.00	0.00	2.34	14.80	2.00	0.00	1.00	0.00
2.36	14.97	2.00	0.00	1.00	0.00	2.38	14.80	2.00	0.00	1.00	0.00
2.40	13.73	2.00	0.00	1.00	0.00	2.42	13.29	2.00	0.00	1.00	0.00
2.44	12.36	2.00	0.00	1.00	0.00	2.46	11.86	2.00	0.00	1.00	0.00
2.48	11.42	2.00	0.00	1.00	0.00	2.50	10.61	2.00	0.00	1.00	0.00
2.52	11.41	2.00	0.00	1.00	0.00	2.54	9.69	2.00	0.00	1.00	0.00
2.56	8.98	2.00	0.00	1.00	0.00	2.58	8.40	2.00	0.00	1.00	0.00
2.60	7.71	2.00	0.00	1.00	0.00	2.62	7.52	2.00	0.00	1.00	0.00
2.64	7.64	2.00	0.00	1.00	0.00	2.66	7.37	2.00	0.00	1.00	0.00
2.68	7.53	2.00	0.00	1.00	0.00	2.70	7.93	2.00	0.00	1.00	0.00
2.72	7.94	2.00	0.00	1.00	0.00	2.74	8.23	2.00	0.00	1.00	0.00
2.76	8.04	2.00	0.00	1.00	0.00	2.78	8.16	2.00	0.00	1.00	0.00
2.80	8.39	2.00	0.00	1.00	0.00	2.82	8.37	2.00	0.00	1.00	0.00
2.84	8.26	2.00	0.00	1.00	0.00	2.86	8.62	2.00	0.00	1.00	0.00
2.88	8.54	2.00	0.00	1.00	0.00	2.90	8.66	2.00	0.00	1.00	0.00
2.92	9.03	2.00	0.00	1.00	0.00	2.94	12.49	2.00	0.00	1.00	0.00
2.96	11.45	2.00	0.00	1.00	0.00	2.98	11.22	2.00	0.00	1.00	0.00
3.00	11.21	2.00	0.00	1.00	0.00	3.02	11.12	2.00	0.00	1.00	0.00
3.04	11.37	2.00	0.00	1.00	0.00	3.06	11.62	2.00	0.00	1.00	0.00
3.08	12.20	2.00	0.00	1.00	0.00	3.10	11.78	2.00	0.00	1.00	0.00
3.12	11.34	2.00	0.00	1.00	0.00	3.14	10.95	2.00	0.00	1.00	0.00
3.16	10.60	2.00	0.00	1.00	0.00	3.18	11.05	2.00	0.00	1.00	0.00
3.20	11.26	2.00	0.00	1.00	0.00	3.22	11.70	2.00	0.00	1.00	0.00
3.24	11.26	2.00	0.00	1.00	0.00	3.26	11.57	2.00	0.00	1.00	0.00
3.28	11.52	2.00	0.00	1.00	0.00	3.30	11.72	2.00	0.00	1.00	0.00
3.32	11.38	2.00	0.00	1.00	0.00	3.34	10.90	2.00	0.00	1.00	0.00
3.36	11.05	2.00	0.00	1.00	0.00	3.38	11.36	2.00	0.00	1.00	0.00
3.40	11.83	2.00	0.00	1.00	0.00	3.42	13.01	2.00	0.00	1.00	0.00
3.44	14.76	2.00	0.00	1.00	0.00	3.46	16.16	2.00	0.00	1.00	0.00
3.48	14.80	2.00	0.00	1.00	0.00	3.50	12.89	2.00	0.00	1.00	0.00
3.52	12.83	2.00	0.00	1.00	0.00	3.54	13.16	2.00	0.00	1.00	0.00
3.56	14.21	2.00	0.00	1.00	0.00	3.58	14.44	2.00	0.00	1.00	0.00
3.60	13.59	2.00	0.00	1.00	0.00	3.62	12.43	2.00	0.00	1.00	0.00
3.64	13.56	2.00	0.00	1.00	0.00	3.66	16.49	2.00	0.00	1.00	0.00
3.68	18.99	2.00	0.00	1.00	0.00	3.70	22.62	2.00	0.00	1.00	0.00
3.72	83.66	2.00	0.00	1.00	0.00	3.74	85.44	2.00	0.00	1.00	0.00
3.76	87.95	2.00	0.00	1.00	0.00	3.78	90.18	2.00	0.00	1.00	0.00
3.80	92.05	2.00	0.00	1.00	0.00	3.82	95.22	2.00	0.00	1.00	0.00
3.84	98.16	2.00	0.00	1.00	0.00	3.86	91.47	2.00	0.00	1.00	0.00
3.88	83.08	2.00	0.00	1.00	0.00	3.90	80.93	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.92	18.32	2.00	0.00	1.00	0.00	3.94	20.86	2.00	0.00	1.00	0.00
3.96	18.57	2.00	0.00	1.00	0.00	3.98	17.50	2.00	0.00	1.00	0.00
4.00	16.23	2.00	0.00	1.00	0.00	4.02	15.59	2.00	0.00	1.00	0.00
4.04	14.93	2.00	0.00	1.00	0.00	4.06	14.14	2.00	0.00	1.00	0.00
4.09	13.16	2.00	0.00	1.00	0.00	4.10	12.73	2.00	0.00	1.00	0.00
4.12	13.01	2.00	0.00	1.00	0.00	4.14	13.17	2.00	0.00	1.00	0.00
4.16	13.36	2.00	0.00	1.00	0.00	4.18	13.31	2.00	0.00	1.00	0.00
4.20	12.74	2.00	0.00	1.00	0.00	4.22	11.90	2.00	0.00	1.00	0.00
4.24	10.97	2.00	0.00	1.00	0.00	4.26	9.83	2.00	0.00	1.00	0.00
4.28	8.96	2.00	0.00	1.00	0.00	4.30	8.06	2.00	0.00	1.00	0.00
4.32	7.56	2.00	0.00	1.00	0.00	4.34	8.03	2.00	0.00	1.00	0.00
4.36	10.17	2.00	0.00	1.00	0.00	4.38	14.39	2.00	0.00	1.00	0.00
4.40	19.29	2.00	0.00	1.00	0.00	4.42	22.98	2.00	0.00	1.00	0.00
4.44	83.21	0.72	3.86	1.00	0.08	4.46	81.80	0.71	3.92	1.00	0.08
4.48	78.98	0.69	4.06	1.00	0.08	4.50	76.33	0.67	4.19	1.00	0.08
4.52	75.40	0.66	4.24	1.00	0.08	4.54	18.20	2.00	0.00	1.00	0.00
4.56	18.54	2.00	0.00	1.00	0.00	4.58	19.14	2.00	0.00	1.00	0.00
4.60	19.64	2.00	0.00	1.00	0.00	4.62	21.40	2.00	0.00	1.00	0.00
4.64	22.85	2.00	0.00	1.00	0.00	4.66	21.73	2.00	0.00	1.00	0.00
4.68	18.42	2.00	0.00	1.00	0.00	4.70	16.28	2.00	0.00	1.00	0.00
4.72	16.73	2.00	0.00	1.00	0.00	4.74	18.84	2.00	0.00	1.00	0.00
4.76	18.99	2.00	0.00	1.00	0.00	4.78	18.47	2.00	0.00	1.00	0.00
4.80	18.24	2.00	0.00	1.00	0.00	4.82	17.61	2.00	0.00	1.00	0.00
4.84	16.89	2.00	0.00	1.00	0.00	4.86	16.69	2.00	0.00	1.00	0.00
4.88	15.49	2.00	0.00	1.00	0.00	4.90	14.12	2.00	0.00	1.00	0.00
4.92	13.80	2.00	0.00	1.00	0.00	4.94	12.27	2.00	0.00	1.00	0.00
4.96	10.78	2.00	0.00	1.00	0.00	4.98	9.58	2.00	0.00	1.00	0.00
5.00	8.93	2.00	0.00	1.00	0.00	5.02	9.41	2.00	0.00	1.00	0.00
5.04	11.99	2.00	0.00	1.00	0.00	5.06	13.95	2.00	0.00	1.00	0.00
5.08	14.50	2.00	0.00	1.00	0.00	5.10	15.33	2.00	0.00	1.00	0.00
5.12	15.17	2.00	0.00	1.00	0.00	5.14	13.07	2.00	0.00	1.00	0.00
5.16	10.18	2.00	0.00	1.00	0.00	5.18	8.82	2.00	0.00	1.00	0.00
5.20	7.23	2.00	0.00	1.00	0.00	5.22	7.02	2.00	0.00	1.00	0.00
5.24	6.87	2.00	0.00	1.00	0.00	5.26	6.95	2.00	0.00	1.00	0.00
5.28	7.00	2.00	0.00	1.00	0.00	5.30	7.22	2.00	0.00	1.00	0.00
5.32	7.50	2.00	0.00	1.00	0.00	5.34	8.01	2.00	0.00	1.00	0.00
5.36	8.65	2.00	0.00	1.00	0.00	5.38	9.04	2.00	0.00	1.00	0.00
5.40	8.55	2.00	0.00	1.00	0.00	5.42	7.84	2.00	0.00	1.00	0.00
5.44	7.60	2.00	0.00	1.00	0.00	5.46	8.19	2.00	0.00	1.00	0.00
5.48	9.43	2.00	0.00	1.00	0.00	5.50	9.42	2.00	0.00	1.00	0.00
5.52	7.27	2.00	0.00	1.00	0.00	5.54	6.67	2.00	0.00	1.00	0.00
5.56	7.38	2.00	0.00	1.00	0.00	5.59	7.34	2.00	0.00	1.00	0.00
5.60	6.66	2.00	0.00	1.00	0.00	5.62	6.97	2.00	0.00	1.00	0.00
5.64	8.37	2.00	0.00	1.00	0.00	5.66	9.23	2.00	0.00	1.00	0.00
5.68	9.30	2.00	0.00	1.00	0.00	5.70	8.85	2.00	0.00	1.00	0.00
5.72	8.12	2.00	0.00	1.00	0.00	5.74	8.06	2.00	0.00	1.00	0.00
5.76	8.17	2.00	0.00	1.00	0.00	5.78	8.58	2.00	0.00	1.00	0.00
5.80	8.88	2.00	0.00	1.00	0.00	5.82	9.26	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.84	9.42	2.00	0.00	1.00	0.00	5.86	9.74	2.00	0.00	1.00	0.00
5.88	9.90	2.00	0.00	1.00	0.00	5.90	12.14	2.00	0.00	1.00	0.00
5.92	11.82	2.00	0.00	1.00	0.00	5.94	10.88	2.00	0.00	1.00	0.00
5.96	10.08	2.00	0.00	1.00	0.00	5.98	9.68	2.00	0.00	1.00	0.00
6.00	9.83	2.00	0.00	1.00	0.00	6.02	9.14	2.00	0.00	1.00	0.00
6.04	8.99	2.00	0.00	1.00	0.00	6.06	9.96	2.00	0.00	1.00	0.00
6.08	10.60	2.00	0.00	1.00	0.00	6.10	11.03	2.00	0.00	1.00	0.00
6.12	11.20	2.00	0.00	1.00	0.00	6.14	10.59	2.00	0.00	1.00	0.00
6.16	9.96	2.00	0.00	1.00	0.00	6.18	8.46	2.00	0.00	1.00	0.00
6.20	8.21	2.00	0.00	1.00	0.00	6.22	8.31	2.00	0.00	1.00	0.00
6.24	8.40	2.00	0.00	1.00	0.00	6.26	7.88	2.00	0.00	1.00	0.00
6.28	7.82	2.00	0.00	1.00	0.00	6.30	8.21	2.00	0.00	1.00	0.00
6.32	8.55	2.00	0.00	1.00	0.00	6.34	8.30	2.00	0.00	1.00	0.00
6.36	8.11	2.00	0.00	1.00	0.00	6.38	7.61	2.00	0.00	1.00	0.00
6.40	7.36	2.00	0.00	1.00	0.00	6.42	7.28	2.00	0.00	1.00	0.00
6.44	7.27	2.00	0.00	1.00	0.00	6.46	7.88	2.00	0.00	1.00	0.00
6.48	8.49	2.00	0.00	1.00	0.00	6.50	9.21	2.00	0.00	1.00	0.00
6.52	9.44	2.00	0.00	1.00	0.00	6.54	9.48	2.00	0.00	1.00	0.00
6.56	9.47	2.00	0.00	1.00	0.00	6.58	9.01	2.00	0.00	1.00	0.00
6.60	8.63	2.00	0.00	1.00	0.00	6.62	8.39	2.00	0.00	1.00	0.00
6.64	7.82	2.00	0.00	1.00	0.00	6.66	7.61	2.00	0.00	1.00	0.00
6.68	7.71	2.00	0.00	1.00	0.00	6.70	7.22	2.00	0.00	1.00	0.00
6.72	6.95	2.00	0.00	1.00	0.00	6.74	7.05	2.00	0.00	1.00	0.00
6.76	7.10	2.00	0.00	1.00	0.00	6.78	7.09	2.00	0.00	1.00	0.00
6.80	7.09	2.00	0.00	1.00	0.00	6.82	6.69	2.00	0.00	1.00	0.00
6.84	6.42	2.00	0.00	1.00	0.00	6.86	6.36	2.00	0.00	1.00	0.00
6.88	6.20	2.00	0.00	1.00	0.00	6.90	7.08	2.00	0.00	1.00	0.00
6.92	7.18	2.00	0.00	1.00	0.00	6.94	7.10	2.00	0.00	1.00	0.00
6.96	6.96	2.00	0.00	1.00	0.00	6.98	6.80	2.00	0.00	1.00	0.00
7.00	6.48	2.00	0.00	1.00	0.00	7.02	6.50	2.00	0.00	1.00	0.00
7.04	6.75	2.00	0.00	1.00	0.00	7.06	6.75	2.00	0.00	1.00	0.00
7.08	6.79	2.00	0.00	1.00	0.00	7.10	6.71	2.00	0.00	1.00	0.00
7.12	6.94	2.00	0.00	1.00	0.00	7.14	7.48	2.00	0.00	1.00	0.00
7.16	8.22	2.00	0.00	1.00	0.00	7.18	8.78	2.00	0.00	1.00	0.00
7.20	9.81	2.00	0.00	1.00	0.00	7.22	10.47	2.00	0.00	1.00	0.00
7.24	10.85	2.00	0.00	1.00	0.00	7.26	10.86	2.00	0.00	1.00	0.00
7.28	10.95	2.00	0.00	1.00	0.00	7.30	10.95	2.00	0.00	1.00	0.00
7.32	10.98	2.00	0.00	1.00	0.00	7.34	11.00	2.00	0.00	1.00	0.00
7.36	10.86	2.00	0.00	1.00	0.00	7.38	10.79	2.00	0.00	1.00	0.00
7.41	10.52	2.00	0.00	1.00	0.00	7.42	10.26	2.00	0.00	1.00	0.00
7.44	10.09	2.00	0.00	1.00	0.00	7.46	9.49	2.00	0.00	1.00	0.00
7.48	9.20	2.00	0.00	1.00	0.00	7.50	8.96	2.00	0.00	1.00	0.00
7.52	9.12	2.00	0.00	1.00	0.00	7.54	9.36	2.00	0.00	1.00	0.00
7.56	9.65	2.00	0.00	1.00	0.00	7.58	10.24	2.00	0.00	1.00	0.00
7.60	10.60	2.00	0.00	1.00	0.00	7.62	10.79	2.00	0.00	1.00	0.00
7.64	10.98	2.00	0.00	1.00	0.00	7.66	10.83	2.00	0.00	1.00	0.00
7.68	10.57	2.00	0.00	1.00	0.00	7.70	10.16	2.00	0.00	1.00	0.00
7.72	9.82	2.00	0.00	1.00	0.00	7.74	9.53	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.76	8.94	2.00	0.00	1.00	0.00	7.78	7.96	2.00	0.00	1.00	0.00
7.80	7.05	2.00	0.00	1.00	0.00	7.82	6.28	2.00	0.00	1.00	0.00
7.84	6.08	2.00	0.00	1.00	0.00	7.86	5.95	2.00	0.00	1.00	0.00
7.88	6.12	2.00	0.00	1.00	0.00	7.90	7.33	2.00	0.00	1.00	0.00
7.92	7.01	2.00	0.00	1.00	0.00	7.94	6.50	2.00	0.00	1.00	0.00
7.96	5.87	2.00	0.00	1.00	0.00	7.98	5.47	2.00	0.00	1.00	0.00
8.00	4.79	2.00	0.00	1.00	0.00	8.02	4.49	2.00	0.00	1.00	0.00
8.04	4.32	2.00	0.00	1.00	0.00	8.06	4.51	2.00	0.00	1.00	0.00
8.08	4.71	2.00	0.00	1.00	0.00	8.10	4.83	2.00	0.00	1.00	0.00
8.12	4.88	2.00	0.00	1.00	0.00	8.14	4.90	2.00	0.00	1.00	0.00
8.16	5.00	2.00	0.00	1.00	0.00	8.18	5.20	2.00	0.00	1.00	0.00
8.20	5.34	2.00	0.00	1.00	0.00	8.22	5.47	2.00	0.00	1.00	0.00
8.24	5.69	2.00	0.00	1.00	0.00	8.26	5.91	2.00	0.00	1.00	0.00
8.28	6.13	2.00	0.00	1.00	0.00	8.30	5.93	2.00	0.00	1.00	0.00
8.32	5.70	2.00	0.00	1.00	0.00	8.34	5.70	2.00	0.00	1.00	0.00
8.36	5.80	2.00	0.00	1.00	0.00	8.38	6.17	2.00	0.00	1.00	0.00
8.40	6.43	2.00	0.00	1.00	0.00	8.42	6.82	2.00	0.00	1.00	0.00
8.44	7.50	2.00	0.00	1.00	0.00	8.46	7.52	2.00	0.00	1.00	0.00
8.48	7.15	2.00	0.00	1.00	0.00	8.50	6.42	2.00	0.00	1.00	0.00
8.52	6.34	2.00	0.00	1.00	0.00	8.54	6.92	2.00	0.00	1.00	0.00
8.56	7.14	2.00	0.00	1.00	0.00	8.58	6.94	2.00	0.00	1.00	0.00
8.60	6.70	2.00	0.00	1.00	0.00	8.62	6.62	2.00	0.00	1.00	0.00
8.64	6.44	2.00	0.00	1.00	0.00	8.66	6.39	2.00	0.00	1.00	0.00
8.68	6.85	2.00	0.00	1.00	0.00	8.70	7.11	2.00	0.00	1.00	0.00
8.72	7.27	2.00	0.00	1.00	0.00	8.74	7.56	2.00	0.00	1.00	0.00
8.76	7.55	2.00	0.00	1.00	0.00	8.78	7.62	2.00	0.00	1.00	0.00
8.80	8.05	2.00	0.00	1.00	0.00	8.82	8.47	2.00	0.00	1.00	0.00
8.84	8.83	2.00	0.00	1.00	0.00	8.86	9.25	2.00	0.00	1.00	0.00
8.88	10.28	2.00	0.00	1.00	0.00	8.90	10.49	2.00	0.00	1.00	0.00
8.92	10.20	2.00	0.00	1.00	0.00	8.94	9.97	2.00	0.00	1.00	0.00
8.96	9.72	2.00	0.00	1.00	0.00	8.98	9.14	2.00	0.00	1.00	0.00
9.00	9.09	2.00	0.00	1.00	0.00	9.02	9.01	2.00	0.00	1.00	0.00
9.04	8.92	2.00	0.00	1.00	0.00	9.06	8.72	2.00	0.00	1.00	0.00
9.08	8.48	2.00	0.00	1.00	0.00	9.10	8.16	2.00	0.00	1.00	0.00
9.12	7.74	2.00	0.00	1.00	0.00	9.14	7.10	2.00	0.00	1.00	0.00
9.16	6.57	2.00	0.00	1.00	0.00	9.18	6.18	2.00	0.00	1.00	0.00
9.20	5.91	2.00	0.00	1.00	0.00	9.22	5.73	2.00	0.00	1.00	0.00
9.24	6.32	2.00	0.00	1.00	0.00	9.26	6.59	2.00	0.00	1.00	0.00
9.28	6.70	2.00	0.00	1.00	0.00	9.30	6.13	2.00	0.00	1.00	0.00
9.32	5.73	2.00	0.00	1.00	0.00	9.34	6.00	2.00	0.00	1.00	0.00
9.36	6.26	2.00	0.00	1.00	0.00	9.38	6.58	2.00	0.00	1.00	0.00
9.40	7.16	2.00	0.00	1.00	0.00	9.42	8.65	2.00	0.00	1.00	0.00
9.44	8.88	2.00	0.00	1.00	0.00	9.46	7.84	2.00	0.00	1.00	0.00
9.48	6.81	2.00	0.00	1.00	0.00	9.50	6.15	2.00	0.00	1.00	0.00
9.52	6.45	2.00	0.00	1.00	0.00	9.54	6.73	2.00	0.00	1.00	0.00
9.56	7.16	2.00	0.00	1.00	0.00	9.58	9.21	2.00	0.00	1.00	0.00
9.60	11.64	2.00	0.00	1.00	0.00	9.62	13.61	2.00	0.00	1.00	0.00
9.64	15.80	2.00	0.00	1.00	0.00	9.66	18.28	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.68	19.67	2.00	0.00	1.00	0.00	9.70	17.60	2.00	0.00	1.00	0.00
9.72	12.88	2.00	0.00	1.00	0.00	9.74	9.71	2.00	0.00	1.00	0.00
9.76	6.93	2.00	0.00	1.00	0.00	9.78	7.64	2.00	0.00	1.00	0.00
9.80	7.87	2.00	0.00	1.00	0.00	9.82	7.42	2.00	0.00	1.00	0.00
9.84	7.44	2.00	0.00	1.00	0.00	9.86	9.41	2.00	0.00	1.00	0.00
9.88	8.16	2.00	0.00	1.00	0.00	9.90	7.08	2.00	0.00	1.00	0.00
9.92	6.64	2.00	0.00	1.00	0.00	9.94	6.77	2.00	0.00	1.00	0.00
9.96	6.69	2.00	0.00	1.00	0.00	9.98	6.43	2.00	0.00	1.00	0.00
10.00	6.08	2.00	0.00	1.00	0.00	10.02	6.08	2.00	0.00	1.00	0.00
10.04	5.98	2.00	0.00	1.00	0.00	10.06	6.09	2.00	0.00	1.00	0.00
10.08	6.29	2.00	0.00	1.00	0.00	10.10	6.54	2.00	0.00	1.00	0.00
10.12	6.67	2.00	0.00	1.00	0.00	10.14	6.73	2.00	0.00	1.00	0.00
10.16	6.68	2.00	0.00	1.00	0.00	10.18	6.56	2.00	0.00	1.00	0.00
10.20	6.60	2.00	0.00	1.00	0.00	10.22	6.58	2.00	0.00	1.00	0.00
10.24	6.55	2.00	0.00	1.00	0.00	10.26	6.66	2.00	0.00	1.00	0.00
10.28	6.61	2.00	0.00	1.00	0.00	10.30	6.51	2.00	0.00	1.00	0.00
10.32	6.46	2.00	0.00	1.00	0.00	10.34	6.48	2.00	0.00	1.00	0.00
10.36	6.50	2.00	0.00	1.00	0.00	10.38	6.45	2.00	0.00	1.00	0.00
10.40	6.38	2.00	0.00	1.00	0.00	10.42	6.33	2.00	0.00	1.00	0.00
10.44	6.75	2.00	0.00	1.00	0.00	10.46	6.70	2.00	0.00	1.00	0.00
10.48	6.79	2.00	0.00	1.00	0.00	10.50	6.60	2.00	0.00	1.00	0.00
10.52	6.49	2.00	0.00	1.00	0.00	10.54	6.35	2.00	0.00	1.00	0.00
10.56	6.10	2.00	0.00	1.00	0.00	10.58	6.27	2.00	0.00	1.00	0.00
10.60	6.89	2.00	0.00	1.00	0.00	10.62	9.53	2.00	0.00	1.00	0.00
10.64	9.34	2.00	0.00	1.00	0.00	10.66	8.73	2.00	0.00	1.00	0.00
10.68	8.30	2.00	0.00	1.00	0.00	10.70	7.38	2.00	0.00	1.00	0.00
10.72	6.97	2.00	0.00	1.00	0.00	10.74	5.90	2.00	0.00	1.00	0.00
10.76	5.87	2.00	0.00	1.00	0.00	10.78	6.02	2.00	0.00	1.00	0.00
10.80	6.13	2.00	0.00	1.00	0.00	10.82	6.10	2.00	0.00	1.00	0.00
10.84	5.99	2.00	0.00	1.00	0.00	10.86	7.84	2.00	0.00	1.00	0.00
10.88	6.75	2.00	0.00	1.00	0.00	10.90	6.06	2.00	0.00	1.00	0.00
10.92	5.66	2.00	0.00	1.00	0.00	10.94	5.59	2.00	0.00	1.00	0.00
10.96	5.72	2.00	0.00	1.00	0.00	10.98	5.58	2.00	0.00	1.00	0.00
11.00	5.71	2.00	0.00	1.00	0.00	11.02	5.97	2.00	0.00	1.00	0.00
11.04	5.90	2.00	0.00	1.00	0.00	11.06	5.85	2.00	0.00	1.00	0.00
11.08	5.82	2.00	0.00	1.00	0.00	11.10	5.86	2.00	0.00	1.00	0.00
11.12	6.32	2.00	0.00	1.00	0.00	11.14	7.13	2.00	0.00	1.00	0.00
11.16	7.89	2.00	0.00	1.00	0.00	11.18	8.19	2.00	0.00	1.00	0.00
11.20	8.12	2.00	0.00	1.00	0.00	11.22	8.18	2.00	0.00	1.00	0.00
11.24	10.10	2.00	0.00	1.00	0.00	11.26	12.91	2.00	0.00	1.00	0.00
11.28	14.17	2.00	0.00	1.00	0.00	11.30	15.43	2.00	0.00	1.00	0.00
11.32	16.53	2.00	0.00	1.00	0.00	11.34	16.01	2.00	0.00	1.00	0.00
11.36	15.13	2.00	0.00	1.00	0.00	11.38	14.11	2.00	0.00	1.00	0.00
11.40	13.01	2.00	0.00	1.00	0.00	11.42	12.43	2.00	0.00	1.00	0.00
11.44	12.18	2.00	0.00	1.00	0.00	11.46	12.38	2.00	0.00	1.00	0.00
11.48	12.74	2.00	0.00	1.00	0.00	11.50	13.47	2.00	0.00	1.00	0.00
11.52	14.95	2.00	0.00	1.00	0.00	11.54	16.51	2.00	0.00	1.00	0.00
11.56	17.97	2.00	0.00	1.00	0.00	11.58	18.25	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.60	17.95	2.00	0.00	1.00	0.00	11.62	19.35	2.00	0.00	1.00	0.00
11.64	21.75	2.00	0.00	1.00	0.00	11.66	22.89	2.00	0.00	1.00	0.00
11.68	24.49	2.00	0.00	1.00	0.00	11.70	24.63	2.00	0.00	1.00	0.00
11.72	23.90	2.00	0.00	1.00	0.00	11.74	22.56	2.00	0.00	1.00	0.00
11.76	20.76	2.00	0.00	1.00	0.00	11.78	18.88	2.00	0.00	1.00	0.00
11.80	16.29	2.00	0.00	1.00	0.00	11.82	12.82	2.00	0.00	1.00	0.00
11.84	11.46	2.00	0.00	1.00	0.00	11.86	9.45	2.00	0.00	1.00	0.00
11.88	7.82	2.00	0.00	1.00	0.00	11.90	7.45	2.00	0.00	1.00	0.00
11.93	6.85	2.00	0.00	1.00	0.00	11.94	6.42	2.00	0.00	1.00	0.00
11.96	6.90	2.00	0.00	1.00	0.00	11.98	8.17	2.00	0.00	1.00	0.00
12.00	8.78	2.00	0.00	1.00	0.00	12.02	9.00	2.00	0.00	1.00	0.00
12.04	8.28	2.00	0.00	1.00	0.00	12.06	7.82	2.00	0.00	1.00	0.00
12.08	7.80	2.00	0.00	1.00	0.00	12.10	7.18	2.00	0.00	1.00	0.00
12.12	7.05	2.00	0.00	1.00	0.00	12.14	7.06	2.00	0.00	1.00	0.00
12.16	7.01	2.00	0.00	1.00	0.00	12.18	7.05	2.00	0.00	1.00	0.00
12.20	7.30	2.00	0.00	1.00	0.00	12.22	7.38	2.00	0.00	1.00	0.00
12.24	7.44	2.00	0.00	1.00	0.00	12.26	7.45	2.00	0.00	1.00	0.00
12.28	7.55	2.00	0.00	1.00	0.00	12.30	7.49	2.00	0.00	1.00	0.00
12.32	7.36	2.00	0.00	1.00	0.00	12.34	7.23	2.00	0.00	1.00	0.00
12.36	7.58	2.00	0.00	1.00	0.00	12.38	7.66	2.00	0.00	1.00	0.00
12.40	7.49	2.00	0.00	1.00	0.00	12.42	7.40	2.00	0.00	1.00	0.00
12.44	7.23	2.00	0.00	1.00	0.00	12.46	7.41	2.00	0.00	1.00	0.00
12.48	7.72	2.00	0.00	1.00	0.00	12.50	7.99	2.00	0.00	1.00	0.00
12.52	8.13	2.00	0.00	1.00	0.00	12.54	8.21	2.00	0.00	1.00	0.00
12.56	8.31	2.00	0.00	1.00	0.00	12.58	8.39	2.00	0.00	1.00	0.00
12.60	8.34	2.00	0.00	1.00	0.00	12.62	8.11	2.00	0.00	1.00	0.00
12.64	8.17	2.00	0.00	1.00	0.00	12.66	8.24	2.00	0.00	1.00	0.00
12.68	8.49	2.00	0.00	1.00	0.00	12.70	8.83	2.00	0.00	1.00	0.00
12.72	8.93	2.00	0.00	1.00	0.00	12.74	9.07	2.00	0.00	1.00	0.00
12.76	8.87	2.00	0.00	1.00	0.00	12.78	8.70	2.00	0.00	1.00	0.00
12.80	8.53	2.00	0.00	1.00	0.00	12.82	8.62	2.00	0.00	1.00	0.00
12.84	8.94	2.00	0.00	1.00	0.00	12.86	9.02	2.00	0.00	1.00	0.00
12.89	9.23	2.00	0.00	1.00	0.00	12.90	9.44	2.00	0.00	1.00	0.00
12.92	9.63	2.00	0.00	1.00	0.00	12.95	9.81	2.00	0.00	1.00	0.00
12.96	9.82	2.00	0.00	1.00	0.00	12.98	9.65	2.00	0.00	1.00	0.00
13.00	9.46	2.00	0.00	1.00	0.00	13.02	9.47	2.00	0.00	1.00	0.00
13.04	9.48	2.00	0.00	1.00	0.00	13.06	9.18	2.00	0.00	1.00	0.00
13.08	9.25	2.00	0.00	1.00	0.00	13.10	9.08	2.00	0.00	1.00	0.00
13.12	8.83	2.00	0.00	1.00	0.00	13.14	8.55	2.00	0.00	1.00	0.00
13.16	8.09	2.00	0.00	1.00	0.00	13.18	7.72	2.00	0.00	1.00	0.00
13.20	7.38	2.00	0.00	1.00	0.00	13.22	7.31	2.00	0.00	1.00	0.00
13.24	7.18	2.00	0.00	1.00	0.00	13.26	7.09	2.00	0.00	1.00	0.00
13.28	6.84	2.00	0.00	1.00	0.00	13.30	6.61	2.00	0.00	1.00	0.00
13.32	6.46	2.00	0.00	1.00	0.00	13.34	6.50	2.00	0.00	1.00	0.00
13.36	6.59	2.00	0.00	1.00	0.00	13.38	6.40	2.00	0.00	1.00	0.00
13.40	6.14	2.00	0.00	1.00	0.00	13.42	5.89	2.00	0.00	1.00	0.00
13.44	5.70	2.00	0.00	1.00	0.00	13.46	5.60	2.00	0.00	1.00	0.00
13.48	5.62	2.00	0.00	1.00	0.00	13.50	5.59	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.52	5.65	2.00	0.00	1.00	0.00	13.54	5.63	2.00	0.00	1.00	0.00
13.56	5.62	2.00	0.00	1.00	0.00	13.58	5.86	2.00	0.00	1.00	0.00
13.60	6.06	2.00	0.00	1.00	0.00	13.62	6.32	2.00	0.00	1.00	0.00
13.64	6.34	2.00	0.00	1.00	0.00	13.66	6.18	2.00	0.00	1.00	0.00
13.68	6.01	2.00	0.00	1.00	0.00	13.70	5.83	2.00	0.00	1.00	0.00
13.72	5.83	2.00	0.00	1.00	0.00	13.74	5.87	2.00	0.00	1.00	0.00
13.76	5.91	2.00	0.00	1.00	0.00	13.78	5.93	2.00	0.00	1.00	0.00
13.80	6.06	2.00	0.00	1.00	0.00	13.82	6.20	2.00	0.00	1.00	0.00
13.84	6.55	2.00	0.00	1.00	0.00	13.86	6.39	2.00	0.00	1.00	0.00
13.88	5.99	2.00	0.00	1.00	0.00	13.90	5.77	2.00	0.00	1.00	0.00
13.92	6.04	2.00	0.00	1.00	0.00	13.94	6.67	2.00	0.00	1.00	0.00
13.96	6.89	2.00	0.00	1.00	0.00	13.98	6.53	2.00	0.00	1.00	0.00
14.00	5.49	2.00	0.00	1.00	0.00	14.02	5.37	2.00	0.00	1.00	0.00
14.04	5.31	2.00	0.00	1.00	0.00	14.06	5.21	2.00	0.00	1.00	0.00
14.08	5.05	2.00	0.00	1.00	0.00	14.10	5.06	2.00	0.00	1.00	0.00
14.12	5.34	2.00	0.00	1.00	0.00	14.14	5.47	2.00	0.00	1.00	0.00
14.16	5.53	2.00	0.00	1.00	0.00	14.18	5.46	2.00	0.00	1.00	0.00
14.20	5.46	2.00	0.00	1.00	0.00	14.22	5.81	2.00	0.00	1.00	0.00
14.24	6.46	2.00	0.00	1.00	0.00	14.26	6.49	2.00	0.00	1.00	0.00
14.28	6.06	2.00	0.00	1.00	0.00	14.30	5.64	2.00	0.00	1.00	0.00
14.32	5.60	2.00	0.00	1.00	0.00	14.34	6.32	2.00	0.00	1.00	0.00
14.36	7.79	2.00	0.00	1.00	0.00	14.38	8.95	2.00	0.00	1.00	0.00
14.40	9.39	2.00	0.00	1.00	0.00	14.42	7.27	2.00	0.00	1.00	0.00
14.44	6.48	2.00	0.00	1.00	0.00	14.46	6.83	2.00	0.00	1.00	0.00
14.48	6.93	2.00	0.00	1.00	0.00	14.50	7.57	2.00	0.00	1.00	0.00
14.52	9.32	2.00	0.00	1.00	0.00	14.54	11.26	2.00	0.00	1.00	0.00
14.56	12.57	2.00	0.00	1.00	0.00	14.58	12.17	2.00	0.00	1.00	0.00
14.60	11.50	2.00	0.00	1.00	0.00	14.62	10.04	2.00	0.00	1.00	0.00
14.64	8.51	2.00	0.00	1.00	0.00	14.66	7.74	2.00	0.00	1.00	0.00
14.68	7.45	2.00	0.00	1.00	0.00	14.70	8.41	2.00	0.00	1.00	0.00
14.72	10.24	2.00	0.00	1.00	0.00	14.74	11.99	2.00	0.00	1.00	0.00
14.76	11.94	2.00	0.00	1.00	0.00	14.78	12.23	2.00	0.00	1.00	0.00
14.80	10.75	2.00	0.00	1.00	0.00	14.82	12.07	2.00	0.00	1.00	0.00
14.84	11.05	2.00	0.00	1.00	0.00	14.87	11.62	2.00	0.00	1.00	0.00
14.88	10.84	2.00	0.00	1.00	0.00	14.91	9.99	2.00	0.00	1.00	0.00
14.92	8.98	2.00	0.00	1.00	0.00	14.94	9.15	2.00	0.00	1.00	0.00
14.96	8.08	2.00	0.00	1.00	0.00	14.98	5.95	2.00	0.00	1.00	0.00
15.00	5.58	2.00	0.00	1.00	0.00	15.02	6.23	2.00	0.00	1.00	0.00
15.04	7.80	2.00	0.00	1.00	0.00	15.06	10.51	2.00	0.00	1.00	0.00
15.08	13.11	2.00	0.00	1.00	0.00	15.10	15.64	2.00	0.00	1.00	0.00
15.12	17.81	2.00	0.00	1.00	0.00	15.14	17.89	2.00	0.00	1.00	0.00
15.16	14.72	2.00	0.00	1.00	0.00	15.18	11.93	2.00	0.00	1.00	0.00
15.20	9.74	2.00	0.00	1.00	0.00	15.22	7.73	2.00	0.00	1.00	0.00
15.24	7.15	2.00	0.00	1.00	0.00	15.26	7.07	2.00	0.00	1.00	0.00
15.28	7.40	2.00	0.00	1.00	0.00	15.30	9.86	2.00	0.00	1.00	0.00
15.32	13.08	2.00	0.00	1.00	0.00	15.34	15.97	2.00	0.00	1.00	0.00
15.36	17.21	2.00	0.00	1.00	0.00	15.38	18.26	2.00	0.00	1.00	0.00
15.40	17.25	2.00	0.00	1.00	0.00	15.42	13.89	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.44	11.12	2.00	0.00	1.00	0.00	15.46	9.49	2.00	0.00	1.00	0.00
15.48	10.51	2.00	0.00	1.00	0.00	15.50	13.16	2.00	0.00	1.00	0.00
15.52	15.53	2.00	0.00	1.00	0.00	15.54	16.11	2.00	0.00	1.00	0.00
15.56	15.24	2.00	0.00	1.00	0.00	15.58	14.77	2.00	0.00	1.00	0.00
15.60	15.02	2.00	0.00	1.00	0.00	15.62	13.82	2.00	0.00	1.00	0.00

Total estimated settlement: 0.41

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.18	3.00	12.22	36.65	3.39	0.05	45.08
0.04	0.44	7.39	7.76	57.40	3.09	0.06	52.64
0.06	0.51	8.67	7.30	63.26	3.05	0.06	40.11
0.08	0.60	10.12	6.90	69.82	3.01	0.06	34.53
0.10	0.66	11.17	6.72	75.09	3.00	0.06	30.07
0.12	0.71	11.98	6.82	81.77	3.01	0.06	26.58
0.14	1.45	24.66	3.60	88.65	2.64	0.07	46.24
0.16	2.72	46.22	1.94	89.66	2.30	0.11	0.72
0.18	3.55	60.38	1.55	93.34	2.15	0.14	0.76
0.20	3.58	60.79	1.45	87.87	2.09	0.10	0.76
0.22	3.19	54.22	1.42	76.97	2.08	0.09	0.74
0.24	3.24	54.94	1.29	70.98	1.99	0.09	0.75
0.26	3.71	62.93	1.00	62.93	1.88	0.08	0.76
0.28	3.48	59.00	1.23	72.68	1.94	0.11	0.76
0.30	2.98	50.56	1.37	69.49	2.05	0.08	0.74
0.32	2.24	38.01	1.84	70.01	2.27	0.08	0.70
0.34	2.15	36.41	2.05	74.77	2.33	0.09	0.69
0.36	2.20	37.38	2.12	79.27	2.35	0.10	0.70
0.38	1.87	31.66	2.79	88.22	2.50	0.10	0.68
0.40	1.39	23.46	4.59	107.62	2.78	0.08	14.67
0.42	1.02	17.22	7.28	125.38	3.05	0.07	10.22
0.44	0.96	16.12	8.52	137.32	3.15	0.07	9.10
0.46	0.95	16.08	8.77	140.93	3.16	0.07	8.65
0.48	0.94	15.87	9.14	145.01	3.19	0.07	8.16
0.50	0.93	15.70	9.50	149.04	3.22	0.07	7.72
0.52	0.91	15.37	10.01	153.81	3.25	0.07	7.25
0.54	0.89	14.95	10.23	152.88	3.27	0.07	6.77
0.56	0.86	14.47	10.37	149.95	3.28	0.07	6.30
0.58	0.83	13.97	10.45	145.95	3.28	0.07	5.87
0.60	0.81	13.53	10.70	144.81	3.30	0.07	5.48
0.62	0.78	13.07	10.93	142.83	3.31	0.06	5.12
0.64	0.76	12.75	11.07	141.14	3.32	0.06	4.83
0.66	0.75	12.53	11.14	139.59	3.33	0.06	4.59
0.68	0.75	12.47	11.09	138.27	3.32	0.06	4.43
0.70	0.76	12.78	10.73	137.15	3.30	0.06	4.41
0.72	0.79	13.15	10.36	136.14	3.28	0.07	4.40
0.74	0.82	13.64	9.93	135.50	3.25	0.07	4.44
0.76	0.83	13.83	9.76	135.09	3.24	0.07	4.38
0.78	0.84	14.02	9.64	135.24	3.23	0.07	4.32
0.80	0.84	14.01	9.69	135.79	3.23	0.07	4.21
0.82	0.84	14.03	9.78	137.22	3.24	0.07	4.11
0.84	0.84	14.08	9.85	138.58	3.24	0.07	4.02
0.86	0.85	14.19	9.82	139.38	3.24	0.07	3.95
0.88	0.86	14.30	9.77	139.72	3.24	0.07	3.89
0.90	0.88	14.77	9.52	140.56	3.22	0.07	3.93
0.92	0.94	15.69	9.05	141.95	3.19	0.07	4.08
0.94	0.86	14.30	9.85	140.78	3.24	0.07	3.64
0.96	0.89	14.90	9.36	139.44	3.21	0.06	3.71

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	0.92	15.36	8.92	136.97	3.18	0.07	3.74
1.00	1.09	18.27	7.40	135.16	3.06	0.07	4.36
1.02	1.12	18.73	7.14	133.77	3.03	0.07	4.38
1.04	1.13	18.83	7.07	133.17	3.03	0.07	4.31
1.06	1.12	18.76	7.10	133.18	3.03	0.07	4.21
1.09	1.15	19.15	7.00	134.00	3.02	0.07	4.18
1.10	1.18	19.76	6.90	136.39	3.01	0.07	4.27
1.12	1.22	20.36	6.88	140.20	3.01	0.07	4.32
1.14	1.23	20.53	7.01	143.99	3.02	0.07	4.28
1.16	1.22	20.46	7.18	146.87	3.04	0.07	4.19
1.18	1.22	20.45	7.28	148.91	3.05	0.07	4.11
1.20	1.22	20.35	7.42	151.03	3.06	0.07	4.02
1.23	1.21	20.23	7.56	152.97	3.07	0.07	3.90
1.24	1.21	20.25	7.61	154.06	3.07	0.07	3.87
1.26	1.24	20.71	7.45	154.30	3.06	0.07	3.89
1.28	1.29	21.60	7.13	153.92	3.03	0.08	3.99
1.30	1.35	22.64	6.78	153.41	3.00	0.08	4.12
1.32	1.42	23.71	6.45	152.90	2.97	0.08	4.24
1.34	1.47	24.67	6.20	152.94	2.95	0.08	4.35
1.36	1.53	25.66	6.01	154.29	2.93	0.08	4.45
1.38	1.57	26.36	5.96	157.05	2.93	0.08	4.50
1.40	1.61	26.98	5.94	160.23	2.92	0.08	4.54
1.42	1.63	27.34	5.95	162.60	2.92	0.08	4.53
1.44	1.64	27.50	5.97	164.28	2.93	0.09	4.49
1.46	1.64	27.42	6.06	166.07	2.94	0.08	4.42
1.48	1.62	27.04	6.21	168.05	2.95	0.08	4.29
1.50	1.59	26.58	6.38	169.46	2.97	0.08	4.16
1.52	1.56	26.13	6.51	170.02	2.98	0.08	4.03
1.54	1.54	25.79	6.62	170.80	2.99	0.08	3.93
1.56	1.53	25.49	6.74	171.88	3.00	0.08	3.83
1.59	1.50	24.93	6.92	172.56	3.02	0.08	3.67
1.60	1.45	24.12	7.13	172.03	3.03	0.08	3.53
1.62	1.39	23.08	7.37	170.10	3.05	0.08	3.33
1.64	1.34	22.35	7.50	167.58	3.06	0.08	3.19
1.66	1.31	21.79	7.55	164.51	3.07	0.08	3.07
1.68	1.29	21.49	7.53	161.79	3.07	0.07	2.99
1.70	1.27	21.05	7.59	159.85	3.07	0.07	2.89
1.72	1.25	20.64	7.68	158.51	3.08	0.07	2.80
1.74	1.21	20.07	7.85	157.47	3.09	0.07	2.69
1.76	1.18	19.56	7.96	155.76	3.10	0.07	2.59
1.78	1.15	19.02	8.10	153.95	3.11	0.07	2.49
1.80	1.12	18.55	8.20	152.06	3.12	0.07	2.40
1.82	1.10	18.07	8.30	149.99	3.13	0.07	2.31
1.84	1.08	17.72	8.33	147.66	3.13	0.07	2.24
1.86	1.08	17.74	8.20	145.55	3.12	0.07	2.22
1.88	1.09	17.93	8.03	143.98	3.11	0.07	2.22
1.90	1.10	18.17	7.89	143.45	3.10	0.07	2.23
1.92	1.09	17.89	8.01	143.18	3.11	0.07	2.17

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	1.02	16.71	8.55	142.91	3.15	0.07	2.01
1.96	0.91	14.85	9.54	141.65	3.22	0.07	1.76
1.99	0.78	12.69	10.90	138.36	3.31	0.06	1.49
2.00	0.68	10.87	12.25	133.12	3.40	0.06	1.27
2.02	0.58	9.28	13.61	126.31	3.47	0.06	1.07
2.04	0.51	8.01	14.81	118.65	3.54	0.06	0.92
2.06	0.46	7.20	15.46	111.29	3.57	0.06	0.81
2.08	0.43	6.73	15.39	103.64	3.57	0.06	0.75
2.10	0.43	6.69	14.38	96.16	3.52	0.06	0.74
2.12	0.45	6.92	12.85	88.96	3.43	0.06	0.76
2.14	0.48	7.56	10.87	82.17	3.31	0.06	0.82
2.16	0.53	8.34	9.03	75.32	3.18	0.06	0.90
2.18	0.58	9.25	7.41	68.53	3.06	0.06	0.99
2.20	0.63	10.12	6.32	63.98	2.96	0.06	1.08
2.22	0.69	11.08	5.66	62.72	2.90	0.07	1.17
2.24	0.76	12.27	5.17	63.47	2.84	0.07	1.28
2.26	0.83	13.47	4.88	65.70	2.81	0.07	1.40
2.28	0.89	14.39	4.84	69.67	2.81	0.07	1.48
2.30	0.90	14.65	5.11	74.84	2.84	0.07	1.50
2.32	0.91	14.80	5.53	81.84	2.88	0.07	1.50
2.34	0.92	14.94	5.89	88.08	2.92	0.07	1.50
2.36	0.93	15.15	6.21	94.12	2.95	0.07	1.51
2.38	0.91	14.80	6.71	99.34	3.00	0.07	1.46
2.40	0.88	14.22	7.32	104.04	3.05	0.07	1.40
2.42	0.83	13.36	8.07	107.78	3.11	0.07	1.30
2.44	0.79	12.70	8.66	110.02	3.16	0.06	1.23
2.46	0.75	12.03	9.34	112.40	3.21	0.06	1.15
2.48	0.71	11.40	10.07	114.85	3.26	0.06	1.08
2.50	0.71	11.26	10.40	117.13	3.28	0.06	1.06
2.52	0.67	10.66	10.98	116.98	3.32	0.06	1.00
2.54	0.64	10.08	11.38	114.76	3.34	0.06	0.94
2.56	0.57	8.99	12.27	110.29	3.40	0.06	0.84
2.58	0.53	8.28	12.73	105.45	3.42	0.06	0.77
2.60	0.50	7.76	12.93	100.36	3.43	0.06	0.72
2.62	0.49	7.50	12.73	95.52	3.42	0.06	0.69
2.64	0.48	7.40	12.30	91.08	3.40	0.06	0.68
2.66	0.48	7.43	11.70	86.93	3.36	0.06	0.68
2.68	0.49	7.57	11.02	83.43	3.32	0.06	0.69
2.70	0.51	7.81	10.26	80.20	3.27	0.06	0.71
2.72	0.53	8.11	9.54	77.33	3.22	0.06	0.74
2.74	0.53	8.19	9.08	74.32	3.19	0.06	0.74
2.76	0.54	8.31	8.57	71.23	3.15	0.06	0.75
2.78	0.54	8.42	8.10	68.25	3.11	0.06	0.76
2.80	0.55	8.59	7.54	64.75	3.07	0.06	0.77
2.82	0.56	8.66	7.23	62.56	3.04	0.06	0.78
2.84	0.57	8.77	7.07	61.98	3.03	0.06	0.79
2.86	0.57	8.85	7.06	62.51	3.03	0.06	0.79
2.88	0.58	9.02	6.99	62.99	3.02	0.06	0.80

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.59	9.18	6.91	63.42	3.01	0.06	0.82
2.92	0.68	10.71	5.96	63.84	2.93	0.06	0.95
2.94	0.75	11.79	5.63	66.41	2.89	0.07	1.04
2.96	0.80	12.65	5.46	69.04	2.88	0.07	1.11
2.98	0.77	12.17	5.93	72.18	2.92	0.07	1.07
3.00	0.76	12.08	6.04	72.97	2.93	0.06	1.06
3.02	0.77	12.16	6.06	73.69	2.94	0.06	1.06
3.04	0.78	12.35	6.03	74.47	2.93	0.06	1.08
3.06	0.81	12.80	5.87	75.13	2.92	0.07	1.11
3.08	0.82	12.99	5.76	74.88	2.91	0.07	1.13
3.10	0.81	12.91	5.72	73.80	2.90	0.07	1.12
3.12	0.79	12.44	5.87	73.02	2.92	0.07	1.07
3.14	0.76	12.00	6.09	73.01	2.94	0.06	1.03
3.16	0.76	11.91	6.18	73.60	2.95	0.06	1.02
3.18	0.77	12.06	6.12	73.83	2.94	0.06	1.03
3.20	0.79	12.51	5.89	73.73	2.92	0.07	1.07
3.22	0.80	12.61	5.84	73.67	2.91	0.07	1.07
3.24	0.81	12.73	5.76	73.34	2.91	0.07	1.08
3.26	0.80	12.66	5.72	72.40	2.90	0.07	1.07
3.28	0.81	12.85	5.58	71.66	2.89	0.07	1.08
3.30	0.81	12.79	5.68	72.71	2.90	0.07	1.08
3.32	0.80	12.58	5.92	74.49	2.92	0.07	1.06
3.34	0.78	12.35	6.04	74.65	2.93	0.06	1.03
3.36	0.79	12.38	5.88	72.83	2.92	0.07	1.03
3.38	0.81	12.78	5.57	71.21	2.89	0.07	1.06
3.40	0.86	13.58	5.21	70.78	2.85	0.07	1.13
3.42	0.94	14.98	4.76	71.31	2.80	0.07	1.24
3.44	1.04	16.74	4.29	71.81	2.74	0.08	1.38
3.46	1.09	17.47	4.22	73.80	2.73	0.08	1.44
3.48	1.05	16.73	4.56	76.23	2.77	0.08	1.38
3.50	0.97	15.41	5.07	78.16	2.83	0.07	1.26
3.52	0.93	14.76	5.36	79.06	2.86	0.07	1.21
3.54	0.96	15.31	5.24	80.30	2.85	0.07	1.25
3.56	1.00	15.96	5.14	82.11	2.84	0.07	1.30
3.58	1.01	16.07	5.21	83.73	2.85	0.07	1.30
3.60	0.96	15.25	5.61	85.57	2.89	0.07	1.23
3.62	0.93	14.80	5.79	85.69	2.91	0.07	1.19
3.64	1.00	15.98	5.35	85.42	2.86	0.07	1.28
3.66	1.16	18.64	4.49	83.65	2.76	0.08	1.49
3.68	1.38	22.34	3.83	85.62	2.68	0.08	1.79
3.70	1.61	26.20	3.40	89.20	2.61	0.09	2.09
3.72	1.83	30.03	3.07	92.35	2.56	0.09	0.67
3.74	2.04	33.44	2.73	91.42	2.49	0.09	0.68
3.76	2.25	36.30	2.44	88.62	2.43	0.09	0.69
3.78	2.47	39.31	2.19	86.25	2.37	0.09	0.70
3.80	2.72	42.68	2.00	85.42	2.32	0.09	0.71
3.82	2.95	45.83	1.86	85.06	2.27	0.09	0.72
3.84	2.93	45.45	1.86	84.67	2.27	0.10	0.72

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	2.59	40.48	2.06	83.32	2.33	0.09	0.71
3.88	2.09	33.29	2.50	83.36	2.44	0.09	0.68
3.90	1.65	26.90	3.27	88.04	2.59	0.09	0.66
3.92	1.51	24.51	3.76	92.26	2.67	0.08	1.89
3.94	1.40	22.70	4.29	97.49	2.74	0.08	1.75
3.96	1.40	22.65	4.44	100.51	2.76	0.08	1.74
3.98	1.30	20.92	4.95	103.63	2.82	0.08	1.60
4.00	1.24	19.85	5.26	104.38	2.85	0.07	1.52
4.02	1.18	18.87	5.51	103.89	2.88	0.07	1.44
4.04	1.13	18.00	5.71	102.82	2.90	0.07	1.37
4.06	1.07	16.98	6.06	102.82	2.94	0.07	1.29
4.09	1.02	16.05	6.37	102.30	2.97	0.07	1.21
4.10	0.99	15.61	6.51	101.62	2.98	0.06	1.18
4.12	0.99	15.64	6.40	100.10	2.97	0.06	1.17
4.14	1.01	15.94	6.15	98.03	2.94	0.07	1.19
4.16	1.02	16.07	6.00	96.41	2.93	0.07	1.20
4.18	1.01	15.89	5.99	95.25	2.93	0.07	1.18
4.20	0.97	15.26	6.21	94.80	2.95	0.07	1.13
4.22	0.91	14.25	6.63	94.46	2.99	0.06	1.06
4.24	0.83	12.90	7.33	94.58	3.05	0.06	0.95
4.26	0.75	11.49	8.26	94.94	3.13	0.06	0.85
4.28	0.67	10.11	9.46	95.65	3.22	0.06	0.74
4.30	0.61	9.09	10.55	95.89	3.29	0.06	0.67
4.32	0.59	8.71	11.03	96.04	3.32	0.06	0.64
4.34	0.64	9.63	10.05	96.77	3.26	0.06	0.70
4.36	0.82	12.58	7.71	97.00	3.08	0.06	0.92
4.38	1.09	17.32	5.46	94.58	2.88	0.07	1.26
4.40	1.41	22.02	4.13	91.05	2.72	0.08	1.65
4.42	1.69	25.94	3.46	89.79	2.62	0.09	1.98
4.44	1.82	27.76	3.21	89.11	2.58	0.09	0.66
4.46	1.80	27.34	3.14	85.75	2.57	0.09	0.66
4.48	1.67	25.20	3.11	78.32	2.56	0.08	0.65
4.50	1.54	23.06	3.05	70.39	2.55	0.08	0.64
4.52	1.44	21.50	3.18	68.44	2.58	0.08	0.63
4.54	1.40	21.02	3.54	74.45	2.63	0.08	1.60
4.56	1.40	21.16	3.90	82.57	2.69	0.08	1.59
4.58	1.44	21.86	4.10	89.54	2.71	0.08	1.63
4.60	1.51	23.05	4.11	94.77	2.72	0.08	1.72
4.62	1.61	24.51	4.00	98.14	2.70	0.08	1.83
4.64	1.67	25.32	3.95	99.91	2.69	0.09	1.90
4.66	1.59	24.19	4.16	100.62	2.72	0.08	1.80
4.68	1.42	21.71	4.71	102.16	2.79	0.08	1.60
4.70	1.30	19.76	5.12	101.22	2.84	0.08	1.44
4.72	1.31	19.84	4.93	97.85	2.82	0.08	1.45
4.74	1.38	20.81	4.61	95.93	2.78	0.08	1.53
4.76	1.43	21.48	4.55	97.74	2.77	0.08	1.58
4.78	1.42	21.31	4.77	101.73	2.80	0.08	1.56
4.80	1.38	20.81	5.01	104.33	2.83	0.08	1.52

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	1.34	20.19	5.17	104.31	2.84	0.08	1.47
4.84	1.30	19.55	5.26	102.76	2.85	0.08	1.42
4.86	1.25	18.70	5.43	101.60	2.87	0.07	1.35
4.88	1.18	17.62	5.74	101.15	2.90	0.07	1.27
4.90	1.10	16.49	6.08	100.22	2.94	0.07	1.18
4.92	1.02	15.11	6.52	98.45	2.98	0.07	1.08
4.94	0.94	13.69	7.01	96.01	3.02	0.06	0.98
4.96	0.83	11.91	7.88	93.89	3.10	0.06	0.85
4.98	0.74	10.51	8.68	91.23	3.16	0.06	0.75
5.00	0.71	9.95	9.05	89.98	3.19	0.06	0.71
5.02	0.77	10.96	8.21	89.98	3.12	0.06	0.78
5.04	0.91	13.06	6.87	89.80	3.01	0.06	0.93
5.06	1.04	15.14	5.94	89.93	2.92	0.07	1.08
5.08	1.13	16.39	5.51	90.28	2.88	0.07	1.18
5.10	1.17	16.84	5.40	90.97	2.87	0.07	1.22
5.12	1.13	16.25	5.50	89.39	2.88	0.07	1.17
5.14	1.00	14.24	6.20	88.22	2.95	0.07	1.02
5.16	0.83	11.59	7.42	86.02	3.06	0.06	0.83
5.18	0.68	9.17	9.10	83.40	3.19	0.06	0.65
5.20	0.59	7.88	10.12	79.73	3.26	0.06	0.56
5.22	0.55	7.09	10.75	76.25	3.30	0.06	0.51
5.24	0.54	6.99	10.64	74.40	3.29	0.06	0.50
5.26	0.54	6.99	10.54	73.66	3.29	0.06	0.50
5.28	0.55	7.14	10.12	72.20	3.26	0.06	0.51
5.30	0.57	7.36	9.47	69.69	3.22	0.06	0.53
5.32	0.60	7.77	8.67	67.33	3.16	0.06	0.55
5.34	0.63	8.34	8.06	67.28	3.11	0.06	0.60
5.36	0.68	8.96	7.62	68.32	3.08	0.06	0.64
5.38	0.69	9.17	7.63	69.98	3.08	0.06	0.65
5.40	0.67	8.82	8.04	70.97	3.11	0.06	0.63
5.42	0.63	8.22	8.72	71.72	3.16	0.06	0.59
5.44	0.62	8.07	8.96	72.33	3.18	0.06	0.58
5.46	0.67	8.71	8.47	73.82	3.14	0.06	0.62
5.48	0.72	9.44	7.97	75.17	3.10	0.06	0.67
5.50	0.69	9.05	8.41	76.10	3.14	0.06	0.65
5.52	0.62	7.92	9.40	74.41	3.21	0.06	0.57
5.54	0.57	7.09	10.18	72.20	3.26	0.06	0.51
5.56	0.57	7.12	9.86	70.20	3.24	0.06	0.51
5.59	0.57	7.10	9.77	69.32	3.24	0.06	0.51
5.60	0.56	6.94	9.85	68.33	3.24	0.06	0.50
5.62	0.59	7.35	9.20	67.69	3.20	0.06	0.53
5.64	0.66	8.39	7.99	67.02	3.10	0.06	0.60
5.66	0.72	9.32	7.19	67.06	3.04	0.06	0.67
5.68	0.74	9.51	7.22	68.69	3.04	0.06	0.68
5.70	0.71	9.05	7.89	71.48	3.10	0.06	0.65
5.72	0.68	8.55	8.53	72.87	3.15	0.06	0.61
5.74	0.66	8.27	8.80	72.73	3.17	0.06	0.59
5.76	0.67	8.45	8.54	72.16	3.15	0.06	0.60

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	0.70	8.77	8.22	72.13	3.12	0.06	0.63
5.80	0.73	9.22	7.80	71.94	3.09	0.06	0.66
5.82	0.75	9.58	7.39	70.75	3.06	0.06	0.68
5.84	0.78	9.94	6.96	69.22	3.02	0.06	0.71
5.86	0.80	10.22	6.71	68.58	3.00	0.06	0.73
5.88	0.88	11.42	6.26	71.46	2.96	0.06	0.82
5.90	0.95	12.33	6.20	76.44	2.95	0.06	0.88
5.92	0.98	12.78	6.39	81.64	2.97	0.06	0.91
5.94	0.92	11.91	7.08	84.30	3.03	0.06	0.85
5.96	0.87	11.05	7.67	84.76	3.08	0.06	0.79
5.98	0.84	10.63	7.91	84.06	3.10	0.06	0.76
6.00	0.81	10.20	8.09	82.58	3.11	0.06	0.73
6.02	0.79	9.91	8.21	81.38	3.12	0.06	0.71
6.04	0.80	9.98	7.93	79.13	3.10	0.06	0.71
6.06	0.85	10.62	7.27	77.28	3.05	0.06	0.76
6.08	0.91	11.45	6.58	75.34	2.98	0.06	0.82
6.10	0.94	11.91	6.26	74.64	2.96	0.06	0.85
6.12	0.94	11.85	6.34	75.10	2.96	0.06	0.85
6.14	0.91	11.37	6.68	75.94	2.99	0.06	0.81
6.16	0.83	10.23	7.54	77.09	3.07	0.06	0.73
6.18	0.76	9.25	8.45	78.17	3.14	0.06	0.66
6.20	0.72	8.60	9.22	79.27	3.20	0.06	0.61
6.22	0.72	8.59	9.23	79.29	3.20	0.06	0.61
6.24	0.71	8.48	9.26	78.48	3.20	0.06	0.61
6.26	0.70	8.27	9.20	76.12	3.20	0.06	0.59
6.28	0.69	8.20	9.03	74.04	3.18	0.06	0.59
6.30	0.71	8.48	8.40	71.19	3.14	0.06	0.61
6.32	0.73	8.68	7.92	68.74	3.10	0.06	0.62
6.34	0.73	8.63	7.81	67.41	3.09	0.06	0.62
6.36	0.70	8.26	8.11	66.92	3.11	0.06	0.59
6.38	0.68	7.88	8.39	66.11	3.14	0.06	0.56
6.40	0.66	7.55	8.65	65.29	3.16	0.06	0.54
6.42	0.65	7.41	8.72	64.61	3.16	0.06	0.53
6.44	0.66	7.60	8.52	64.75	3.15	0.06	0.54
6.46	0.70	8.08	8.10	65.37	3.11	0.06	0.58
6.48	0.75	8.83	7.49	66.14	3.06	0.06	0.63
6.50	0.80	9.42	7.15	67.38	3.04	0.06	0.67
6.52	0.83	9.79	7.04	68.95	3.03	0.06	0.70
6.54	0.83	9.87	7.08	69.91	3.03	0.06	0.71
6.56	0.82	9.69	7.29	70.67	3.05	0.06	0.69
6.58	0.80	9.34	7.62	71.17	3.08	0.06	0.67
6.60	0.77	8.90	8.06	71.75	3.11	0.06	0.64
6.62	0.73	8.43	8.60	72.43	3.15	0.06	0.60
6.64	0.71	8.01	9.08	72.75	3.19	0.06	0.57
6.66	0.69	7.73	9.45	73.09	3.21	0.06	0.55
6.68	0.67	7.49	9.82	73.55	3.24	0.06	0.54
6.70	0.65	7.23	10.16	73.43	3.26	0.06	0.52
6.72	0.63	6.97	10.48	72.99	3.28	0.06	0.50

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	0.63	6.91	10.33	71.45	3.27	0.06	0.49
6.76	0.64	6.96	10.04	69.87	3.25	0.06	0.50
6.78	0.64	6.97	9.84	68.51	3.24	0.06	0.50
6.80	0.63	6.79	9.99	67.87	3.25	0.06	0.49
6.82	0.61	6.52	10.36	67.52	3.28	0.06	0.47
6.84	0.59	6.22	10.89	67.77	3.31	0.06	0.44
6.86	0.57	6.02	11.36	68.43	3.34	0.06	0.43
6.88	0.59	6.27	11.02	69.11	3.32	0.06	0.45
6.90	0.62	6.59	10.52	69.34	3.29	0.06	0.47
6.92	0.64	6.93	9.98	69.21	3.25	0.06	0.50
6.94	0.64	6.88	10.01	68.95	3.25	0.06	0.49
6.96	0.63	6.73	10.09	67.97	3.26	0.06	0.48
6.98	0.61	6.50	10.14	65.96	3.26	0.06	0.46
7.00	0.60	6.33	10.04	63.59	3.26	0.06	0.45
7.02	0.60	6.33	9.68	61.26	3.23	0.06	0.45
7.04	0.61	6.44	9.23	59.41	3.20	0.06	0.46
7.06	0.62	6.55	8.86	58.05	3.17	0.06	0.47
7.08	0.62	6.53	8.72	56.99	3.16	0.06	0.47
7.10	0.63	6.61	8.49	56.08	3.14	0.06	0.47
7.12	0.65	6.87	8.09	55.61	3.11	0.06	0.49
7.14	0.70	7.45	7.48	55.74	3.06	0.06	0.53
7.16	0.75	8.16	6.96	56.78	3.02	0.06	0.58
7.18	0.82	9.03	6.52	58.92	2.98	0.06	0.65
7.20	0.89	9.85	6.34	62.44	2.96	0.06	0.70
7.22	0.94	10.56	6.42	67.76	2.97	0.06	0.75
7.24	0.97	10.85	6.78	73.59	3.00	0.06	0.78
7.26	0.98	10.95	7.31	79.99	3.05	0.06	0.78
7.28	0.98	10.94	7.83	85.66	3.09	0.06	0.78
7.30	0.98	10.97	8.27	90.70	3.13	0.06	0.78
7.32	0.98	10.97	8.60	94.26	3.15	0.06	0.78
7.34	0.98	10.90	8.85	96.50	3.17	0.06	0.78
7.36	0.98	10.81	9.04	97.70	3.18	0.06	0.77
7.38	0.96	10.60	9.26	98.14	3.20	0.06	0.76
7.41	0.94	10.34	9.48	98.02	3.22	0.06	0.74
7.42	0.92	10.05	9.68	97.33	3.23	0.06	0.72
7.44	0.89	9.64	10.02	96.61	3.25	0.06	0.69
7.46	0.86	9.24	10.38	95.94	3.28	0.06	0.66
7.48	0.83	8.82	10.81	95.41	3.31	0.06	0.63
7.50	0.82	8.69	10.89	94.61	3.31	0.06	0.62
7.52	0.83	8.74	10.74	93.94	3.30	0.06	0.62
7.54	0.85	9.00	10.36	93.24	3.28	0.06	0.64
7.56	0.88	9.42	9.82	92.50	3.24	0.06	0.67
7.58	0.92	9.88	9.22	91.05	3.20	0.06	0.71
7.60	0.96	10.30	8.70	89.65	3.16	0.06	0.74
7.62	0.98	10.57	8.35	88.23	3.13	0.06	0.75
7.64	0.99	10.65	8.19	87.19	3.12	0.06	0.76
7.66	0.99	10.56	8.16	86.13	3.12	0.06	0.75
7.68	0.96	10.24	8.39	85.87	3.14	0.06	0.73

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	0.93	9.84	8.77	86.32	3.17	0.06	0.70
7.72	0.90	9.44	9.22	87.02	3.20	0.06	0.67
7.74	0.86	8.97	9.70	87.03	3.23	0.06	0.64
7.76	0.81	8.26	10.42	86.03	3.28	0.06	0.59
7.78	0.73	7.32	11.46	83.93	3.35	0.06	0.52
7.80	0.65	6.34	12.77	80.97	3.43	0.06	0.45
7.82	0.60	5.65	13.74	77.64	3.48	0.06	0.40
7.84	0.57	5.25	14.16	74.35	3.50	0.06	0.38
7.86	0.56	5.19	13.74	71.39	3.48	0.06	0.37
7.88	0.60	5.69	12.06	68.59	3.38	0.06	0.41
7.90	0.64	6.09	10.80	65.78	3.31	0.06	0.44
7.92	0.65	6.24	10.17	63.51	3.26	0.06	0.45
7.94	0.61	5.69	10.88	61.91	3.31	0.06	0.41
7.96	0.56	5.12	11.70	59.91	3.36	0.06	0.37
7.98	0.51	4.49	12.75	57.23	3.42	0.06	0.32
8.00	0.47	3.99	13.74	54.76	3.48	0.06	0.28
8.02	0.44	3.57	14.59	52.15	3.53	0.06	0.26
8.04	0.43	3.49	14.34	49.99	3.51	0.05	0.25
8.06	0.44	3.58	13.43	48.07	3.46	0.06	0.26
8.08	0.46	3.78	12.46	47.07	3.41	0.06	0.27
8.10	0.47	3.92	11.95	46.83	3.38	0.06	0.28
8.12	0.47	3.99	11.78	47.05	3.37	0.06	0.29
8.14	0.48	4.06	11.55	46.86	3.35	0.06	0.29
8.16	0.49	4.17	11.15	46.55	3.33	0.06	0.30
8.18	0.51	4.34	10.69	46.36	3.30	0.06	0.31
8.20	0.52	4.51	10.30	46.44	3.27	0.06	0.32
8.22	0.54	4.69	9.95	46.67	3.25	0.06	0.34
8.24	0.56	4.90	9.58	46.97	3.22	0.06	0.35
8.26	0.58	5.14	9.22	47.40	3.20	0.06	0.37
8.28	0.59	5.23	9.15	47.87	3.19	0.06	0.37
8.30	0.58	5.16	9.32	48.10	3.21	0.06	0.37
8.32	0.57	5.01	9.55	47.88	3.22	0.06	0.36
8.34	0.57	4.98	9.55	47.58	3.22	0.06	0.36
8.36	0.59	5.18	9.19	47.59	3.20	0.06	0.37
8.38	0.61	5.46	8.78	48.00	3.17	0.06	0.39
8.40	0.64	5.85	8.39	49.12	3.14	0.06	0.42
8.42	0.69	6.35	7.92	50.30	3.10	0.06	0.45
8.44	0.72	6.74	7.67	51.68	3.08	0.06	0.48
8.46	0.73	6.83	7.81	53.33	3.09	0.06	0.49
8.48	0.70	6.40	8.61	55.06	3.15	0.06	0.46
8.50	0.66	5.96	9.45	56.29	3.21	0.06	0.43
8.52	0.65	5.88	9.64	56.70	3.23	0.06	0.42
8.54	0.68	6.15	9.28	57.10	3.20	0.06	0.44
8.56	0.70	6.36	9.08	57.77	3.19	0.06	0.45
8.58	0.69	6.26	9.37	58.70	3.21	0.06	0.45
8.60	0.67	6.06	9.78	59.27	3.24	0.06	0.43
8.62	0.66	5.87	10.03	58.86	3.25	0.06	0.42
8.64	0.65	5.76	10.04	57.81	3.26	0.06	0.41

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	0.66	5.84	9.71	56.73	3.23	0.06	0.42
8.68	0.68	6.09	9.19	55.90	3.20	0.06	0.43
8.70	0.71	6.41	8.60	55.08	3.15	0.06	0.46
8.72	0.73	6.66	8.21	54.67	3.12	0.06	0.48
8.74	0.75	6.81	8.08	55.04	3.11	0.06	0.49
8.76	0.76	6.93	8.13	56.31	3.12	0.06	0.50
8.78	0.78	7.10	8.06	57.23	3.11	0.06	0.51
8.80	0.81	7.43	7.81	58.03	3.09	0.06	0.53
8.82	0.84	7.86	7.47	58.68	3.06	0.06	0.56
8.84	0.88	8.29	7.35	60.89	3.05	0.06	0.59
8.86	0.94	8.91	7.09	63.16	3.03	0.06	0.64
8.88	0.99	9.47	6.95	65.83	3.02	0.06	0.68
8.90	1.02	9.75	6.99	68.12	3.02	0.06	0.70
8.92	1.01	9.59	7.40	70.98	3.06	0.06	0.69
8.94	0.98	9.28	7.91	73.39	3.10	0.06	0.66
8.96	0.95	8.88	8.56	75.99	3.15	0.06	0.63
8.98	0.92	8.54	9.08	77.60	3.19	0.06	0.61
9.00	0.89	8.27	9.57	79.10	3.22	0.06	0.59
9.02	0.89	8.18	9.74	79.68	3.23	0.06	0.58
9.04	0.88	8.04	9.95	79.97	3.25	0.06	0.57
9.06	0.86	7.85	10.15	79.64	3.26	0.06	0.56
9.08	0.84	7.56	10.34	78.18	3.28	0.06	0.54
9.10	0.81	7.20	10.57	76.14	3.29	0.06	0.51
9.12	0.76	6.69	11.03	73.85	3.32	0.06	0.48
9.14	0.71	6.11	11.75	71.85	3.37	0.06	0.44
9.16	0.66	5.55	12.61	70.00	3.42	0.06	0.40
9.18	0.62	5.13	13.23	67.84	3.45	0.06	0.37
9.20	0.60	4.84	13.64	65.99	3.48	0.06	0.35
9.22	0.60	4.90	13.23	64.82	3.45	0.06	0.35
9.24	0.63	5.16	12.40	63.98	3.40	0.06	0.37
9.26	0.66	5.51	11.39	62.73	3.34	0.06	0.39
9.28	0.66	5.44	11.10	60.35	3.32	0.06	0.39
9.30	0.63	5.13	11.13	57.08	3.33	0.06	0.37
9.32	0.61	4.88	11.02	53.79	3.32	0.06	0.35
9.34	0.61	4.93	10.41	51.35	3.28	0.06	0.35
9.36	0.64	5.24	9.70	50.79	3.23	0.06	0.37
9.38	0.68	5.65	9.15	51.68	3.19	0.06	0.40
9.40	0.76	6.49	8.28	53.78	3.13	0.06	0.46
9.42	0.83	7.28	7.68	55.89	3.08	0.06	0.52
9.44	0.85	7.47	7.69	57.42	3.08	0.06	0.53
9.46	0.79	6.76	8.57	57.96	3.15	0.06	0.48
9.48	0.70	5.79	9.89	57.21	3.24	0.06	0.41
9.50	0.66	5.32	10.51	55.95	3.29	0.06	0.38
9.52	0.66	5.32	10.43	55.52	3.28	0.06	0.38
9.54	0.69	5.70	9.90	56.39	3.25	0.06	0.41
9.56	0.79	6.67	8.66	57.75	3.16	0.06	0.48
9.58	0.94	8.34	7.02	58.48	3.02	0.06	0.60
9.60	1.14	10.47	5.62	58.88	2.89	0.07	0.75

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	1.35	12.59	4.78	60.15	2.80	0.07	0.90
9.64	1.56	14.77	4.27	63.01	2.74	0.08	1.06
9.66	1.75	16.78	3.97	66.55	2.70	0.08	1.20
9.68	1.81	17.36	3.99	69.31	2.70	0.08	1.25
9.70	1.63	15.48	4.56	70.65	2.77	0.08	1.11
9.72	1.31	12.08	5.72	69.05	2.90	0.07	0.86
9.74	0.98	8.57	7.71	66.10	3.08	0.06	0.61
9.76	0.83	7.02	8.82	61.96	3.17	0.06	0.50
9.78	0.79	6.55	9.15	59.93	3.19	0.06	0.47
9.80	0.80	6.71	8.79	59.05	3.17	0.06	0.48
9.82	0.79	6.59	8.99	59.22	3.18	0.06	0.47
9.84	0.83	6.99	8.85	61.82	3.17	0.06	0.50
9.86	0.85	7.10	9.19	65.22	3.20	0.06	0.51
9.88	0.82	6.83	10.00	68.34	3.25	0.06	0.49
9.90	0.73	5.92	11.50	68.08	3.35	0.06	0.42
9.92	0.70	5.49	12.09	66.43	3.39	0.06	0.39
9.94	0.69	5.40	11.96	64.61	3.38	0.06	0.39
9.96	0.68	5.35	11.66	62.41	3.36	0.06	0.38
9.98	0.66	5.13	11.62	59.61	3.36	0.06	0.37
10.00	0.64	4.93	11.45	56.45	3.35	0.06	0.35
10.02	0.63	4.78	11.18	53.48	3.33	0.06	0.34
10.04	0.63	4.80	10.75	51.63	3.30	0.06	0.34
10.06	0.64	4.89	10.47	51.23	3.28	0.06	0.35
10.08	0.66	5.09	10.16	51.75	3.26	0.06	0.36
10.10	0.69	5.30	9.90	52.46	3.25	0.06	0.38
10.12	0.70	5.45	9.68	52.78	3.23	0.06	0.39
10.14	0.71	5.50	9.64	52.97	3.23	0.06	0.39
10.16	0.70	5.45	9.83	53.59	3.24	0.06	0.39
10.18	0.70	5.40	10.06	54.37	3.26	0.06	0.39
10.20	0.70	5.37	10.24	54.95	3.27	0.06	0.38
10.22	0.70	5.36	10.28	55.10	3.27	0.06	0.38
10.24	0.70	5.38	10.19	54.78	3.27	0.06	0.38
10.26	0.70	5.39	10.10	54.41	3.26	0.06	0.38
10.28	0.70	5.37	10.10	54.26	3.26	0.06	0.38
10.30	0.70	5.31	10.19	54.09	3.27	0.06	0.38
10.32	0.69	5.26	10.25	53.89	3.27	0.06	0.38
10.34	0.69	5.25	10.22	53.64	3.27	0.06	0.37
10.36	0.69	5.24	10.27	53.80	3.27	0.06	0.37
10.38	0.69	5.20	10.47	54.45	3.28	0.06	0.37
10.40	0.69	5.15	10.66	54.87	3.30	0.06	0.37
10.42	0.70	5.25	10.50	55.10	3.29	0.06	0.37
10.44	0.71	5.36	10.31	55.22	3.27	0.06	0.38
10.46	0.72	5.50	10.11	55.63	3.26	0.06	0.39
10.48	0.72	5.44	10.42	56.71	3.28	0.06	0.39
10.50	0.71	5.36	10.69	57.31	3.30	0.06	0.38
10.52	0.70	5.20	11.04	57.41	3.32	0.06	0.37
10.54	0.68	5.02	11.38	57.18	3.34	0.06	0.36
10.56	0.67	4.94	11.57	57.23	3.35	0.06	0.35

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	0.69	5.13	11.18	57.33	3.33	0.06	0.37
10.60	0.81	6.28	9.21	57.89	3.20	0.06	0.45
10.62	0.91	7.28	7.94	57.80	3.10	0.06	0.52
10.64	0.97	7.83	7.50	58.73	3.06	0.06	0.56
10.66	0.92	7.33	8.23	60.33	3.12	0.06	0.52
10.68	0.85	6.63	9.35	62.04	3.21	0.06	0.47
10.70	0.79	6.02	10.35	62.30	3.28	0.06	0.43
10.72	0.71	5.23	11.71	61.21	3.36	0.06	0.37
10.74	0.66	4.73	12.54	59.33	3.41	0.06	0.34
10.76	0.63	4.45	12.98	57.69	3.44	0.06	0.32
10.78	0.64	4.55	12.37	56.33	3.40	0.06	0.33
10.80	0.65	4.64	11.84	54.91	3.37	0.06	0.33
10.82	0.65	4.63	11.54	53.44	3.35	0.06	0.33
10.84	0.71	5.13	10.89	55.84	3.31	0.06	0.37
10.86	0.72	5.27	11.11	58.56	3.33	0.06	0.38
10.88	0.72	5.23	11.67	61.06	3.36	0.06	0.37
10.90	0.65	4.54	13.15	59.73	3.45	0.06	0.32
10.92	0.62	4.20	13.84	58.14	3.49	0.06	0.30
10.94	0.61	4.13	13.78	56.93	3.48	0.06	0.30
10.96	0.61	4.13	13.42	55.43	3.46	0.06	0.29
10.98	0.62	4.18	12.90	53.97	3.43	0.06	0.30
11.00	0.63	4.28	12.24	52.38	3.39	0.06	0.31
11.02	0.64	4.39	11.65	51.20	3.36	0.06	0.31
11.04	0.65	4.44	11.36	50.51	3.34	0.06	0.32
11.06	0.64	4.40	11.40	50.14	3.34	0.06	0.31
11.08	0.64	4.39	11.40	50.02	3.34	0.06	0.31
11.10	0.66	4.55	11.01	50.13	3.32	0.06	0.33
11.12	0.71	5.00	10.17	50.79	3.26	0.06	0.36
11.14	0.78	5.68	9.17	52.12	3.19	0.06	0.41
11.16	0.84	6.31	8.46	53.36	3.14	0.06	0.45
11.18	0.88	6.60	8.29	54.72	3.13	0.06	0.47
11.20	0.88	6.66	8.44	56.21	3.14	0.06	0.48
11.22	0.95	7.27	8.01	58.26	3.11	0.06	0.52
11.24	1.11	8.83	6.86	60.53	3.01	0.06	0.63
11.26	1.31	10.70	5.91	63.18	2.92	0.07	0.76
11.28	1.48	12.31	5.47	67.34	2.88	0.07	0.88
11.30	1.59	13.38	5.44	72.75	2.87	0.07	0.96
11.32	1.65	13.93	5.53	77.07	2.88	0.07	0.99
11.34	1.64	13.79	5.77	79.56	2.91	0.07	0.99
11.36	1.56	12.99	6.25	81.19	2.95	0.07	0.93
11.38	1.46	12.00	6.73	80.70	3.00	0.07	0.86
11.40	1.37	11.11	7.15	79.48	3.04	0.06	0.79
11.42	1.30	10.48	7.43	77.84	3.06	0.06	0.75
11.44	1.28	10.28	7.60	78.09	3.07	0.06	0.73
11.46	1.29	10.37	7.62	79.02	3.08	0.06	0.74
11.48	1.34	10.77	7.47	80.46	3.06	0.06	0.77
11.50	1.43	11.59	7.10	82.30	3.03	0.07	0.83
11.52	1.56	12.80	6.58	84.26	2.99	0.07	0.91

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	1.72	14.26	6.04	86.05	2.93	0.07	1.02
11.56	1.83	15.32	5.69	87.13	2.90	0.07	1.09
11.58	1.89	15.77	5.51	86.88	2.88	0.08	1.13
11.60	1.93	16.22	5.17	83.88	2.84	0.08	1.16
11.62	2.06	17.37	4.59	79.68	2.78	0.08	1.24
11.64	2.23	19.00	4.09	77.67	2.71	0.08	1.35
11.66	2.41	20.68	3.79	78.36	2.67	0.09	1.47
11.68	2.51	21.60	3.72	80.27	2.66	0.09	1.53
11.70	2.55	21.91	3.69	80.85	2.66	0.09	1.56
11.72	2.49	21.26	3.75	79.64	2.66	0.09	1.51
11.74	2.35	19.98	3.88	77.43	2.68	0.09	1.42
11.76	2.18	18.32	4.16	76.16	2.72	0.08	1.30
11.78	1.96	16.23	4.77	77.41	2.80	0.08	1.16
11.80	1.68	13.62	5.84	79.48	2.91	0.07	0.97
11.82	1.43	11.24	7.08	79.58	3.03	0.06	0.80
11.84	1.19	9.04	8.48	76.66	3.14	0.06	0.65
11.86	1.02	7.46	9.91	73.91	3.25	0.06	0.53
11.88	0.88	6.20	11.47	71.11	3.35	0.06	0.44
11.90	0.79	5.40	12.83	69.28	3.43	0.06	0.39
11.93	0.75	4.97	13.44	66.84	3.46	0.06	0.36
11.94	0.74	4.85	13.27	64.34	3.45	0.06	0.35
11.96	0.79	5.32	11.71	62.31	3.36	0.06	0.38
11.98	0.88	6.12	9.94	60.81	3.25	0.06	0.44
12.00	0.95	6.80	8.74	59.39	3.16	0.06	0.49
12.02	0.96	6.82	8.75	59.67	3.16	0.06	0.49
12.04	0.92	6.50	9.21	59.86	3.20	0.06	0.46
12.06	0.88	6.10	9.81	59.88	3.24	0.06	0.44
12.08	0.84	5.75	10.30	59.18	3.27	0.06	0.41
12.10	0.82	5.50	10.78	59.27	3.30	0.06	0.39
12.12	0.79	5.26	11.41	60.04	3.34	0.06	0.38
12.14	0.79	5.22	11.65	60.79	3.36	0.06	0.37
12.16	0.79	5.23	11.58	60.56	3.35	0.06	0.37
12.18	0.80	5.31	11.21	59.57	3.33	0.06	0.38
12.20	0.81	5.44	10.74	58.36	3.30	0.06	0.39
12.22	0.83	5.57	10.26	57.12	3.27	0.06	0.40
12.24	0.84	5.62	10.04	56.41	3.26	0.06	0.40
12.26	0.84	5.67	9.91	56.22	3.25	0.06	0.41
12.28	0.85	5.69	9.95	56.60	3.25	0.06	0.41
12.30	0.84	5.66	10.02	56.67	3.25	0.06	0.40
12.32	0.83	5.55	10.16	56.39	3.26	0.06	0.40
12.34	0.84	5.58	9.98	55.68	3.25	0.06	0.40
12.36	0.85	5.68	9.72	55.22	3.23	0.06	0.41
12.38	0.86	5.76	9.57	55.13	3.22	0.06	0.41
12.40	0.85	5.70	9.76	55.62	3.24	0.06	0.41
12.42	0.84	5.56	10.10	56.13	3.26	0.06	0.40
12.44	0.84	5.53	10.26	56.78	3.27	0.06	0.40
12.46	0.85	5.64	10.19	57.46	3.27	0.06	0.40
12.48	0.88	5.88	9.93	58.42	3.25	0.06	0.42

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	0.91	6.11	9.73	59.44	3.23	0.06	0.44
12.52	0.92	6.26	9.70	60.72	3.23	0.06	0.45
12.54	0.94	6.35	9.79	62.21	3.24	0.06	0.45
12.56	0.95	6.43	9.90	63.65	3.25	0.06	0.46
12.58	0.95	6.46	10.07	65.04	3.26	0.06	0.46
12.60	0.94	6.39	10.39	66.39	3.28	0.06	0.46
12.62	0.94	6.31	10.70	67.49	3.30	0.06	0.45
12.64	0.93	6.27	10.84	68.03	3.31	0.06	0.45
12.66	0.95	6.39	10.68	68.30	3.30	0.06	0.46
12.68	0.97	6.61	10.34	68.30	3.28	0.06	0.47
12.70	1.00	6.82	10.00	68.19	3.25	0.06	0.49
12.72	1.02	7.00	9.75	68.24	3.24	0.06	0.50
12.74	1.02	7.00	9.79	68.56	3.24	0.06	0.50
12.76	1.02	6.92	10.03	69.41	3.25	0.06	0.49
12.78	1.00	6.74	10.40	70.16	3.28	0.06	0.48
12.80	0.99	6.66	10.58	70.50	3.29	0.06	0.48
12.82	1.01	6.80	10.45	71.10	3.28	0.06	0.49
12.84	1.03	7.02	10.27	72.05	3.27	0.06	0.50
12.86	1.06	7.26	10.09	73.28	3.26	0.06	0.52
12.89	1.08	7.40	10.00	74.01	3.25	0.06	0.53
12.90	1.10	7.58	9.81	74.41	3.24	0.06	0.54
12.92	1.12	7.75	9.70	75.18	3.23	0.06	0.55
12.95	1.14	7.85	9.72	76.30	3.23	0.06	0.56
12.96	1.14	7.85	9.88	77.51	3.24	0.06	0.56
12.98	1.13	7.72	10.16	78.37	3.26	0.06	0.55
13.00	1.11	7.59	10.41	79.00	3.28	0.06	0.54
13.02	1.11	7.52	10.57	79.46	3.29	0.06	0.54
13.04	1.10	7.42	10.76	79.85	3.30	0.06	0.53
13.06	1.09	7.34	10.88	79.87	3.31	0.06	0.52
13.08	1.07	7.20	11.08	79.79	3.32	0.06	0.51
13.10	1.06	7.07	11.24	79.48	3.33	0.06	0.51
13.12	1.03	6.84	11.57	79.07	3.35	0.06	0.49
13.14	0.99	6.51	12.03	78.33	3.38	0.06	0.46
13.16	0.95	6.15	12.58	77.34	3.41	0.06	0.44
13.18	0.91	5.77	13.14	75.79	3.45	0.06	0.41
13.20	0.88	5.52	13.44	74.11	3.46	0.06	0.39
13.22	0.86	5.34	13.49	72.12	3.47	0.06	0.38
13.24	0.85	5.25	13.34	70.01	3.46	0.06	0.37
13.26	0.83	5.10	13.26	67.55	3.45	0.06	0.36
13.28	0.81	4.91	13.25	65.06	3.45	0.06	0.35
13.30	0.79	4.71	13.32	62.74	3.46	0.06	0.34
13.32	0.78	4.60	13.17	60.56	3.45	0.06	0.33
13.34	0.78	4.59	12.80	58.82	3.43	0.06	0.33
13.36	0.78	4.57	12.61	57.65	3.42	0.06	0.33
13.38	0.76	4.46	12.81	57.05	3.43	0.06	0.32
13.40	0.74	4.23	13.26	56.13	3.45	0.06	0.30
13.42	0.71	4.02	13.62	54.76	3.47	0.06	0.29
13.44	0.69	3.86	13.73	52.97	3.48	0.06	0.28

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	0.68	3.78	13.71	51.79	3.48	0.06	0.27
13.48	0.68	3.75	13.53	50.73	3.47	0.06	0.27
13.50	0.69	3.77	13.23	49.90	3.45	0.06	0.27
13.52	0.69	3.78	12.87	48.68	3.43	0.06	0.27
13.54	0.69	3.80	12.59	47.83	3.42	0.06	0.27
13.56	0.70	3.87	12.23	47.35	3.39	0.06	0.28
13.58	0.72	4.01	11.82	47.44	3.37	0.06	0.29
13.60	0.75	4.23	11.28	47.78	3.34	0.06	0.30
13.62	0.77	4.38	11.04	48.40	3.32	0.06	0.31
13.64	0.77	4.41	11.11	49.02	3.33	0.06	0.32
13.66	0.76	4.31	11.56	49.83	3.35	0.06	0.31
13.68	0.74	4.15	12.15	50.37	3.39	0.06	0.30
13.70	0.73	4.04	12.57	50.75	3.41	0.06	0.29
13.72	0.72	3.99	12.73	50.82	3.42	0.06	0.29
13.74	0.73	4.02	12.62	50.68	3.42	0.06	0.29
13.76	0.73	4.05	12.45	50.38	3.41	0.06	0.29
13.78	0.74	4.11	12.15	49.94	3.39	0.06	0.29
13.80	0.75	4.19	11.60	48.67	3.36	0.06	0.30
13.82	0.77	4.38	11.04	48.40	3.32	0.06	0.31
13.84	0.79	4.48	10.86	48.68	3.31	0.06	0.32
13.86	0.78	4.42	11.40	50.34	3.34	0.06	0.32
13.88	0.75	4.18	12.16	50.79	3.39	0.06	0.30
13.90	0.74	4.08	12.50	51.03	3.41	0.06	0.29
13.92	0.77	4.31	11.91	51.33	3.37	0.06	0.31
13.94	0.81	4.66	11.06	51.55	3.32	0.06	0.33
13.96	0.83	4.80	10.70	51.37	3.30	0.06	0.34
13.98	0.79	4.41	11.42	50.39	3.34	0.06	0.32
14.00	0.73	3.93	12.43	48.87	3.41	0.06	0.28
14.02	0.68	3.56	13.24	47.10	3.45	0.06	0.25
14.04	0.67	3.47	13.29	46.18	3.46	0.06	0.25
14.06	0.66	3.38	13.57	45.86	3.47	0.06	0.24
14.08	0.65	3.30	13.88	45.84	3.49	0.06	0.24
14.10	0.66	3.35	13.69	45.84	3.48	0.06	0.24
14.12	0.68	3.48	13.11	45.65	3.45	0.06	0.25
14.14	0.69	3.63	12.49	45.33	3.41	0.06	0.26
14.16	0.70	3.66	12.27	44.98	3.40	0.06	0.26
14.18	0.70	3.66	12.25	44.80	3.40	0.06	0.26
14.20	0.71	3.74	11.90	44.55	3.37	0.06	0.27
14.22	0.75	4.06	10.94	44.40	3.31	0.06	0.29
14.24	0.78	4.32	10.30	44.47	3.27	0.06	0.31
14.26	0.79	4.32	10.48	45.32	3.28	0.06	0.31
14.28	0.75	4.02	11.52	46.28	3.35	0.06	0.29
14.30	0.72	3.78	12.39	46.82	3.40	0.06	0.27
14.32	0.74	3.91	12.10	47.30	3.39	0.06	0.28
14.34	0.82	4.60	10.57	48.59	3.29	0.06	0.33
14.36	0.96	5.64	8.86	49.95	3.17	0.06	0.40
14.38	1.07	6.54	7.84	51.26	3.09	0.06	0.47
14.40	1.05	6.37	8.03	51.15	3.11	0.06	0.45

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	0.96	5.64	8.92	50.32	3.18	0.06	0.40
14.44	0.87	4.94	9.91	48.97	3.25	0.06	0.35
14.46	0.87	4.89	9.98	48.82	3.25	0.06	0.35
14.48	0.91	5.25	9.36	49.10	3.21	0.06	0.37
14.50	1.02	6.04	8.35	50.40	3.13	0.06	0.43
14.52	1.18	7.30	7.15	52.22	3.04	0.06	0.52
14.54	1.35	8.64	6.18	53.40	2.95	0.06	0.62
14.56	1.43	9.27	5.90	54.71	2.92	0.07	0.66
14.58	1.42	9.18	6.08	55.87	2.94	0.07	0.66
14.60	1.32	8.38	6.92	57.98	3.02	0.06	0.60
14.62	1.18	7.27	8.21	59.69	3.12	0.06	0.52
14.64	1.04	6.14	9.99	61.36	3.25	0.06	0.44
14.66	0.94	5.39	11.58	62.42	3.35	0.06	0.39
14.68	0.95	5.42	11.69	63.34	3.36	0.06	0.39
14.70	1.05	6.23	10.30	64.20	3.27	0.06	0.45
14.72	1.23	7.59	8.49	64.43	3.14	0.06	0.54
14.74	1.36	8.62	7.45	64.24	3.06	0.06	0.62
14.76	1.43	9.15	6.89	63.04	3.01	0.06	0.65
14.78	1.38	8.73	7.17	62.67	3.04	0.06	0.62
14.80	1.38	8.75	7.51	65.64	3.07	0.06	0.62
14.82	1.34	8.39	8.34	70.01	3.13	0.06	0.60
14.84	1.38	8.67	8.48	73.56	3.14	0.06	0.62
14.87	1.33	8.28	8.96	74.25	3.18	0.06	0.59
14.88	1.29	7.94	9.21	73.13	3.20	0.06	0.57
14.91	1.18	7.13	9.96	70.97	3.25	0.06	0.51
14.92	1.12	6.63	10.19	67.55	3.26	0.06	0.47
14.94	1.05	6.07	10.66	64.68	3.30	0.06	0.43
14.96	0.93	5.16	11.75	60.71	3.37	0.06	0.37
14.98	0.79	4.12	13.72	56.49	3.48	0.06	0.29
15.00	0.73	3.62	14.49	52.52	3.52	0.06	0.26
15.02	0.81	4.26	12.17	51.79	3.39	0.06	0.30
15.04	1.02	5.80	8.97	52.01	3.18	0.06	0.41
15.06	1.29	7.88	6.74	53.08	3.00	0.06	0.56
15.08	1.59	10.14	5.42	54.95	2.87	0.07	0.72
15.10	1.86	12.22	4.75	58.03	2.80	0.08	0.87
15.12	2.03	13.50	4.61	62.16	2.78	0.08	0.96
15.14	1.98	13.05	5.05	65.98	2.83	0.08	0.93
15.16	1.75	11.28	6.04	68.18	2.93	0.07	0.81
15.18	1.43	8.88	7.76	68.86	3.09	0.06	0.63
15.20	1.16	6.82	9.90	67.56	3.25	0.06	0.49
15.22	0.98	5.44	12.05	65.47	3.38	0.06	0.39
15.24	0.88	4.68	13.59	63.58	3.47	0.06	0.33
15.26	0.87	4.61	13.78	63.60	3.48	0.06	0.33
15.28	0.98	5.44	12.06	65.63	3.38	0.06	0.39
15.30	1.23	7.24	9.25	67.02	3.20	0.06	0.52
15.32	1.56	9.76	6.70	65.41	3.00	0.06	0.70
15.34	1.85	11.89	5.36	63.72	2.86	0.07	0.85
15.36	2.05	13.44	4.71	63.34	2.79	0.08	0.95

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	2.10	13.77	4.77	65.75	2.80	0.08	0.98
15.40	1.97	12.71	5.35	68.03	2.86	0.08	0.91
15.42	1.69	10.60	6.59	69.91	2.99	0.07	0.76
15.44	1.38	8.32	8.24	68.60	3.12	0.06	0.59
15.46	1.25	7.34	8.96	65.72	3.18	0.06	0.52
15.48	1.33	7.95	8.02	63.76	3.11	0.06	0.57
15.50	1.57	9.72	6.54	63.60	2.98	0.07	0.69
15.52	1.80	11.35	5.90	66.98	2.92	0.07	0.81
15.54	1.88	11.94	5.89	70.39	2.92	0.07	0.85
15.56	1.85	11.71	6.28	73.56	2.96	0.07	0.84
15.58	1.81	11.38	6.52	74.24	2.98	0.07	0.81
15.60	1.80	11.31	6.58	74.45	2.99	0.07	0.81
15.62	1.72	10.68	6.95	74.17	3.02	0.07	0.76

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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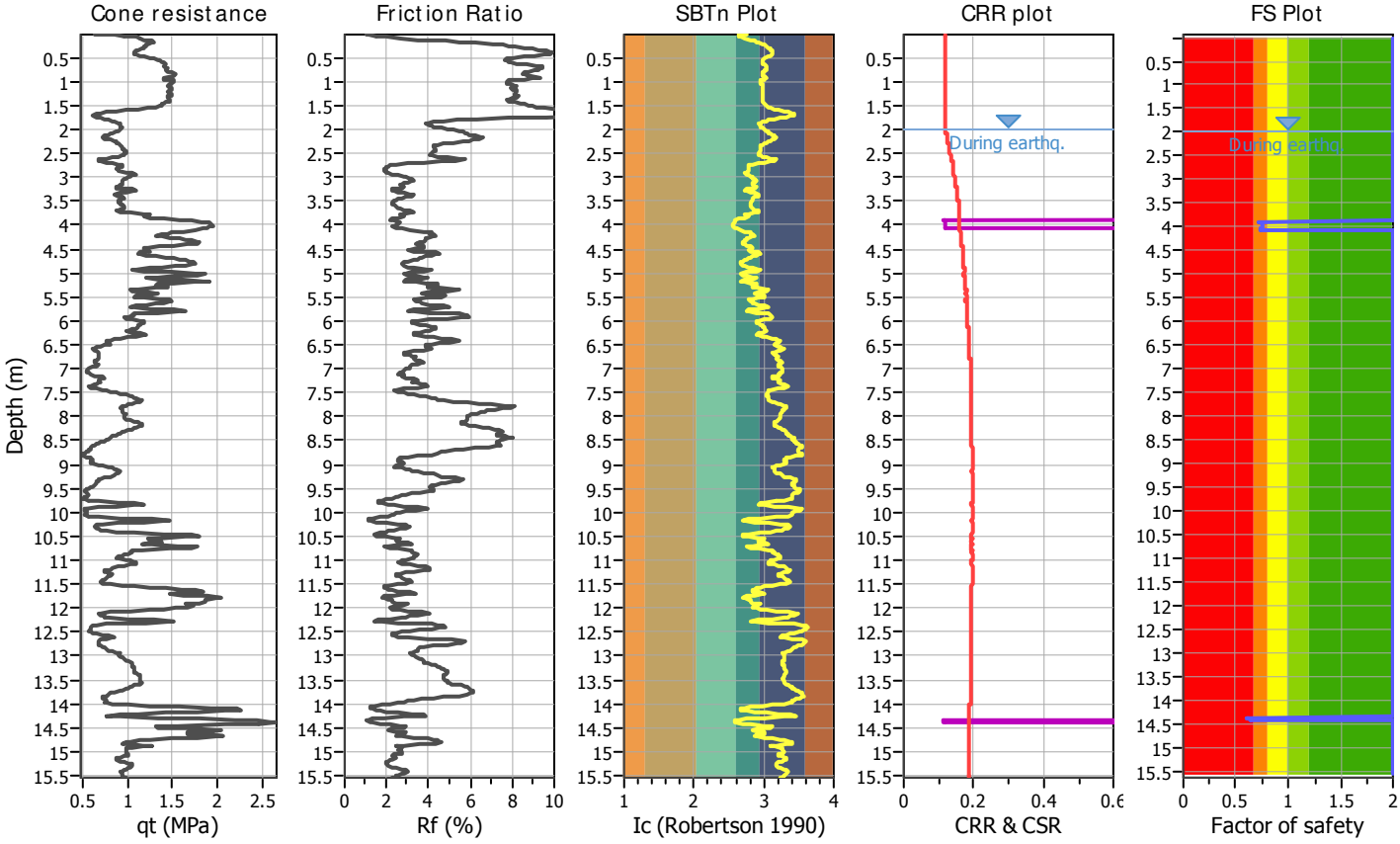
LIQUEFACTION ANALYSIS REPORT

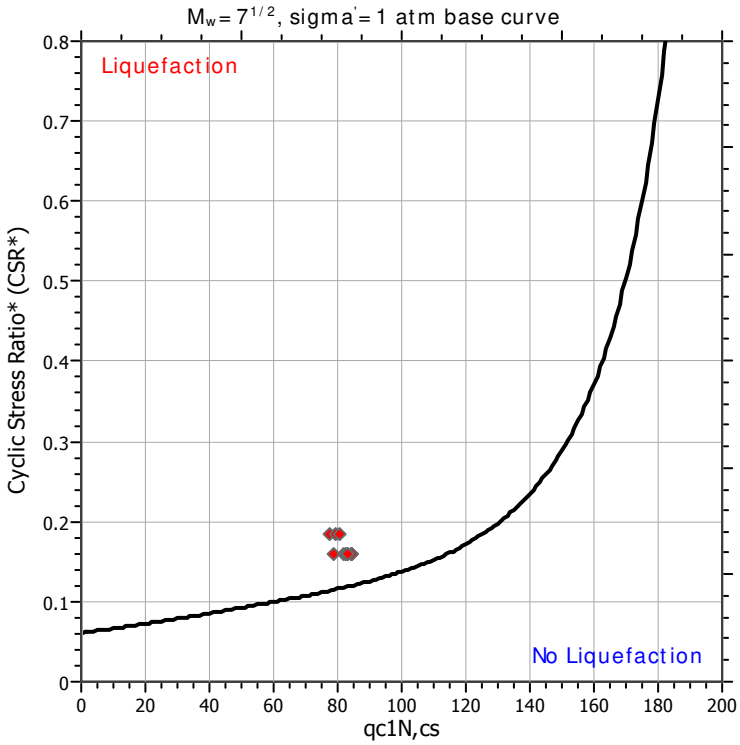
Project title : Location :

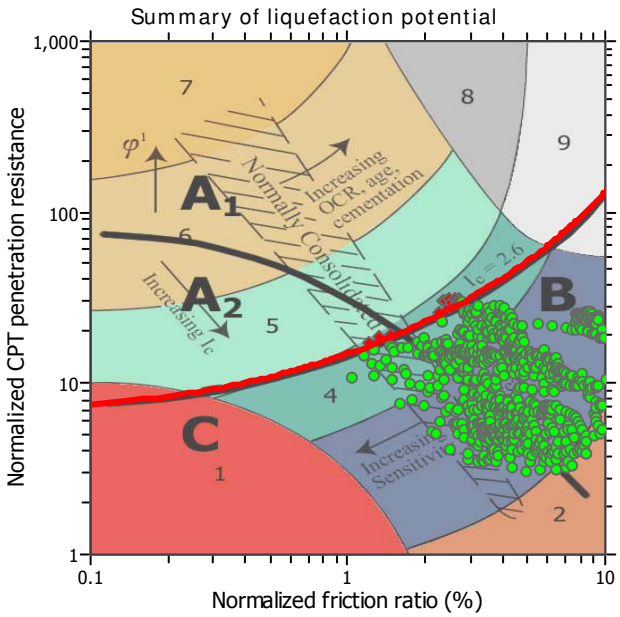
CPT file : Cptu-2

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.50 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.22	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

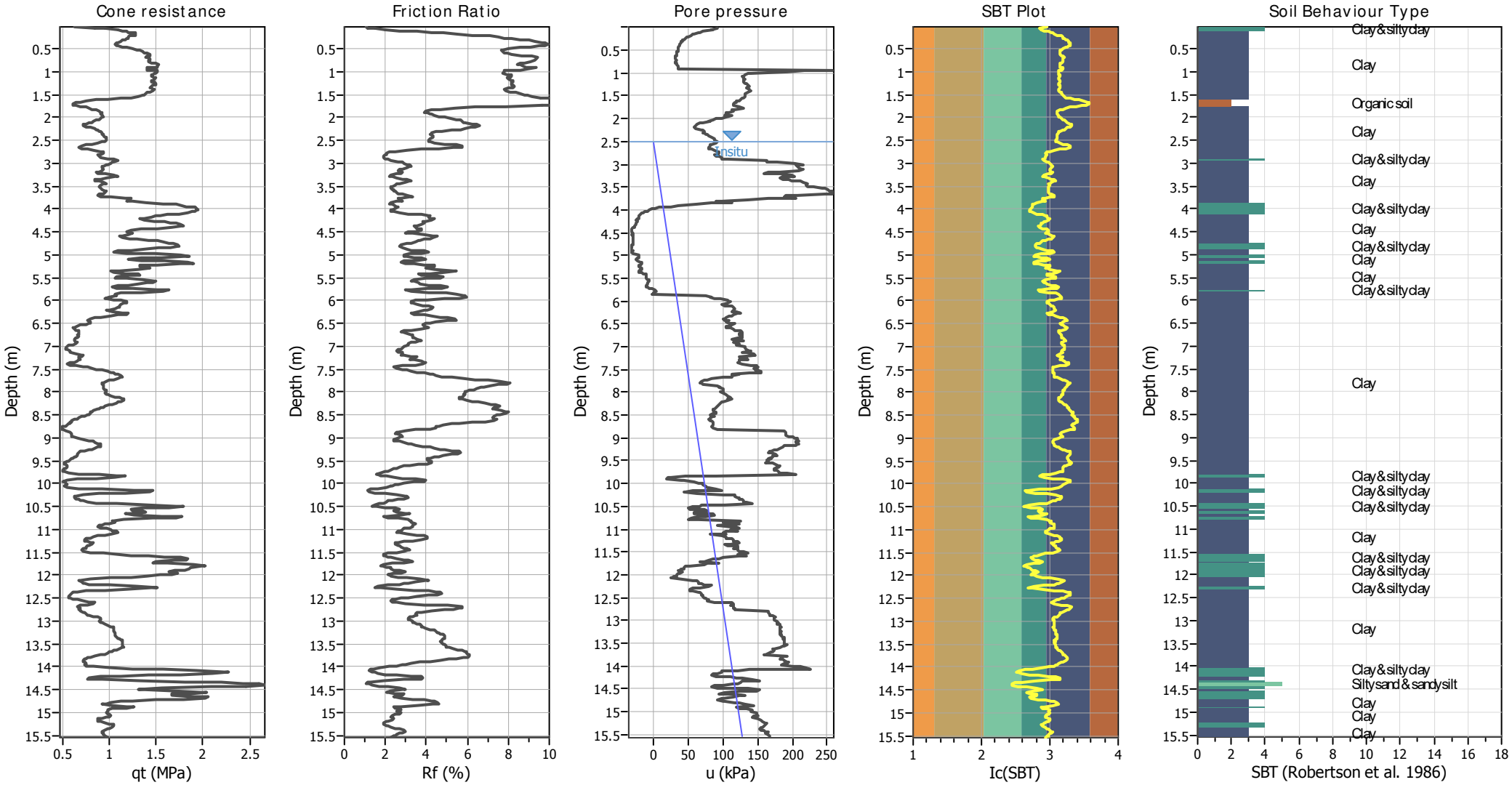






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



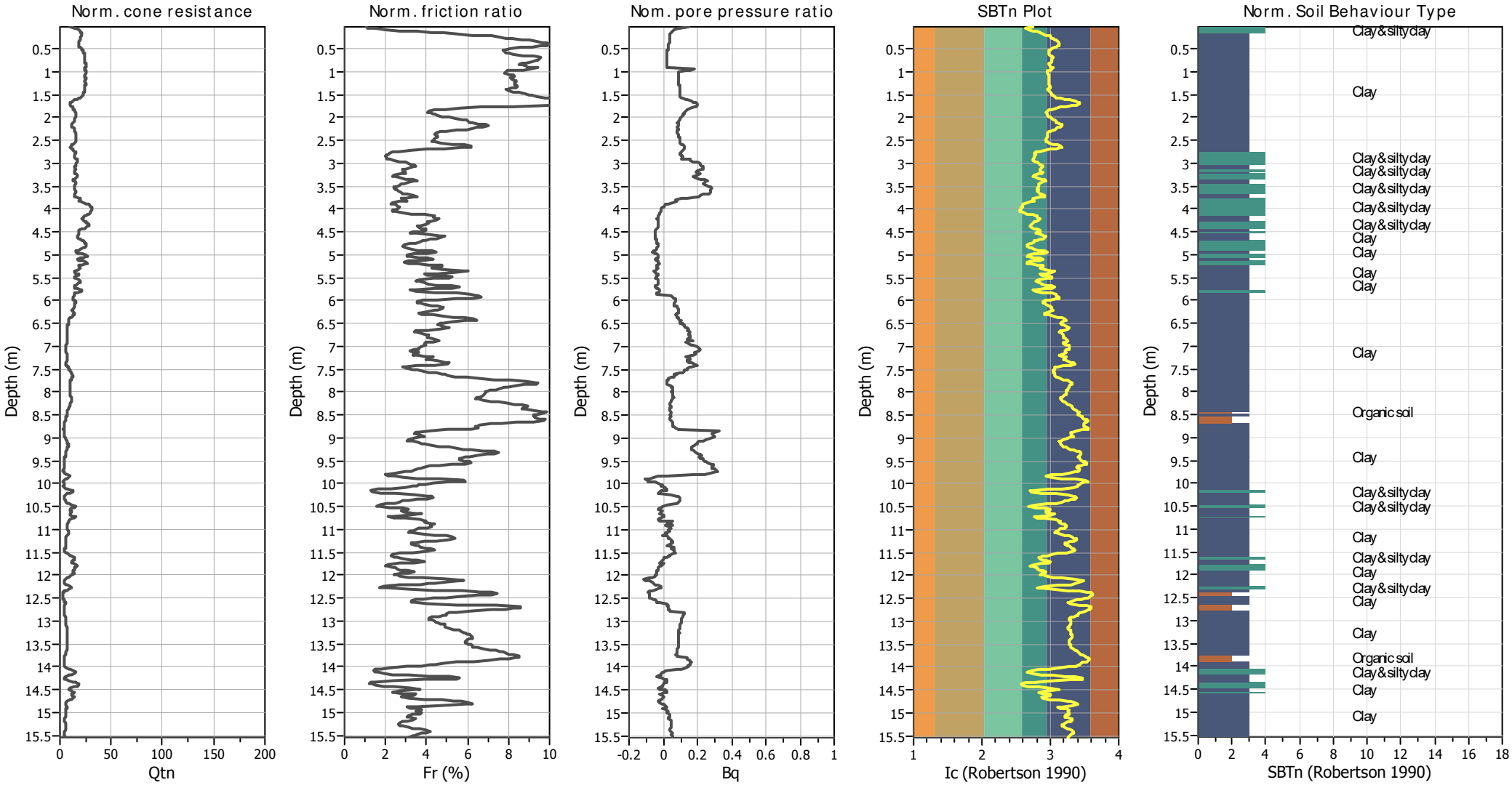
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained	4. Clayey silt to silty	7. Gravely sand to sand
2. Organic material	5. Silty sand to sandy silt	8. Very stiff sand to
3. Clay to silty clay	6. Clean sand to silty sand	9. Very stiff fine grained

CPT basic interpretation plots (normalized)



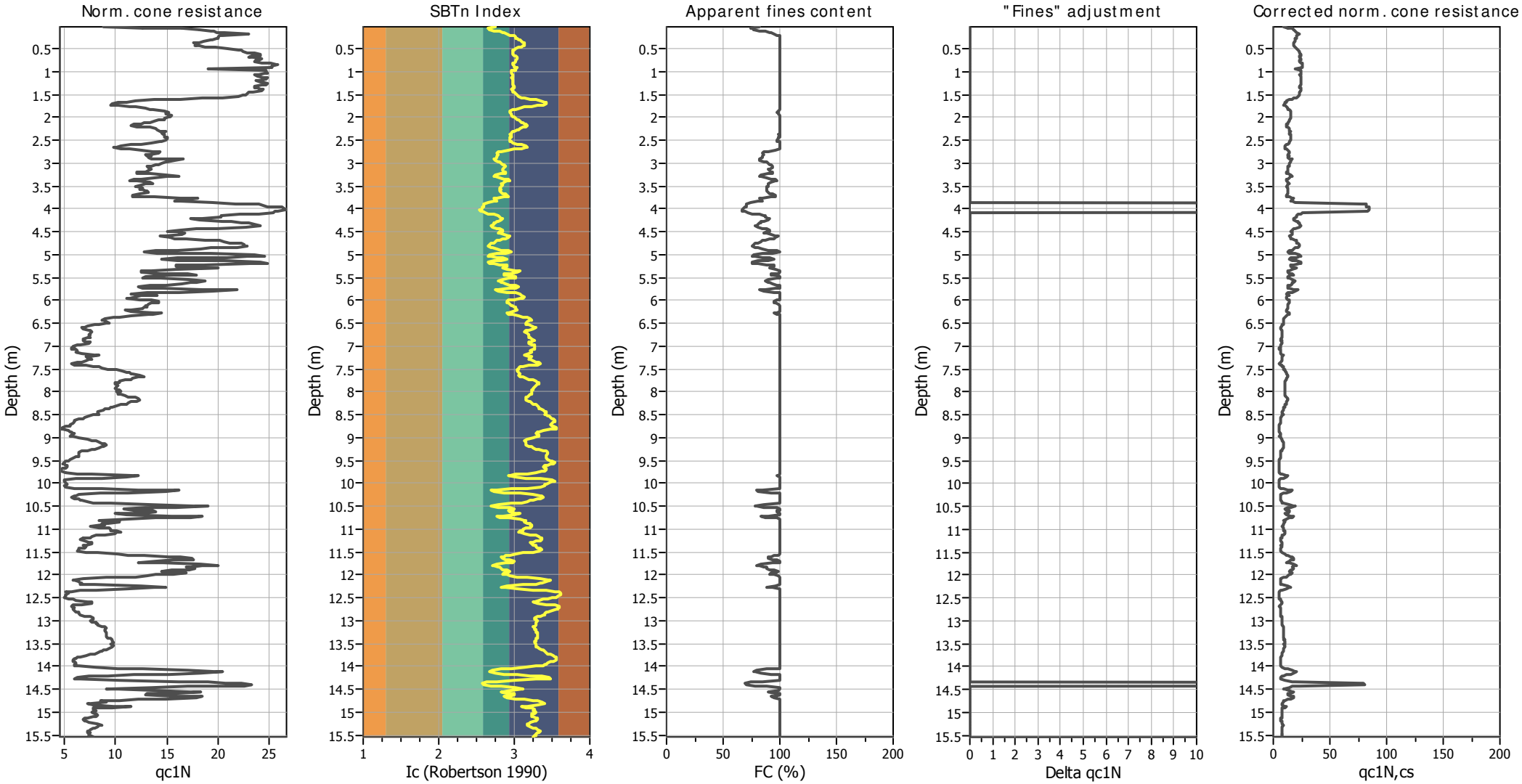
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

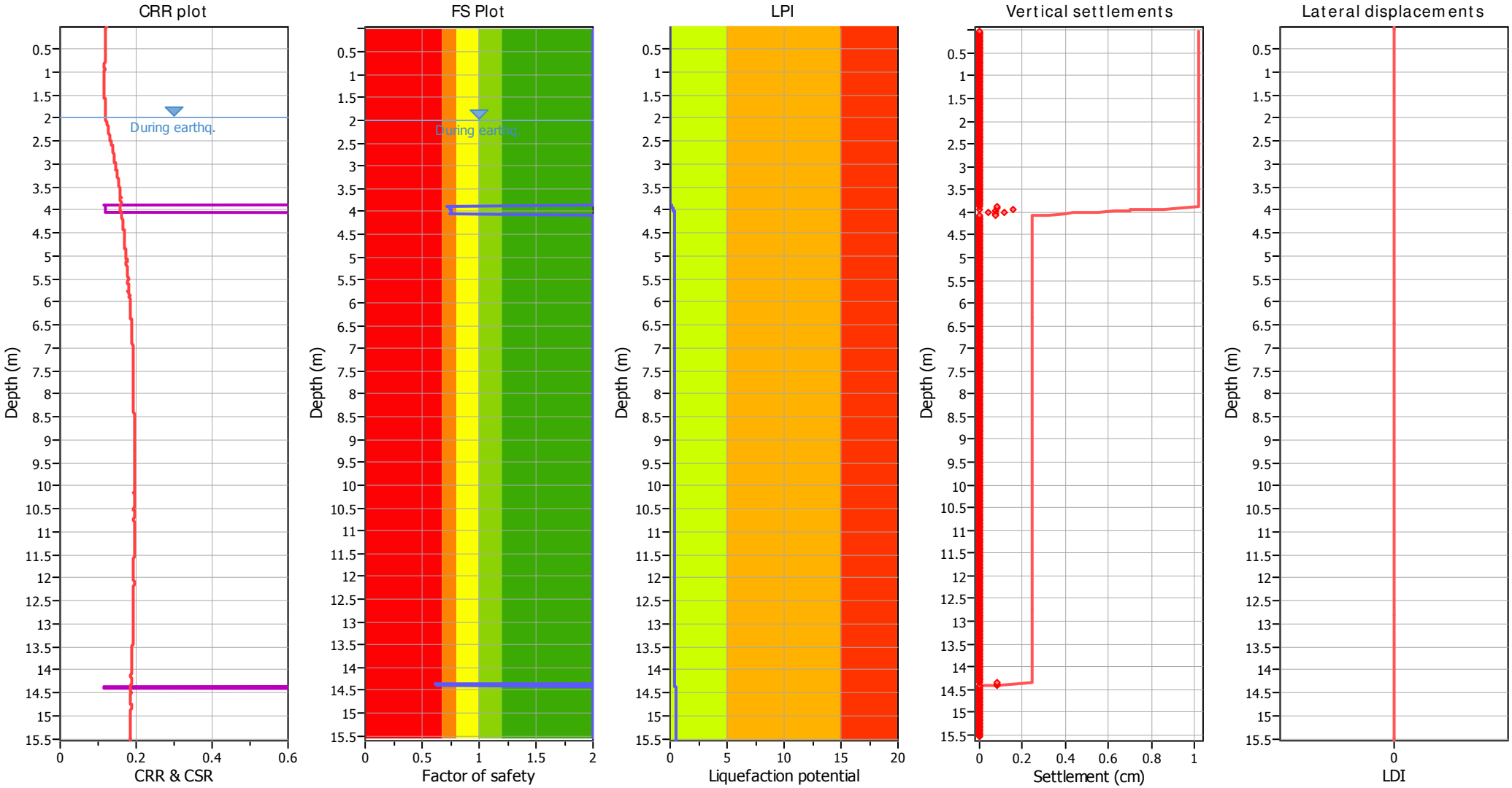
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

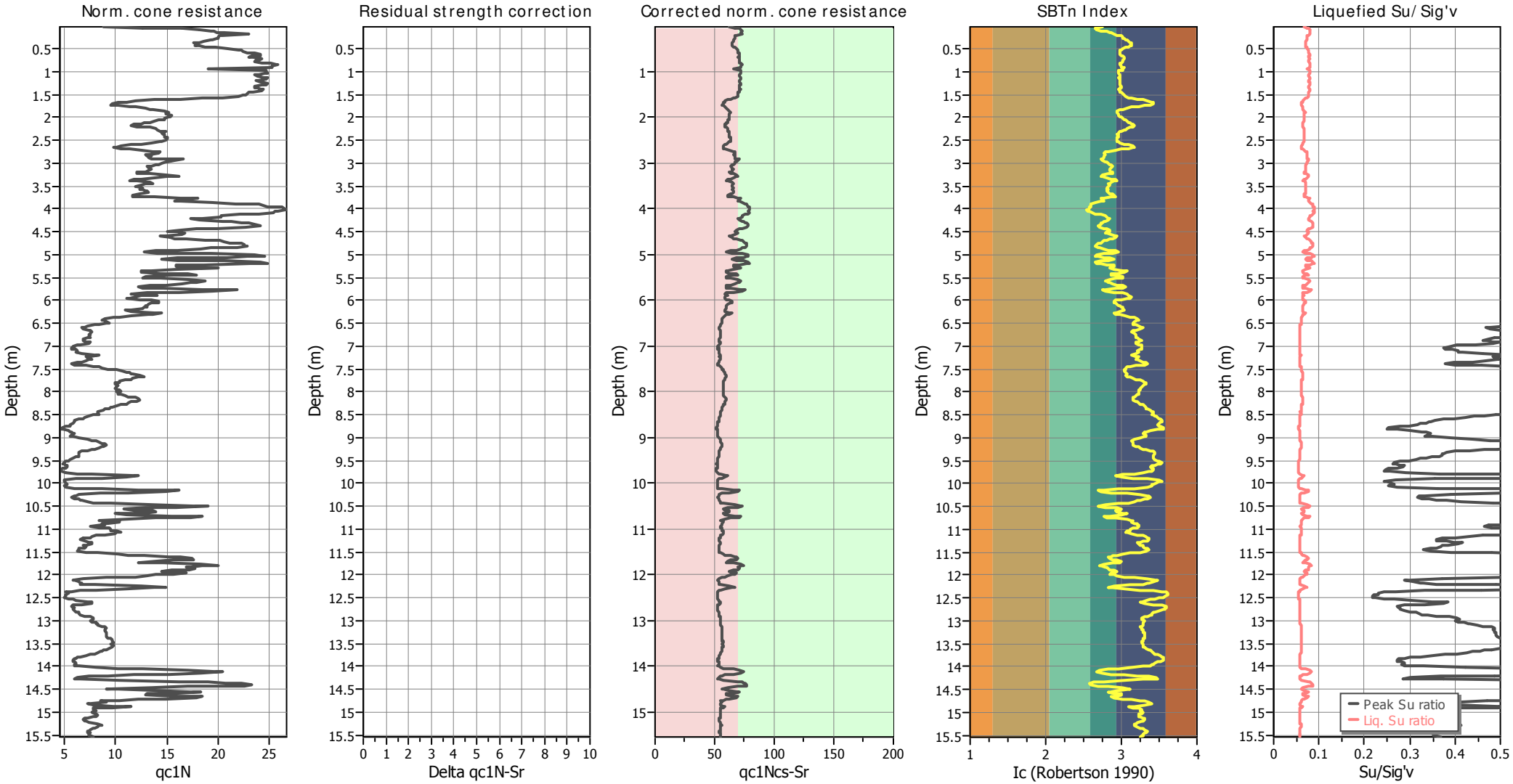
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

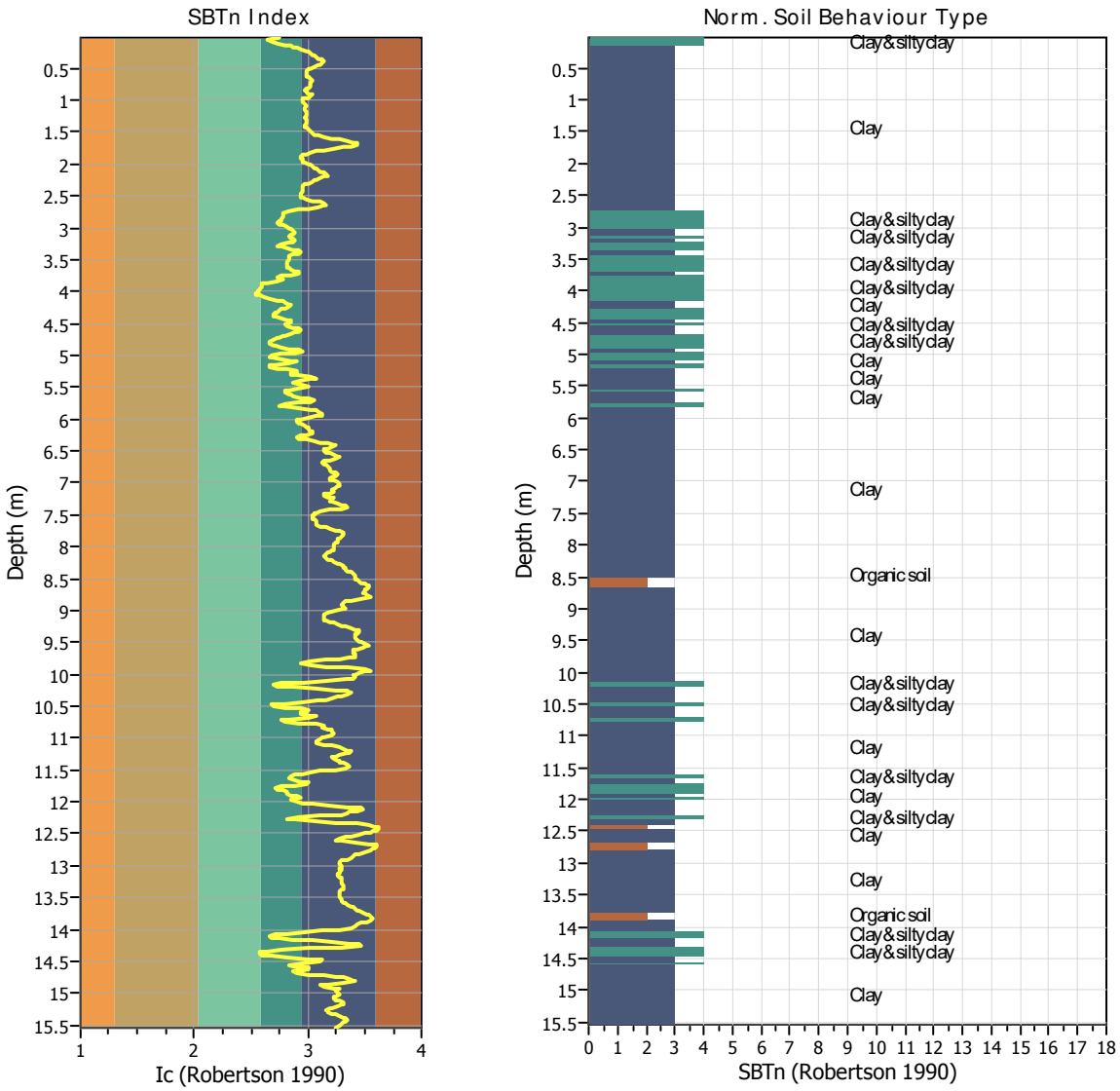
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	777
I_c maximum check value:	3.00	Total points excluded:	0
I_c change ratio value:	0.0100	Exclusion percentage:	0.00%
Minimum number of points in layer:	4	Number of layers detected:	0

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.53	5.98	91.82	42.82	14.95
2	0.04	0.75	7.45	84.07	37.63	15.55
3	0.06	0.98	14.51	84.75	38.01	16.02
4	0.08	1.08	20.43	70.68	39.16	16.55
5	0.10	1.15	29.57	67.02	42.30	16.98
6	0.13	1.17	42.14	63.36	45.92	17.34
7	0.14	1.19	53.33	58.52	48.64	17.60
8	0.16	1.23	59.28	54.74	49.57	17.82
9	0.18	1.37	71.29	54.12	51.79	17.98
10	0.20	1.22	80.40	48.98	54.37	18.12
11	0.22	1.20	87.20	47.12	57.94	18.19
12	0.24	1.20	91.74	46.13	59.15	18.24
13	0.26	1.20	92.89	42.84	60.12	18.28
14	0.28	1.18	96.61	40.67	61.27	18.31
15	0.30	1.16	100.83	40.05	62.68	18.35
16	0.32	1.15	104.46	38.87	64.16	18.37
17	0.35	1.11	104.31	38.07	65.36	18.38
18	0.36	1.09	104.31	37.63	66.83	18.37
19	0.38	1.05	105.89	36.83	67.57	18.38
20	0.40	1.07	106.57	36.08	68.06	18.38
21	0.42	1.06	105.57	34.72	67.51	18.38
22	0.44	1.08	104.39	34.72	66.59	18.37
23	0.46	1.12	102.81	34.35	64.78	18.37
24	0.48	1.18	102.19	35.59	62.42	18.37
25	0.50	1.24	99.53	34.90	59.92	18.37
26	0.52	1.31	98.76	34.84	58.34	18.39
27	0.54	1.33	103.01	32.98	57.69	18.42
28	0.56	1.34	104.62	32.11	57.69	18.45
29	0.58	1.36	106.84	31.87	57.41	18.49
30	0.60	1.40	110.06	31.93	57.26	18.54
31	0.62	1.44	117.88	31.99	57.54	18.61
32	0.64	1.44	123.62	31.37	58.87	18.67
33	0.66	1.38	129.59	30.25	60.34	18.70
34	0.68	1.37	131.65	30.25	61.31	18.73
35	0.70	1.40	133.12	31.00	61.00	18.75
36	0.72	1.45	135.37	31.93	60.60	18.76
37	0.74	1.43	134.58	31.37	60.35	18.76
38	0.76	1.41	131.40	30.94	60.43	18.74
39	0.78	1.41	129.28	31.06	59.91	18.72
40	0.80	1.44	127.37	32.36	58.92	18.71
41	0.82	1.49	127.28	33.54	57.71	18.72
42	0.84	1.53	129.03	34.66	57.07	18.74
43	0.86	1.54	131.37	35.15	57.27	18.76
44	0.88	1.51	133.57	35.03	57.91	18.77
45	0.90	1.49	133.96	35.52	58.31	18.78
46	0.92	1.50	133.13	36.02	61.04	18.72
47	0.94	1.14	124.98	257.47	60.05	18.68
48	0.96	1.47	118.42	217.30	59.20	18.63

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.47	118.01	191.63	55.80	18.63
50	1.00	1.47	117.71	139.06	55.72	18.62
51	1.02	1.48	115.54	134.53	55.69	18.61
52	1.04	1.46	114.19	130.94	55.95	18.60
53	1.06	1.43	114.72	129.45	56.73	18.60
54	1.08	1.41	117.44	128.08	57.52	18.61
55	1.10	1.42	119.76	128.89	57.58	18.63
56	1.12	1.45	119.34	130.13	56.98	18.64
57	1.14	1.48	119.11	131.43	56.41	18.64
58	1.16	1.47	118.78	130.13	56.65	18.64
59	1.18	1.43	119.57	129.20	57.36	18.64
60	1.20	1.41	120.45	128.70	57.75	18.63
61	1.22	1.43	118.95	130.87	57.69	18.64
62	1.24	1.44	120.82	133.48	57.19	18.65
63	1.26	1.48	121.90	135.90	56.97	18.66
64	1.28	1.47	121.58	137.01	56.98	18.67
65	1.30	1.45	121.66	136.02	57.58	18.65
66	1.32	1.40	120.10	134.22	58.07	18.64
67	1.34	1.40	118.37	134.41	58.03	18.61
68	1.36	1.42	115.61	137.01	57.32	18.60
69	1.38	1.44	113.73	138.25	56.62	18.59
70	1.40	1.46	114.67	139.43	56.33	18.59
71	1.42	1.45	115.19	135.28	56.79	18.59
72	1.44	1.40	115.13	131.68	57.78	18.59
73	1.46	1.37	117.09	130.63	58.98	18.60
74	1.48	1.36	120.01	131.99	59.82	18.61
75	1.50	1.35	121.12	132.30	60.46	18.63
76	1.52	1.34	122.23	131.12	61.04	18.63
77	1.54	1.31	121.20	130.13	62.38	18.60
78	1.56	1.21	117.92	126.22	64.73	18.56
79	1.58	1.10	114.60	125.17	68.47	18.48
80	1.60	0.97	110.32	123.43	73.70	18.40
81	1.62	0.82	106.48	119.28	79.77	18.29
82	1.64	0.71	100.00	117.85	85.57	18.19
83	1.66	0.66	95.69	116.37	89.88	18.09
84	1.68	0.61	91.26	115.19	92.24	18.00
85	1.70	0.58	83.93	114.38	92.48	17.87
86	1.72	0.57	71.74	114.07	88.92	17.73
87	1.74	0.61	62.07	122.63	82.05	17.58
88	1.76	0.68	53.48	128.89	75.14	17.44
89	1.78	0.71	47.71	130.19	68.47	17.31
90	1.80	0.77	40.88	117.48	63.83	17.20
91	1.82	0.80	38.13	113.39	60.19	17.11
92	1.84	0.81	36.31	114.32	57.31	17.06
93	1.86	0.88	34.43	109.05	55.17	17.04
94	1.88	0.90	35.07	104.90	54.18	17.06
95	1.90	0.89	37.39	105.08	54.68	17.11
96	1.92	0.89	38.27	101.80	55.38	17.13

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	0.89	38.11	113.21	55.37	17.17
98	1.96	0.93	40.60	103.35	55.87	17.22
99	1.98	0.91	43.32	96.96	56.66	17.29
100	2.00	0.91	44.87	90.39	58.33	17.34
101	2.02	0.88	47.10	85.06	59.71	17.38
102	2.05	0.88	48.92	79.85	61.40	17.41
103	2.06	0.85	49.53	79.91	62.66	17.41
104	2.08	0.82	48.27	71.36	63.80	17.38
105	2.10	0.80	46.78	66.27	64.92	17.33
106	2.12	0.76	45.55	63.05	66.14	17.30
107	2.14	0.75	46.40	60.88	68.37	17.29
108	2.16	0.70	47.54	60.69	70.18	17.29
109	2.18	0.69	46.66	58.83	71.02	17.29
110	2.20	0.72	47.13	57.97	69.05	17.32
111	2.22	0.80	48.94	60.63	66.49	17.38
112	2.24	0.84	51.29	69.13	64.21	17.42
113	2.26	0.85	49.47	69.68	62.74	17.41
114	2.28	0.86	46.13	72.29	60.90	17.34
115	2.30	0.87	41.99	70.92	58.47	17.26
116	2.32	0.92	39.62	73.47	56.96	17.21
117	2.34	0.90	40.09	74.15	55.79	17.18
118	2.36	0.91	38.21	75.82	55.57	17.18
119	2.38	0.93	39.21	78.12	55.29	17.19
120	2.40	0.93	41.29	82.02	55.55	17.23
121	2.42	0.93	41.70	83.82	55.51	17.26
122	2.44	0.95	41.87	87.17	55.03	17.26
123	2.46	0.95	40.58	88.10	54.55	17.24
124	2.48	0.95	40.02	87.29	54.19	17.23
125	2.50	0.96	39.96	91.26	54.36	17.21
126	2.52	0.93	39.64	91.32	54.33	17.19
127	2.54	0.92	37.56	89.15	55.54	17.16
128	2.56	0.87	38.67	83.14	57.77	17.15
129	2.58	0.80	40.64	81.77	61.74	17.16
130	2.60	0.73	41.54	80.66	65.86	17.15
131	2.62	0.68	40.84	79.54	69.07	17.11
132	2.64	0.65	38.64	79.48	70.44	17.02
133	2.66	0.63	34.83	79.73	68.87	16.93
134	2.68	0.67	32.08	84.00	64.78	16.83
135	2.70	0.74	28.97	86.92	58.78	16.74
136	2.72	0.82	24.69	90.64	52.86	16.64
137	2.74	0.89	22.38	92.62	47.98	16.53
138	2.76	0.94	20.44	94.05	45.26	16.45
139	2.78	0.93	19.27	91.44	44.62	16.37
140	2.80	0.87	18.27	87.54	45.00	16.28
141	2.82	0.85	16.98	88.72	45.22	16.21
142	2.84	0.86	16.52	94.30	44.55	16.19
143	2.86	0.89	16.87	98.76	44.30	16.19
144	2.88	0.87	17.13	98.76	44.40	16.24

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.89	18.45	105.83	42.86	16.38
146	2.92	1.11	22.33	162.24	42.31	16.56
147	2.94	1.05	24.94	163.61	42.74	16.72
148	2.96	1.00	27.66	177.68	45.18	16.81
149	2.98	0.99	29.13	202.85	46.89	16.87
150	3.01	0.97	29.74	215.93	47.85	16.89
151	3.02	0.95	29.98	205.15	49.14	16.92
152	3.04	0.93	31.76	206.20	50.26	16.92
153	3.06	0.90	30.62	206.88	51.28	16.91
154	3.08	0.88	29.89	208.37	51.23	16.85
155	3.10	0.88	28.10	213.45	50.42	16.80
156	3.12	0.90	26.31	215.13	49.13	16.73
157	3.14	0.90	25.05	208.18	48.44	16.68
158	3.16	0.89	24.44	181.96	48.59	16.64
159	3.18	0.87	24.00	164.48	49.85	16.61
160	3.20	0.81	24.17	159.14	51.00	16.60
161	3.22	0.81	24.64	182.46	50.49	16.62
162	3.24	0.90	24.52	197.83	47.55	16.64
163	3.26	1.01	24.11	203.04	43.69	16.66
164	3.28	1.11	23.38	185.31	42.48	16.68
165	3.30	1.02	24.96	182.77	43.65	16.70
166	3.32	0.94	25.69	186.61	46.99	16.69
167	3.34	0.85	24.82	194.79	50.09	16.67
168	3.36	0.81	25.72	198.26	53.04	16.69
169	3.38	0.78	28.21	210.48	54.19	16.74
170	3.40	0.83	28.89	215.44	52.78	16.79
171	3.42	0.92	27.98	220.71	49.96	16.78
172	3.44	0.94	26.19	219.40	48.19	16.73
173	3.46	0.89	24.32	218.85	47.86	16.63
174	3.48	0.86	22.32	222.57	48.30	16.53
175	3.50	0.82	20.57	230.13	48.01	16.43
176	3.52	0.84	19.60	242.16	47.26	16.39
177	3.54	0.87	20.10	247.99	46.91	16.42
178	3.56	0.86	21.56	250.84	46.89	16.47
179	3.58	0.88	22.12	253.32	47.15	16.53
180	3.60	0.90	22.94	256.66	46.87	16.57
181	3.62	0.91	23.67	256.73	46.85	16.62
182	3.64	0.92	24.70	256.79	47.64	16.63
183	3.66	0.86	24.23	246.00	48.60	16.64
184	3.68	0.87	24.43	206.32	50.73	16.65
185	3.70	0.82	26.72	189.40	52.73	16.72
186	3.72	0.82	29.59	188.53	52.90	16.86
187	3.74	0.97	33.52	204.22	49.44	16.99
188	3.76	1.16	33.52	165.59	44.36	17.05
189	3.78	1.28	30.56	135.21	42.37	17.08
190	3.80	1.20	33.81	97.77	42.96	17.08
191	3.82	1.12	34.40	89.34	44.54	17.10
192	3.84	1.16	32.90	113.08	41.93	17.07

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	1.40	29.41	83.88	37.83	17.08
194	3.88	1.56	31.55	62.00	35.19	17.23
195	3.90	1.74	42.20	34.78	34.85	17.45
196	3.94	1.81	47.24	24.30	34.89	17.63
197	3.94	1.90	49.46	7.56	34.72	17.71
198	3.96	1.92	50.87	1.74	34.38	17.74
199	3.98	1.93	49.81	-2.54	33.80	17.71
200	4.01	1.96	45.62	-6.88	33.05	17.65
201	4.02	1.95	42.72	-10.04	32.63	17.59
202	4.04	1.90	42.87	-12.83	32.99	17.58
203	4.06	1.88	45.10	-15.44	33.96	17.62
204	4.08	1.87	48.58	-17.30	35.74	17.71
205	4.10	1.76	54.76	-19.47	38.50	17.81
206	4.13	1.64	60.86	-21.20	42.40	17.90
207	4.14	1.49	66.57	-22.75	45.01	17.93
208	4.16	1.50	62.64	-22.69	45.87	17.90
209	4.18	1.50	57.84	-23.00	46.09	17.82
210	4.20	1.36	56.70	-24.92	47.75	17.78
211	4.22	1.28	59.04	-25.67	49.22	17.76
212	4.24	1.34	57.43	-24.86	47.96	17.79
213	4.26	1.52	58.86	-24.61	45.50	17.82
214	4.28	1.58	59.39	-25.29	43.74	17.89
215	4.30	1.67	64.78	-26.10	43.16	17.97
216	4.32	1.72	68.70	-26.84	42.57	18.03
217	4.34	1.77	67.61	-27.59	41.62	18.04
218	4.36	1.82	63.80	-28.46	40.47	17.99
219	4.38	1.81	59.91	-29.20	40.17	17.93
220	4.40	1.71	57.82	-30.25	41.52	17.84
221	4.42	1.49	54.57	-31.68	43.92	17.73
222	4.44	1.34	49.06	-32.67	46.88	17.61
223	4.46	1.23	47.65	-33.54	48.81	17.46
224	4.48	1.13	40.47	-32.30	48.59	17.33
225	4.50	1.21	35.11	-30.13	46.88	17.21
226	4.52	1.25	35.81	-30.13	45.60	17.23
227	4.54	1.26	40.38	-30.56	46.84	17.35
228	4.56	1.24	47.01	-31.62	50.36	17.48
229	4.58	1.11	53.16	-31.25	53.27	17.52
230	4.60	1.08	48.21	-29.76	54.69	17.54
231	4.62	1.16	50.49	-29.88	53.32	17.53
232	4.64	1.20	50.20	-29.51	51.43	17.57
233	4.66	1.29	50.96	-29.82	48.85	17.61
234	4.68	1.44	51.63	-29.94	46.35	17.68
235	4.70	1.54	55.06	-30.19	44.60	17.74
236	4.72	1.58	56.12	-30.75	43.48	17.77
237	4.74	1.62	54.01	-31.25	41.90	17.76
238	4.76	1.72	50.55	-31.43	40.15	17.71
239	4.78	1.75	48.35	-31.80	38.73	17.66
240	4.80	1.75	46.62	-32.42	38.16	17.64

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	1.77	46.98	-32.92	38.30	17.62
242	4.84	1.70	46.42	-33.54	40.05	17.61
243	4.86	1.50	47.86	-34.66	41.22	17.48
244	4.88	1.42	34.75	-31.06	44.39	17.40
245	4.90	1.24	42.75	-33.73	47.80	17.33
246	4.92	1.07	43.84	-34.41	53.51	17.35
247	4.94	0.99	42.23	-33.54	55.54	17.33
248	4.96	1.09	42.43	-29.88	51.10	17.42
249	4.98	1.50	49.35	-23.06	44.00	17.56
250	5.00	1.85	48.65	-21.70	39.44	17.73
251	5.03	1.94	55.36	-21.64	38.38	17.80
252	5.04	1.80	56.03	-22.57	39.84	17.80
253	5.06	1.64	51.46	-23.87	44.06	17.72
254	5.08	1.25	50.93	-25.98	48.77	17.60
255	5.10	1.13	47.30	-25.91	52.00	17.52
256	5.13	1.26	46.04	-23.62	47.68	17.51
257	5.14	1.63	45.24	-19.90	41.68	17.59
258	5.16	1.91	49.40	-18.72	38.42	17.75
259	5.18	1.98	59.04	-18.54	38.59	17.87
260	5.20	1.84	60.74	-19.34	41.95	17.90
261	5.22	1.47	58.14	-21.26	46.97	17.84
262	5.24	1.26	57.67	-22.38	52.07	17.78
263	5.26	1.26	60.42	-21.70	52.21	17.78
264	5.28	1.45	57.46	-18.72	48.62	17.77
265	5.30	1.60	52.63	-18.10	48.77	17.79
266	5.32	1.28	62.71	-20.58	52.55	17.77
267	5.34	1.07	59.34	-21.64	60.18	17.72
268	5.36	0.99	55.12	-21.95	63.20	17.62
269	5.38	1.00	52.33	-17.92	60.55	17.53
270	5.40	1.14	46.27	-15.07	54.56	17.52
271	5.42	1.37	47.38	-12.40	49.61	17.54
272	5.44	1.43	49.40	-11.10	49.88	17.60
273	5.46	1.21	53.77	-12.59	53.97	17.62
274	5.48	1.04	53.50	-12.46	59.27	17.56
275	5.50	1.01	48.35	-12.03	59.24	17.50
276	5.52	1.15	46.88	-10.17	53.64	17.48
277	5.54	1.39	45.62	-8.18	48.27	17.52
278	5.56	1.52	46.50	-7.56	45.76	17.60
279	5.58	1.52	52.68	-8.12	46.17	17.67
280	5.60	1.46	54.21	-8.87	47.67	17.69
281	5.62	1.41	51.39	-9.30	48.78	17.64
282	5.64	1.34	47.47	-10.42	50.48	17.57
283	5.66	1.21	47.85	-11.22	54.09	17.54
284	5.68	1.08	52.39	-11.10	59.31	17.54
285	5.70	0.99	52.80	-9.11	62.33	17.55
286	5.72	1.03	51.04	-6.57	60.25	17.54
287	5.74	1.20	49.72	-2.60	53.27	17.58
288	5.76	1.52	50.08	0.43	45.79	17.62

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	1.81	47.41	2.42	42.80	17.65
290	5.80	1.60	49.32	1.30	44.89	17.70
291	5.82	1.33	57.64	-0.68	52.19	17.70
292	5.84	1.07	56.61	-1.98	60.39	17.65
293	5.86	0.95	52.89	-2.36	63.66	17.69
294	5.88	1.16	65.58	74.52	65.11	17.74
295	5.90	1.03	65.26	82.89	65.01	17.79
296	5.92	0.99	59.28	81.84	67.37	17.69
297	5.94	0.93	53.60	86.24	67.29	17.55
298	5.96	0.91	47.68	94.67	64.15	17.42
299	5.98	1.03	40.76	105.58	58.94	17.30
300	6.00	1.12	37.86	108.80	53.93	17.25
301	6.02	1.18	38.39	111.10	51.83	17.24
302	6.04	1.18	38.48	106.70	51.93	17.25
303	6.06	1.12	38.39	100.19	53.01	17.25
304	6.08	1.10	39.03	98.45	54.73	17.27
305	6.10	1.09	42.20	101.36	56.45	17.34
306	6.12	1.08	46.56	112.71	57.84	17.42
307	6.14	1.09	48.14	114.69	58.91	17.47
308	6.16	1.07	48.35	117.23	59.22	17.46
309	6.18	1.06	45.95	117.36	60.02	17.39
310	6.20	0.97	40.59	113.76	60.64	17.26
311	6.22	0.92	36.04	112.21	60.78	17.16
312	6.24	0.97	37.10	119.28	57.60	17.16
313	6.26	1.15	38.62	125.91	53.84	17.22
314	6.28	1.22	37.80	120.46	52.33	17.27
315	6.30	1.15	40.85	115.00	53.43	17.30
316	6.32	1.11	42.35	112.71	57.76	17.35
317	6.34	0.97	45.25	107.32	61.83	17.31
318	6.36	0.88	40.97	103.91	66.64	17.27
319	6.38	0.83	41.47	101.80	71.05	17.23
320	6.40	0.75	44.92	100.68	74.60	17.23
321	6.42	0.74	42.64	101.80	76.15	17.18
322	6.44	0.74	38.10	109.18	74.09	17.09
323	6.46	0.77	34.93	103.41	70.93	17.01
324	6.48	0.80	33.73	107.63	69.01	16.94
325	6.50	0.77	31.39	116.24	68.85	16.85
326	6.52	0.72	28.58	112.46	70.07	16.73
327	6.54	0.68	25.97	108.87	72.65	16.63
328	6.56	0.62	25.44	104.46	75.28	16.55
329	6.58	0.60	25.18	104.65	78.56	16.53
330	6.60	0.57	25.65	110.35	79.36	16.50
331	6.62	0.59	24.27	114.26	76.84	16.44
332	6.64	0.64	20.82	117.48	72.60	16.34
333	6.66	0.65	18.88	124.43	68.89	16.25
334	6.68	0.66	18.88	128.02	67.95	16.23
335	6.70	0.66	19.21	127.40	68.46	16.25
336	6.72	0.65	20.18	123.62	70.43	16.31

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	0.63	22.26	123.37	71.70	16.36
338	6.76	0.64	22.26	126.72	72.56	16.41
339	6.78	0.64	22.61	127.22	72.00	16.40
340	6.80	0.65	21.76	126.16	72.41	16.38
341	6.82	0.63	21.44	121.57	74.02	16.36
342	6.84	0.59	22.03	112.77	75.94	16.39
343	6.86	0.61	23.93	129.14	77.75	16.42
344	6.88	0.59	23.72	122.13	76.95	16.44
345	6.90	0.62	22.61	114.26	74.91	16.41
346	6.92	0.66	21.59	121.70	72.56	16.36
347	6.95	0.64	20.30	123.00	72.99	16.29
348	6.96	0.57	19.27	123.12	75.42	16.19
349	6.98	0.54	17.66	119.40	78.55	16.06
350	7.00	0.51	15.76	130.56	78.65	15.96
351	7.02	0.53	14.94	132.18	78.86	15.87
352	7.04	0.50	14.58	130.38	79.08	15.87
353	7.06	0.50	15.55	134.16	78.61	15.86
354	7.08	0.54	14.58	137.07	76.32	15.85
355	7.10	0.55	13.85	139.49	74.35	15.84
356	7.13	0.55	14.85	127.53	75.26	15.90
357	7.14	0.54	16.61	132.55	75.84	16.02
358	7.16	0.59	18.51	143.71	72.53	16.15
359	7.18	0.70	19.45	147.12	68.08	16.26
360	7.20	0.74	20.18	143.52	68.10	16.38
361	7.22	0.66	23.79	122.63	71.72	16.45
362	7.24	0.62	24.34	124.12	75.17	16.46
363	7.26	0.64	22.26	134.47	73.99	16.42
364	7.28	0.67	21.06	135.15	72.54	16.40
365	7.30	0.66	22.70	123.87	73.97	16.46
366	7.32	0.63	25.93	123.19	77.33	16.50
367	7.34	0.60	24.40	122.07	80.51	16.47
368	7.36	0.56	22.30	121.76	84.07	16.37
369	7.38	0.50	21.62	126.16	85.42	16.29
370	7.40	0.53	20.25	139.43	81.09	16.23
371	7.42	0.63	18.22	148.73	72.97	16.18
372	7.45	0.70	17.08	148.85	66.06	16.16
373	7.46	0.75	17.49	150.03	63.51	16.23
374	7.48	0.77	20.39	144.14	62.93	16.41
375	7.50	0.83	24.82	150.59	62.60	16.61
376	7.52	0.90	28.22	146.56	61.73	16.79
377	7.54	0.95	31.24	153.63	61.43	16.97
378	7.56	0.99	37.10	154.49	61.78	17.12
379	7.58	1.02	40.38	137.38	62.76	17.26
380	7.60	1.03	44.42	113.02	63.50	17.36
381	7.62	1.05	47.03	123.93	63.47	17.45
382	7.64	1.12	50.05	113.45	63.08	17.55
383	7.66	1.15	54.44	112.40	63.87	17.64
384	7.68	1.10	58.93	99.26	66.46	17.72

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	1.06	63.14	83.38	69.80	17.79
386	7.72	1.04	67.01	76.32	73.11	17.84
387	7.74	0.99	70.23	73.53	76.55	17.89
388	7.76	0.94	74.31	68.07	79.80	17.92
389	7.78	0.93	76.53	67.08	82.23	17.94
390	7.80	0.91	75.62	68.94	82.95	17.93
391	7.82	0.90	72.90	69.75	82.90	17.90
392	7.84	0.92	71.72	71.42	81.11	17.85
393	7.86	0.94	65.78	90.64	79.73	17.80
394	7.88	0.92	64.05	95.60	78.48	17.75
395	7.90	0.92	62.09	92.62	78.53	17.72
396	7.92	0.91	61.65	100.00	77.69	17.70
397	7.94	0.94	59.86	100.50	76.64	17.68
398	7.96	0.95	58.80	100.68	75.38	17.67
399	7.99	0.96	58.42	100.12	75.20	17.64
400	8.00	0.93	56.34	95.72	75.06	17.62
401	8.02	0.94	55.61	99.94	75.30	17.61
402	8.04	0.94	56.72	103.35	74.87	17.62
403	8.06	0.96	57.45	103.53	74.26	17.65
404	8.08	1.00	59.59	106.82	72.99	17.69
405	8.10	1.04	60.85	110.79	71.25	17.74
406	8.12	1.10	62.52	110.66	69.64	17.78
407	8.14	1.13	63.60	106.88	68.79	17.83
408	8.16	1.14	66.45	112.90	68.86	17.87
409	8.18	1.14	68.44	106.08	69.90	17.90
410	8.20	1.11	70.02	99.63	71.70	17.93
411	8.22	1.07	73.09	98.33	73.80	17.94
412	8.24	1.05	72.63	95.10	75.68	17.95
413	8.26	1.03	74.21	93.18	77.73	17.95
414	8.28	0.97	74.94	92.99	79.82	17.94
415	8.30	0.94	72.74	91.75	82.10	17.90
416	8.32	0.90	69.66	90.95	82.92	17.84
417	8.34	0.90	66.59	88.72	83.29	17.78
418	8.36	0.88	63.80	86.79	84.04	17.74
419	8.38	0.84	63.68	85.74	85.30	17.71
420	8.40	0.83	62.80	85.37	88.04	17.70
421	8.42	0.78	64.36	86.61	90.17	17.69
422	8.44	0.77	64.00	88.59	91.66	17.68
423	8.46	0.78	62.86	89.27	91.04	17.65
424	8.48	0.78	59.75	84.69	90.85	17.59
425	8.50	0.74	55.88	80.35	91.75	17.52
426	8.52	0.70	53.54	86.98	93.24	17.45
427	8.54	0.70	51.28	84.38	94.99	17.38
428	8.56	0.66	49.03	80.66	96.33	17.32
429	8.58	0.64	47.47	80.29	98.92	17.27
430	8.60	0.61	46.18	79.85	100.00	17.22
431	8.62	0.57	44.95	80.16	100.00	17.14
432	8.64	0.57	39.88	83.38	100.00	17.04

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	0.57	35.99	85.99	100.00	16.91
434	8.68	0.56	32.74	84.62	98.86	16.78
435	8.70	0.55	28.84	85.18	98.44	16.66
436	8.72	0.53	27.02	84.50	97.27	16.54
437	8.74	0.53	24.30	83.76	98.75	16.43
438	8.76	0.49	22.34	82.70	100.00	16.32
439	8.78	0.46	21.25	85.68	100.00	16.21
440	8.80	0.44	19.91	91.07	100.00	16.13
441	8.82	0.47	18.06	94.17	96.29	16.02
442	8.84	0.52	14.81	188.59	88.69	15.95
443	8.86	0.53	15.54	187.60	83.23	15.90
444	8.88	0.55	15.10	189.83	81.62	15.91
445	8.90	0.57	14.69	189.71	80.15	15.91
446	8.92	0.57	15.25	191.20	80.59	15.94
447	8.94	0.55	16.42	189.83	82.55	15.99
448	8.96	0.54	16.89	194.05	83.86	16.03
449	8.98	0.56	17.01	200.06	81.77	16.05
450	9.00	0.61	16.92	201.98	76.60	16.11
451	9.02	0.70	17.86	207.07	71.56	16.16
452	9.05	0.74	18.04	207.44	68.71	16.26
453	9.06	0.77	20.24	208.18	68.00	16.36
454	9.08	0.79	22.29	205.77	68.44	16.49
455	9.10	0.81	24.75	205.89	68.92	16.62
456	9.12	0.83	27.53	208.49	68.93	16.74
457	9.14	0.87	29.50	207.19	68.78	16.83
458	9.16	0.88	30.79	204.96	70.04	16.94
459	9.18	0.86	35.42	187.85	72.18	17.02
460	9.20	0.85	37.03	185.06	75.25	17.08
461	9.22	0.81	37.88	181.84	77.66	17.09
462	9.25	0.78	37.65	176.81	80.52	17.09
463	9.26	0.75	38.06	173.96	83.74	17.08
464	9.28	0.70	38.64	170.18	88.06	17.07
465	9.30	0.65	39.17	166.09	92.01	17.05
466	9.32	0.63	38.14	164.04	94.41	17.02
467	9.34	0.62	36.59	170.24	94.28	16.96
468	9.36	0.62	34.22	174.52	93.18	16.90
469	9.38	0.62	32.26	177.99	91.56	16.81
470	9.40	0.62	29.38	171.05	90.98	16.73
471	9.42	0.60	27.71	170.43	91.38	16.63
472	9.44	0.57	25.95	165.90	91.76	16.54
473	9.46	0.58	23.73	169.37	92.64	16.47
474	9.48	0.55	23.70	165.65	93.82	16.42
475	9.50	0.53	23.49	163.73	96.62	16.39
476	9.52	0.51	22.73	164.72	100.00	16.36
477	9.54	0.49	22.67	161.69	100.00	16.30
478	9.56	0.47	20.97	170.43	100.00	16.23
479	9.58	0.50	18.92	175.39	97.61	16.14
480	9.60	0.51	17.43	180.04	93.21	16.05

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	0.52	16.31	180.78	90.20	15.97
482	9.64	0.53	14.97	179.73	89.03	15.88
483	9.66	0.50	13.85	176.94	89.48	15.76
484	9.68	0.47	12.33	174.21	91.20	15.63
485	9.70	0.46	11.10	173.40	91.24	15.53
486	9.72	0.47	10.87	177.43	90.60	15.45
487	9.74	0.46	10.25	179.54	87.22	15.42
488	9.76	0.51	9.84	182.70	79.96	15.43
489	9.78	0.62	10.25	192.06	70.32	15.56
490	9.80	0.76	11.98	204.15	59.47	16.00
491	9.82	1.18	20.58	89.46	54.73	16.41
492	9.84	1.21	24.86	44.70	53.98	16.70
493	9.86	1.11	26.38	24.61	59.57	16.74
494	9.88	0.86	25.10	18.97	70.15	16.61
495	9.90	0.61	22.19	18.78	85.79	16.43
496	9.92	0.50	21.55	39.93	100.00	16.29
497	9.94	0.50	21.05	42.53	100.00	16.16
498	9.96	0.50	16.66	58.21	100.00	16.04
499	9.98	0.52	15.57	63.67	94.69	15.90
500	10.01	0.54	14.34	70.12	91.32	15.82
501	10.02	0.53	13.38	71.30	90.19	15.74
502	10.04	0.51	12.44	69.81	90.53	15.65
503	10.06	0.50	11.71	73.71	90.12	15.58
504	10.08	0.52	11.35	77.62	84.96	15.55
505	10.10	0.60	10.89	78.67	71.43	15.63
506	10.12	0.87	11.74	89.15	56.06	15.82
507	10.14	1.24	13.41	98.76	44.46	16.10
508	10.16	1.62	16.54	55.11	40.55	16.34
509	10.18	1.51	18.53	45.88	42.07	16.37
510	10.20	1.13	15.52	43.52	50.32	16.34
511	10.22	0.86	18.21	62.62	64.02	16.26
512	10.24	0.64	19.94	99.63	76.74	16.24
513	10.26	0.62	18.04	115.69	84.83	16.21
514	10.28	0.61	19.18	117.67	87.12	16.21
515	10.30	0.58	20.41	120.58	87.89	16.23
516	10.32	0.61	19.18	123.37	85.53	16.19
517	10.34	0.65	16.66	123.93	81.28	16.12
518	10.36	0.66	16.25	126.47	77.38	16.03
519	10.38	0.69	15.08	128.33	73.96	16.01
520	10.40	0.74	15.11	130.13	70.49	16.06
521	10.42	0.80	17.07	133.97	64.88	16.18
522	10.44	0.98	18.33	141.60	55.65	16.38
523	10.46	1.37	20.38	102.73	45.60	16.59
524	10.48	1.79	22.58	67.58	39.83	16.83
525	10.50	1.94	27.56	65.34	40.36	17.05
526	10.52	1.63	33.86	54.80	45.63	17.17
527	10.54	1.32	34.74	49.66	54.13	17.15
528	10.56	1.11	32.33	51.33	58.65	17.08

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	1.21	31.22	72.97	57.16	17.05
530	10.60	1.39	31.37	77.00	53.98	17.12
531	10.62	1.43	35.47	63.55	54.36	17.21
532	10.64	1.30	39.28	58.03	59.84	17.25
533	10.66	1.02	38.25	58.34	63.58	17.20
534	10.68	1.13	33.71	84.13	58.37	17.15
535	10.70	1.59	31.66	87.17	48.29	17.16
536	10.72	1.89	32.13	73.84	43.79	17.26
537	10.74	1.78	37.52	62.93	46.22	17.34
538	10.76	1.43	40.24	53.87	53.44	17.31
539	10.78	1.14	35.67	48.61	63.76	17.16
540	10.80	0.87	32.04	64.48	68.02	17.05
541	10.82	1.07	33.06	125.91	68.76	17.02
542	10.84	1.07	34.15	116.74	67.71	17.07
543	10.86	0.96	35.14	99.50	71.09	17.06
544	10.88	0.90	33.91	119.09	73.32	17.00
545	10.90	0.93	30.89	122.50	73.47	16.92
546	10.92	0.89	28.90	91.75	74.99	16.83
547	10.94	0.78	28.46	109.61	75.83	16.81
548	10.96	0.88	29.37	119.28	73.81	16.81
549	10.98	0.97	28.23	122.19	69.14	16.82
550	11.00	0.99	26.91	109.67	67.20	16.84
551	11.02	1.00	30.10	109.80	65.96	16.85
552	11.04	1.05	28.46	121.02	64.08	16.86
553	11.06	1.10	26.47	104.28	63.08	16.86
554	11.08	1.06	29.72	99.38	63.92	16.91
555	11.10	1.05	31.92	103.72	68.33	16.97
556	11.12	0.93	33.26	81.28	73.72	17.02
557	11.14	0.85	36.14	97.33	79.39	17.01
558	11.16	0.81	33.82	104.40	82.66	16.97
559	11.19	0.79	31.92	104.65	85.09	16.90
560	11.20	0.72	31.27	107.44	87.47	16.80
561	11.22	0.68	27.34	112.21	87.39	16.69
562	11.24	0.73	24.41	115.44	84.58	16.55
563	11.26	0.73	21.66	114.51	79.87	16.46
564	11.28	0.78	21.10	120.40	76.57	16.41
565	11.30	0.81	20.58	122.50	74.04	16.39
566	11.32	0.81	19.75	111.04	74.69	16.37
567	11.34	0.75	20.46	101.55	77.35	16.35
568	11.36	0.72	20.52	105.64	79.40	16.36
569	11.38	0.75	20.75	121.02	80.05	16.37
570	11.40	0.74	21.22	121.51	81.89	16.41
571	11.42	0.68	22.92	114.20	84.54	16.43
572	11.44	0.68	22.39	121.20	86.92	16.43
573	11.46	0.67	21.84	121.70	86.74	16.40
574	11.48	0.67	21.37	123.31	83.29	16.36
575	11.50	0.76	19.40	129.76	76.44	16.35
576	11.52	0.88	19.58	135.21	66.52	16.39

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	1.08	19.96	130.01	59.74	16.50
578	11.56	1.20	22.57	120.46	55.16	16.70
579	11.58	1.36	28.11	132.49	51.61	16.94
580	11.60	1.62	32.33	122.38	49.46	17.21
581	11.62	1.74	40.41	98.82	48.02	17.45
582	11.64	1.86	47.48	93.12	48.43	17.64
583	11.66	1.88	51.84	85.06	50.95	17.77
584	11.68	1.66	58.23	77.81	54.33	17.76
585	11.70	1.49	50.08	72.54	58.91	17.65
586	11.72	1.30	42.58	67.02	57.37	17.46
587	11.74	1.56	36.61	94.11	50.83	17.35
588	11.76	1.95	33.94	76.50	43.76	17.36
589	11.78	2.14	37.81	72.04	41.07	17.37
590	11.80	1.97	35.38	50.65	42.32	17.42
591	11.82	1.85	38.69	44.45	45.12	17.44
592	11.84	1.81	42.73	43.03	46.70	17.52
593	11.86	1.90	43.76	42.28	47.09	17.54
594	11.89	1.84	40.83	39.93	48.72	17.56
595	11.90	1.66	46.16	36.83	52.19	17.59
596	11.92	1.56	50.12	35.21	54.80	17.65
597	11.94	1.67	50.56	40.05	52.57	17.61
598	11.96	1.82	39.01	36.45	50.07	17.50
599	11.98	1.68	36.52	34.10	49.05	17.30
600	12.00	1.50	31.66	32.11	51.80	17.20
601	12.03	1.42	33.12	32.67	55.14	17.12
602	12.04	1.29	32.65	28.08	61.22	17.06
603	12.06	0.99	30.86	25.67	71.13	16.93
604	12.08	0.75	28.55	25.05	85.61	16.79
605	12.10	0.64	28.84	41.79	96.14	16.68
606	12.12	0.65	26.76	55.67	97.13	16.61
607	12.14	0.69	24.41	62.93	92.03	16.53
608	12.16	0.72	22.28	64.35	87.24	16.45
609	12.18	0.73	21.19	63.98	85.45	16.41
610	12.20	0.72	21.42	68.75	80.58	16.42
611	12.22	0.87	21.39	71.48	66.17	16.51
612	12.24	1.36	21.34	82.46	52.73	16.59
613	12.26	1.62	20.02	79.79	47.03	16.70
614	12.28	1.49	24.44	65.22	50.74	16.87
615	12.30	1.22	32.91	56.23	62.34	17.01
616	12.32	0.88	35.28	50.84	77.13	16.98
617	12.34	0.72	29.60	51.33	92.32	16.84
618	12.36	0.63	28.69	55.86	100.00	16.69
619	12.38	0.57	28.45	63.86	100.00	16.65
620	12.40	0.59	28.34	66.46	100.00	16.62
621	12.42	0.56	27.40	68.13	100.00	16.56
622	12.44	0.56	24.32	69.13	100.00	16.42
623	12.46	0.56	19.52	70.24	100.00	16.24
624	12.48	0.55	17.03	70.30	100.00	16.07

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	0.55	16.21	72.16	100.00	15.97
626	12.52	0.60	14.62	75.02	94.06	15.93
627	12.54	0.64	14.77	76.75	88.62	15.94
628	12.56	0.68	15.74	77.93	83.00	16.08
629	12.58	0.80	18.70	76.44	79.06	16.26
630	12.60	0.84	21.22	87.66	76.96	16.45
631	12.62	0.85	24.18	113.08	81.33	16.62
632	12.64	0.74	29.71	113.64	91.20	16.81
633	12.66	0.64	36.72	111.35	100.00	16.94
634	12.68	0.63	38.94	114.07	100.00	17.02
635	12.70	0.65	39.03	115.25	100.00	17.04
636	12.72	0.66	38.24	114.88	100.00	17.03
637	12.74	0.66	36.75	115.62	100.00	16.97
638	12.76	0.65	33.99	117.54	100.00	16.87
639	12.78	0.67	28.60	118.78	100.00	16.75
640	12.81	0.69	26.54	164.10	94.41	16.66
641	12.82	0.71	26.33	164.72	91.55	16.64
642	12.84	0.72	26.51	165.41	90.19	16.65
643	12.86	0.73	26.77	166.15	89.79	16.68
644	12.88	0.74	27.71	168.07	88.02	16.70
645	12.90	0.79	27.68	172.04	85.02	16.73
646	12.92	0.84	27.45	175.02	81.17	16.75
647	12.94	0.88	27.65	172.97	79.11	16.77
648	12.96	0.88	28.32	173.34	78.89	16.80
649	12.98	0.87	29.20	173.16	80.05	16.82
650	13.00	0.85	29.56	174.09	80.97	16.84
651	13.02	0.86	30.17	177.43	80.60	16.88
652	13.04	0.91	31.81	178.74	80.10	16.94
653	13.07	0.91	33.25	176.69	80.04	17.02
654	13.08	0.92	36.50	178.30	80.60	17.08
655	13.10	0.93	37.11	180.78	79.94	17.14
656	13.12	0.98	37.79	181.65	78.73	17.18
657	13.14	1.00	39.52	183.20	77.64	17.24
658	13.16	1.03	41.89	181.84	78.24	17.30
659	13.18	1.01	44.14	181.03	79.22	17.36
660	13.20	1.01	46.20	180.84	80.42	17.40
661	13.22	1.01	47.04	182.27	80.72	17.44
662	13.24	1.03	48.36	183.63	80.89	17.47
663	13.26	1.03	49.33	182.70	81.01	17.50
664	13.28	1.03	50.47	181.34	81.42	17.52
665	13.30	1.03	50.97	183.38	81.93	17.54
666	13.32	1.03	51.73	182.77	82.33	17.56
667	13.34	1.04	53.11	183.94	82.38	17.58
668	13.37	1.05	53.87	186.55	81.75	17.60
669	13.38	1.07	53.75	187.91	80.59	17.61
670	13.40	1.10	53.13	188.22	79.79	17.61
671	13.42	1.09	53.72	186.48	79.35	17.62
672	13.44	1.10	53.98	187.97	79.46	17.62

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	1.10	54.01	187.35	78.94	17.62
674	13.48	1.12	53.36	189.15	79.11	17.63
675	13.50	1.10	54.71	188.22	79.81	17.64
676	13.52	1.08	56.29	188.41	80.24	17.66
677	13.54	1.12	56.12	191.32	80.45	17.68
678	13.56	1.11	57.05	187.97	80.30	17.69
679	13.58	1.11	58.11	186.61	81.74	17.71
680	13.60	1.07	59.25	181.09	83.66	17.72
681	13.62	1.03	59.69	173.71	85.83	17.72
682	13.64	1.02	60.39	171.98	87.71	17.72
683	13.66	0.99	60.18	173.71	89.27	17.72
684	13.68	0.98	60.86	171.54	90.71	17.70
685	13.70	0.95	58.28	168.51	92.08	17.67
686	13.72	0.92	57.28	164.48	94.22	17.62
687	13.74	0.87	55.85	161.75	96.89	17.56
688	13.76	0.82	51.86	158.21	100.00	17.47
689	13.78	0.76	48.15	191.44	100.00	17.36
690	13.80	0.73	44.84	185.99	100.00	17.26
691	13.83	0.71	41.26	182.89	100.00	17.15
692	13.84	0.69	36.93	181.53	100.00	17.03
693	13.86	0.67	33.97	185.49	100.00	16.91
694	13.88	0.68	30.51	187.72	100.00	16.79
695	13.90	0.70	26.99	192.87	96.67	16.68
696	13.92	0.72	24.41	194.23	93.30	16.56
697	13.94	0.71	22.42	191.38	91.29	16.46
698	13.96	0.70	20.43	188.03	90.75	16.37
699	13.99	0.69	19.64	184.07	87.99	16.28
700	14.00	0.75	17.76	201.18	79.47	16.25
701	14.02	0.94	16.83	210.66	67.44	16.28
702	14.04	1.18	17.79	220.21	56.40	16.39
703	14.06	1.47	19.35	226.97	47.12	16.62
704	14.08	1.97	23.22	137.20	41.14	16.89
705	14.10	2.28	29.13	120.95	38.68	17.19
706	14.12	2.36	36.31	96.84	39.51	17.34
707	14.14	2.12	35.08	98.20	43.07	17.36
708	14.16	1.76	33.30	92.06	50.30	17.30
709	14.18	1.37	37.40	85.74	61.08	17.26
710	14.20	1.07	38.84	83.32	74.08	17.16
711	14.22	0.87	32.57	89.58	86.55	17.01
712	14.24	0.73	30.66	111.22	95.07	16.83
713	14.26	0.70	28.02	119.16	96.48	16.73
714	14.28	0.78	26.47	127.46	80.53	16.73
715	14.30	1.22	25.24	142.53	58.98	16.82
716	14.32	1.89	24.83	152.63	44.03	16.84
717	14.34	2.22	20.08	126.66	37.36	16.99
718	14.36	2.41	29.78	125.36	34.61	17.09
719	14.38	2.60	29.23	120.40	34.32	17.30
720	14.40	2.70	34.09	114.63	35.09	17.47

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	2.62	43.61	100.31	39.84	17.62
722	14.44	1.99	47.10	87.85	47.25	17.63
723	14.46	1.58	41.94	82.39	59.15	17.46
724	14.48	1.07	36.96	91.88	67.11	17.29
725	14.50	1.20	36.84	135.15	65.52	17.29
726	14.52	1.67	40.62	151.77	54.91	17.37
727	14.55	2.03	37.19	148.73	48.19	17.50
728	14.56	2.15	43.05	122.13	47.89	17.58
729	14.58	1.86	48.45	101.80	52.65	17.64
730	14.60	1.55	47.45	93.74	59.00	17.65
731	14.62	1.52	50.32	116.06	58.71	17.63
732	14.64	1.84	44.99	131.56	53.37	17.68
733	14.66	2.17	48.53	122.07	49.82	17.76
734	14.68	2.10	56.32	113.58	52.17	17.88
735	14.70	1.76	61.69	99.38	59.18	17.91
736	14.72	1.44	60.04	98.08	68.05	17.83
737	14.74	1.24	54.74	92.19	76.62	17.65
738	14.76	1.01	45.19	99.69	81.60	17.53
739	14.78	1.09	50.02	102.67	87.06	17.41
740	14.80	0.90	44.08	115.87	89.64	17.35
741	14.82	0.87	40.59	123.37	90.86	17.20
742	14.84	0.94	35.14	131.00	82.28	17.13
743	14.86	1.16	33.59	144.45	70.70	17.08
744	14.88	1.37	30.54	145.01	65.80	17.01
745	14.90	1.16	27.40	119.78	68.92	16.95
746	14.92	0.94	31.27	123.62	75.84	16.84
747	14.94	0.93	25.35	134.35	79.06	16.77
748	14.96	0.98	24.44	141.41	77.30	16.69
749	14.98	0.96	25.85	140.61	78.17	16.73
750	15.01	0.92	27.73	140.42	79.42	16.76
751	15.03	0.96	27.05	148.11	78.74	16.76
752	15.04	0.98	25.15	148.79	76.17	16.69
753	15.06	0.98	22.80	149.10	74.68	16.62
754	15.08	0.97	22.54	149.54	74.68	16.57
755	15.10	0.95	22.37	144.95	77.01	16.56
756	15.12	0.88	22.66	141.54	80.06	16.53
757	15.14	0.84	21.96	141.97	82.41	16.47
758	15.16	0.83	19.88	150.59	82.06	16.38
759	15.18	0.85	18.41	153.69	80.17	16.32
760	15.20	0.87	18.29	155.36	77.84	16.30
761	15.22	0.90	18.44	157.35	74.51	16.33
762	15.24	0.99	18.94	161.25	72.45	16.39
763	15.26	1.00	20.67	162.80	70.32	16.47
764	15.28	1.05	21.52	161.07	70.95	16.53
765	15.30	1.01	22.19	161.38	71.63	16.58
766	15.32	1.00	23.04	158.21	74.39	16.63
767	15.34	0.97	25.27	155.73	76.64	16.69
768	15.36	0.96	26.27	153.44	79.79	16.75

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	0.92	28.32	151.64	82.36	16.78
770	15.40	0.89	28.11	154.87	84.37	16.78
771	15.42	0.88	26.74	158.34	85.17	16.76
772	15.45	0.88	27.06	161.81	83.67	16.72
773	15.46	0.92	25.16	164.91	82.33	16.68
774	15.48	0.90	23.78	161.62	80.73	16.63
775	15.50	0.91	23.84	164.04	79.99	16.59
776	15.52	0.92	22.46	165.96	79.16	16.57
777	15.54	0.96	22.05	167.27	76.75	16.55

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.30	0.00	0.30	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
2	0.04	0.61	0.00	0.61	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
3	0.06	0.93	0.00	0.93	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
4	0.08	1.26	0.00	1.26	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
5	0.10	1.60	0.00	1.60	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
6	0.13	2.12	0.00	2.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
7	0.14	2.30	0.00	2.30	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
8	0.16	2.65	0.00	2.65	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
9	0.18	3.01	0.00	3.01	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
10	0.20	3.38	0.00	3.38	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
11	0.22	3.74	0.00	3.74	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
12	0.24	4.10	0.00	4.10	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
13	0.26	4.47	0.00	4.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
14	0.28	4.84	0.00	4.84	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
15	0.30	5.20	0.00	5.20	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
16	0.32	5.57	0.00	5.57	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
17	0.35	6.12	0.00	6.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
18	0.36	6.31	0.00	6.31	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
19	0.38	6.67	0.00	6.67	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
20	0.40	7.04	0.00	7.04	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
21	0.42	7.41	0.00	7.41	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
22	0.44	7.78	0.00	7.78	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
23	0.46	8.14	0.00	8.14	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
24	0.48	8.51	0.00	8.51	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
25	0.50	8.88	0.00	8.88	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
26	0.52	9.25	0.00	9.25	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
27	0.54	9.61	0.00	9.61	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
28	0.56	9.98	0.00	9.98	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
29	0.58	10.35	0.00	10.35	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
30	0.60	10.72	0.00	10.72	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
31	0.62	11.10	0.00	11.10	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
32	0.64	11.47	0.00	11.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
33	0.66	11.84	0.00	11.84	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
34	0.68	12.22	0.00	12.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
35	0.70	12.59	0.00	12.59	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
36	0.72	12.97	0.00	12.97	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
37	0.74	13.34	0.00	13.34	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
38	0.76	13.72	0.00	13.72	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
39	0.78	14.09	0.00	14.09	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
40	0.80	14.47	0.00	14.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
41	0.82	14.84	0.00	14.84	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
42	0.84	15.22	0.00	15.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
43	0.86	15.59	0.00	15.59	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
44	0.88	15.97	0.00	15.97	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
45	0.90	16.34	0.00	16.34	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
46	0.92	16.72	0.00	16.72	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
47	0.94	17.09	0.00	17.09	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
48	0.96	17.46	0.00	17.46	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	17.84	0.00	17.84	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
50	1.00	18.21	0.00	18.21	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
51	1.02	18.58	0.00	18.58	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
52	1.04	18.95	0.00	18.95	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
53	1.06	19.32	0.00	19.32	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
54	1.08	19.70	0.00	19.70	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
55	1.10	20.07	0.00	20.07	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
56	1.12	20.44	0.00	20.44	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
57	1.14	20.81	0.00	20.81	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
58	1.16	21.19	0.00	21.19	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
59	1.18	21.56	0.00	21.56	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
60	1.20	21.93	0.00	21.93	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
61	1.22	22.30	0.00	22.30	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
62	1.24	22.68	0.00	22.68	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
63	1.26	23.05	0.00	23.05	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
64	1.28	23.42	0.00	23.42	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
65	1.30	23.80	0.00	23.80	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
66	1.32	24.17	0.00	24.17	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
67	1.34	24.54	0.00	24.54	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
68	1.36	24.91	0.00	24.91	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
69	1.38	25.29	0.00	25.29	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
70	1.40	25.66	0.00	25.66	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
71	1.42	26.03	0.00	26.03	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
72	1.44	26.40	0.00	26.40	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
73	1.46	26.77	0.00	26.77	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
74	1.48	27.15	0.00	27.15	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
75	1.50	27.52	0.00	27.52	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
76	1.52	27.89	0.00	27.89	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
77	1.54	28.26	0.00	28.26	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
78	1.56	28.63	0.00	28.63	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
79	1.58	29.00	0.00	29.00	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
80	1.60	29.37	0.00	29.37	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
81	1.62	29.74	0.00	29.74	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
82	1.64	30.10	0.00	30.10	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
83	1.66	30.46	0.00	30.46	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
84	1.68	30.82	0.00	30.82	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
85	1.70	31.18	0.00	31.18	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
86	1.72	31.53	0.00	31.53	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
87	1.74	31.89	0.00	31.89	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
88	1.76	32.24	0.00	32.24	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
89	1.78	32.58	0.00	32.58	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
90	1.80	32.93	0.00	32.93	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
91	1.82	33.27	0.00	33.27	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
92	1.84	33.61	0.00	33.61	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
93	1.86	33.95	0.00	33.95	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
94	1.88	34.29	0.00	34.29	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
95	1.90	34.63	0.00	34.63	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
96	1.92	34.98	0.00	34.98	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	35.32	0.00	35.32	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
98	1.96	35.66	0.00	35.66	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
99	1.98	36.01	0.00	36.01	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
100	2.00	36.36	0.00	36.36	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
101	2.02	36.70	0.20	36.51	0.98	0.141	1.43	0.098	1.09	1.00	0.119	No
102	2.05	37.23	0.49	36.74	0.98	0.142	1.43	0.099	1.09	1.00	0.120	No
103	2.06	37.40	0.59	36.81	0.98	0.142	1.43	0.099	1.09	1.00	0.121	No
104	2.08	37.75	0.78	36.96	0.98	0.143	1.43	0.100	1.09	1.00	0.121	No
105	2.10	38.09	0.98	37.11	0.98	0.143	1.43	0.100	1.09	1.00	0.122	No
106	2.12	38.44	1.18	37.26	0.98	0.144	1.43	0.101	1.08	1.00	0.123	No
107	2.14	38.79	1.37	37.41	0.98	0.145	1.43	0.101	1.08	1.00	0.124	No
108	2.16	39.13	1.57	37.56	0.98	0.145	1.43	0.102	1.08	1.00	0.124	No
109	2.18	39.48	1.77	37.71	0.98	0.146	1.43	0.102	1.08	1.00	0.125	No
110	2.20	39.82	1.96	37.86	0.98	0.147	1.43	0.103	1.08	1.00	0.126	No
111	2.22	40.17	2.16	38.01	0.98	0.147	1.43	0.103	1.08	1.00	0.126	No
112	2.24	40.52	2.35	38.17	0.97	0.148	1.43	0.104	1.08	1.00	0.126	No
113	2.26	40.87	2.55	38.32	0.97	0.149	1.43	0.104	1.08	1.00	0.127	No
114	2.28	41.21	2.75	38.47	0.97	0.149	1.43	0.104	1.08	1.00	0.127	No
115	2.30	41.56	2.94	38.62	0.97	0.150	1.43	0.105	1.08	1.00	0.128	No
116	2.32	41.90	3.14	38.77	0.97	0.150	1.43	0.105	1.08	1.00	0.128	No
117	2.34	42.25	3.34	38.91	0.97	0.151	1.43	0.106	1.08	1.00	0.129	No
118	2.36	42.59	3.53	39.06	0.97	0.152	1.43	0.106	1.08	1.00	0.129	No
119	2.38	42.94	3.73	39.21	0.97	0.152	1.43	0.107	1.08	1.00	0.130	No
120	2.40	43.28	3.92	39.36	0.97	0.153	1.43	0.107	1.08	1.00	0.130	No
121	2.42	43.63	4.12	39.51	0.97	0.153	1.43	0.107	1.08	1.00	0.131	No
122	2.44	43.97	4.32	39.65	0.97	0.154	1.43	0.108	1.08	1.00	0.131	No
123	2.46	44.32	4.51	39.80	0.97	0.155	1.43	0.108	1.08	1.00	0.132	No
124	2.48	44.66	4.71	39.95	0.97	0.155	1.43	0.109	1.08	1.00	0.132	No
125	2.50	45.00	4.91	40.10	0.97	0.156	1.43	0.109	1.08	1.00	0.133	No
126	2.52	45.35	5.10	40.25	0.97	0.156	1.43	0.109	1.08	1.00	0.134	No
127	2.54	45.69	5.30	40.39	0.97	0.157	1.43	0.110	1.08	1.00	0.134	No
128	2.56	46.03	5.49	40.54	0.97	0.157	1.43	0.110	1.08	1.00	0.135	No
129	2.58	46.38	5.69	40.69	0.97	0.158	1.43	0.111	1.08	1.00	0.136	No
130	2.60	46.72	5.89	40.83	0.97	0.158	1.43	0.111	1.08	1.00	0.137	No
131	2.62	47.06	6.08	40.98	0.97	0.159	1.43	0.111	1.07	1.00	0.137	No
132	2.64	47.40	6.28	41.12	0.97	0.160	1.43	0.112	1.07	1.00	0.138	No
133	2.66	47.74	6.47	41.27	0.97	0.160	1.43	0.112	1.07	1.00	0.139	No
134	2.68	48.08	6.67	41.41	0.97	0.161	1.43	0.112	1.07	1.00	0.139	No
135	2.70	48.41	6.87	41.55	0.97	0.161	1.43	0.113	1.07	1.00	0.139	No
136	2.72	48.75	7.06	41.68	0.97	0.162	1.43	0.113	1.07	1.00	0.139	No
137	2.74	49.08	7.26	41.82	0.97	0.162	1.43	0.113	1.07	1.00	0.140	No
138	2.76	49.41	7.46	41.95	0.97	0.163	1.43	0.114	1.07	1.00	0.140	No
139	2.78	49.73	7.65	42.08	0.97	0.163	1.43	0.114	1.07	1.00	0.140	No
140	2.80	50.06	7.85	42.21	0.97	0.164	1.43	0.115	1.07	1.00	0.141	No
141	2.82	50.38	8.04	42.34	0.96	0.164	1.43	0.115	1.07	1.00	0.142	No
142	2.84	50.71	8.24	42.47	0.96	0.165	1.43	0.115	1.07	1.00	0.142	No
143	2.86	51.03	8.44	42.59	0.96	0.165	1.43	0.116	1.07	1.00	0.143	No
144	2.88	51.35	8.63	42.72	0.96	0.166	1.43	0.116	1.07	1.00	0.143	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	51.68	8.83	42.85	0.96	0.166	1.43	0.116	1.07	1.00	0.144	No
146	2.92	52.01	9.03	42.99	0.96	0.167	1.43	0.117	1.07	1.00	0.143	No
147	2.94	52.35	9.22	43.13	0.96	0.167	1.43	0.117	1.07	1.00	0.144	No
148	2.96	52.68	9.42	43.27	0.96	0.168	1.43	0.117	1.07	1.00	0.144	No
149	2.98	53.02	9.61	43.41	0.96	0.168	1.43	0.118	1.07	1.00	0.145	No
150	3.01	53.53	9.91	43.62	0.96	0.169	1.43	0.118	1.07	1.00	0.145	No
151	3.02	53.70	10.01	43.69	0.96	0.169	1.43	0.118	1.07	1.00	0.146	No
152	3.04	54.04	10.20	43.83	0.96	0.169	1.43	0.119	1.07	1.00	0.146	No
153	3.06	54.37	10.40	43.98	0.96	0.170	1.43	0.119	1.07	1.00	0.147	No
154	3.08	54.71	10.59	44.12	0.96	0.170	1.43	0.119	1.07	1.00	0.147	No
155	3.10	55.05	10.79	44.26	0.96	0.171	1.43	0.119	1.07	1.00	0.148	No
156	3.12	55.38	10.99	44.39	0.96	0.171	1.43	0.120	1.07	1.00	0.148	No
157	3.14	55.72	11.18	44.53	0.96	0.172	1.43	0.120	1.07	1.00	0.148	No
158	3.16	56.05	11.38	44.67	0.96	0.172	1.43	0.120	1.07	1.00	0.149	No
159	3.18	56.38	11.58	44.80	0.96	0.172	1.43	0.121	1.07	1.00	0.149	No
160	3.20	56.71	11.77	44.94	0.96	0.173	1.43	0.121	1.07	1.00	0.150	No
161	3.22	57.04	11.97	45.08	0.96	0.173	1.43	0.121	1.07	1.00	0.150	No
162	3.24	57.38	12.16	45.21	0.96	0.174	1.43	0.122	1.07	1.00	0.151	No
163	3.26	57.71	12.36	45.35	0.96	0.174	1.43	0.122	1.07	1.00	0.151	No
164	3.28	58.04	12.56	45.49	0.96	0.175	1.43	0.122	1.07	1.00	0.151	No
165	3.30	58.38	12.75	45.62	0.96	0.175	1.43	0.122	1.07	1.00	0.151	No
166	3.32	58.71	12.95	45.76	0.96	0.175	1.43	0.123	1.07	1.00	0.152	No
167	3.34	59.05	13.15	45.90	0.96	0.176	1.43	0.123	1.07	1.00	0.153	No
168	3.36	59.38	13.34	46.04	0.95	0.176	1.43	0.123	1.07	1.00	0.153	No
169	3.38	59.71	13.54	46.18	0.95	0.177	1.43	0.124	1.07	1.00	0.154	No
170	3.40	60.05	13.73	46.32	0.95	0.177	1.43	0.124	1.07	1.00	0.154	No
171	3.42	60.39	13.93	46.45	0.95	0.177	1.43	0.124	1.07	1.00	0.154	No
172	3.44	60.72	14.13	46.59	0.95	0.178	1.43	0.124	1.07	1.00	0.154	No
173	3.46	61.05	14.32	46.73	0.95	0.178	1.43	0.125	1.06	1.00	0.155	No
174	3.48	61.38	14.52	46.86	0.95	0.178	1.43	0.125	1.06	1.00	0.155	No
175	3.50	61.71	14.72	47.00	0.95	0.179	1.43	0.125	1.06	1.00	0.156	No
176	3.52	62.04	14.91	47.13	0.95	0.179	1.43	0.125	1.06	1.00	0.156	No
177	3.54	62.37	15.11	47.26	0.95	0.180	1.43	0.126	1.06	1.00	0.156	No
178	3.56	62.70	15.30	47.39	0.95	0.180	1.43	0.126	1.06	1.00	0.157	No
179	3.58	63.03	15.50	47.53	0.95	0.180	1.43	0.126	1.06	1.00	0.157	No
180	3.60	63.36	15.70	47.66	0.95	0.181	1.43	0.126	1.06	1.00	0.157	No
181	3.62	63.69	15.89	47.80	0.95	0.181	1.43	0.127	1.06	1.00	0.158	No
182	3.64	64.02	16.09	47.94	0.95	0.181	1.43	0.127	1.06	1.00	0.158	No
183	3.66	64.36	16.28	48.07	0.95	0.182	1.43	0.127	1.06	1.00	0.159	No
184	3.68	64.69	16.48	48.21	0.95	0.182	1.43	0.127	1.06	1.00	0.159	No
185	3.70	65.02	16.68	48.35	0.95	0.182	1.43	0.128	1.06	1.00	0.159	No
186	3.72	65.36	16.87	48.49	0.95	0.183	1.43	0.128	1.06	1.00	0.160	No
187	3.74	65.70	17.07	48.63	0.95	0.183	1.43	0.128	1.06	1.00	0.159	No
188	3.76	66.04	17.27	48.78	0.95	0.183	1.43	0.128	1.06	1.00	0.159	No
189	3.78	66.38	17.46	48.92	0.95	0.184	1.43	0.129	1.06	1.00	0.159	No
190	3.80	66.73	17.66	49.07	0.95	0.184	1.43	0.129	1.06	1.00	0.159	No
191	3.82	67.07	17.85	49.21	0.95	0.184	1.43	0.129	1.06	1.00	0.160	No
192	3.84	67.41	18.05	49.36	0.95	0.185	1.43	0.129	1.06	1.00	0.160	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	67.75	18.25	49.50	0.95	0.185	1.43	0.129	1.06	1.00	0.160	No
194	3.88	68.10	18.44	49.65	0.94	0.185	1.43	0.130	1.06	1.00	0.159	No
195	3.90	68.44	18.64	49.81	0.94	0.186	1.43	0.130	1.07	1.00	0.159	No
196	3.94	69.15	19.03	50.12	0.94	0.186	1.43	0.130	1.07	1.00	0.159	No
197	3.94	69.15	19.03	50.12	0.94	0.186	1.43	0.130	1.07	1.00	0.158	No
198	3.96	69.50	19.23	50.28	0.94	0.186	1.43	0.131	1.07	1.00	0.159	No
199	3.98	69.86	19.42	50.43	0.94	0.187	1.43	0.131	1.07	1.00	0.159	No
200	4.01	70.39	19.72	50.67	0.94	0.187	1.43	0.131	1.07	1.00	0.159	No
201	4.02	70.56	19.82	50.75	0.94	0.187	1.43	0.131	1.06	1.00	0.159	No
202	4.04	70.92	20.01	50.90	0.94	0.188	1.43	0.131	1.06	1.00	0.160	No
203	4.06	71.27	20.21	51.06	0.94	0.188	1.43	0.132	1.06	1.00	0.160	No
204	4.08	71.62	20.40	51.22	0.94	0.188	1.43	0.132	1.06	1.00	0.161	No
205	4.10	71.98	20.60	51.38	0.94	0.188	1.43	0.132	1.06	1.00	0.161	No
206	4.13	72.52	20.90	51.62	0.94	0.189	1.43	0.132	1.06	1.00	0.162	No
207	4.14	72.69	20.99	51.70	0.94	0.189	1.43	0.132	1.06	1.00	0.163	No
208	4.16	73.05	21.19	51.86	0.94	0.189	1.43	0.132	1.06	1.00	0.163	No
209	4.18	73.41	21.39	52.02	0.94	0.189	1.43	0.133	1.06	1.00	0.163	No
210	4.20	73.76	21.58	52.18	0.94	0.190	1.43	0.133	1.06	1.00	0.164	No
211	4.22	74.12	21.78	52.34	0.94	0.190	1.43	0.133	1.06	1.00	0.165	No
212	4.24	74.48	21.97	52.50	0.94	0.190	1.43	0.133	1.06	1.00	0.165	No
213	4.26	74.83	22.17	52.66	0.94	0.190	1.43	0.133	1.06	1.00	0.164	No
214	4.28	75.19	22.37	52.82	0.94	0.191	1.43	0.134	1.06	1.00	0.164	No
215	4.30	75.55	22.56	52.99	0.94	0.191	1.43	0.134	1.06	1.00	0.164	No
216	4.32	75.91	22.76	53.15	0.94	0.191	1.43	0.134	1.06	1.00	0.164	No
217	4.34	76.27	22.96	53.31	0.94	0.191	1.43	0.134	1.06	1.00	0.164	No
218	4.36	76.63	23.15	53.48	0.94	0.192	1.43	0.134	1.06	1.00	0.164	No
219	4.38	76.99	23.35	53.64	0.93	0.192	1.43	0.134	1.06	1.00	0.165	No
220	4.40	77.35	23.54	53.80	0.93	0.192	1.43	0.134	1.06	1.00	0.165	No
221	4.42	77.70	23.74	53.96	0.93	0.192	1.43	0.135	1.06	1.00	0.167	No
222	4.44	78.05	23.94	54.12	0.93	0.193	1.43	0.135	1.06	1.00	0.168	No
223	4.46	78.40	24.13	54.27	0.93	0.193	1.43	0.135	1.05	1.00	0.168	No
224	4.48	78.75	24.33	54.42	0.93	0.193	1.43	0.135	1.05	1.00	0.169	No
225	4.50	79.09	24.53	54.57	0.93	0.193	1.43	0.135	1.05	1.00	0.169	No
226	4.52	79.44	24.72	54.72	0.93	0.194	1.43	0.135	1.05	1.00	0.169	No
227	4.54	79.78	24.92	54.87	0.93	0.194	1.43	0.136	1.05	1.00	0.169	No
228	4.56	80.13	25.11	55.02	0.93	0.194	1.43	0.136	1.05	1.00	0.169	No
229	4.58	80.48	25.31	55.17	0.93	0.194	1.43	0.136	1.05	1.00	0.170	No
230	4.60	80.83	25.51	55.33	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
231	4.62	81.19	25.70	55.48	0.93	0.195	1.43	0.136	1.05	1.00	0.170	No
232	4.64	81.54	25.90	55.64	0.93	0.195	1.43	0.136	1.05	1.00	0.171	No
233	4.66	81.89	26.09	55.79	0.93	0.195	1.43	0.137	1.05	1.00	0.170	No
234	4.68	82.24	26.29	55.95	0.93	0.195	1.43	0.137	1.05	1.00	0.170	No
235	4.70	82.60	26.49	56.11	0.93	0.195	1.43	0.137	1.05	1.00	0.170	No
236	4.72	82.95	26.68	56.27	0.93	0.196	1.43	0.137	1.05	1.00	0.170	No
237	4.74	83.31	26.88	56.43	0.93	0.196	1.43	0.137	1.05	1.00	0.170	No
238	4.76	83.66	27.08	56.59	0.93	0.196	1.43	0.137	1.05	1.00	0.170	No
239	4.78	84.02	27.27	56.74	0.93	0.196	1.43	0.137	1.05	1.00	0.170	No
240	4.80	84.37	27.47	56.90	0.93	0.196	1.43	0.137	1.05	1.00	0.170	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	84.72	27.66	57.06	0.93	0.197	1.43	0.138	1.05	1.00	0.170	No
242	4.84	85.07	27.86	57.21	0.93	0.197	1.43	0.138	1.05	1.00	0.171	No
243	4.86	85.42	28.06	57.37	0.93	0.197	1.43	0.138	1.05	1.00	0.172	No
244	4.88	85.77	28.25	57.52	0.92	0.197	1.43	0.138	1.05	1.00	0.172	No
245	4.90	86.12	28.45	57.67	0.92	0.197	1.43	0.138	1.05	1.00	0.173	No
246	4.92	86.46	28.65	57.82	0.92	0.198	1.43	0.138	1.05	1.00	0.174	No
247	4.94	86.81	28.84	57.97	0.92	0.198	1.43	0.138	1.05	1.00	0.175	No
248	4.96	87.16	29.04	58.12	0.92	0.198	1.43	0.139	1.05	1.00	0.175	No
249	4.98	87.51	29.23	58.28	0.92	0.198	1.43	0.139	1.05	1.00	0.173	No
250	5.00	87.86	29.43	58.43	0.92	0.198	1.43	0.139	1.05	1.00	0.172	No
251	5.03	88.40	29.72	58.67	0.92	0.199	1.43	0.139	1.05	1.00	0.171	No
252	5.04	88.58	29.82	58.75	0.92	0.199	1.43	0.139	1.05	1.00	0.172	No
253	5.06	88.93	30.02	58.91	0.92	0.199	1.43	0.139	1.05	1.00	0.173	No
254	5.08	89.28	30.21	59.07	0.92	0.199	1.43	0.139	1.05	1.00	0.175	No
255	5.10	89.63	30.41	59.22	0.92	0.199	1.43	0.139	1.05	1.00	0.176	No
256	5.13	90.16	30.71	59.45	0.92	0.199	1.43	0.140	1.05	1.00	0.176	No
257	5.14	90.33	30.80	59.53	0.92	0.199	1.43	0.140	1.05	1.00	0.174	No
258	5.16	90.69	31.00	59.69	0.92	0.200	1.43	0.140	1.05	1.00	0.173	No
259	5.18	91.05	31.20	59.85	0.92	0.200	1.43	0.140	1.05	1.00	0.173	No
260	5.20	91.41	31.39	60.01	0.92	0.200	1.43	0.140	1.05	1.00	0.173	No
261	5.22	91.76	31.59	60.17	0.92	0.200	1.43	0.140	1.05	1.00	0.175	No
262	5.24	92.12	31.78	60.33	0.92	0.200	1.43	0.140	1.05	1.00	0.176	No
263	5.26	92.47	31.98	60.49	0.92	0.200	1.43	0.140	1.04	1.00	0.177	No
264	5.28	92.83	32.18	60.65	0.92	0.201	1.43	0.140	1.05	1.00	0.176	No
265	5.30	93.18	32.37	60.81	0.92	0.201	1.43	0.140	1.05	1.00	0.175	No
266	5.32	93.54	32.57	60.97	0.92	0.201	1.43	0.141	1.04	1.00	0.177	No
267	5.34	93.89	32.77	61.13	0.92	0.201	1.43	0.141	1.04	1.00	0.178	No
268	5.36	94.25	32.96	61.28	0.91	0.201	1.43	0.141	1.04	1.00	0.179	No
269	5.38	94.60	33.16	61.44	0.91	0.201	1.43	0.141	1.04	1.00	0.179	No
270	5.40	94.95	33.35	61.59	0.91	0.201	1.43	0.141	1.04	1.00	0.178	No
271	5.42	95.30	33.55	61.75	0.91	0.202	1.43	0.141	1.04	1.00	0.178	No
272	5.44	95.65	33.75	61.90	0.91	0.202	1.43	0.141	1.04	1.00	0.177	No
273	5.46	96.00	33.94	62.06	0.91	0.202	1.43	0.141	1.04	1.00	0.179	No
274	5.48	96.35	34.14	62.21	0.91	0.202	1.43	0.141	1.04	1.00	0.179	No
275	5.50	96.70	34.34	62.37	0.91	0.202	1.43	0.141	1.04	1.00	0.180	No
276	5.52	97.05	34.53	62.52	0.91	0.202	1.43	0.142	1.04	1.00	0.179	No
277	5.54	97.40	34.73	62.68	0.91	0.202	1.43	0.142	1.04	1.00	0.178	No
278	5.56	97.76	34.92	62.83	0.91	0.203	1.43	0.142	1.04	1.00	0.178	No
279	5.58	98.11	35.12	62.99	0.91	0.203	1.43	0.142	1.04	1.00	0.178	No
280	5.60	98.46	35.32	63.15	0.91	0.203	1.43	0.142	1.04	1.00	0.179	No
281	5.62	98.82	35.51	63.30	0.91	0.203	1.43	0.142	1.04	1.00	0.179	No
282	5.64	99.17	35.71	63.46	0.91	0.203	1.43	0.142	1.04	1.00	0.179	No
283	5.66	99.52	35.90	63.61	0.91	0.203	1.43	0.142	1.04	1.00	0.180	No
284	5.68	99.87	36.10	63.77	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
285	5.70	100.22	36.30	63.92	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
286	5.72	100.57	36.49	64.08	0.91	0.204	1.43	0.142	1.04	1.00	0.181	No
287	5.74	100.92	36.69	64.23	0.91	0.204	1.43	0.143	1.04	1.00	0.181	No
288	5.76	101.27	36.89	64.39	0.91	0.204	1.43	0.143	1.04	1.00	0.180	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	101.63	37.08	64.55	0.91	0.204	1.43	0.143	1.04	1.00	0.179	No
290	5.80	101.98	37.28	64.70	0.91	0.204	1.43	0.143	1.04	1.00	0.180	No
291	5.82	102.34	37.47	64.86	0.90	0.204	1.43	0.143	1.04	1.00	0.181	No
292	5.84	102.69	37.67	65.02	0.90	0.204	1.43	0.143	1.04	1.00	0.182	No
293	5.86	103.04	37.87	65.18	0.90	0.204	1.43	0.143	1.04	1.00	0.183	No
294	5.88	103.40	38.06	65.33	0.90	0.204	1.43	0.143	1.04	1.00	0.182	No
295	5.90	103.75	38.26	65.49	0.90	0.205	1.43	0.143	1.04	1.00	0.183	No
296	5.92	104.11	38.46	65.65	0.90	0.205	1.43	0.143	1.04	1.00	0.183	No
297	5.94	104.46	38.65	65.81	0.90	0.205	1.43	0.143	1.04	1.00	0.183	No
298	5.96	104.81	38.85	65.96	0.90	0.205	1.43	0.143	1.04	1.00	0.184	No
299	5.98	105.15	39.04	66.11	0.90	0.205	1.43	0.143	1.04	1.00	0.183	No
300	6.00	105.50	39.24	66.26	0.90	0.205	1.43	0.144	1.04	1.00	0.183	No
301	6.02	105.84	39.44	66.41	0.90	0.205	1.43	0.144	1.04	1.00	0.183	No
302	6.04	106.19	39.63	66.55	0.90	0.205	1.43	0.144	1.04	1.00	0.183	No
303	6.06	106.53	39.83	66.70	0.90	0.205	1.43	0.144	1.04	1.00	0.183	No
304	6.08	106.88	40.02	66.85	0.90	0.206	1.43	0.144	1.04	1.00	0.184	No
305	6.10	107.22	40.22	67.00	0.90	0.206	1.43	0.144	1.04	1.00	0.184	No
306	6.12	107.57	40.42	67.16	0.90	0.206	1.43	0.144	1.03	1.00	0.184	No
307	6.14	107.92	40.61	67.31	0.90	0.206	1.43	0.144	1.03	1.00	0.184	No
308	6.16	108.27	40.81	67.46	0.90	0.206	1.43	0.144	1.03	1.00	0.184	No
309	6.18	108.62	41.01	67.61	0.90	0.206	1.43	0.144	1.03	1.00	0.184	No
310	6.20	108.96	41.20	67.76	0.90	0.206	1.43	0.144	1.03	1.00	0.185	No
311	6.22	109.31	41.40	67.91	0.90	0.206	1.43	0.144	1.03	1.00	0.185	No
312	6.24	109.65	41.59	68.06	0.90	0.206	1.43	0.144	1.03	1.00	0.185	No
313	6.26	110.00	41.79	68.20	0.89	0.206	1.43	0.144	1.03	1.00	0.185	No
314	6.28	110.34	41.99	68.35	0.89	0.206	1.43	0.145	1.03	1.00	0.184	No
315	6.30	110.69	42.18	68.50	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
316	6.32	111.03	42.38	68.65	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
317	6.34	111.38	42.58	68.80	0.89	0.207	1.43	0.145	1.03	1.00	0.186	No
318	6.36	111.73	42.77	68.95	0.89	0.207	1.43	0.145	1.03	1.00	0.186	No
319	6.38	112.07	42.97	69.10	0.89	0.207	1.43	0.145	1.03	1.00	0.187	No
320	6.40	112.41	43.16	69.25	0.89	0.207	1.43	0.145	1.03	1.00	0.187	No
321	6.42	112.76	43.36	69.40	0.89	0.207	1.43	0.145	1.03	1.00	0.187	No
322	6.44	113.10	43.56	69.54	0.89	0.207	1.43	0.145	1.03	1.00	0.187	No
323	6.46	113.44	43.75	69.69	0.89	0.207	1.43	0.145	1.03	1.00	0.187	No
324	6.48	113.78	43.95	69.83	0.89	0.207	1.43	0.145	1.03	1.00	0.187	No
325	6.50	114.12	44.15	69.97	0.89	0.207	1.43	0.145	1.03	1.00	0.187	No
326	6.52	114.45	44.34	70.11	0.89	0.208	1.43	0.145	1.03	1.00	0.188	No
327	6.54	114.78	44.54	70.25	0.89	0.208	1.43	0.145	1.03	1.00	0.188	No
328	6.56	115.11	44.73	70.38	0.89	0.208	1.43	0.145	1.03	1.00	0.188	No
329	6.58	115.44	44.93	70.51	0.89	0.208	1.43	0.145	1.03	1.00	0.189	No
330	6.60	115.77	45.13	70.65	0.89	0.208	1.43	0.146	1.03	1.00	0.189	No
331	6.62	116.10	45.32	70.78	0.89	0.208	1.43	0.146	1.03	1.00	0.189	No
332	6.64	116.43	45.52	70.91	0.89	0.208	1.43	0.146	1.03	1.00	0.189	No
333	6.66	116.76	45.71	71.04	0.89	0.208	1.43	0.146	1.03	1.00	0.189	No
334	6.68	117.08	45.91	71.17	0.89	0.208	1.43	0.146	1.03	1.00	0.189	No
335	6.70	117.40	46.11	71.30	0.89	0.208	1.43	0.146	1.03	1.00	0.189	No
336	6.72	117.73	46.30	71.43	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	118.06	46.50	71.56	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
338	6.76	118.39	46.70	71.69	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
339	6.78	118.71	46.89	71.82	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
340	6.80	119.04	47.09	71.95	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
341	6.82	119.37	47.28	72.09	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
342	6.84	119.70	47.48	72.22	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
343	6.86	120.03	47.68	72.35	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
344	6.88	120.35	47.87	72.48	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
345	6.90	120.68	48.07	72.61	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
346	6.92	121.01	48.27	72.74	0.88	0.209	1.43	0.147	1.03	1.00	0.190	No
347	6.95	121.50	48.56	72.94	0.88	0.209	1.43	0.147	1.03	1.00	0.190	No
348	6.96	121.66	48.66	73.00	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
349	6.98	121.98	48.85	73.13	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
350	7.00	122.30	49.05	73.25	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
351	7.02	122.62	49.25	73.37	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
352	7.04	122.94	49.44	73.49	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
353	7.06	123.25	49.64	73.61	0.88	0.210	1.43	0.147	1.03	1.00	0.192	No
354	7.08	123.57	49.83	73.73	0.88	0.210	1.43	0.147	1.02	1.00	0.191	No
355	7.10	123.89	50.03	73.86	0.88	0.210	1.43	0.147	1.02	1.00	0.192	No
356	7.13	124.36	50.33	74.04	0.88	0.210	1.43	0.147	1.02	1.00	0.192	No
357	7.14	124.52	50.42	74.10	0.88	0.210	1.43	0.147	1.02	1.00	0.192	No
358	7.16	124.85	50.62	74.23	0.87	0.210	1.43	0.147	1.02	1.00	0.192	No
359	7.18	125.17	50.82	74.36	0.87	0.210	1.43	0.147	1.02	1.00	0.191	No
360	7.20	125.50	51.01	74.49	0.87	0.211	1.43	0.147	1.02	1.00	0.191	No
361	7.22	125.83	51.21	74.62	0.87	0.211	1.43	0.147	1.02	1.00	0.192	No
362	7.24	126.16	51.40	74.75	0.87	0.211	1.43	0.147	1.02	1.00	0.192	No
363	7.26	126.49	51.60	74.89	0.87	0.211	1.43	0.147	1.02	1.00	0.192	No
364	7.28	126.81	51.80	75.02	0.87	0.211	1.43	0.148	1.02	1.00	0.192	No
365	7.30	127.14	51.99	75.15	0.87	0.211	1.43	0.148	1.02	1.00	0.192	No
366	7.32	127.47	52.19	75.28	0.87	0.211	1.43	0.148	1.02	1.00	0.192	No
367	7.34	127.80	52.39	75.42	0.87	0.211	1.43	0.148	1.02	1.00	0.192	No
368	7.36	128.13	52.58	75.55	0.87	0.211	1.43	0.148	1.02	1.00	0.193	No
369	7.38	128.46	52.78	75.68	0.87	0.211	1.43	0.148	1.02	1.00	0.193	No
370	7.40	128.78	52.97	75.81	0.87	0.211	1.43	0.148	1.02	1.00	0.193	No
371	7.42	129.10	53.17	75.93	0.87	0.211	1.43	0.148	1.02	1.00	0.193	No
372	7.45	129.59	53.46	76.12	0.87	0.211	1.43	0.148	1.02	1.00	0.193	No
373	7.46	129.75	53.56	76.19	0.87	0.211	1.43	0.148	1.02	1.00	0.192	No
374	7.48	130.08	53.76	76.32	0.87	0.211	1.43	0.148	1.02	1.00	0.192	No
375	7.50	130.41	53.96	76.46	0.87	0.211	1.43	0.148	1.02	1.00	0.192	No
376	7.52	130.75	54.15	76.60	0.87	0.211	1.43	0.148	1.02	1.00	0.192	No
377	7.54	131.09	54.35	76.74	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
378	7.56	131.43	54.54	76.89	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
379	7.58	131.77	54.74	77.03	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
380	7.60	132.12	54.94	77.19	0.86	0.212	1.43	0.148	1.02	1.00	0.192	No
381	7.62	132.47	55.13	77.34	0.86	0.212	1.43	0.148	1.02	1.00	0.192	No
382	7.64	132.82	55.33	77.49	0.86	0.212	1.43	0.148	1.02	1.00	0.192	No
383	7.66	133.17	55.52	77.65	0.86	0.212	1.43	0.148	1.02	1.00	0.192	No
384	7.68	133.53	55.72	77.81	0.86	0.212	1.43	0.148	1.02	1.00	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	133.88	55.92	77.97	0.86	0.212	1.43	0.148	1.02	1.00	0.192	No
386	7.72	134.24	56.11	78.13	0.86	0.212	1.43	0.148	1.02	1.00	0.192	No
387	7.74	134.60	56.31	78.29	0.86	0.212	1.43	0.148	1.02	1.00	0.192	No
388	7.76	134.96	56.51	78.45	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
389	7.78	135.32	56.70	78.61	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
390	7.80	135.67	56.90	78.78	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
391	7.82	136.03	57.09	78.94	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
392	7.84	136.39	57.29	79.10	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
393	7.86	136.75	57.49	79.26	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
394	7.88	137.10	57.68	79.42	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
395	7.90	137.46	57.88	79.58	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
396	7.92	137.81	58.08	79.73	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
397	7.94	138.16	58.27	79.89	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
398	7.96	138.52	58.47	80.05	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
399	7.99	139.05	58.76	80.28	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
400	8.00	139.22	58.86	80.36	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
401	8.02	139.57	59.06	80.52	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
402	8.04	139.93	59.25	80.67	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
403	8.06	140.28	59.45	80.83	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
404	8.08	140.63	59.64	80.99	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
405	8.10	140.99	59.84	81.15	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
406	8.12	141.34	60.04	81.31	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
407	8.14	141.70	60.23	81.47	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
408	8.16	142.06	60.43	81.63	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
409	8.18	142.42	60.63	81.79	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
410	8.20	142.77	60.82	81.95	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
411	8.22	143.13	61.02	82.11	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
412	8.24	143.49	61.21	82.28	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
413	8.26	143.85	61.41	82.44	0.85	0.212	1.43	0.148	1.02	1.00	0.193	No
414	8.28	144.21	61.61	82.60	0.85	0.212	1.43	0.148	1.02	1.00	0.194	No
415	8.30	144.57	61.80	82.76	0.85	0.212	1.43	0.148	1.02	1.00	0.194	No
416	8.32	144.92	62.00	82.93	0.85	0.212	1.43	0.148	1.02	1.00	0.194	No
417	8.34	145.28	62.20	83.08	0.85	0.212	1.43	0.148	1.02	1.00	0.194	No
418	8.36	145.64	62.39	83.24	0.85	0.212	1.43	0.148	1.02	1.00	0.194	No
419	8.38	145.99	62.59	83.40	0.85	0.212	1.43	0.148	1.02	1.00	0.194	No
420	8.40	146.34	62.78	83.56	0.85	0.212	1.43	0.148	1.02	1.00	0.194	No
421	8.42	146.70	62.98	83.72	0.85	0.212	1.43	0.148	1.02	1.00	0.194	No
422	8.44	147.05	63.18	83.87	0.84	0.212	1.43	0.148	1.02	1.00	0.194	No
423	8.46	147.40	63.37	84.03	0.84	0.212	1.43	0.148	1.02	1.00	0.194	No
424	8.48	147.76	63.57	84.19	0.84	0.212	1.43	0.148	1.01	1.00	0.194	No
425	8.50	148.11	63.77	84.34	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
426	8.52	148.45	63.96	84.49	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
427	8.54	148.80	64.16	84.64	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
428	8.56	149.15	64.35	84.80	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
429	8.58	149.49	64.55	84.94	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
430	8.60	149.84	64.75	85.09	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
431	8.62	150.18	64.94	85.24	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
432	8.64	150.52	65.14	85.38	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	150.86	65.33	85.53	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
434	8.68	151.20	65.53	85.66	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
435	8.70	151.53	65.73	85.80	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
436	8.72	151.86	65.92	85.94	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
437	8.74	152.19	66.12	86.07	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
438	8.76	152.51	66.32	86.20	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
439	8.78	152.84	66.51	86.33	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
440	8.80	153.16	66.71	86.45	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
441	8.82	153.48	66.90	86.58	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
442	8.84	153.80	67.10	86.70	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
443	8.86	154.12	67.30	86.82	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
444	8.88	154.44	67.49	86.94	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
445	8.90	154.76	67.69	87.07	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
446	8.92	155.07	67.89	87.19	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
447	8.94	155.39	68.08	87.31	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
448	8.96	155.71	68.28	87.44	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
449	8.98	156.04	68.47	87.56	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
450	9.00	156.36	68.67	87.69	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
451	9.02	156.68	68.87	87.81	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
452	9.05	157.17	69.16	88.01	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
453	9.06	157.33	69.26	88.07	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
454	9.08	157.66	69.45	88.21	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
455	9.10	157.99	69.65	88.34	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
456	9.12	158.33	69.85	88.48	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
457	9.14	158.67	70.04	88.62	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
458	9.16	159.01	70.24	88.77	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
459	9.18	159.35	70.44	88.91	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
460	9.20	159.69	70.63	89.06	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
461	9.22	160.03	70.83	89.20	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
462	9.25	160.54	71.12	89.42	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
463	9.26	160.71	71.22	89.49	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
464	9.28	161.05	71.42	89.64	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
465	9.30	161.39	71.61	89.78	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
466	9.32	161.74	71.81	89.93	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
467	9.34	162.07	72.01	90.07	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
468	9.36	162.41	72.20	90.21	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
469	9.38	162.75	72.40	90.35	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
470	9.40	163.08	72.59	90.49	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
471	9.42	163.42	72.79	90.63	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
472	9.44	163.75	72.99	90.76	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
473	9.46	164.08	73.18	90.89	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
474	9.48	164.40	73.38	91.03	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
475	9.50	164.73	73.58	91.16	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
476	9.52	165.06	73.77	91.29	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
477	9.54	165.39	73.97	91.42	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
478	9.56	165.71	74.16	91.55	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
479	9.58	166.03	74.36	91.67	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
480	9.60	166.35	74.56	91.80	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	166.67	74.75	91.92	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
482	9.64	166.99	74.95	92.04	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
483	9.66	167.31	75.14	92.16	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
484	9.68	167.62	75.34	92.28	0.82	0.212	1.43	0.148	1.01	1.00	0.197	No
485	9.70	167.93	75.54	92.39	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
486	9.72	168.24	75.73	92.50	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
487	9.74	168.55	75.93	92.62	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
488	9.76	168.86	76.13	92.73	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
489	9.78	169.17	76.32	92.84	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
490	9.80	169.49	76.52	92.97	0.81	0.212	1.43	0.148	1.01	1.00	0.196	No
491	9.82	169.81	76.71	93.10	0.81	0.212	1.43	0.148	1.01	1.00	0.195	No
492	9.84	170.15	76.91	93.24	0.81	0.212	1.43	0.148	1.01	1.00	0.195	No
493	9.86	170.48	77.11	93.38	0.81	0.212	1.43	0.148	1.01	1.00	0.195	No
494	9.88	170.82	77.30	93.51	0.81	0.212	1.43	0.148	1.01	1.00	0.196	No
495	9.90	171.14	77.50	93.65	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
496	9.92	171.47	77.70	93.77	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
497	9.94	171.79	77.89	93.90	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
498	9.96	172.11	78.09	94.03	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
499	9.98	172.43	78.28	94.15	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
500	10.01	172.91	78.58	94.33	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
501	10.02	173.06	78.68	94.39	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
502	10.04	173.38	78.87	94.50	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
503	10.06	173.69	79.07	94.62	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
504	10.08	174.00	79.26	94.74	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
505	10.10	174.31	79.46	94.85	0.81	0.212	1.43	0.148	1.01	1.00	0.197	No
506	10.12	174.63	79.66	94.97	0.80	0.212	1.43	0.148	1.01	1.00	0.196	No
507	10.14	174.95	79.85	95.10	0.80	0.212	1.43	0.148	1.01	1.00	0.195	No
508	10.16	175.28	80.05	95.23	0.80	0.212	1.43	0.148	1.01	1.00	0.194	No
509	10.18	175.61	80.25	95.36	0.80	0.212	1.43	0.148	1.01	1.00	0.195	No
510	10.20	175.93	80.44	95.49	0.80	0.212	1.43	0.148	1.00	1.00	0.195	No
511	10.22	176.26	80.64	95.62	0.80	0.212	1.43	0.148	1.00	1.00	0.196	No
512	10.24	176.58	80.83	95.75	0.80	0.212	1.43	0.148	1.00	1.00	0.197	No
513	10.26	176.91	81.03	95.88	0.80	0.212	1.43	0.148	1.00	1.00	0.197	No
514	10.28	177.23	81.23	96.00	0.80	0.211	1.43	0.148	1.00	1.00	0.197	No
515	10.30	177.55	81.42	96.13	0.80	0.211	1.43	0.148	1.00	1.00	0.197	No
516	10.32	177.88	81.62	96.26	0.80	0.211	1.43	0.148	1.00	1.00	0.197	No
517	10.34	178.20	81.82	96.39	0.80	0.211	1.43	0.148	1.00	1.00	0.197	No
518	10.36	178.52	82.01	96.51	0.80	0.211	1.43	0.148	1.00	1.00	0.197	No
519	10.38	178.84	82.21	96.63	0.80	0.211	1.43	0.148	1.00	1.00	0.197	No
520	10.40	179.16	82.40	96.76	0.80	0.211	1.43	0.148	1.00	1.00	0.196	No
521	10.42	179.49	82.60	96.89	0.80	0.211	1.43	0.148	1.00	1.00	0.196	No
522	10.44	179.81	82.80	97.02	0.80	0.211	1.43	0.148	1.00	1.00	0.196	No
523	10.46	180.15	82.99	97.15	0.80	0.211	1.43	0.148	1.00	1.00	0.195	No
524	10.48	180.48	83.19	97.29	0.80	0.211	1.43	0.148	1.00	1.00	0.194	No
525	10.50	180.82	83.39	97.44	0.80	0.211	1.43	0.148	1.00	1.00	0.193	No
526	10.52	181.17	83.58	97.59	0.80	0.211	1.43	0.148	1.00	1.00	0.194	No
527	10.54	181.51	83.78	97.73	0.79	0.211	1.43	0.148	1.00	1.00	0.195	No
528	10.56	181.85	83.97	97.88	0.79	0.211	1.43	0.148	1.00	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	182.19	84.17	98.02	0.79	0.211	1.43	0.148	1.00	1.00	0.195	No
530	10.60	182.53	84.37	98.17	0.79	0.211	1.43	0.148	1.00	1.00	0.194	No
531	10.62	182.88	84.56	98.32	0.79	0.211	1.43	0.148	1.00	1.00	0.194	No
532	10.64	183.22	84.76	98.47	0.79	0.211	1.43	0.148	1.00	1.00	0.195	No
533	10.66	183.57	84.95	98.61	0.79	0.211	1.43	0.148	1.00	1.00	0.196	No
534	10.68	183.91	85.15	98.76	0.79	0.211	1.43	0.148	1.00	1.00	0.195	No
535	10.70	184.25	85.35	98.91	0.79	0.211	1.43	0.148	1.00	1.00	0.194	No
536	10.72	184.60	85.54	99.06	0.79	0.211	1.43	0.147	1.00	1.00	0.193	No
537	10.74	184.95	85.74	99.21	0.79	0.211	1.43	0.147	1.00	1.00	0.193	No
538	10.76	185.29	85.94	99.36	0.79	0.211	1.43	0.147	1.00	1.00	0.194	No
539	10.78	185.64	86.13	99.50	0.79	0.211	1.43	0.147	1.00	1.00	0.195	No
540	10.80	185.98	86.33	99.65	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
541	10.82	186.32	86.52	99.79	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
542	10.84	186.66	86.72	99.94	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
543	10.86	187.00	86.92	100.08	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
544	10.88	187.34	87.11	100.23	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
545	10.90	187.68	87.31	100.37	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
546	10.92	188.01	87.51	100.51	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
547	10.94	188.35	87.70	100.65	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
548	10.96	188.69	87.90	100.79	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
549	10.98	189.02	88.09	100.93	0.78	0.210	1.43	0.147	1.00	1.00	0.195	No
550	11.00	189.36	88.29	101.07	0.78	0.210	1.43	0.147	1.00	1.00	0.195	No
551	11.02	189.70	88.49	101.21	0.78	0.210	1.43	0.147	1.00	1.00	0.195	No
552	11.04	190.03	88.68	101.35	0.78	0.210	1.43	0.147	1.00	1.00	0.195	No
553	11.06	190.37	88.88	101.49	0.78	0.210	1.43	0.147	1.00	1.00	0.195	No
554	11.08	190.71	89.07	101.64	0.78	0.210	1.43	0.147	1.00	1.00	0.195	No
555	11.10	191.05	89.27	101.78	0.78	0.210	1.43	0.147	1.00	1.00	0.195	No
556	11.12	191.39	89.47	101.92	0.78	0.210	1.43	0.147	1.00	1.00	0.195	No
557	11.14	191.73	89.66	102.07	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
558	11.16	192.07	89.86	102.21	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
559	11.19	192.58	90.15	102.42	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
560	11.20	192.74	90.25	102.49	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
561	11.22	193.08	90.45	102.63	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
562	11.24	193.41	90.64	102.76	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
563	11.26	193.74	90.84	102.90	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
564	11.28	194.07	91.04	103.03	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
565	11.30	194.39	91.23	103.16	0.78	0.209	1.43	0.147	1.00	1.00	0.195	No
566	11.32	194.72	91.43	103.29	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
567	11.34	195.05	91.63	103.42	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
568	11.36	195.38	91.82	103.55	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
569	11.38	195.70	92.02	103.69	0.77	0.209	1.43	0.146	1.00	1.00	0.196	No
570	11.40	196.03	92.21	103.82	0.77	0.209	1.43	0.146	1.00	1.00	0.196	No
571	11.42	196.36	92.41	103.95	0.77	0.209	1.43	0.146	1.00	1.00	0.196	No
572	11.44	196.69	92.61	104.08	0.77	0.209	1.43	0.146	1.00	1.00	0.196	No
573	11.46	197.02	92.80	104.21	0.77	0.209	1.43	0.146	1.00	1.00	0.196	No
574	11.48	197.34	93.00	104.35	0.77	0.209	1.43	0.146	1.00	1.00	0.196	No
575	11.50	197.67	93.19	104.48	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
576	11.52	198.00	93.39	104.61	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	198.33	93.59	104.74	0.77	0.209	1.43	0.146	1.00	1.00	0.194	No
578	11.56	198.66	93.78	104.88	0.77	0.209	1.43	0.146	1.00	1.00	0.194	No
579	11.58	199.00	93.98	105.02	0.77	0.209	1.43	0.146	1.00	1.00	0.194	No
580	11.60	199.35	94.18	105.17	0.77	0.209	1.43	0.146	1.00	1.00	0.193	No
581	11.62	199.69	94.37	105.32	0.77	0.209	1.43	0.146	1.00	1.00	0.193	No
582	11.64	200.05	94.57	105.48	0.77	0.208	1.43	0.146	1.00	1.00	0.192	No
583	11.66	200.40	94.76	105.64	0.77	0.208	1.43	0.146	1.00	1.00	0.192	No
584	11.68	200.76	94.96	105.80	0.77	0.208	1.43	0.146	1.00	1.00	0.193	No
585	11.70	201.11	95.16	105.95	0.77	0.208	1.43	0.146	1.00	1.00	0.193	No
586	11.72	201.46	95.35	106.11	0.77	0.208	1.43	0.146	1.00	1.00	0.194	No
587	11.74	201.81	95.55	106.26	0.77	0.208	1.43	0.146	1.00	1.00	0.193	No
588	11.76	202.15	95.75	106.41	0.77	0.208	1.43	0.146	1.00	1.00	0.192	No
589	11.78	202.50	95.94	106.56	0.77	0.208	1.43	0.146	1.00	1.00	0.191	No
590	11.80	202.85	96.14	106.71	0.76	0.208	1.43	0.146	1.00	1.00	0.192	No
591	11.82	203.20	96.33	106.87	0.76	0.208	1.43	0.145	1.00	1.00	0.192	No
592	11.84	203.55	96.53	107.02	0.76	0.208	1.43	0.145	1.00	1.00	0.192	No
593	11.86	203.90	96.73	107.17	0.76	0.208	1.43	0.145	1.00	1.00	0.192	No
594	11.89	204.43	97.02	107.41	0.76	0.208	1.43	0.145	0.99	1.00	0.192	No
595	11.90	204.60	97.12	107.48	0.76	0.208	1.43	0.145	0.99	1.00	0.192	No
596	11.92	204.96	97.32	107.64	0.76	0.207	1.43	0.145	0.99	1.00	0.192	No
597	11.94	205.31	97.51	107.80	0.76	0.207	1.43	0.145	0.99	1.00	0.192	No
598	11.96	205.66	97.71	107.95	0.76	0.207	1.43	0.145	0.99	1.00	0.192	No
599	11.98	206.00	97.90	108.10	0.76	0.207	1.43	0.145	0.99	1.00	0.192	No
600	12.00	206.35	98.10	108.25	0.76	0.207	1.43	0.145	0.99	1.00	0.193	No
601	12.03	206.86	98.39	108.47	0.76	0.207	1.43	0.145	0.99	1.00	0.193	No
602	12.04	207.03	98.49	108.54	0.76	0.207	1.43	0.145	0.99	1.00	0.193	No
603	12.06	207.37	98.69	108.68	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
604	12.08	207.71	98.88	108.82	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
605	12.10	208.04	99.08	108.96	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
606	12.12	208.37	99.28	109.10	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
607	12.14	208.70	99.47	109.23	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
608	12.16	209.03	99.67	109.36	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
609	12.18	209.36	99.87	109.50	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
610	12.20	209.69	100.06	109.63	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
611	12.22	210.02	100.26	109.76	0.75	0.207	1.43	0.145	0.99	1.00	0.194	No
612	12.24	210.35	100.45	109.90	0.75	0.206	1.43	0.145	0.99	1.00	0.193	No
613	12.26	210.69	100.65	110.03	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No
614	12.28	211.02	100.85	110.18	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No
615	12.30	211.36	101.04	110.32	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
616	12.32	211.70	101.24	110.46	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
617	12.34	212.04	101.44	110.60	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
618	12.36	212.37	101.63	110.74	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
619	12.38	212.71	101.83	110.88	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
620	12.40	213.04	102.02	111.01	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
621	12.42	213.37	102.22	111.15	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
622	12.44	213.70	102.42	111.28	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
623	12.46	214.02	102.61	111.41	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
624	12.48	214.34	102.81	111.53	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	214.66	103.01	111.66	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
626	12.52	214.98	103.20	111.78	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
627	12.54	215.30	103.40	111.90	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
628	12.56	215.62	103.59	112.03	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
629	12.58	215.95	103.79	112.16	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
630	12.60	216.28	103.99	112.29	0.75	0.205	1.43	0.144	0.99	1.00	0.193	No
631	12.62	216.61	104.18	112.43	0.75	0.205	1.43	0.144	0.99	1.00	0.193	No
632	12.64	216.94	104.38	112.57	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
633	12.66	217.28	104.57	112.71	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
634	12.68	217.62	104.77	112.85	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
635	12.70	217.96	104.97	113.00	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
636	12.72	218.31	105.16	113.14	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
637	12.74	218.64	105.36	113.29	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
638	12.76	218.98	105.56	113.43	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
639	12.78	219.32	105.75	113.57	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
640	12.81	219.82	106.05	113.77	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
641	12.82	219.98	106.14	113.84	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
642	12.84	220.32	106.34	113.98	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
643	12.86	220.65	106.54	114.11	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
644	12.88	220.98	106.73	114.25	0.74	0.204	1.43	0.143	0.99	1.00	0.193	No
645	12.90	221.32	106.93	114.39	0.74	0.204	1.43	0.143	0.99	1.00	0.193	No
646	12.92	221.65	107.13	114.53	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
647	12.94	221.99	107.32	114.67	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
648	12.96	222.33	107.52	114.81	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
649	12.98	222.66	107.71	114.95	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
650	13.00	223.00	107.91	115.09	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
651	13.02	223.34	108.11	115.23	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
652	13.04	223.67	108.30	115.37	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
653	13.07	224.19	108.60	115.59	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
654	13.08	224.36	108.69	115.66	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
655	13.10	224.70	108.89	115.81	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
656	13.12	225.04	109.09	115.96	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
657	13.14	225.39	109.28	116.10	0.73	0.204	1.43	0.142	0.99	1.00	0.192	No
658	13.16	225.73	109.48	116.25	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
659	13.18	226.08	109.68	116.40	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
660	13.20	226.43	109.87	116.56	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
661	13.22	226.78	110.07	116.71	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
662	13.24	227.13	110.26	116.86	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
663	13.26	227.48	110.46	117.02	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
664	13.28	227.83	110.66	117.17	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
665	13.30	228.18	110.85	117.33	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
666	13.32	228.53	111.05	117.48	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
667	13.34	228.88	111.25	117.64	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
668	13.37	229.41	111.54	117.87	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
669	13.38	229.58	111.64	117.95	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
670	13.40	229.94	111.83	118.10	0.73	0.202	1.43	0.142	0.99	1.00	0.191	No
671	13.42	230.29	112.03	118.26	0.73	0.202	1.43	0.142	0.99	1.00	0.191	No
672	13.44	230.64	112.23	118.42	0.73	0.202	1.43	0.142	0.99	1.00	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	230.99	112.42	118.57	0.73	0.202	1.43	0.142	0.99	1.00	0.190	No
674	13.48	231.35	112.62	118.73	0.73	0.202	1.43	0.141	0.99	1.00	0.190	No
675	13.50	231.70	112.82	118.88	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
676	13.52	232.05	113.01	119.04	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
677	13.54	232.41	113.21	119.20	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
678	13.56	232.76	113.40	119.36	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
679	13.58	233.11	113.60	119.51	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
680	13.60	233.47	113.80	119.67	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
681	13.62	233.82	113.99	119.83	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
682	13.64	234.18	114.19	119.99	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
683	13.66	234.53	114.38	120.15	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
684	13.68	234.89	114.58	120.31	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
685	13.70	235.24	114.78	120.46	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
686	13.72	235.59	114.97	120.62	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
687	13.74	235.94	115.17	120.77	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
688	13.76	236.29	115.37	120.93	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
689	13.78	236.64	115.56	121.08	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
690	13.80	236.98	115.76	121.23	0.72	0.201	1.43	0.140	0.99	1.00	0.190	No
691	13.83	237.50	116.05	121.45	0.72	0.201	1.43	0.140	0.99	1.00	0.190	No
692	13.84	237.67	116.15	121.52	0.72	0.201	1.43	0.140	0.99	1.00	0.190	No
693	13.86	238.01	116.35	121.66	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
694	13.88	238.34	116.54	121.80	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
695	13.90	238.68	116.74	121.94	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
696	13.92	239.01	116.94	122.07	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
697	13.94	239.34	117.13	122.21	0.71	0.200	1.43	0.140	0.99	1.00	0.190	No
698	13.96	239.66	117.33	122.34	0.71	0.200	1.43	0.140	0.99	1.00	0.190	No
699	13.99	240.15	117.62	122.53	0.71	0.200	1.43	0.140	0.99	1.00	0.190	No
700	14.00	240.32	117.72	122.60	0.71	0.200	1.43	0.140	0.98	1.00	0.190	No
701	14.02	240.64	117.92	122.73	0.71	0.200	1.43	0.140	0.98	1.00	0.189	No
702	14.04	240.97	118.11	122.86	0.71	0.200	1.43	0.140	0.98	1.00	0.189	No
703	14.06	241.30	118.31	122.99	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
704	14.08	241.64	118.50	123.13	0.71	0.200	1.43	0.140	0.98	1.00	0.187	No
705	14.10	241.98	118.70	123.28	0.71	0.200	1.43	0.140	0.98	1.00	0.186	No
706	14.12	242.33	118.90	123.43	0.71	0.200	1.43	0.140	0.98	1.00	0.186	No
707	14.14	242.68	119.09	123.58	0.71	0.199	1.43	0.140	0.98	1.00	0.186	No
708	14.16	243.02	119.29	123.73	0.71	0.199	1.43	0.140	0.98	1.00	0.187	No
709	14.18	243.37	119.49	123.88	0.71	0.199	1.43	0.139	0.98	1.00	0.188	No
710	14.20	243.71	119.68	124.03	0.71	0.199	1.43	0.139	0.98	1.00	0.188	No
711	14.22	244.05	119.88	124.17	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
712	14.24	244.39	120.07	124.31	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
713	14.26	244.72	120.27	124.45	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
714	14.28	245.06	120.47	124.59	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
715	14.30	245.39	120.66	124.73	0.71	0.199	1.43	0.139	0.98	1.00	0.188	No
716	14.32	245.73	120.86	124.87	0.71	0.199	1.43	0.139	0.98	1.00	0.187	No
717	14.34	246.07	121.06	125.02	0.71	0.199	1.43	0.139	0.98	1.00	0.186	No
718	14.36	246.41	121.25	125.16	0.71	0.199	1.43	0.139	0.98	1.00	0.186	No
719	14.38	246.76	121.45	125.31	0.70	0.198	1.43	0.139	0.98	1.00	0.185	No
720	14.40	247.11	121.64	125.46	0.70	0.198	1.43	0.139	0.98	1.00	0.184	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	247.46	121.84	125.62	0.70	0.198	1.43	0.139	0.98	1.00	0.184	No
722	14.44	247.81	122.04	125.78	0.70	0.198	1.43	0.139	0.98	1.00	0.186	No
723	14.46	248.16	122.23	125.93	0.70	0.198	1.43	0.139	0.98	1.00	0.187	No
724	14.48	248.51	122.43	126.08	0.70	0.198	1.43	0.139	0.98	1.00	0.188	No
725	14.50	248.85	122.63	126.23	0.70	0.198	1.43	0.139	0.98	1.00	0.187	No
726	14.52	249.20	122.82	126.38	0.70	0.198	1.43	0.138	0.98	1.00	0.186	No
727	14.55	249.73	123.12	126.61	0.70	0.198	1.43	0.138	0.98	1.00	0.185	No
728	14.56	249.90	123.21	126.69	0.70	0.198	1.43	0.138	0.98	1.00	0.185	No
729	14.58	250.26	123.41	126.85	0.70	0.198	1.43	0.138	0.98	1.00	0.186	No
730	14.60	250.61	123.61	127.00	0.70	0.197	1.43	0.138	0.98	1.00	0.186	No
731	14.62	250.96	123.80	127.16	0.70	0.197	1.43	0.138	0.98	1.00	0.186	No
732	14.64	251.31	124.00	127.32	0.70	0.197	1.43	0.138	0.98	1.00	0.185	No
733	14.66	251.67	124.19	127.47	0.70	0.197	1.43	0.138	0.98	1.00	0.185	No
734	14.68	252.03	124.39	127.64	0.70	0.197	1.43	0.138	0.98	1.00	0.185	No
735	14.70	252.39	124.59	127.80	0.70	0.197	1.43	0.138	0.98	1.00	0.185	No
736	14.72	252.74	124.78	127.96	0.70	0.197	1.43	0.138	0.98	1.00	0.186	No
737	14.74	253.09	124.98	128.12	0.70	0.197	1.43	0.138	0.98	1.00	0.186	No
738	14.76	253.45	125.18	128.27	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
739	14.78	253.79	125.37	128.42	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
740	14.80	254.14	125.57	128.57	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
741	14.82	254.48	125.76	128.72	0.69	0.196	1.43	0.138	0.98	1.00	0.187	No
742	14.84	254.83	125.96	128.87	0.69	0.196	1.43	0.137	0.98	1.00	0.187	No
743	14.86	255.17	126.16	129.01	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
744	14.88	255.51	126.35	129.16	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
745	14.90	255.85	126.55	129.30	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
746	14.92	256.18	126.75	129.44	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
747	14.94	256.52	126.94	129.58	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
748	14.96	256.85	127.14	129.72	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
749	14.98	257.19	127.33	129.86	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
750	15.01	257.69	127.63	130.06	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
751	15.03	258.03	127.82	130.20	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
752	15.04	258.19	127.92	130.27	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
753	15.06	258.53	128.12	130.41	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
754	15.08	258.86	128.31	130.54	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
755	15.10	259.19	128.51	130.68	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
756	15.12	259.52	128.71	130.81	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
757	15.14	259.85	128.90	130.95	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
758	15.16	260.18	129.10	131.08	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
759	15.18	260.50	129.30	131.21	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
760	15.20	260.83	129.49	131.34	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
761	15.22	261.16	129.69	131.47	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
762	15.24	261.48	129.88	131.60	0.69	0.195	1.43	0.136	0.98	1.00	0.185	No
763	15.26	261.81	130.08	131.73	0.69	0.195	1.43	0.136	0.98	1.00	0.185	No
764	15.28	262.14	130.28	131.87	0.68	0.195	1.43	0.136	0.98	1.00	0.185	No
765	15.30	262.47	130.47	132.00	0.68	0.195	1.43	0.136	0.98	1.00	0.185	No
766	15.32	262.81	130.67	132.14	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
767	15.34	263.14	130.87	132.28	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
768	15.36	263.48	131.06	132.41	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	263.81	131.26	132.55	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
770	15.40	264.15	131.45	132.69	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
771	15.42	264.48	131.65	132.83	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
772	15.45	264.98	131.94	133.04	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
773	15.46	265.15	132.04	133.11	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
774	15.48	265.48	132.24	133.24	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
775	15.50	265.82	132.44	133.38	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
776	15.52	266.15	132.63	133.52	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
777	15.54	266.48	132.83	133.65	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.62	82.50	2.74	0.59	1.70	8.84	0.00	8.84	4.000	No	Yes	2.00
2	0.04	0.85	74.65	2.65	0.58	1.70	12.59	0.00	12.59	4.000	No	Yes	2.00
3	0.06	0.96	75.24	2.65	0.57	1.70	16.52	0.00	16.52	4.000	No	Yes	2.00
4	0.08	1.09	77.03	2.68	0.56	1.70	18.19	0.00	18.19	4.000	No	Yes	2.00
5	0.10	1.15	81.74	2.73	0.55	1.70	19.25	0.00	19.25	4.000	No	Yes	2.00
6	0.13	1.18	86.89	2.80	0.55	1.70	19.55	0.00	19.55	4.000	No	Yes	2.00
7	0.14	1.20	90.60	2.85	0.55	1.70	19.93	0.00	19.93	4.000	No	Yes	2.00
8	0.16	1.27	91.85	2.86	0.55	1.70	20.57	0.00	20.57	4.000	No	Yes	2.00
9	0.18	1.28	94.74	2.90	0.54	1.70	23.04	0.00	23.04	4.000	No	Yes	2.00
10	0.20	1.27	98.00	2.94	0.54	1.70	20.39	0.00	20.39	4.000	No	Yes	2.00
11	0.22	1.21	100.00	2.99	0.55	1.70	20.20	0.00	20.20	4.000	No	Yes	2.00
12	0.24	1.21	100.00	3.01	0.55	1.70	20.05	0.00	20.05	4.000	No	Yes	2.00
13	0.26	1.20	100.00	3.02	0.55	1.70	20.05	0.00	20.05	4.000	No	Yes	2.00
14	0.28	1.19	100.00	3.04	0.55	1.70	19.86	0.00	19.86	4.000	No	Yes	2.00
15	0.30	1.17	100.00	3.06	0.55	1.70	19.41	0.00	19.41	4.000	No	Yes	2.00
16	0.32	1.15	100.00	3.08	0.55	1.70	19.29	0.00	19.29	4.000	No	Yes	2.00
17	0.35	1.12	100.00	3.10	0.55	1.70	18.65	0.00	18.65	4.000	No	Yes	2.00
18	0.36	1.09	100.00	3.12	0.55	1.70	18.22	0.00	18.22	4.000	No	Yes	2.00
19	0.38	1.08	100.00	3.13	0.55	1.70	17.61	0.00	17.61	4.000	No	Yes	2.00
20	0.40	1.07	100.00	3.14	0.55	1.70	17.98	0.00	17.98	4.000	No	Yes	2.00
21	0.42	1.08	100.00	3.13	0.55	1.70	17.78	0.00	17.78	4.000	No	Yes	2.00
22	0.44	1.09	100.00	3.12	0.55	1.70	18.16	0.00	18.16	4.000	No	Yes	2.00
23	0.46	1.13	100.00	3.09	0.55	1.70	18.79	0.00	18.79	4.000	No	Yes	2.00
24	0.48	1.19	100.00	3.06	0.55	1.70	19.76	0.00	19.76	4.000	No	Yes	2.00
25	0.50	1.25	100.00	3.02	0.54	1.70	20.84	0.00	20.84	4.000	No	Yes	2.00
26	0.52	1.30	100.00	3.00	0.54	1.70	21.97	0.00	21.97	4.000	No	Yes	2.00
27	0.54	1.33	100.00	2.99	0.54	1.70	22.29	0.00	22.29	4.000	No	Yes	2.00
28	0.56	1.35	100.00	2.99	0.54	1.70	22.46	0.00	22.46	4.000	No	Yes	2.00
29	0.58	1.37	100.00	2.98	0.54	1.70	22.87	0.00	22.87	4.000	No	Yes	2.00
30	0.60	1.41	100.00	2.98	0.53	1.70	23.53	0.00	23.53	4.000	No	Yes	2.00
31	0.62	1.43	100.00	2.99	0.53	1.70	24.16	0.00	24.16	4.000	No	Yes	2.00
32	0.64	1.43	100.00	3.01	0.53	1.70	24.14	0.00	24.14	4.000	No	Yes	2.00
33	0.66	1.40	100.00	3.03	0.54	1.70	23.21	0.00	23.21	4.000	No	Yes	2.00
34	0.68	1.39	100.00	3.04	0.54	1.70	23.01	0.00	23.01	4.000	No	Yes	2.00
35	0.70	1.41	100.00	3.04	0.53	1.70	23.44	0.00	23.44	4.000	No	Yes	2.00
36	0.72	1.43	100.00	3.03	0.53	1.70	24.25	0.00	24.25	4.000	No	Yes	2.00
37	0.74	1.44	100.00	3.03	0.53	1.70	23.97	0.00	23.97	4.000	No	Yes	2.00
38	0.76	1.42	100.00	3.03	0.53	1.70	23.72	0.00	23.72	4.000	No	Yes	2.00
39	0.78	1.43	100.00	3.02	0.53	1.70	23.58	0.00	23.58	4.000	No	Yes	2.00
40	0.80	1.45	100.00	3.01	0.53	1.70	24.19	0.00	24.19	4.000	No	Yes	2.00
41	0.82	1.50	100.00	2.99	0.53	1.70	25.03	0.00	25.03	4.000	No	Yes	2.00
42	0.84	1.53	100.00	2.98	0.53	1.70	25.72	0.00	25.72	4.000	No	Yes	2.00
43	0.86	1.53	100.00	2.98	0.53	1.70	25.78	0.00	25.78	4.000	No	Yes	2.00
44	0.88	1.52	100.00	2.99	0.53	1.70	25.29	0.00	25.29	4.000	No	Yes	2.00
45	0.90	1.51	100.00	3.00	0.53	1.70	25.04	0.00	25.04	4.000	No	Yes	2.00
46	0.92	1.40	100.00	3.04	0.53	1.70	25.23	0.00	25.23	4.000	No	Yes	2.00
47	0.94	1.40	100.00	3.02	0.55	1.70	19.06	0.00	19.06	4.000	No	Yes	2.00
48	0.96	1.40	100.00	3.01	0.53	1.70	24.63	0.00	24.63	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	1.51	99.77	2.96	0.53	1.70	24.70	0.00	24.70	4.000	No	Yes	2.00
50	1.00	1.51	99.67	2.96	0.53	1.70	24.73	0.00	24.73	4.000	No	Yes	2.00
51	1.02	1.50	99.63	2.96	0.53	1.70	24.76	0.00	24.76	4.000	No	Yes	2.00
52	1.04	1.48	99.95	2.96	0.53	1.70	24.57	0.00	24.57	4.000	No	Yes	2.00
53	1.06	1.46	100.00	2.97	0.53	1.70	23.99	0.00	23.99	4.000	No	Yes	2.00
54	1.08	1.44	100.00	2.99	0.53	1.70	23.60	0.00	23.60	4.000	No	Yes	2.00
55	1.10	1.45	100.00	2.99	0.53	1.70	23.78	0.00	23.78	4.000	No	Yes	2.00
56	1.12	1.48	100.00	2.98	0.53	1.70	24.37	0.00	24.37	4.000	No	Yes	2.00
57	1.14	1.50	100.00	2.97	0.53	1.70	24.85	0.00	24.85	4.000	No	Yes	2.00
58	1.16	1.49	100.00	2.97	0.53	1.70	24.72	0.00	24.72	4.000	No	Yes	2.00
59	1.18	1.46	100.00	2.98	0.53	1.70	23.98	0.00	23.98	4.000	No	Yes	2.00
60	1.20	1.45	100.00	2.99	0.53	1.70	23.74	0.00	23.74	4.000	No	Yes	2.00
61	1.22	1.46	100.00	2.99	0.53	1.70	24.06	0.00	24.06	4.000	No	Yes	2.00
62	1.24	1.48	100.00	2.98	0.53	1.70	24.22	0.00	24.22	4.000	No	Yes	2.00
63	1.26	1.49	100.00	2.98	0.53	1.70	24.77	0.00	24.77	4.000	No	Yes	2.00
64	1.28	1.49	100.00	2.98	0.53	1.70	24.71	0.00	24.71	4.000	No	Yes	2.00
65	1.30	1.47	100.00	2.99	0.53	1.70	24.31	0.00	24.31	4.000	No	Yes	2.00
66	1.32	1.45	100.00	2.99	0.53	1.70	23.53	0.00	23.53	4.000	No	Yes	2.00
67	1.34	1.44	100.00	2.99	0.53	1.70	23.55	0.00	23.55	4.000	No	Yes	2.00
68	1.36	1.45	100.00	2.98	0.53	1.70	23.79	0.00	23.79	4.000	No	Yes	2.00
69	1.38	1.46	100.00	2.97	0.53	1.70	24.11	0.00	24.11	4.000	No	Yes	2.00
70	1.40	1.47	100.00	2.97	0.53	1.70	24.42	0.00	24.42	4.000	No	Yes	2.00
71	1.42	1.46	100.00	2.97	0.53	1.70	24.28	0.00	24.28	4.000	No	Yes	2.00
72	1.44	1.43	100.00	2.99	0.53	1.70	23.47	0.00	23.47	4.000	No	Yes	2.00
73	1.46	1.40	100.00	3.01	0.54	1.70	22.99	0.00	22.99	4.000	No	Yes	2.00
74	1.48	1.39	100.00	3.02	0.54	1.70	22.78	0.00	22.78	4.000	No	Yes	2.00
75	1.50	1.38	100.00	3.03	0.54	1.70	22.68	0.00	22.68	4.000	No	Yes	2.00
76	1.52	1.36	100.00	3.04	0.54	1.70	22.46	0.00	22.46	4.000	No	Yes	2.00
77	1.54	1.31	100.00	3.06	0.54	1.70	21.99	0.00	21.99	4.000	No	Yes	2.00
78	1.56	1.23	100.00	3.09	0.54	1.70	20.37	0.00	20.37	4.000	No	Yes	2.00
79	1.58	1.12	100.00	3.14	0.55	1.70	18.46	0.00	18.46	4.000	No	Yes	2.00
80	1.60	0.99	100.00	3.21	0.56	1.70	16.32	0.00	16.32	4.000	No	Yes	2.00
81	1.62	0.86	100.00	3.28	0.57	1.70	13.80	0.00	13.80	4.000	No	Yes	2.00
82	1.64	0.76	100.00	3.35	0.57	1.70	11.96	0.00	11.96	4.000	No	Yes	2.00
83	1.66	0.68	100.00	3.40	0.58	1.70	11.07	0.00	11.07	4.000	No	Yes	2.00
84	1.68	0.64	100.00	3.43	0.58	1.70	10.18	0.00	10.18	4.000	No	Yes	2.00
85	1.70	0.61	100.00	3.43	0.58	1.70	9.74	0.00	9.74	4.000	No	Yes	2.00
86	1.72	0.61	100.00	3.39	0.58	1.70	9.60	0.00	9.60	4.000	No	Yes	2.00
87	1.74	0.65	100.00	3.31	0.58	1.70	10.27	0.00	10.27	4.000	No	Yes	2.00
88	1.76	0.69	100.00	3.23	0.58	1.70	11.43	0.00	11.43	4.000	No	Yes	2.00
89	1.78	0.75	100.00	3.14	0.57	1.70	11.91	0.00	11.91	4.000	No	Yes	2.00
90	1.80	0.78	100.00	3.08	0.57	1.70	12.95	0.00	12.95	4.000	No	Yes	2.00
91	1.82	0.82	100.00	3.03	0.57	1.70	13.40	0.00	13.40	4.000	No	Yes	2.00
92	1.84	0.85	100.00	2.98	0.57	1.70	13.62	0.00	13.62	4.000	No	Yes	2.00
93	1.86	0.89	98.99	2.95	0.56	1.70	14.78	0.00	14.78	4.000	No	Yes	2.00
94	1.88	0.91	97.77	2.93	0.56	1.70	15.15	0.00	15.15	4.000	No	Yes	2.00
95	1.90	0.92	98.38	2.94	0.56	1.70	14.96	0.00	14.96	4.000	No	Yes	2.00
96	1.92	0.91	99.24	2.95	0.56	1.70	14.95	0.00	14.95	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	0.92	99.24	2.95	0.56	1.70	14.89	0.00	14.89	4.000	No	Yes	2.00
98	1.96	0.93	99.85	2.96	0.56	1.70	15.54	0.00	15.54	4.000	No	Yes	2.00
99	1.98	0.93	100.00	2.97	0.56	1.70	15.28	0.00	15.28	4.000	No	Yes	2.00
100	2.00	0.92	100.00	3.00	0.56	1.70	15.20	0.00	15.20	4.000	No	Yes	2.00
101	2.02	0.91	100.00	3.02	0.56	1.70	14.78	0.00	14.78	4.000	No	Yes	2.00
102	2.05	0.88	100.00	3.04	0.56	1.70	14.71	0.00	14.71	4.000	No	Yes	2.00
103	2.06	0.86	100.00	3.06	0.57	1.70	14.18	0.00	14.18	4.000	No	Yes	2.00
104	2.08	0.84	100.00	3.08	0.57	1.70	13.76	0.00	13.76	4.000	No	Yes	2.00
105	2.10	0.81	100.00	3.09	0.57	1.70	13.42	0.00	13.42	4.000	No	Yes	2.00
106	2.12	0.78	100.00	3.11	0.57	1.70	12.74	0.00	12.74	4.000	No	Yes	2.00
107	2.14	0.75	100.00	3.14	0.57	1.70	12.54	0.00	12.54	4.000	No	Yes	2.00
108	2.16	0.72	100.00	3.16	0.58	1.70	11.74	0.00	11.74	4.000	No	Yes	2.00
109	2.18	0.71	100.00	3.17	0.58	1.70	11.51	0.00	11.51	4.000	No	Yes	2.00
110	2.20	0.75	100.00	3.15	0.57	1.70	12.04	0.00	12.04	4.000	No	Yes	2.00
111	2.22	0.80	100.00	3.11	0.57	1.69	13.34	0.00	13.34	4.000	No	Yes	2.00
112	2.24	0.84	100.00	3.08	0.57	1.68	13.96	0.00	13.96	4.000	No	Yes	2.00
113	2.26	0.87	100.00	3.06	0.57	1.67	14.10	0.00	14.10	4.000	No	Yes	2.00
114	2.28	0.88	100.00	3.04	0.57	1.66	14.10	0.00	14.10	4.000	No	Yes	2.00
115	2.30	0.90	100.00	3.00	0.57	1.66	14.28	0.00	14.28	4.000	No	Yes	2.00
116	2.32	0.91	100.00	2.98	0.56	1.65	14.87	0.00	14.87	4.000	No	Yes	2.00
117	2.34	0.92	99.75	2.96	0.57	1.64	14.52	0.00	14.52	4.000	No	Yes	2.00
118	2.36	0.93	99.49	2.96	0.56	1.63	14.70	0.00	14.70	4.000	No	Yes	2.00
119	2.38	0.94	99.14	2.95	0.56	1.62	14.84	0.00	14.84	4.000	No	Yes	2.00
120	2.40	0.94	99.46	2.96	0.56	1.62	14.80	0.00	14.80	4.000	No	Yes	2.00
121	2.42	0.95	99.41	2.96	0.56	1.61	14.77	0.00	14.77	4.000	No	Yes	2.00
122	2.44	0.96	98.82	2.95	0.56	1.60	15.08	0.00	15.08	4.000	No	Yes	2.00
123	2.46	0.97	98.22	2.94	0.56	1.59	15.01	0.00	15.01	4.000	No	Yes	2.00
124	2.48	0.97	97.78	2.93	0.56	1.59	14.84	0.00	14.84	4.000	No	Yes	2.00
125	2.50	0.96	97.98	2.94	0.56	1.58	14.98	0.00	14.98	4.000	No	Yes	2.00
126	2.52	0.96	97.95	2.94	0.57	1.58	14.55	0.00	14.55	4.000	No	Yes	2.00
127	2.54	0.93	99.45	2.96	0.57	1.58	14.38	0.00	14.38	4.000	No	Yes	2.00
128	2.56	0.88	100.00	2.99	0.57	1.58	13.51	0.00	13.51	4.000	No	Yes	2.00
129	2.58	0.82	100.00	3.05	0.57	1.58	12.53	0.00	12.53	4.000	No	Yes	2.00
130	2.60	0.75	100.00	3.11	0.58	1.58	11.46	0.00	11.46	4.000	No	Yes	2.00
131	2.62	0.70	100.00	3.15	0.58	1.58	10.58	0.00	10.58	4.000	No	Yes	2.00
132	2.64	0.67	100.00	3.17	0.58	1.58	10.08	0.00	10.08	4.000	No	Yes	2.00
133	2.66	0.67	100.00	3.15	0.58	1.58	9.82	0.00	9.82	4.000	No	Yes	2.00
134	2.68	0.70	100.00	3.09	0.58	1.58	10.48	0.00	10.48	4.000	No	Yes	2.00
135	2.70	0.76	100.00	3.00	0.58	1.57	11.41	0.00	11.41	4.000	No	Yes	2.00
136	2.72	0.83	96.10	2.91	0.57	1.56	12.57	0.00	12.57	4.000	No	Yes	2.00
137	2.74	0.90	89.71	2.83	0.57	1.56	13.70	0.00	13.70	4.000	No	Yes	2.00
138	2.76	0.94	85.97	2.79	0.57	1.55	14.35	0.00	14.35	4.000	No	Yes	2.00
139	2.78	0.93	85.08	2.78	0.57	1.55	14.20	0.00	14.20	4.000	No	Yes	2.00
140	2.80	0.90	85.61	2.78	0.57	1.55	13.31	0.00	13.31	4.000	No	Yes	2.00
141	2.82	0.88	85.92	2.79	0.57	1.55	12.96	0.00	12.96	4.000	No	Yes	2.00
142	2.84	0.88	84.97	2.77	0.57	1.55	13.14	0.00	13.14	4.000	No	Yes	2.00
143	2.86	0.89	84.62	2.77	0.57	1.54	13.55	0.00	13.55	4.000	No	Yes	2.00
144	2.88	0.90	84.76	2.77	0.57	1.54	13.20	0.00	13.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.98	82.56	2.74	0.57	1.54	13.52	0.00	13.52	4.000	No	Yes	2.00
146	2.92	1.04	81.75	2.73	0.56	1.52	16.63	0.00	16.63	4.000	No	Yes	2.00
147	2.94	1.09	82.38	2.74	0.57	1.52	15.82	0.00	15.82	4.000	No	Yes	2.00
148	2.96	1.05	85.87	2.79	0.57	1.52	15.07	0.00	15.07	4.000	No	Yes	2.00
149	2.98	1.03	88.23	2.82	0.57	1.52	14.88	0.00	14.88	4.000	No	Yes	2.00
150	3.01	1.01	89.54	2.83	0.57	1.52	14.55	0.00	14.55	4.000	No	Yes	2.00
151	3.02	0.99	91.27	2.85	0.57	1.52	14.27	0.00	14.27	4.000	No	Yes	2.00
152	3.04	0.97	92.75	2.87	0.57	1.52	13.86	0.00	13.86	4.000	No	Yes	2.00
153	3.06	0.94	94.08	2.89	0.57	1.52	13.47	0.00	13.47	4.000	No	Yes	2.00
154	3.08	0.93	94.01	2.89	0.57	1.51	13.12	0.00	13.12	4.000	No	Yes	2.00
155	3.10	0.93	92.96	2.87	0.57	1.51	13.17	0.00	13.17	4.000	No	Yes	2.00
156	3.12	0.94	91.25	2.85	0.57	1.51	13.41	0.00	13.41	4.000	No	Yes	2.00
157	3.14	0.94	90.33	2.84	0.57	1.51	13.46	0.00	13.46	4.000	No	Yes	2.00
158	3.16	0.92	90.53	2.84	0.57	1.51	13.18	0.00	13.18	4.000	No	Yes	2.00
159	3.18	0.89	92.22	2.87	0.57	1.50	12.86	0.00	12.86	4.000	No	Yes	2.00
160	3.20	0.87	93.72	2.88	0.58	1.50	12.09	0.00	12.09	4.000	No	Yes	2.00
161	3.22	0.88	93.04	2.88	0.58	1.50	12.08	0.00	12.08	4.000	No	Yes	2.00
162	3.24	0.95	89.14	2.83	0.57	1.50	13.32	0.00	13.32	4.000	No	Yes	2.00
163	3.26	1.05	83.76	2.76	0.57	1.49	14.89	0.00	14.89	4.000	No	Yes	2.00
164	3.28	1.09	82.00	2.74	0.56	1.48	16.20	0.00	16.20	4.000	No	Yes	2.00
165	3.30	1.06	83.70	2.76	0.57	1.48	15.00	0.00	15.00	4.000	No	Yes	2.00
166	3.32	0.98	88.37	2.82	0.57	1.49	13.75	0.00	13.75	4.000	No	Yes	2.00
167	3.34	0.90	92.52	2.87	0.57	1.49	12.50	0.00	12.50	4.000	No	Yes	2.00
168	3.36	0.85	96.33	2.92	0.58	1.49	11.84	0.00	11.84	4.000	No	Yes	2.00
169	3.38	0.85	97.78	2.93	0.58	1.49	11.37	0.00	11.37	4.000	No	Yes	2.00
170	3.40	0.88	96.00	2.91	0.58	1.48	12.12	0.00	12.12	4.000	No	Yes	2.00
171	3.42	0.94	92.35	2.87	0.57	1.47	13.38	0.00	13.38	4.000	No	Yes	2.00
172	3.44	0.96	90.00	2.84	0.57	1.47	13.65	0.00	13.65	4.000	No	Yes	2.00
173	3.46	0.94	89.55	2.83	0.57	1.47	13.00	0.00	13.00	4.000	No	Yes	2.00
174	3.48	0.90	90.15	2.84	0.58	1.47	12.50	0.00	12.50	4.000	No	Yes	2.00
175	3.50	0.89	89.76	2.83	0.58	1.47	11.91	0.00	11.91	4.000	No	Yes	2.00
176	3.52	0.89	88.74	2.82	0.58	1.47	12.12	0.00	12.12	4.000	No	Yes	2.00
177	3.54	0.90	88.27	2.82	0.58	1.47	12.61	0.00	12.61	4.000	No	Yes	2.00
178	3.56	0.92	88.23	2.82	0.58	1.46	12.40	0.00	12.40	4.000	No	Yes	2.00
179	3.58	0.93	88.59	2.82	0.58	1.46	12.67	0.00	12.67	4.000	No	Yes	2.00
180	3.60	0.95	88.21	2.82	0.57	1.46	12.93	0.00	12.93	4.000	No	Yes	2.00
181	3.62	0.96	88.19	2.81	0.57	1.45	13.10	0.00	13.10	4.000	No	Yes	2.00
182	3.64	0.95	89.26	2.83	0.57	1.45	13.21	0.00	13.21	4.000	No	Yes	2.00
183	3.66	0.93	90.55	2.84	0.58	1.45	12.37	0.00	12.37	4.000	No	Yes	2.00
184	3.68	0.89	93.37	2.88	0.57	1.45	12.38	0.00	12.38	4.000	No	Yes	2.00
185	3.70	0.87	95.93	2.91	0.58	1.45	11.70	0.00	11.70	4.000	No	Yes	2.00
186	3.72	0.91	96.15	2.91	0.58	1.45	11.68	0.00	11.68	4.000	No	Yes	2.00
187	3.74	1.02	91.67	2.86	0.57	1.44	13.76	0.00	13.76	4.000	No	Yes	2.00
188	3.76	1.17	84.71	2.77	0.56	1.43	16.31	0.00	16.31	4.000	No	Yes	2.00
189	3.78	1.24	81.84	2.74	0.56	1.42	18.01	0.00	18.01	4.000	No	Yes	2.00
190	3.80	1.22	82.70	2.75	0.56	1.42	16.82	0.00	16.82	4.000	No	Yes	2.00
191	3.82	1.18	84.96	2.77	0.56	1.42	15.81	0.00	15.81	4.000	No	Yes	2.00
192	3.84	1.25	81.20	2.73	0.56	1.42	16.35	0.00	16.35	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	1.39	74.97	2.65	0.56	1.41	19.50	0.00	19.50	4.000	No	Yes	2.00
194	3.88	1.58	70.73	2.60	0.55	1.41	21.68	57.06	78.75	0.115	No	No	0.72
195	3.90	1.71	70.16	2.59	0.54	1.40	23.95	57.62	81.58	0.117	No	No	0.74
196	3.94	1.82	70.23	2.59	0.54	1.39	24.80	57.88	82.68	0.118	No	No	0.75
197	3.94	1.88	69.95	2.59	0.54	1.39	25.95	58.17	84.11	0.120	No	No	0.76
198	3.96	1.92	69.38	2.58	0.53	1.38	26.27	58.15	84.42	0.120	No	No	0.76
199	3.98	1.94	68.42	2.57	0.53	1.38	26.38	58.00	84.38	0.120	No	No	0.76
200	4.01	1.95	67.14	2.55	0.53	1.38	26.66	57.83	84.48	0.120	No	No	0.75
201	4.02	1.93	66.42	2.54	0.54	1.38	26.53	57.64	84.17	0.120	No	No	0.75
202	4.04	1.91	67.03	2.55	0.54	1.38	25.84	57.57	83.41	0.119	No	No	0.74
203	4.06	1.88	68.68	2.57	0.54	1.38	25.59	57.82	83.41	0.119	No	No	0.74
204	4.08	1.84	71.63	2.61	0.54	1.37	25.33	0.00	25.33	4.000	No	Yes	2.00
205	4.10	1.75	76.01	2.66	0.54	1.37	23.92	0.00	23.92	4.000	No	Yes	2.00
206	4.13	1.63	81.88	2.74	0.54	1.37	22.17	0.00	22.17	4.000	No	Yes	2.00
207	4.14	1.54	85.62	2.78	0.55	1.38	20.29	0.00	20.29	4.000	No	Yes	2.00
208	4.16	1.49	86.83	2.80	0.55	1.37	20.31	0.00	20.31	4.000	No	Yes	2.00
209	4.18	1.45	87.14	2.80	0.55	1.37	20.28	0.00	20.28	4.000	No	Yes	2.00
210	4.20	1.37	89.40	2.83	0.55	1.37	18.47	0.00	18.47	4.000	No	Yes	2.00
211	4.22	1.32	91.38	2.85	0.56	1.37	17.31	0.00	17.31	4.000	No	Yes	2.00
212	4.24	1.37	89.69	2.83	0.55	1.37	18.14	0.00	18.14	4.000	No	Yes	2.00
213	4.26	1.47	86.31	2.79	0.55	1.36	20.40	0.00	20.40	4.000	No	Yes	2.00
214	4.28	1.58	83.82	2.76	0.55	1.36	21.22	0.00	21.22	4.000	No	Yes	2.00
215	4.30	1.65	82.99	2.75	0.54	1.35	22.31	0.00	22.31	4.000	No	Yes	2.00
216	4.32	1.72	82.14	2.74	0.54	1.35	22.97	0.00	22.97	4.000	No	Yes	2.00
217	4.34	1.77	80.74	2.72	0.54	1.35	23.60	0.00	23.60	4.000	No	Yes	2.00
218	4.36	1.80	79.02	2.70	0.54	1.35	24.13	0.00	24.13	4.000	No	Yes	2.00
219	4.38	1.77	78.57	2.69	0.54	1.34	24.04	0.00	24.04	4.000	No	Yes	2.00
220	4.40	1.66	80.60	2.72	0.54	1.34	22.64	0.00	22.64	4.000	No	Yes	2.00
221	4.42	1.51	84.08	2.76	0.55	1.35	19.83	0.00	19.83	4.000	No	Yes	2.00
222	4.44	1.35	88.23	2.82	0.56	1.35	17.90	0.00	17.90	4.000	No	Yes	2.00
223	4.46	1.23	90.84	2.85	0.56	1.35	16.38	0.00	16.38	4.000	No	Yes	2.00
224	4.48	1.18	90.54	2.84	0.57	1.35	15.07	0.00	15.07	4.000	No	Yes	2.00
225	4.50	1.19	88.22	2.82	0.56	1.35	16.07	0.00	16.07	4.000	No	Yes	2.00
226	4.52	1.23	86.46	2.79	0.56	1.35	16.63	0.00	16.63	4.000	No	Yes	2.00
227	4.54	1.25	88.16	2.81	0.56	1.34	16.75	0.00	16.75	4.000	No	Yes	2.00
228	4.56	1.20	92.88	2.87	0.56	1.34	16.42	0.00	16.42	4.000	No	Yes	2.00
229	4.58	1.14	96.62	2.92	0.57	1.34	14.71	0.00	14.71	4.000	No	Yes	2.00
230	4.60	1.11	98.39	2.94	0.57	1.34	14.36	0.00	14.36	4.000	No	Yes	2.00
231	4.62	1.14	96.69	2.92	0.56	1.34	15.30	0.00	15.30	4.000	No	Yes	2.00
232	4.64	1.21	94.27	2.89	0.56	1.34	15.83	0.00	15.83	4.000	No	Yes	2.00
233	4.66	1.30	90.88	2.85	0.56	1.33	16.93	0.00	16.93	4.000	No	Yes	2.00
234	4.68	1.42	87.50	2.81	0.55	1.33	18.78	0.00	18.78	4.000	No	Yes	2.00
235	4.70	1.51	85.04	2.78	0.55	1.32	20.13	0.00	20.13	4.000	No	Yes	2.00
236	4.72	1.57	83.45	2.76	0.55	1.32	20.53	0.00	20.53	4.000	No	Yes	2.00
237	4.74	1.63	81.16	2.73	0.55	1.32	21.08	0.00	21.08	4.000	No	Yes	2.00
238	4.76	1.69	78.54	2.69	0.54	1.31	22.27	0.00	22.27	4.000	No	Yes	2.00
239	4.78	1.73	76.36	2.67	0.54	1.31	22.59	0.00	22.59	4.000	No	Yes	2.00
240	4.80	1.75	75.48	2.66	0.54	1.31	22.62	0.00	22.62	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	1.73	75.70	2.66	0.54	1.31	22.78	0.00	22.78	4.000	No	Yes	2.00
242	4.84	1.65	78.39	2.69	0.55	1.31	21.90	0.00	21.90	4.000	No	Yes	2.00
243	4.86	1.53	80.15	2.71	0.55	1.31	19.34	0.00	19.34	4.000	No	Yes	2.00
244	4.88	1.38	84.76	2.77	0.56	1.31	18.32	0.00	18.32	4.000	No	Yes	2.00
245	4.90	1.24	89.48	2.83	0.56	1.31	16.08	0.00	16.08	4.000	No	Yes	2.00
246	4.92	1.09	96.92	2.92	0.57	1.31	13.92	0.00	13.92	4.000	No	Yes	2.00
247	4.94	1.04	99.44	2.96	0.57	1.31	12.81	0.00	12.81	4.000	No	Yes	2.00
248	4.96	1.19	93.84	2.89	0.57	1.31	14.06	0.00	14.06	4.000	No	Yes	2.00
249	4.98	1.47	84.19	2.76	0.55	1.30	19.25	0.00	19.25	4.000	No	Yes	2.00
250	5.00	1.76	77.46	2.68	0.54	1.29	23.48	0.00	23.48	4.000	No	Yes	2.00
251	5.03	1.86	75.82	2.66	0.54	1.28	24.60	0.00	24.60	4.000	No	Yes	2.00
252	5.04	1.79	78.07	2.69	0.54	1.29	22.81	0.00	22.81	4.000	No	Yes	2.00
253	5.06	1.56	84.28	2.77	0.55	1.29	20.82	0.00	20.82	4.000	No	Yes	2.00
254	5.08	1.33	90.78	2.85	0.56	1.29	16.00	0.00	16.00	4.000	No	Yes	2.00
255	5.10	1.21	95.01	2.90	0.57	1.30	14.43	0.00	14.43	4.000	No	Yes	2.00
256	5.13	1.34	89.31	2.83	0.56	1.29	16.06	0.00	16.06	4.000	No	Yes	2.00
257	5.14	1.60	80.83	2.72	0.55	1.28	20.63	0.00	20.63	4.000	No	Yes	2.00
258	5.16	1.84	75.89	2.66	0.54	1.27	24.06	0.00	24.06	4.000	No	Yes	2.00
259	5.18	1.91	76.15	2.66	0.54	1.27	24.85	0.00	24.85	4.000	No	Yes	2.00
260	5.20	1.76	81.22	2.73	0.54	1.27	23.10	0.00	23.10	4.000	No	Yes	2.00
261	5.22	1.52	88.35	2.82	0.55	1.28	18.54	0.00	18.54	4.000	No	Yes	2.00
262	5.24	1.33	95.09	2.90	0.56	1.28	15.93	0.00	15.93	4.000	No	Yes	2.00
263	5.26	1.32	95.28	2.90	0.56	1.28	15.96	0.00	15.96	4.000	No	Yes	2.00
264	5.28	1.44	90.58	2.84	0.55	1.27	18.27	0.00	18.27	4.000	No	Yes	2.00
265	5.30	1.44	90.78	2.85	0.55	1.27	20.06	0.00	20.06	4.000	No	Yes	2.00
266	5.32	1.31	95.70	2.91	0.56	1.27	16.06	0.00	16.06	4.000	No	Yes	2.00
267	5.34	1.11	100.00	3.02	0.57	1.28	13.51	0.00	13.51	4.000	No	Yes	2.00
268	5.36	1.02	100.00	3.07	0.57	1.28	12.47	0.00	12.47	4.000	No	Yes	2.00
269	5.38	1.04	100.00	3.03	0.57	1.27	12.53	0.00	12.53	4.000	No	Yes	2.00
270	5.40	1.17	98.23	2.94	0.57	1.27	14.34	0.00	14.34	4.000	No	Yes	2.00
271	5.42	1.31	91.89	2.86	0.56	1.26	17.03	0.00	17.03	4.000	No	Yes	2.00
272	5.44	1.33	92.24	2.87	0.56	1.26	17.82	0.00	17.82	4.000	No	Yes	2.00
273	5.46	1.22	97.50	2.93	0.56	1.26	15.05	0.00	15.05	4.000	No	Yes	2.00
274	5.48	1.08	100.00	3.01	0.57	1.27	12.93	0.00	12.93	4.000	No	Yes	2.00
275	5.50	1.06	100.00	3.01	0.57	1.26	12.64	0.00	12.64	4.000	No	Yes	2.00
276	5.52	1.18	97.08	2.93	0.57	1.26	14.33	0.00	14.33	4.000	No	Yes	2.00
277	5.54	1.35	90.11	2.84	0.56	1.25	17.24	0.00	17.24	4.000	No	Yes	2.00
278	5.56	1.48	86.67	2.80	0.55	1.25	18.78	0.00	18.78	4.000	No	Yes	2.00
279	5.58	1.50	87.24	2.80	0.55	1.25	18.75	0.00	18.75	4.000	No	Yes	2.00
280	5.60	1.46	89.29	2.83	0.56	1.25	17.94	0.00	17.94	4.000	No	Yes	2.00
281	5.62	1.40	90.79	2.85	0.56	1.25	17.29	0.00	17.29	4.000	No	Yes	2.00
282	5.64	1.32	93.03	2.88	0.56	1.25	16.49	0.00	16.49	4.000	No	Yes	2.00
283	5.66	1.21	97.64	2.93	0.56	1.25	14.88	0.00	14.88	4.000	No	Yes	2.00
284	5.68	1.09	100.00	3.01	0.57	1.25	13.29	0.00	13.29	4.000	No	Yes	2.00
285	5.70	1.03	100.00	3.06	0.57	1.25	12.18	0.00	12.18	4.000	No	Yes	2.00
286	5.72	1.07	100.00	3.03	0.57	1.25	12.71	0.00	12.71	4.000	No	Yes	2.00
287	5.74	1.25	96.62	2.92	0.57	1.24	14.69	0.00	14.69	4.000	No	Yes	2.00
288	5.76	1.51	86.71	2.80	0.55	1.23	18.48	0.00	18.48	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	1.64	82.47	2.74	0.54	1.23	21.88	0.00	21.88	4.000	No	Yes	2.00
290	5.80	1.58	85.46	2.78	0.55	1.23	19.43	0.00	19.43	4.000	No	Yes	2.00
291	5.82	1.34	95.24	2.90	0.56	1.23	16.23	0.00	16.23	4.000	No	Yes	2.00
292	5.84	1.12	100.00	3.03	0.57	1.24	13.06	0.00	13.06	4.000	No	Yes	2.00
293	5.86	1.06	100.00	3.07	0.58	1.24	11.56	0.00	11.56	4.000	No	Yes	2.00
294	5.88	1.06	100.00	3.09	0.57	1.23	14.10	0.00	14.10	4.000	No	Yes	2.00
295	5.90	1.07	100.00	3.09	0.57	1.23	12.50	0.00	12.50	4.000	No	Yes	2.00
296	5.92	1.00	100.00	3.13	0.57	1.23	12.00	0.00	12.00	4.000	No	Yes	2.00
297	5.94	0.96	100.00	3.12	0.58	1.23	11.31	0.00	11.31	4.000	No	Yes	2.00
298	5.96	0.97	100.00	3.08	0.58	1.23	11.03	0.00	11.03	4.000	No	Yes	2.00
299	5.98	1.04	100.00	3.01	0.57	1.23	12.41	0.00	12.41	4.000	No	Yes	2.00
300	6.00	1.13	97.45	2.93	0.57	1.22	13.52	0.00	13.52	4.000	No	Yes	2.00
301	6.02	1.18	94.79	2.90	0.57	1.22	14.18	0.00	14.18	4.000	No	Yes	2.00
302	6.04	1.18	94.92	2.90	0.57	1.22	14.21	0.00	14.21	4.000	No	Yes	2.00
303	6.06	1.15	96.29	2.92	0.57	1.22	13.53	0.00	13.53	4.000	No	Yes	2.00
304	6.08	1.12	98.45	2.94	0.57	1.22	13.19	0.00	13.19	4.000	No	Yes	2.00
305	6.10	1.11	100.00	2.97	0.57	1.22	13.09	0.00	13.09	4.000	No	Yes	2.00
306	6.12	1.11	100.00	2.99	0.57	1.21	13.00	0.00	13.00	4.000	No	Yes	2.00
307	6.14	1.10	100.00	3.01	0.57	1.21	13.03	0.00	13.03	4.000	No	Yes	2.00
308	6.16	1.10	100.00	3.01	0.57	1.21	12.83	0.00	12.83	4.000	No	Yes	2.00
309	6.18	1.06	100.00	3.02	0.57	1.21	12.66	0.00	12.66	4.000	No	Yes	2.00
310	6.20	1.00	100.00	3.03	0.58	1.21	11.56	0.00	11.56	4.000	No	Yes	2.00
311	6.22	0.97	100.00	3.03	0.58	1.21	10.99	0.00	10.99	4.000	No	Yes	2.00
312	6.24	1.04	100.00	2.99	0.58	1.21	11.54	0.00	11.54	4.000	No	Yes	2.00
313	6.26	1.14	97.33	2.93	0.57	1.20	13.72	0.00	13.72	4.000	No	Yes	2.00
314	6.28	1.20	95.43	2.91	0.57	1.20	14.47	0.00	14.47	4.000	No	Yes	2.00
315	6.30	1.18	96.82	2.92	0.57	1.20	13.59	0.00	13.59	4.000	No	Yes	2.00
316	6.32	1.10	100.00	2.99	0.57	1.20	13.15	0.00	13.15	4.000	No	Yes	2.00
317	6.34	1.01	100.00	3.05	0.58	1.20	11.53	0.00	11.53	4.000	No	Yes	2.00
318	6.36	0.91	100.00	3.12	0.58	1.20	10.41	0.00	10.41	4.000	No	Yes	2.00
319	6.38	0.84	100.00	3.17	0.58	1.20	9.82	0.00	9.82	4.000	No	Yes	2.00
320	6.40	0.79	100.00	3.22	0.59	1.20	8.93	0.00	8.93	4.000	No	Yes	2.00
321	6.42	0.76	100.00	3.24	0.59	1.20	8.71	0.00	8.71	4.000	No	Yes	2.00
322	6.44	0.77	100.00	3.21	0.59	1.20	8.78	0.00	8.78	4.000	No	Yes	2.00
323	6.46	0.79	100.00	3.17	0.59	1.20	9.06	0.00	9.06	4.000	No	Yes	2.00
324	6.48	0.80	100.00	3.15	0.58	1.19	9.45	0.00	9.45	4.000	No	Yes	2.00
325	6.50	0.79	100.00	3.15	0.59	1.19	9.10	0.00	9.10	4.000	No	Yes	2.00
326	6.52	0.75	100.00	3.16	0.59	1.19	8.46	0.00	8.46	4.000	No	Yes	2.00
327	6.54	0.69	100.00	3.20	0.59	1.19	8.01	0.00	8.01	4.000	No	Yes	2.00
328	6.56	0.65	100.00	3.23	0.59	1.19	7.32	0.00	7.32	4.000	No	Yes	2.00
329	6.58	0.62	100.00	3.27	0.59	1.19	7.05	0.00	7.05	4.000	No	Yes	2.00
330	6.60	0.61	100.00	3.28	0.60	1.19	6.75	0.00	6.75	4.000	No	Yes	2.00
331	6.62	0.62	100.00	3.25	0.59	1.19	6.91	0.00	6.91	4.000	No	Yes	2.00
332	6.64	0.65	100.00	3.19	0.59	1.19	7.48	0.00	7.48	4.000	No	Yes	2.00
333	6.66	0.67	100.00	3.15	0.59	1.19	7.58	0.00	7.58	4.000	No	Yes	2.00
334	6.68	0.68	100.00	3.13	0.59	1.18	7.73	0.00	7.73	4.000	No	Yes	2.00
335	6.70	0.68	100.00	3.14	0.59	1.18	7.65	0.00	7.65	4.000	No	Yes	2.00
336	6.72	0.67	100.00	3.17	0.59	1.18	7.54	0.00	7.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	0.67	100.00	3.18	0.59	1.18	7.36	0.00	7.36	4.000	No	Yes	2.00
338	6.76	0.66	100.00	3.19	0.59	1.18	7.51	0.00	7.51	4.000	No	Yes	2.00
339	6.78	0.67	100.00	3.19	0.59	1.18	7.48	0.00	7.48	4.000	No	Yes	2.00
340	6.80	0.66	100.00	3.19	0.59	1.18	7.53	0.00	7.53	4.000	No	Yes	2.00
341	6.82	0.64	100.00	3.21	0.59	1.18	7.27	0.00	7.27	4.000	No	Yes	2.00
342	6.84	0.63	100.00	3.24	0.59	1.18	6.82	0.00	6.82	4.000	No	Yes	2.00
343	6.86	0.62	100.00	3.26	0.59	1.17	7.06	0.00	7.06	4.000	No	Yes	2.00
344	6.88	0.63	100.00	3.25	0.59	1.17	6.87	0.00	6.87	4.000	No	Yes	2.00
345	6.90	0.65	100.00	3.22	0.59	1.17	7.17	0.00	7.17	4.000	No	Yes	2.00
346	6.92	0.66	100.00	3.19	0.59	1.17	7.58	0.00	7.58	4.000	No	Yes	2.00
347	6.95	0.65	100.00	3.20	0.59	1.17	7.39	0.00	7.39	4.000	No	Yes	2.00
348	6.96	0.61	100.00	3.23	0.60	1.17	6.61	0.00	6.61	4.000	No	Yes	2.00
349	6.98	0.56	100.00	3.27	0.60	1.17	6.22	0.00	6.22	4.000	No	Yes	2.00
350	7.00	0.55	100.00	3.27	0.60	1.17	5.83	0.00	5.83	4.000	No	Yes	2.00
351	7.02	0.54	100.00	3.27	0.60	1.17	6.06	0.00	6.06	4.000	No	Yes	2.00
352	7.04	0.54	100.00	3.28	0.60	1.17	5.77	0.00	5.77	4.000	No	Yes	2.00
353	7.06	0.54	100.00	3.27	0.60	1.17	5.74	0.00	5.74	4.000	No	Yes	2.00
354	7.08	0.56	100.00	3.24	0.60	1.16	6.14	0.00	6.14	4.000	No	Yes	2.00
355	7.10	0.57	100.00	3.22	0.60	1.16	6.35	0.00	6.35	4.000	No	Yes	2.00
356	7.13	0.57	100.00	3.23	0.60	1.16	6.29	0.00	6.29	4.000	No	Yes	2.00
357	7.14	0.59	100.00	3.24	0.60	1.16	6.16	0.00	6.16	4.000	No	Yes	2.00
358	7.16	0.64	100.00	3.19	0.60	1.16	6.74	0.00	6.74	4.000	No	Yes	2.00
359	7.18	0.71	100.00	3.14	0.59	1.16	7.99	0.00	7.99	4.000	No	Yes	2.00
360	7.20	0.73	100.00	3.14	0.59	1.15	8.42	0.00	8.42	4.000	No	Yes	2.00
361	7.22	0.70	100.00	3.18	0.59	1.15	7.49	0.00	7.49	4.000	No	Yes	2.00
362	7.24	0.67	100.00	3.23	0.59	1.15	7.08	0.00	7.08	4.000	No	Yes	2.00
363	7.26	0.67	100.00	3.21	0.59	1.15	7.30	0.00	7.30	4.000	No	Yes	2.00
364	7.28	0.68	100.00	3.19	0.59	1.15	7.63	0.00	7.63	4.000	No	Yes	2.00
365	7.30	0.68	100.00	3.21	0.59	1.15	7.47	0.00	7.47	4.000	No	Yes	2.00
366	7.32	0.65	100.00	3.25	0.59	1.15	7.19	0.00	7.19	4.000	No	Yes	2.00
367	7.34	0.62	100.00	3.29	0.60	1.15	6.75	0.00	6.75	4.000	No	Yes	2.00
368	7.36	0.58	100.00	3.34	0.60	1.15	6.34	0.00	6.34	4.000	No	Yes	2.00
369	7.38	0.55	100.00	3.35	0.60	1.15	5.68	0.00	5.68	4.000	No	Yes	2.00
370	7.40	0.58	100.00	3.30	0.60	1.15	5.95	0.00	5.95	4.000	No	Yes	2.00
371	7.42	0.65	100.00	3.20	0.59	1.14	7.13	0.00	7.13	4.000	No	Yes	2.00
372	7.45	0.72	100.00	3.11	0.59	1.14	7.83	0.00	7.83	4.000	No	Yes	2.00
373	7.46	0.77	100.00	3.07	0.59	1.14	8.41	0.00	8.41	4.000	No	Yes	2.00
374	7.48	0.81	100.00	3.06	0.59	1.14	8.68	0.00	8.68	4.000	No	Yes	2.00
375	7.50	0.86	100.00	3.06	0.59	1.14	9.30	0.00	9.30	4.000	No	Yes	2.00
376	7.52	0.92	100.00	3.05	0.58	1.14	10.12	0.00	10.12	4.000	No	Yes	2.00
377	7.54	0.98	100.00	3.04	0.58	1.13	10.64	0.00	10.64	4.000	No	Yes	2.00
378	7.56	1.02	100.00	3.05	0.58	1.13	11.05	0.00	11.05	4.000	No	Yes	2.00
379	7.58	1.04	100.00	3.06	0.58	1.13	11.37	0.00	11.37	4.000	No	Yes	2.00
380	7.60	1.06	100.00	3.07	0.58	1.13	11.53	0.00	11.53	4.000	No	Yes	2.00
381	7.62	1.09	100.00	3.07	0.58	1.13	11.64	0.00	11.64	4.000	No	Yes	2.00
382	7.64	1.13	100.00	3.07	0.57	1.13	12.43	0.00	12.43	4.000	No	Yes	2.00
383	7.66	1.15	100.00	3.08	0.57	1.12	12.81	0.00	12.81	4.000	No	Yes	2.00
384	7.68	1.12	100.00	3.11	0.57	1.12	12.23	0.00	12.23	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	1.09	100.00	3.16	0.58	1.12	11.72	0.00	11.72	4.000	No	Yes	2.00
386	7.72	1.05	100.00	3.20	0.58	1.12	11.55	0.00	11.55	4.000	No	Yes	2.00
387	7.74	1.01	100.00	3.24	0.58	1.12	10.95	0.00	10.95	4.000	No	Yes	2.00
388	7.76	0.97	100.00	3.28	0.58	1.12	10.41	0.00	10.41	4.000	No	Yes	2.00
389	7.78	0.94	100.00	3.31	0.58	1.12	10.32	0.00	10.32	4.000	No	Yes	2.00
390	7.80	0.93	100.00	3.32	0.58	1.12	9.99	0.00	9.99	4.000	No	Yes	2.00
391	7.82	0.92	100.00	3.32	0.58	1.12	9.97	0.00	9.97	4.000	No	Yes	2.00
392	7.84	0.93	100.00	3.30	0.58	1.12	10.08	0.00	10.08	4.000	No	Yes	2.00
393	7.86	0.94	100.00	3.28	0.58	1.11	10.29	0.00	10.29	4.000	No	Yes	2.00
394	7.88	0.94	100.00	3.27	0.58	1.11	10.11	0.00	10.11	4.000	No	Yes	2.00
395	7.90	0.94	100.00	3.27	0.58	1.11	10.10	0.00	10.10	4.000	No	Yes	2.00
396	7.92	0.94	100.00	3.26	0.58	1.11	9.99	0.00	9.99	4.000	No	Yes	2.00
397	7.94	0.95	100.00	3.25	0.58	1.11	10.27	0.00	10.27	4.000	No	Yes	2.00
398	7.96	0.97	100.00	3.23	0.58	1.11	10.43	0.00	10.43	4.000	No	Yes	2.00
399	7.99	0.97	100.00	3.23	0.58	1.11	10.46	0.00	10.46	4.000	No	Yes	2.00
400	8.00	0.96	100.00	3.23	0.58	1.11	10.16	0.00	10.16	4.000	No	Yes	2.00
401	8.02	0.96	100.00	3.23	0.58	1.10	10.27	0.00	10.27	4.000	No	Yes	2.00
402	8.04	0.97	100.00	3.22	0.58	1.10	10.21	0.00	10.21	4.000	No	Yes	2.00
403	8.06	0.99	100.00	3.22	0.58	1.10	10.47	0.00	10.47	4.000	No	Yes	2.00
404	8.08	1.02	100.00	3.20	0.58	1.10	10.89	0.00	10.89	4.000	No	Yes	2.00
405	8.10	1.07	100.00	3.18	0.58	1.10	11.24	0.00	11.24	4.000	No	Yes	2.00
406	8.12	1.11	100.00	3.16	0.57	1.10	11.91	0.00	11.91	4.000	No	Yes	2.00
407	8.14	1.14	100.00	3.14	0.57	1.10	12.25	0.00	12.25	4.000	No	Yes	2.00
408	8.16	1.16	100.00	3.15	0.57	1.09	12.26	0.00	12.26	4.000	No	Yes	2.00
409	8.18	1.15	100.00	3.16	0.57	1.09	12.32	0.00	12.32	4.000	No	Yes	2.00
410	8.20	1.13	100.00	3.18	0.57	1.09	12.01	0.00	12.01	4.000	No	Yes	2.00
411	8.22	1.10	100.00	3.21	0.58	1.09	11.54	0.00	11.54	4.000	No	Yes	2.00
412	8.24	1.07	100.00	3.23	0.58	1.09	11.26	0.00	11.26	4.000	No	Yes	2.00
413	8.26	1.04	100.00	3.26	0.58	1.09	11.13	0.00	11.13	4.000	No	Yes	2.00
414	8.28	1.00	100.00	3.29	0.58	1.09	10.46	0.00	10.46	4.000	No	Yes	2.00
415	8.30	0.96	100.00	3.31	0.58	1.09	10.11	0.00	10.11	4.000	No	Yes	2.00
416	8.32	0.93	100.00	3.32	0.58	1.09	9.69	0.00	9.69	4.000	No	Yes	2.00
417	8.34	0.91	100.00	3.33	0.58	1.09	9.60	0.00	9.60	4.000	No	Yes	2.00
418	8.36	0.89	100.00	3.34	0.58	1.08	9.44	0.00	9.44	4.000	No	Yes	2.00
419	8.38	0.87	100.00	3.35	0.59	1.08	9.02	0.00	9.02	4.000	No	Yes	2.00
420	8.40	0.83	100.00	3.38	0.59	1.08	8.84	0.00	8.84	4.000	No	Yes	2.00
421	8.42	0.81	100.00	3.41	0.59	1.08	8.33	0.00	8.33	4.000	No	Yes	2.00
422	8.44	0.79	100.00	3.42	0.59	1.08	8.19	0.00	8.19	4.000	No	Yes	2.00
423	8.46	0.79	100.00	3.41	0.59	1.08	8.28	0.00	8.28	4.000	No	Yes	2.00
424	8.48	0.78	100.00	3.41	0.59	1.08	8.34	0.00	8.34	4.000	No	Yes	2.00
425	8.50	0.76	100.00	3.42	0.59	1.08	7.87	0.00	7.87	4.000	No	Yes	2.00
426	8.52	0.73	100.00	3.44	0.59	1.08	7.48	0.00	7.48	4.000	No	Yes	2.00
427	8.54	0.70	100.00	3.46	0.59	1.08	7.40	0.00	7.40	4.000	No	Yes	2.00
428	8.56	0.68	100.00	3.47	0.59	1.08	6.96	0.00	6.96	4.000	No	Yes	2.00
429	8.58	0.65	100.00	3.50	0.60	1.07	6.79	0.00	6.79	4.000	No	Yes	2.00
430	8.60	0.62	100.00	3.53	0.60	1.07	6.42	0.00	6.42	4.000	No	Yes	2.00
431	8.62	0.60	100.00	3.54	0.60	1.07	6.06	0.00	6.06	4.000	No	Yes	2.00
432	8.64	0.59	100.00	3.54	0.60	1.07	6.05	0.00	6.05	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	0.58	100.00	3.52	0.60	1.07	6.02	0.00	6.02	4.000	No	Yes	2.00
434	8.68	0.58	100.00	3.50	0.60	1.07	5.88	0.00	5.88	4.000	No	Yes	2.00
435	8.70	0.56	100.00	3.49	0.60	1.07	5.85	0.00	5.85	4.000	No	Yes	2.00
436	8.72	0.56	100.00	3.48	0.60	1.07	5.58	0.00	5.58	4.000	No	Yes	2.00
437	8.74	0.53	100.00	3.50	0.60	1.07	5.60	0.00	5.60	4.000	No	Yes	2.00
438	8.76	0.51	100.00	3.52	0.60	1.07	5.10	0.00	5.10	4.000	No	Yes	2.00
439	8.78	0.48	100.00	3.56	0.60	1.07	4.80	0.00	4.80	4.000	No	Yes	2.00
440	8.80	0.47	100.00	3.55	0.60	1.06	4.58	0.00	4.58	4.000	No	Yes	2.00
441	8.82	0.50	100.00	3.47	0.60	1.06	4.91	0.00	4.91	4.000	No	Yes	2.00
442	8.84	0.54	100.00	3.39	0.60	1.06	5.50	0.00	5.50	4.000	No	Yes	2.00
443	8.86	0.57	100.00	3.33	0.60	1.06	5.59	0.00	5.59	4.000	No	Yes	2.00
444	8.88	0.59	100.00	3.31	0.60	1.06	5.73	0.00	5.73	4.000	No	Yes	2.00
445	8.90	0.60	100.00	3.29	0.60	1.06	5.92	0.00	5.92	4.000	No	Yes	2.00
446	8.92	0.60	100.00	3.29	0.60	1.06	5.96	0.00	5.96	4.000	No	Yes	2.00
447	8.94	0.59	100.00	3.32	0.60	1.06	5.77	0.00	5.77	4.000	No	Yes	2.00
448	8.96	0.59	100.00	3.33	0.60	1.06	5.63	0.00	5.63	4.000	No	Yes	2.00
449	8.98	0.61	100.00	3.31	0.60	1.06	5.79	0.00	5.79	4.000	No	Yes	2.00
450	9.00	0.66	100.00	3.25	0.60	1.06	6.37	0.00	6.37	4.000	No	Yes	2.00
451	9.02	0.73	100.00	3.18	0.59	1.05	7.28	0.00	7.28	4.000	No	Yes	2.00
452	9.05	0.78	100.00	3.14	0.59	1.05	7.70	0.00	7.70	4.000	No	Yes	2.00
453	9.06	0.81	100.00	3.13	0.59	1.05	7.98	0.00	7.98	4.000	No	Yes	2.00
454	9.08	0.83	100.00	3.14	0.59	1.05	8.18	0.00	8.18	4.000	No	Yes	2.00
455	9.10	0.85	100.00	3.15	0.59	1.05	8.36	0.00	8.36	4.000	No	Yes	2.00
456	9.12	0.88	100.00	3.15	0.59	1.05	8.64	0.00	8.64	4.000	No	Yes	2.00
457	9.14	0.90	100.00	3.14	0.59	1.05	9.01	0.00	9.01	4.000	No	Yes	2.00
458	9.16	0.91	100.00	3.16	0.59	1.05	9.12	0.00	9.12	4.000	No	Yes	2.00
459	9.18	0.90	100.00	3.19	0.59	1.05	8.88	0.00	8.88	4.000	No	Yes	2.00
460	9.20	0.88	100.00	3.23	0.59	1.05	8.73	0.00	8.73	4.000	No	Yes	2.00
461	9.22	0.85	100.00	3.26	0.59	1.04	8.36	0.00	8.36	4.000	No	Yes	2.00
462	9.25	0.81	100.00	3.29	0.59	1.04	8.02	0.00	8.02	4.000	No	Yes	2.00
463	9.26	0.78	100.00	3.33	0.59	1.04	7.67	0.00	7.67	4.000	No	Yes	2.00
464	9.28	0.73	100.00	3.38	0.59	1.04	7.20	0.00	7.20	4.000	No	Yes	2.00
465	9.30	0.69	100.00	3.43	0.60	1.04	6.66	0.00	6.66	4.000	No	Yes	2.00
466	9.32	0.67	100.00	3.45	0.60	1.04	6.47	0.00	6.47	4.000	No	Yes	2.00
467	9.34	0.66	100.00	3.45	0.60	1.04	6.40	0.00	6.40	4.000	No	Yes	2.00
468	9.36	0.66	100.00	3.44	0.60	1.04	6.39	0.00	6.39	4.000	No	Yes	2.00
469	9.38	0.66	100.00	3.42	0.60	1.04	6.38	0.00	6.38	4.000	No	Yes	2.00
470	9.40	0.65	100.00	3.41	0.60	1.04	6.38	0.00	6.38	4.000	No	Yes	2.00
471	9.42	0.63	100.00	3.42	0.60	1.04	6.12	0.00	6.12	4.000	No	Yes	2.00
472	9.44	0.62	100.00	3.42	0.60	1.04	5.86	0.00	5.86	4.000	No	Yes	2.00
473	9.46	0.60	100.00	3.43	0.60	1.03	5.88	0.00	5.88	4.000	No	Yes	2.00
474	9.48	0.59	100.00	3.45	0.60	1.03	5.62	0.00	5.62	4.000	No	Yes	2.00
475	9.50	0.56	100.00	3.48	0.60	1.03	5.41	0.00	5.41	4.000	No	Yes	2.00
476	9.52	0.54	100.00	3.51	0.60	1.03	5.20	0.00	5.20	4.000	No	Yes	2.00
477	9.54	0.52	100.00	3.53	0.60	1.03	4.94	0.00	4.94	4.000	No	Yes	2.00
478	9.56	0.52	100.00	3.52	0.60	1.03	4.80	0.00	4.80	4.000	No	Yes	2.00
479	9.58	0.53	100.00	3.49	0.60	1.03	5.07	0.00	5.07	4.000	No	Yes	2.00
480	9.60	0.55	100.00	3.44	0.60	1.03	5.18	0.00	5.18	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	0.56	100.00	3.41	0.60	1.03	5.29	0.00	5.29	4.000	No	Yes	2.00
482	9.64	0.55	100.00	3.39	0.60	1.03	5.35	0.00	5.35	4.000	No	Yes	2.00
483	9.66	0.54	100.00	3.40	0.60	1.03	5.10	0.00	5.10	4.000	No	Yes	2.00
484	9.68	0.51	100.00	3.42	0.60	1.03	4.80	0.00	4.80	4.000	No	Yes	2.00
485	9.70	0.50	100.00	3.42	0.60	1.02	4.62	0.00	4.62	4.000	No	Yes	2.00
486	9.72	0.50	100.00	3.41	0.60	1.02	4.78	0.00	4.78	4.000	No	Yes	2.00
487	9.74	0.52	100.00	3.37	0.60	1.02	4.68	0.00	4.68	4.000	No	Yes	2.00
488	9.76	0.57	100.00	3.29	0.60	1.02	5.11	0.00	5.11	4.000	No	Yes	2.00
489	9.78	0.67	100.00	3.17	0.60	1.02	6.29	0.00	6.29	4.000	No	Yes	2.00
490	9.80	0.89	100.00	3.01	0.59	1.02	7.70	0.00	7.70	4.000	No	Yes	2.00
491	9.82	1.07	98.44	2.94	0.58	1.02	11.85	0.00	11.85	4.000	No	Yes	2.00
492	9.84	1.18	97.51	2.93	0.57	1.02	12.21	0.00	12.21	4.000	No	Yes	2.00
493	9.86	1.07	100.00	3.02	0.58	1.02	11.13	0.00	11.13	4.000	No	Yes	2.00
494	9.88	0.86	100.00	3.16	0.59	1.02	8.66	0.00	8.66	4.000	No	Yes	2.00
495	9.90	0.66	100.00	3.36	0.60	1.02	6.12	0.00	6.12	4.000	No	Yes	2.00
496	9.92	0.54	100.00	3.51	0.60	1.02	4.99	0.00	4.99	4.000	No	Yes	2.00
497	9.94	0.51	100.00	3.55	0.60	1.02	5.03	0.00	5.03	4.000	No	Yes	2.00
498	9.96	0.52	100.00	3.51	0.60	1.01	4.98	0.00	4.98	4.000	No	Yes	2.00
499	9.98	0.53	100.00	3.45	0.60	1.01	5.18	0.00	5.18	4.000	No	Yes	2.00
500	10.01	0.54	100.00	3.42	0.60	1.01	5.35	0.00	5.35	4.000	No	Yes	2.00
501	10.02	0.54	100.00	3.41	0.60	1.01	5.33	0.00	5.33	4.000	No	Yes	2.00
502	10.04	0.53	100.00	3.41	0.60	1.01	5.08	0.00	5.08	4.000	No	Yes	2.00
503	10.06	0.53	100.00	3.40	0.60	1.01	5.01	0.00	5.01	4.000	No	Yes	2.00
504	10.08	0.56	100.00	3.35	0.60	1.01	5.19	0.00	5.19	4.000	No	Yes	2.00
505	10.10	0.68	100.00	3.18	0.60	1.01	5.97	0.00	5.97	4.000	No	Yes	2.00
506	10.12	0.92	100.00	2.96	0.59	1.01	8.68	0.00	8.68	4.000	No	Yes	2.00
507	10.14	1.26	84.85	2.77	0.58	1.01	12.28	0.00	12.28	4.000	No	Yes	2.00
508	10.16	1.47	79.14	2.70	0.57	1.01	16.12	0.00	16.12	4.000	No	Yes	2.00
509	10.18	1.43	81.40	2.73	0.57	1.01	14.95	0.00	14.95	4.000	No	Yes	2.00
510	10.20	1.17	92.83	2.87	0.58	1.01	11.18	0.00	11.18	4.000	No	Yes	2.00
511	10.22	0.89	100.00	3.08	0.59	1.00	8.49	0.00	8.49	4.000	No	Yes	2.00
512	10.24	0.73	100.00	3.25	0.60	1.00	6.36	0.00	6.36	4.000	No	Yes	2.00
513	10.26	0.65	100.00	3.34	0.60	1.00	6.16	0.00	6.16	4.000	No	Yes	2.00
514	10.28	0.63	100.00	3.37	0.60	1.00	6.04	0.00	6.04	4.000	No	Yes	2.00
515	10.30	0.63	100.00	3.38	0.60	1.00	5.77	0.00	5.77	4.000	No	Yes	2.00
516	10.32	0.64	100.00	3.35	0.60	1.00	6.06	0.00	6.06	4.000	No	Yes	2.00
517	10.34	0.67	100.00	3.30	0.60	1.00	6.41	0.00	6.41	4.000	No	Yes	2.00
518	10.36	0.69	100.00	3.26	0.60	1.00	6.52	0.00	6.52	4.000	No	Yes	2.00
519	10.38	0.72	100.00	3.21	0.60	1.00	6.76	0.00	6.76	4.000	No	Yes	2.00
520	10.40	0.77	100.00	3.17	0.59	1.00	7.33	0.00	7.33	4.000	No	Yes	2.00
521	10.42	0.87	100.00	3.09	0.59	1.00	7.88	0.00	7.88	4.000	No	Yes	2.00
522	10.44	1.08	99.58	2.96	0.58	1.00	9.60	0.00	9.60	4.000	No	Yes	2.00
523	10.46	1.40	86.45	2.79	0.57	1.00	13.50	0.00	13.50	4.000	No	Yes	2.00
524	10.48	1.72	78.06	2.69	0.56	1.00	17.63	0.00	17.63	4.000	No	Yes	2.00
525	10.50	1.80	78.86	2.70	0.56	0.99	19.01	0.00	19.01	4.000	No	Yes	2.00
526	10.52	1.64	86.50	2.79	0.56	0.99	15.96	0.00	15.96	4.000	No	Yes	2.00
527	10.54	1.36	97.69	2.93	0.57	0.99	12.94	0.00	12.94	4.000	No	Yes	2.00
528	10.56	1.23	100.00	3.00	0.58	0.99	10.85	0.00	10.85	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	1.25	100.00	2.98	0.58	0.99	11.86	0.00	11.86	4.000	No	Yes	2.00
530	10.60	1.36	97.51	2.93	0.57	0.99	13.59	0.00	13.59	4.000	No	Yes	2.00
531	10.62	1.39	97.98	2.94	0.57	0.99	13.93	0.00	13.93	4.000	No	Yes	2.00
532	10.64	1.26	100.00	3.02	0.57	0.99	12.69	0.00	12.69	4.000	No	Yes	2.00
533	10.66	1.16	100.00	3.07	0.58	0.99	9.95	0.00	9.95	4.000	No	Yes	2.00
534	10.68	1.26	100.00	3.00	0.58	0.99	11.04	0.00	11.04	4.000	No	Yes	2.00
535	10.70	1.56	90.13	2.84	0.56	0.99	15.49	0.00	15.49	4.000	No	Yes	2.00
536	10.72	1.77	83.90	2.76	0.56	0.99	18.42	0.00	18.42	4.000	No	Yes	2.00
537	10.74	1.71	87.32	2.80	0.56	0.98	17.30	0.00	17.30	4.000	No	Yes	2.00
538	10.76	1.46	96.83	2.92	0.57	0.98	13.87	0.00	13.87	4.000	No	Yes	2.00
539	10.78	1.16	100.00	3.08	0.58	0.98	11.03	0.00	11.03	4.000	No	Yes	2.00
540	10.80	1.04	100.00	3.13	0.59	0.98	8.41	0.00	8.41	4.000	No	Yes	2.00
541	10.82	1.02	100.00	3.14	0.58	0.98	10.40	0.00	10.40	4.000	No	Yes	2.00
542	10.84	1.06	100.00	3.13	0.58	0.98	10.34	0.00	10.34	4.000	No	Yes	2.00
543	10.86	1.00	100.00	3.18	0.59	0.98	9.25	0.00	9.25	4.000	No	Yes	2.00
544	10.88	0.95	100.00	3.20	0.59	0.98	8.69	0.00	8.69	4.000	No	Yes	2.00
545	10.90	0.93	100.00	3.21	0.59	0.98	8.95	0.00	8.95	4.000	No	Yes	2.00
546	10.92	0.89	100.00	3.23	0.59	0.98	8.61	0.00	8.61	4.000	No	Yes	2.00
547	10.94	0.87	100.00	3.24	0.59	0.98	7.54	0.00	7.54	4.000	No	Yes	2.00
548	10.96	0.90	100.00	3.21	0.59	0.98	8.46	0.00	8.46	4.000	No	Yes	2.00
549	10.98	0.97	100.00	3.15	0.58	0.97	9.35	0.00	9.35	4.000	No	Yes	2.00
550	11.00	1.01	100.00	3.12	0.58	0.97	9.56	0.00	9.56	4.000	No	Yes	2.00
551	11.02	1.04	100.00	3.11	0.58	0.97	9.57	0.00	9.57	4.000	No	Yes	2.00
552	11.04	1.07	100.00	3.08	0.58	0.97	10.06	0.00	10.06	4.000	No	Yes	2.00
553	11.06	1.09	100.00	3.07	0.58	0.97	10.59	0.00	10.59	4.000	No	Yes	2.00
554	11.08	1.09	100.00	3.08	0.58	0.97	10.15	0.00	10.15	4.000	No	Yes	2.00
555	11.10	1.03	100.00	3.14	0.58	0.97	10.01	0.00	10.01	4.000	No	Yes	2.00
556	11.12	0.96	100.00	3.21	0.59	0.97	8.90	0.00	8.90	4.000	No	Yes	2.00
557	11.14	0.88	100.00	3.28	0.59	0.97	8.09	0.00	8.09	4.000	No	Yes	2.00
558	11.16	0.84	100.00	3.32	0.59	0.97	7.74	0.00	7.74	4.000	No	Yes	2.00
559	11.19	0.79	100.00	3.35	0.59	0.97	7.52	0.00	7.52	4.000	No	Yes	2.00
560	11.20	0.75	100.00	3.37	0.59	0.97	6.89	0.00	6.89	4.000	No	Yes	2.00
561	11.22	0.73	100.00	3.37	0.60	0.97	6.49	0.00	6.49	4.000	No	Yes	2.00
562	11.24	0.74	100.00	3.34	0.59	0.96	6.96	0.00	6.96	4.000	No	Yes	2.00
563	11.26	0.77	100.00	3.29	0.59	0.96	6.93	0.00	6.93	4.000	No	Yes	2.00
564	11.28	0.80	100.00	3.25	0.59	0.96	7.40	0.00	7.40	4.000	No	Yes	2.00
565	11.30	0.82	100.00	3.21	0.59	0.96	7.70	0.00	7.70	4.000	No	Yes	2.00
566	11.32	0.81	100.00	3.22	0.59	0.96	7.67	0.00	7.67	4.000	No	Yes	2.00
567	11.34	0.78	100.00	3.25	0.59	0.96	7.13	0.00	7.13	4.000	No	Yes	2.00
568	11.36	0.76	100.00	3.28	0.60	0.96	6.78	0.00	6.78	4.000	No	Yes	2.00
569	11.38	0.76	100.00	3.29	0.59	0.96	7.07	0.00	7.07	4.000	No	Yes	2.00
570	11.40	0.74	100.00	3.31	0.59	0.96	6.96	0.00	6.96	4.000	No	Yes	2.00
571	11.42	0.72	100.00	3.34	0.60	0.96	6.42	0.00	6.42	4.000	No	Yes	2.00
572	11.44	0.70	100.00	3.37	0.60	0.96	6.44	0.00	6.44	4.000	No	Yes	2.00
573	11.46	0.70	100.00	3.37	0.60	0.96	6.35	0.00	6.35	4.000	No	Yes	2.00
574	11.48	0.72	100.00	3.33	0.60	0.96	6.33	0.00	6.33	4.000	No	Yes	2.00
575	11.50	0.80	100.00	3.24	0.59	0.96	7.13	0.00	7.13	4.000	No	Yes	2.00
576	11.52	0.93	100.00	3.11	0.59	0.96	8.30	0.00	8.30	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	1.08	100.00	3.02	0.58	0.96	10.21	0.00	10.21	4.000	No	Yes	2.00
578	11.56	1.24	98.98	2.95	0.58	0.95	11.27	0.00	11.27	4.000	No	Yes	2.00
579	11.58	1.41	94.51	2.89	0.57	0.95	12.78	0.00	12.78	4.000	No	Yes	2.00
580	11.60	1.59	91.69	2.86	0.56	0.95	15.22	0.00	15.22	4.000	No	Yes	2.00
581	11.62	1.76	89.77	2.83	0.56	0.95	16.34	0.00	16.34	4.000	No	Yes	2.00
582	11.64	1.84	90.33	2.84	0.56	0.95	17.50	0.00	17.50	4.000	No	Yes	2.00
583	11.66	1.82	93.65	2.88	0.56	0.95	17.64	0.00	17.64	4.000	No	Yes	2.00
584	11.68	1.69	97.94	2.94	0.56	0.95	15.62	0.00	15.62	4.000	No	Yes	2.00
585	11.70	1.50	100.00	3.01	0.57	0.95	13.98	0.00	13.98	4.000	No	Yes	2.00
586	11.72	1.46	100.00	2.98	0.57	0.95	12.16	0.00	12.16	4.000	No	Yes	2.00
587	11.74	1.62	93.49	2.88	0.57	0.95	14.59	0.00	14.59	4.000	No	Yes	2.00
588	11.76	1.90	83.85	2.76	0.56	0.95	18.25	0.00	18.25	4.000	No	Yes	2.00
589	11.78	2.03	79.92	2.71	0.55	0.95	20.01	0.00	20.01	4.000	No	Yes	2.00
590	11.80	2.00	81.76	2.73	0.56	0.95	18.44	0.00	18.44	4.000	No	Yes	2.00
591	11.82	1.89	85.78	2.78	0.56	0.95	17.28	0.00	17.28	4.000	No	Yes	2.00
592	11.84	1.86	87.98	2.81	0.56	0.95	16.91	0.00	16.91	4.000	No	Yes	2.00
593	11.86	1.86	88.52	2.82	0.56	0.95	17.70	0.00	17.70	4.000	No	Yes	2.00
594	11.89	1.80	90.72	2.85	0.56	0.94	17.11	0.00	17.11	4.000	No	Yes	2.00
595	11.90	1.69	95.25	2.90	0.56	0.94	15.42	0.00	15.42	4.000	No	Yes	2.00
596	11.92	1.64	98.54	2.94	0.57	0.94	14.54	0.00	14.54	4.000	No	Yes	2.00
597	11.94	1.69	95.74	2.91	0.56	0.94	15.54	0.00	15.54	4.000	No	Yes	2.00
598	11.96	1.73	92.50	2.87	0.56	0.94	16.92	0.00	16.92	4.000	No	Yes	2.00
599	11.98	1.67	91.15	2.85	0.56	0.94	15.55	0.00	15.55	4.000	No	Yes	2.00
600	12.00	1.54	94.75	2.90	0.57	0.94	13.92	0.00	13.92	4.000	No	Yes	2.00
601	12.03	1.41	98.96	2.95	0.57	0.94	13.13	0.00	13.13	4.000	No	Yes	2.00
602	12.04	1.24	100.00	3.04	0.57	0.94	11.95	0.00	11.95	4.000	No	Yes	2.00
603	12.06	1.02	100.00	3.18	0.59	0.94	9.16	0.00	9.16	4.000	No	Yes	2.00
604	12.08	0.80	100.00	3.35	0.59	0.93	6.91	0.00	6.91	4.000	No	Yes	2.00
605	12.10	0.69	100.00	3.47	0.60	0.93	5.91	0.00	5.91	4.000	No	Yes	2.00
606	12.12	0.67	100.00	3.48	0.60	0.93	5.94	0.00	5.94	4.000	No	Yes	2.00
607	12.14	0.70	100.00	3.43	0.60	0.93	6.35	0.00	6.35	4.000	No	Yes	2.00
608	12.16	0.73	100.00	3.37	0.60	0.93	6.62	0.00	6.62	4.000	No	Yes	2.00
609	12.18	0.74	100.00	3.35	0.60	0.93	6.73	0.00	6.73	4.000	No	Yes	2.00
610	12.20	0.79	100.00	3.29	0.60	0.93	6.58	0.00	6.58	4.000	No	Yes	2.00
611	12.22	1.00	100.00	3.11	0.59	0.93	7.99	0.00	7.99	4.000	No	Yes	2.00
612	12.24	1.30	95.93	2.91	0.57	0.93	12.49	0.00	12.49	4.000	No	Yes	2.00
613	12.26	1.51	88.42	2.82	0.57	0.93	14.87	0.00	14.87	4.000	No	Yes	2.00
614	12.28	1.46	93.38	2.88	0.57	0.93	13.72	0.00	13.72	4.000	No	Yes	2.00
615	12.30	1.21	100.00	3.06	0.58	0.93	11.13	0.00	11.13	4.000	No	Yes	2.00
616	12.32	0.95	100.00	3.25	0.59	0.93	8.08	0.00	8.08	4.000	No	Yes	2.00
617	12.34	0.75	100.00	3.43	0.60	0.92	6.56	0.00	6.56	4.000	No	Yes	2.00
618	12.36	0.65	100.00	3.54	0.60	0.92	5.71	0.00	5.71	4.000	No	Yes	2.00
619	12.38	0.61	100.00	3.60	0.60	0.92	5.21	0.00	5.21	4.000	No	Yes	2.00
620	12.40	0.59	100.00	3.62	0.60	0.92	5.39	0.00	5.39	4.000	No	Yes	2.00
621	12.42	0.59	100.00	3.62	0.60	0.92	5.12	0.00	5.12	4.000	No	Yes	2.00
622	12.44	0.58	100.00	3.61	0.60	0.92	5.12	0.00	5.12	4.000	No	Yes	2.00
623	12.46	0.57	100.00	3.58	0.60	0.92	5.09	0.00	5.09	4.000	No	Yes	2.00
624	12.48	0.57	100.00	3.55	0.60	0.92	4.98	0.00	4.98	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	0.58	100.00	3.51	0.60	0.92	5.02	0.00	5.02	4.000	No	Yes	2.00
626	12.52	0.61	100.00	3.45	0.60	0.92	5.41	0.00	5.41	4.000	No	Yes	2.00
627	12.54	0.65	100.00	3.39	0.60	0.92	5.80	0.00	5.80	4.000	No	Yes	2.00
628	12.56	0.72	100.00	3.32	0.60	0.92	6.12	0.00	6.12	4.000	No	Yes	2.00
629	12.58	0.79	100.00	3.28	0.59	0.92	7.22	0.00	7.22	4.000	No	Yes	2.00
630	12.60	0.85	100.00	3.25	0.59	0.92	7.63	0.00	7.63	4.000	No	Yes	2.00
631	12.62	0.83	100.00	3.30	0.59	0.92	7.66	0.00	7.66	4.000	No	Yes	2.00
632	12.64	0.77	100.00	3.42	0.60	0.92	6.72	0.00	6.72	4.000	No	Yes	2.00
633	12.66	0.69	100.00	3.54	0.60	0.91	5.82	0.00	5.82	4.000	No	Yes	2.00
634	12.68	0.66	100.00	3.60	0.60	0.91	5.67	0.00	5.67	4.000	No	Yes	2.00
635	12.70	0.67	100.00	3.60	0.60	0.91	5.89	0.00	5.89	4.000	No	Yes	2.00
636	12.72	0.68	100.00	3.58	0.60	0.91	5.97	0.00	5.97	4.000	No	Yes	2.00
637	12.74	0.68	100.00	3.57	0.60	0.91	5.93	0.00	5.93	4.000	No	Yes	2.00
638	12.76	0.68	100.00	3.55	0.60	0.91	5.84	0.00	5.84	4.000	No	Yes	2.00
639	12.78	0.70	100.00	3.50	0.60	0.91	5.98	0.00	5.98	4.000	No	Yes	2.00
640	12.81	0.72	100.00	3.45	0.60	0.91	6.21	0.00	6.21	4.000	No	Yes	2.00
641	12.82	0.74	100.00	3.42	0.60	0.91	6.41	0.00	6.41	4.000	No	Yes	2.00
642	12.84	0.76	100.00	3.41	0.60	0.91	6.47	0.00	6.47	4.000	No	Yes	2.00
643	12.86	0.76	100.00	3.40	0.60	0.91	6.58	0.00	6.58	4.000	No	Yes	2.00
644	12.88	0.79	100.00	3.38	0.60	0.91	6.62	0.00	6.62	4.000	No	Yes	2.00
645	12.90	0.82	100.00	3.35	0.59	0.91	7.04	0.00	7.04	4.000	No	Yes	2.00
646	12.92	0.87	100.00	3.30	0.59	0.91	7.52	0.00	7.52	4.000	No	Yes	2.00
647	12.94	0.90	100.00	3.28	0.59	0.91	7.88	0.00	7.88	4.000	No	Yes	2.00
648	12.96	0.91	100.00	3.27	0.59	0.91	7.84	0.00	7.84	4.000	No	Yes	2.00
649	12.98	0.90	100.00	3.29	0.59	0.91	7.77	0.00	7.77	4.000	No	Yes	2.00
650	13.00	0.90	100.00	3.30	0.59	0.90	7.62	0.00	7.62	4.000	No	Yes	2.00
651	13.02	0.91	100.00	3.29	0.59	0.90	7.66	0.00	7.66	4.000	No	Yes	2.00
652	13.04	0.93	100.00	3.29	0.59	0.90	8.12	0.00	8.12	4.000	No	Yes	2.00
653	13.07	0.95	100.00	3.29	0.59	0.90	8.11	0.00	8.11	4.000	No	Yes	2.00
654	13.08	0.96	100.00	3.29	0.59	0.90	8.21	0.00	8.21	4.000	No	Yes	2.00
655	13.10	0.98	100.00	3.29	0.59	0.90	8.30	0.00	8.30	4.000	No	Yes	2.00
656	13.12	1.01	100.00	3.27	0.59	0.90	8.72	0.00	8.72	4.000	No	Yes	2.00
657	13.14	1.04	100.00	3.26	0.59	0.90	8.93	0.00	8.93	4.000	No	Yes	2.00
658	13.16	1.05	100.00	3.27	0.59	0.90	9.15	0.00	9.15	4.000	No	Yes	2.00
659	13.18	1.05	100.00	3.28	0.59	0.90	8.94	0.00	8.94	4.000	No	Yes	2.00
660	13.20	1.05	100.00	3.29	0.59	0.90	8.99	0.00	8.99	4.000	No	Yes	2.00
661	13.22	1.05	100.00	3.30	0.59	0.90	8.98	0.00	8.98	4.000	No	Yes	2.00
662	13.24	1.06	100.00	3.30	0.59	0.90	9.09	0.00	9.09	4.000	No	Yes	2.00
663	13.26	1.07	100.00	3.30	0.59	0.90	9.13	0.00	9.13	4.000	No	Yes	2.00
664	13.28	1.07	100.00	3.30	0.59	0.90	9.16	0.00	9.16	4.000	No	Yes	2.00
665	13.30	1.07	100.00	3.31	0.59	0.90	9.09	0.00	9.09	4.000	No	Yes	2.00
666	13.32	1.07	100.00	3.32	0.59	0.90	9.06	0.00	9.06	4.000	No	Yes	2.00
667	13.34	1.07	100.00	3.32	0.59	0.89	9.15	0.00	9.15	4.000	No	Yes	2.00
668	13.37	1.09	100.00	3.31	0.59	0.89	9.24	0.00	9.24	4.000	No	Yes	2.00
669	13.38	1.11	100.00	3.29	0.58	0.89	9.47	0.00	9.47	4.000	No	Yes	2.00
670	13.40	1.12	100.00	3.28	0.58	0.89	9.66	0.00	9.66	4.000	No	Yes	2.00
671	13.42	1.13	100.00	3.28	0.58	0.89	9.61	0.00	9.61	4.000	No	Yes	2.00
672	13.44	1.14	100.00	3.28	0.58	0.89	9.70	0.00	9.70	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	1.15	100.00	3.27	0.58	0.89	9.67	0.00	9.67	4.000	No	Yes	2.00
674	13.48	1.14	100.00	3.28	0.58	0.89	9.84	0.00	9.84	4.000	No	Yes	2.00
675	13.50	1.14	100.00	3.28	0.58	0.89	9.67	0.00	9.67	4.000	No	Yes	2.00
676	13.52	1.14	100.00	3.29	0.58	0.89	9.49	0.00	9.49	4.000	No	Yes	2.00
677	13.54	1.14	100.00	3.29	0.58	0.89	9.81	0.00	9.81	4.000	No	Yes	2.00
678	13.56	1.15	100.00	3.29	0.58	0.89	9.72	0.00	9.72	4.000	No	Yes	2.00
679	13.58	1.13	100.00	3.31	0.58	0.89	9.68	0.00	9.68	4.000	No	Yes	2.00
680	13.60	1.11	100.00	3.33	0.58	0.89	9.35	0.00	9.35	4.000	No	Yes	2.00
681	13.62	1.08	100.00	3.36	0.59	0.89	9.04	0.00	9.04	4.000	No	Yes	2.00
682	13.64	1.05	100.00	3.38	0.59	0.88	8.89	0.00	8.89	4.000	No	Yes	2.00
683	13.66	1.03	100.00	3.40	0.59	0.88	8.64	0.00	8.64	4.000	No	Yes	2.00
684	13.68	1.01	100.00	3.41	0.59	0.88	8.50	0.00	8.50	4.000	No	Yes	2.00
685	13.70	0.98	100.00	3.43	0.59	0.88	8.25	0.00	8.25	4.000	No	Yes	2.00
686	13.72	0.95	100.00	3.45	0.59	0.88	8.03	0.00	8.03	4.000	No	Yes	2.00
687	13.74	0.90	100.00	3.48	0.59	0.88	7.54	0.00	7.54	4.000	No	Yes	2.00
688	13.76	0.85	100.00	3.52	0.59	0.88	7.12	0.00	7.12	4.000	No	Yes	2.00
689	13.78	0.80	100.00	3.54	0.60	0.88	6.55	0.00	6.55	4.000	No	Yes	2.00
690	13.80	0.77	100.00	3.56	0.60	0.88	6.33	0.00	6.33	4.000	No	Yes	2.00
691	13.83	0.75	100.00	3.57	0.60	0.88	6.17	0.00	6.17	4.000	No	Yes	2.00
692	13.84	0.73	100.00	3.57	0.60	0.88	5.97	0.00	5.97	4.000	No	Yes	2.00
693	13.86	0.72	100.00	3.55	0.60	0.88	5.79	0.00	5.79	4.000	No	Yes	2.00
694	13.88	0.72	100.00	3.52	0.60	0.87	5.91	0.00	5.91	4.000	No	Yes	2.00
695	13.90	0.74	100.00	3.48	0.60	0.87	6.06	0.00	6.06	4.000	No	Yes	2.00
696	13.92	0.75	100.00	3.44	0.60	0.87	6.19	0.00	6.19	4.000	No	Yes	2.00
697	13.94	0.75	100.00	3.42	0.60	0.87	6.15	0.00	6.15	4.000	No	Yes	2.00
698	13.96	0.74	100.00	3.41	0.60	0.87	6.07	0.00	6.07	4.000	No	Yes	2.00
699	13.99	0.75	100.00	3.38	0.60	0.87	5.96	0.00	5.96	4.000	No	Yes	2.00
700	14.00	0.83	100.00	3.28	0.60	0.87	6.43	0.00	6.43	4.000	No	Yes	2.00
701	14.02	1.00	100.00	3.13	0.59	0.87	8.07	0.00	8.07	4.000	No	Yes	2.00
702	14.04	1.24	100.00	2.97	0.58	0.87	10.20	0.00	10.20	4.000	No	Yes	2.00
703	14.06	1.58	88.55	2.82	0.57	0.87	12.71	0.00	12.71	4.000	No	Yes	2.00
704	14.08	1.94	80.02	2.71	0.56	0.88	17.03	0.00	17.03	4.000	No	Yes	2.00
705	14.10	2.22	76.29	2.67	0.55	0.88	19.74	0.00	19.74	4.000	No	Yes	2.00
706	14.12	2.27	77.57	2.68	0.55	0.88	20.42	0.00	20.42	4.000	No	Yes	2.00
707	14.14	2.10	82.86	2.75	0.56	0.88	18.30	0.00	18.30	4.000	No	Yes	2.00
708	14.16	1.77	92.81	2.87	0.56	0.87	15.19	0.00	15.19	4.000	No	Yes	2.00
709	14.18	1.42	100.00	3.04	0.58	0.87	11.77	0.00	11.77	4.000	No	Yes	2.00
710	14.20	1.12	100.00	3.21	0.59	0.87	9.21	0.00	9.21	4.000	No	Yes	2.00
711	14.22	0.91	100.00	3.36	0.59	0.87	7.41	0.00	7.41	4.000	No	Yes	2.00
712	14.24	0.79	100.00	3.46	0.60	0.86	6.26	0.00	6.26	4.000	No	Yes	2.00
713	14.26	0.76	100.00	3.47	0.60	0.86	5.99	0.00	5.99	4.000	No	Yes	2.00
714	14.28	0.92	100.00	3.29	0.60	0.86	6.62	0.00	6.62	4.000	No	Yes	2.00
715	14.30	1.32	100.00	3.01	0.58	0.87	10.41	0.00	10.41	4.000	No	Yes	2.00
716	14.32	1.80	84.24	2.77	0.56	0.87	16.25	0.00	16.25	4.000	No	Yes	2.00
717	14.34	2.20	74.23	2.64	0.56	0.87	19.05	0.00	19.05	4.000	No	Yes	2.00
718	14.36	2.43	69.76	2.58	0.55	0.87	20.72	56.61	77.33	0.114	No	No	0.61
719	14.38	2.59	69.29	2.58	0.55	0.87	22.33	56.99	79.33	0.115	No	No	0.62
720	14.40	2.66	70.56	2.59	0.54	0.87	23.26	57.49	80.76	0.117	No	No	0.63

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	2.46	78.08	2.69	0.54	0.87	22.51	0.00	22.51	4.000	No	Yes	2.00
722	14.44	2.08	88.73	2.82	0.56	0.87	17.01	0.00	17.01	4.000	No	Yes	2.00
723	14.46	1.56	100.00	3.01	0.57	0.86	13.48	0.00	13.48	4.000	No	Yes	2.00
724	14.48	1.30	100.00	3.12	0.59	0.86	9.12	0.00	9.12	4.000	No	Yes	2.00
725	14.50	1.34	100.00	3.10	0.58	0.86	10.18	0.00	10.18	4.000	No	Yes	2.00
726	14.52	1.66	98.67	2.95	0.57	0.86	14.23	0.00	14.23	4.000	No	Yes	2.00
727	14.55	1.98	90.00	2.84	0.56	0.86	17.29	0.00	17.29	4.000	No	Yes	2.00
728	14.56	2.04	89.60	2.83	0.55	0.87	18.34	0.00	18.34	4.000	No	Yes	2.00
729	14.58	1.87	95.84	2.91	0.56	0.86	15.83	0.00	15.83	4.000	No	Yes	2.00
730	14.60	1.66	100.00	3.01	0.57	0.86	13.14	0.00	13.14	4.000	No	Yes	2.00
731	14.62	1.66	100.00	3.00	0.57	0.86	12.89	0.00	12.89	4.000	No	Yes	2.00
732	14.64	1.87	96.74	2.92	0.56	0.86	15.68	0.00	15.68	4.000	No	Yes	2.00
733	14.66	2.06	92.18	2.86	0.55	0.86	18.48	0.00	18.48	4.000	No	Yes	2.00
734	14.68	2.03	95.23	2.90	0.55	0.86	17.83	0.00	17.83	4.000	No	Yes	2.00
735	14.70	1.79	100.00	3.01	0.56	0.86	14.88	0.00	14.88	4.000	No	Yes	2.00
736	14.72	1.50	100.00	3.14	0.57	0.86	12.20	0.00	12.20	4.000	No	Yes	2.00
737	14.74	1.25	100.00	3.25	0.58	0.85	10.42	0.00	10.42	4.000	No	Yes	2.00
738	14.76	1.13	100.00	3.31	0.59	0.85	8.47	0.00	8.47	4.000	No	Yes	2.00
739	14.78	1.02	100.00	3.37	0.59	0.85	9.15	0.00	9.15	4.000	No	Yes	2.00
740	14.80	0.97	100.00	3.40	0.59	0.85	7.54	0.00	7.54	4.000	No	Yes	2.00
741	14.82	0.93	100.00	3.41	0.59	0.85	7.27	0.00	7.27	4.000	No	Yes	2.00
742	14.84	1.02	100.00	3.31	0.59	0.85	7.83	0.00	7.83	4.000	No	Yes	2.00
743	14.86	1.18	100.00	3.17	0.58	0.85	9.75	0.00	9.75	4.000	No	Yes	2.00
744	14.88	1.26	100.00	3.10	0.58	0.85	11.51	0.00	11.51	4.000	No	Yes	2.00
745	14.90	1.18	100.00	3.15	0.58	0.85	9.74	0.00	9.74	4.000	No	Yes	2.00
746	14.92	1.04	100.00	3.24	0.59	0.85	7.83	0.00	7.83	4.000	No	Yes	2.00
747	14.94	0.98	100.00	3.28	0.59	0.85	7.80	0.00	7.80	4.000	No	Yes	2.00
748	14.96	0.98	100.00	3.25	0.59	0.85	8.18	0.00	8.18	4.000	No	Yes	2.00
749	14.98	0.98	100.00	3.26	0.59	0.85	7.97	0.00	7.97	4.000	No	Yes	2.00
750	15.01	0.97	100.00	3.28	0.59	0.84	7.69	0.00	7.69	4.000	No	Yes	2.00
751	15.03	0.98	100.00	3.27	0.59	0.84	7.95	0.00	7.95	4.000	No	Yes	2.00
752	15.04	1.00	100.00	3.24	0.59	0.84	8.14	0.00	8.14	4.000	No	Yes	2.00
753	15.06	1.01	100.00	3.22	0.59	0.84	8.19	0.00	8.19	4.000	No	Yes	2.00
754	15.08	1.00	100.00	3.22	0.59	0.84	8.09	0.00	8.09	4.000	No	Yes	2.00
755	15.10	0.96	100.00	3.25	0.59	0.84	7.86	0.00	7.86	4.000	No	Yes	2.00
756	15.12	0.92	100.00	3.29	0.59	0.84	7.31	0.00	7.31	4.000	No	Yes	2.00
757	15.14	0.88	100.00	3.32	0.59	0.84	6.99	0.00	6.99	4.000	No	Yes	2.00
758	15.16	0.87	100.00	3.31	0.59	0.84	6.87	0.00	6.87	4.000	No	Yes	2.00
759	15.18	0.88	100.00	3.29	0.59	0.84	7.00	0.00	7.00	4.000	No	Yes	2.00
760	15.20	0.90	100.00	3.26	0.59	0.84	7.19	0.00	7.19	4.000	No	Yes	2.00
761	15.22	0.95	100.00	3.22	0.59	0.84	7.47	0.00	7.47	4.000	No	Yes	2.00
762	15.24	1.00	100.00	3.19	0.59	0.84	8.22	0.00	8.22	4.000	No	Yes	2.00
763	15.26	1.05	100.00	3.17	0.59	0.84	8.25	0.00	8.25	4.000	No	Yes	2.00
764	15.28	1.05	100.00	3.17	0.59	0.84	8.72	0.00	8.72	4.000	No	Yes	2.00
765	15.30	1.05	100.00	3.18	0.59	0.84	8.34	0.00	8.34	4.000	No	Yes	2.00
766	15.32	1.02	100.00	3.22	0.59	0.84	8.24	0.00	8.24	4.000	No	Yes	2.00
767	15.34	1.00	100.00	3.25	0.59	0.84	7.99	0.00	7.99	4.000	No	Yes	2.00
768	15.36	0.98	100.00	3.28	0.59	0.84	7.88	0.00	7.88	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	0.95	100.00	3.32	0.59	0.83	7.57	0.00	7.57	4.000	No	Yes	2.00
770	15.40	0.93	100.00	3.34	0.59	0.83	7.35	0.00	7.35	4.000	No	Yes	2.00
771	15.42	0.92	100.00	3.35	0.59	0.83	7.25	0.00	7.25	4.000	No	Yes	2.00
772	15.45	0.93	100.00	3.33	0.59	0.83	7.21	0.00	7.21	4.000	No	Yes	2.00
773	15.46	0.93	100.00	3.32	0.59	0.83	7.58	0.00	7.58	4.000	No	Yes	2.00
774	15.48	0.94	100.00	3.30	0.59	0.83	7.43	0.00	7.43	4.000	No	Yes	2.00
775	15.50	0.95	100.00	3.29	0.59	0.83	7.46	0.00	7.46	4.000	No	Yes	2.00
776	15.52	0.95	100.00	3.28	0.59	0.83	7.59	0.00	7.59	4.000	No	Yes	2.00
777	15.54	0.98	100.00	3.25	0.59	0.83	7.85	0.00	7.85	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.13	2.00	0.00	9.94	0.03	0.00
0.14	2.00	0.00	9.93	0.01	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.35	2.00	0.00	9.82	0.03	0.00	0.36	2.00	0.00	9.82	0.01	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.05	2.00	0.00	8.98	0.03	0.00
2.06	2.00	0.00	8.97	0.01	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.01	2.00	0.00	8.49	0.03	0.00
3.02	2.00	0.00	8.49	0.01	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	0.72	0.28	8.06	0.02	0.05
3.90	0.74	0.26	8.05	0.02	0.04	3.94	0.75	0.25	8.03	0.04	0.08
3.94	0.76	0.24	8.03	0.00	0.00	3.96	0.76	0.24	8.02	0.02	0.04
3.98	0.76	0.24	8.01	0.02	0.04	4.01	0.75	0.25	8.00	0.03	0.06
4.02	0.75	0.25	7.99	0.01	0.02	4.04	0.74	0.26	7.98	0.02	0.04
4.06	0.74	0.26	7.97	0.02	0.04	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.13	2.00	0.00	7.94	0.03	0.00
4.14	2.00	0.00	7.93	0.01	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.03	2.00	0.00	7.49	0.03	0.00	5.04	2.00	0.00	7.48	0.01	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.13	2.00	0.00	7.44	0.03	0.00
5.14	2.00	0.00	7.43	0.01	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.95	2.00	0.00	6.53	0.03	0.00	6.96	2.00	0.00	6.52	0.01	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.13	2.00	0.00	6.44	0.03	0.00
7.14	2.00	0.00	6.43	0.01	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.45	2.00	0.00	6.28	0.03	0.00
7.46	2.00	0.00	6.27	0.01	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.99	2.00	0.00	6.01	0.03	0.00	8.00	2.00	0.00	6.00	0.01	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.05	2.00	0.00	5.47	0.03	0.00
9.06	2.00	0.00	5.47	0.01	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.25	2.00	0.00	5.38	0.03	0.00
9.26	2.00	0.00	5.37	0.01	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.01	2.00	0.00	5.00	0.03	0.00
10.02	2.00	0.00	4.99	0.01	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.19	2.00	0.00	4.41	0.03	0.00	11.20	2.00	0.00	4.40	0.01	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.89	2.00	0.00	4.06	0.03	0.00
11.90	2.00	0.00	4.05	0.01	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.03	2.00	0.00	3.99	0.03	0.00	12.04	2.00	0.00	3.98	0.01	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.81	2.00	0.00	3.60	0.03	0.00
12.82	2.00	0.00	3.59	0.01	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.07	2.00	0.00	3.47	0.03	0.00	13.08	2.00	0.00	3.46	0.01	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.20	2.00	0.00	3.40	0.02	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.37	2.00	0.00	3.32	0.03	0.00
13.38	2.00	0.00	3.31	0.01	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.83	2.00	0.00	3.09	0.03	0.00	13.84	2.00	0.00	3.08	0.01	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.99	2.00	0.00	3.01	0.03	0.00	14.00	2.00	0.00	3.00	0.01	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	0.61	0.39	2.82	0.02	0.02
14.38	0.62	0.38	2.81	0.02	0.02	14.40	0.63	0.37	2.80	0.02	0.02
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.55	2.00	0.00	2.73	0.03	0.00	14.56	2.00	0.00	2.72	0.01	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.80	2.00	0.00	2.60	0.02	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.84	2.00	0.00	2.58	0.02	0.00
14.86	2.00	0.00	2.57	0.02	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.01	2.00	0.00	2.50	0.03	0.00
15.03	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.01	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.45	2.00	0.00	2.28	0.03	0.00
15.46	2.00	0.00	2.27	0.01	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00						

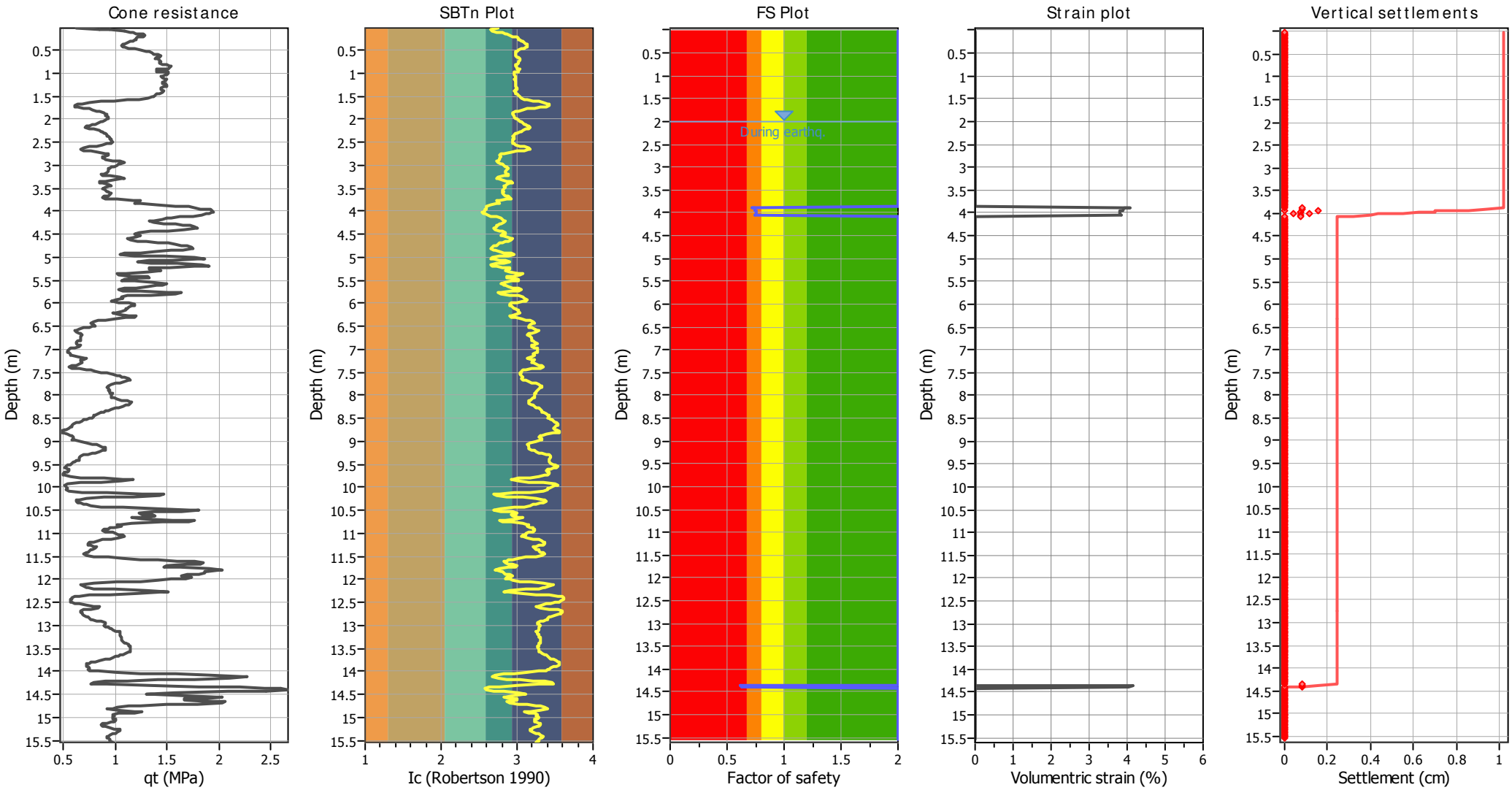
Overall liquefaction potential: 0.47

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.00	15.20	2.00	0.00	1.00	0.00	2.02	14.78	2.00	0.00	1.00	0.00
2.05	14.71	2.00	0.00	1.00	0.00	2.06	14.18	2.00	0.00	1.00	0.00
2.08	13.76	2.00	0.00	1.00	0.00	2.10	13.42	2.00	0.00	1.00	0.00
2.12	12.74	2.00	0.00	1.00	0.00	2.14	12.54	2.00	0.00	1.00	0.00
2.16	11.74	2.00	0.00	1.00	0.00	2.18	11.51	2.00	0.00	1.00	0.00
2.20	12.04	2.00	0.00	1.00	0.00	2.22	13.34	2.00	0.00	1.00	0.00
2.24	13.96	2.00	0.00	1.00	0.00	2.26	14.10	2.00	0.00	1.00	0.00
2.28	14.10	2.00	0.00	1.00	0.00	2.30	14.28	2.00	0.00	1.00	0.00
2.32	14.87	2.00	0.00	1.00	0.00	2.34	14.52	2.00	0.00	1.00	0.00
2.36	14.70	2.00	0.00	1.00	0.00	2.38	14.84	2.00	0.00	1.00	0.00
2.40	14.80	2.00	0.00	1.00	0.00	2.42	14.77	2.00	0.00	1.00	0.00
2.44	15.08	2.00	0.00	1.00	0.00	2.46	15.01	2.00	0.00	1.00	0.00
2.48	14.84	2.00	0.00	1.00	0.00	2.50	14.98	2.00	0.00	1.00	0.00
2.52	14.55	2.00	0.00	1.00	0.00	2.54	14.38	2.00	0.00	1.00	0.00
2.56	13.51	2.00	0.00	1.00	0.00	2.58	12.53	2.00	0.00	1.00	0.00
2.60	11.46	2.00	0.00	1.00	0.00	2.62	10.58	2.00	0.00	1.00	0.00
2.64	10.08	2.00	0.00	1.00	0.00	2.66	9.82	2.00	0.00	1.00	0.00
2.68	10.48	2.00	0.00	1.00	0.00	2.70	11.41	2.00	0.00	1.00	0.00
2.72	12.57	2.00	0.00	1.00	0.00	2.74	13.70	2.00	0.00	1.00	0.00
2.76	14.35	2.00	0.00	1.00	0.00	2.78	14.20	2.00	0.00	1.00	0.00
2.80	13.31	2.00	0.00	1.00	0.00	2.82	12.96	2.00	0.00	1.00	0.00
2.84	13.14	2.00	0.00	1.00	0.00	2.86	13.55	2.00	0.00	1.00	0.00
2.88	13.20	2.00	0.00	1.00	0.00	2.90	13.52	2.00	0.00	1.00	0.00
2.92	16.63	2.00	0.00	1.00	0.00	2.94	15.82	2.00	0.00	1.00	0.00
2.96	15.07	2.00	0.00	1.00	0.00	2.98	14.88	2.00	0.00	1.00	0.00
3.01	14.55	2.00	0.00	1.00	0.00	3.02	14.27	2.00	0.00	1.00	0.00
3.04	13.86	2.00	0.00	1.00	0.00	3.06	13.47	2.00	0.00	1.00	0.00
3.08	13.12	2.00	0.00	1.00	0.00	3.10	13.17	2.00	0.00	1.00	0.00
3.12	13.41	2.00	0.00	1.00	0.00	3.14	13.46	2.00	0.00	1.00	0.00
3.16	13.18	2.00	0.00	1.00	0.00	3.18	12.86	2.00	0.00	1.00	0.00
3.20	12.09	2.00	0.00	1.00	0.00	3.22	12.08	2.00	0.00	1.00	0.00
3.24	13.32	2.00	0.00	1.00	0.00	3.26	14.89	2.00	0.00	1.00	0.00
3.28	16.20	2.00	0.00	1.00	0.00	3.30	15.00	2.00	0.00	1.00	0.00
3.32	13.75	2.00	0.00	1.00	0.00	3.34	12.50	2.00	0.00	1.00	0.00
3.36	11.84	2.00	0.00	1.00	0.00	3.38	11.37	2.00	0.00	1.00	0.00
3.40	12.12	2.00	0.00	1.00	0.00	3.42	13.38	2.00	0.00	1.00	0.00
3.44	13.65	2.00	0.00	1.00	0.00	3.46	13.00	2.00	0.00	1.00	0.00
3.48	12.50	2.00	0.00	1.00	0.00	3.50	11.91	2.00	0.00	1.00	0.00
3.52	12.12	2.00	0.00	1.00	0.00	3.54	12.61	2.00	0.00	1.00	0.00
3.56	12.40	2.00	0.00	1.00	0.00	3.58	12.67	2.00	0.00	1.00	0.00
3.60	12.93	2.00	0.00	1.00	0.00	3.62	13.10	2.00	0.00	1.00	0.00
3.64	13.21	2.00	0.00	1.00	0.00	3.66	12.37	2.00	0.00	1.00	0.00
3.68	12.38	2.00	0.00	1.00	0.00	3.70	11.70	2.00	0.00	1.00	0.00
3.72	11.68	2.00	0.00	1.00	0.00	3.74	13.76	2.00	0.00	1.00	0.00
3.76	16.31	2.00	0.00	1.00	0.00	3.78	18.01	2.00	0.00	1.00	0.00
3.80	16.82	2.00	0.00	1.00	0.00	3.82	15.81	2.00	0.00	1.00	0.00
3.84	16.35	2.00	0.00	1.00	0.00	3.86	19.50	2.00	0.00	1.00	0.00
3.88	78.75	0.72	4.07	1.00	0.08	3.90	81.58	0.74	3.93	1.00	0.08

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.94	82.68	0.75	3.88	1.00	0.16	3.94	84.11	0.76	3.82	1.00	0.00
3.96	84.42	0.76	3.81	1.00	0.08	3.98	84.38	0.76	3.81	1.00	0.08
4.01	84.48	0.75	3.80	1.00	0.11	4.02	84.17	0.75	3.82	1.00	0.04
4.04	83.41	0.74	3.85	1.00	0.08	4.06	83.41	0.74	3.85	1.00	0.08
4.08	25.33	2.00	0.00	1.00	0.00	4.10	23.92	2.00	0.00	1.00	0.00
4.13	22.17	2.00	0.00	1.00	0.00	4.14	20.29	2.00	0.00	1.00	0.00
4.16	20.31	2.00	0.00	1.00	0.00	4.18	20.28	2.00	0.00	1.00	0.00
4.20	18.47	2.00	0.00	1.00	0.00	4.22	17.31	2.00	0.00	1.00	0.00
4.24	18.14	2.00	0.00	1.00	0.00	4.26	20.40	2.00	0.00	1.00	0.00
4.28	21.22	2.00	0.00	1.00	0.00	4.30	22.31	2.00	0.00	1.00	0.00
4.32	22.97	2.00	0.00	1.00	0.00	4.34	23.60	2.00	0.00	1.00	0.00
4.36	24.13	2.00	0.00	1.00	0.00	4.38	24.04	2.00	0.00	1.00	0.00
4.40	22.64	2.00	0.00	1.00	0.00	4.42	19.83	2.00	0.00	1.00	0.00
4.44	17.90	2.00	0.00	1.00	0.00	4.46	16.38	2.00	0.00	1.00	0.00
4.48	15.07	2.00	0.00	1.00	0.00	4.50	16.07	2.00	0.00	1.00	0.00
4.52	16.63	2.00	0.00	1.00	0.00	4.54	16.75	2.00	0.00	1.00	0.00
4.56	16.42	2.00	0.00	1.00	0.00	4.58	14.71	2.00	0.00	1.00	0.00
4.60	14.36	2.00	0.00	1.00	0.00	4.62	15.30	2.00	0.00	1.00	0.00
4.64	15.83	2.00	0.00	1.00	0.00	4.66	16.93	2.00	0.00	1.00	0.00
4.68	18.78	2.00	0.00	1.00	0.00	4.70	20.13	2.00	0.00	1.00	0.00
4.72	20.53	2.00	0.00	1.00	0.00	4.74	21.08	2.00	0.00	1.00	0.00
4.76	22.27	2.00	0.00	1.00	0.00	4.78	22.59	2.00	0.00	1.00	0.00
4.80	22.62	2.00	0.00	1.00	0.00	4.82	22.78	2.00	0.00	1.00	0.00
4.84	21.90	2.00	0.00	1.00	0.00	4.86	19.34	2.00	0.00	1.00	0.00
4.88	18.32	2.00	0.00	1.00	0.00	4.90	16.08	2.00	0.00	1.00	0.00
4.92	13.92	2.00	0.00	1.00	0.00	4.94	12.81	2.00	0.00	1.00	0.00
4.96	14.06	2.00	0.00	1.00	0.00	4.98	19.25	2.00	0.00	1.00	0.00
5.00	23.48	2.00	0.00	1.00	0.00	5.03	24.60	2.00	0.00	1.00	0.00
5.04	22.81	2.00	0.00	1.00	0.00	5.06	20.82	2.00	0.00	1.00	0.00
5.08	16.00	2.00	0.00	1.00	0.00	5.10	14.43	2.00	0.00	1.00	0.00
5.13	16.06	2.00	0.00	1.00	0.00	5.14	20.63	2.00	0.00	1.00	0.00
5.16	24.06	2.00	0.00	1.00	0.00	5.18	24.85	2.00	0.00	1.00	0.00
5.20	23.10	2.00	0.00	1.00	0.00	5.22	18.54	2.00	0.00	1.00	0.00
5.24	15.93	2.00	0.00	1.00	0.00	5.26	15.96	2.00	0.00	1.00	0.00
5.28	18.27	2.00	0.00	1.00	0.00	5.30	20.06	2.00	0.00	1.00	0.00
5.32	16.06	2.00	0.00	1.00	0.00	5.34	13.51	2.00	0.00	1.00	0.00
5.36	12.47	2.00	0.00	1.00	0.00	5.38	12.53	2.00	0.00	1.00	0.00
5.40	14.34	2.00	0.00	1.00	0.00	5.42	17.03	2.00	0.00	1.00	0.00
5.44	17.82	2.00	0.00	1.00	0.00	5.46	15.05	2.00	0.00	1.00	0.00
5.48	12.93	2.00	0.00	1.00	0.00	5.50	12.64	2.00	0.00	1.00	0.00
5.52	14.33	2.00	0.00	1.00	0.00	5.54	17.24	2.00	0.00	1.00	0.00
5.56	18.78	2.00	0.00	1.00	0.00	5.58	18.75	2.00	0.00	1.00	0.00
5.60	17.94	2.00	0.00	1.00	0.00	5.62	17.29	2.00	0.00	1.00	0.00
5.64	16.49	2.00	0.00	1.00	0.00	5.66	14.88	2.00	0.00	1.00	0.00
5.68	13.29	2.00	0.00	1.00	0.00	5.70	12.18	2.00	0.00	1.00	0.00
5.72	12.71	2.00	0.00	1.00	0.00	5.74	14.69	2.00	0.00	1.00	0.00
5.76	18.48	2.00	0.00	1.00	0.00	5.78	21.88	2.00	0.00	1.00	0.00
5.80	19.43	2.00	0.00	1.00	0.00	5.82	16.23	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.84	13.06	2.00	0.00	1.00	0.00	5.86	11.56	2.00	0.00	1.00	0.00
5.88	14.10	2.00	0.00	1.00	0.00	5.90	12.50	2.00	0.00	1.00	0.00
5.92	12.00	2.00	0.00	1.00	0.00	5.94	11.31	2.00	0.00	1.00	0.00
5.96	11.03	2.00	0.00	1.00	0.00	5.98	12.41	2.00	0.00	1.00	0.00
6.00	13.52	2.00	0.00	1.00	0.00	6.02	14.18	2.00	0.00	1.00	0.00
6.04	14.21	2.00	0.00	1.00	0.00	6.06	13.53	2.00	0.00	1.00	0.00
6.08	13.19	2.00	0.00	1.00	0.00	6.10	13.09	2.00	0.00	1.00	0.00
6.12	13.00	2.00	0.00	1.00	0.00	6.14	13.03	2.00	0.00	1.00	0.00
6.16	12.83	2.00	0.00	1.00	0.00	6.18	12.66	2.00	0.00	1.00	0.00
6.20	11.56	2.00	0.00	1.00	0.00	6.22	10.99	2.00	0.00	1.00	0.00
6.24	11.54	2.00	0.00	1.00	0.00	6.26	13.72	2.00	0.00	1.00	0.00
6.28	14.47	2.00	0.00	1.00	0.00	6.30	13.59	2.00	0.00	1.00	0.00
6.32	13.15	2.00	0.00	1.00	0.00	6.34	11.53	2.00	0.00	1.00	0.00
6.36	10.41	2.00	0.00	1.00	0.00	6.38	9.82	2.00	0.00	1.00	0.00
6.40	8.93	2.00	0.00	1.00	0.00	6.42	8.71	2.00	0.00	1.00	0.00
6.44	8.78	2.00	0.00	1.00	0.00	6.46	9.06	2.00	0.00	1.00	0.00
6.48	9.45	2.00	0.00	1.00	0.00	6.50	9.10	2.00	0.00	1.00	0.00
6.52	8.46	2.00	0.00	1.00	0.00	6.54	8.01	2.00	0.00	1.00	0.00
6.56	7.32	2.00	0.00	1.00	0.00	6.58	7.05	2.00	0.00	1.00	0.00
6.60	6.75	2.00	0.00	1.00	0.00	6.62	6.91	2.00	0.00	1.00	0.00
6.64	7.48	2.00	0.00	1.00	0.00	6.66	7.58	2.00	0.00	1.00	0.00
6.68	7.73	2.00	0.00	1.00	0.00	6.70	7.65	2.00	0.00	1.00	0.00
6.72	7.54	2.00	0.00	1.00	0.00	6.74	7.36	2.00	0.00	1.00	0.00
6.76	7.51	2.00	0.00	1.00	0.00	6.78	7.48	2.00	0.00	1.00	0.00
6.80	7.53	2.00	0.00	1.00	0.00	6.82	7.27	2.00	0.00	1.00	0.00
6.84	6.82	2.00	0.00	1.00	0.00	6.86	7.06	2.00	0.00	1.00	0.00
6.88	6.87	2.00	0.00	1.00	0.00	6.90	7.17	2.00	0.00	1.00	0.00
6.92	7.58	2.00	0.00	1.00	0.00	6.95	7.39	2.00	0.00	1.00	0.00
6.96	6.61	2.00	0.00	1.00	0.00	6.98	6.22	2.00	0.00	1.00	0.00
7.00	5.83	2.00	0.00	1.00	0.00	7.02	6.06	2.00	0.00	1.00	0.00
7.04	5.77	2.00	0.00	1.00	0.00	7.06	5.74	2.00	0.00	1.00	0.00
7.08	6.14	2.00	0.00	1.00	0.00	7.10	6.35	2.00	0.00	1.00	0.00
7.13	6.29	2.00	0.00	1.00	0.00	7.14	6.16	2.00	0.00	1.00	0.00
7.16	6.74	2.00	0.00	1.00	0.00	7.18	7.99	2.00	0.00	1.00	0.00
7.20	8.42	2.00	0.00	1.00	0.00	7.22	7.49	2.00	0.00	1.00	0.00
7.24	7.08	2.00	0.00	1.00	0.00	7.26	7.30	2.00	0.00	1.00	0.00
7.28	7.63	2.00	0.00	1.00	0.00	7.30	7.47	2.00	0.00	1.00	0.00
7.32	7.19	2.00	0.00	1.00	0.00	7.34	6.75	2.00	0.00	1.00	0.00
7.36	6.34	2.00	0.00	1.00	0.00	7.38	5.68	2.00	0.00	1.00	0.00
7.40	5.95	2.00	0.00	1.00	0.00	7.42	7.13	2.00	0.00	1.00	0.00
7.45	7.83	2.00	0.00	1.00	0.00	7.46	8.41	2.00	0.00	1.00	0.00
7.48	8.68	2.00	0.00	1.00	0.00	7.50	9.30	2.00	0.00	1.00	0.00
7.52	10.12	2.00	0.00	1.00	0.00	7.54	10.64	2.00	0.00	1.00	0.00
7.56	11.05	2.00	0.00	1.00	0.00	7.58	11.37	2.00	0.00	1.00	0.00
7.60	11.53	2.00	0.00	1.00	0.00	7.62	11.64	2.00	0.00	1.00	0.00
7.64	12.43	2.00	0.00	1.00	0.00	7.66	12.81	2.00	0.00	1.00	0.00
7.68	12.23	2.00	0.00	1.00	0.00	7.70	11.72	2.00	0.00	1.00	0.00
7.72	11.55	2.00	0.00	1.00	0.00	7.74	10.95	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.76	10.41	2.00	0.00	1.00	0.00	7.78	10.32	2.00	0.00	1.00	0.00
7.80	9.99	2.00	0.00	1.00	0.00	7.82	9.97	2.00	0.00	1.00	0.00
7.84	10.08	2.00	0.00	1.00	0.00	7.86	10.29	2.00	0.00	1.00	0.00
7.88	10.11	2.00	0.00	1.00	0.00	7.90	10.10	2.00	0.00	1.00	0.00
7.92	9.99	2.00	0.00	1.00	0.00	7.94	10.27	2.00	0.00	1.00	0.00
7.96	10.43	2.00	0.00	1.00	0.00	7.99	10.46	2.00	0.00	1.00	0.00
8.00	10.16	2.00	0.00	1.00	0.00	8.02	10.27	2.00	0.00	1.00	0.00
8.04	10.21	2.00	0.00	1.00	0.00	8.06	10.47	2.00	0.00	1.00	0.00
8.08	10.89	2.00	0.00	1.00	0.00	8.10	11.24	2.00	0.00	1.00	0.00
8.12	11.91	2.00	0.00	1.00	0.00	8.14	12.25	2.00	0.00	1.00	0.00
8.16	12.26	2.00	0.00	1.00	0.00	8.18	12.32	2.00	0.00	1.00	0.00
8.20	12.01	2.00	0.00	1.00	0.00	8.22	11.54	2.00	0.00	1.00	0.00
8.24	11.26	2.00	0.00	1.00	0.00	8.26	11.13	2.00	0.00	1.00	0.00
8.28	10.46	2.00	0.00	1.00	0.00	8.30	10.11	2.00	0.00	1.00	0.00
8.32	9.69	2.00	0.00	1.00	0.00	8.34	9.60	2.00	0.00	1.00	0.00
8.36	9.44	2.00	0.00	1.00	0.00	8.38	9.02	2.00	0.00	1.00	0.00
8.40	8.84	2.00	0.00	1.00	0.00	8.42	8.33	2.00	0.00	1.00	0.00
8.44	8.19	2.00	0.00	1.00	0.00	8.46	8.28	2.00	0.00	1.00	0.00
8.48	8.34	2.00	0.00	1.00	0.00	8.50	7.87	2.00	0.00	1.00	0.00
8.52	7.48	2.00	0.00	1.00	0.00	8.54	7.40	2.00	0.00	1.00	0.00
8.56	6.96	2.00	0.00	1.00	0.00	8.58	6.79	2.00	0.00	1.00	0.00
8.60	6.42	2.00	0.00	1.00	0.00	8.62	6.06	2.00	0.00	1.00	0.00
8.64	6.05	2.00	0.00	1.00	0.00	8.66	6.02	2.00	0.00	1.00	0.00
8.68	5.88	2.00	0.00	1.00	0.00	8.70	5.85	2.00	0.00	1.00	0.00
8.72	5.58	2.00	0.00	1.00	0.00	8.74	5.60	2.00	0.00	1.00	0.00
8.76	5.10	2.00	0.00	1.00	0.00	8.78	4.80	2.00	0.00	1.00	0.00
8.80	4.58	2.00	0.00	1.00	0.00	8.82	4.91	2.00	0.00	1.00	0.00
8.84	5.50	2.00	0.00	1.00	0.00	8.86	5.59	2.00	0.00	1.00	0.00
8.88	5.73	2.00	0.00	1.00	0.00	8.90	5.92	2.00	0.00	1.00	0.00
8.92	5.96	2.00	0.00	1.00	0.00	8.94	5.77	2.00	0.00	1.00	0.00
8.96	5.63	2.00	0.00	1.00	0.00	8.98	5.79	2.00	0.00	1.00	0.00
9.00	6.37	2.00	0.00	1.00	0.00	9.02	7.28	2.00	0.00	1.00	0.00
9.05	7.70	2.00	0.00	1.00	0.00	9.06	7.98	2.00	0.00	1.00	0.00
9.08	8.18	2.00	0.00	1.00	0.00	9.10	8.36	2.00	0.00	1.00	0.00
9.12	8.64	2.00	0.00	1.00	0.00	9.14	9.01	2.00	0.00	1.00	0.00
9.16	9.12	2.00	0.00	1.00	0.00	9.18	8.88	2.00	0.00	1.00	0.00
9.20	8.73	2.00	0.00	1.00	0.00	9.22	8.36	2.00	0.00	1.00	0.00
9.25	8.02	2.00	0.00	1.00	0.00	9.26	7.67	2.00	0.00	1.00	0.00
9.28	7.20	2.00	0.00	1.00	0.00	9.30	6.66	2.00	0.00	1.00	0.00
9.32	6.47	2.00	0.00	1.00	0.00	9.34	6.40	2.00	0.00	1.00	0.00
9.36	6.39	2.00	0.00	1.00	0.00	9.38	6.38	2.00	0.00	1.00	0.00
9.40	6.38	2.00	0.00	1.00	0.00	9.42	6.12	2.00	0.00	1.00	0.00
9.44	5.86	2.00	0.00	1.00	0.00	9.46	5.88	2.00	0.00	1.00	0.00
9.48	5.62	2.00	0.00	1.00	0.00	9.50	5.41	2.00	0.00	1.00	0.00
9.52	5.20	2.00	0.00	1.00	0.00	9.54	4.94	2.00	0.00	1.00	0.00
9.56	4.80	2.00	0.00	1.00	0.00	9.58	5.07	2.00	0.00	1.00	0.00
9.60	5.18	2.00	0.00	1.00	0.00	9.62	5.29	2.00	0.00	1.00	0.00
9.64	5.35	2.00	0.00	1.00	0.00	9.66	5.10	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.68	4.80	2.00	0.00	1.00	0.00	9.70	4.62	2.00	0.00	1.00	0.00
9.72	4.78	2.00	0.00	1.00	0.00	9.74	4.68	2.00	0.00	1.00	0.00
9.76	5.11	2.00	0.00	1.00	0.00	9.78	6.29	2.00	0.00	1.00	0.00
9.80	7.70	2.00	0.00	1.00	0.00	9.82	11.85	2.00	0.00	1.00	0.00
9.84	12.21	2.00	0.00	1.00	0.00	9.86	11.13	2.00	0.00	1.00	0.00
9.88	8.66	2.00	0.00	1.00	0.00	9.90	6.12	2.00	0.00	1.00	0.00
9.92	4.99	2.00	0.00	1.00	0.00	9.94	5.03	2.00	0.00	1.00	0.00
9.96	4.98	2.00	0.00	1.00	0.00	9.98	5.18	2.00	0.00	1.00	0.00
10.01	5.35	2.00	0.00	1.00	0.00	10.02	5.33	2.00	0.00	1.00	0.00
10.04	5.08	2.00	0.00	1.00	0.00	10.06	5.01	2.00	0.00	1.00	0.00
10.08	5.19	2.00	0.00	1.00	0.00	10.10	5.97	2.00	0.00	1.00	0.00
10.12	8.68	2.00	0.00	1.00	0.00	10.14	12.28	2.00	0.00	1.00	0.00
10.16	16.12	2.00	0.00	1.00	0.00	10.18	14.95	2.00	0.00	1.00	0.00
10.20	11.18	2.00	0.00	1.00	0.00	10.22	8.49	2.00	0.00	1.00	0.00
10.24	6.36	2.00	0.00	1.00	0.00	10.26	6.16	2.00	0.00	1.00	0.00
10.28	6.04	2.00	0.00	1.00	0.00	10.30	5.77	2.00	0.00	1.00	0.00
10.32	6.06	2.00	0.00	1.00	0.00	10.34	6.41	2.00	0.00	1.00	0.00
10.36	6.52	2.00	0.00	1.00	0.00	10.38	6.76	2.00	0.00	1.00	0.00
10.40	7.33	2.00	0.00	1.00	0.00	10.42	7.88	2.00	0.00	1.00	0.00
10.44	9.60	2.00	0.00	1.00	0.00	10.46	13.50	2.00	0.00	1.00	0.00
10.48	17.63	2.00	0.00	1.00	0.00	10.50	19.01	2.00	0.00	1.00	0.00
10.52	15.96	2.00	0.00	1.00	0.00	10.54	12.94	2.00	0.00	1.00	0.00
10.56	10.85	2.00	0.00	1.00	0.00	10.58	11.86	2.00	0.00	1.00	0.00
10.60	13.59	2.00	0.00	1.00	0.00	10.62	13.93	2.00	0.00	1.00	0.00
10.64	12.69	2.00	0.00	1.00	0.00	10.66	9.95	2.00	0.00	1.00	0.00
10.68	11.04	2.00	0.00	1.00	0.00	10.70	15.49	2.00	0.00	1.00	0.00
10.72	18.42	2.00	0.00	1.00	0.00	10.74	17.30	2.00	0.00	1.00	0.00
10.76	13.87	2.00	0.00	1.00	0.00	10.78	11.03	2.00	0.00	1.00	0.00
10.80	8.41	2.00	0.00	1.00	0.00	10.82	10.40	2.00	0.00	1.00	0.00
10.84	10.34	2.00	0.00	1.00	0.00	10.86	9.25	2.00	0.00	1.00	0.00
10.88	8.69	2.00	0.00	1.00	0.00	10.90	8.95	2.00	0.00	1.00	0.00
10.92	8.61	2.00	0.00	1.00	0.00	10.94	7.54	2.00	0.00	1.00	0.00
10.96	8.46	2.00	0.00	1.00	0.00	10.98	9.35	2.00	0.00	1.00	0.00
11.00	9.56	2.00	0.00	1.00	0.00	11.02	9.57	2.00	0.00	1.00	0.00
11.04	10.06	2.00	0.00	1.00	0.00	11.06	10.59	2.00	0.00	1.00	0.00
11.08	10.15	2.00	0.00	1.00	0.00	11.10	10.01	2.00	0.00	1.00	0.00
11.12	8.90	2.00	0.00	1.00	0.00	11.14	8.09	2.00	0.00	1.00	0.00
11.16	7.74	2.00	0.00	1.00	0.00	11.19	7.52	2.00	0.00	1.00	0.00
11.20	6.89	2.00	0.00	1.00	0.00	11.22	6.49	2.00	0.00	1.00	0.00
11.24	6.96	2.00	0.00	1.00	0.00	11.26	6.93	2.00	0.00	1.00	0.00
11.28	7.40	2.00	0.00	1.00	0.00	11.30	7.70	2.00	0.00	1.00	0.00
11.32	7.67	2.00	0.00	1.00	0.00	11.34	7.13	2.00	0.00	1.00	0.00
11.36	6.78	2.00	0.00	1.00	0.00	11.38	7.07	2.00	0.00	1.00	0.00
11.40	6.96	2.00	0.00	1.00	0.00	11.42	6.42	2.00	0.00	1.00	0.00
11.44	6.44	2.00	0.00	1.00	0.00	11.46	6.35	2.00	0.00	1.00	0.00
11.48	6.33	2.00	0.00	1.00	0.00	11.50	7.13	2.00	0.00	1.00	0.00
11.52	8.30	2.00	0.00	1.00	0.00	11.54	10.21	2.00	0.00	1.00	0.00
11.56	11.27	2.00	0.00	1.00	0.00	11.58	12.78	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.60	15.22	2.00	0.00	1.00	0.00	11.62	16.34	2.00	0.00	1.00	0.00
11.64	17.50	2.00	0.00	1.00	0.00	11.66	17.64	2.00	0.00	1.00	0.00
11.68	15.62	2.00	0.00	1.00	0.00	11.70	13.98	2.00	0.00	1.00	0.00
11.72	12.16	2.00	0.00	1.00	0.00	11.74	14.59	2.00	0.00	1.00	0.00
11.76	18.25	2.00	0.00	1.00	0.00	11.78	20.01	2.00	0.00	1.00	0.00
11.80	18.44	2.00	0.00	1.00	0.00	11.82	17.28	2.00	0.00	1.00	0.00
11.84	16.91	2.00	0.00	1.00	0.00	11.86	17.70	2.00	0.00	1.00	0.00
11.89	17.11	2.00	0.00	1.00	0.00	11.90	15.42	2.00	0.00	1.00	0.00
11.92	14.54	2.00	0.00	1.00	0.00	11.94	15.54	2.00	0.00	1.00	0.00
11.96	16.92	2.00	0.00	1.00	0.00	11.98	15.55	2.00	0.00	1.00	0.00
12.00	13.92	2.00	0.00	1.00	0.00	12.03	13.13	2.00	0.00	1.00	0.00
12.04	11.95	2.00	0.00	1.00	0.00	12.06	9.16	2.00	0.00	1.00	0.00
12.08	6.91	2.00	0.00	1.00	0.00	12.10	5.91	2.00	0.00	1.00	0.00
12.12	5.94	2.00	0.00	1.00	0.00	12.14	6.35	2.00	0.00	1.00	0.00
12.16	6.62	2.00	0.00	1.00	0.00	12.18	6.73	2.00	0.00	1.00	0.00
12.20	6.58	2.00	0.00	1.00	0.00	12.22	7.99	2.00	0.00	1.00	0.00
12.24	12.49	2.00	0.00	1.00	0.00	12.26	14.87	2.00	0.00	1.00	0.00
12.28	13.72	2.00	0.00	1.00	0.00	12.30	11.13	2.00	0.00	1.00	0.00
12.32	8.08	2.00	0.00	1.00	0.00	12.34	6.56	2.00	0.00	1.00	0.00
12.36	5.71	2.00	0.00	1.00	0.00	12.38	5.21	2.00	0.00	1.00	0.00
12.40	5.39	2.00	0.00	1.00	0.00	12.42	5.12	2.00	0.00	1.00	0.00
12.44	5.12	2.00	0.00	1.00	0.00	12.46	5.09	2.00	0.00	1.00	0.00
12.48	4.98	2.00	0.00	1.00	0.00	12.50	5.02	2.00	0.00	1.00	0.00
12.52	5.41	2.00	0.00	1.00	0.00	12.54	5.80	2.00	0.00	1.00	0.00
12.56	6.12	2.00	0.00	1.00	0.00	12.58	7.22	2.00	0.00	1.00	0.00
12.60	7.63	2.00	0.00	1.00	0.00	12.62	7.66	2.00	0.00	1.00	0.00
12.64	6.72	2.00	0.00	1.00	0.00	12.66	5.82	2.00	0.00	1.00	0.00
12.68	5.67	2.00	0.00	1.00	0.00	12.70	5.89	2.00	0.00	1.00	0.00
12.72	5.97	2.00	0.00	1.00	0.00	12.74	5.93	2.00	0.00	1.00	0.00
12.76	5.84	2.00	0.00	1.00	0.00	12.78	5.98	2.00	0.00	1.00	0.00
12.81	6.21	2.00	0.00	1.00	0.00	12.82	6.41	2.00	0.00	1.00	0.00
12.84	6.47	2.00	0.00	1.00	0.00	12.86	6.58	2.00	0.00	1.00	0.00
12.88	6.62	2.00	0.00	1.00	0.00	12.90	7.04	2.00	0.00	1.00	0.00
12.92	7.52	2.00	0.00	1.00	0.00	12.94	7.88	2.00	0.00	1.00	0.00
12.96	7.84	2.00	0.00	1.00	0.00	12.98	7.77	2.00	0.00	1.00	0.00
13.00	7.62	2.00	0.00	1.00	0.00	13.02	7.66	2.00	0.00	1.00	0.00
13.04	8.12	2.00	0.00	1.00	0.00	13.07	8.11	2.00	0.00	1.00	0.00
13.08	8.21	2.00	0.00	1.00	0.00	13.10	8.30	2.00	0.00	1.00	0.00
13.12	8.72	2.00	0.00	1.00	0.00	13.14	8.93	2.00	0.00	1.00	0.00
13.16	9.15	2.00	0.00	1.00	0.00	13.18	8.94	2.00	0.00	1.00	0.00
13.20	8.99	2.00	0.00	1.00	0.00	13.22	8.98	2.00	0.00	1.00	0.00
13.24	9.09	2.00	0.00	1.00	0.00	13.26	9.13	2.00	0.00	1.00	0.00
13.28	9.16	2.00	0.00	1.00	0.00	13.30	9.09	2.00	0.00	1.00	0.00
13.32	9.06	2.00	0.00	1.00	0.00	13.34	9.15	2.00	0.00	1.00	0.00
13.37	9.24	2.00	0.00	1.00	0.00	13.38	9.47	2.00	0.00	1.00	0.00
13.40	9.66	2.00	0.00	1.00	0.00	13.42	9.61	2.00	0.00	1.00	0.00
13.44	9.70	2.00	0.00	1.00	0.00	13.46	9.67	2.00	0.00	1.00	0.00
13.48	9.84	2.00	0.00	1.00	0.00	13.50	9.67	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.52	9.49	2.00	0.00	1.00	0.00	13.54	9.81	2.00	0.00	1.00	0.00
13.56	9.72	2.00	0.00	1.00	0.00	13.58	9.68	2.00	0.00	1.00	0.00
13.60	9.35	2.00	0.00	1.00	0.00	13.62	9.04	2.00	0.00	1.00	0.00
13.64	8.89	2.00	0.00	1.00	0.00	13.66	8.64	2.00	0.00	1.00	0.00
13.68	8.50	2.00	0.00	1.00	0.00	13.70	8.25	2.00	0.00	1.00	0.00
13.72	8.03	2.00	0.00	1.00	0.00	13.74	7.54	2.00	0.00	1.00	0.00
13.76	7.12	2.00	0.00	1.00	0.00	13.78	6.55	2.00	0.00	1.00	0.00
13.80	6.33	2.00	0.00	1.00	0.00	13.83	6.17	2.00	0.00	1.00	0.00
13.84	5.97	2.00	0.00	1.00	0.00	13.86	5.79	2.00	0.00	1.00	0.00
13.88	5.91	2.00	0.00	1.00	0.00	13.90	6.06	2.00	0.00	1.00	0.00
13.92	6.19	2.00	0.00	1.00	0.00	13.94	6.15	2.00	0.00	1.00	0.00
13.96	6.07	2.00	0.00	1.00	0.00	13.99	5.96	2.00	0.00	1.00	0.00
14.00	6.43	2.00	0.00	1.00	0.00	14.02	8.07	2.00	0.00	1.00	0.00
14.04	10.20	2.00	0.00	1.00	0.00	14.06	12.71	2.00	0.00	1.00	0.00
14.08	17.03	2.00	0.00	1.00	0.00	14.10	19.74	2.00	0.00	1.00	0.00
14.12	20.42	2.00	0.00	1.00	0.00	14.14	18.30	2.00	0.00	1.00	0.00
14.16	15.19	2.00	0.00	1.00	0.00	14.18	11.77	2.00	0.00	1.00	0.00
14.20	9.21	2.00	0.00	1.00	0.00	14.22	7.41	2.00	0.00	1.00	0.00
14.24	6.26	2.00	0.00	1.00	0.00	14.26	5.99	2.00	0.00	1.00	0.00
14.28	6.62	2.00	0.00	1.00	0.00	14.30	10.41	2.00	0.00	1.00	0.00
14.32	16.25	2.00	0.00	1.00	0.00	14.34	19.05	2.00	0.00	1.00	0.00
14.36	77.33	0.61	4.14	1.00	0.08	14.38	79.33	0.62	4.04	1.00	0.08
14.40	80.76	0.63	3.97	1.00	0.08	14.42	22.51	2.00	0.00	1.00	0.00
14.44	17.01	2.00	0.00	1.00	0.00	14.46	13.48	2.00	0.00	1.00	0.00
14.48	9.12	2.00	0.00	1.00	0.00	14.50	10.18	2.00	0.00	1.00	0.00
14.52	14.23	2.00	0.00	1.00	0.00	14.55	17.29	2.00	0.00	1.00	0.00
14.56	18.34	2.00	0.00	1.00	0.00	14.58	15.83	2.00	0.00	1.00	0.00
14.60	13.14	2.00	0.00	1.00	0.00	14.62	12.89	2.00	0.00	1.00	0.00
14.64	15.68	2.00	0.00	1.00	0.00	14.66	18.48	2.00	0.00	1.00	0.00
14.68	17.83	2.00	0.00	1.00	0.00	14.70	14.88	2.00	0.00	1.00	0.00
14.72	12.20	2.00	0.00	1.00	0.00	14.74	10.42	2.00	0.00	1.00	0.00
14.76	8.47	2.00	0.00	1.00	0.00	14.78	9.15	2.00	0.00	1.00	0.00
14.80	7.54	2.00	0.00	1.00	0.00	14.82	7.27	2.00	0.00	1.00	0.00
14.84	7.83	2.00	0.00	1.00	0.00	14.86	9.75	2.00	0.00	1.00	0.00
14.88	11.51	2.00	0.00	1.00	0.00	14.90	9.74	2.00	0.00	1.00	0.00
14.92	7.83	2.00	0.00	1.00	0.00	14.94	7.80	2.00	0.00	1.00	0.00
14.96	8.18	2.00	0.00	1.00	0.00	14.98	7.97	2.00	0.00	1.00	0.00
15.01	7.69	2.00	0.00	1.00	0.00	15.03	7.95	2.00	0.00	1.00	0.00
15.04	8.14	2.00	0.00	1.00	0.00	15.06	8.19	2.00	0.00	1.00	0.00
15.08	8.09	2.00	0.00	1.00	0.00	15.10	7.86	2.00	0.00	1.00	0.00
15.12	7.31	2.00	0.00	1.00	0.00	15.14	6.99	2.00	0.00	1.00	0.00
15.16	6.87	2.00	0.00	1.00	0.00	15.18	7.00	2.00	0.00	1.00	0.00
15.20	7.19	2.00	0.00	1.00	0.00	15.22	7.47	2.00	0.00	1.00	0.00
15.24	8.22	2.00	0.00	1.00	0.00	15.26	8.25	2.00	0.00	1.00	0.00
15.28	8.72	2.00	0.00	1.00	0.00	15.30	8.34	2.00	0.00	1.00	0.00
15.32	8.24	2.00	0.00	1.00	0.00	15.34	7.99	2.00	0.00	1.00	0.00
15.36	7.88	2.00	0.00	1.00	0.00	15.38	7.57	2.00	0.00	1.00	0.00
15.40	7.35	2.00	0.00	1.00	0.00	15.42	7.25	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.45	7.21	2.00	0.00	1.00	0.00	15.46	7.58	2.00	0.00	1.00	0.00
15.48	7.43	2.00	0.00	1.00	0.00	15.50	7.46	2.00	0.00	1.00	0.00
15.52	7.59	2.00	0.00	1.00	0.00	15.54	7.85	2.00	0.00	1.00	0.00

Total estimated settlement: 1.02

Abbreviations

$Q_{tn,cs}$: Equivalent clean sand normalized cone resistance
FS: Factor of safety against liquefaction
e_v (%): Post-liquefaction volumentric strain
DF: e_v depth weighting factor
Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.62	10.52	4.33	45.51	2.74	0.07	147.84
0.04	0.85	14.36	3.62	51.95	2.65	0.07	98.90
0.06	0.96	16.23	3.67	59.52	2.65	0.08	73.30
0.08	1.09	18.45	3.82	70.51	2.68	0.08	61.48
0.10	1.15	19.45	4.25	82.70	2.73	0.08	51.04
0.13	1.18	20.01	4.77	95.53	2.80	0.08	39.64
0.14	1.20	20.45	5.18	105.91	2.85	0.08	37.40
0.16	1.27	21.61	5.32	114.99	2.86	0.08	34.21
0.18	1.28	21.74	5.67	123.20	2.90	0.08	30.32
0.20	1.27	21.60	6.07	131.22	2.94	0.08	26.89
0.22	1.21	20.58	6.65	136.94	2.99	0.07	23.13
0.24	1.21	20.45	6.85	140.19	3.01	0.07	20.94
0.26	1.20	20.33	7.02	142.59	3.02	0.07	19.11
0.28	1.19	20.09	7.21	144.85	3.04	0.07	17.46
0.30	1.17	19.83	7.45	147.65	3.06	0.07	16.01
0.32	1.15	19.41	7.70	149.43	3.08	0.07	14.64
0.35	1.12	18.99	7.91	150.17	3.10	0.07	13.04
0.36	1.09	18.42	8.16	150.34	3.12	0.07	12.28
0.38	1.08	18.19	8.29	150.78	3.13	0.07	11.45
0.40	1.07	18.03	8.37	151.01	3.14	0.07	10.76
0.42	1.08	18.21	8.28	150.73	3.13	0.07	10.33
0.44	1.09	18.47	8.12	149.96	3.12	0.07	9.98
0.46	1.13	19.13	7.81	149.33	3.09	0.07	9.87
0.48	1.19	20.03	7.40	148.30	3.06	0.07	9.89
0.50	1.25	21.10	6.98	147.34	3.02	0.07	9.99
0.52	1.30	21.95	6.72	147.49	3.00	0.08	9.97
0.54	1.33	22.48	6.61	148.68	2.99	0.08	9.83
0.56	1.35	22.78	6.61	150.63	2.99	0.08	9.59
0.58	1.37	23.19	6.57	152.29	2.98	0.08	9.41
0.60	1.41	23.75	6.54	155.40	2.98	0.08	9.31
0.62	1.43	24.18	6.59	159.31	2.99	0.08	9.16
0.64	1.43	24.06	6.81	163.82	3.01	0.08	8.82
0.66	1.40	23.67	7.05	166.93	3.03	0.08	8.40
0.68	1.39	23.42	7.22	169.02	3.04	0.08	8.06
0.70	1.41	23.77	7.16	170.28	3.04	0.08	7.93
0.72	1.43	24.09	7.10	170.92	3.03	0.08	7.80
0.74	1.44	24.18	7.05	170.55	3.03	0.08	7.61
0.76	1.42	23.94	7.07	169.22	3.03	0.08	7.33
0.78	1.43	24.01	6.98	167.63	3.02	0.08	7.16
0.80	1.45	24.45	6.82	166.69	3.01	0.08	7.10
0.82	1.50	25.18	6.62	166.56	2.99	0.08	7.13
0.84	1.53	25.71	6.51	167.39	2.98	0.08	7.10
0.86	1.53	25.79	6.54	168.79	2.98	0.08	6.95
0.88	1.52	25.55	6.65	169.92	2.99	0.08	6.72
0.90	1.51	25.36	6.72	170.33	3.00	0.08	6.52
0.92	1.40	23.51	7.17	168.52	3.04	0.08	5.91
0.94	1.40	23.57	7.00	165.07	3.02	0.07	5.79
0.96	1.40	23.56	6.86	161.65	3.01	0.08	5.67

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	1.51	25.33	6.31	159.72	2.96	0.08	5.97
1.00	1.51	25.28	6.29	159.06	2.96	0.08	5.83
1.02	1.50	25.16	6.29	158.18	2.96	0.08	5.69
1.04	1.48	24.89	6.33	157.52	2.96	0.08	5.52
1.06	1.46	24.48	6.46	158.04	2.97	0.08	5.32
1.08	1.44	24.21	6.58	159.39	2.99	0.08	5.16
1.10	1.45	24.33	6.60	160.45	2.99	0.08	5.09
1.12	1.48	24.75	6.50	160.78	2.98	0.08	5.09
1.14	1.50	25.06	6.40	160.50	2.97	0.08	5.06
1.16	1.49	24.92	6.44	160.58	2.97	0.08	4.94
1.18	1.46	24.54	6.56	160.95	2.98	0.08	4.78
1.20	1.45	24.31	6.62	161.01	2.99	0.08	4.66
1.22	1.46	24.39	6.61	161.29	2.99	0.08	4.59
1.24	1.48	24.74	6.53	161.58	2.98	0.08	4.58
1.26	1.49	24.96	6.50	162.16	2.98	0.08	4.55
1.28	1.49	24.99	6.50	162.35	2.98	0.08	4.48
1.30	1.47	24.56	6.59	161.99	2.99	0.08	4.34
1.32	1.45	24.16	6.68	161.30	2.99	0.08	4.20
1.34	1.44	23.98	6.67	159.92	2.99	0.08	4.11
1.36	1.45	24.17	6.55	158.41	2.98	0.08	4.08
1.38	1.46	24.46	6.44	157.49	2.97	0.08	4.07
1.40	1.47	24.62	6.39	157.36	2.97	0.08	4.03
1.42	1.46	24.39	6.47	157.73	2.97	0.08	3.94
1.44	1.43	23.89	6.63	158.37	2.99	0.08	3.80
1.46	1.40	23.37	6.83	159.55	3.01	0.08	3.67
1.48	1.39	23.10	6.97	160.94	3.02	0.08	3.58
1.50	1.38	22.92	7.07	162.12	3.03	0.08	3.50
1.52	1.36	22.65	7.17	162.39	3.04	0.08	3.41
1.54	1.31	21.85	7.40	161.63	3.06	0.08	3.25
1.56	1.23	20.49	7.80	159.73	3.09	0.07	3.01
1.58	1.12	18.56	8.45	156.76	3.14	0.07	2.69
1.60	0.99	16.32	9.38	153.03	3.21	0.07	2.33
1.62	0.86	14.11	10.48	147.88	3.28	0.07	1.99
1.64	0.76	12.33	11.55	142.41	3.35	0.06	1.72
1.66	0.68	11.09	12.36	137.14	3.40	0.06	1.53
1.68	0.64	10.33	12.81	132.35	3.43	0.06	1.41
1.70	0.61	9.83	12.86	126.37	3.43	0.06	1.32
1.72	0.61	9.86	12.18	120.14	3.39	0.06	1.31
1.74	0.65	10.44	10.90	113.81	3.31	0.06	1.38
1.76	0.69	11.23	9.63	108.23	3.23	0.06	1.46
1.78	0.75	12.13	8.45	102.45	3.14	0.06	1.56
1.80	0.78	12.77	7.64	97.60	3.08	0.06	1.63
1.82	0.82	13.32	7.03	93.63	3.03	0.07	1.68
1.84	0.85	13.92	6.55	91.21	2.98	0.07	1.74
1.86	0.89	14.50	6.20	89.96	2.95	0.07	1.79
1.88	0.91	14.94	6.04	90.30	2.93	0.07	1.83
1.90	0.92	14.98	6.12	91.76	2.94	0.07	1.82
1.92	0.91	14.90	6.24	92.92	2.95	0.07	1.79

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	0.92	15.09	6.24	94.09	2.95	0.07	1.80
1.96	0.93	15.19	6.32	95.93	2.96	0.07	1.79
1.98	0.93	15.26	6.44	98.34	2.97	0.07	1.78
2.00	0.92	14.98	6.72	100.64	3.00	0.07	1.73
2.02	0.91	14.76	6.95	102.55	3.02	0.07	1.69
2.05	0.88	14.40	7.23	104.09	3.04	0.07	1.62
2.06	0.86	14.03	7.44	104.44	3.06	0.07	1.58
2.08	0.84	13.57	7.64	103.68	3.08	0.07	1.51
2.10	0.81	13.06	7.83	102.28	3.09	0.07	1.44
2.12	0.78	12.63	8.04	101.56	3.11	0.06	1.38
2.14	0.75	12.05	8.43	101.60	3.14	0.06	1.31
2.16	0.72	11.63	8.75	101.75	3.16	0.06	1.25
2.18	0.71	11.45	8.90	101.88	3.17	0.06	1.22
2.20	0.75	12.00	8.55	102.60	3.15	0.06	1.27
2.22	0.80	12.89	8.10	104.40	3.11	0.07	1.35
2.24	0.84	13.67	7.71	105.33	3.08	0.07	1.42
2.26	0.87	14.01	7.46	104.48	3.06	0.07	1.44
2.28	0.88	14.19	7.15	101.44	3.04	0.07	1.45
2.30	0.90	14.54	6.74	98.04	3.00	0.07	1.47
2.32	0.91	14.76	6.49	95.87	2.98	0.07	1.48
2.34	0.92	14.99	6.30	94.46	2.96	0.07	1.49
2.36	0.93	15.04	6.27	94.29	2.96	0.07	1.48
2.38	0.94	15.22	6.22	94.71	2.95	0.07	1.49
2.40	0.94	15.32	6.26	95.96	2.96	0.07	1.49
2.42	0.95	15.48	6.26	96.90	2.96	0.07	1.49
2.44	0.96	15.63	6.18	96.62	2.95	0.07	1.49
2.46	0.97	15.73	6.10	95.99	2.94	0.07	1.49
2.48	0.97	15.76	6.05	95.28	2.93	0.07	1.48
2.50	0.96	15.64	6.07	94.96	2.94	0.07	1.46
2.52	0.96	15.50	6.07	94.08	2.94	0.07	1.44
2.54	0.93	14.96	6.26	93.70	2.96	0.07	1.39
2.56	0.88	14.21	6.63	94.17	2.99	0.07	1.31
2.58	0.82	13.12	7.29	95.61	3.05	0.06	1.21
2.60	0.75	12.03	7.99	96.16	3.11	0.06	1.11
2.62	0.70	11.12	8.55	95.14	3.15	0.06	1.02
2.64	0.67	10.52	8.79	92.56	3.17	0.06	0.96
2.66	0.67	10.51	8.52	89.49	3.15	0.06	0.96
2.68	0.70	11.03	7.81	86.09	3.09	0.06	1.00
2.70	0.76	12.09	6.79	82.16	3.00	0.06	1.09
2.72	0.83	13.33	5.83	77.79	2.91	0.07	1.20
2.74	0.90	14.47	5.08	73.50	2.83	0.07	1.30
2.76	0.94	15.10	4.68	70.62	2.79	0.07	1.35
2.78	0.93	14.96	4.58	68.58	2.78	0.07	1.34
2.80	0.90	14.44	4.64	66.95	2.78	0.07	1.29
2.82	0.88	14.05	4.67	65.61	2.79	0.07	1.25
2.84	0.88	14.17	4.57	64.80	2.77	0.07	1.26
2.86	0.89	14.29	4.54	64.84	2.77	0.07	1.26
2.88	0.90	14.46	4.55	65.83	2.77	0.07	1.28

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.98	15.75	4.33	68.24	2.74	0.07	1.39
2.92	1.04	16.87	4.25	71.74	2.73	0.08	1.48
2.94	1.09	17.58	4.31	75.84	2.74	0.08	1.54
2.96	1.05	16.97	4.67	79.18	2.79	0.08	1.48
2.98	1.03	16.57	4.92	81.45	2.82	0.07	1.44
3.01	1.01	16.31	5.06	82.54	2.83	0.07	1.41
3.02	0.99	15.94	5.26	83.79	2.85	0.07	1.38
3.04	0.97	15.53	5.43	84.29	2.87	0.07	1.34
3.06	0.94	15.10	5.59	84.38	2.89	0.07	1.30
3.08	0.93	14.86	5.58	82.90	2.89	0.07	1.27
3.10	0.93	14.86	5.45	81.05	2.87	0.07	1.27
3.12	0.94	15.01	5.25	78.87	2.85	0.07	1.28
3.14	0.94	15.00	5.15	77.22	2.84	0.07	1.27
3.16	0.92	14.74	5.17	76.24	2.84	0.07	1.25
3.18	0.89	14.17	5.37	76.01	2.87	0.07	1.20
3.20	0.87	13.75	5.54	76.22	2.88	0.07	1.16
3.22	0.88	13.98	5.46	76.40	2.88	0.07	1.18
3.24	0.95	15.15	5.02	76.00	2.83	0.07	1.27
3.26	1.05	16.81	4.45	74.79	2.76	0.08	1.41
3.28	1.09	17.47	4.28	74.73	2.74	0.08	1.46
3.30	1.06	17.02	4.44	75.65	2.76	0.08	1.42
3.32	0.98	15.58	4.93	76.87	2.82	0.07	1.29
3.34	0.90	14.37	5.40	77.61	2.87	0.07	1.19
3.36	0.85	13.47	5.86	78.98	2.92	0.07	1.11
3.38	0.85	13.36	6.05	80.78	2.93	0.06	1.10
3.40	0.88	14.02	5.82	81.62	2.91	0.07	1.15
3.42	0.94	14.96	5.38	80.48	2.87	0.07	1.22
3.44	0.96	15.32	5.11	78.33	2.84	0.07	1.25
3.46	0.94	14.99	5.06	75.85	2.83	0.07	1.22
3.48	0.90	14.31	5.13	73.41	2.84	0.07	1.16
3.50	0.89	14.00	5.08	71.19	2.83	0.07	1.13
3.52	0.89	14.09	4.97	70.05	2.82	0.07	1.14
3.54	0.90	14.32	4.92	70.47	2.82	0.07	1.15
3.56	0.92	14.57	4.92	71.64	2.82	0.07	1.17
3.58	0.93	14.73	4.96	72.98	2.82	0.07	1.18
3.60	0.95	15.04	4.91	73.89	2.82	0.07	1.20
3.62	0.96	15.28	4.91	75.03	2.81	0.07	1.22
3.64	0.95	15.05	5.03	75.72	2.83	0.07	1.20
3.66	0.93	14.72	5.17	76.18	2.84	0.07	1.17
3.68	0.89	14.05	5.50	77.32	2.88	0.07	1.11
3.70	0.87	13.73	5.81	79.80	2.91	0.07	1.08
3.72	0.91	14.31	5.84	83.56	2.91	0.07	1.13
3.74	1.02	16.19	5.30	85.85	2.86	0.07	1.27
3.76	1.17	18.76	4.55	85.28	2.77	0.08	1.47
3.78	1.24	19.92	4.26	84.91	2.74	0.08	1.55
3.80	1.22	19.65	4.35	85.39	2.75	0.08	1.53
3.82	1.18	18.95	4.57	86.64	2.77	0.08	1.47
3.84	1.25	20.08	4.20	84.35	2.73	0.08	1.55

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	1.39	22.53	3.64	82.11	2.65	0.08	1.74
3.88	1.58	25.54	3.31	84.44	2.60	0.08	0.65
3.90	1.71	27.66	3.26	90.26	2.59	0.09	0.66
3.94	1.82	29.32	3.27	95.82	2.59	0.09	0.67
3.94	1.88	30.29	3.25	98.38	2.59	0.09	0.67
3.96	1.92	30.84	3.20	98.83	2.58	0.09	0.67
3.98	1.94	31.01	3.13	97.21	2.57	0.09	0.67
4.01	1.95	30.92	3.04	94.12	2.55	0.09	0.67
4.02	1.93	30.62	2.99	91.68	2.54	0.09	0.67
4.04	1.91	30.18	3.04	91.63	2.55	0.09	0.67
4.06	1.88	29.78	3.15	93.93	2.57	0.09	0.67
4.08	1.84	29.19	3.38	98.53	2.61	0.09	2.25
4.10	1.75	28.08	3.73	104.80	2.66	0.09	2.13
4.13	1.63	26.29	4.27	112.15	2.74	0.09	1.96
4.14	1.54	24.91	4.64	115.59	2.78	0.08	1.85
4.16	1.49	24.12	4.77	114.98	2.80	0.08	1.79
4.18	1.45	23.37	4.80	112.15	2.80	0.08	1.72
4.20	1.37	22.10	5.05	111.50	2.83	0.08	1.63
4.22	1.32	21.21	5.27	111.71	2.85	0.08	1.56
4.24	1.37	22.07	5.08	112.08	2.83	0.08	1.62
4.26	1.47	23.56	4.71	111.00	2.79	0.08	1.74
4.28	1.58	25.16	4.46	112.12	2.76	0.08	1.87
4.30	1.65	26.17	4.37	114.46	2.75	0.09	1.95
4.32	1.72	27.10	4.29	116.27	2.74	0.09	2.02
4.34	1.77	27.74	4.16	115.30	2.72	0.09	2.07
4.36	1.80	28.03	4.00	112.07	2.70	0.09	2.10
4.38	1.77	27.56	3.96	109.05	2.69	0.09	2.07
4.40	1.66	25.84	4.14	107.07	2.72	0.09	1.93
4.42	1.51	23.42	4.48	104.99	2.76	0.08	1.73
4.44	1.35	20.96	4.92	103.06	2.82	0.08	1.54
4.46	1.23	19.04	5.21	99.15	2.85	0.07	1.39
4.48	1.18	18.23	5.17	94.29	2.84	0.07	1.33
4.50	1.19	18.21	4.92	89.51	2.82	0.08	1.33
4.52	1.23	18.82	4.73	88.96	2.79	0.08	1.38
4.54	1.25	19.03	4.91	93.40	2.81	0.08	1.39
4.56	1.20	18.41	5.44	100.20	2.87	0.07	1.33
4.58	1.14	17.53	5.90	103.42	2.92	0.07	1.26
4.60	1.11	17.10	6.13	104.75	2.94	0.07	1.22
4.62	1.14	17.50	5.91	103.36	2.92	0.07	1.25
4.64	1.21	18.47	5.61	103.60	2.89	0.07	1.33
4.66	1.30	19.76	5.21	103.01	2.85	0.08	1.44
4.68	1.42	21.38	4.84	103.44	2.81	0.08	1.57
4.70	1.51	22.73	4.58	104.11	2.78	0.08	1.67
4.72	1.57	23.57	4.42	104.18	2.76	0.08	1.74
4.74	1.63	24.31	4.20	102.00	2.73	0.08	1.81
4.76	1.69	24.97	3.95	98.75	2.69	0.09	1.87
4.78	1.73	25.45	3.76	95.75	2.67	0.09	1.91
4.80	1.75	25.58	3.69	94.31	2.66	0.09	1.92

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	1.73	25.29	3.71	93.71	2.66	0.09	1.90
4.84	1.65	24.07	3.94	94.85	2.69	0.08	1.80
4.86	1.53	22.31	4.10	91.53	2.71	0.08	1.66
4.88	1.38	20.12	4.55	91.56	2.77	0.08	1.48
4.90	1.24	18.07	5.05	91.32	2.83	0.08	1.32
4.92	1.09	16.04	5.94	95.21	2.92	0.07	1.15
4.94	1.04	15.21	6.26	95.26	2.96	0.07	1.09
4.96	1.19	17.30	5.56	96.13	2.89	0.07	1.25
4.98	1.47	21.29	4.49	95.68	2.76	0.08	1.57
5.00	1.76	25.23	3.86	97.35	2.68	0.09	1.88
5.03	1.86	26.52	3.72	98.55	2.66	0.09	1.99
5.04	1.79	25.57	3.91	100.04	2.69	0.09	1.91
5.06	1.56	22.35	4.50	100.66	2.77	0.08	1.64
5.08	1.33	19.18	5.20	99.72	2.85	0.07	1.39
5.10	1.21	17.35	5.70	98.88	2.90	0.07	1.25
5.13	1.34	19.01	5.04	95.71	2.83	0.08	1.38
5.14	1.60	22.57	4.17	94.03	2.72	0.08	1.67
5.16	1.84	25.84	3.72	96.18	2.66	0.09	1.93
5.18	1.91	26.83	3.74	100.45	2.66	0.09	2.00
5.20	1.76	24.85	4.20	104.41	2.73	0.09	1.84
5.22	1.52	21.53	4.93	106.11	2.82	0.08	1.57
5.24	1.33	18.84	5.71	107.57	2.90	0.07	1.35
5.26	1.32	18.72	5.73	107.30	2.90	0.07	1.34
5.28	1.44	20.22	5.18	104.67	2.84	0.08	1.46
5.30	1.44	20.24	5.20	105.25	2.85	0.08	1.47
5.32	1.31	18.46	5.78	106.78	2.91	0.07	1.32
5.34	1.11	15.38	7.03	108.07	3.02	0.07	1.10
5.36	1.02	13.92	7.54	104.91	3.07	0.06	0.99
5.38	1.04	14.25	7.09	101.00	3.03	0.06	1.02
5.40	1.17	16.11	6.10	98.32	2.94	0.07	1.15
5.42	1.31	18.06	5.33	96.22	2.86	0.08	1.30
5.44	1.33	18.34	5.37	98.44	2.87	0.08	1.32
5.46	1.22	16.83	6.01	101.15	2.93	0.07	1.20
5.48	1.08	14.70	6.87	101.03	3.01	0.06	1.05
5.50	1.06	14.39	6.87	98.86	3.01	0.06	1.03
5.52	1.18	16.12	5.96	96.02	2.93	0.07	1.15
5.54	1.35	18.35	5.12	94.05	2.84	0.08	1.33
5.56	1.48	19.98	4.75	94.89	2.80	0.08	1.46
5.58	1.50	20.26	4.81	97.43	2.80	0.08	1.47
5.60	1.46	19.71	5.03	99.23	2.83	0.08	1.43
5.62	1.40	18.84	5.20	97.98	2.85	0.08	1.36
5.64	1.32	17.67	5.46	96.49	2.88	0.07	1.27
5.66	1.21	16.17	6.03	97.47	2.93	0.07	1.15
5.68	1.09	14.42	6.88	99.22	3.01	0.07	1.03
5.70	1.03	13.54	7.39	100.02	3.06	0.06	0.97
5.72	1.07	14.09	7.04	99.18	3.03	0.06	1.01
5.74	1.25	16.59	5.90	97.87	2.92	0.07	1.19
5.76	1.51	19.92	4.75	94.69	2.80	0.08	1.45

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	1.64	21.61	4.32	93.41	2.74	0.08	1.58
5.80	1.58	20.82	4.62	96.24	2.78	0.08	1.52
5.82	1.34	17.61	5.73	100.88	2.90	0.07	1.26
5.84	1.12	14.51	7.06	102.46	3.03	0.06	1.04
5.86	1.06	13.72	7.61	104.47	3.07	0.06	0.98
5.88	1.06	13.56	7.86	106.63	3.09	0.07	0.97
5.90	1.07	13.79	7.85	108.23	3.09	0.06	0.99
5.92	1.00	12.68	8.25	104.69	3.13	0.06	0.91
5.94	0.96	12.10	8.24	99.71	3.12	0.06	0.86
5.96	0.97	12.27	7.70	94.45	3.08	0.06	0.88
5.98	1.04	13.15	6.82	89.65	3.01	0.06	0.94
6.00	1.13	14.39	6.00	86.39	2.93	0.07	1.03
6.02	1.18	15.03	5.67	85.24	2.90	0.07	1.08
6.04	1.18	15.01	5.69	85.36	2.90	0.07	1.08
6.06	1.15	14.62	5.86	85.67	2.92	0.07	1.05
6.08	1.12	14.18	6.13	86.97	2.94	0.07	1.01
6.10	1.11	13.97	6.41	89.55	2.97	0.06	1.00
6.12	1.11	13.91	6.64	92.30	2.99	0.06	0.99
6.14	1.10	13.80	6.81	94.07	3.01	0.06	0.99
6.16	1.10	13.66	6.87	93.80	3.01	0.06	0.98
6.18	1.06	13.07	7.00	91.46	3.02	0.06	0.93
6.20	1.00	12.33	7.10	87.57	3.03	0.06	0.88
6.22	0.97	11.88	7.13	84.66	3.03	0.06	0.85
6.24	1.04	12.72	6.60	83.94	2.99	0.06	0.91
6.26	1.14	14.07	5.99	84.25	2.93	0.07	1.00
6.28	1.20	14.81	5.75	85.16	2.91	0.07	1.06
6.30	1.18	14.59	5.92	86.44	2.92	0.07	1.04
6.32	1.10	13.42	6.62	88.90	2.99	0.07	0.96
6.34	1.01	12.17	7.30	88.85	3.05	0.06	0.87
6.36	0.91	10.86	8.13	88.23	3.12	0.06	0.78
6.38	0.84	9.84	8.90	87.58	3.17	0.06	0.70
6.40	0.79	9.17	9.54	87.50	3.22	0.06	0.66
6.42	0.76	8.77	9.82	86.14	3.24	0.06	0.63
6.44	0.77	8.82	9.45	83.29	3.21	0.06	0.63
6.46	0.79	9.09	8.88	80.77	3.17	0.06	0.65
6.48	0.80	9.21	8.54	78.67	3.15	0.06	0.66
6.50	0.79	8.98	8.51	76.43	3.15	0.06	0.64
6.52	0.75	8.42	8.73	73.48	3.16	0.06	0.60
6.54	0.69	7.72	9.19	70.94	3.20	0.06	0.55
6.56	0.65	7.17	9.66	69.25	3.23	0.06	0.51
6.58	0.62	6.69	10.26	68.58	3.27	0.06	0.48
6.60	0.61	6.53	10.40	67.96	3.28	0.06	0.47
6.62	0.62	6.70	9.94	66.62	3.25	0.06	0.48
6.64	0.65	7.02	9.18	64.41	3.19	0.06	0.50
6.66	0.67	7.33	8.52	62.49	3.15	0.06	0.52
6.68	0.68	7.40	8.36	61.83	3.13	0.06	0.53
6.70	0.68	7.38	8.45	62.31	3.14	0.06	0.53
6.72	0.67	7.22	8.79	63.51	3.17	0.06	0.52

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	0.67	7.16	9.02	64.59	3.18	0.06	0.51
6.76	0.66	7.13	9.17	65.43	3.19	0.06	0.51
6.78	0.67	7.19	9.07	65.25	3.19	0.06	0.51
6.80	0.66	7.09	9.15	64.82	3.19	0.06	0.51
6.82	0.64	6.82	9.43	64.34	3.21	0.06	0.49
6.84	0.63	6.64	9.78	64.91	3.24	0.06	0.47
6.86	0.62	6.48	10.11	65.50	3.26	0.06	0.46
6.88	0.63	6.61	9.96	65.80	3.25	0.06	0.47
6.90	0.65	6.79	9.59	65.12	3.22	0.06	0.48
6.92	0.66	6.98	9.17	64.00	3.19	0.06	0.50
6.95	0.65	6.76	9.25	62.51	3.20	0.06	0.48
6.96	0.61	6.25	9.69	60.53	3.23	0.06	0.45
6.98	0.56	5.67	10.25	58.09	3.27	0.06	0.40
7.00	0.55	5.46	10.27	56.09	3.27	0.06	0.39
7.02	0.54	5.29	10.31	54.59	3.27	0.06	0.38
7.04	0.54	5.26	10.35	54.42	3.28	0.06	0.38
7.06	0.54	5.29	10.27	54.29	3.27	0.06	0.38
7.08	0.56	5.50	9.85	54.21	3.24	0.06	0.39
7.10	0.57	5.70	9.49	54.08	3.22	0.06	0.41
7.13	0.57	5.68	9.66	54.89	3.23	0.06	0.41
7.14	0.59	5.84	9.76	56.96	3.24	0.06	0.42
7.16	0.64	6.48	9.17	59.37	3.19	0.06	0.46
7.18	0.71	7.32	8.38	61.31	3.14	0.06	0.52
7.20	0.73	7.57	8.38	63.45	3.14	0.06	0.54
7.22	0.70	7.20	9.02	64.99	3.18	0.06	0.51
7.24	0.67	6.78	9.64	65.32	3.23	0.06	0.48
7.26	0.67	6.83	9.43	64.38	3.21	0.06	0.49
7.28	0.68	6.97	9.17	63.86	3.19	0.06	0.50
7.30	0.68	6.91	9.42	65.07	3.21	0.06	0.49
7.32	0.65	6.56	10.03	65.83	3.25	0.06	0.47
7.34	0.62	6.14	10.61	65.14	3.29	0.06	0.44
7.36	0.58	5.58	11.27	62.86	3.34	0.06	0.40
7.38	0.55	5.29	11.52	60.98	3.35	0.06	0.38
7.40	0.58	5.60	10.72	60.04	3.30	0.06	0.40
7.42	0.65	6.41	9.24	59.23	3.20	0.06	0.46
7.45	0.72	7.31	8.03	58.65	3.11	0.06	0.52
7.46	0.77	7.87	7.59	59.73	3.07	0.06	0.56
7.48	0.81	8.40	7.49	62.93	3.06	0.06	0.60
7.50	0.86	9.02	7.43	67.06	3.06	0.06	0.64
7.52	0.92	9.74	7.29	70.97	3.05	0.06	0.70
7.54	0.98	10.38	7.24	75.09	3.04	0.06	0.74
7.56	1.02	10.82	7.30	78.92	3.05	0.06	0.77
7.58	1.04	11.10	7.46	82.82	3.06	0.06	0.79
7.60	1.06	11.28	7.59	85.61	3.07	0.06	0.81
7.62	1.09	11.64	7.58	88.25	3.07	0.06	0.83
7.64	1.13	12.10	7.52	90.92	3.07	0.06	0.86
7.66	1.15	12.28	7.65	93.93	3.08	0.06	0.88
7.68	1.12	11.98	8.10	97.00	3.11	0.06	0.86

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	1.09	11.48	8.68	99.65	3.16	0.06	0.82
7.72	1.05	10.98	9.27	101.77	3.20	0.06	0.78
7.74	1.01	10.48	9.89	103.62	3.24	0.06	0.75
7.76	0.97	10.01	10.48	104.96	3.28	0.06	0.72
7.78	0.94	9.65	10.93	105.45	3.31	0.06	0.69
7.80	0.93	9.48	11.06	104.86	3.32	0.06	0.68
7.82	0.92	9.38	11.06	103.73	3.32	0.06	0.67
7.84	0.93	9.50	10.72	101.89	3.30	0.06	0.68
7.86	0.94	9.56	10.47	100.11	3.28	0.06	0.68
7.88	0.94	9.57	10.24	98.06	3.27	0.06	0.68
7.90	0.94	9.46	10.25	96.99	3.27	0.06	0.68
7.92	0.94	9.51	10.10	96.08	3.26	0.06	0.68
7.94	0.95	9.63	9.91	95.41	3.25	0.06	0.69
7.96	0.97	9.79	9.68	94.78	3.23	0.06	0.70
7.99	0.97	9.73	9.65	93.83	3.23	0.06	0.69
8.00	0.96	9.67	9.62	93.03	3.23	0.06	0.69
8.02	0.96	9.57	9.66	92.49	3.23	0.06	0.68
8.04	0.97	9.68	9.59	92.76	3.22	0.06	0.69
8.06	0.99	9.89	9.48	93.77	3.22	0.06	0.71
8.08	1.02	10.26	9.25	94.90	3.20	0.06	0.73
8.10	1.07	10.77	8.94	96.30	3.18	0.06	0.77
8.12	1.11	11.25	8.65	97.38	3.16	0.06	0.80
8.14	1.14	11.61	8.50	98.72	3.14	0.06	0.83
8.16	1.16	11.74	8.52	100.01	3.15	0.06	0.84
8.18	1.15	11.64	8.70	101.26	3.16	0.06	0.83
8.20	1.13	11.36	9.02	102.42	3.18	0.06	0.81
8.22	1.10	10.96	9.39	102.93	3.21	0.06	0.78
8.24	1.07	10.62	9.73	103.41	3.23	0.06	0.76
8.26	1.04	10.22	10.10	103.31	3.26	0.06	0.73
8.28	1.00	9.80	10.49	102.78	3.29	0.06	0.70
8.30	0.96	9.28	10.91	101.17	3.31	0.06	0.66
8.32	0.93	8.96	11.06	99.06	3.32	0.06	0.64
8.34	0.91	8.71	11.13	96.91	3.33	0.06	0.62
8.36	0.89	8.46	11.27	95.31	3.34	0.06	0.60
8.38	0.87	8.18	11.50	94.06	3.35	0.06	0.58
8.40	0.83	7.77	12.02	93.39	3.38	0.06	0.56
8.42	0.81	7.47	12.42	92.80	3.41	0.06	0.53
8.44	0.79	7.27	12.70	92.32	3.42	0.06	0.52
8.46	0.79	7.26	12.58	91.39	3.41	0.06	0.52
8.48	0.78	7.14	12.55	89.54	3.41	0.06	0.51
8.50	0.76	6.85	12.72	87.07	3.42	0.06	0.49
8.52	0.73	6.51	13.00	84.60	3.44	0.06	0.46
8.54	0.70	6.18	13.33	82.42	3.46	0.06	0.44
8.56	0.68	5.93	13.59	80.52	3.47	0.06	0.42
8.58	0.65	5.57	14.09	78.50	3.50	0.06	0.40
8.60	0.62	5.25	14.61	76.69	3.53	0.06	0.37
8.62	0.60	4.99	14.90	74.32	3.54	0.06	0.36
8.64	0.59	4.85	14.81	71.79	3.54	0.06	0.35

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	0.58	4.78	14.42	68.98	3.52	0.06	0.34
8.68	0.58	4.71	14.08	66.25	3.50	0.06	0.34
8.70	0.56	4.55	13.99	63.63	3.49	0.06	0.32
8.72	0.56	4.45	13.77	61.22	3.48	0.06	0.32
8.74	0.53	4.18	14.05	58.74	3.50	0.06	0.30
8.76	0.51	3.90	14.44	56.33	3.52	0.06	0.28
8.78	0.48	3.55	15.21	53.94	3.56	0.06	0.25
8.80	0.47	3.48	15.08	52.53	3.55	0.06	0.25
8.82	0.50	3.80	13.58	51.62	3.47	0.06	0.27
8.84	0.54	4.22	12.14	51.19	3.39	0.06	0.30
8.86	0.57	4.57	11.12	50.77	3.33	0.06	0.33
8.88	0.59	4.71	10.82	50.94	3.31	0.06	0.34
8.90	0.60	4.83	10.55	50.99	3.29	0.06	0.35
8.92	0.60	4.84	10.63	51.47	3.29	0.06	0.35
8.94	0.59	4.74	10.99	52.10	3.32	0.06	0.34
8.96	0.59	4.68	11.23	52.60	3.33	0.06	0.33
8.98	0.61	4.89	10.85	53.09	3.31	0.06	0.35
9.00	0.66	5.47	9.90	54.18	3.25	0.06	0.39
9.02	0.73	6.13	8.99	55.16	3.18	0.06	0.44
9.05	0.78	6.68	8.49	56.72	3.14	0.06	0.48
9.06	0.81	6.99	8.36	58.49	3.13	0.06	0.50
9.08	0.83	7.21	8.44	60.91	3.14	0.06	0.52
9.10	0.85	7.44	8.53	63.41	3.15	0.06	0.53
9.12	0.88	7.71	8.53	65.80	3.15	0.06	0.55
9.14	0.90	7.97	8.50	67.73	3.14	0.06	0.57
9.16	0.91	8.03	8.72	70.03	3.16	0.06	0.57
9.18	0.90	7.91	9.10	72.00	3.19	0.06	0.56
9.20	0.88	7.62	9.65	73.59	3.23	0.06	0.54
9.22	0.85	7.31	10.09	73.80	3.26	0.06	0.52
9.25	0.81	6.93	10.62	73.53	3.29	0.06	0.49
9.26	0.78	6.52	11.21	73.11	3.33	0.06	0.47
9.28	0.73	6.04	12.02	72.58	3.38	0.06	0.43
9.30	0.69	5.61	12.77	71.67	3.43	0.06	0.40
9.32	0.67	5.33	13.22	70.52	3.45	0.06	0.38
9.34	0.66	5.24	13.20	69.16	3.45	0.06	0.37
9.36	0.66	5.21	12.99	67.73	3.44	0.06	0.37
9.38	0.66	5.20	12.68	65.98	3.42	0.06	0.37
9.40	0.65	5.10	12.57	64.13	3.41	0.06	0.36
9.42	0.63	4.91	12.65	62.08	3.42	0.06	0.35
9.44	0.62	4.73	12.72	60.17	3.42	0.06	0.34
9.46	0.60	4.55	12.88	58.66	3.43	0.06	0.33
9.48	0.59	4.39	13.11	57.57	3.45	0.06	0.31
9.50	0.56	4.15	13.65	56.65	3.48	0.06	0.30
9.52	0.54	3.91	14.23	55.65	3.51	0.06	0.28
9.54	0.52	3.71	14.66	54.31	3.53	0.06	0.26
9.56	0.52	3.67	14.50	53.16	3.52	0.06	0.26
9.58	0.53	3.76	13.84	51.95	3.49	0.06	0.27
9.60	0.55	3.93	12.99	51.01	3.44	0.06	0.28

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	0.56	4.02	12.42	49.96	3.41	0.06	0.29
9.64	0.55	3.99	12.20	48.66	3.39	0.06	0.28
9.66	0.54	3.81	12.29	46.87	3.40	0.06	0.27
9.68	0.51	3.56	12.61	44.85	3.42	0.06	0.25
9.70	0.50	3.44	12.62	43.44	3.42	0.06	0.25
9.72	0.50	3.40	12.50	42.52	3.41	0.06	0.24
9.74	0.52	3.57	11.86	42.38	3.37	0.06	0.26
9.76	0.57	4.09	10.51	43.04	3.29	0.06	0.29
9.78	0.67	5.13	8.77	44.97	3.17	0.06	0.37
9.80	0.89	7.34	6.91	50.70	3.01	0.06	0.52
9.82	1.07	9.23	6.13	56.62	2.94	0.06	0.66
9.84	1.18	10.26	6.01	61.69	2.93	0.07	0.73
9.86	1.07	9.13	6.92	63.20	3.02	0.06	0.65
9.88	0.86	7.05	8.74	61.62	3.16	0.06	0.50
9.90	0.66	4.98	11.59	57.74	3.36	0.06	0.36
9.92	0.54	3.77	14.25	53.69	3.51	0.06	0.27
9.94	0.51	3.41	14.98	51.00	3.55	0.06	0.24
9.96	0.52	3.48	14.24	49.59	3.51	0.06	0.25
9.98	0.53	3.61	13.28	47.89	3.45	0.06	0.26
10.01	0.54	3.73	12.64	47.09	3.42	0.06	0.27
10.02	0.54	3.70	12.42	45.92	3.41	0.06	0.26
10.04	0.53	3.58	12.49	44.68	3.41	0.06	0.26
10.06	0.53	3.53	12.41	43.81	3.40	0.06	0.25
10.08	0.56	3.83	11.44	43.82	3.35	0.06	0.27
10.10	0.68	5.07	8.97	45.47	3.18	0.06	0.36
10.12	0.92	7.46	6.35	47.35	2.96	0.06	0.53
10.14	1.26	10.85	4.56	49.46	2.77	0.07	0.77
10.16	1.47	12.91	4.01	51.76	2.70	0.08	0.92
10.18	1.43	12.49	4.22	52.72	2.73	0.08	0.89
10.20	1.17	9.93	5.44	54.01	2.87	0.07	0.71
10.22	0.89	7.09	7.68	54.41	3.08	0.06	0.51
10.24	0.73	5.45	9.92	54.12	3.25	0.06	0.39
10.26	0.65	4.67	11.41	53.27	3.34	0.06	0.33
10.28	0.63	4.48	11.84	53.04	3.37	0.06	0.32
10.30	0.63	4.45	11.99	53.30	3.38	0.06	0.32
10.32	0.64	4.57	11.55	52.74	3.35	0.06	0.33
10.34	0.67	4.82	10.76	51.80	3.30	0.06	0.34
10.36	0.69	5.05	10.04	50.68	3.26	0.06	0.36
10.38	0.72	5.35	9.42	50.44	3.21	0.06	0.38
10.40	0.77	5.81	8.80	51.12	3.17	0.06	0.41
10.42	0.87	6.76	7.82	52.86	3.09	0.06	0.48
10.44	1.08	8.78	6.28	55.18	2.96	0.06	0.63
10.46	1.40	11.98	4.73	56.64	2.79	0.07	0.86
10.48	1.72	15.06	3.91	58.91	2.69	0.08	1.07
10.50	1.80	15.84	3.98	63.08	2.70	0.08	1.13
10.52	1.64	14.24	4.73	67.39	2.79	0.08	1.02
10.54	1.36	11.51	6.04	69.48	2.93	0.07	0.82
10.56	1.23	10.16	6.77	68.77	3.00	0.06	0.73

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	1.25	10.38	6.53	67.76	2.98	0.06	0.74
10.60	1.36	11.40	6.01	68.54	2.93	0.07	0.81
10.62	1.39	11.65	6.07	70.77	2.94	0.07	0.83
10.64	1.26	10.43	6.97	72.68	3.02	0.06	0.74
10.66	1.16	9.48	7.60	72.04	3.07	0.06	0.68
10.68	1.26	10.42	6.72	70.04	3.00	0.06	0.74
10.70	1.56	13.22	5.13	67.75	2.84	0.07	0.94
10.72	1.77	15.27	4.46	68.17	2.76	0.08	1.09
10.74	1.71	14.69	4.82	70.80	2.80	0.08	1.05
10.76	1.46	12.22	5.93	72.40	2.92	0.07	0.87
10.78	1.16	9.29	7.63	70.88	3.08	0.06	0.66
10.80	1.04	8.19	8.37	68.54	3.13	0.06	0.58
10.82	1.02	8.00	8.50	68.00	3.14	0.06	0.57
10.84	1.06	8.29	8.31	68.93	3.13	0.06	0.59
10.86	1.00	7.72	8.91	68.79	3.18	0.06	0.55
10.88	0.95	7.26	9.31	67.57	3.20	0.06	0.52
10.90	0.93	7.04	9.34	65.74	3.21	0.06	0.50
10.92	0.89	6.65	9.61	63.91	3.23	0.06	0.48
10.94	0.87	6.49	9.76	63.30	3.24	0.06	0.46
10.96	0.90	6.74	9.39	63.33	3.21	0.06	0.48
10.98	0.97	7.40	8.56	63.34	3.15	0.06	0.53
11.00	1.01	7.74	8.23	63.70	3.12	0.06	0.55
11.02	1.04	7.97	8.01	63.83	3.11	0.06	0.57
11.04	1.07	8.30	7.69	63.79	3.08	0.06	0.59
11.06	1.09	8.47	7.52	63.69	3.07	0.06	0.61
11.08	1.09	8.44	7.66	64.65	3.08	0.06	0.60
11.10	1.03	7.87	8.42	66.28	3.14	0.06	0.56
11.12	0.96	7.19	9.38	67.46	3.21	0.06	0.51
11.14	0.88	6.45	10.41	67.11	3.28	0.06	0.46
11.16	0.84	6.01	11.01	66.15	3.32	0.06	0.43
11.19	0.79	5.61	11.46	64.32	3.35	0.06	0.40
11.20	0.75	5.21	11.91	62.05	3.37	0.06	0.37
11.22	0.73	5.03	11.89	59.85	3.37	0.06	0.36
11.24	0.74	5.05	11.37	57.38	3.34	0.06	0.36
11.26	0.77	5.34	10.50	56.07	3.29	0.06	0.38
11.28	0.80	5.58	9.89	55.21	3.25	0.06	0.40
11.30	0.82	5.81	9.44	54.84	3.21	0.06	0.42
11.32	0.81	5.71	9.55	54.51	3.22	0.06	0.41
11.34	0.78	5.39	10.03	54.13	3.25	0.06	0.39
11.36	0.76	5.20	10.41	54.16	3.28	0.06	0.37
11.38	0.76	5.16	10.53	54.31	3.29	0.06	0.37
11.40	0.74	5.04	10.87	54.82	3.31	0.06	0.36
11.42	0.72	4.83	11.36	54.92	3.34	0.06	0.35
11.44	0.70	4.63	11.80	54.70	3.37	0.06	0.33
11.46	0.70	4.60	11.77	54.20	3.37	0.06	0.33
11.48	0.72	4.83	11.13	53.73	3.33	0.06	0.34
11.50	0.80	5.46	9.87	53.91	3.24	0.06	0.39
11.52	0.93	6.71	8.11	54.41	3.11	0.06	0.48

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	1.08	8.03	6.95	55.85	3.02	0.06	0.57
11.56	1.24	9.46	6.20	58.70	2.95	0.06	0.68
11.58	1.41	11.06	5.64	62.35	2.89	0.07	0.79
11.60	1.59	12.67	5.30	67.20	2.86	0.07	0.90
11.62	1.76	14.16	5.09	72.01	2.83	0.08	1.01
11.64	1.84	14.89	5.15	76.68	2.84	0.08	1.06
11.66	1.82	14.62	5.53	80.92	2.88	0.07	1.04
11.68	1.69	13.47	6.07	81.74	2.94	0.07	0.96
11.70	1.50	11.70	6.82	79.77	3.01	0.07	0.84
11.72	1.46	11.38	6.56	74.64	2.98	0.06	0.81
11.74	1.62	12.73	5.52	70.24	2.88	0.07	0.91
11.76	1.90	15.30	4.46	68.21	2.76	0.08	1.09
11.78	2.03	16.52	4.08	67.43	2.71	0.08	1.17
11.80	2.00	16.17	4.25	68.80	2.73	0.08	1.15
11.82	1.89	15.12	4.66	70.41	2.78	0.08	1.08
11.84	1.86	14.85	4.89	72.62	2.81	0.08	1.06
11.86	1.86	14.78	4.95	73.14	2.82	0.08	1.05
11.89	1.80	14.26	5.19	74.07	2.85	0.08	1.02
11.90	1.69	13.24	5.73	75.86	2.90	0.07	0.95
11.92	1.64	12.73	6.14	78.23	2.94	0.07	0.91
11.94	1.69	13.20	5.79	76.40	2.91	0.07	0.94
11.96	1.73	13.51	5.40	72.93	2.87	0.07	0.96
11.98	1.67	12.99	5.24	68.11	2.85	0.07	0.93
12.00	1.54	11.78	5.67	66.75	2.90	0.07	0.84
12.03	1.41	10.62	6.20	65.81	2.95	0.07	0.76
12.04	1.24	9.10	7.20	65.55	3.04	0.06	0.65
12.06	1.02	7.13	8.92	63.53	3.18	0.06	0.51
12.08	0.80	5.22	11.56	60.30	3.35	0.06	0.37
12.10	0.69	4.21	13.55	57.10	3.47	0.06	0.30
12.12	0.67	4.05	13.74	55.71	3.48	0.06	0.29
12.14	0.70	4.29	12.77	54.75	3.43	0.06	0.31
12.16	0.73	4.54	11.87	53.86	3.37	0.06	0.32
12.18	0.74	4.61	11.53	53.17	3.35	0.06	0.33
12.20	0.79	5.04	10.63	53.61	3.29	0.06	0.36
12.22	1.00	6.87	8.05	55.26	3.11	0.06	0.49
12.24	1.30	9.48	5.81	55.10	2.91	0.07	0.68
12.26	1.51	11.30	4.94	55.80	2.82	0.07	0.81
12.28	1.46	10.82	5.50	59.54	2.88	0.07	0.77
12.30	1.21	8.66	7.39	63.99	3.06	0.06	0.62
12.32	0.95	6.40	10.00	63.93	3.25	0.06	0.46
12.34	0.75	4.69	12.82	60.09	3.43	0.06	0.33
12.36	0.65	3.79	14.81	56.08	3.54	0.06	0.27
12.38	0.61	3.42	15.91	54.47	3.60	0.06	0.24
12.40	0.59	3.24	16.48	53.45	3.62	0.06	0.23
12.42	0.59	3.21	16.34	52.49	3.62	0.06	0.23
12.44	0.58	3.12	16.12	50.25	3.61	0.06	0.22
12.46	0.57	3.07	15.53	47.74	3.58	0.06	0.22
12.48	0.57	3.04	14.99	45.61	3.55	0.06	0.22

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	0.58	3.14	14.20	44.62	3.51	0.06	0.22
12.52	0.61	3.40	13.16	44.70	3.45	0.06	0.24
12.54	0.65	3.74	12.12	45.38	3.39	0.06	0.27
12.56	0.72	4.31	11.07	47.72	3.32	0.06	0.31
12.58	0.79	4.89	10.35	50.55	3.28	0.06	0.35
12.60	0.85	5.38	9.96	53.65	3.25	0.06	0.38
12.62	0.83	5.24	10.77	56.46	3.30	0.06	0.37
12.64	0.77	4.69	12.61	59.11	3.42	0.06	0.33
12.66	0.69	4.06	14.86	60.33	3.54	0.06	0.29
12.68	0.66	3.80	16.06	61.01	3.60	0.06	0.27
12.70	0.67	3.84	15.98	61.43	3.60	0.06	0.27
12.72	0.68	3.92	15.64	61.32	3.58	0.06	0.28
12.74	0.68	3.90	15.46	60.35	3.57	0.06	0.28
12.76	0.68	3.91	14.99	58.56	3.55	0.06	0.28
12.78	0.70	4.02	14.15	56.88	3.50	0.06	0.29
12.81	0.72	4.22	13.22	55.74	3.45	0.06	0.30
12.82	0.74	4.39	12.68	55.69	3.42	0.06	0.31
12.84	0.76	4.51	12.42	55.98	3.41	0.06	0.32
12.86	0.76	4.57	12.34	56.42	3.40	0.06	0.33
12.88	0.79	4.75	12.01	57.04	3.38	0.06	0.34
12.90	0.82	5.04	11.45	57.73	3.35	0.06	0.36
12.92	0.87	5.43	10.74	58.31	3.30	0.06	0.39
12.94	0.90	5.67	10.36	58.78	3.28	0.06	0.41
12.96	0.91	5.75	10.32	59.28	3.27	0.06	0.41
12.98	0.90	5.66	10.53	59.61	3.29	0.06	0.40
13.00	0.90	5.60	10.70	59.95	3.30	0.06	0.40
13.02	0.91	5.71	10.63	60.69	3.29	0.06	0.41
13.04	0.93	5.86	10.54	61.72	3.29	0.06	0.42
13.07	0.95	6.02	10.53	63.34	3.29	0.06	0.43
13.08	0.96	6.08	10.63	64.58	3.29	0.06	0.43
13.10	0.98	6.26	10.51	65.79	3.29	0.06	0.45
13.12	1.01	6.48	10.29	66.68	3.27	0.06	0.46
13.14	1.04	6.74	10.09	67.97	3.26	0.06	0.48
13.16	1.05	6.80	10.20	69.34	3.27	0.06	0.49
13.18	1.05	6.81	10.38	70.68	3.28	0.06	0.49
13.20	1.05	6.76	10.60	71.60	3.29	0.06	0.48
13.22	1.05	6.80	10.65	72.44	3.30	0.06	0.49
13.24	1.06	6.84	10.68	73.05	3.30	0.06	0.49
13.26	1.07	6.89	10.71	73.73	3.30	0.06	0.49
13.28	1.07	6.88	10.78	74.17	3.30	0.06	0.49
13.30	1.07	6.85	10.88	74.54	3.31	0.06	0.49
13.32	1.07	6.85	10.95	74.97	3.32	0.06	0.49
13.34	1.07	6.89	10.96	75.52	3.32	0.06	0.49
13.37	1.09	7.01	10.84	76.00	3.31	0.06	0.50
13.38	1.11	7.17	10.63	76.20	3.29	0.06	0.51
13.40	1.12	7.28	10.48	76.27	3.28	0.06	0.52
13.42	1.13	7.34	10.40	76.36	3.28	0.06	0.52
13.44	1.14	7.34	10.42	76.48	3.28	0.06	0.52

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	1.15	7.40	10.33	76.45	3.27	0.06	0.53
13.48	1.14	7.39	10.36	76.53	3.28	0.06	0.53
13.50	1.14	7.33	10.49	76.83	3.28	0.06	0.52
13.52	1.14	7.31	10.56	77.27	3.29	0.06	0.52
13.54	1.14	7.32	10.60	77.65	3.29	0.06	0.52
13.56	1.15	7.37	10.58	78.00	3.29	0.06	0.53
13.58	1.13	7.22	10.84	78.30	3.31	0.06	0.52
13.60	1.11	7.00	11.20	78.38	3.33	0.06	0.50
13.62	1.08	6.75	11.60	78.32	3.36	0.06	0.48
13.64	1.05	6.53	11.95	78.03	3.38	0.06	0.47
13.66	1.03	6.36	12.25	77.85	3.40	0.06	0.45
13.68	1.01	6.16	12.52	77.06	3.41	0.06	0.44
13.70	0.98	5.96	12.78	76.14	3.43	0.06	0.43
13.72	0.95	5.66	13.19	74.62	3.45	0.06	0.40
13.74	0.90	5.31	13.70	72.68	3.48	0.06	0.38
13.76	0.85	4.87	14.37	69.98	3.52	0.06	0.35
13.78	0.80	4.51	14.87	67.10	3.54	0.06	0.32
13.80	0.77	4.23	15.23	64.45	3.56	0.06	0.30
13.83	0.75	4.04	15.31	61.94	3.57	0.06	0.29
13.84	0.73	3.88	15.34	59.51	3.57	0.06	0.28
13.86	0.72	3.80	15.09	57.31	3.55	0.06	0.27
13.88	0.72	3.83	14.51	55.53	3.52	0.06	0.27
13.90	0.74	3.95	13.65	53.94	3.48	0.06	0.28
13.92	0.75	4.02	13.01	52.34	3.44	0.06	0.29
13.94	0.75	4.02	12.63	50.77	3.42	0.06	0.29
13.96	0.74	3.94	12.53	49.40	3.41	0.06	0.28
13.99	0.75	4.03	12.01	48.35	3.38	0.06	0.29
14.00	0.83	4.64	10.42	48.40	3.28	0.06	0.33
14.02	1.00	5.93	8.27	49.06	3.13	0.06	0.42
14.04	1.24	7.83	6.40	50.12	2.97	0.06	0.56
14.06	1.58	10.50	4.95	51.97	2.82	0.07	0.75
14.08	1.94	13.42	4.09	54.90	2.71	0.08	0.95
14.10	2.22	15.74	3.76	59.12	2.67	0.08	1.10
14.12	2.27	16.06	3.87	62.14	2.68	0.08	1.13
14.14	2.10	14.58	4.36	63.57	2.75	0.08	1.03
14.16	1.77	11.85	5.43	64.40	2.87	0.07	0.85
14.18	1.42	9.13	7.18	65.52	3.04	0.06	0.65
14.20	1.12	6.80	9.44	64.23	3.21	0.06	0.49
14.22	0.91	5.16	11.74	60.60	3.36	0.06	0.37
14.24	0.79	4.21	13.35	56.26	3.46	0.06	0.30
14.26	0.76	3.99	13.62	54.40	3.47	0.06	0.29
14.28	0.92	5.25	10.62	55.71	3.29	0.06	0.37
14.30	1.32	8.32	6.83	56.77	3.01	0.06	0.59
14.32	1.80	12.10	4.50	54.45	2.77	0.08	0.86
14.34	2.20	15.36	3.58	55.02	2.64	0.08	1.07
14.36	2.43	17.26	3.23	55.80	2.58	0.08	0.61
14.38	2.59	18.52	3.20	59.23	2.58	0.08	0.61
14.40	2.66	19.00	3.29	62.57	2.59	0.09	0.62

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	2.46	17.20	3.91	67.29	2.69	0.09	1.21
14.44	2.08	14.05	4.97	69.85	2.82	0.08	1.00
14.46	1.56	10.06	6.85	68.97	3.01	0.07	0.72
14.48	1.30	8.06	8.21	66.20	3.12	0.06	0.58
14.50	1.34	8.32	7.93	65.98	3.10	0.06	0.59
14.52	1.66	10.75	6.16	66.23	2.95	0.07	0.77
14.55	1.98	13.14	5.11	67.16	2.84	0.08	0.94
14.56	2.04	13.59	5.07	68.85	2.83	0.08	0.97
14.58	1.87	12.31	5.80	71.42	2.91	0.07	0.88
14.60	1.66	10.71	6.83	73.12	3.01	0.07	0.76
14.62	1.66	10.67	6.78	72.35	3.00	0.06	0.76
14.64	1.87	12.24	5.91	72.39	2.92	0.07	0.87
14.66	2.06	13.67	5.36	73.30	2.86	0.08	0.98
14.68	2.03	13.41	5.73	76.81	2.90	0.07	0.96
14.70	1.79	11.56	6.86	79.28	3.01	0.07	0.83
14.72	1.50	9.37	8.37	78.49	3.14	0.06	0.67
14.74	1.25	7.49	9.90	74.14	3.25	0.06	0.53
14.76	1.13	6.59	10.82	71.25	3.31	0.06	0.47
14.78	1.02	5.75	11.83	67.98	3.37	0.06	0.41
14.80	0.97	5.40	12.32	66.46	3.40	0.06	0.39
14.82	0.93	5.02	12.55	62.99	3.41	0.06	0.36
14.84	1.02	5.68	10.94	62.18	3.31	0.06	0.41
14.86	1.18	6.94	8.84	61.32	3.17	0.06	0.50
14.88	1.26	7.49	7.98	59.76	3.10	0.06	0.53
14.90	1.18	6.91	8.53	58.88	3.15	0.06	0.49
14.92	1.04	5.81	9.76	56.71	3.24	0.06	0.42
14.94	0.98	5.36	10.35	55.46	3.28	0.06	0.38
14.96	0.98	5.40	10.03	54.18	3.25	0.06	0.39
14.98	0.98	5.37	10.18	54.70	3.26	0.06	0.38
15.01	0.97	5.30	10.41	55.21	3.28	0.06	0.38
15.03	0.98	5.35	10.29	55.09	3.27	0.06	0.38
15.04	1.00	5.50	9.82	54.06	3.24	0.06	0.39
15.06	1.01	5.54	9.55	52.93	3.22	0.06	0.40
15.08	1.00	5.45	9.55	52.10	3.22	0.06	0.39
15.10	0.96	5.19	9.97	51.75	3.25	0.06	0.37
15.12	0.92	4.86	10.53	51.15	3.29	0.06	0.35
15.14	0.88	4.57	10.96	50.06	3.32	0.06	0.33
15.16	0.87	4.48	10.90	48.80	3.31	0.06	0.32
15.18	0.88	4.54	10.55	47.89	3.29	0.06	0.32
15.20	0.90	4.71	10.12	47.72	3.26	0.06	0.34
15.22	0.95	5.07	9.52	48.27	3.22	0.06	0.36
15.24	1.00	5.38	9.15	49.24	3.19	0.06	0.38
15.26	1.05	5.74	8.77	50.40	3.17	0.06	0.41
15.28	1.05	5.78	8.88	51.32	3.17	0.06	0.41
15.30	1.05	5.77	9.01	51.94	3.18	0.06	0.41
15.32	1.02	5.55	9.50	52.71	3.22	0.06	0.40
15.34	1.00	5.41	9.91	53.57	3.25	0.06	0.39
15.36	0.98	5.21	10.48	54.57	3.28	0.06	0.37

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	0.95	5.01	10.96	54.92	3.32	0.06	0.36
15.40	0.93	4.83	11.33	54.71	3.34	0.06	0.34
15.42	0.92	4.72	11.48	54.23	3.35	0.06	0.34
15.45	0.93	4.79	11.20	53.65	3.33	0.06	0.34
15.46	0.93	4.84	10.95	53.04	3.32	0.06	0.35
15.48	0.94	4.91	10.65	52.36	3.30	0.06	0.35
15.50	0.95	4.91	10.52	51.69	3.29	0.06	0.35
15.52	0.95	4.96	10.37	51.40	3.28	0.06	0.35
15.54	0.98	5.14	9.93	51.06	3.25	0.06	0.37

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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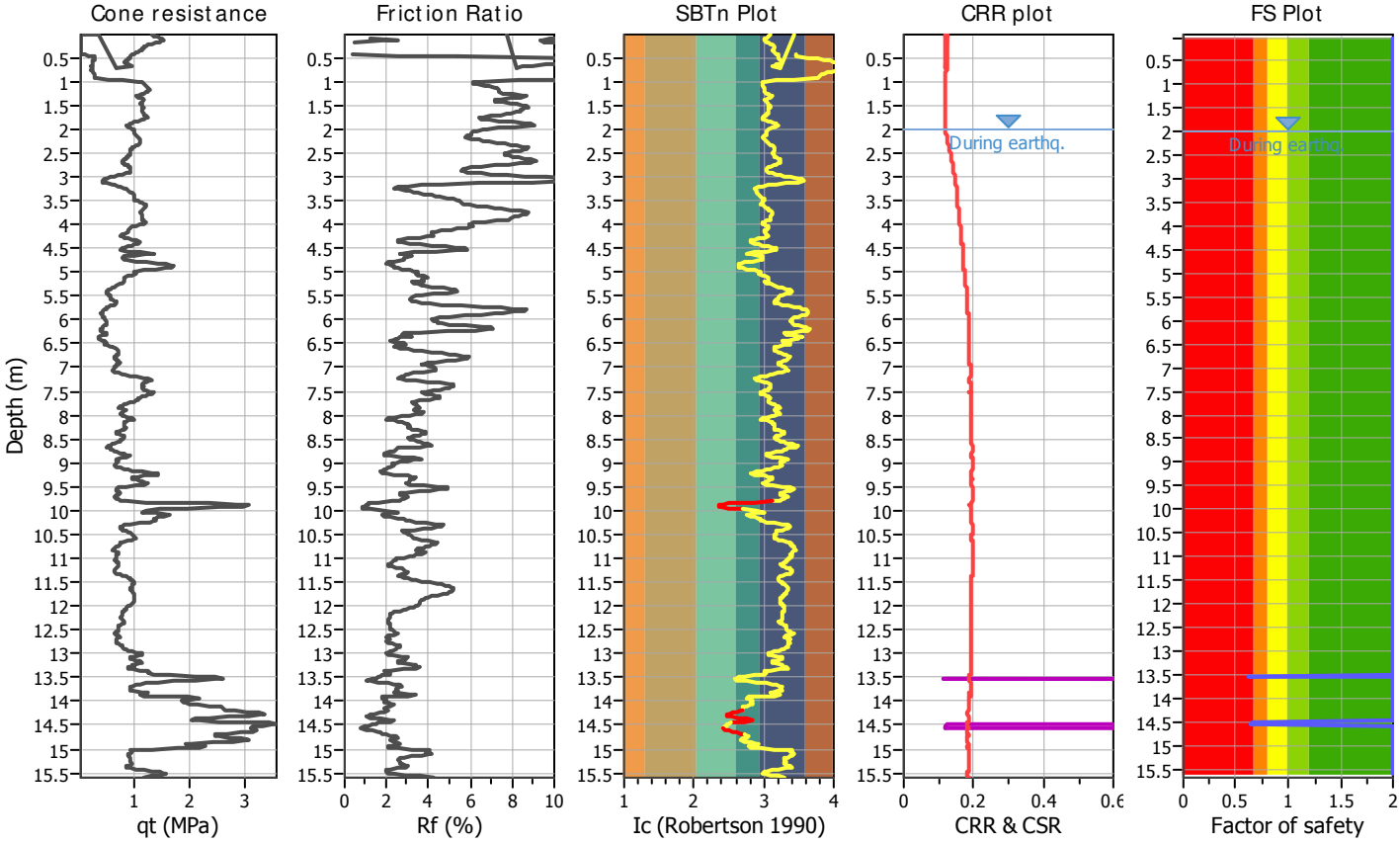
LIQUEFACTION ANALYSIS REPORT

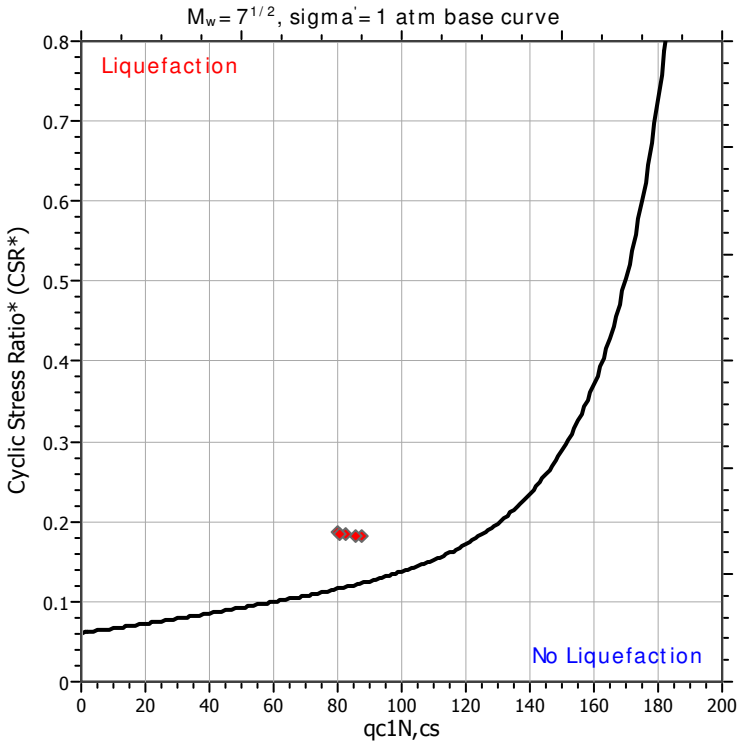
Project title : Location :

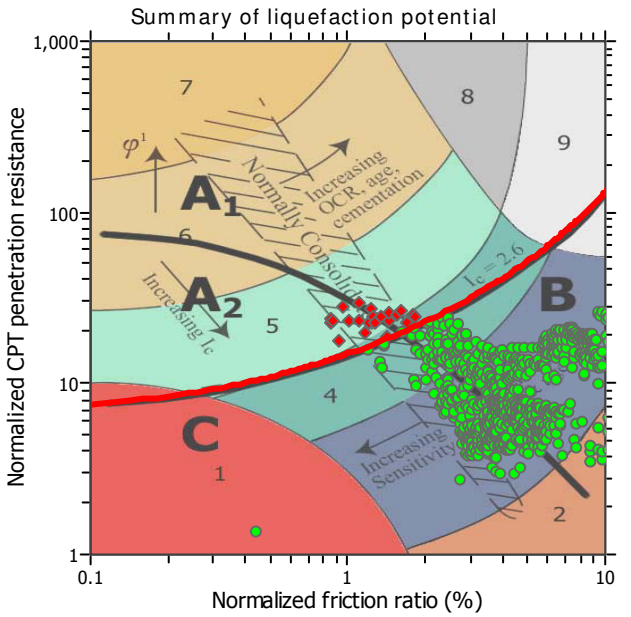
CPT file : Cptu-3

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.50 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.22	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

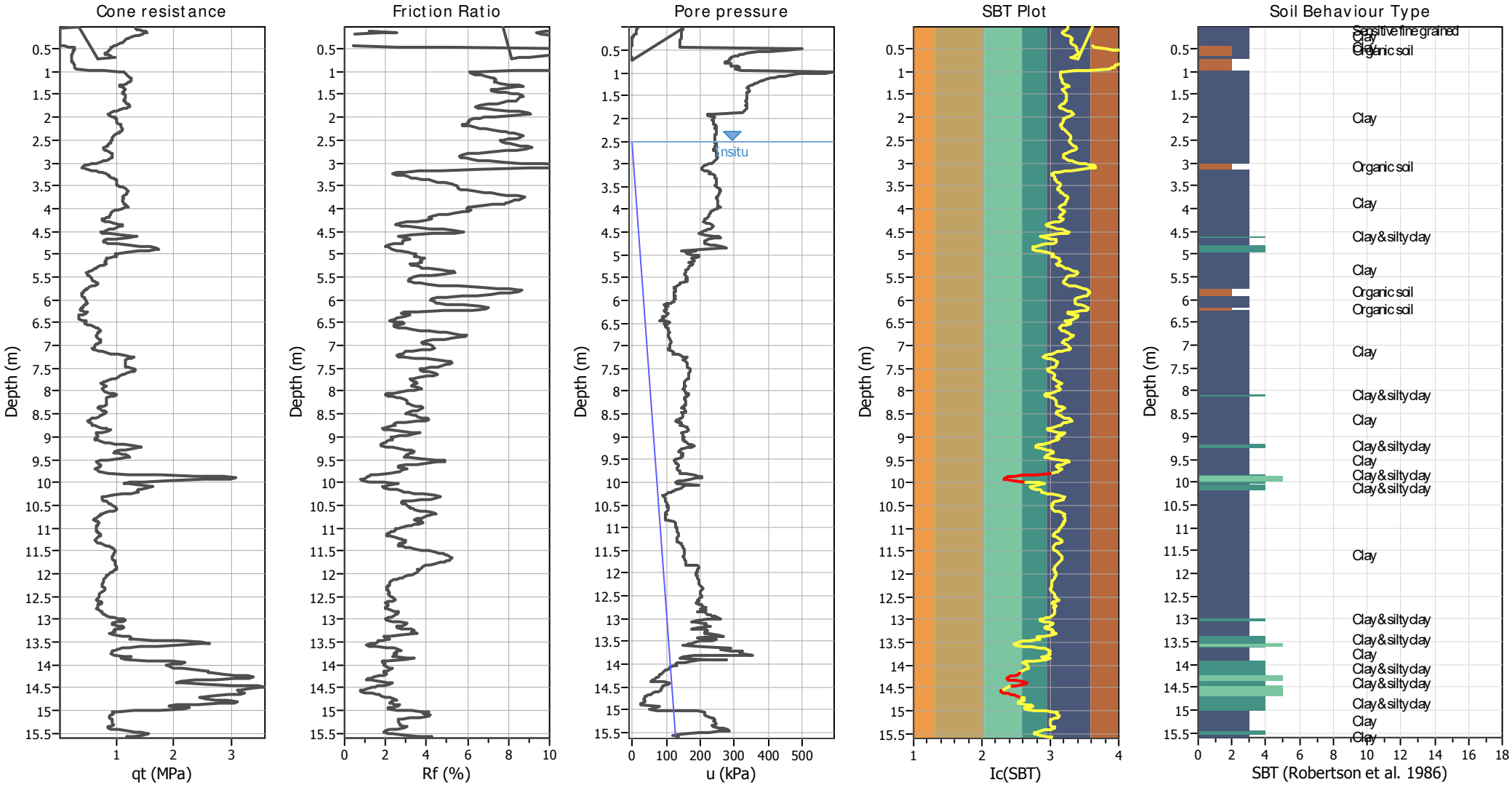






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



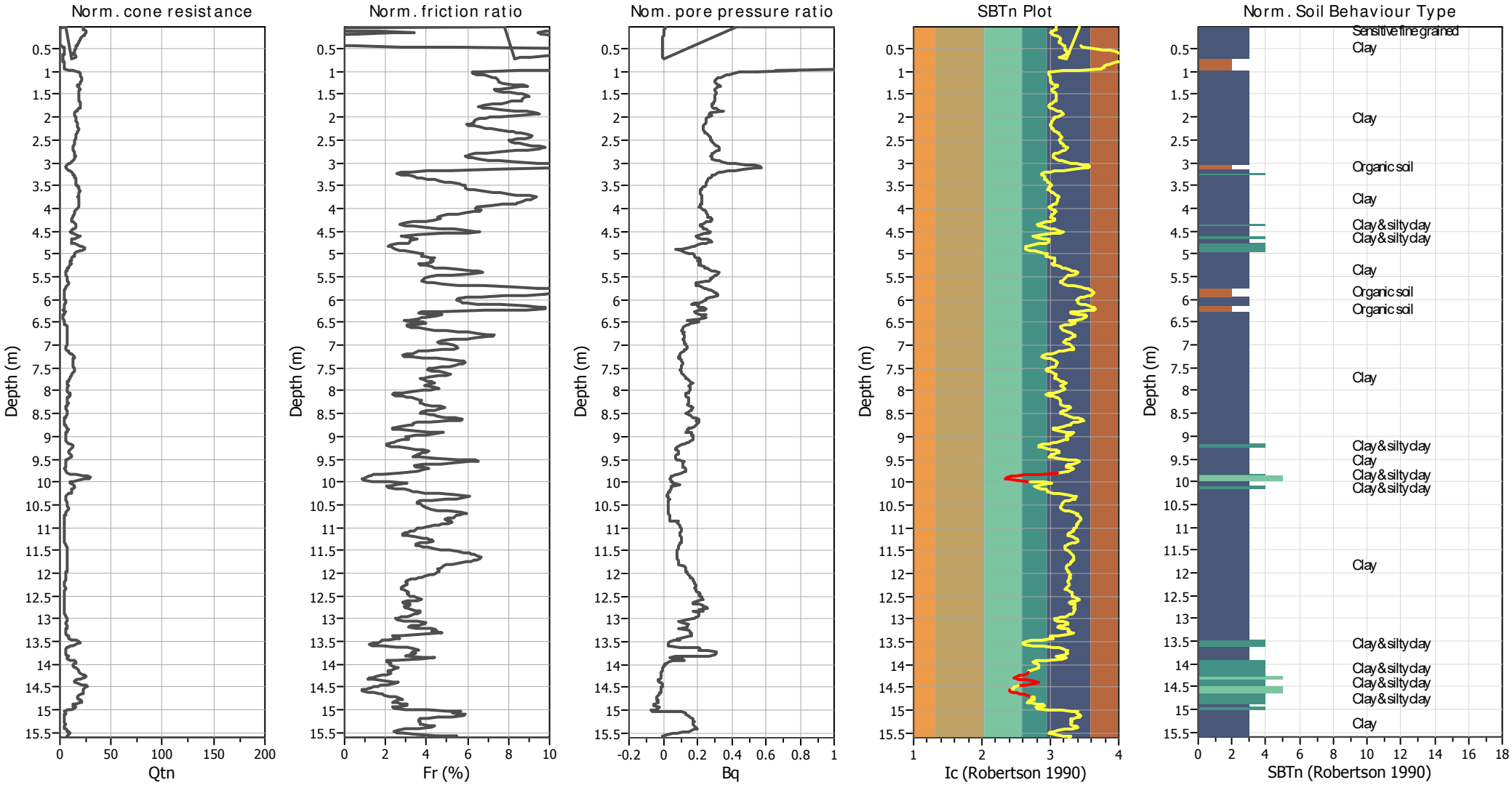
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



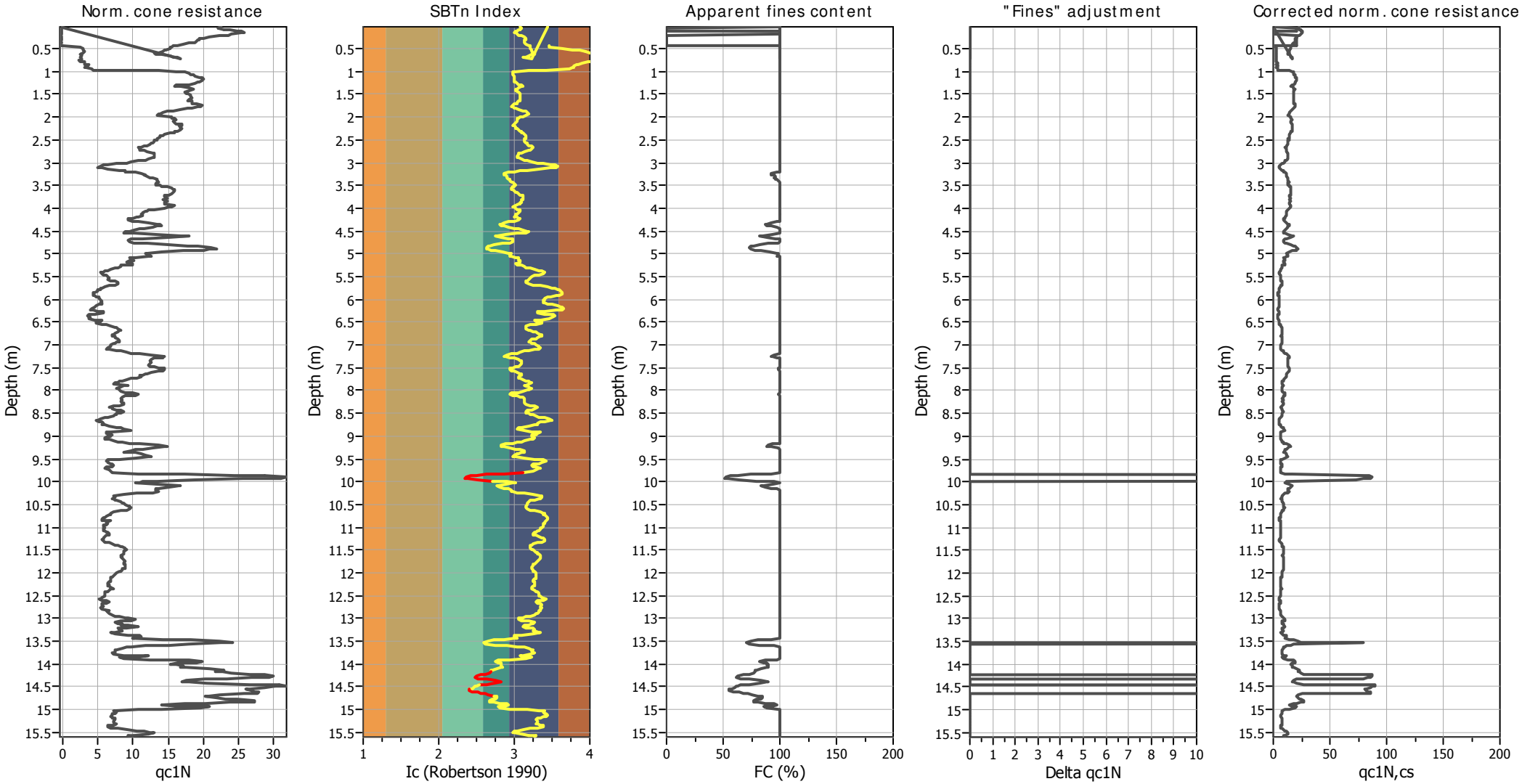
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

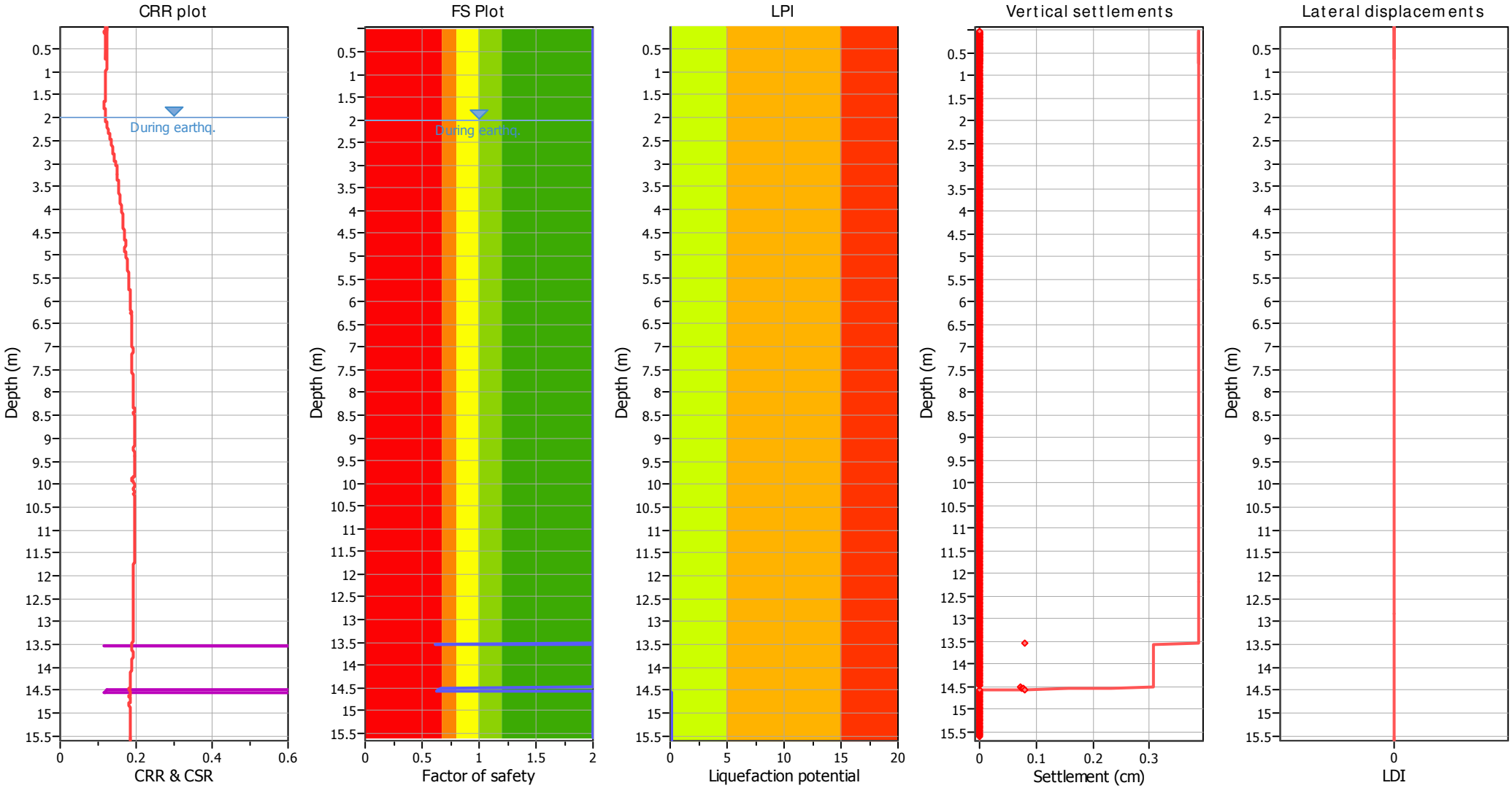
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

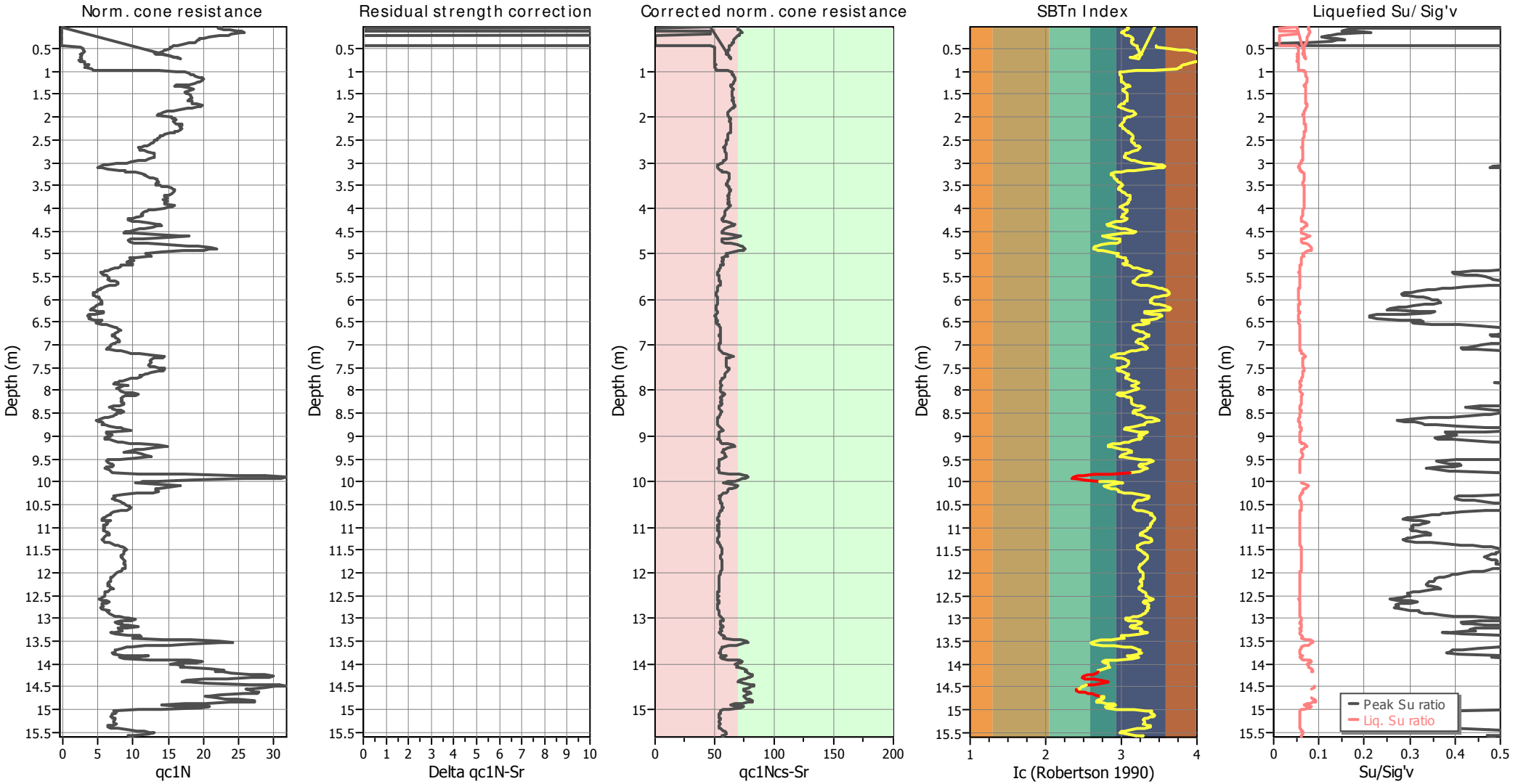
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

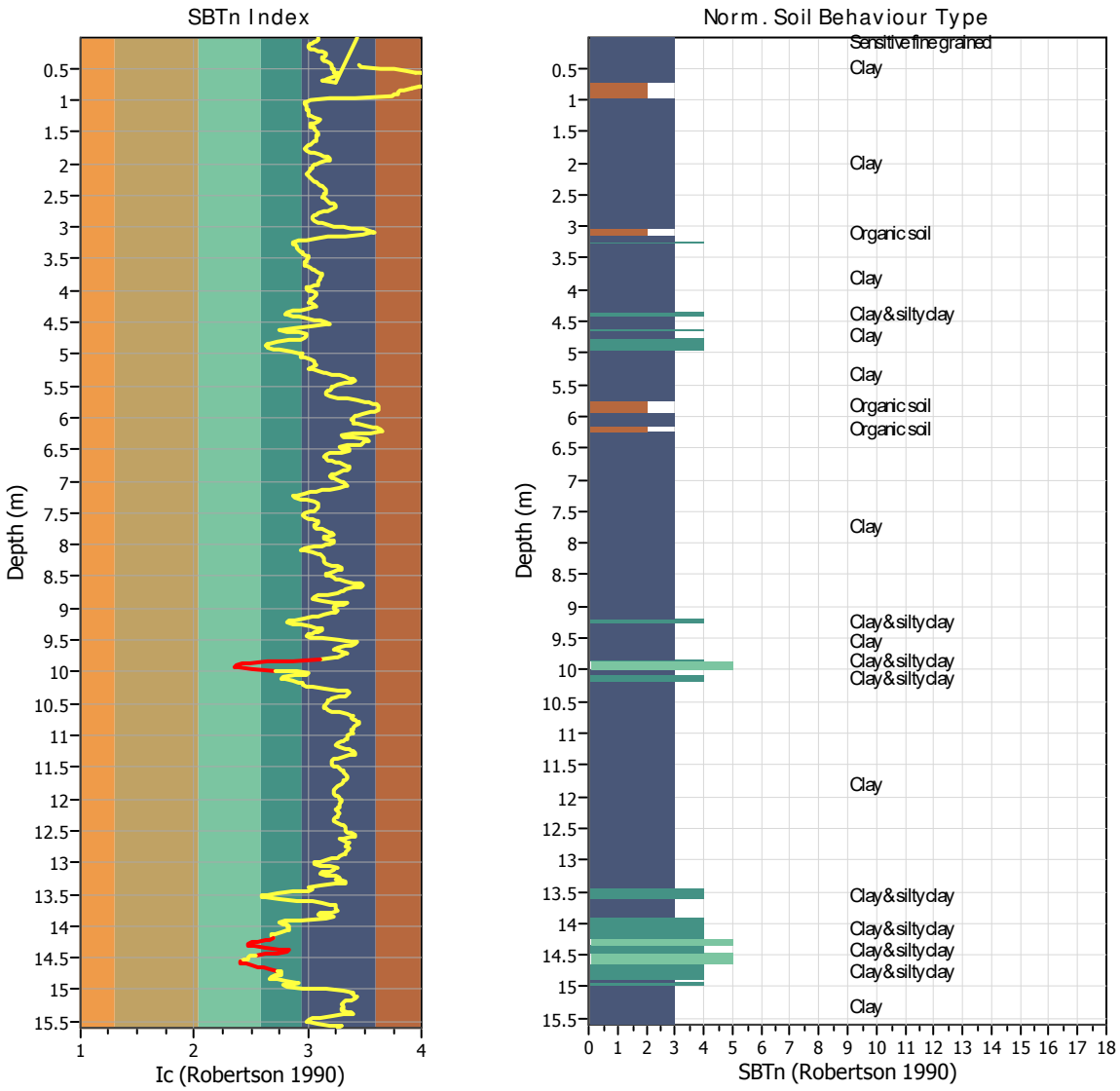
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	816
I_c maximum check value:	3.00	Total points excluded:	33
I_c change ratio value:	0.0100	Exclusion percentage:	4.04%
Minimum number of points in layer:	4	Number of layers detected:	6

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	5	Start depth: 9.82 (m)	4	Clay & silty clay
		End depth: 9.90 (m)	5	Silty sand & sandy silt
Transition layer 2	5	Start depth: 9.92 (m)	5	Silty sand & sandy silt
		End depth: 10.00 (m)	3	Clay
Transition layer 3	5	Start depth: 14.21 (m)	4	Clay & silty clay
		End depth: 14.28 (m)	5	Silty sand & sandy silt
Transition layer 4	5	Start depth: 14.30 (m)	5	Silty sand & sandy silt
		End depth: 14.38 (m)	4	Clay & silty clay
Transition layer 5	5	Start depth: 14.40 (m)	4	Clay & silty clay
		End depth: 14.48 (m)	5	Silty sand & sandy silt
Transition layer 6	8	Start depth: 14.58 (m)	5	Silty sand & sandy silt
		End depth: 14.72 (m)	4	Clay & silty clay

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	1.35	140.39	17.85	64.26	18.80
2	0.04	1.31	144.40	13.14	64.94	18.82
3	0.07	1.36	144.43	10.85	63.95	18.84
4	0.08	1.42	147.30	10.79	62.53	18.86
5	0.10	1.47	149.19	11.04	61.31	18.89
6	0.12	1.51	149.35	11.47	60.07	18.89
7	0.14	1.54	145.53	11.59	58.98	18.86
8	0.16	1.51	134.71	9.24	59.34	18.83
9	0.19	1.43	140.77	4.46	60.45	18.80
10	0.20	1.40	140.16	2.11	62.83	18.81
11	0.22	1.32	142.70	0.50	65.10	18.80
12	0.24	1.24	144.50	-0.93	67.68	18.79
13	0.26	1.19	143.71	-1.86	69.50	18.76
14	0.28	1.16	138.27	-2.48	69.84	18.71
15	0.30	1.15	130.20	-1.55	69.39	18.65
16	0.32	1.15	124.92	-1.61	68.55	18.59
17	0.34	1.13	118.07	-1.92	67.84	18.52
18	0.36	1.12	111.24	-2.42	67.68	18.45
19	0.38	1.07	106.11	-2.98	68.36	18.39
20	0.40	1.02	104.67	-3.47	70.11	18.35
21	0.42	0.97	104.02	-4.09	71.94	18.32
22	0.44	0.94	103.02	-4.46	73.46	18.30
23	0.46	0.92	102.41	-4.77	74.04	18.27
24	0.48	0.92	99.56	-4.90	74.25	18.25
25	0.50	0.91	98.21	-5.08	74.43	18.22
26	0.52	0.88	95.19	-5.15	74.70	18.18
27	0.54	0.87	92.02	-5.27	75.10	18.14
28	0.56	0.85	90.67	-5.33	75.81	18.11
29	0.58	0.82	90.00	-5.70	77.47	18.09
30	0.60	0.77	89.53	-5.33	78.59	18.07
31	0.62	0.79	89.14	-4.65	78.01	18.07
32	0.64	0.84	88.15	-3.72	74.93	18.07
33	0.66	0.91	85.68	-2.17	71.87	18.07
34	0.68	0.94	84.89	-1.24	69.09	18.06
35	0.70	0.97	82.04	-0.31	67.11	18.05
36	0.72	1.00	80.11	0.56	75.95	17.42
37	0.02	-0.02	-0.42	147.18	92.74	16.34
38	0.04	-0.02	-0.39	147.12	N/A	21.58
39	0.06	-0.01	-0.33	146.25	N/A	21.58
40	0.08	-0.01	-0.09	146.31	N/A	21.58
41	0.10	-0.02	-0.30	145.44	N/A	21.58
42	0.12	-0.02	0.38	144.95	100.00	13.73
43	0.14	-0.01	0.41	144.45	100.00	13.73
44	0.16	-0.01	0.50	144.20	100.00	13.73
45	0.18	-0.01	0.00	143.65	100.00	13.73
46	0.20	-0.02	-0.29	143.27	N/A	21.58
47	0.22	-0.02	-0.09	142.84	N/A	21.58
48	0.24	-0.01	-0.38	142.47	N/A	21.58

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.26	-0.02	-0.44	142.10	N/A	21.58
50	0.28	-0.01	-0.41	141.79	N/A	21.58
51	0.30	-0.01	-0.41	141.35	N/A	21.58
52	0.32	-0.01	-0.50	141.04	N/A	21.58
53	0.34	-0.02	-0.38	140.67	N/A	21.58
54	0.36	-0.01	-0.35	140.30	N/A	21.58
55	0.38	-0.02	-0.41	139.93	N/A	21.58
56	0.40	-0.02	-0.41	139.62	N/A	21.58
57	0.42	-0.02	-0.38	139.24	N/A	21.58
58	0.44	-0.01	-0.40	138.93	94.61	13.73
59	0.46	0.15	1.82	469.25	95.04	14.00
60	0.48	0.16	11.67	499.69	95.59	15.47
61	0.50	0.18	27.34	457.35	100.00	16.29
62	0.52	0.17	44.46	408.12	100.00	16.78
63	0.54	0.18	56.18	370.06	100.00	17.12
64	0.56	0.18	72.26	335.59	100.00	17.36
65	0.58	0.17	86.85	323.81	100.00	17.56
66	0.60	0.18	96.32	315.62	100.00	17.64
67	0.62	0.15	95.41	311.84	100.00	17.66
68	0.64	0.16	94.06	303.16	100.00	17.63
69	0.66	0.16	93.94	290.14	100.00	17.62
70	0.68	0.14	93.68	289.09	100.00	17.61
71	0.70	0.15	91.43	286.79	100.00	17.58
72	0.72	0.16	88.52	284.25	100.00	17.56
73	0.74	0.17	86.27	278.98	100.00	17.51
74	0.76	0.14	83.25	273.22	100.00	17.46
75	0.78	0.15	77.51	272.47	100.00	17.40
76	0.80	0.19	70.86	291.13	100.00	17.30
77	0.82	0.19	58.90	288.96	100.00	17.17
78	0.84	0.18	51.52	290.02	100.00	17.07
79	0.86	0.22	52.98	311.16	100.00	17.05
80	0.88	0.21	54.39	316.12	100.00	16.99
81	0.90	0.19	43.34	302.23	100.00	16.91
82	0.92	0.20	43.87	302.98	100.00	16.92
83	0.94	0.25	53.74	318.54	100.00	17.08
84	0.96	0.26	58.67	332.11	91.59	17.46
85	0.98	0.82	69.30	591.01	72.41	17.69
86	1.00	0.96	66.37	567.45	59.99	17.86
87	1.02	1.04	68.89	493.18	57.15	17.90
88	1.04	1.07	70.71	470.86	56.68	17.95
89	1.06	1.08	74.63	451.33	56.92	18.01
90	1.08	1.11	79.23	430.75	57.60	18.09
91	1.10	1.12	84.21	420.40	57.91	18.16
92	1.12	1.16	88.29	412.59	58.18	18.23
93	1.14	1.19	92.85	395.10	58.22	18.27
94	1.16	1.19	93.12	386.79	58.35	18.29
95	1.18	1.18	92.47	380.04	58.36	18.29
96	1.20	1.19	92.21	373.22	58.63	18.27

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.22	1.15	90.56	365.59	58.91	18.25
98	1.24	1.14	88.74	361.13	59.45	18.23
99	1.26	1.12	88.95	357.04	60.48	18.22
100	1.28	1.07	90.03	349.91	63.00	18.21
101	1.30	0.96	91.49	341.48	65.51	18.19
102	1.32	0.95	90.05	339.24	66.47	18.18
103	1.34	1.00	89.58	340.05	64.99	18.20
104	1.36	1.07	91.45	343.34	62.67	18.20
105	1.38	1.10	87.06	345.82	60.60	18.18
106	1.40	1.11	80.78	344.51	59.74	18.13
107	1.42	1.07	80.87	340.67	60.34	18.10
108	1.44	1.04	83.85	338.62	61.84	18.13
109	1.46	1.04	87.90	339.37	62.97	18.17
110	1.48	1.05	90.62	339.18	63.66	18.22
111	1.50	1.06	95.54	339.31	64.04	18.28
112	1.52	1.08	100.34	339.80	64.36	18.33
113	1.54	1.08	101.33	339.06	64.42	18.35
114	1.56	1.08	100.13	338.31	64.02	18.33
115	1.58	1.09	95.99	337.82	63.91	18.31
116	1.60	1.07	96.64	335.96	63.90	18.29
117	1.63	1.06	95.96	334.35	63.87	18.28
118	1.64	1.08	93.38	336.08	63.23	18.26
119	1.66	1.09	92.23	336.08	62.29	18.24
120	1.68	1.09	89.53	335.83	61.69	18.22
121	1.70	1.10	88.24	335.52	60.58	18.20
122	1.72	1.14	85.37	336.58	58.84	18.16
123	1.74	1.18	80.21	338.87	57.16	18.12
124	1.76	1.17	77.83	338.19	56.45	18.08
125	1.78	1.14	77.10	337.01	56.99	18.06
126	1.80	1.10	76.19	335.15	58.15	18.04
127	1.82	1.06	75.98	333.29	60.02	18.02
128	1.84	1.00	77.79	327.84	62.64	18.02
129	1.86	0.94	80.19	322.88	65.98	18.03
130	1.88	0.88	82.53	318.35	68.87	18.02
131	1.90	0.85	80.28	240.73	71.06	18.00
132	1.92	0.83	79.07	223.12	72.46	17.97
133	1.94	0.81	79.25	222.07	72.55	17.92
134	1.96	0.80	70.77	243.09	69.68	17.86
135	1.98	0.91	66.11	237.76	66.25	17.80
136	2.01	0.92	65.41	237.14	63.63	17.79
137	2.02	0.93	65.35	235.46	62.64	17.77
138	2.04	0.94	62.24	237.26	61.51	17.74
139	2.06	0.96	60.13	238.31	60.75	17.71
140	2.08	0.94	60.31	237.38	60.55	17.70
141	2.10	0.94	60.33	239.74	60.63	17.71
142	2.12	0.96	60.95	241.10	60.18	17.72
143	2.14	0.98	61.53	241.91	58.87	17.73
144	2.16	1.03	60.04	246.62	57.84	17.74

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.18	1.04	61.24	245.94	57.82	17.77
146	2.20	1.01	65.34	243.40	58.77	17.83
147	2.22	1.04	69.65	244.95	59.77	17.89
148	2.24	1.04	71.99	245.88	60.21	17.95
149	2.26	1.05	75.51	245.63	60.88	18.00
150	2.28	1.05	79.31	246.68	62.08	18.06
151	2.30	1.03	83.71	247.68	63.62	18.10
152	2.32	1.00	84.99	246.31	64.68	18.11
153	2.34	1.00	82.91	246.00	65.52	18.09
154	2.36	0.97	82.91	243.83	66.76	18.08
155	2.38	0.92	84.90	242.41	68.23	18.08
156	2.40	0.91	83.46	242.59	69.64	18.06
157	2.42	0.89	82.67	242.03	69.80	18.04
158	2.44	0.89	80.24	243.96	70.01	18.01
159	2.46	0.87	78.01	244.70	69.44	17.96
160	2.48	0.87	74.20	243.71	68.63	17.91
161	2.50	0.88	70.30	244.64	68.06	17.86
162	2.52	0.85	68.66	243.58	67.98	17.83
163	2.54	0.85	69.15	244.20	68.49	17.82
164	2.56	0.85	69.36	245.75	69.32	17.83
165	2.58	0.82	71.03	245.82	70.21	17.83
166	2.60	0.81	71.17	245.51	71.63	17.84
167	2.62	0.79	72.05	244.33	73.05	17.84
168	2.64	0.76	72.46	243.03	74.78	17.83
169	2.66	0.74	72.31	241.29	76.33	17.81
170	2.68	0.71	71.14	239.31	76.58	17.79
171	2.70	0.73	68.20	241.10	76.13	17.76
172	2.72	0.73	66.97	242.65	74.00	17.73
173	2.74	0.77	64.10	246.56	71.76	17.71
174	2.76	0.81	62.66	247.99	68.30	17.67
175	2.78	0.86	58.41	250.34	65.44	17.62
176	2.80	0.87	54.19	248.48	63.13	17.56
177	2.82	0.87	52.58	247.92	61.92	17.52
178	2.84	0.88	51.64	247.06	61.48	17.51
179	2.86	0.88	52.29	250.90	61.22	17.51
180	2.88	0.88	52.08	251.83	61.64	17.52
181	2.90	0.87	53.37	247.68	62.85	17.53
182	2.92	0.83	54.66	242.65	64.67	17.53
183	2.94	0.79	53.95	245.07	67.47	17.51
184	2.96	0.73	54.54	239.18	70.98	17.49
185	2.98	0.66	54.48	232.92	75.57	17.46
186	3.00	0.61	55.45	226.78	81.54	17.43
187	3.02	0.52	55.48	218.23	88.67	17.37
188	3.04	0.44	52.93	213.08	96.88	17.28
189	3.06	0.39	50.87	207.94	100.00	17.18
190	3.09	0.36	47.77	202.91	100.00	17.09
191	3.10	0.34	44.37	203.47	100.00	16.97
192	3.12	0.38	37.92	204.71	97.86	16.85

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.14	0.43	32.18	211.35	83.69	16.71
194	3.16	0.55	25.88	222.94	71.55	16.56
195	3.18	0.62	22.66	228.52	63.64	16.44
196	3.21	0.62	21.43	224.92	57.98	16.33
197	3.22	0.71	17.94	232.92	53.54	16.27
198	3.24	0.77	17.82	242.59	49.97	16.30
199	3.26	0.82	21.37	243.09	50.38	16.46
200	3.28	0.80	25.94	241.41	51.50	16.64
201	3.30	0.84	27.70	244.89	52.56	16.77
202	3.32	0.86	30.01	246.37	52.30	16.87
203	3.34	0.90	32.59	247.49	52.46	17.00
204	3.36	0.94	37.11	249.47	53.19	17.13
205	3.38	0.94	41.33	248.85	54.27	17.25
206	3.40	0.95	43.91	248.42	55.11	17.32
207	3.42	0.96	44.82	248.36	56.00	17.39
208	3.44	0.95	48.77	247.37	57.35	17.46
209	3.46	0.93	52.38	245.07	58.83	17.52
210	3.48	0.94	54.11	245.44	59.29	17.58
211	3.50	0.98	55.81	248.17	58.98	17.63
212	3.52	1.01	58.74	249.10	58.17	17.69
213	3.54	1.06	61.34	254.06	57.22	17.77
214	3.56	1.12	64.27	258.40	56.49	17.82
215	3.58	1.12	66.24	258.09	56.28	17.88
216	3.60	1.14	69.43	258.83	57.00	17.95
217	3.62	1.15	76.08	257.66	58.27	18.04
218	3.64	1.14	82.06	257.66	59.66	18.11
219	3.66	1.14	84.96	256.23	60.82	18.16
220	3.68	1.13	86.80	254.49	62.15	18.19
221	3.70	1.09	90.09	251.27	63.94	18.22
222	3.72	1.06	93.66	249.91	65.91	18.26
223	3.74	1.06	98.41	248.92	67.04	18.29
224	3.76	1.06	98.76	249.47	66.91	18.30
225	3.78	1.08	96.29	251.15	66.55	18.29
226	3.80	1.06	94.97	251.27	66.21	18.27
227	3.82	1.05	93.13	250.65	65.70	18.24
228	3.84	1.08	90.28	252.51	65.28	18.21
229	3.86	1.06	88.79	249.97	64.55	18.20
230	3.88	1.08	88.87	251.70	64.47	18.19
231	3.90	1.07	87.61	252.45	64.27	18.18
232	3.92	1.07	87.58	252.45	61.83	18.13
233	3.94	1.17	75.33	258.34	59.82	18.08
234	3.96	1.14	73.77	253.19	57.54	17.99
235	3.98	1.12	69.53	251.52	58.04	17.93
236	4.00	1.07	66.80	248.48	59.18	17.85
237	4.02	0.97	61.97	237.63	61.30	17.76
238	4.04	0.91	59.45	231.06	63.21	17.68
239	4.06	0.89	57.81	229.20	63.81	17.61
240	4.08	0.87	52.97	228.46	63.58	17.53

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.10	0.85	49.28	225.98	62.66	17.43
242	4.12	0.85	44.74	226.53	61.76	17.32
243	4.14	0.84	41.07	225.29	60.07	17.22
244	4.16	0.86	37.91	225.91	59.52	17.13
245	4.18	0.80	35.51	221.45	59.07	17.04
246	4.20	0.80	33.54	219.65	60.56	16.97
247	4.22	0.74	33.43	214.38	61.83	16.91
248	4.24	0.70	31.38	211.47	63.54	16.86
249	4.26	0.69	30.50	209.49	62.44	16.79
250	4.28	0.74	27.86	211.90	59.12	16.73
251	4.30	0.81	25.61	218.23	54.05	16.69
252	4.32	0.91	25.22	227.77	49.74	16.70
253	4.34	1.01	25.93	235.71	47.07	16.76
254	4.36	1.05	27.34	238.93	46.19	16.84
255	4.38	1.06	29.53	240.86	47.35	16.93
256	4.40	1.02	32.76	235.65	49.74	17.02
257	4.42	0.97	35.95	230.94	53.66	17.12
258	4.44	0.88	39.91	222.26	57.91	17.19
259	4.46	0.83	42.14	217.23	62.71	17.23
260	4.48	0.77	43.92	211.90	66.60	17.25
261	4.50	0.72	44.01	203.66	70.36	17.22
262	4.52	0.67	42.52	197.09	72.27	17.17
263	4.54	0.67	40.12	195.41	69.69	17.12
264	4.56	0.78	37.37	213.45	61.26	17.11
265	4.58	1.02	35.55	237.14	50.61	17.12
266	4.61	1.31	33.38	257.66	44.06	17.17
267	4.62	1.40	35.81	261.13	42.87	17.20
268	4.64	1.17	36.14	243.83	47.01	17.16
269	4.66	0.88	34.12	223.25	52.99	16.94
270	4.68	0.75	23.86	215.81	57.52	16.68
271	4.70	0.71	20.96	213.45	57.33	16.44
272	4.72	0.74	20.99	214.88	57.61	16.43
273	4.74	0.73	23.34	213.64	57.08	16.49
274	4.76	0.78	23.72	216.92	54.63	16.59
275	4.78	0.93	25.18	229.82	48.26	16.65
276	4.80	1.18	23.51	243.71	42.50	16.79
277	4.82	1.39	28.03	262.93	38.88	16.96
278	4.84	1.51	33.10	277.06	37.62	17.20
279	4.86	1.66	39.10	264.17	36.94	17.36
280	4.88	1.74	40.22	198.70	37.28	17.45
281	4.90	1.65	42.07	146.19	37.72	17.43
282	4.92	1.58	37.34	187.29	40.22	17.39
283	4.94	1.36	39.37	160.82	43.55	17.28
284	4.96	1.11	35.62	159.45	49.17	17.17
285	4.98	0.94	33.33	161.93	53.43	17.06
286	5.00	0.93	33.68	179.29	55.31	17.04
287	5.02	0.97	35.41	195.10	54.71	17.06
288	5.04	0.99	34.47	195.29	54.26	17.07

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.06	0.96	33.57	184.00	56.30	17.02
290	5.08	0.82	33.57	174.64	59.89	16.97
291	5.10	0.76	32.54	178.24	62.73	16.91
292	5.12	0.78	30.64	180.84	62.39	16.86
293	5.14	0.80	29.79	181.77	62.19	16.83
294	5.16	0.76	30.49	165.41	63.28	16.82
295	5.18	0.73	30.43	175.95	63.23	16.79
296	5.20	0.79	27.73	177.74	61.44	16.72
297	5.22	0.78	24.72	175.88	59.41	16.66
298	5.24	0.79	25.74	169.93	61.72	16.61
299	5.26	0.65	25.62	167.45	64.66	16.59
300	5.28	0.66	24.86	167.76	68.40	16.54
301	5.30	0.62	24.51	164.66	69.91	16.52
302	5.32	0.59	25.04	162.49	73.78	16.55
303	5.34	0.55	27.85	159.02	78.83	16.60
304	5.36	0.51	29.84	156.97	83.28	16.60
305	5.38	0.49	26.71	156.48	86.65	16.55
306	5.40	0.46	26.21	155.55	89.62	16.48
307	5.42	0.43	26.27	152.51	90.68	16.43
308	5.44	0.45	23.81	152.51	88.45	16.35
309	5.46	0.47	20.91	155.36	83.05	16.25
310	5.48	0.50	19.27	160.82	78.14	16.16
311	5.51	0.52	18.19	162.37	74.95	16.12
312	5.52	0.54	18.16	159.14	73.50	16.10
313	5.54	0.53	18.16	159.89	73.55	16.10
314	5.56	0.52	17.86	159.52	72.66	16.09
315	5.58	0.56	17.69	162.18	71.01	16.14
316	5.60	0.60	19.77	162.74	69.33	16.26
317	5.62	0.64	22.79	141.79	69.30	16.41
318	5.64	0.65	24.90	141.04	70.03	16.52
319	5.66	0.65	26.31	139.80	72.58	16.60
320	5.68	0.60	28.45	132.05	77.51	16.67
321	5.70	0.54	31.49	128.95	85.09	16.74
322	5.72	0.49	34.81	124.86	93.07	16.80
323	5.74	0.46	36.21	124.67	100.00	16.85
324	5.76	0.44	38.35	125.42	100.00	16.88
325	5.78	0.44	39.17	126.22	100.00	16.90
326	5.80	0.41	39.06	125.23	100.00	16.87
327	5.82	0.40	36.57	125.17	100.00	16.78
328	5.84	0.38	32.55	123.31	100.00	16.66
329	5.86	0.37	29.65	122.32	100.00	16.54
330	5.88	0.37	27.46	122.26	100.00	16.44
331	5.90	0.36	25.85	121.39	100.00	16.35
332	5.92	0.38	22.73	127.15	100.00	16.26
333	5.95	0.40	21.06	124.80	97.50	16.17
334	5.96	0.42	19.89	126.16	93.51	16.11
335	5.98	0.42	18.80	122.32	90.57	16.09
336	6.00	0.44	19.12	122.38	89.80	16.10

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.02	0.44	20.00	123.25	88.71	16.16
338	6.04	0.47	21.59	120.64	89.18	16.22
339	6.06	0.46	21.79	114.01	89.15	16.24
340	6.08	0.46	21.23	102.67	90.26	16.27
341	6.10	0.46	23.17	94.42	93.20	16.33
342	6.12	0.43	25.95	105.27	100.00	16.42
343	6.14	0.39	28.50	99.32	100.00	16.49
344	6.16	0.39	29.44	98.20	100.00	16.50
345	6.18	0.38	27.42	102.42	100.00	16.45
346	6.20	0.35	26.45	102.98	100.00	16.35
347	6.22	0.33	23.38	98.02	100.00	16.21
348	6.24	0.37	18.89	93.74	100.00	16.02
349	6.26	0.42	15.00	97.21	89.47	15.84
350	6.28	0.48	13.21	104.46	81.16	15.73
351	6.30	0.48	13.33	105.70	81.65	15.66
352	6.32	0.38	12.74	101.74	90.30	15.56
353	6.34	0.31	11.72	97.52	100.00	15.37
354	6.36	0.30	9.40	87.29	100.00	15.20
355	6.38	0.33	8.38	90.64	100.00	15.06
356	6.40	0.31	8.32	94.61	98.04	15.04
357	6.42	0.31	8.90	90.64	95.17	15.08
358	6.44	0.38	8.99	80.53	85.02	15.18
359	6.46	0.48	9.40	97.15	79.17	15.33
360	6.48	0.45	11.40	108.68	80.56	15.48
361	6.50	0.40	12.98	106.01	86.52	15.56
362	6.52	0.40	12.75	91.88	86.72	15.62
363	6.54	0.47	12.98	95.41	80.32	15.65
364	6.56	0.53	12.95	100.25	73.18	15.73
365	6.58	0.59	13.69	99.44	69.88	15.89
366	6.60	0.63	17.55	101.92	68.86	16.09
367	6.62	0.66	20.05	105.08	69.63	16.30
368	6.64	0.67	23.15	106.01	70.09	16.46
369	6.67	0.70	25.70	105.58	71.84	16.62
370	6.68	0.69	30.01	105.83	74.06	16.75
371	6.70	0.67	32.44	109.36	76.91	16.84
372	6.72	0.67	34.05	109.42	79.61	16.89
373	6.74	0.64	34.99	105.58	81.93	16.93
374	6.76	0.63	36.87	106.51	84.80	16.96
375	6.78	0.61	38.01	107.32	86.73	16.99
376	6.80	0.60	38.45	107.50	86.31	17.00
377	6.82	0.65	37.07	108.62	85.00	16.99
378	6.84	0.64	36.40	109.73	81.71	16.96
379	6.86	0.68	33.97	110.48	79.45	16.90
380	6.88	0.68	31.16	111.41	75.96	16.80
381	6.90	0.70	27.56	114.88	73.81	16.71
382	6.92	0.70	26.80	114.69	72.89	16.64
383	6.94	0.67	25.84	113.89	73.56	16.60
384	6.96	0.66	25.54	112.34	75.78	16.58

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	6.98	0.62	26.42	111.53	78.26	16.59
386	7.00	0.61	27.15	111.41	80.74	16.59
387	7.02	0.59	26.63	111.16	82.55	16.57
388	7.05	0.57	25.95	109.98	83.81	16.54
389	7.06	0.56	25.31	107.75	84.92	16.50
390	7.08	0.55	24.96	106.76	83.84	16.47
391	7.10	0.59	23.93	107.69	79.09	16.45
392	7.12	0.67	22.03	116.86	72.72	16.44
393	7.14	0.73	22.23	121.64	67.38	16.48
394	7.16	0.80	24.08	121.26	64.13	16.58
395	7.18	0.87	26.25	119.78	60.62	16.69
396	7.20	0.98	27.16	134.04	56.23	16.80
397	7.22	1.12	28.80	144.33	51.78	16.94
398	7.24	1.29	32.55	147.24	50.24	17.11
399	7.26	1.28	38.32	159.64	50.90	17.28
400	7.28	1.26	43.24	157.59	54.38	17.41
401	7.30	1.16	47.96	147.99	58.24	17.52
402	7.32	1.13	53.91	154.68	62.05	17.62
403	7.34	1.11	57.63	158.34	64.46	17.70
404	7.36	1.10	61.15	156.97	65.16	17.74
405	7.38	1.12	59.12	161.25	65.29	17.75
406	7.40	1.12	59.21	162.37	64.68	17.72
407	7.42	1.12	57.34	161.62	64.51	17.69
408	7.44	1.10	54.52	160.57	63.82	17.64
409	7.46	1.11	52.30	161.00	62.45	17.60
410	7.48	1.17	51.04	162.86	60.01	17.58
411	7.50	1.24	48.81	168.51	57.14	17.56
412	7.52	1.31	48.25	170.86	55.24	17.56
413	7.54	1.30	48.08	171.54	54.92	17.57
414	7.56	1.29	50.48	171.30	56.23	17.59
415	7.58	1.23	51.56	169.13	58.72	17.61
416	7.60	1.15	52.94	165.34	61.37	17.60
417	7.62	1.09	51.47	166.34	63.50	17.56
418	7.64	1.06	49.36	164.66	64.61	17.51
419	7.66	1.03	47.31	165.41	64.82	17.42
420	7.68	1.00	41.66	165.65	63.98	17.30
421	7.70	1.01	37.00	167.02	62.63	17.14
422	7.72	0.95	31.08	166.03	62.43	16.98
423	7.74	0.88	28.85	161.13	63.78	16.83
424	7.76	0.83	27.33	156.48	66.80	16.76
425	7.78	0.77	27.68	154.93	69.54	16.71
426	7.80	0.74	26.92	154.12	71.97	16.67
427	7.82	0.71	25.77	152.63	73.92	16.62
428	7.84	0.67	25.63	151.15	75.21	16.58
429	7.86	0.67	24.75	151.02	71.73	16.62
430	7.88	0.85	26.49	157.78	69.27	16.67
431	7.90	0.80	27.61	154.93	68.32	16.72
432	7.92	0.75	27.96	152.94	72.44	16.73

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	7.94	0.70	28.87	149.66	74.65	16.72
434	7.96	0.72	27.76	151.95	74.72	16.70
435	7.98	0.74	26.82	153.81	72.54	16.64
436	8.00	0.74	24.03	155.11	70.20	16.56
437	8.02	0.76	22.04	155.49	66.74	16.47
438	8.04	0.82	20.26	159.39	61.82	16.41
439	8.06	0.92	19.29	163.92	56.53	16.38
440	8.08	1.00	18.73	168.07	54.66	16.41
441	8.10	0.95	21.14	161.75	56.65	16.44
442	8.12	0.83	21.25	155.92	60.90	16.45
443	8.14	0.79	20.64	154.62	64.29	16.42
444	8.16	0.79	21.28	155.73	66.41	16.46
445	8.18	0.77	23.66	153.32	67.73	16.53
446	8.20	0.79	25.27	156.04	68.46	16.59
447	8.22	0.80	24.95	156.91	68.71	16.62
448	8.24	0.77	25.09	155.86	68.69	16.61
449	8.26	0.79	24.51	155.42	68.50	16.61
450	8.28	0.81	25.39	156.17	68.43	16.65
451	8.30	0.80	27.41	154.74	69.75	16.68
452	8.32	0.75	26.85	155.86	73.46	16.67
453	8.34	0.67	26.15	149.41	78.59	16.62
454	8.36	0.61	26.32	143.71	81.45	16.58
455	8.38	0.65	25.27	151.58	81.46	16.57
456	8.40	0.67	25.74	153.19	78.17	16.61
457	8.42	0.73	27.23	156.29	75.27	16.66
458	8.44	0.78	27.53	159.21	71.60	16.68
459	8.46	0.81	25.21	155.30	69.69	16.63
460	8.48	0.77	23.25	146.50	69.84	16.55
461	8.50	0.73	23.31	148.17	72.13	16.55
462	8.52	0.73	25.74	149.66	74.63	16.58
463	8.54	0.70	25.94	149.85	76.38	16.59
464	8.56	0.68	24.39	149.10	79.64	16.53
465	8.58	0.60	23.51	145.07	83.95	16.47
466	8.60	0.56	23.98	142.22	90.17	16.40
467	8.62	0.50	22.46	139.43	95.17	16.32
468	8.64	0.47	20.26	132.80	98.02	16.16
469	8.66	0.46	16.92	127.53	96.48	16.01
470	8.68	0.48	15.34	134.72	90.04	15.88
471	8.70	0.53	13.73	144.95	84.20	15.79
472	8.72	0.54	12.99	145.44	81.62	15.79
473	8.74	0.54	14.63	142.22	81.14	15.83
474	8.76	0.56	15.16	149.72	77.88	15.87
475	8.78	0.64	13.64	155.49	71.68	15.91
476	8.80	0.72	14.43	160.69	65.34	15.94
477	8.82	0.80	14.78	161.69	62.04	16.05
478	8.84	0.83	16.75	167.33	60.90	16.15
479	8.86	0.84	17.83	167.39	61.38	16.39
480	8.88	0.94	25.23	161.25	67.73	16.54

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	8.90	0.66	26.55	144.89	74.98	16.57
482	8.92	0.59	22.54	145.51	84.50	16.45
483	8.94	0.60	21.54	147.12	82.18	16.36
484	8.96	0.67	20.72	150.59	79.52	16.27
485	8.98	0.63	17.70	149.54	75.80	16.17
486	9.00	0.65	15.91	151.95	75.19	16.02
487	9.02	0.62	14.21	149.23	75.21	15.91
488	9.04	0.58	13.92	147.06	77.81	15.89
489	9.06	0.57	15.59	148.23	77.05	15.90
490	9.08	0.64	14.33	153.44	73.27	15.93
491	9.10	0.70	14.21	155.24	68.34	15.97
492	9.12	0.76	16.03	158.65	64.79	16.05
493	9.14	0.82	16.21	161.62	61.23	16.15
494	9.16	0.92	17.17	165.84	56.64	16.27
495	9.18	1.07	19.11	175.26	51.31	16.47
496	9.20	1.32	23.21	182.52	47.69	16.73
497	9.22	1.45	28.22	173.65	47.36	17.00
498	9.24	1.41	35.40	161.56	49.94	17.14
499	9.26	1.26	35.08	147.68	54.55	17.17
500	9.28	1.12	34.14	142.59	59.56	17.13
501	9.30	1.01	35.14	138.81	63.96	17.07
502	9.32	0.95	33.32	136.39	67.95	17.00
503	9.34	0.85	30.68	136.02	67.62	16.96
504	9.36	1.00	32.15	146.81	64.90	16.98
505	9.38	1.10	33.29	146.93	62.27	17.08
506	9.40	1.09	36.83	143.09	60.65	17.14
507	9.42	1.16	35.54	146.31	58.85	17.16
508	9.44	1.24	34.11	149.04	57.49	17.18
509	9.46	1.20	37.13	145.07	60.11	17.21
510	9.48	1.02	40.58	133.04	67.72	17.20
511	9.50	0.80	38.03	125.73	78.91	17.10
512	9.52	0.64	34.31	121.33	88.75	16.94
513	9.54	0.62	32.11	125.48	92.61	16.80
514	9.56	0.63	28.98	128.83	91.59	16.72
515	9.58	0.62	27.75	129.14	87.48	16.63
516	9.60	0.68	24.79	132.11	83.05	16.53
517	9.62	0.70	21.04	134.10	77.57	16.38
518	9.64	0.71	18.16	135.09	74.95	16.27
519	9.66	0.71	18.72	134.41	76.41	16.22
520	9.68	0.62	18.84	131.12	80.83	16.22
521	9.70	0.59	19.31	130.50	84.97	16.20
522	9.72	0.59	18.84	130.94	83.92	16.20
523	9.74	0.65	18.84	136.45	80.29	16.20
524	9.76	0.68	18.52	139.55	77.46	16.23
525	9.78	0.69	19.31	139.80	76.34	16.25
526	9.80	0.70	19.22	141.04	66.52	16.30
527	9.82	1.07	18.05	158.15	49.79	16.42
528	9.84	1.72	18.75	185.31	37.24	16.78

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	9.86	2.42	29.95	195.91	30.66	17.15
530	9.88	2.87	35.20	206.39	27.17	17.41
531	9.90	3.18	33.38	206.01	25.01	17.41
532	9.92	3.10	27.43	185.37	24.35	17.19
533	9.94	2.56	19.82	169.19	26.02	16.81
534	9.96	1.86	13.78	150.22	31.29	16.46
535	9.98	1.35	15.48	135.65	41.02	16.42
536	10.00	1.14	22.92	129.20	52.37	16.69
537	10.03	1.10	31.68	130.13	59.40	16.87
538	10.04	1.03	29.57	138.00	57.74	17.01
539	10.06	1.37	32.03	197.58	50.88	17.06
540	10.08	1.69	30.98	157.22	45.38	17.12
541	10.10	1.66	30.22	149.16	43.84	17.09
542	10.12	1.51	28.34	142.41	46.12	17.03
543	10.15	1.37	28.75	131.99	50.05	17.08
544	10.16	1.34	36.34	126.41	53.70	17.19
545	10.18	1.33	39.18	121.64	55.48	17.30
546	10.20	1.36	39.27	117.98	55.90	17.35
547	10.22	1.37	40.82	113.58	57.37	17.40
548	10.24	1.29	45.86	106.39	61.20	17.40
549	10.26	1.08	41.79	100.37	68.29	17.34
550	10.28	0.88	40.11	93.74	77.63	17.20
551	10.30	0.74	38.41	90.39	84.85	17.08
552	10.32	0.73	34.52	94.85	87.34	16.98
553	10.34	0.75	32.93	95.72	86.99	16.91
554	10.36	0.71	32.44	96.03	85.64	16.84
555	10.38	0.74	28.86	97.58	83.42	16.73
556	10.40	0.76	24.20	96.90	79.08	16.62
557	10.42	0.78	23.32	98.64	74.47	16.53
558	10.44	0.85	22.24	100.12	72.27	16.56
559	10.46	0.86	24.87	100.74	71.03	16.63
560	10.48	0.88	27.01	102.42	71.18	16.73
561	10.50	0.91	28.30	103.78	70.44	16.82
562	10.52	0.95	30.23	103.04	69.57	16.88
563	10.54	0.97	30.82	103.16	69.20	16.94
564	10.56	0.98	32.52	104.22	68.93	16.99
565	10.58	1.01	33.75	105.33	69.45	17.03
566	10.60	0.98	34.30	104.96	70.59	17.05
567	10.62	0.94	34.48	104.03	74.13	17.04
568	10.64	0.84	34.92	101.30	79.26	17.00
569	10.66	0.75	33.92	98.95	85.26	16.95
570	10.68	0.71	33.13	97.83	88.89	16.89
571	10.70	0.71	31.87	98.88	89.38	16.84
572	10.72	0.71	30.03	100.19	88.72	16.77
573	10.74	0.69	27.94	99.38	89.75	16.69
574	10.76	0.64	26.22	97.89	91.53	16.58
575	10.78	0.62	23.61	97.89	93.43	16.46
576	10.80	0.60	21.56	98.26	93.68	16.35

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	10.82	0.59	20.39	98.51	94.08	16.28
578	10.84	0.58	19.83	99.75	91.90	16.42
579	10.86	0.70	28.46	123.99	91.08	16.53
580	10.88	0.65	26.49	124.98	89.58	16.62
581	10.91	0.65	24.94	126.97	89.47	16.54
582	10.92	0.66	23.24	128.33	88.45	16.46
583	10.94	0.64	21.72	128.58	88.84	16.38
584	10.96	0.61	20.72	127.59	89.11	16.28
585	10.98	0.61	18.20	128.33	87.56	16.18
586	11.00	0.63	16.53	130.44	85.84	16.08
587	11.02	0.61	16.33	130.32	84.80	16.02
588	11.05	0.62	15.68	130.25	85.23	15.99
589	11.06	0.61	15.27	131.68	83.87	15.97
590	11.08	0.64	15.30	133.17	82.15	15.95
591	11.10	0.66	14.81	133.35	80.27	15.96
592	11.12	0.67	15.19	134.72	78.34	15.96
593	11.14	0.69	14.83	136.52	76.91	15.96
594	11.16	0.70	14.51	136.39	77.12	15.96
595	11.18	0.66	15.22	135.34	79.62	16.00
596	11.20	0.64	16.59	133.97	83.85	16.06
597	11.22	0.62	17.91	132.49	86.91	16.12
598	11.24	0.61	18.15	133.17	88.72	16.13
599	11.26	0.60	17.47	133.35	89.87	16.14
600	11.28	0.60	18.59	132.61	90.87	16.16
601	11.30	0.60	19.35	131.99	90.55	16.21
602	11.32	0.63	19.44	135.59	86.90	16.24
603	11.34	0.70	19.09	139.74	81.82	16.27
604	11.36	0.75	19.67	143.09	77.52	16.35
605	11.38	0.80	21.72	146.13	75.28	16.46
606	11.40	0.84	24.13	148.11	74.37	16.60
607	11.42	0.88	27.12	149.72	74.14	16.74
608	11.44	0.90	29.69	150.96	73.86	16.86
609	11.46	0.94	32.10	152.76	74.51	16.98
610	11.48	0.94	36.46	152.76	75.36	17.11
611	11.50	0.96	40.39	152.32	77.41	17.22
612	11.52	0.93	42.62	152.20	79.12	17.29
613	11.54	0.93	44.99	152.20	80.72	17.34
614	11.56	0.93	46.10	152.57	81.72	17.37
615	11.58	0.92	46.83	152.51	82.13	17.39
616	11.60	0.93	46.83	152.08	83.36	17.40
617	11.62	0.89	47.48	150.34	84.25	17.40
618	11.64	0.90	48.18	150.46	85.30	17.41
619	11.66	0.90	48.15	151.27	85.36	17.42
620	11.68	0.90	48.76	152.01	84.72	17.43
621	11.70	0.93	48.53	154.62	83.90	17.43
622	11.72	0.93	48.26	155.92	82.53	17.44
623	11.74	0.95	48.12	157.35	81.79	17.42
624	11.76	0.95	46.21	157.10	81.02	17.38

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	11.78	0.93	43.25	157.35	80.17	17.31
626	11.80	0.94	40.06	158.83	78.64	17.23
627	11.82	0.95	38.01	159.14	77.14	17.19
628	11.84	0.96	38.36	192.25	76.21	17.17
629	11.86	0.96	37.78	193.92	75.66	17.16
630	11.89	0.97	36.90	194.36	75.35	17.13
631	11.90	0.95	35.23	193.92	75.46	17.09
632	11.92	0.92	34.50	193.18	75.93	17.06
633	11.94	0.93	34.55	192.00	76.86	17.04
634	11.96	0.90	33.94	190.95	77.64	17.00
635	11.98	0.87	31.80	190.02	78.77	16.93
636	12.00	0.84	29.63	188.59	79.94	16.84
637	12.02	0.80	28.22	187.79	80.21	16.76
638	12.04	0.80	25.82	189.21	80.26	16.67
639	12.06	0.78	24.15	189.77	79.59	16.58
640	12.08	0.77	22.57	189.83	79.90	16.49
641	12.10	0.75	21.05	190.70	80.03	16.41
642	12.12	0.74	19.93	192.25	79.69	16.32
643	12.14	0.74	18.32	195.04	78.56	16.25
644	12.16	0.74	17.35	196.22	77.61	16.19
645	12.18	0.73	16.89	196.71	77.26	16.14
646	12.20	0.73	16.51	196.47	78.12	16.12
647	12.22	0.71	16.68	196.03	78.73	16.11
648	12.24	0.71	16.42	197.15	79.00	16.09
649	12.26	0.71	15.89	200.19	78.54	16.07
650	12.28	0.71	15.77	201.80	77.95	16.06
651	12.30	0.72	15.89	203.04	77.06	16.08
652	12.32	0.75	16.27	205.39	75.23	16.11
653	12.34	0.79	16.57	208.00	74.68	16.13
654	12.36	0.76	16.60	206.26	75.82	16.14
655	12.38	0.72	16.95	202.98	78.38	16.11
656	12.40	0.70	16.01	201.86	80.79	16.06
657	12.42	0.66	15.25	199.57	82.25	16.01
658	12.44	0.65	15.07	200.50	83.23	15.97
659	12.46	0.65	14.72	201.67	83.14	15.95
660	12.48	0.66	14.72	199.63	83.32	15.98
661	12.50	0.66	16.19	204.22	83.38	16.03
662	12.52	0.67	16.51	204.77	85.32	16.06
663	12.54	0.62	16.10	200.93	87.45	16.04
664	12.56	0.61	15.84	198.14	91.29	16.01
665	12.58	0.58	16.07	194.79	91.77	16.01
666	12.60	0.62	16.19	190.08	88.35	16.00
667	12.62	0.68	15.02	198.02	82.30	15.98
668	12.64	0.72	14.14	190.76	79.49	15.96
669	12.66	0.69	14.73	186.17	81.62	15.95
670	12.68	0.62	15.05	195.47	85.51	15.92
671	12.70	0.61	14.02	202.98	87.16	15.88
672	12.72	0.63	13.58	205.33	85.69	15.84

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	12.74	0.63	13.20	215.13	84.39	15.80
674	12.76	0.63	12.62	216.31	85.38	15.80
675	12.78	0.61	13.88	212.83	86.75	15.82
676	12.80	0.61	13.91	201.80	85.46	16.00
677	12.82	0.74	18.87	217.67	85.15	16.15
678	12.84	0.69	19.51	192.68	84.13	16.30
679	12.86	0.71	20.39	212.46	84.14	16.31
680	12.88	0.74	19.13	217.73	82.10	16.33
681	12.90	0.75	19.83	222.75	79.96	16.34
682	12.92	0.78	20.45	230.01	77.81	16.38
683	12.94	0.83	20.42	233.54	74.10	16.41
684	12.96	0.90	20.39	243.96	69.54	16.45
685	12.98	1.00	20.92	252.26	66.04	16.52
686	13.00	1.04	22.50	258.46	62.36	16.58
687	13.02	1.16	22.41	221.95	62.18	16.66
688	13.04	1.09	25.20	190.14	65.68	16.74
689	13.06	0.93	28.57	172.97	72.75	16.78
690	13.08	0.85	27.34	181.59	77.95	16.79
691	13.10	0.88	27.75	207.38	77.18	16.77
692	13.12	0.94	27.25	216.80	75.65	16.82
693	13.14	0.94	29.77	213.02	72.62	16.86
694	13.16	1.04	29.68	224.49	67.71	16.88
695	13.18	1.20	26.16	232.30	66.30	16.89
696	13.20	1.03	29.91	191.13	69.90	16.93
697	13.22	0.90	34.04	174.58	77.14	16.98
698	13.24	0.91	33.11	213.45	79.05	17.00
699	13.26	0.96	32.11	222.63	77.29	16.98
700	13.28	0.95	31.96	221.64	78.84	16.96
701	13.30	0.83	32.34	213.27	83.20	16.93
702	13.32	0.78	31.20	214.45	84.35	16.84
703	13.34	0.85	25.84	227.22	76.68	16.74
704	13.36	1.05	23.20	251.89	65.69	16.68
705	13.38	1.23	23.11	268.13	59.11	16.70
706	13.40	1.27	24.11	233.73	58.83	16.78
707	13.42	1.16	27.48	193.55	61.67	16.84
708	13.44	1.12	28.32	197.02	58.33	16.95
709	13.46	1.60	29.23	245.94	49.93	17.09
710	13.48	2.06	32.48	235.09	41.87	17.36
711	13.50	2.52	43.06	199.63	37.75	17.58
712	13.52	2.73	44.23	181.40	35.40	17.57
713	13.54	2.54	29.79	175.33	35.05	17.30
714	13.56	2.04	20.44	164.10	36.43	16.87
715	13.58	1.71	18.01	155.67	42.92	16.67
716	13.60	1.34	23.11	149.91	52.10	16.69
717	13.62	1.12	25.42	203.84	61.78	16.77
718	13.64	1.04	26.80	290.95	67.87	16.79
719	13.66	0.98	26.86	279.17	72.43	16.78
720	13.68	0.88	26.97	259.02	76.07	16.73

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	13.70	0.85	25.13	289.15	77.12	16.63
722	13.72	0.86	21.14	324.49	76.06	16.54
723	13.74	0.85	21.46	320.33	76.48	16.51
724	13.76	0.82	23.84	316.86	77.77	16.56
725	13.78	0.84	24.04	330.25	74.48	16.59
726	13.80	1.00	22.22	353.38	66.38	16.81
727	13.82	1.40	33.42	184.75	64.25	17.02
728	13.84	1.20	37.53	149.72	69.10	17.22
729	13.86	0.94	40.37	140.30	75.55	17.17
730	13.89	1.01	33.04	220.64	70.14	17.12
731	13.90	1.41	30.58	276.50	54.38	17.15
732	13.92	2.07	33.19	201.36	45.66	17.35
733	13.94	2.26	43.00	176.69	42.83	17.54
734	13.96	2.17	44.97	154.37	44.79	17.59
735	13.98	1.88	39.22	133.29	47.07	17.47
736	14.00	1.76	33.57	126.29	47.98	17.33
737	14.02	1.85	33.89	130.63	47.32	17.35
738	14.04	1.98	39.87	121.51	47.84	17.49
739	14.06	1.93	46.46	111.28	48.26	17.62
740	14.08	2.02	46.99	109.49	47.19	17.77
741	14.10	2.40	55.42	108.06	43.75	17.87
742	14.12	2.64	53.84	103.72	40.89	17.91
743	14.14	2.62	48.92	98.76	39.70	17.86
744	14.16	2.50	47.22	93.99	39.70	17.84
745	14.18	2.62	52.40	89.27	39.96	17.92
746	14.21	2.75	58.15	85.93	38.87	18.06
747	14.22	3.07	63.33	83.08	36.41	18.10
748	14.24	3.30	55.01	81.84	33.26	18.06
749	14.26	3.44	47.24	79.85	30.83	17.92
750	14.28	3.37	43.32	76.57	29.67	17.73
751	14.30	3.10	33.29	72.66	29.91	17.47
752	14.32	2.70	25.32	67.39	31.89	17.25
753	14.34	2.34	28.49	60.32	36.76	17.22
754	14.37	2.03	35.34	55.86	43.23	17.40
755	14.38	1.97	44.13	84.62	47.59	17.60
756	14.40	2.09	51.07	94.30	47.49	17.80
757	14.42	2.38	56.26	108.37	42.47	17.96
758	14.44	3.09	58.46	106.94	36.66	18.08
759	14.46	3.57	58.22	99.75	32.25	18.12
760	14.48	3.67	54.38	90.33	30.52	18.07
761	14.50	3.49	50.10	86.92	29.67	17.91
762	14.52	3.33	37.47	86.61	29.19	17.66
763	14.54	3.10	28.98	84.50	27.88	17.33
764	14.56	3.03	22.67	85.12	26.67	17.10
765	14.58	3.14	21.68	85.24	26.70	17.13
766	14.60	3.18	30.96	77.62	28.52	17.44
767	14.62	3.25	44.85	65.28	31.26	17.76
768	14.64	3.21	52.94	59.95	33.60	17.92

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	14.66	3.00	51.53	55.24	35.86	17.89
770	14.68	2.61	43.76	45.88	38.53	17.79
771	14.70	2.41	45.55	41.41	41.99	17.80
772	14.72	2.37	55.63	39.06	43.94	17.93
773	14.74	2.57	61.75	35.90	44.47	18.10
774	14.76	2.70	68.96	34.47	43.66	18.26
775	14.78	2.92	79.80	34.04	40.97	18.30
776	14.80	3.19	62.63	37.88	39.26	18.33
777	14.82	3.18	71.86	35.34	38.75	18.24
778	14.84	2.79	64.89	31.25	41.91	18.19
779	14.86	2.40	59.82	28.33	46.08	18.02
780	14.88	2.06	52.82	25.67	51.89	17.86
781	14.90	1.67	50.97	24.18	53.58	17.76
782	14.92	2.01	48.69	81.71	49.53	17.71
783	14.94	2.46	42.80	79.42	45.44	17.75
784	14.96	2.31	51.68	66.83	46.96	17.69
785	14.98	1.68	43.44	56.29	55.27	17.58
786	15.00	1.28	39.08	49.47	70.20	17.39
787	15.02	0.89	43.56	73.34	82.86	17.23
788	15.04	0.88	35.59	191.82	90.37	17.14
789	15.06	0.91	34.71	213.64	88.07	17.09
790	15.08	0.91	37.78	213.89	89.37	17.13
791	15.10	0.86	39.51	211.84	91.89	17.14
792	15.12	0.84	37.37	215.19	93.01	17.07
793	15.15	0.83	31.89	219.71	91.06	16.94
794	15.16	0.84	27.67	222.81	87.67	16.79
795	15.18	0.86	25.36	234.90	84.15	16.70
796	15.20	0.89	25.03	240.36	81.59	16.65
797	15.22	0.89	23.60	243.27	80.90	16.62
798	15.24	0.87	23.71	240.79	81.36	16.61
799	15.26	0.87	24.48	242.65	82.12	16.62
800	15.28	0.88	24.51	244.08	81.55	16.66
801	15.30	0.91	25.50	246.00	80.68	16.69
802	15.32	0.92	25.94	247.12	81.13	16.72
803	15.34	0.88	26.50	242.84	85.13	16.72
804	15.36	0.77	27.00	235.52	88.91	16.68
805	15.38	0.78	24.86	238.62	89.14	16.62
806	15.40	0.84	22.75	254.12	82.49	16.57
807	15.42	0.95	22.05	268.82	73.47	16.58
808	15.44	1.14	22.90	280.41	66.39	16.69
809	15.46	1.28	26.24	287.35	61.29	16.83
810	15.48	1.40	28.11	257.78	59.05	17.00
811	15.50	1.49	32.57	225.54	57.62	17.15
812	15.52	1.58	35.91	193.99	59.05	17.30
813	15.54	1.49	41.45	149.85	64.74	17.44
814	15.56	1.23	49.39	119.47	73.12	17.52
815	15.58	1.13	50.44	122.07	80.56	17.56
816	15.60	1.22	48.69	136.33	78.61	17.55

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.38	0.00	0.38	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
2	0.04	0.75	0.00	0.75	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
3	0.07	1.32	0.00	1.32	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
4	0.08	1.51	0.00	1.51	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
5	0.10	1.88	0.00	1.88	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
6	0.12	2.26	0.00	2.26	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
7	0.14	2.64	0.00	2.64	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
8	0.16	3.02	0.00	3.02	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
9	0.19	3.58	0.00	3.58	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
10	0.20	3.77	0.00	3.77	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
11	0.22	4.14	0.00	4.14	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
12	0.24	4.52	0.00	4.52	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
13	0.26	4.89	0.00	4.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
14	0.28	5.27	0.00	5.27	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
15	0.30	5.64	0.00	5.64	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
16	0.32	6.01	0.00	6.01	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
17	0.34	6.38	0.00	6.38	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
18	0.36	6.75	0.00	6.75	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
19	0.38	7.12	0.00	7.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
20	0.40	7.49	0.00	7.49	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
21	0.42	7.85	0.00	7.85	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
22	0.44	8.22	0.00	8.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
23	0.46	8.59	0.00	8.59	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
24	0.48	8.95	0.00	8.95	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
25	0.50	9.31	0.00	9.31	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
26	0.52	9.68	0.00	9.68	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
27	0.54	10.04	0.00	10.04	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
28	0.56	10.40	0.00	10.40	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
29	0.58	10.77	0.00	10.77	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
30	0.60	11.13	0.00	11.13	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
31	0.62	11.49	0.00	11.49	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
32	0.64	11.85	0.00	11.85	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
33	0.66	12.21	0.00	12.21	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
34	0.68	12.57	0.00	12.57	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
35	0.70	12.93	0.00	12.93	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
36	0.72	13.28	0.00	13.28	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
37	0.02	1.84	0.00	1.84	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
38	0.04	2.27	0.00	2.27	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
39	0.06	2.70	0.00	2.70	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
40	0.08	3.14	0.00	3.14	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
41	0.10	3.57	0.00	3.57	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
42	0.12	3.84	0.00	3.84	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
43	0.14	4.12	0.00	4.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
44	0.16	4.39	0.00	4.39	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
45	0.18	4.67	0.00	4.67	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
46	0.20	5.10	0.00	5.10	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
47	0.22	5.53	0.00	5.53	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
48	0.24	5.96	0.00	5.96	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.26	6.39	0.00	6.39	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
50	0.28	6.82	0.00	6.82	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
51	0.30	7.26	0.00	7.26	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
52	0.32	7.69	0.00	7.69	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
53	0.34	8.12	0.00	8.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
54	0.36	8.55	0.00	8.55	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
55	0.38	8.98	0.00	8.98	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
56	0.40	9.41	0.00	9.41	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
57	0.42	9.85	0.00	9.85	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
58	0.44	10.12	0.00	10.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
59	0.46	10.40	0.00	10.40	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
60	0.48	10.71	0.00	10.71	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
61	0.50	11.04	0.00	11.04	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
62	0.52	11.37	0.00	11.37	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
63	0.54	11.71	0.00	11.71	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
64	0.56	12.06	0.00	12.06	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
65	0.58	12.41	0.00	12.41	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
66	0.60	12.77	0.00	12.77	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
67	0.62	13.12	0.00	13.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
68	0.64	13.47	0.00	13.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
69	0.66	13.82	0.00	13.82	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
70	0.68	14.18	0.00	14.18	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
71	0.70	14.53	0.00	14.53	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
72	0.72	14.88	0.00	14.88	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
73	0.74	15.23	0.00	15.23	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
74	0.76	15.58	0.00	15.58	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
75	0.78	15.93	0.00	15.93	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
76	0.80	16.27	0.00	16.27	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
77	0.82	16.62	0.00	16.62	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
78	0.84	16.96	0.00	16.96	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
79	0.86	17.30	0.00	17.30	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
80	0.88	17.64	0.00	17.64	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
81	0.90	17.98	0.00	17.98	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
82	0.92	18.31	0.00	18.31	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
83	0.94	18.66	0.00	18.66	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
84	0.96	19.00	0.00	19.00	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
85	0.98	19.36	0.00	19.36	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
86	1.00	19.72	0.00	19.72	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
87	1.02	20.07	0.00	20.07	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
88	1.04	20.43	0.00	20.43	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
89	1.06	20.79	0.00	20.79	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
90	1.08	21.15	0.00	21.15	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
91	1.10	21.52	0.00	21.52	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
92	1.12	21.88	0.00	21.88	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
93	1.14	22.25	0.00	22.25	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
94	1.16	22.61	0.00	22.61	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
95	1.18	22.98	0.00	22.98	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
96	1.20	23.34	0.00	23.34	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.22	23.71	0.00	23.71	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
98	1.24	24.07	0.00	24.07	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
99	1.26	24.44	0.00	24.44	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
100	1.28	24.80	0.00	24.80	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
101	1.30	25.17	0.00	25.17	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
102	1.32	25.53	0.00	25.53	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
103	1.34	25.89	0.00	25.89	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
104	1.36	26.26	0.00	26.26	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
105	1.38	26.62	0.00	26.62	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
106	1.40	26.98	0.00	26.98	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
107	1.42	27.35	0.00	27.35	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
108	1.44	27.71	0.00	27.71	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
109	1.46	28.07	0.00	28.07	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
110	1.48	28.44	0.00	28.44	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
111	1.50	28.80	0.00	28.80	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
112	1.52	29.17	0.00	29.17	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
113	1.54	29.54	0.00	29.54	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
114	1.56	29.90	0.00	29.90	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
115	1.58	30.27	0.00	30.27	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
116	1.60	30.63	0.00	30.63	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
117	1.63	31.18	0.00	31.18	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
118	1.64	31.37	0.00	31.37	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
119	1.66	31.73	0.00	31.73	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
120	1.68	32.10	0.00	32.10	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
121	1.70	32.46	0.00	32.46	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
122	1.72	32.82	0.00	32.82	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
123	1.74	33.18	0.00	33.18	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
124	1.76	33.55	0.00	33.55	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
125	1.78	33.91	0.00	33.91	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
126	1.80	34.27	0.00	34.27	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
127	1.82	34.63	0.00	34.63	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
128	1.84	34.99	0.00	34.99	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
129	1.86	35.35	0.00	35.35	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
130	1.88	35.71	0.00	35.71	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
131	1.90	36.07	0.00	36.07	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
132	1.92	36.43	0.00	36.43	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
133	1.94	36.79	0.00	36.79	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
134	1.96	37.15	0.00	37.15	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
135	1.98	37.50	0.00	37.50	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
136	2.01	38.03	0.10	37.94	0.98	0.140	1.43	0.098	1.09	1.00	0.119	No
137	2.02	38.21	0.20	38.02	0.98	0.141	1.43	0.098	1.09	1.00	0.119	No
138	2.04	38.57	0.39	38.17	0.98	0.141	1.43	0.099	1.09	1.00	0.120	No
139	2.06	38.92	0.59	38.33	0.98	0.142	1.43	0.099	1.08	1.00	0.120	No
140	2.08	39.28	0.78	38.49	0.98	0.143	1.43	0.100	1.08	1.00	0.121	No
141	2.10	39.63	0.98	38.65	0.98	0.143	1.43	0.100	1.08	1.00	0.122	No
142	2.12	39.98	1.18	38.81	0.98	0.144	1.43	0.101	1.08	1.00	0.122	No
143	2.14	40.34	1.37	38.97	0.98	0.145	1.43	0.101	1.08	1.00	0.123	No
144	2.16	40.69	1.57	39.12	0.98	0.145	1.43	0.102	1.08	1.00	0.123	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.18	41.05	1.77	39.28	0.98	0.146	1.43	0.102	1.08	1.00	0.124	No
146	2.20	41.41	1.96	39.44	0.98	0.146	1.43	0.103	1.08	1.00	0.124	No
147	2.22	41.76	2.16	39.60	0.98	0.147	1.43	0.103	1.08	1.00	0.125	No
148	2.24	42.12	2.35	39.77	0.97	0.148	1.43	0.103	1.08	1.00	0.125	No
149	2.26	42.48	2.55	39.93	0.97	0.148	1.43	0.104	1.08	1.00	0.126	No
150	2.28	42.84	2.75	40.10	0.97	0.149	1.43	0.104	1.08	1.00	0.126	No
151	2.30	43.21	2.94	40.26	0.97	0.149	1.43	0.105	1.08	1.00	0.127	No
152	2.32	43.57	3.14	40.43	0.97	0.150	1.43	0.105	1.08	1.00	0.128	No
153	2.34	43.93	3.34	40.59	0.97	0.151	1.43	0.105	1.08	1.00	0.128	No
154	2.36	44.29	3.53	40.76	0.97	0.151	1.43	0.106	1.08	1.00	0.129	No
155	2.38	44.65	3.73	40.92	0.97	0.152	1.43	0.106	1.08	1.00	0.130	No
156	2.40	45.01	3.92	41.09	0.97	0.152	1.43	0.107	1.08	1.00	0.130	No
157	2.42	45.37	4.12	41.25	0.97	0.153	1.43	0.107	1.08	1.00	0.131	No
158	2.44	45.73	4.32	41.42	0.97	0.153	1.43	0.107	1.08	1.00	0.132	No
159	2.46	46.09	4.51	41.58	0.97	0.154	1.43	0.108	1.08	1.00	0.132	No
160	2.48	46.45	4.71	41.74	0.97	0.154	1.43	0.108	1.08	1.00	0.133	No
161	2.50	46.81	4.91	41.90	0.97	0.155	1.43	0.109	1.08	1.00	0.133	No
162	2.52	47.17	5.10	42.06	0.97	0.156	1.43	0.109	1.07	1.00	0.134	No
163	2.54	47.52	5.30	42.22	0.97	0.156	1.43	0.109	1.07	1.00	0.134	No
164	2.56	47.88	5.49	42.39	0.97	0.157	1.43	0.110	1.07	1.00	0.135	No
165	2.58	48.24	5.69	42.55	0.97	0.157	1.43	0.110	1.07	1.00	0.136	No
166	2.60	48.59	5.89	42.71	0.97	0.158	1.43	0.110	1.07	1.00	0.136	No
167	2.62	48.95	6.08	42.87	0.97	0.158	1.43	0.111	1.07	1.00	0.137	No
168	2.64	49.31	6.28	43.03	0.97	0.159	1.43	0.111	1.07	1.00	0.137	No
169	2.66	49.66	6.47	43.19	0.97	0.159	1.43	0.111	1.07	1.00	0.138	No
170	2.68	50.02	6.67	43.35	0.97	0.160	1.43	0.112	1.07	1.00	0.138	No
171	2.70	50.37	6.87	43.51	0.97	0.160	1.43	0.112	1.07	1.00	0.139	No
172	2.72	50.73	7.06	43.66	0.97	0.161	1.43	0.112	1.07	1.00	0.139	No
173	2.74	51.08	7.26	43.82	0.97	0.161	1.43	0.113	1.07	1.00	0.140	No
174	2.76	51.43	7.46	43.98	0.97	0.162	1.43	0.113	1.07	1.00	0.140	No
175	2.78	51.79	7.65	44.14	0.97	0.162	1.43	0.113	1.07	1.00	0.140	No
176	2.80	52.14	7.85	44.29	0.97	0.162	1.43	0.114	1.07	1.00	0.140	No
177	2.82	52.49	8.04	44.44	0.96	0.163	1.43	0.114	1.07	1.00	0.141	No
178	2.84	52.84	8.24	44.60	0.96	0.163	1.43	0.114	1.07	1.00	0.141	No
179	2.86	53.19	8.44	44.75	0.96	0.164	1.43	0.115	1.07	1.00	0.142	No
180	2.88	53.54	8.63	44.91	0.96	0.164	1.43	0.115	1.07	1.00	0.142	No
181	2.90	53.89	8.83	45.06	0.96	0.165	1.43	0.115	1.07	1.00	0.143	No
182	2.92	54.24	9.03	45.22	0.96	0.165	1.43	0.116	1.07	1.00	0.143	No
183	2.94	54.59	9.22	45.37	0.96	0.166	1.43	0.116	1.07	1.00	0.144	No
184	2.96	54.94	9.42	45.52	0.96	0.166	1.43	0.116	1.07	1.00	0.145	No
185	2.98	55.29	9.61	45.68	0.96	0.166	1.43	0.117	1.07	1.00	0.145	No
186	3.00	55.64	9.81	45.83	0.96	0.167	1.43	0.117	1.06	1.00	0.146	No
187	3.02	55.99	10.01	45.98	0.96	0.167	1.43	0.117	1.06	1.00	0.147	No
188	3.04	56.33	10.20	46.13	0.96	0.168	1.43	0.117	1.06	1.00	0.148	No
189	3.06	56.68	10.40	46.28	0.96	0.168	1.43	0.118	1.06	1.00	0.148	No
190	3.09	57.19	10.69	46.49	0.96	0.169	1.43	0.118	1.06	1.00	0.149	No
191	3.10	57.36	10.79	46.57	0.96	0.169	1.43	0.118	1.06	1.00	0.149	No
192	3.12	57.69	10.99	46.71	0.96	0.169	1.43	0.119	1.06	1.00	0.149	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.14	58.03	11.18	46.85	0.96	0.170	1.43	0.119	1.06	1.00	0.150	No
194	3.16	58.36	11.38	46.98	0.96	0.170	1.43	0.119	1.06	1.00	0.149	No
195	3.18	58.69	11.58	47.11	0.96	0.171	1.43	0.119	1.06	1.00	0.150	No
196	3.21	59.18	11.87	47.31	0.96	0.171	1.43	0.120	1.06	1.00	0.150	No
197	3.22	59.34	11.97	47.37	0.96	0.172	1.43	0.120	1.06	1.00	0.150	No
198	3.24	59.67	12.16	47.50	0.96	0.172	1.43	0.120	1.06	1.00	0.150	No
199	3.26	60.00	12.36	47.64	0.96	0.172	1.43	0.121	1.06	1.00	0.150	No
200	3.28	60.33	12.56	47.77	0.96	0.173	1.43	0.121	1.06	1.00	0.151	No
201	3.30	60.66	12.75	47.91	0.96	0.173	1.43	0.121	1.06	1.00	0.151	No
202	3.32	61.00	12.95	48.05	0.96	0.173	1.43	0.121	1.06	1.00	0.151	No
203	3.34	61.34	13.15	48.20	0.96	0.174	1.43	0.122	1.06	1.00	0.151	No
204	3.36	61.68	13.34	48.34	0.95	0.174	1.43	0.122	1.06	1.00	0.152	No
205	3.38	62.03	13.54	48.49	0.95	0.175	1.43	0.122	1.06	1.00	0.152	No
206	3.40	62.38	13.73	48.64	0.95	0.175	1.43	0.122	1.06	1.00	0.152	No
207	3.42	62.72	13.93	48.79	0.95	0.175	1.43	0.123	1.06	1.00	0.152	No
208	3.44	63.07	14.13	48.95	0.95	0.176	1.43	0.123	1.06	1.00	0.153	No
209	3.46	63.42	14.32	49.10	0.95	0.176	1.43	0.123	1.06	1.00	0.153	No
210	3.48	63.78	14.52	49.26	0.95	0.176	1.43	0.123	1.06	1.00	0.154	No
211	3.50	64.13	14.72	49.41	0.95	0.177	1.43	0.124	1.06	1.00	0.154	No
212	3.52	64.48	14.91	49.57	0.95	0.177	1.43	0.124	1.06	1.00	0.154	No
213	3.54	64.84	15.11	49.73	0.95	0.177	1.43	0.124	1.06	1.00	0.154	No
214	3.56	65.19	15.30	49.89	0.95	0.178	1.43	0.124	1.06	1.00	0.154	No
215	3.58	65.55	15.50	50.05	0.95	0.178	1.43	0.125	1.06	1.00	0.154	No
216	3.60	65.91	15.70	50.21	0.95	0.178	1.43	0.125	1.06	1.00	0.155	No
217	3.62	66.27	15.89	50.38	0.95	0.179	1.43	0.125	1.06	1.00	0.155	No
218	3.64	66.63	16.09	50.54	0.95	0.179	1.43	0.125	1.06	1.00	0.155	No
219	3.66	67.00	16.28	50.71	0.95	0.179	1.43	0.126	1.06	1.00	0.156	No
220	3.68	67.36	16.48	50.88	0.95	0.180	1.43	0.126	1.06	1.00	0.156	No
221	3.70	67.72	16.68	51.05	0.95	0.180	1.43	0.126	1.06	1.00	0.157	No
222	3.72	68.09	16.87	51.22	0.95	0.180	1.43	0.126	1.06	1.00	0.157	No
223	3.74	68.46	17.07	51.39	0.95	0.181	1.43	0.126	1.06	1.00	0.157	No
224	3.76	68.82	17.27	51.56	0.95	0.181	1.43	0.127	1.06	1.00	0.158	No
225	3.78	69.19	17.46	51.73	0.95	0.181	1.43	0.127	1.06	1.00	0.158	No
226	3.80	69.55	17.66	51.89	0.95	0.181	1.43	0.127	1.06	1.00	0.158	No
227	3.82	69.92	17.85	52.06	0.95	0.182	1.43	0.127	1.06	1.00	0.159	No
228	3.84	70.28	18.05	52.23	0.95	0.182	1.43	0.127	1.06	1.00	0.159	No
229	3.86	70.65	18.25	52.40	0.95	0.182	1.43	0.128	1.06	1.00	0.159	No
230	3.88	71.01	18.44	52.57	0.94	0.183	1.43	0.128	1.06	1.00	0.159	No
231	3.90	71.37	18.64	52.73	0.94	0.183	1.43	0.128	1.06	1.00	0.160	No
232	3.92	71.74	18.84	52.90	0.94	0.183	1.43	0.128	1.06	1.00	0.160	No
233	3.94	72.10	19.03	53.07	0.94	0.183	1.43	0.128	1.06	1.00	0.160	No
234	3.96	72.46	19.23	53.23	0.94	0.184	1.43	0.129	1.06	1.00	0.160	No
235	3.98	72.82	19.42	53.39	0.94	0.184	1.43	0.129	1.06	1.00	0.161	No
236	4.00	73.17	19.62	53.55	0.94	0.184	1.43	0.129	1.05	1.00	0.161	No
237	4.02	73.53	19.82	53.71	0.94	0.184	1.43	0.129	1.05	1.00	0.162	No
238	4.04	73.88	20.01	53.87	0.94	0.185	1.43	0.129	1.05	1.00	0.162	No
239	4.06	74.23	20.21	54.02	0.94	0.185	1.43	0.129	1.05	1.00	0.163	No
240	4.08	74.58	20.40	54.18	0.94	0.185	1.43	0.130	1.05	1.00	0.163	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.10	74.93	20.60	54.33	0.94	0.186	1.43	0.130	1.05	1.00	0.164	No
242	4.12	75.28	20.80	54.48	0.94	0.186	1.43	0.130	1.05	1.00	0.164	No
243	4.14	75.62	20.99	54.63	0.94	0.186	1.43	0.130	1.05	1.00	0.164	No
244	4.16	75.97	21.19	54.78	0.94	0.186	1.43	0.130	1.05	1.00	0.164	No
245	4.18	76.31	21.39	54.92	0.94	0.187	1.43	0.131	1.05	1.00	0.165	No
246	4.20	76.65	21.58	55.06	0.94	0.187	1.43	0.131	1.05	1.00	0.165	No
247	4.22	76.98	21.78	55.21	0.94	0.187	1.43	0.131	1.05	1.00	0.166	No
248	4.24	77.32	21.97	55.35	0.94	0.187	1.43	0.131	1.05	1.00	0.166	No
249	4.26	77.66	22.17	55.49	0.94	0.188	1.43	0.131	1.05	1.00	0.166	No
250	4.28	77.99	22.37	55.63	0.94	0.188	1.43	0.131	1.05	1.00	0.166	No
251	4.30	78.33	22.56	55.76	0.94	0.188	1.43	0.132	1.05	1.00	0.166	No
252	4.32	78.66	22.76	55.90	0.94	0.188	1.43	0.132	1.05	1.00	0.166	No
253	4.34	78.99	22.96	56.04	0.94	0.189	1.43	0.132	1.05	1.00	0.166	No
254	4.36	79.33	23.15	56.18	0.94	0.189	1.43	0.132	1.05	1.00	0.166	No
255	4.38	79.67	23.35	56.32	0.93	0.189	1.43	0.132	1.05	1.00	0.167	No
256	4.40	80.01	23.54	56.47	0.93	0.189	1.43	0.133	1.05	1.00	0.167	No
257	4.42	80.35	23.74	56.61	0.93	0.190	1.43	0.133	1.05	1.00	0.167	No
258	4.44	80.70	23.94	56.76	0.93	0.190	1.43	0.133	1.05	1.00	0.168	No
259	4.46	81.04	24.13	56.91	0.93	0.190	1.43	0.133	1.05	1.00	0.168	No
260	4.48	81.39	24.33	57.06	0.93	0.190	1.43	0.133	1.05	1.00	0.169	No
261	4.50	81.73	24.53	57.21	0.93	0.191	1.43	0.133	1.05	1.00	0.169	No
262	4.52	82.07	24.72	57.35	0.93	0.191	1.43	0.134	1.05	1.00	0.170	No
263	4.54	82.42	24.92	57.50	0.93	0.191	1.43	0.134	1.05	1.00	0.170	No
264	4.56	82.76	25.11	57.65	0.93	0.191	1.43	0.134	1.05	1.00	0.170	No
265	4.58	83.10	25.31	57.79	0.93	0.191	1.43	0.134	1.05	1.00	0.169	No
266	4.61	83.62	25.60	58.01	0.93	0.192	1.43	0.134	1.05	1.00	0.168	No
267	4.62	83.79	25.70	58.09	0.93	0.192	1.43	0.134	1.05	1.00	0.168	No
268	4.64	84.13	25.90	58.23	0.93	0.192	1.43	0.134	1.05	1.00	0.169	No
269	4.66	84.47	26.09	58.38	0.93	0.192	1.43	0.135	1.05	1.00	0.171	No
270	4.68	84.80	26.29	58.51	0.93	0.193	1.43	0.135	1.04	1.00	0.171	No
271	4.70	85.13	26.49	58.65	0.93	0.193	1.43	0.135	1.04	1.00	0.172	No
272	4.72	85.46	26.68	58.78	0.93	0.193	1.43	0.135	1.04	1.00	0.172	No
273	4.74	85.79	26.88	58.91	0.93	0.193	1.43	0.135	1.04	1.00	0.172	No
274	4.76	86.12	27.08	59.05	0.93	0.193	1.43	0.135	1.04	1.00	0.172	No
275	4.78	86.46	27.27	59.18	0.93	0.194	1.43	0.136	1.04	1.00	0.172	No
276	4.80	86.79	27.47	59.32	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
277	4.82	87.13	27.66	59.47	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
278	4.84	87.48	27.86	59.61	0.93	0.194	1.43	0.136	1.05	1.00	0.170	No
279	4.86	87.82	28.06	59.77	0.93	0.194	1.43	0.136	1.05	1.00	0.170	No
280	4.88	88.17	28.25	59.92	0.92	0.195	1.43	0.136	1.05	1.00	0.170	No
281	4.90	88.52	28.45	60.07	0.92	0.195	1.43	0.136	1.05	1.00	0.170	No
282	4.92	88.87	28.65	60.22	0.92	0.195	1.43	0.136	1.05	1.00	0.171	No
283	4.94	89.21	28.84	60.37	0.92	0.195	1.43	0.137	1.05	1.00	0.172	No
284	4.96	89.56	29.04	60.52	0.92	0.195	1.43	0.137	1.04	1.00	0.173	No
285	4.98	89.90	29.23	60.66	0.92	0.196	1.43	0.137	1.04	1.00	0.174	No
286	5.00	90.24	29.43	60.81	0.92	0.196	1.43	0.137	1.04	1.00	0.174	No
287	5.02	90.58	29.63	60.95	0.92	0.196	1.43	0.137	1.04	1.00	0.174	No
288	5.04	90.92	29.82	61.10	0.92	0.196	1.43	0.137	1.04	1.00	0.174	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.06	91.26	30.02	61.24	0.92	0.196	1.43	0.137	1.04	1.00	0.174	No
290	5.08	91.60	30.21	61.39	0.92	0.196	1.43	0.137	1.04	1.00	0.175	No
291	5.10	91.94	30.41	61.53	0.92	0.197	1.43	0.138	1.04	1.00	0.176	No
292	5.12	92.28	30.61	61.67	0.92	0.197	1.43	0.138	1.04	1.00	0.176	No
293	5.14	92.61	30.80	61.81	0.92	0.197	1.43	0.138	1.04	1.00	0.176	No
294	5.16	92.95	31.00	61.95	0.92	0.197	1.43	0.138	1.04	1.00	0.176	No
295	5.18	93.29	31.20	62.09	0.92	0.197	1.43	0.138	1.04	1.00	0.177	No
296	5.20	93.62	31.39	62.23	0.92	0.197	1.43	0.138	1.04	1.00	0.177	No
297	5.22	93.95	31.59	62.37	0.92	0.198	1.43	0.138	1.04	1.00	0.177	No
298	5.24	94.29	31.78	62.50	0.92	0.198	1.43	0.138	1.04	1.00	0.177	No
299	5.26	94.62	31.98	62.64	0.92	0.198	1.43	0.139	1.04	1.00	0.178	No
300	5.28	94.95	32.18	62.77	0.92	0.198	1.43	0.139	1.04	1.00	0.178	No
301	5.30	95.28	32.37	62.91	0.92	0.198	1.43	0.139	1.04	1.00	0.178	No
302	5.32	95.61	32.57	63.04	0.92	0.199	1.43	0.139	1.04	1.00	0.178	No
303	5.34	95.94	32.77	63.18	0.92	0.199	1.43	0.139	1.04	1.00	0.179	No
304	5.36	96.27	32.96	63.31	0.91	0.199	1.43	0.139	1.04	1.00	0.179	No
305	5.38	96.60	33.16	63.45	0.91	0.199	1.43	0.139	1.04	1.00	0.179	No
306	5.40	96.93	33.35	63.58	0.91	0.199	1.43	0.139	1.04	1.00	0.180	No
307	5.42	97.26	33.55	63.71	0.91	0.199	1.43	0.140	1.04	1.00	0.180	No
308	5.44	97.59	33.75	63.84	0.91	0.200	1.43	0.140	1.04	1.00	0.180	No
309	5.46	97.91	33.94	63.97	0.91	0.200	1.43	0.140	1.04	1.00	0.180	No
310	5.48	98.24	34.14	64.10	0.91	0.200	1.43	0.140	1.04	1.00	0.180	No
311	5.51	98.72	34.43	64.29	0.91	0.200	1.43	0.140	1.04	1.00	0.180	No
312	5.52	98.88	34.53	64.35	0.91	0.200	1.43	0.140	1.04	1.00	0.180	No
313	5.54	99.20	34.73	64.48	0.91	0.200	1.43	0.140	1.04	1.00	0.181	No
314	5.56	99.53	34.92	64.60	0.91	0.201	1.43	0.140	1.04	1.00	0.181	No
315	5.58	99.85	35.12	64.73	0.91	0.201	1.43	0.140	1.04	1.00	0.181	No
316	5.60	100.17	35.32	64.86	0.91	0.201	1.43	0.141	1.04	1.00	0.181	No
317	5.62	100.50	35.51	64.99	0.91	0.201	1.43	0.141	1.04	1.00	0.181	No
318	5.64	100.83	35.71	65.12	0.91	0.201	1.43	0.141	1.04	1.00	0.181	No
319	5.66	101.16	35.90	65.26	0.91	0.201	1.43	0.141	1.04	1.00	0.181	No
320	5.68	101.50	36.10	65.40	0.91	0.201	1.43	0.141	1.03	1.00	0.182	No
321	5.70	101.83	36.30	65.54	0.91	0.202	1.43	0.141	1.03	1.00	0.182	No
322	5.72	102.17	36.49	65.68	0.91	0.202	1.43	0.141	1.03	1.00	0.182	No
323	5.74	102.51	36.69	65.82	0.91	0.202	1.43	0.141	1.03	1.00	0.183	No
324	5.76	102.84	36.89	65.96	0.91	0.202	1.43	0.141	1.03	1.00	0.183	No
325	5.78	103.18	37.08	66.10	0.91	0.202	1.43	0.141	1.03	1.00	0.183	No
326	5.80	103.52	37.28	66.24	0.91	0.202	1.43	0.142	1.03	1.00	0.183	No
327	5.82	103.85	37.47	66.38	0.90	0.202	1.43	0.142	1.03	1.00	0.183	No
328	5.84	104.19	37.67	66.52	0.90	0.203	1.43	0.142	1.03	1.00	0.184	No
329	5.86	104.52	37.87	66.65	0.90	0.203	1.43	0.142	1.03	1.00	0.184	No
330	5.88	104.85	38.06	66.78	0.90	0.203	1.43	0.142	1.03	1.00	0.184	No
331	5.90	105.17	38.26	66.92	0.90	0.203	1.43	0.142	1.03	1.00	0.184	No
332	5.92	105.50	38.46	67.04	0.90	0.203	1.43	0.142	1.03	1.00	0.184	No
333	5.95	105.98	38.75	67.24	0.90	0.203	1.43	0.142	1.03	1.00	0.184	No
334	5.96	106.15	38.85	67.30	0.90	0.203	1.43	0.142	1.03	1.00	0.184	No
335	5.98	106.47	39.04	67.42	0.90	0.203	1.43	0.142	1.03	1.00	0.185	No
336	6.00	106.79	39.24	67.55	0.90	0.204	1.43	0.143	1.03	1.00	0.185	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.02	107.11	39.44	67.68	0.90	0.204	1.43	0.143	1.03	1.00	0.185	No
338	6.04	107.44	39.63	67.80	0.90	0.204	1.43	0.143	1.03	1.00	0.185	No
339	6.06	107.76	39.83	67.93	0.90	0.204	1.43	0.143	1.03	1.00	0.185	No
340	6.08	108.09	40.02	68.06	0.90	0.204	1.43	0.143	1.03	1.00	0.185	No
341	6.10	108.41	40.22	68.19	0.90	0.204	1.43	0.143	1.03	1.00	0.185	No
342	6.12	108.74	40.42	68.32	0.90	0.204	1.43	0.143	1.03	1.00	0.186	No
343	6.14	109.07	40.61	68.46	0.90	0.205	1.43	0.143	1.03	1.00	0.186	No
344	6.16	109.40	40.81	68.59	0.90	0.205	1.43	0.143	1.03	1.00	0.186	No
345	6.18	109.73	41.01	68.73	0.90	0.205	1.43	0.143	1.03	1.00	0.186	No
346	6.20	110.06	41.20	68.86	0.90	0.205	1.43	0.143	1.03	1.00	0.186	No
347	6.22	110.38	41.40	68.98	0.90	0.205	1.43	0.143	1.03	1.00	0.187	No
348	6.24	110.70	41.59	69.11	0.90	0.205	1.43	0.144	1.03	1.00	0.187	No
349	6.26	111.02	41.79	69.23	0.89	0.205	1.43	0.144	1.03	1.00	0.187	No
350	6.28	111.33	41.99	69.35	0.89	0.205	1.43	0.144	1.03	1.00	0.186	No
351	6.30	111.65	42.18	69.46	0.89	0.206	1.43	0.144	1.03	1.00	0.187	No
352	6.32	111.96	42.38	69.58	0.89	0.206	1.43	0.144	1.03	1.00	0.187	No
353	6.34	112.27	42.58	69.69	0.89	0.206	1.43	0.144	1.03	1.00	0.187	No
354	6.36	112.57	42.77	69.80	0.89	0.206	1.43	0.144	1.03	1.00	0.188	No
355	6.38	112.87	42.97	69.90	0.89	0.206	1.43	0.144	1.03	1.00	0.188	No
356	6.40	113.17	43.16	70.01	0.89	0.206	1.43	0.144	1.03	1.00	0.188	No
357	6.42	113.47	43.36	70.11	0.89	0.206	1.43	0.144	1.03	1.00	0.188	No
358	6.44	113.78	43.56	70.22	0.89	0.206	1.43	0.145	1.03	1.00	0.188	No
359	6.46	114.08	43.75	70.33	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
360	6.48	114.39	43.95	70.44	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
361	6.50	114.70	44.15	70.56	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
362	6.52	115.02	44.34	70.68	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
363	6.54	115.33	44.54	70.79	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
364	6.56	115.64	44.73	70.91	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
365	6.58	115.96	44.93	71.03	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
366	6.60	116.28	45.13	71.16	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
367	6.62	116.61	45.32	71.29	0.89	0.207	1.43	0.145	1.03	1.00	0.188	No
368	6.64	116.94	45.52	71.42	0.89	0.208	1.43	0.145	1.03	1.00	0.188	No
369	6.67	117.44	45.81	71.62	0.89	0.208	1.43	0.145	1.03	1.00	0.188	No
370	6.68	117.60	45.91	71.69	0.89	0.208	1.43	0.145	1.03	1.00	0.188	No
371	6.70	117.94	46.11	71.83	0.89	0.208	1.43	0.145	1.03	1.00	0.189	No
372	6.72	118.28	46.30	71.98	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
373	6.74	118.62	46.50	72.12	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
374	6.76	118.96	46.70	72.26	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
375	6.78	119.30	46.89	72.41	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
376	6.80	119.64	47.09	72.55	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
377	6.82	119.98	47.28	72.69	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
378	6.84	120.32	47.48	72.84	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
379	6.86	120.65	47.68	72.98	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
380	6.88	120.99	47.87	73.12	0.88	0.208	1.43	0.146	1.03	1.00	0.189	No
381	6.90	121.32	48.07	73.26	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
382	6.92	121.66	48.27	73.39	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
383	6.94	121.99	48.46	73.53	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
384	6.96	122.32	48.66	73.66	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	6.98	122.65	48.85	73.80	0.88	0.209	1.43	0.146	1.03	1.00	0.190	No
386	7.00	122.98	49.05	73.93	0.88	0.209	1.43	0.146	1.02	1.00	0.190	No
387	7.02	123.32	49.25	74.07	0.88	0.209	1.43	0.146	1.02	1.00	0.190	No
388	7.05	123.81	49.54	74.27	0.88	0.209	1.43	0.146	1.02	1.00	0.191	No
389	7.06	123.98	49.64	74.34	0.88	0.209	1.43	0.146	1.02	1.00	0.191	No
390	7.08	124.31	49.83	74.47	0.88	0.209	1.43	0.146	1.02	1.00	0.191	No
391	7.10	124.64	50.03	74.60	0.88	0.209	1.43	0.146	1.02	1.00	0.191	No
392	7.12	124.96	50.23	74.74	0.88	0.209	1.43	0.147	1.02	1.00	0.191	No
393	7.14	125.29	50.42	74.87	0.88	0.209	1.43	0.147	1.02	1.00	0.190	No
394	7.16	125.63	50.62	75.01	0.87	0.209	1.43	0.147	1.02	1.00	0.190	No
395	7.18	125.96	50.82	75.14	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
396	7.20	126.29	51.01	75.28	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
397	7.22	126.63	51.21	75.43	0.87	0.210	1.43	0.147	1.02	1.00	0.189	No
398	7.24	126.98	51.40	75.57	0.87	0.210	1.43	0.147	1.03	1.00	0.189	No
399	7.26	127.32	51.60	75.72	0.87	0.210	1.43	0.147	1.02	1.00	0.189	No
400	7.28	127.67	51.80	75.87	0.87	0.210	1.43	0.147	1.02	1.00	0.189	No
401	7.30	128.02	51.99	76.03	0.87	0.210	1.43	0.147	1.02	1.00	0.189	No
402	7.32	128.37	52.19	76.18	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
403	7.34	128.73	52.39	76.34	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
404	7.36	129.08	52.58	76.50	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
405	7.38	129.44	52.78	76.66	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
406	7.40	129.79	52.97	76.82	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
407	7.42	130.14	53.17	76.97	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
408	7.44	130.50	53.37	77.13	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
409	7.46	130.85	53.56	77.29	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
410	7.48	131.20	53.76	77.44	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
411	7.50	131.55	53.96	77.60	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
412	7.52	131.90	54.15	77.75	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
413	7.54	132.25	54.35	77.91	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
414	7.56	132.61	54.54	78.06	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
415	7.58	132.96	54.74	78.22	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
416	7.60	133.31	54.94	78.37	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
417	7.62	133.66	55.13	78.53	0.86	0.210	1.43	0.147	1.02	1.00	0.191	No
418	7.64	134.01	55.33	78.68	0.86	0.210	1.43	0.147	1.02	1.00	0.191	No
419	7.66	134.36	55.52	78.84	0.86	0.210	1.43	0.147	1.02	1.00	0.191	No
420	7.68	134.71	55.72	78.99	0.86	0.210	1.43	0.147	1.02	1.00	0.191	No
421	7.70	135.05	55.92	79.13	0.86	0.210	1.43	0.147	1.02	1.00	0.191	No
422	7.72	135.39	56.11	79.28	0.86	0.210	1.43	0.147	1.02	1.00	0.192	No
423	7.74	135.73	56.31	79.42	0.86	0.210	1.43	0.147	1.02	1.00	0.192	No
424	7.76	136.06	56.51	79.55	0.86	0.211	1.43	0.147	1.02	1.00	0.192	No
425	7.78	136.39	56.70	79.69	0.86	0.211	1.43	0.147	1.02	1.00	0.192	No
426	7.80	136.73	56.90	79.83	0.86	0.211	1.43	0.147	1.02	1.00	0.193	No
427	7.82	137.06	57.09	79.97	0.86	0.211	1.43	0.147	1.02	1.00	0.193	No
428	7.84	137.39	57.29	80.10	0.86	0.211	1.43	0.147	1.02	1.00	0.193	No
429	7.86	137.72	57.49	80.24	0.86	0.211	1.43	0.147	1.02	1.00	0.193	No
430	7.88	138.06	57.68	80.38	0.86	0.211	1.43	0.148	1.02	1.00	0.192	No
431	7.90	138.39	57.88	80.51	0.86	0.211	1.43	0.148	1.02	1.00	0.193	No
432	7.92	138.73	58.08	80.65	0.86	0.211	1.43	0.148	1.02	1.00	0.193	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	7.94	139.06	58.27	80.79	0.86	0.211	1.43	0.148	1.02	1.00	0.193	No
434	7.96	139.40	58.47	80.93	0.86	0.211	1.43	0.148	1.02	1.00	0.193	No
435	7.98	139.73	58.66	81.06	0.86	0.211	1.43	0.148	1.02	1.00	0.193	No
436	8.00	140.06	58.86	81.20	0.86	0.211	1.43	0.148	1.02	1.00	0.193	No
437	8.02	140.39	59.06	81.33	0.85	0.211	1.43	0.148	1.02	1.00	0.193	No
438	8.04	140.72	59.25	81.46	0.85	0.211	1.43	0.148	1.02	1.00	0.193	No
439	8.06	141.04	59.45	81.60	0.85	0.211	1.43	0.148	1.02	1.00	0.193	No
440	8.08	141.37	59.64	81.73	0.85	0.211	1.43	0.148	1.02	1.00	0.193	No
441	8.10	141.70	59.84	81.86	0.85	0.211	1.43	0.148	1.02	1.00	0.193	No
442	8.12	142.03	60.04	81.99	0.85	0.211	1.43	0.148	1.02	1.00	0.193	No
443	8.14	142.36	60.23	82.13	0.85	0.211	1.43	0.148	1.02	1.00	0.193	No
444	8.16	142.69	60.43	82.26	0.85	0.211	1.43	0.148	1.02	1.00	0.193	No
445	8.18	143.02	60.63	82.39	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
446	8.20	143.35	60.82	82.53	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
447	8.22	143.68	61.02	82.66	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
448	8.24	144.02	61.21	82.80	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
449	8.26	144.35	61.41	82.94	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
450	8.28	144.68	61.61	83.07	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
451	8.30	145.01	61.80	83.21	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
452	8.32	145.35	62.00	83.35	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
453	8.34	145.68	62.20	83.48	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
454	8.36	146.01	62.39	83.62	0.85	0.211	1.43	0.148	1.02	1.00	0.195	No
455	8.38	146.34	62.59	83.76	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
456	8.40	146.68	62.78	83.89	0.85	0.211	1.43	0.148	1.02	1.00	0.194	No
457	8.42	147.01	62.98	84.03	0.85	0.211	1.43	0.148	1.01	1.00	0.194	No
458	8.44	147.34	63.18	84.17	0.84	0.212	1.43	0.148	1.01	1.00	0.194	No
459	8.46	147.67	63.37	84.30	0.84	0.212	1.43	0.148	1.01	1.00	0.194	No
460	8.48	148.01	63.57	84.44	0.84	0.212	1.43	0.148	1.01	1.00	0.194	No
461	8.50	148.34	63.77	84.57	0.84	0.212	1.43	0.148	1.01	1.00	0.194	No
462	8.52	148.67	63.96	84.71	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
463	8.54	149.00	64.16	84.84	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
464	8.56	149.33	64.35	84.98	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
465	8.58	149.66	64.55	85.11	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
466	8.60	149.99	64.75	85.24	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
467	8.62	150.31	64.94	85.37	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
468	8.64	150.64	65.14	85.50	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
469	8.66	150.96	65.33	85.62	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
470	8.68	151.28	65.53	85.74	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
471	8.70	151.59	65.73	85.86	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
472	8.72	151.91	65.92	85.98	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
473	8.74	152.22	66.12	86.10	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
474	8.76	152.54	66.32	86.23	0.84	0.212	1.43	0.148	1.01	1.00	0.196	No
475	8.78	152.86	66.51	86.35	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
476	8.80	153.18	66.71	86.47	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
477	8.82	153.50	66.90	86.60	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
478	8.84	153.82	67.10	86.72	0.84	0.212	1.43	0.148	1.01	1.00	0.195	No
479	8.86	154.15	67.30	86.85	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
480	8.88	154.48	67.49	86.99	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	8.90	154.81	67.69	87.12	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
482	8.92	155.14	67.89	87.26	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
483	8.94	155.47	68.08	87.39	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
484	8.96	155.79	68.28	87.52	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
485	8.98	156.12	68.47	87.64	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
486	9.00	156.44	68.67	87.77	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
487	9.02	156.76	68.87	87.89	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
488	9.04	157.07	69.06	88.01	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
489	9.06	157.39	69.26	88.13	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
490	9.08	157.71	69.45	88.26	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
491	9.10	158.03	69.65	88.38	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
492	9.12	158.35	69.85	88.50	0.83	0.212	1.43	0.148	1.01	1.00	0.196	No
493	9.14	158.67	70.04	88.63	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
494	9.16	159.00	70.24	88.76	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
495	9.18	159.33	70.44	88.89	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
496	9.20	159.66	70.63	89.03	0.83	0.212	1.43	0.148	1.01	1.00	0.194	No
497	9.22	160.00	70.83	89.17	0.83	0.212	1.43	0.148	1.01	1.00	0.194	No
498	9.24	160.35	71.02	89.32	0.83	0.212	1.43	0.148	1.01	1.00	0.194	No
499	9.26	160.69	71.22	89.47	0.83	0.212	1.43	0.148	1.01	1.00	0.194	No
500	9.28	161.03	71.42	89.61	0.83	0.212	1.43	0.148	1.01	1.00	0.195	No
501	9.30	161.37	71.61	89.76	0.82	0.212	1.43	0.148	1.01	1.00	0.195	No
502	9.32	161.71	71.81	89.90	0.82	0.212	1.43	0.148	1.01	1.00	0.195	No
503	9.34	162.05	72.01	90.05	0.82	0.212	1.43	0.148	1.01	1.00	0.195	No
504	9.36	162.39	72.20	90.19	0.82	0.212	1.43	0.148	1.01	1.00	0.195	No
505	9.38	162.73	72.40	90.34	0.82	0.212	1.43	0.148	1.01	1.00	0.195	No
506	9.40	163.08	72.59	90.48	0.82	0.212	1.43	0.148	1.01	1.00	0.195	No
507	9.42	163.42	72.79	90.63	0.82	0.212	1.43	0.148	1.01	1.00	0.195	No
508	9.44	163.76	72.99	90.78	0.82	0.212	1.43	0.148	1.01	1.00	0.194	No
509	9.46	164.11	73.18	90.92	0.82	0.212	1.43	0.148	1.01	1.00	0.194	No
510	9.48	164.45	73.38	91.07	0.82	0.212	1.43	0.148	1.01	1.00	0.195	No
511	9.50	164.79	73.58	91.22	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
512	9.52	165.13	73.77	91.36	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
513	9.54	165.47	73.97	91.50	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
514	9.56	165.80	74.16	91.64	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
515	9.58	166.14	74.36	91.78	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
516	9.60	166.47	74.56	91.91	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
517	9.62	166.79	74.75	92.04	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
518	9.64	167.12	74.95	92.17	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
519	9.66	167.44	75.14	92.30	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
520	9.68	167.77	75.34	92.43	0.82	0.212	1.43	0.148	1.01	1.00	0.196	No
521	9.70	168.09	75.54	92.55	0.81	0.212	1.43	0.148	1.01	1.00	0.196	No
522	9.72	168.42	75.73	92.68	0.81	0.212	1.43	0.148	1.01	1.00	0.196	No
523	9.74	168.74	75.93	92.81	0.81	0.212	1.43	0.148	1.01	1.00	0.196	No
524	9.76	169.06	76.13	92.94	0.81	0.212	1.43	0.148	1.01	1.00	0.196	No
525	9.78	169.39	76.32	93.07	0.81	0.212	1.43	0.148	1.01	1.00	0.196	No
526	9.80	169.72	76.52	93.20	0.81	0.212	1.43	0.148	1.01	1.00	0.196	No
527	9.82	170.04	76.71	93.33	0.81	0.212	1.43	0.148	1.01	1.00	2.000	Yes
528	9.84	170.38	76.91	93.47	0.81	0.212	1.43	0.148	1.01	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	9.86	170.72	77.11	93.62	0.81	0.212	1.43	0.148	1.01	1.00	2.000	Yes
530	9.88	171.07	77.30	93.77	0.81	0.211	1.43	0.148	1.01	1.00	2.000	Yes
531	9.90	171.42	77.50	93.92	0.81	0.211	1.43	0.148	1.01	1.00	2.000	Yes
532	9.92	171.76	77.70	94.07	0.81	0.211	1.43	0.148	1.01	1.00	2.000	Yes
533	9.94	172.10	77.89	94.21	0.81	0.211	1.43	0.148	1.01	1.00	2.000	Yes
534	9.96	172.43	78.09	94.34	0.81	0.211	1.43	0.148	1.01	1.00	2.000	Yes
535	9.98	172.76	78.28	94.47	0.81	0.211	1.43	0.148	1.01	1.00	2.000	Yes
536	10.00	173.09	78.48	94.61	0.81	0.211	1.43	0.148	1.01	1.00	2.000	Yes
537	10.03	173.60	78.77	94.82	0.81	0.211	1.43	0.148	1.01	1.00	0.195	No
538	10.04	173.77	78.87	94.89	0.81	0.211	1.43	0.148	1.01	1.00	0.195	No
539	10.06	174.11	79.07	95.04	0.81	0.211	1.43	0.148	1.01	1.00	0.194	No
540	10.08	174.45	79.26	95.19	0.81	0.211	1.43	0.148	1.01	1.00	0.193	No
541	10.10	174.79	79.46	95.33	0.81	0.211	1.43	0.148	1.01	1.00	0.194	No
542	10.12	175.13	79.66	95.48	0.80	0.211	1.43	0.148	1.01	1.00	0.194	No
543	10.15	175.64	79.95	95.69	0.80	0.211	1.43	0.148	1.00	1.00	0.194	No
544	10.16	175.82	80.05	95.77	0.80	0.211	1.43	0.148	1.00	1.00	0.194	No
545	10.18	176.16	80.25	95.92	0.80	0.211	1.43	0.148	1.00	1.00	0.194	No
546	10.20	176.51	80.44	96.07	0.80	0.211	1.43	0.148	1.00	1.00	0.194	No
547	10.22	176.86	80.64	96.22	0.80	0.211	1.43	0.148	1.00	1.00	0.194	No
548	10.24	177.21	80.83	96.37	0.80	0.211	1.43	0.148	1.00	1.00	0.194	No
549	10.26	177.55	81.03	96.52	0.80	0.211	1.43	0.148	1.00	1.00	0.195	No
550	10.28	177.90	81.23	96.67	0.80	0.211	1.43	0.148	1.00	1.00	0.196	No
551	10.30	178.24	81.42	96.82	0.80	0.211	1.43	0.148	1.00	1.00	0.196	No
552	10.32	178.58	81.62	96.96	0.80	0.211	1.43	0.148	1.00	1.00	0.196	No
553	10.34	178.92	81.82	97.10	0.80	0.211	1.43	0.147	1.00	1.00	0.196	No
554	10.36	179.25	82.01	97.24	0.80	0.211	1.43	0.147	1.00	1.00	0.196	No
555	10.38	179.59	82.21	97.38	0.80	0.211	1.43	0.147	1.00	1.00	0.196	No
556	10.40	179.92	82.40	97.52	0.80	0.211	1.43	0.147	1.00	1.00	0.196	No
557	10.42	180.25	82.60	97.65	0.80	0.211	1.43	0.147	1.00	1.00	0.196	No
558	10.44	180.58	82.80	97.79	0.80	0.211	1.43	0.147	1.00	1.00	0.196	No
559	10.46	180.91	82.99	97.92	0.80	0.211	1.43	0.147	1.00	1.00	0.196	No
560	10.48	181.25	83.19	98.06	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
561	10.50	181.58	83.39	98.20	0.80	0.210	1.43	0.147	1.00	1.00	0.195	No
562	10.52	181.92	83.58	98.34	0.80	0.210	1.43	0.147	1.00	1.00	0.195	No
563	10.54	182.26	83.78	98.48	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
564	10.56	182.60	83.97	98.63	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
565	10.58	182.94	84.17	98.77	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
566	10.60	183.28	84.37	98.92	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
567	10.62	183.62	84.56	99.06	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
568	10.64	183.96	84.76	99.21	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
569	10.66	184.30	84.95	99.35	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
570	10.68	184.64	85.15	99.49	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
571	10.70	184.98	85.35	99.63	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
572	10.72	185.31	85.54	99.77	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
573	10.74	185.65	85.74	99.91	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
574	10.76	185.98	85.94	100.04	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
575	10.78	186.31	86.13	100.18	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
576	10.80	186.63	86.33	100.31	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	10.82	186.96	86.52	100.44	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
578	10.84	187.29	86.72	100.57	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
579	10.86	187.62	86.92	100.70	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
580	10.88	187.95	87.11	100.84	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
581	10.91	188.45	87.41	101.04	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
582	10.92	188.61	87.51	101.11	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
583	10.94	188.94	87.70	101.24	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
584	10.96	189.27	87.90	101.37	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
585	10.98	189.59	88.09	101.49	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
586	11.00	189.91	88.29	101.62	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
587	11.02	190.23	88.49	101.74	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
588	11.05	190.71	88.78	101.93	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
589	11.06	190.87	88.88	101.99	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
590	11.08	191.19	89.07	102.11	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
591	11.10	191.51	89.27	102.24	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
592	11.12	191.83	89.47	102.36	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
593	11.14	192.15	89.66	102.48	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
594	11.16	192.47	89.86	102.61	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
595	11.18	192.79	90.06	102.73	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
596	11.20	193.11	90.25	102.86	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
597	11.22	193.43	90.45	102.98	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
598	11.24	193.75	90.64	103.11	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
599	11.26	194.08	90.84	103.23	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
600	11.28	194.40	91.04	103.36	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
601	11.30	194.72	91.23	103.49	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
602	11.32	195.05	91.43	103.62	0.78	0.209	1.43	0.146	1.00	1.00	0.196	No
603	11.34	195.37	91.63	103.75	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
604	11.36	195.70	91.82	103.88	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
605	11.38	196.03	92.02	104.01	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
606	11.40	196.36	92.21	104.15	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
607	11.42	196.70	92.41	104.29	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
608	11.44	197.03	92.61	104.43	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
609	11.46	197.37	92.80	104.57	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
610	11.48	197.71	93.00	104.72	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
611	11.50	198.06	93.19	104.86	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
612	11.52	198.41	93.39	105.01	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
613	11.54	198.75	93.59	105.16	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
614	11.56	199.10	93.78	105.32	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
615	11.58	199.45	93.98	105.47	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
616	11.60	199.80	94.18	105.62	0.77	0.208	1.43	0.146	1.00	1.00	0.194	No
617	11.62	200.14	94.37	105.77	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
618	11.64	200.49	94.57	105.92	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
619	11.66	200.84	94.76	106.08	0.77	0.208	1.43	0.146	1.00	1.00	0.194	No
620	11.68	201.19	94.96	106.23	0.77	0.208	1.43	0.146	1.00	1.00	0.194	No
621	11.70	201.54	95.16	106.38	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
622	11.72	201.89	95.35	106.53	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
623	11.74	202.23	95.55	106.68	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
624	11.76	202.58	95.75	106.84	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	11.78	202.93	95.94	106.99	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
626	11.80	203.27	96.14	107.13	0.76	0.208	1.43	0.145	1.00	1.00	0.194	No
627	11.82	203.62	96.33	107.28	0.76	0.207	1.43	0.145	1.00	1.00	0.194	No
628	11.84	203.96	96.53	107.43	0.76	0.207	1.43	0.145	1.00	1.00	0.194	No
629	11.86	204.30	96.73	107.58	0.76	0.207	1.43	0.145	1.00	1.00	0.194	No
630	11.89	204.82	97.02	107.80	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
631	11.90	204.99	97.12	107.87	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
632	11.92	205.33	97.32	108.01	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
633	11.94	205.67	97.51	108.16	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
634	11.96	206.01	97.71	108.30	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
635	11.98	206.35	97.90	108.44	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
636	12.00	206.69	98.10	108.59	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
637	12.02	207.02	98.30	108.72	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
638	12.04	207.35	98.49	108.86	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
639	12.06	207.69	98.69	109.00	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
640	12.08	208.01	98.88	109.13	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
641	12.10	208.34	99.08	109.26	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
642	12.12	208.67	99.28	109.39	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
643	12.14	208.99	99.47	109.52	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
644	12.16	209.32	99.67	109.65	0.76	0.206	1.43	0.145	0.99	1.00	0.194	No
645	12.18	209.64	99.87	109.78	0.76	0.206	1.43	0.144	0.99	1.00	0.194	No
646	12.20	209.96	100.06	109.90	0.76	0.206	1.43	0.144	0.99	1.00	0.194	No
647	12.22	210.29	100.26	110.03	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
648	12.24	210.61	100.45	110.15	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
649	12.26	210.93	100.65	110.28	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
650	12.28	211.25	100.85	110.40	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
651	12.30	211.57	101.04	110.53	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
652	12.32	211.89	101.24	110.65	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
653	12.34	212.22	101.44	110.78	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
654	12.36	212.54	101.63	110.91	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
655	12.38	212.86	101.83	111.03	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
656	12.40	213.18	102.02	111.16	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
657	12.42	213.50	102.22	111.28	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
658	12.44	213.82	102.42	111.41	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
659	12.46	214.14	102.61	111.53	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
660	12.48	214.46	102.81	111.65	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
661	12.50	214.78	103.01	111.78	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
662	12.52	215.10	103.20	111.90	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
663	12.54	215.42	103.40	112.03	0.75	0.206	1.43	0.144	0.99	1.00	0.194	No
664	12.56	215.74	103.59	112.15	0.75	0.205	1.43	0.144	0.99	1.00	0.194	No
665	12.58	216.06	103.79	112.27	0.75	0.205	1.43	0.144	0.99	1.00	0.194	No
666	12.60	216.38	103.99	112.40	0.75	0.205	1.43	0.144	0.99	1.00	0.194	No
667	12.62	216.70	104.18	112.52	0.75	0.205	1.43	0.144	0.99	1.00	0.193	No
668	12.64	217.02	104.38	112.64	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
669	12.66	217.34	104.57	112.77	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
670	12.68	217.66	104.77	112.89	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
671	12.70	217.98	104.97	113.01	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No
672	12.72	218.29	105.16	113.13	0.74	0.205	1.43	0.144	0.99	1.00	0.193	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	12.74	218.61	105.36	113.25	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
674	12.76	218.93	105.56	113.37	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
675	12.78	219.24	105.75	113.49	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
676	12.80	219.56	105.95	113.61	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
677	12.82	219.89	106.14	113.74	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
678	12.84	220.21	106.34	113.87	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
679	12.86	220.54	106.54	114.00	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
680	12.88	220.86	106.73	114.13	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
681	12.90	221.19	106.93	114.26	0.74	0.205	1.43	0.143	0.99	1.00	0.193	No
682	12.92	221.52	107.13	114.39	0.74	0.204	1.43	0.143	0.99	1.00	0.193	No
683	12.94	221.85	107.32	114.53	0.74	0.204	1.43	0.143	0.99	1.00	0.193	No
684	12.96	222.18	107.52	114.66	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
685	12.98	222.51	107.71	114.79	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
686	13.00	222.84	107.91	114.93	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
687	13.02	223.17	108.11	115.07	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
688	13.04	223.51	108.30	115.20	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
689	13.06	223.84	108.50	115.34	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
690	13.08	224.18	108.69	115.48	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
691	13.10	224.51	108.89	115.62	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
692	13.12	224.85	109.09	115.76	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
693	13.14	225.19	109.28	115.90	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
694	13.16	225.52	109.48	116.04	0.73	0.204	1.43	0.143	0.99	1.00	0.192	No
695	13.18	225.86	109.68	116.19	0.73	0.204	1.43	0.143	0.99	1.00	0.191	No
696	13.20	226.20	109.87	116.33	0.73	0.204	1.43	0.142	0.99	1.00	0.192	No
697	13.22	226.54	110.07	116.47	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
698	13.24	226.88	110.26	116.62	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
699	13.26	227.22	110.46	116.76	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
700	13.28	227.56	110.66	116.90	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
701	13.30	227.90	110.85	117.04	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
702	13.32	228.23	111.05	117.19	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
703	13.34	228.57	111.25	117.32	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
704	13.36	228.90	111.44	117.46	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
705	13.38	229.24	111.64	117.60	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
706	13.40	229.57	111.83	117.74	0.73	0.203	1.43	0.142	0.99	1.00	0.190	No
707	13.42	229.91	112.03	117.88	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
708	13.44	230.25	112.23	118.02	0.73	0.203	1.43	0.142	0.99	1.00	0.191	No
709	13.46	230.59	112.42	118.17	0.73	0.203	1.43	0.142	0.99	1.00	0.190	No
710	13.48	230.94	112.62	118.32	0.73	0.202	1.43	0.142	0.99	1.00	0.189	No
711	13.50	231.29	112.82	118.47	0.72	0.202	1.43	0.142	0.99	1.00	0.187	No
712	13.52	231.64	113.01	118.63	0.72	0.202	1.43	0.142	0.99	1.00	0.187	No
713	13.54	231.99	113.21	118.78	0.72	0.202	1.43	0.142	0.99	1.00	0.187	No
714	13.56	232.32	113.40	118.92	0.72	0.202	1.43	0.141	0.99	1.00	0.189	No
715	13.58	232.66	113.60	119.06	0.72	0.202	1.43	0.141	0.99	1.00	0.189	No
716	13.60	232.99	113.80	119.19	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
717	13.62	233.33	113.99	119.33	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
718	13.64	233.66	114.19	119.47	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
719	13.66	234.00	114.38	119.61	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
720	13.68	234.33	114.58	119.75	0.72	0.202	1.43	0.141	0.99	1.00	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	13.70	234.66	114.78	119.89	0.72	0.202	1.43	0.141	0.99	1.00	0.191	No
722	13.72	235.00	114.97	120.02	0.72	0.202	1.43	0.141	0.99	1.00	0.191	No
723	13.74	235.33	115.17	120.16	0.72	0.201	1.43	0.141	0.99	1.00	0.191	No
724	13.76	235.66	115.37	120.29	0.72	0.201	1.43	0.141	0.99	1.00	0.191	No
725	13.78	235.99	115.56	120.43	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
726	13.80	236.33	115.76	120.57	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
727	13.82	236.67	115.95	120.71	0.72	0.201	1.43	0.141	0.99	1.00	0.189	No
728	13.84	237.01	116.15	120.86	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
729	13.86	237.35	116.35	121.01	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
730	13.89	237.87	116.64	121.23	0.72	0.201	1.43	0.141	0.99	1.00	0.190	No
731	13.90	238.04	116.74	121.30	0.72	0.201	1.43	0.141	0.98	1.00	0.189	No
732	13.92	238.39	116.94	121.45	0.72	0.201	1.43	0.141	0.98	1.00	0.187	No
733	13.94	238.74	117.13	121.61	0.71	0.201	1.43	0.140	0.98	1.00	0.187	No
734	13.96	239.09	117.33	121.76	0.71	0.201	1.43	0.140	0.98	1.00	0.187	No
735	13.98	239.44	117.52	121.91	0.71	0.201	1.43	0.140	0.98	1.00	0.188	No
736	14.00	239.78	117.72	122.06	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
737	14.02	240.13	117.92	122.22	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
738	14.04	240.48	118.11	122.37	0.71	0.200	1.43	0.140	0.98	1.00	0.187	No
739	14.06	240.83	118.31	122.52	0.71	0.200	1.43	0.140	0.98	1.00	0.187	No
740	14.08	241.19	118.50	122.68	0.71	0.200	1.43	0.140	0.98	1.00	0.187	No
741	14.10	241.55	118.70	122.85	0.71	0.200	1.43	0.140	0.98	1.00	0.186	No
742	14.12	241.90	118.90	123.01	0.71	0.200	1.43	0.140	0.98	1.00	0.185	No
743	14.14	242.26	119.09	123.17	0.71	0.200	1.43	0.140	0.98	1.00	0.185	No
744	14.16	242.62	119.29	123.33	0.71	0.200	1.43	0.140	0.98	1.00	0.186	No
745	14.18	242.98	119.49	123.49	0.71	0.200	1.43	0.140	0.98	1.00	0.185	No
746	14.21	243.52	119.78	123.74	0.71	0.199	1.43	0.140	0.98	1.00	2.000	Yes
747	14.22	243.70	119.88	123.82	0.71	0.199	1.43	0.140	0.98	1.00	2.000	Yes
748	14.24	244.06	120.07	123.99	0.71	0.199	1.43	0.139	0.98	1.00	2.000	Yes
749	14.26	244.42	120.27	124.15	0.71	0.199	1.43	0.139	0.98	1.00	2.000	Yes
750	14.28	244.77	120.47	124.31	0.71	0.199	1.43	0.139	0.98	1.00	2.000	Yes
751	14.30	245.12	120.66	124.46	0.71	0.199	1.43	0.139	0.98	1.00	2.000	Yes
752	14.32	245.47	120.86	124.61	0.71	0.199	1.43	0.139	0.98	1.00	2.000	Yes
753	14.34	245.81	121.06	124.76	0.71	0.199	1.43	0.139	0.98	1.00	2.000	Yes
754	14.37	246.33	121.35	124.98	0.71	0.199	1.43	0.139	0.98	1.00	2.000	Yes
755	14.38	246.51	121.45	125.06	0.70	0.199	1.43	0.139	0.98	1.00	2.000	Yes
756	14.40	246.87	121.64	125.22	0.70	0.199	1.43	0.139	0.98	1.00	2.000	Yes
757	14.42	247.23	121.84	125.39	0.70	0.198	1.43	0.139	0.98	1.00	2.000	Yes
758	14.44	247.59	122.04	125.55	0.70	0.198	1.43	0.139	0.98	1.00	2.000	Yes
759	14.46	247.95	122.23	125.72	0.70	0.198	1.43	0.139	0.98	1.00	2.000	Yes
760	14.48	248.31	122.43	125.88	0.70	0.198	1.43	0.139	0.98	1.00	2.000	Yes
761	14.50	248.67	122.63	126.04	0.70	0.198	1.43	0.139	0.98	1.00	0.182	No
762	14.52	249.02	122.82	126.20	0.70	0.198	1.43	0.139	0.98	1.00	0.183	No
763	14.54	249.37	123.02	126.35	0.70	0.198	1.43	0.139	0.98	1.00	0.184	No
764	14.56	249.71	123.21	126.50	0.70	0.198	1.43	0.138	0.98	1.00	0.184	No
765	14.58	250.05	123.41	126.64	0.70	0.198	1.43	0.138	0.98	1.00	2.000	Yes
766	14.60	250.40	123.61	126.80	0.70	0.198	1.43	0.138	0.98	1.00	2.000	Yes
767	14.62	250.76	123.80	126.96	0.70	0.198	1.43	0.138	0.98	1.00	2.000	Yes
768	14.64	251.12	124.00	127.12	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	14.66	251.47	124.19	127.28	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes
770	14.68	251.83	124.39	127.44	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes
771	14.70	252.19	124.59	127.60	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes
772	14.72	252.54	124.78	127.76	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes
773	14.74	252.91	124.98	127.93	0.70	0.197	1.43	0.138	0.98	1.00	0.183	No
774	14.76	253.27	125.18	128.10	0.70	0.197	1.43	0.138	0.98	1.00	0.183	No
775	14.78	253.64	125.37	128.27	0.70	0.197	1.43	0.138	0.98	1.00	0.182	No
776	14.80	254.00	125.57	128.44	0.70	0.197	1.43	0.138	0.98	1.00	0.181	No
777	14.82	254.37	125.76	128.60	0.69	0.197	1.43	0.138	0.98	1.00	0.181	No
778	14.84	254.73	125.96	128.77	0.69	0.196	1.43	0.138	0.98	1.00	0.183	No
779	14.86	255.09	126.16	128.94	0.69	0.196	1.43	0.137	0.98	1.00	0.183	No
780	14.88	255.45	126.35	129.10	0.69	0.196	1.43	0.137	0.98	1.00	0.184	No
781	14.90	255.81	126.55	129.26	0.69	0.196	1.43	0.137	0.98	1.00	0.185	No
782	14.92	256.16	126.75	129.41	0.69	0.196	1.43	0.137	0.98	1.00	0.184	No
783	14.94	256.51	126.94	129.57	0.69	0.196	1.43	0.137	0.98	1.00	0.183	No
784	14.96	256.87	127.14	129.73	0.69	0.196	1.43	0.137	0.98	1.00	0.183	No
785	14.98	257.22	127.33	129.89	0.69	0.196	1.43	0.137	0.98	1.00	0.185	No
786	15.00	257.57	127.53	130.04	0.69	0.196	1.43	0.137	0.98	1.00	0.185	No
787	15.02	257.91	127.73	130.19	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
788	15.04	258.26	127.92	130.33	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
789	15.06	258.60	128.12	130.48	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
790	15.08	258.94	128.31	130.62	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
791	15.10	259.28	128.51	130.77	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
792	15.12	259.62	128.71	130.92	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
793	15.15	260.13	129.00	131.13	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
794	15.16	260.30	129.10	131.20	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
795	15.18	260.63	129.30	131.34	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
796	15.20	260.97	129.49	131.47	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
797	15.22	261.30	129.69	131.61	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
798	15.24	261.63	129.88	131.75	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
799	15.26	261.96	130.08	131.88	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
800	15.28	262.30	130.28	132.02	0.68	0.195	1.43	0.136	0.98	1.00	0.185	No
801	15.30	262.63	130.47	132.16	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
802	15.32	262.96	130.67	132.30	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
803	15.34	263.30	130.87	132.43	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
804	15.36	263.63	131.06	132.57	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
805	15.38	263.97	131.26	132.71	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
806	15.40	264.30	131.45	132.84	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
807	15.42	264.63	131.65	132.98	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
808	15.44	264.96	131.85	133.12	0.68	0.194	1.43	0.136	0.98	1.00	0.184	No
809	15.46	265.30	132.04	133.26	0.68	0.194	1.43	0.136	0.98	1.00	0.184	No
810	15.48	265.64	132.24	133.40	0.68	0.194	1.43	0.136	0.98	1.00	0.184	No
811	15.50	265.98	132.44	133.55	0.68	0.194	1.43	0.136	0.98	1.00	0.184	No
812	15.52	266.33	132.63	133.70	0.68	0.194	1.43	0.135	0.98	1.00	0.183	No
813	15.54	266.68	132.83	133.85	0.68	0.193	1.43	0.135	0.98	1.00	0.183	No
814	15.56	267.03	133.02	134.00	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No
815	15.58	267.38	133.22	134.16	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No
816	15.60	267.73	133.42	134.31	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	1.34	100.00	3.08	0.54	1.70	22.59	0.00	22.59	4.000	No	Yes	2.00
2	0.04	1.33	100.00	3.09	0.54	1.70	22.00	0.00	22.00	4.000	No	Yes	2.00
3	0.07	1.37	100.00	3.08	0.54	1.70	22.88	0.00	22.88	4.000	No	Yes	2.00
4	0.08	1.42	100.00	3.06	0.53	1.70	23.79	0.00	23.79	4.000	No	Yes	2.00
5	0.10	1.47	100.00	3.04	0.53	1.70	24.70	0.00	24.70	4.000	No	Yes	2.00
6	0.12	1.51	100.00	3.02	0.53	1.70	25.38	0.00	25.38	4.000	No	Yes	2.00
7	0.14	1.52	100.00	3.01	0.53	1.70	25.83	0.00	25.83	4.000	No	Yes	2.00
8	0.16	1.50	100.00	3.01	0.53	1.70	25.40	0.00	25.40	4.000	No	Yes	2.00
9	0.19	1.45	100.00	3.03	0.53	1.70	23.99	0.00	23.99	4.000	No	Yes	2.00
10	0.20	1.38	100.00	3.06	0.53	1.70	23.43	0.00	23.43	4.000	No	Yes	2.00
11	0.22	1.32	100.00	3.09	0.54	1.70	22.19	0.00	22.19	4.000	No	Yes	2.00
12	0.24	1.25	100.00	3.13	0.54	1.70	20.83	0.00	20.83	4.000	No	Yes	2.00
13	0.26	1.20	100.00	3.15	0.55	1.70	20.03	0.00	20.03	4.000	No	Yes	2.00
14	0.28	1.17	100.00	3.16	0.55	1.70	19.46	0.00	19.46	4.000	No	Yes	2.00
15	0.30	1.15	100.00	3.15	0.55	1.70	19.38	0.00	19.38	4.000	No	Yes	2.00
16	0.32	1.14	100.00	3.14	0.55	1.70	19.22	0.00	19.22	4.000	No	Yes	2.00
17	0.34	1.13	100.00	3.13	0.55	1.70	18.98	0.00	18.98	4.000	No	Yes	2.00
18	0.36	1.11	100.00	3.13	0.55	1.70	18.78	0.00	18.78	4.000	No	Yes	2.00
19	0.38	1.07	100.00	3.14	0.55	1.70	17.89	0.00	17.89	4.000	No	Yes	2.00
20	0.40	1.02	100.00	3.16	0.56	1.70	17.09	0.00	17.09	4.000	No	Yes	2.00
21	0.42	0.97	100.00	3.19	0.56	1.70	16.24	0.00	16.24	4.000	No	Yes	2.00
22	0.44	0.94	100.00	3.21	0.56	1.70	15.73	0.00	15.73	4.000	No	Yes	2.00
23	0.46	0.92	100.00	3.21	0.56	1.70	15.42	0.00	15.42	4.000	No	Yes	2.00
24	0.48	0.91	100.00	3.22	0.56	1.70	15.36	0.00	15.36	4.000	No	Yes	2.00
25	0.50	0.90	100.00	3.22	0.56	1.70	15.19	0.00	15.19	4.000	No	Yes	2.00
26	0.52	0.88	100.00	3.22	0.56	1.70	14.73	0.00	14.73	4.000	No	Yes	2.00
27	0.54	0.86	100.00	3.23	0.57	1.70	14.56	0.00	14.56	4.000	No	Yes	2.00
28	0.56	0.84	100.00	3.24	0.57	1.70	14.28	0.00	14.28	4.000	No	Yes	2.00
29	0.58	0.81	100.00	3.26	0.57	1.70	13.74	0.00	13.74	4.000	No	Yes	2.00
30	0.60	0.79	100.00	3.27	0.57	1.70	13.00	0.00	13.00	4.000	No	Yes	2.00
31	0.62	0.80	100.00	3.26	0.57	1.70	13.29	0.00	13.29	4.000	No	Yes	2.00
32	0.64	0.85	100.00	3.22	0.57	1.70	14.07	0.00	14.07	4.000	No	Yes	2.00
33	0.66	0.89	100.00	3.19	0.56	1.70	15.27	0.00	15.27	4.000	No	Yes	2.00
34	0.68	0.94	100.00	3.15	0.56	1.70	15.70	0.00	15.70	4.000	No	Yes	2.00
35	0.70	0.97	100.00	3.12	0.56	1.70	16.25	0.00	16.25	4.000	No	Yes	2.00
36	0.72	0.66	100.00	3.24	0.56	1.70	16.80	0.00	16.80	4.000	No	Yes	2.00
37	0.02	0.34	100.00	3.43	0.63	1.70	-0.32	0.00	-0.32	4.000	No	Yes	2.00
38	0.04	0.01	0.00	N/A	0.78	1.70	-0.28	0.00	21.00	4.000	No	No	2.00
39	0.06	0.02	0.00	N/A	0.78	1.70	-0.23	0.00	21.00	4.000	No	No	2.00
40	0.08	0.01	0.00	N/A	0.78	1.70	-0.19	0.00	21.00	4.000	No	No	2.00
41	0.10	0.01	0.00	N/A	0.78	1.70	-0.38	0.00	21.00	4.000	No	No	2.00
42	0.12	0.01	100.00	4.06	0.63	1.70	-0.26	0.00	-0.26	4.000	No	Yes	2.00
43	0.14	0.02	100.00	4.06	0.63	1.70	-0.14	0.00	-0.14	4.000	No	Yes	2.00
44	0.16	0.02	100.00	4.06	0.63	1.70	-0.22	0.00	-0.22	4.000	No	Yes	2.00
45	0.18	0.01	100.00	4.06	0.63	1.70	-0.25	0.00	-0.25	4.000	No	Yes	2.00
46	0.20	0.01	0.00	N/A	0.78	1.70	-0.28	0.00	21.00	4.000	No	No	2.00
47	0.22	0.01	0.00	N/A	0.78	1.70	-0.32	0.00	21.00	4.000	No	No	2.00
48	0.24	0.01	0.00	N/A	0.78	1.70	-0.24	0.00	21.00	4.000	No	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.26	0.01	0.00	N/A	0.78	1.70	-0.31	0.00	21.00	4.000	No	No	2.00
50	0.28	0.01	0.00	N/A	0.78	1.70	-0.23	0.00	21.00	4.000	No	No	2.00
51	0.30	0.02	0.00	N/A	0.78	1.70	-0.15	0.00	21.00	4.000	No	No	2.00
52	0.32	0.02	0.00	N/A	0.78	1.70	-0.19	0.00	21.00	4.000	No	No	2.00
53	0.34	0.01	0.00	N/A	0.78	1.70	-0.30	0.00	21.00	4.000	No	No	2.00
54	0.36	0.01	0.00	N/A	0.78	1.70	-0.18	0.00	21.00	4.000	No	No	2.00
55	0.38	0.01	0.00	N/A	0.78	1.70	-0.33	0.00	21.00	4.000	No	No	2.00
56	0.40	0.01	0.00	N/A	0.78	1.70	-0.29	0.00	21.00	4.000	No	No	2.00
57	0.42	0.01	0.00	N/A	0.78	1.70	-0.28	0.00	21.00	4.000	No	No	2.00
58	0.44	0.09	100.00	3.45	0.63	1.70	-0.20	0.00	-0.20	4.000	No	Yes	2.00
59	0.46	0.17	100.00	3.46	0.61	1.70	2.45	0.00	2.45	4.000	No	Yes	2.00
60	0.48	0.25	100.00	3.46	0.61	1.70	2.60	0.00	2.60	4.000	No	Yes	2.00
61	0.50	0.26	100.00	3.64	0.61	1.70	2.98	0.00	2.98	4.000	No	Yes	2.00
62	0.52	0.26	100.00	3.77	0.61	1.70	2.84	0.00	2.84	4.000	No	Yes	2.00
63	0.54	0.25	100.00	3.87	0.61	1.70	2.95	0.00	2.95	4.000	No	Yes	2.00
64	0.56	0.24	100.00	3.95	0.61	1.70	3.03	0.00	3.03	4.000	No	Yes	2.00
65	0.58	0.24	100.00	4.01	0.61	1.70	2.88	0.00	2.88	4.000	No	Yes	2.00
66	0.60	0.23	100.00	4.06	0.61	1.70	3.00	0.00	3.00	4.000	No	Yes	2.00
67	0.62	0.22	100.00	4.06	0.61	1.70	2.54	0.00	2.54	4.000	No	Yes	2.00
68	0.64	0.22	100.00	4.06	0.61	1.70	2.66	0.00	2.66	4.000	No	Yes	2.00
69	0.66	0.21	100.00	4.06	0.61	1.70	2.70	0.00	2.70	4.000	No	Yes	2.00
70	0.68	0.21	100.00	4.06	0.61	1.70	2.43	0.00	2.43	4.000	No	Yes	2.00
71	0.70	0.21	100.00	4.06	0.61	1.70	2.58	0.00	2.58	4.000	No	Yes	2.00
72	0.72	0.22	100.00	4.06	0.61	1.70	2.62	0.00	2.62	4.000	No	Yes	2.00
73	0.74	0.21	100.00	4.06	0.61	1.70	2.77	0.00	2.77	4.000	No	Yes	2.00
74	0.76	0.21	100.00	4.06	0.61	1.70	2.39	0.00	2.39	4.000	No	Yes	2.00
75	0.78	0.22	100.00	4.06	0.61	1.70	2.54	0.00	2.54	4.000	No	Yes	2.00
76	0.80	0.23	100.00	3.98	0.61	1.70	3.11	0.00	3.11	4.000	No	Yes	2.00
77	0.82	0.24	100.00	3.91	0.61	1.70	3.22	0.00	3.22	4.000	No	Yes	2.00
78	0.84	0.26	100.00	3.85	0.61	1.70	3.07	0.00	3.07	4.000	No	Yes	2.00
79	0.86	0.27	100.00	3.82	0.61	1.70	3.71	0.00	3.71	4.000	No	Yes	2.00
80	0.88	0.27	100.00	3.80	0.61	1.70	3.52	0.00	3.52	4.000	No	Yes	2.00
81	0.90	0.26	100.00	3.80	0.61	1.70	3.18	0.00	3.18	4.000	No	Yes	2.00
82	0.92	0.27	100.00	3.76	0.61	1.70	3.40	0.00	3.40	4.000	No	Yes	2.00
83	0.94	0.30	100.00	3.73	0.61	1.70	4.16	0.00	4.16	4.000	No	Yes	2.00
84	0.96	0.53	100.00	3.42	0.60	1.70	4.43	0.00	4.43	4.000	No	Yes	2.00
85	0.98	0.78	100.00	3.19	0.57	1.70	13.71	0.00	13.71	4.000	No	Yes	2.00
86	1.00	1.05	100.00	3.02	0.56	1.70	16.06	0.00	16.06	4.000	No	Yes	2.00
87	1.02	1.12	100.00	2.98	0.55	1.70	17.38	0.00	17.38	4.000	No	Yes	2.00
88	1.04	1.16	100.00	2.97	0.55	1.70	17.99	0.00	17.99	4.000	No	Yes	2.00
89	1.06	1.18	100.00	2.98	0.55	1.70	18.18	0.00	18.18	4.000	No	Yes	2.00
90	1.08	1.19	100.00	2.99	0.55	1.70	18.59	0.00	18.59	4.000	No	Yes	2.00
91	1.10	1.22	100.00	2.99	0.55	1.70	18.85	0.00	18.85	4.000	No	Yes	2.00
92	1.12	1.24	100.00	3.00	0.55	1.70	19.49	0.00	19.49	4.000	No	Yes	2.00
93	1.14	1.26	100.00	3.00	0.55	1.70	19.90	0.00	19.90	4.000	No	Yes	2.00
94	1.16	1.26	100.00	3.00	0.55	1.70	19.93	0.00	19.93	4.000	No	Yes	2.00
95	1.18	1.26	100.00	3.00	0.55	1.70	19.88	0.00	19.88	4.000	No	Yes	2.00
96	1.20	1.25	100.00	3.00	0.55	1.70	19.91	0.00	19.91	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.22	1.23	100.00	3.01	0.55	1.70	19.33	0.00	19.33	4.000	No	Yes	2.00
98	1.24	1.21	100.00	3.01	0.55	1.70	19.13	0.00	19.13	4.000	No	Yes	2.00
99	1.26	1.18	100.00	3.03	0.55	1.70	18.85	0.00	18.85	4.000	No	Yes	2.00
100	1.28	1.12	100.00	3.07	0.55	1.70	17.89	0.00	17.89	4.000	No	Yes	2.00
101	1.30	1.06	100.00	3.10	0.56	1.70	16.17	0.00	16.17	4.000	No	Yes	2.00
102	1.32	1.04	100.00	3.11	0.56	1.70	15.97	0.00	15.97	4.000	No	Yes	2.00
103	1.34	1.07	100.00	3.09	0.56	1.70	16.79	0.00	16.79	4.000	No	Yes	2.00
104	1.36	1.13	100.00	3.06	0.55	1.70	17.91	0.00	17.91	4.000	No	Yes	2.00
105	1.38	1.16	100.00	3.03	0.55	1.70	18.53	0.00	18.53	4.000	No	Yes	2.00
106	1.40	1.16	100.00	3.02	0.55	1.70	18.59	0.00	18.59	4.000	No	Yes	2.00
107	1.42	1.14	100.00	3.03	0.55	1.70	17.93	0.00	17.93	4.000	No	Yes	2.00
108	1.44	1.12	100.00	3.05	0.55	1.70	17.42	0.00	17.42	4.000	No	Yes	2.00
109	1.46	1.11	100.00	3.06	0.55	1.70	17.44	0.00	17.44	4.000	No	Yes	2.00
110	1.48	1.12	100.00	3.07	0.55	1.70	17.54	0.00	17.54	4.000	No	Yes	2.00
111	1.50	1.13	100.00	3.08	0.55	1.70	17.75	0.00	17.75	4.000	No	Yes	2.00
112	1.52	1.14	100.00	3.08	0.55	1.70	18.18	0.00	18.18	4.000	No	Yes	2.00
113	1.54	1.15	100.00	3.09	0.55	1.70	18.17	0.00	18.17	4.000	No	Yes	2.00
114	1.56	1.15	100.00	3.08	0.55	1.70	18.11	0.00	18.11	4.000	No	Yes	2.00
115	1.58	1.15	100.00	3.08	0.55	1.70	18.32	0.00	18.32	4.000	No	Yes	2.00
116	1.60	1.14	100.00	3.08	0.55	1.70	17.89	0.00	17.89	4.000	No	Yes	2.00
117	1.63	1.14	100.00	3.08	0.55	1.70	17.76	0.00	17.76	4.000	No	Yes	2.00
118	1.64	1.14	100.00	3.07	0.55	1.70	18.15	0.00	18.15	4.000	No	Yes	2.00
119	1.66	1.16	100.00	3.06	0.55	1.70	18.29	0.00	18.29	4.000	No	Yes	2.00
120	1.68	1.16	100.00	3.05	0.55	1.70	18.35	0.00	18.35	4.000	No	Yes	2.00
121	1.70	1.18	100.00	3.03	0.55	1.70	18.44	0.00	18.44	4.000	No	Yes	2.00
122	1.72	1.20	100.00	3.01	0.55	1.70	19.07	0.00	19.07	4.000	No	Yes	2.00
123	1.74	1.23	100.00	2.98	0.55	1.70	19.73	0.00	19.73	4.000	No	Yes	2.00
124	1.76	1.23	100.00	2.97	0.55	1.70	19.67	0.00	19.67	4.000	No	Yes	2.00
125	1.78	1.21	100.00	2.98	0.55	1.70	19.13	0.00	19.13	4.000	No	Yes	2.00
126	1.80	1.17	100.00	2.99	0.55	1.70	18.47	0.00	18.47	4.000	No	Yes	2.00
127	1.82	1.12	100.00	3.02	0.55	1.70	17.85	0.00	17.85	4.000	No	Yes	2.00
128	1.84	1.06	100.00	3.06	0.56	1.70	16.74	0.00	16.74	4.000	No	Yes	2.00
129	1.86	1.00	100.00	3.11	0.56	1.70	15.70	0.00	15.70	4.000	No	Yes	2.00
130	1.88	0.95	100.00	3.15	0.56	1.70	14.78	0.00	14.78	4.000	No	Yes	2.00
131	1.90	0.90	100.00	3.17	0.57	1.70	14.28	0.00	14.28	4.000	No	Yes	2.00
132	1.92	0.87	100.00	3.19	0.57	1.70	13.85	0.00	13.85	4.000	No	Yes	2.00
133	1.94	0.86	100.00	3.19	0.57	1.70	13.57	0.00	13.57	4.000	No	Yes	2.00
134	1.96	0.88	100.00	3.16	0.57	1.70	13.38	0.00	13.38	4.000	No	Yes	2.00
135	1.98	0.92	100.00	3.11	0.56	1.70	15.20	0.00	15.20	4.000	No	Yes	2.00
136	2.01	0.96	100.00	3.07	0.56	1.70	15.43	0.00	15.43	4.000	No	Yes	2.00
137	2.02	0.98	100.00	3.06	0.56	1.70	15.54	0.00	15.54	4.000	No	Yes	2.00
138	2.04	0.99	100.00	3.04	0.56	1.70	15.84	0.00	15.84	4.000	No	Yes	2.00
139	2.06	0.99	100.00	3.03	0.56	1.70	16.06	0.00	16.06	4.000	No	Yes	2.00
140	2.08	0.99	100.00	3.03	0.56	1.70	15.79	0.00	15.79	4.000	No	Yes	2.00
141	2.10	1.00	100.00	3.03	0.56	1.69	15.76	0.00	15.76	4.000	No	Yes	2.00
142	2.12	1.01	100.00	3.02	0.56	1.68	15.93	0.00	15.93	4.000	No	Yes	2.00
143	2.14	1.04	100.00	3.01	0.56	1.67	16.21	0.00	16.21	4.000	No	Yes	2.00
144	2.16	1.07	100.00	2.99	0.56	1.66	16.93	0.00	16.93	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.18	1.08	100.00	2.99	0.56	1.65	16.92	0.00	16.92	4.000	No	Yes	2.00
146	2.20	1.08	100.00	3.00	0.56	1.65	16.49	0.00	16.49	4.000	No	Yes	2.00
147	2.22	1.08	100.00	3.02	0.56	1.64	16.76	0.00	16.76	4.000	No	Yes	2.00
148	2.24	1.09	100.00	3.03	0.56	1.63	16.78	0.00	16.78	4.000	No	Yes	2.00
149	2.26	1.10	100.00	3.04	0.56	1.62	16.87	0.00	16.87	4.000	No	Yes	2.00
150	2.28	1.10	100.00	3.05	0.56	1.62	16.79	0.00	16.79	4.000	No	Yes	2.00
151	2.30	1.08	100.00	3.07	0.56	1.61	16.40	0.00	16.40	4.000	No	Yes	2.00
152	2.32	1.06	100.00	3.09	0.56	1.60	15.88	0.00	15.88	4.000	No	Yes	2.00
153	2.34	1.04	100.00	3.10	0.56	1.60	15.80	0.00	15.80	4.000	No	Yes	2.00
154	2.36	1.01	100.00	3.12	0.56	1.59	15.29	0.00	15.29	4.000	No	Yes	2.00
155	2.38	0.99	100.00	3.14	0.57	1.59	14.46	0.00	14.46	4.000	No	Yes	2.00
156	2.40	0.96	100.00	3.16	0.57	1.58	14.29	0.00	14.29	4.000	No	Yes	2.00
157	2.42	0.95	100.00	3.16	0.57	1.58	13.81	0.00	13.81	4.000	No	Yes	2.00
158	2.44	0.93	100.00	3.16	0.57	1.57	13.78	0.00	13.78	4.000	No	Yes	2.00
159	2.46	0.93	100.00	3.15	0.57	1.57	13.51	0.00	13.51	4.000	No	Yes	2.00
160	2.48	0.93	100.00	3.14	0.57	1.56	13.44	0.00	13.44	4.000	No	Yes	2.00
161	2.50	0.92	100.00	3.14	0.57	1.55	13.48	0.00	13.48	4.000	No	Yes	2.00
162	2.52	0.91	100.00	3.13	0.57	1.55	13.08	0.00	13.08	4.000	No	Yes	2.00
163	2.54	0.90	100.00	3.14	0.57	1.55	12.98	0.00	12.98	4.000	No	Yes	2.00
164	2.56	0.89	100.00	3.15	0.57	1.55	12.91	0.00	12.91	4.000	No	Yes	2.00
165	2.58	0.88	100.00	3.16	0.57	1.54	12.55	0.00	12.55	4.000	No	Yes	2.00
166	2.60	0.86	100.00	3.18	0.57	1.54	12.38	0.00	12.38	4.000	No	Yes	2.00
167	2.62	0.84	100.00	3.20	0.57	1.54	11.99	0.00	11.99	4.000	No	Yes	2.00
168	2.64	0.81	100.00	3.22	0.58	1.54	11.56	0.00	11.56	4.000	No	Yes	2.00
169	2.66	0.79	100.00	3.24	0.58	1.54	11.20	0.00	11.20	4.000	No	Yes	2.00
170	2.68	0.78	100.00	3.25	0.58	1.54	10.84	0.00	10.84	4.000	No	Yes	2.00
171	2.70	0.77	100.00	3.24	0.58	1.53	11.05	0.00	11.05	4.000	No	Yes	2.00
172	2.72	0.79	100.00	3.21	0.58	1.53	11.05	0.00	11.05	4.000	No	Yes	2.00
173	2.74	0.82	100.00	3.18	0.58	1.52	11.65	0.00	11.65	4.000	No	Yes	2.00
174	2.76	0.86	100.00	3.14	0.57	1.52	12.08	0.00	12.08	4.000	No	Yes	2.00
175	2.78	0.89	100.00	3.10	0.57	1.51	12.81	0.00	12.81	4.000	No	Yes	2.00
176	2.80	0.91	100.00	3.07	0.57	1.51	12.94	0.00	12.94	4.000	No	Yes	2.00
177	2.82	0.92	100.00	3.05	0.57	1.51	12.95	0.00	12.95	4.000	No	Yes	2.00
178	2.84	0.93	100.00	3.04	0.57	1.50	13.08	0.00	13.08	4.000	No	Yes	2.00
179	2.86	0.93	100.00	3.04	0.57	1.50	13.06	0.00	13.06	4.000	No	Yes	2.00
180	2.88	0.93	100.00	3.05	0.57	1.50	13.06	0.00	13.06	4.000	No	Yes	2.00
181	2.90	0.91	100.00	3.06	0.57	1.50	12.84	0.00	12.84	4.000	No	Yes	2.00
182	2.92	0.88	100.00	3.09	0.57	1.50	12.24	0.00	12.24	4.000	No	Yes	2.00
183	2.94	0.83	100.00	3.13	0.58	1.50	11.73	0.00	11.73	4.000	No	Yes	2.00
184	2.96	0.78	100.00	3.17	0.58	1.50	10.78	0.00	10.78	4.000	No	Yes	2.00
185	2.98	0.71	100.00	3.23	0.58	1.50	9.76	0.00	9.76	4.000	No	Yes	2.00
186	3.00	0.64	100.00	3.31	0.59	1.50	9.03	0.00	9.03	4.000	No	Yes	2.00
187	3.02	0.56	100.00	3.39	0.59	1.50	7.67	0.00	7.67	4.000	No	Yes	2.00
188	3.04	0.49	100.00	3.48	0.60	1.51	6.48	0.00	6.48	4.000	No	Yes	2.00
189	3.06	0.44	100.00	3.54	0.60	1.51	5.77	0.00	5.77	4.000	No	Yes	2.00
190	3.09	0.41	100.00	3.58	0.60	1.50	5.40	0.00	5.40	4.000	No	Yes	2.00
191	3.10	0.40	100.00	3.56	0.60	1.50	5.06	0.00	5.06	4.000	No	Yes	2.00
192	3.12	0.42	100.00	3.49	0.60	1.50	5.58	0.00	5.58	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.14	0.50	100.00	3.33	0.60	1.49	6.32	0.00	6.32	4.000	No	Yes	2.00
194	3.16	0.58	100.00	3.18	0.59	1.48	8.10	0.00	8.10	4.000	No	Yes	2.00
195	3.18	0.64	100.00	3.07	0.59	1.48	8.98	0.00	8.98	4.000	No	Yes	2.00
196	3.21	0.69	100.00	2.99	0.59	1.48	8.96	0.00	8.96	4.000	No	Yes	2.00
197	3.22	0.74	96.96	2.92	0.58	1.47	10.24	0.00	10.24	4.000	No	Yes	2.00
198	3.24	0.81	92.36	2.87	0.58	1.47	11.13	0.00	11.13	4.000	No	Yes	2.00
199	3.26	0.84	92.91	2.87	0.58	1.46	11.78	0.00	11.78	4.000	No	Yes	2.00
200	3.28	0.87	94.36	2.89	0.58	1.46	11.57	0.00	11.57	4.000	No	Yes	2.00
201	3.30	0.88	95.71	2.91	0.58	1.45	12.06	0.00	12.06	4.000	No	Yes	2.00
202	3.32	0.92	95.38	2.90	0.57	1.45	12.36	0.00	12.36	4.000	No	Yes	2.00
203	3.34	0.95	95.59	2.91	0.57	1.45	12.91	0.00	12.91	4.000	No	Yes	2.00
204	3.36	0.98	96.52	2.92	0.57	1.44	13.42	0.00	13.42	4.000	No	Yes	2.00
205	3.38	0.99	97.88	2.94	0.57	1.44	13.37	0.00	13.37	4.000	No	Yes	2.00
206	3.40	1.00	98.92	2.95	0.57	1.44	13.45	0.00	13.45	4.000	No	Yes	2.00
207	3.42	1.00	100.00	2.96	0.57	1.43	13.61	0.00	13.61	4.000	No	Yes	2.00
208	3.44	1.00	100.00	2.98	0.57	1.43	13.44	0.00	13.44	4.000	No	Yes	2.00
209	3.46	0.99	100.00	3.01	0.57	1.43	13.18	0.00	13.18	4.000	No	Yes	2.00
210	3.48	1.00	100.00	3.01	0.57	1.43	13.28	0.00	13.28	4.000	No	Yes	2.00
211	3.50	1.02	100.00	3.01	0.57	1.42	13.75	0.00	13.75	4.000	No	Yes	2.00
212	3.52	1.06	100.00	3.00	0.57	1.42	14.10	0.00	14.10	4.000	No	Yes	2.00
213	3.54	1.11	100.00	2.98	0.56	1.42	14.78	0.00	14.78	4.000	No	Yes	2.00
214	3.56	1.15	100.00	2.97	0.56	1.41	15.55	0.00	15.55	4.000	No	Yes	2.00
215	3.58	1.18	100.00	2.97	0.56	1.41	15.62	0.00	15.62	4.000	No	Yes	2.00
216	3.60	1.19	100.00	2.98	0.56	1.41	15.81	0.00	15.81	4.000	No	Yes	2.00
217	3.62	1.19	100.00	3.00	0.56	1.40	15.93	0.00	15.93	4.000	No	Yes	2.00
218	3.64	1.19	100.00	3.02	0.56	1.40	15.72	0.00	15.72	4.000	No	Yes	2.00
219	3.66	1.18	100.00	3.03	0.56	1.40	15.69	0.00	15.69	4.000	No	Yes	2.00
220	3.68	1.17	100.00	3.05	0.56	1.40	15.58	0.00	15.58	4.000	No	Yes	2.00
221	3.70	1.14	100.00	3.08	0.56	1.40	14.98	0.00	14.98	4.000	No	Yes	2.00
222	3.72	1.12	100.00	3.11	0.57	1.40	14.56	0.00	14.56	4.000	No	Yes	2.00
223	3.74	1.11	100.00	3.12	0.57	1.39	14.53	0.00	14.53	4.000	No	Yes	2.00
224	3.76	1.11	100.00	3.12	0.57	1.39	14.50	0.00	14.50	4.000	No	Yes	2.00
225	3.78	1.12	100.00	3.11	0.56	1.39	14.80	0.00	14.80	4.000	No	Yes	2.00
226	3.80	1.11	100.00	3.11	0.57	1.39	14.56	0.00	14.56	4.000	No	Yes	2.00
227	3.82	1.12	100.00	3.10	0.57	1.39	14.35	0.00	14.35	4.000	No	Yes	2.00
228	3.84	1.11	100.00	3.10	0.56	1.38	14.77	0.00	14.77	4.000	No	Yes	2.00
229	3.86	1.12	100.00	3.09	0.57	1.38	14.44	0.00	14.44	4.000	No	Yes	2.00
230	3.88	1.12	100.00	3.09	0.56	1.38	14.65	0.00	14.65	4.000	No	Yes	2.00
231	3.90	1.12	100.00	3.08	0.56	1.38	14.59	0.00	14.59	4.000	No	Yes	2.00
232	3.92	1.16	100.00	3.05	0.57	1.37	14.47	0.00	14.47	4.000	No	Yes	2.00
233	3.94	1.18	100.00	3.02	0.56	1.37	15.85	0.00	15.85	4.000	No	Yes	2.00
234	3.96	1.20	100.00	2.99	0.56	1.37	15.38	0.00	15.38	4.000	No	Yes	2.00
235	3.98	1.16	100.00	2.99	0.56	1.36	15.15	0.00	15.15	4.000	No	Yes	2.00
236	4.00	1.11	100.00	3.01	0.57	1.36	14.46	0.00	14.46	4.000	No	Yes	2.00
237	4.02	1.03	100.00	3.04	0.57	1.37	13.07	0.00	13.07	4.000	No	Yes	2.00
238	4.04	0.97	100.00	3.07	0.57	1.37	12.22	0.00	12.22	4.000	No	Yes	2.00
239	4.06	0.94	100.00	3.08	0.57	1.37	12.00	0.00	12.00	4.000	No	Yes	2.00
240	4.08	0.92	100.00	3.07	0.58	1.36	11.77	0.00	11.77	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.10	0.90	100.00	3.06	0.58	1.36	11.46	0.00	11.46	4.000	No	Yes	2.00
242	4.12	0.89	100.00	3.05	0.58	1.36	11.41	0.00	11.41	4.000	No	Yes	2.00
243	4.14	0.89	100.00	3.02	0.58	1.36	11.21	0.00	11.21	4.000	No	Yes	2.00
244	4.16	0.88	100.00	3.02	0.58	1.36	11.46	0.00	11.46	4.000	No	Yes	2.00
245	4.18	0.86	100.00	3.01	0.58	1.36	10.74	0.00	10.74	4.000	No	Yes	2.00
246	4.20	0.82	100.00	3.03	0.58	1.36	10.64	0.00	10.64	4.000	No	Yes	2.00
247	4.22	0.79	100.00	3.05	0.58	1.36	9.86	0.00	9.86	4.000	No	Yes	2.00
248	4.24	0.75	100.00	3.07	0.58	1.36	9.40	0.00	9.40	4.000	No	Yes	2.00
249	4.26	0.75	100.00	3.06	0.59	1.35	9.21	0.00	9.21	4.000	No	Yes	2.00
250	4.28	0.79	100.00	3.01	0.58	1.35	9.85	0.00	9.85	4.000	No	Yes	2.00
251	4.30	0.86	97.60	2.93	0.58	1.35	10.75	0.00	10.75	4.000	No	Yes	2.00
252	4.32	0.96	92.07	2.86	0.58	1.34	12.10	0.00	12.10	4.000	No	Yes	2.00
253	4.34	1.04	88.48	2.82	0.57	1.34	13.40	0.00	13.40	4.000	No	Yes	2.00
254	4.36	1.09	87.27	2.80	0.57	1.33	13.88	0.00	13.88	4.000	No	Yes	2.00
255	4.38	1.09	88.87	2.82	0.57	1.33	13.95	0.00	13.95	4.000	No	Yes	2.00
256	4.40	1.06	92.07	2.86	0.57	1.33	13.35	0.00	13.35	4.000	No	Yes	2.00
257	4.42	1.00	97.11	2.93	0.57	1.33	12.72	0.00	12.72	4.000	No	Yes	2.00
258	4.44	0.94	100.00	2.99	0.58	1.33	11.58	0.00	11.58	4.000	No	Yes	2.00
259	4.46	0.87	100.00	3.06	0.58	1.33	10.96	0.00	10.96	4.000	No	Yes	2.00
260	4.48	0.82	100.00	3.12	0.58	1.33	10.08	0.00	10.08	4.000	No	Yes	2.00
261	4.50	0.76	100.00	3.17	0.58	1.33	9.46	0.00	9.46	4.000	No	Yes	2.00
262	4.52	0.73	100.00	3.19	0.59	1.33	8.81	0.00	8.81	4.000	No	Yes	2.00
263	4.54	0.75	100.00	3.16	0.59	1.33	8.74	0.00	8.74	4.000	No	Yes	2.00
264	4.56	0.87	100.00	3.04	0.58	1.32	10.21	0.00	10.21	4.000	No	Yes	2.00
265	4.58	1.09	93.21	2.88	0.57	1.32	13.26	0.00	13.26	4.000	No	Yes	2.00
266	4.61	1.30	84.28	2.77	0.56	1.31	16.94	0.00	16.94	4.000	No	Yes	2.00
267	4.62	1.35	82.56	2.74	0.56	1.30	18.04	0.00	18.04	4.000	No	Yes	2.00
268	4.64	1.20	88.40	2.82	0.57	1.31	15.10	0.00	15.10	4.000	No	Yes	2.00
269	4.66	0.98	96.26	2.92	0.58	1.31	11.45	0.00	11.45	4.000	No	Yes	2.00
270	4.68	0.82	100.00	2.99	0.58	1.31	9.69	0.00	9.69	4.000	No	Yes	2.00
271	4.70	0.77	100.00	2.98	0.59	1.31	9.22	0.00	9.22	4.000	No	Yes	2.00
272	4.72	0.77	100.00	2.99	0.58	1.31	9.53	0.00	9.53	4.000	No	Yes	2.00
273	4.74	0.79	100.00	2.98	0.58	1.31	9.43	0.00	9.43	4.000	No	Yes	2.00
274	4.76	0.86	98.32	2.94	0.58	1.31	10.03	0.00	10.03	4.000	No	Yes	2.00
275	4.78	1.01	90.10	2.84	0.58	1.30	11.94	0.00	11.94	4.000	No	Yes	2.00
276	4.80	1.22	82.04	2.74	0.57	1.30	15.14	0.00	15.14	4.000	No	Yes	2.00
277	4.82	1.41	76.60	2.67	0.56	1.29	17.65	0.00	17.65	4.000	No	Yes	2.00
278	4.84	1.57	74.64	2.65	0.56	1.29	19.17	0.00	19.17	4.000	No	Yes	2.00
279	4.86	1.69	73.57	2.63	0.55	1.28	21.04	0.00	21.04	4.000	No	Yes	2.00
280	4.88	1.73	74.10	2.64	0.55	1.28	21.95	0.00	21.95	4.000	No	Yes	2.00
281	4.90	1.69	74.80	2.65	0.55	1.28	20.80	0.00	20.80	4.000	No	Yes	2.00
282	4.92	1.56	78.65	2.70	0.55	1.28	19.93	0.00	19.93	4.000	No	Yes	2.00
283	4.94	1.38	83.56	2.76	0.56	1.28	17.13	0.00	17.13	4.000	No	Yes	2.00
284	4.96	1.17	91.31	2.85	0.57	1.28	14.07	0.00	14.07	4.000	No	Yes	2.00
285	4.98	1.03	96.83	2.92	0.58	1.28	11.92	0.00	11.92	4.000	No	Yes	2.00
286	5.00	0.98	99.17	2.95	0.58	1.28	11.73	0.00	11.73	4.000	No	Yes	2.00
287	5.02	1.00	98.42	2.94	0.57	1.28	12.28	0.00	12.28	4.000	No	Yes	2.00
288	5.04	1.01	97.86	2.94	0.57	1.28	12.52	0.00	12.52	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.06	0.96	100.00	2.97	0.57	1.28	12.11	0.00	12.11	4.000	No	Yes	2.00
290	5.08	0.88	100.00	3.02	0.58	1.28	10.36	0.00	10.36	4.000	No	Yes	2.00
291	5.10	0.82	100.00	3.06	0.58	1.28	9.59	0.00	9.59	4.000	No	Yes	2.00
292	5.12	0.82	100.00	3.06	0.58	1.28	9.86	0.00	9.86	4.000	No	Yes	2.00
293	5.14	0.82	100.00	3.05	0.58	1.28	10.10	0.00	10.10	4.000	No	Yes	2.00
294	5.16	0.80	100.00	3.07	0.58	1.27	9.50	0.00	9.50	4.000	No	Yes	2.00
295	5.18	0.79	100.00	3.07	0.59	1.27	9.18	0.00	9.18	4.000	No	Yes	2.00
296	5.20	0.80	100.00	3.04	0.58	1.27	9.89	0.00	9.89	4.000	No	Yes	2.00
297	5.22	0.82	100.00	3.01	0.58	1.27	9.83	0.00	9.83	4.000	No	Yes	2.00
298	5.24	0.78	100.00	3.05	0.58	1.27	9.84	0.00	9.84	4.000	No	Yes	2.00
299	5.26	0.73	100.00	3.09	0.59	1.27	8.19	0.00	8.19	4.000	No	Yes	2.00
300	5.28	0.68	100.00	3.14	0.59	1.27	8.21	0.00	8.21	4.000	No	Yes	2.00
301	5.30	0.66	100.00	3.16	0.59	1.27	7.81	0.00	7.81	4.000	No	Yes	2.00
302	5.32	0.62	100.00	3.21	0.59	1.27	7.44	0.00	7.44	4.000	No	Yes	2.00
303	5.34	0.59	100.00	3.27	0.59	1.27	6.90	0.00	6.90	4.000	No	Yes	2.00
304	5.36	0.55	100.00	3.33	0.60	1.27	6.42	0.00	6.42	4.000	No	Yes	2.00
305	5.38	0.52	100.00	3.37	0.60	1.27	6.08	0.00	6.08	4.000	No	Yes	2.00
306	5.40	0.49	100.00	3.40	0.60	1.26	5.74	0.00	5.74	4.000	No	Yes	2.00
307	5.42	0.48	100.00	3.41	0.60	1.26	5.32	0.00	5.32	4.000	No	Yes	2.00
308	5.44	0.48	100.00	3.39	0.60	1.26	5.59	0.00	5.59	4.000	No	Yes	2.00
309	5.46	0.50	100.00	3.32	0.60	1.26	5.90	0.00	5.90	4.000	No	Yes	2.00
310	5.48	0.53	100.00	3.26	0.60	1.26	6.17	0.00	6.17	4.000	No	Yes	2.00
311	5.51	0.55	100.00	3.22	0.60	1.26	6.49	0.00	6.49	4.000	No	Yes	2.00
312	5.52	0.56	100.00	3.21	0.60	1.25	6.66	0.00	6.66	4.000	No	Yes	2.00
313	5.54	0.56	100.00	3.21	0.60	1.25	6.54	0.00	6.54	4.000	No	Yes	2.00
314	5.56	0.57	100.00	3.20	0.60	1.25	6.45	0.00	6.45	4.000	No	Yes	2.00
315	5.58	0.59	100.00	3.17	0.59	1.25	6.92	0.00	6.92	4.000	No	Yes	2.00
316	5.60	0.63	100.00	3.15	0.59	1.25	7.38	0.00	7.38	4.000	No	Yes	2.00
317	5.62	0.66	100.00	3.15	0.59	1.25	7.84	0.00	7.84	4.000	No	Yes	2.00
318	5.64	0.67	100.00	3.16	0.59	1.24	7.92	0.00	7.92	4.000	No	Yes	2.00
319	5.66	0.66	100.00	3.19	0.59	1.24	7.91	0.00	7.91	4.000	No	Yes	2.00
320	5.68	0.62	100.00	3.26	0.59	1.24	7.39	0.00	7.39	4.000	No	Yes	2.00
321	5.70	0.57	100.00	3.35	0.60	1.24	6.62	0.00	6.62	4.000	No	Yes	2.00
322	5.72	0.52	100.00	3.44	0.60	1.24	6.01	0.00	6.01	4.000	No	Yes	2.00
323	5.74	0.49	100.00	3.51	0.60	1.24	5.60	0.00	5.60	4.000	No	Yes	2.00
324	5.76	0.47	100.00	3.54	0.60	1.24	5.43	0.00	5.43	4.000	No	Yes	2.00
325	5.78	0.46	100.00	3.58	0.60	1.24	5.37	0.00	5.37	4.000	No	Yes	2.00
326	5.80	0.44	100.00	3.60	0.60	1.24	4.98	0.00	4.98	4.000	No	Yes	2.00
327	5.82	0.42	100.00	3.62	0.60	1.24	4.93	0.00	4.93	4.000	No	Yes	2.00
328	5.84	0.41	100.00	3.63	0.60	1.24	4.62	0.00	4.62	4.000	No	Yes	2.00
329	5.86	0.39	100.00	3.63	0.60	1.23	4.45	0.00	4.45	4.000	No	Yes	2.00
330	5.88	0.39	100.00	3.63	0.60	1.23	4.45	0.00	4.45	4.000	No	Yes	2.00
331	5.90	0.39	100.00	3.60	0.61	1.23	4.34	0.00	4.34	4.000	No	Yes	2.00
332	5.92	0.40	100.00	3.55	0.60	1.23	4.57	0.00	4.57	4.000	No	Yes	2.00
333	5.95	0.43	100.00	3.48	0.60	1.23	4.84	0.00	4.84	4.000	No	Yes	2.00
334	5.96	0.44	100.00	3.44	0.60	1.23	5.14	0.00	5.14	4.000	No	Yes	2.00
335	5.98	0.45	100.00	3.41	0.60	1.23	5.10	0.00	5.10	4.000	No	Yes	2.00
336	6.00	0.46	100.00	3.40	0.60	1.22	5.34	0.00	5.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.02	0.48	100.00	3.39	0.60	1.22	5.34	0.00	5.34	4.000	No	Yes	2.00
338	6.04	0.48	100.00	3.39	0.60	1.22	5.63	0.00	5.63	4.000	No	Yes	2.00
339	6.06	0.48	100.00	3.39	0.60	1.22	5.49	0.00	5.49	4.000	No	Yes	2.00
340	6.08	0.48	100.00	3.41	0.60	1.22	5.51	0.00	5.51	4.000	No	Yes	2.00
341	6.10	0.47	100.00	3.44	0.60	1.22	5.56	0.00	5.56	4.000	No	Yes	2.00
342	6.12	0.45	100.00	3.50	0.60	1.22	5.16	0.00	5.16	4.000	No	Yes	2.00
343	6.14	0.42	100.00	3.57	0.60	1.22	4.72	0.00	4.72	4.000	No	Yes	2.00
344	6.16	0.41	100.00	3.61	0.60	1.21	4.66	0.00	4.66	4.000	No	Yes	2.00
345	6.18	0.39	100.00	3.63	0.60	1.21	4.58	0.00	4.58	4.000	No	Yes	2.00
346	6.20	0.37	100.00	3.66	0.61	1.21	4.20	0.00	4.20	4.000	No	Yes	2.00
347	6.22	0.37	100.00	3.64	0.61	1.21	3.90	0.00	3.90	4.000	No	Yes	2.00
348	6.24	0.39	100.00	3.55	0.61	1.21	4.38	0.00	4.38	4.000	No	Yes	2.00
349	6.26	0.44	100.00	3.40	0.60	1.21	4.97	0.00	4.97	4.000	No	Yes	2.00
350	6.28	0.48	100.00	3.30	0.60	1.20	5.76	0.00	5.76	4.000	No	Yes	2.00
351	6.30	0.47	100.00	3.31	0.60	1.20	5.73	0.00	5.73	4.000	No	Yes	2.00
352	6.32	0.41	100.00	3.41	0.60	1.20	4.56	0.00	4.56	4.000	No	Yes	2.00
353	6.34	0.35	100.00	3.52	0.61	1.20	3.67	0.00	3.67	4.000	No	Yes	2.00
354	6.36	0.33	100.00	3.53	0.61	1.20	3.59	0.00	3.59	4.000	No	Yes	2.00
355	6.38	0.33	100.00	3.50	0.61	1.20	3.96	0.00	3.96	4.000	No	Yes	2.00
356	6.40	0.34	100.00	3.49	0.61	1.20	3.70	0.00	3.70	4.000	No	Yes	2.00
357	6.42	0.35	100.00	3.46	0.61	1.20	3.72	0.00	3.72	4.000	No	Yes	2.00
358	6.44	0.41	100.00	3.35	0.60	1.20	4.49	0.00	4.49	4.000	No	Yes	2.00
359	6.46	0.46	100.00	3.28	0.60	1.20	5.63	0.00	5.63	4.000	No	Yes	2.00
360	6.48	0.46	100.00	3.29	0.60	1.19	5.36	0.00	5.36	4.000	No	Yes	2.00
361	6.50	0.44	100.00	3.36	0.60	1.19	4.67	0.00	4.67	4.000	No	Yes	2.00
362	6.52	0.44	100.00	3.37	0.60	1.19	4.70	0.00	4.70	4.000	No	Yes	2.00
363	6.54	0.49	100.00	3.29	0.60	1.19	5.54	0.00	5.54	4.000	No	Yes	2.00
364	6.56	0.55	100.00	3.20	0.60	1.19	6.22	0.00	6.22	4.000	No	Yes	2.00
365	6.58	0.60	100.00	3.16	0.59	1.19	6.90	0.00	6.90	4.000	No	Yes	2.00
366	6.60	0.65	100.00	3.15	0.59	1.19	7.37	0.00	7.37	4.000	No	Yes	2.00
367	6.62	0.67	100.00	3.16	0.59	1.18	7.65	0.00	7.65	4.000	No	Yes	2.00
368	6.64	0.70	100.00	3.16	0.59	1.18	7.86	0.00	7.86	4.000	No	Yes	2.00
369	6.67	0.71	100.00	3.19	0.59	1.18	8.18	0.00	8.18	4.000	No	Yes	2.00
370	6.68	0.71	100.00	3.21	0.59	1.18	8.05	0.00	8.05	4.000	No	Yes	2.00
371	6.70	0.70	100.00	3.25	0.59	1.18	7.84	0.00	7.84	4.000	No	Yes	2.00
372	6.72	0.68	100.00	3.28	0.59	1.18	7.78	0.00	7.78	4.000	No	Yes	2.00
373	6.74	0.67	100.00	3.31	0.59	1.18	7.41	0.00	7.41	4.000	No	Yes	2.00
374	6.76	0.65	100.00	3.34	0.59	1.18	7.33	0.00	7.33	4.000	No	Yes	2.00
375	6.78	0.64	100.00	3.37	0.59	1.17	7.06	0.00	7.06	4.000	No	Yes	2.00
376	6.80	0.64	100.00	3.36	0.59	1.17	7.00	0.00	7.00	4.000	No	Yes	2.00
377	6.82	0.65	100.00	3.35	0.59	1.17	7.49	0.00	7.49	4.000	No	Yes	2.00
378	6.84	0.68	100.00	3.31	0.59	1.17	7.40	0.00	7.40	4.000	No	Yes	2.00
379	6.86	0.69	100.00	3.28	0.59	1.17	7.86	0.00	7.86	4.000	No	Yes	2.00
380	6.88	0.71	100.00	3.24	0.59	1.17	7.87	0.00	7.87	4.000	No	Yes	2.00
381	6.90	0.72	100.00	3.21	0.59	1.17	8.02	0.00	8.02	4.000	No	Yes	2.00
382	6.92	0.71	100.00	3.20	0.59	1.16	8.07	0.00	8.07	4.000	No	Yes	2.00
383	6.94	0.70	100.00	3.21	0.59	1.16	7.72	0.00	7.72	4.000	No	Yes	2.00
384	6.96	0.67	100.00	3.24	0.59	1.16	7.54	0.00	7.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	6.98	0.65	100.00	3.27	0.59	1.16	7.15	0.00	7.15	4.000	No	Yes	2.00
386	7.00	0.63	100.00	3.30	0.59	1.16	6.93	0.00	6.93	4.000	No	Yes	2.00
387	7.02	0.61	100.00	3.32	0.60	1.16	6.77	0.00	6.77	4.000	No	Yes	2.00
388	7.05	0.60	100.00	3.33	0.60	1.16	6.51	0.00	6.51	4.000	No	Yes	2.00
389	7.06	0.58	100.00	3.35	0.60	1.16	6.40	0.00	6.40	4.000	No	Yes	2.00
390	7.08	0.59	100.00	3.33	0.60	1.16	6.29	0.00	6.29	4.000	No	Yes	2.00
391	7.10	0.62	100.00	3.28	0.60	1.16	6.67	0.00	6.67	4.000	No	Yes	2.00
392	7.12	0.69	100.00	3.20	0.59	1.15	7.61	0.00	7.61	4.000	No	Yes	2.00
393	7.14	0.76	100.00	3.13	0.59	1.15	8.34	0.00	8.34	4.000	No	Yes	2.00
394	7.16	0.82	100.00	3.08	0.59	1.15	9.02	0.00	9.02	4.000	No	Yes	2.00
395	7.18	0.90	100.00	3.03	0.58	1.15	9.82	0.00	9.82	4.000	No	Yes	2.00
396	7.20	1.02	100.00	2.97	0.58	1.14	11.05	0.00	11.05	4.000	No	Yes	2.00
397	7.22	1.16	94.72	2.90	0.57	1.14	12.68	0.00	12.68	4.000	No	Yes	2.00
398	7.24	1.26	92.72	2.87	0.57	1.14	14.47	0.00	14.47	4.000	No	Yes	2.00
399	7.26	1.31	93.58	2.88	0.57	1.14	14.33	0.00	14.33	4.000	No	Yes	2.00
400	7.28	1.26	98.01	2.94	0.57	1.14	14.16	0.00	14.16	4.000	No	Yes	2.00
401	7.30	1.21	100.00	3.00	0.57	1.14	13.03	0.00	13.03	4.000	No	Yes	2.00
402	7.32	1.16	100.00	3.05	0.57	1.14	12.64	0.00	12.64	4.000	No	Yes	2.00
403	7.34	1.15	100.00	3.09	0.57	1.13	12.45	0.00	12.45	4.000	No	Yes	2.00
404	7.36	1.14	100.00	3.10	0.57	1.13	12.34	0.00	12.34	4.000	No	Yes	2.00
405	7.38	1.15	100.00	3.10	0.57	1.13	12.55	0.00	12.55	4.000	No	Yes	2.00
406	7.40	1.15	100.00	3.09	0.57	1.13	12.48	0.00	12.48	4.000	No	Yes	2.00
407	7.42	1.15	100.00	3.09	0.57	1.13	12.47	0.00	12.47	4.000	No	Yes	2.00
408	7.44	1.14	100.00	3.08	0.57	1.13	12.28	0.00	12.28	4.000	No	Yes	2.00
409	7.46	1.16	100.00	3.06	0.57	1.13	12.39	0.00	12.39	4.000	No	Yes	2.00
410	7.48	1.20	100.00	3.02	0.57	1.13	12.95	0.00	12.95	4.000	No	Yes	2.00
411	7.50	1.27	100.00	2.98	0.57	1.12	13.70	0.00	13.70	4.000	No	Yes	2.00
412	7.52	1.32	99.08	2.95	0.57	1.12	14.48	0.00	14.48	4.000	No	Yes	2.00
413	7.54	1.33	98.68	2.95	0.57	1.12	14.41	0.00	14.41	4.000	No	Yes	2.00
414	7.56	1.31	100.00	2.97	0.57	1.12	14.22	0.00	14.22	4.000	No	Yes	2.00
415	7.58	1.25	100.00	3.00	0.57	1.12	13.59	0.00	13.59	4.000	No	Yes	2.00
416	7.60	1.19	100.00	3.04	0.57	1.12	12.66	0.00	12.66	4.000	No	Yes	2.00
417	7.62	1.13	100.00	3.07	0.57	1.12	12.08	0.00	12.08	4.000	No	Yes	2.00
418	7.64	1.09	100.00	3.09	0.58	1.12	11.72	0.00	11.72	4.000	No	Yes	2.00
419	7.66	1.06	100.00	3.09	0.58	1.12	11.31	0.00	11.31	4.000	No	Yes	2.00
420	7.68	1.04	100.00	3.08	0.58	1.12	11.00	0.00	11.00	4.000	No	Yes	2.00
421	7.70	1.02	100.00	3.06	0.58	1.11	11.06	0.00	11.06	4.000	No	Yes	2.00
422	7.72	0.98	100.00	3.06	0.58	1.11	10.48	0.00	10.48	4.000	No	Yes	2.00
423	7.74	0.92	100.00	3.08	0.58	1.11	9.66	0.00	9.66	4.000	No	Yes	2.00
424	7.76	0.86	100.00	3.12	0.59	1.11	9.08	0.00	9.08	4.000	No	Yes	2.00
425	7.78	0.81	100.00	3.15	0.59	1.11	8.41	0.00	8.41	4.000	No	Yes	2.00
426	7.80	0.77	100.00	3.19	0.59	1.11	8.08	0.00	8.08	4.000	No	Yes	2.00
427	7.82	0.74	100.00	3.21	0.59	1.11	7.80	0.00	7.80	4.000	No	Yes	2.00
428	7.84	0.72	100.00	3.23	0.59	1.11	7.38	0.00	7.38	4.000	No	Yes	2.00
429	7.86	0.76	100.00	3.18	0.59	1.11	7.35	0.00	7.35	4.000	No	Yes	2.00
430	7.88	0.81	100.00	3.15	0.58	1.11	9.32	0.00	9.32	4.000	No	Yes	2.00
431	7.90	0.83	100.00	3.14	0.59	1.11	8.73	0.00	8.73	4.000	No	Yes	2.00
432	7.92	0.78	100.00	3.19	0.59	1.10	8.18	0.00	8.18	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	7.94	0.75	100.00	3.22	0.59	1.10	7.66	0.00	7.66	4.000	No	Yes	2.00
434	7.96	0.75	100.00	3.22	0.59	1.10	7.80	0.00	7.80	4.000	No	Yes	2.00
435	7.98	0.76	100.00	3.19	0.59	1.10	8.04	0.00	8.04	4.000	No	Yes	2.00
436	8.00	0.78	100.00	3.16	0.59	1.10	8.08	0.00	8.08	4.000	No	Yes	2.00
437	8.02	0.80	100.00	3.12	0.59	1.10	8.20	0.00	8.20	4.000	No	Yes	2.00
438	8.04	0.86	100.00	3.05	0.59	1.10	8.85	0.00	8.85	4.000	No	Yes	2.00
439	8.06	0.95	100.00	2.97	0.58	1.10	9.96	0.00	9.96	4.000	No	Yes	2.00
440	8.08	0.99	98.36	2.94	0.58	1.10	10.84	0.00	10.84	4.000	No	Yes	2.00
441	8.10	0.96	100.00	2.97	0.58	1.09	10.28	0.00	10.28	4.000	No	Yes	2.00
442	8.12	0.89	100.00	3.04	0.59	1.09	8.96	0.00	8.96	4.000	No	Yes	2.00
443	8.14	0.83	100.00	3.08	0.59	1.09	8.55	0.00	8.55	4.000	No	Yes	2.00
444	8.16	0.81	100.00	3.11	0.59	1.09	8.47	0.00	8.47	4.000	No	Yes	2.00
445	8.18	0.81	100.00	3.13	0.59	1.09	8.24	0.00	8.24	4.000	No	Yes	2.00
446	8.20	0.82	100.00	3.14	0.59	1.09	8.50	0.00	8.50	4.000	No	Yes	2.00
447	8.22	0.82	100.00	3.14	0.59	1.09	8.57	0.00	8.57	4.000	No	Yes	2.00
448	8.24	0.82	100.00	3.14	0.59	1.09	8.30	0.00	8.30	4.000	No	Yes	2.00
449	8.26	0.82	100.00	3.14	0.59	1.09	8.43	0.00	8.43	4.000	No	Yes	2.00
450	8.28	0.83	100.00	3.14	0.59	1.09	8.72	0.00	8.72	4.000	No	Yes	2.00
451	8.30	0.82	100.00	3.16	0.59	1.09	8.61	0.00	8.61	4.000	No	Yes	2.00
452	8.32	0.77	100.00	3.21	0.59	1.08	8.08	0.00	8.08	4.000	No	Yes	2.00
453	8.34	0.71	100.00	3.27	0.59	1.08	7.16	0.00	7.16	4.000	No	Yes	2.00
454	8.36	0.67	100.00	3.30	0.60	1.08	6.53	0.00	6.53	4.000	No	Yes	2.00
455	8.38	0.67	100.00	3.30	0.59	1.08	6.95	0.00	6.95	4.000	No	Yes	2.00
456	8.40	0.71	100.00	3.26	0.59	1.08	7.12	0.00	7.12	4.000	No	Yes	2.00
457	8.42	0.75	100.00	3.23	0.59	1.08	7.73	0.00	7.73	4.000	No	Yes	2.00
458	8.44	0.80	100.00	3.18	0.59	1.08	8.27	0.00	8.27	4.000	No	Yes	2.00
459	8.46	0.82	100.00	3.16	0.59	1.08	8.63	0.00	8.63	4.000	No	Yes	2.00
460	8.48	0.80	100.00	3.16	0.59	1.08	8.19	0.00	8.19	4.000	No	Yes	2.00
461	8.50	0.77	100.00	3.19	0.59	1.08	7.75	0.00	7.75	4.000	No	Yes	2.00
462	8.52	0.75	100.00	3.22	0.59	1.08	7.70	0.00	7.70	4.000	No	Yes	2.00
463	8.54	0.73	100.00	3.24	0.59	1.07	7.45	0.00	7.45	4.000	No	Yes	2.00
464	8.56	0.69	100.00	3.28	0.59	1.07	7.18	0.00	7.18	4.000	No	Yes	2.00
465	8.58	0.64	100.00	3.33	0.60	1.07	6.32	0.00	6.32	4.000	No	Yes	2.00
466	8.60	0.58	100.00	3.41	0.60	1.07	5.91	0.00	5.91	4.000	No	Yes	2.00
467	8.62	0.54	100.00	3.46	0.60	1.07	5.34	0.00	5.34	4.000	No	Yes	2.00
468	8.64	0.50	100.00	3.49	0.60	1.07	4.93	0.00	4.93	4.000	No	Yes	2.00
469	8.66	0.49	100.00	3.47	0.60	1.07	4.83	0.00	4.83	4.000	No	Yes	2.00
470	8.68	0.52	100.00	3.40	0.60	1.07	5.09	0.00	5.09	4.000	No	Yes	2.00
471	8.70	0.55	100.00	3.34	0.60	1.07	5.63	0.00	5.63	4.000	No	Yes	2.00
472	8.72	0.57	100.00	3.31	0.60	1.07	5.72	0.00	5.72	4.000	No	Yes	2.00
473	8.74	0.58	100.00	3.30	0.60	1.07	5.64	0.00	5.64	4.000	No	Yes	2.00
474	8.76	0.61	100.00	3.26	0.60	1.07	5.93	0.00	5.93	4.000	No	Yes	2.00
475	8.78	0.67	100.00	3.18	0.60	1.06	6.70	0.00	6.70	4.000	No	Yes	2.00
476	8.80	0.75	100.00	3.10	0.59	1.06	7.60	0.00	7.60	4.000	No	Yes	2.00
477	8.82	0.82	100.00	3.05	0.59	1.06	8.35	0.00	8.35	4.000	No	Yes	2.00
478	8.84	0.86	100.00	3.04	0.59	1.06	8.74	0.00	8.74	4.000	No	Yes	2.00
479	8.86	0.90	100.00	3.04	0.59	1.06	8.76	0.00	8.76	4.000	No	Yes	2.00
480	8.88	0.84	100.00	3.13	0.58	1.06	9.77	0.00	9.77	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	8.90	0.76	100.00	3.23	0.59	1.06	6.85	0.00	6.85	4.000	No	Yes	2.00
482	8.92	0.64	100.00	3.34	0.60	1.06	6.19	0.00	6.19	4.000	No	Yes	2.00
483	8.94	0.65	100.00	3.31	0.60	1.06	6.21	0.00	6.21	4.000	No	Yes	2.00
484	8.96	0.66	100.00	3.28	0.59	1.06	7.00	0.00	7.00	4.000	No	Yes	2.00
485	8.98	0.68	100.00	3.24	0.60	1.06	6.53	0.00	6.53	4.000	No	Yes	2.00
486	9.00	0.66	100.00	3.23	0.60	1.05	6.80	0.00	6.80	4.000	No	Yes	2.00
487	9.02	0.65	100.00	3.23	0.60	1.05	6.42	0.00	6.42	4.000	No	Yes	2.00
488	9.04	0.62	100.00	3.26	0.60	1.05	6.04	0.00	6.04	4.000	No	Yes	2.00
489	9.06	0.63	100.00	3.25	0.60	1.05	5.97	0.00	5.97	4.000	No	Yes	2.00
490	9.08	0.67	100.00	3.20	0.60	1.05	6.67	0.00	6.67	4.000	No	Yes	2.00
491	9.10	0.73	100.00	3.14	0.59	1.05	7.29	0.00	7.29	4.000	No	Yes	2.00
492	9.12	0.79	100.00	3.09	0.59	1.05	7.84	0.00	7.84	4.000	No	Yes	2.00
493	9.14	0.86	100.00	3.04	0.59	1.05	8.47	0.00	8.47	4.000	No	Yes	2.00
494	9.16	0.97	100.00	2.97	0.58	1.05	9.50	0.00	9.50	4.000	No	Yes	2.00
495	9.18	1.14	94.11	2.89	0.58	1.05	11.01	0.00	11.01	4.000	No	Yes	2.00
496	9.20	1.32	89.32	2.83	0.57	1.04	13.59	0.00	13.59	4.000	No	Yes	2.00
497	9.22	1.43	88.88	2.82	0.57	1.04	14.97	0.00	14.97	4.000	No	Yes	2.00
498	9.24	1.40	92.32	2.87	0.57	1.04	14.47	0.00	14.47	4.000	No	Yes	2.00
499	9.26	1.29	98.22	2.94	0.57	1.04	12.91	0.00	12.91	4.000	No	Yes	2.00
500	9.28	1.16	100.00	3.02	0.58	1.04	11.47	0.00	11.47	4.000	No	Yes	2.00
501	9.30	1.05	100.00	3.08	0.58	1.04	10.42	0.00	10.42	4.000	No	Yes	2.00
502	9.32	0.97	100.00	3.13	0.58	1.04	9.72	0.00	9.72	4.000	No	Yes	2.00
503	9.34	0.96	100.00	3.13	0.59	1.04	8.76	0.00	8.76	4.000	No	Yes	2.00
504	9.36	1.01	100.00	3.09	0.58	1.04	10.28	0.00	10.28	4.000	No	Yes	2.00
505	9.38	1.09	100.00	3.05	0.58	1.04	11.25	0.00	11.25	4.000	No	Yes	2.00
506	9.40	1.14	100.00	3.03	0.58	1.04	11.13	0.00	11.13	4.000	No	Yes	2.00
507	9.42	1.19	100.00	3.01	0.58	1.03	11.81	0.00	11.81	4.000	No	Yes	2.00
508	9.44	1.23	100.00	2.99	0.57	1.03	12.69	0.00	12.69	4.000	No	Yes	2.00
509	9.46	1.18	100.00	3.02	0.57	1.03	12.24	0.00	12.24	4.000	No	Yes	2.00
510	9.48	1.03	100.00	3.13	0.58	1.03	10.42	0.00	10.42	4.000	No	Yes	2.00
511	9.50	0.85	100.00	3.27	0.59	1.03	8.12	0.00	8.12	4.000	No	Yes	2.00
512	9.52	0.71	100.00	3.39	0.60	1.03	6.50	0.00	6.50	4.000	No	Yes	2.00
513	9.54	0.65	100.00	3.43	0.60	1.03	6.29	0.00	6.29	4.000	No	Yes	2.00
514	9.56	0.65	100.00	3.42	0.60	1.03	6.40	0.00	6.40	4.000	No	Yes	2.00
515	9.58	0.67	100.00	3.37	0.60	1.03	6.32	0.00	6.32	4.000	No	Yes	2.00
516	9.60	0.69	100.00	3.32	0.59	1.03	6.88	0.00	6.88	4.000	No	Yes	2.00
517	9.62	0.72	100.00	3.26	0.59	1.03	7.06	0.00	7.06	4.000	No	Yes	2.00
518	9.64	0.73	100.00	3.22	0.59	1.03	7.19	0.00	7.19	4.000	No	Yes	2.00
519	9.66	0.71	100.00	3.24	0.59	1.02	7.14	0.00	7.14	4.000	No	Yes	2.00
520	9.68	0.66	100.00	3.30	0.60	1.02	6.31	0.00	6.31	4.000	No	Yes	2.00
521	9.70	0.63	100.00	3.35	0.60	1.02	5.92	0.00	5.92	4.000	No	Yes	2.00
522	9.72	0.64	100.00	3.33	0.60	1.02	5.98	0.00	5.98	4.000	No	Yes	2.00
523	9.74	0.67	100.00	3.29	0.60	1.02	6.59	0.00	6.59	4.000	No	Yes	2.00
524	9.76	0.70	100.00	3.26	0.59	1.02	6.88	0.00	6.88	4.000	No	Yes	2.00
525	9.78	0.72	100.00	3.24	0.59	1.02	6.92	0.00	6.92	4.000	No	Yes	2.00
526	9.80	0.85	100.00	3.11	0.59	1.02	7.01	0.00	7.01	4.000	No	Yes	2.00
527	9.82	1.19	92.13	2.86	0.58	1.02	10.71	0.00	10.71	4.000	Yes	Yes	2.00
528	9.84	1.77	74.03	2.64	0.56	1.02	17.31	0.00	17.31	4.000	Yes	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	9.86	2.38	62.96	2.50	0.54	1.02	24.25	56.23	80.48	4.000	Yes	No	2.00
530	9.88	2.86	56.47	2.42	0.53	1.01	28.74	55.79	84.53	4.000	Yes	No	2.00
531	9.90	3.09	52.20	2.36	0.53	1.01	31.76	55.23	87.00	4.000	Yes	No	2.00
532	9.92	2.98	50.85	2.35	0.53	1.01	30.93	54.52	85.46	4.000	Yes	No	2.00
533	9.94	2.54	54.24	2.39	0.55	1.01	25.56	54.24	79.79	4.000	Yes	No	2.00
534	9.96	1.95	64.08	2.51	0.56	1.01	18.53	54.85	73.38	4.000	Yes	No	2.00
535	9.98	1.47	79.84	2.71	0.58	1.01	13.43	0.00	13.43	4.000	Yes	Yes	2.00
536	10.00	1.22	95.48	2.91	0.58	1.01	11.37	0.00	11.37	4.000	Yes	Yes	2.00
537	10.03	1.12	100.00	3.01	0.58	1.01	10.98	0.00	10.98	4.000	No	Yes	2.00
538	10.04	1.20	100.00	2.99	0.58	1.01	10.30	0.00	10.30	4.000	No	Yes	2.00
539	10.06	1.40	93.56	2.88	0.57	1.01	13.65	0.00	13.65	4.000	No	Yes	2.00
540	10.08	1.61	86.14	2.79	0.56	1.01	16.75	0.00	16.75	4.000	No	Yes	2.00
541	10.10	1.65	83.97	2.76	0.56	1.01	16.47	0.00	16.47	4.000	No	Yes	2.00
542	10.12	1.54	87.17	2.80	0.57	1.01	15.02	0.00	15.02	4.000	No	Yes	2.00
543	10.15	1.44	92.47	2.87	0.57	1.00	13.57	0.00	13.57	4.000	No	Yes	2.00
544	10.16	1.37	97.15	2.93	0.57	1.00	13.32	0.00	13.32	4.000	No	Yes	2.00
545	10.18	1.37	99.38	2.95	0.57	1.00	13.15	0.00	13.15	4.000	No	Yes	2.00
546	10.20	1.38	99.89	2.96	0.57	1.00	13.40	0.00	13.40	4.000	No	Yes	2.00
547	10.22	1.36	100.00	2.98	0.57	1.00	13.55	0.00	13.55	4.000	No	Yes	2.00
548	10.24	1.27	100.00	3.04	0.57	1.00	12.71	0.00	12.71	4.000	No	Yes	2.00
549	10.26	1.10	100.00	3.14	0.58	1.00	10.61	0.00	10.61	4.000	No	Yes	2.00
550	10.28	0.92	100.00	3.26	0.59	1.00	8.70	0.00	8.70	4.000	No	Yes	2.00
551	10.30	0.80	100.00	3.34	0.59	1.00	7.27	0.00	7.27	4.000	No	Yes	2.00
552	10.32	0.76	100.00	3.37	0.59	1.00	7.22	0.00	7.22	4.000	No	Yes	2.00
553	10.34	0.75	100.00	3.37	0.59	1.00	7.37	0.00	7.37	4.000	No	Yes	2.00
554	10.36	0.75	100.00	3.35	0.59	1.00	6.96	0.00	6.96	4.000	No	Yes	2.00
555	10.38	0.75	100.00	3.33	0.59	0.99	7.24	0.00	7.24	4.000	No	Yes	2.00
556	10.40	0.78	100.00	3.28	0.59	0.99	7.41	0.00	7.41	4.000	No	Yes	2.00
557	10.42	0.81	100.00	3.22	0.59	0.99	7.64	0.00	7.64	4.000	No	Yes	2.00
558	10.44	0.85	100.00	3.19	0.59	0.99	8.30	0.00	8.30	4.000	No	Yes	2.00
559	10.46	0.88	100.00	3.17	0.59	0.99	8.38	0.00	8.38	4.000	No	Yes	2.00
560	10.48	0.90	100.00	3.18	0.59	0.99	8.59	0.00	8.59	4.000	No	Yes	2.00
561	10.50	0.93	100.00	3.17	0.59	0.99	8.89	0.00	8.89	4.000	No	Yes	2.00
562	10.52	0.96	100.00	3.16	0.59	0.99	9.30	0.00	9.30	4.000	No	Yes	2.00
563	10.54	0.99	100.00	3.15	0.58	0.99	9.42	0.00	9.42	4.000	No	Yes	2.00
564	10.56	1.00	100.00	3.15	0.58	0.99	9.52	0.00	9.52	4.000	No	Yes	2.00
565	10.58	1.01	100.00	3.15	0.58	0.99	9.80	0.00	9.80	4.000	No	Yes	2.00
566	10.60	1.00	100.00	3.17	0.58	0.99	9.51	0.00	9.51	4.000	No	Yes	2.00
567	10.62	0.94	100.00	3.21	0.59	0.99	9.13	0.00	9.13	4.000	No	Yes	2.00
568	10.64	0.87	100.00	3.28	0.59	0.98	8.20	0.00	8.20	4.000	No	Yes	2.00
569	10.66	0.79	100.00	3.35	0.59	0.98	7.29	0.00	7.29	4.000	No	Yes	2.00
570	10.68	0.74	100.00	3.39	0.59	0.98	6.85	0.00	6.85	4.000	No	Yes	2.00
571	10.70	0.73	100.00	3.40	0.59	0.98	6.84	0.00	6.84	4.000	No	Yes	2.00
572	10.72	0.72	100.00	3.39	0.59	0.98	6.88	0.00	6.88	4.000	No	Yes	2.00
573	10.74	0.70	100.00	3.40	0.60	0.98	6.67	0.00	6.67	4.000	No	Yes	2.00
574	10.76	0.67	100.00	3.42	0.60	0.98	6.15	0.00	6.15	4.000	No	Yes	2.00
575	10.78	0.64	100.00	3.44	0.60	0.98	5.94	0.00	5.94	4.000	No	Yes	2.00
576	10.80	0.62	100.00	3.44	0.60	0.98	5.74	0.00	5.74	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	10.82	0.61	100.00	3.45	0.60	0.98	5.65	0.00	5.65	4.000	No	Yes	2.00
578	10.84	0.64	100.00	3.42	0.60	0.98	5.56	0.00	5.56	4.000	No	Yes	2.00
579	10.86	0.67	100.00	3.42	0.60	0.98	6.74	0.00	6.74	4.000	No	Yes	2.00
580	10.88	0.69	100.00	3.40	0.60	0.97	6.28	0.00	6.28	4.000	No	Yes	2.00
581	10.91	0.68	100.00	3.40	0.60	0.97	6.29	0.00	6.29	4.000	No	Yes	2.00
582	10.92	0.68	100.00	3.39	0.60	0.97	6.38	0.00	6.38	4.000	No	Yes	2.00
583	10.94	0.66	100.00	3.39	0.60	0.97	6.16	0.00	6.16	4.000	No	Yes	2.00
584	10.96	0.65	100.00	3.39	0.60	0.97	5.85	0.00	5.85	4.000	No	Yes	2.00
585	10.98	0.65	100.00	3.38	0.60	0.97	5.89	0.00	5.89	4.000	No	Yes	2.00
586	11.00	0.65	100.00	3.36	0.60	0.97	6.08	0.00	6.08	4.000	No	Yes	2.00
587	11.02	0.65	100.00	3.34	0.60	0.97	5.86	0.00	5.86	4.000	No	Yes	2.00
588	11.05	0.64	100.00	3.35	0.60	0.97	5.90	0.00	5.90	4.000	No	Yes	2.00
589	11.06	0.65	100.00	3.33	0.60	0.97	5.85	0.00	5.85	4.000	No	Yes	2.00
590	11.08	0.66	100.00	3.31	0.60	0.97	6.09	0.00	6.09	4.000	No	Yes	2.00
591	11.10	0.68	100.00	3.29	0.60	0.97	6.26	0.00	6.26	4.000	No	Yes	2.00
592	11.12	0.70	100.00	3.27	0.60	0.97	6.36	0.00	6.36	4.000	No	Yes	2.00
593	11.14	0.71	100.00	3.25	0.60	0.97	6.59	0.00	6.59	4.000	No	Yes	2.00
594	11.16	0.71	100.00	3.25	0.60	0.97	6.65	0.00	6.65	4.000	No	Yes	2.00
595	11.18	0.69	100.00	3.28	0.60	0.96	6.31	0.00	6.31	4.000	No	Yes	2.00
596	11.20	0.67	100.00	3.33	0.60	0.96	6.07	0.00	6.07	4.000	No	Yes	2.00
597	11.22	0.65	100.00	3.37	0.60	0.96	5.87	0.00	5.87	4.000	No	Yes	2.00
598	11.24	0.64	100.00	3.39	0.60	0.96	5.83	0.00	5.83	4.000	No	Yes	2.00
599	11.26	0.63	100.00	3.40	0.60	0.96	5.72	0.00	5.72	4.000	No	Yes	2.00
600	11.28	0.63	100.00	3.41	0.60	0.96	5.67	0.00	5.67	4.000	No	Yes	2.00
601	11.30	0.64	100.00	3.41	0.60	0.96	5.71	0.00	5.71	4.000	No	Yes	2.00
602	11.32	0.67	100.00	3.37	0.60	0.96	5.96	0.00	5.96	4.000	No	Yes	2.00
603	11.34	0.72	100.00	3.31	0.60	0.96	6.60	0.00	6.60	4.000	No	Yes	2.00
604	11.36	0.78	100.00	3.26	0.59	0.96	7.13	0.00	7.13	4.000	No	Yes	2.00
605	11.38	0.83	100.00	3.23	0.59	0.96	7.55	0.00	7.55	4.000	No	Yes	2.00
606	11.40	0.87	100.00	3.22	0.59	0.96	7.93	0.00	7.93	4.000	No	Yes	2.00
607	11.42	0.90	100.00	3.21	0.59	0.96	8.27	0.00	8.27	4.000	No	Yes	2.00
608	11.44	0.93	100.00	3.21	0.59	0.96	8.46	0.00	8.46	4.000	No	Yes	2.00
609	11.46	0.95	100.00	3.22	0.59	0.96	8.83	0.00	8.83	4.000	No	Yes	2.00
610	11.48	0.97	100.00	3.23	0.59	0.95	8.85	0.00	8.85	4.000	No	Yes	2.00
611	11.50	0.97	100.00	3.26	0.59	0.95	9.01	0.00	9.01	4.000	No	Yes	2.00
612	11.52	0.97	100.00	3.28	0.59	0.95	8.77	0.00	8.77	4.000	No	Yes	2.00
613	11.54	0.96	100.00	3.30	0.59	0.95	8.74	0.00	8.74	4.000	No	Yes	2.00
614	11.56	0.96	100.00	3.31	0.59	0.95	8.73	0.00	8.73	4.000	No	Yes	2.00
615	11.58	0.96	100.00	3.31	0.59	0.95	8.64	0.00	8.64	4.000	No	Yes	2.00
616	11.60	0.94	100.00	3.33	0.59	0.95	8.70	0.00	8.70	4.000	No	Yes	2.00
617	11.62	0.93	100.00	3.34	0.59	0.95	8.33	0.00	8.33	4.000	No	Yes	2.00
618	11.64	0.92	100.00	3.35	0.59	0.95	8.38	0.00	8.38	4.000	No	Yes	2.00
619	11.66	0.93	100.00	3.35	0.59	0.95	8.37	0.00	8.37	4.000	No	Yes	2.00
620	11.68	0.94	100.00	3.34	0.59	0.95	8.38	0.00	8.38	4.000	No	Yes	2.00
621	11.70	0.95	100.00	3.33	0.59	0.95	8.65	0.00	8.65	4.000	No	Yes	2.00
622	11.72	0.97	100.00	3.32	0.59	0.95	8.70	0.00	8.70	4.000	No	Yes	2.00
623	11.74	0.98	100.00	3.31	0.59	0.94	8.90	0.00	8.90	4.000	No	Yes	2.00
624	11.76	0.98	100.00	3.30	0.59	0.94	8.81	0.00	8.81	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	11.78	0.97	100.00	3.29	0.59	0.94	8.70	0.00	8.70	4.000	No	Yes	2.00
626	11.80	0.97	100.00	3.27	0.59	0.94	8.71	0.00	8.71	4.000	No	Yes	2.00
627	11.82	0.98	100.00	3.25	0.59	0.94	8.87	0.00	8.87	4.000	No	Yes	2.00
628	11.84	0.99	100.00	3.24	0.59	0.94	8.92	0.00	8.92	4.000	No	Yes	2.00
629	11.86	1.00	100.00	3.23	0.59	0.94	8.89	0.00	8.89	4.000	No	Yes	2.00
630	11.89	1.00	100.00	3.23	0.59	0.94	8.96	0.00	8.96	4.000	No	Yes	2.00
631	11.90	0.99	100.00	3.23	0.59	0.94	8.81	0.00	8.81	4.000	No	Yes	2.00
632	11.92	0.97	100.00	3.24	0.59	0.94	8.56	0.00	8.56	4.000	No	Yes	2.00
633	11.94	0.95	100.00	3.25	0.59	0.94	8.57	0.00	8.57	4.000	No	Yes	2.00
634	11.96	0.94	100.00	3.26	0.59	0.94	8.31	0.00	8.31	4.000	No	Yes	2.00
635	11.98	0.91	100.00	3.27	0.59	0.94	8.01	0.00	8.01	4.000	No	Yes	2.00
636	12.00	0.87	100.00	3.29	0.59	0.94	7.72	0.00	7.72	4.000	No	Yes	2.00
637	12.02	0.85	100.00	3.29	0.59	0.93	7.40	0.00	7.40	4.000	No	Yes	2.00
638	12.04	0.83	100.00	3.29	0.59	0.93	7.41	0.00	7.41	4.000	No	Yes	2.00
639	12.06	0.82	100.00	3.28	0.59	0.93	7.22	0.00	7.22	4.000	No	Yes	2.00
640	12.08	0.81	100.00	3.29	0.59	0.93	7.11	0.00	7.11	4.000	No	Yes	2.00
641	12.10	0.79	100.00	3.29	0.59	0.93	6.85	0.00	6.85	4.000	No	Yes	2.00
642	12.12	0.78	100.00	3.28	0.60	0.93	6.77	0.00	6.77	4.000	No	Yes	2.00
643	12.14	0.78	100.00	3.27	0.60	0.93	6.78	0.00	6.78	4.000	No	Yes	2.00
644	12.16	0.78	100.00	3.26	0.59	0.93	6.82	0.00	6.82	4.000	No	Yes	2.00
645	12.18	0.78	100.00	3.25	0.60	0.93	6.73	0.00	6.73	4.000	No	Yes	2.00
646	12.20	0.76	100.00	3.26	0.60	0.93	6.69	0.00	6.69	4.000	No	Yes	2.00
647	12.22	0.76	100.00	3.27	0.60	0.93	6.48	0.00	6.48	4.000	No	Yes	2.00
648	12.24	0.75	100.00	3.28	0.60	0.93	6.50	0.00	6.50	4.000	No	Yes	2.00
649	12.26	0.75	100.00	3.27	0.60	0.93	6.53	0.00	6.53	4.000	No	Yes	2.00
650	12.28	0.76	100.00	3.26	0.60	0.93	6.51	0.00	6.51	4.000	No	Yes	2.00
651	12.30	0.77	100.00	3.25	0.60	0.93	6.61	0.00	6.61	4.000	No	Yes	2.00
652	12.32	0.80	100.00	3.23	0.59	0.92	6.85	0.00	6.85	4.000	No	Yes	2.00
653	12.34	0.81	100.00	3.22	0.59	0.92	7.20	0.00	7.20	4.000	No	Yes	2.00
654	12.36	0.80	100.00	3.24	0.59	0.92	6.89	0.00	6.89	4.000	No	Yes	2.00
655	12.38	0.76	100.00	3.27	0.60	0.92	6.56	0.00	6.56	4.000	No	Yes	2.00
656	12.40	0.73	100.00	3.30	0.60	0.92	6.33	0.00	6.33	4.000	No	Yes	2.00
657	12.42	0.71	100.00	3.31	0.60	0.92	6.04	0.00	6.04	4.000	No	Yes	2.00
658	12.44	0.70	100.00	3.33	0.60	0.92	5.95	0.00	5.95	4.000	No	Yes	2.00
659	12.46	0.70	100.00	3.32	0.60	0.92	5.93	0.00	5.93	4.000	No	Yes	2.00
660	12.48	0.70	100.00	3.33	0.60	0.92	6.01	0.00	6.01	4.000	No	Yes	2.00
661	12.50	0.71	100.00	3.33	0.60	0.92	6.03	0.00	6.03	4.000	No	Yes	2.00
662	12.52	0.69	100.00	3.35	0.60	0.92	6.11	0.00	6.11	4.000	No	Yes	2.00
663	12.54	0.67	100.00	3.37	0.60	0.92	5.65	0.00	5.65	4.000	No	Yes	2.00
664	12.56	0.64	100.00	3.42	0.60	0.92	5.49	0.00	5.49	4.000	No	Yes	2.00
665	12.58	0.64	100.00	3.42	0.60	0.92	5.22	0.00	5.22	4.000	No	Yes	2.00
666	12.60	0.66	100.00	3.38	0.60	0.92	5.58	0.00	5.58	4.000	No	Yes	2.00
667	12.62	0.71	100.00	3.31	0.60	0.92	6.17	0.00	6.17	4.000	No	Yes	2.00
668	12.64	0.74	100.00	3.28	0.60	0.92	6.54	0.00	6.54	4.000	No	Yes	2.00
669	12.66	0.72	100.00	3.31	0.60	0.91	6.21	0.00	6.21	4.000	No	Yes	2.00
670	12.68	0.68	100.00	3.35	0.60	0.91	5.59	0.00	5.59	4.000	No	Yes	2.00
671	12.70	0.66	100.00	3.37	0.60	0.91	5.51	0.00	5.51	4.000	No	Yes	2.00
672	12.72	0.67	100.00	3.35	0.60	0.91	5.67	0.00	5.67	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	12.74	0.67	100.00	3.34	0.60	0.91	5.71	0.00	5.71	4.000	No	Yes	2.00
674	12.76	0.67	100.00	3.35	0.60	0.91	5.64	0.00	5.64	4.000	No	Yes	2.00
675	12.78	0.66	100.00	3.37	0.60	0.91	5.46	0.00	5.46	4.000	No	Yes	2.00
676	12.80	0.69	100.00	3.35	0.60	0.91	5.50	0.00	5.50	4.000	No	Yes	2.00
677	12.82	0.72	100.00	3.35	0.60	0.91	6.62	0.00	6.62	4.000	No	Yes	2.00
678	12.84	0.75	100.00	3.34	0.60	0.91	6.15	0.00	6.15	4.000	No	Yes	2.00
679	12.86	0.75	100.00	3.34	0.60	0.91	6.39	0.00	6.39	4.000	No	Yes	2.00
680	12.88	0.78	100.00	3.31	0.60	0.91	6.65	0.00	6.65	4.000	No	Yes	2.00
681	12.90	0.80	100.00	3.29	0.60	0.91	6.72	0.00	6.72	4.000	No	Yes	2.00
682	12.92	0.84	100.00	3.26	0.59	0.91	7.02	0.00	7.02	4.000	No	Yes	2.00
683	12.94	0.89	100.00	3.21	0.59	0.91	7.47	0.00	7.47	4.000	No	Yes	2.00
684	12.96	0.96	100.00	3.15	0.59	0.91	8.09	0.00	8.09	4.000	No	Yes	2.00
685	12.98	1.03	100.00	3.11	0.59	0.91	8.92	0.00	8.92	4.000	No	Yes	2.00
686	13.00	1.12	100.00	3.06	0.58	0.91	9.34	0.00	9.34	4.000	No	Yes	2.00
687	13.02	1.14	100.00	3.05	0.58	0.91	10.39	0.00	10.39	4.000	No	Yes	2.00
688	13.04	1.10	100.00	3.10	0.58	0.91	9.73	0.00	9.73	4.000	No	Yes	2.00
689	13.06	0.99	100.00	3.20	0.59	0.90	8.31	0.00	8.31	4.000	No	Yes	2.00
690	13.08	0.92	100.00	3.26	0.59	0.90	7.55	0.00	7.55	4.000	No	Yes	2.00
691	13.10	0.93	100.00	3.25	0.59	0.90	7.81	0.00	7.81	4.000	No	Yes	2.00
692	13.12	0.96	100.00	3.23	0.59	0.90	8.41	0.00	8.41	4.000	No	Yes	2.00
693	13.14	1.02	100.00	3.20	0.59	0.90	8.34	0.00	8.34	4.000	No	Yes	2.00
694	13.16	1.11	100.00	3.13	0.59	0.90	9.28	0.00	9.28	4.000	No	Yes	2.00
695	13.18	1.14	100.00	3.11	0.58	0.90	10.69	0.00	10.69	4.000	No	Yes	2.00
696	13.20	1.08	100.00	3.16	0.59	0.90	9.17	0.00	9.17	4.000	No	Yes	2.00
697	13.22	0.98	100.00	3.25	0.59	0.90	7.95	0.00	7.95	4.000	No	Yes	2.00
698	13.24	0.96	100.00	3.28	0.59	0.90	8.06	0.00	8.06	4.000	No	Yes	2.00
699	13.26	0.98	100.00	3.25	0.59	0.90	8.52	0.00	8.52	4.000	No	Yes	2.00
700	13.28	0.96	100.00	3.27	0.59	0.90	8.41	0.00	8.41	4.000	No	Yes	2.00
701	13.30	0.90	100.00	3.33	0.59	0.90	7.38	0.00	7.38	4.000	No	Yes	2.00
702	13.32	0.87	100.00	3.34	0.59	0.90	6.85	0.00	6.85	4.000	No	Yes	2.00
703	13.34	0.94	100.00	3.25	0.59	0.89	7.55	0.00	7.55	4.000	No	Yes	2.00
704	13.36	1.10	100.00	3.10	0.59	0.90	9.28	0.00	9.28	4.000	No	Yes	2.00
705	13.38	1.23	100.00	3.01	0.58	0.90	10.90	0.00	10.90	4.000	No	Yes	2.00
706	13.40	1.27	100.00	3.01	0.58	0.90	11.22	0.00	11.22	4.000	No	Yes	2.00
707	13.42	1.22	100.00	3.05	0.58	0.89	10.20	0.00	10.20	4.000	No	Yes	2.00
708	13.44	1.34	100.00	3.00	0.58	0.89	9.87	0.00	9.87	4.000	No	Yes	2.00
709	13.46	1.64	92.31	2.87	0.57	0.90	14.16	0.00	14.16	4.000	No	Yes	2.00
710	13.48	2.11	81.11	2.73	0.56	0.90	18.19	0.00	18.19	4.000	No	Yes	2.00
711	13.50	2.48	74.84	2.65	0.55	0.90	22.38	0.00	22.38	4.000	No	Yes	2.00
712	13.52	2.63	71.08	2.60	0.54	0.90	24.20	0.00	24.20	4.000	No	Yes	2.00
713	13.54	2.47	70.49	2.59	0.55	0.90	22.46	57.25	79.71	0.116	No	No	0.62
714	13.56	2.13	72.74	2.62	0.56	0.89	17.96	0.00	17.96	4.000	No	Yes	2.00
715	13.58	1.72	82.64	2.75	0.57	0.89	15.01	0.00	15.01	4.000	No	Yes	2.00
716	13.60	1.42	95.13	2.90	0.58	0.89	11.73	0.00	11.73	4.000	No	Yes	2.00
717	13.62	1.21	100.00	3.05	0.58	0.89	9.81	0.00	9.81	4.000	No	Yes	2.00
718	13.64	1.10	100.00	3.13	0.59	0.89	9.12	0.00	9.12	4.000	No	Yes	2.00
719	13.66	1.02	100.00	3.19	0.59	0.89	8.54	0.00	8.54	4.000	No	Yes	2.00
720	13.68	0.96	100.00	3.24	0.59	0.88	7.70	0.00	7.70	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	13.70	0.92	100.00	3.25	0.59	0.88	7.43	0.00	7.43	4.000	No	Yes	2.00
722	13.72	0.92	100.00	3.24	0.59	0.88	7.51	0.00	7.51	4.000	No	Yes	2.00
723	13.74	0.91	100.00	3.24	0.59	0.88	7.44	0.00	7.44	4.000	No	Yes	2.00
724	13.76	0.90	100.00	3.26	0.59	0.88	7.10	0.00	7.10	4.000	No	Yes	2.00
725	13.78	0.95	100.00	3.22	0.59	0.88	7.33	0.00	7.33	4.000	No	Yes	2.00
726	13.80	1.14	100.00	3.11	0.59	0.88	8.71	0.00	8.71	4.000	No	Yes	2.00
727	13.82	1.24	100.00	3.08	0.57	0.88	12.17	0.00	12.17	4.000	No	Yes	2.00
728	13.84	1.21	100.00	3.15	0.58	0.88	10.44	0.00	10.44	4.000	No	Yes	2.00
729	13.86	1.08	100.00	3.23	0.59	0.88	8.12	0.00	8.12	4.000	No	Yes	2.00
730	13.89	1.16	100.00	3.16	0.59	0.88	8.78	0.00	8.78	4.000	No	Yes	2.00
731	13.90	1.54	98.01	2.94	0.57	0.88	12.30	0.00	12.30	4.000	No	Yes	2.00
732	13.92	1.96	86.54	2.79	0.56	0.88	18.04	0.00	18.04	4.000	No	Yes	2.00
733	13.94	2.20	82.52	2.74	0.55	0.88	19.73	0.00	19.73	4.000	No	Yes	2.00
734	13.96	2.13	85.32	2.78	0.55	0.88	18.90	0.00	18.90	4.000	No	Yes	2.00
735	13.98	1.96	88.48	2.82	0.56	0.88	16.31	0.00	16.31	4.000	No	Yes	2.00
736	14.00	1.86	89.71	2.83	0.56	0.88	15.31	0.00	15.31	4.000	No	Yes	2.00
737	14.02	1.89	88.83	2.82	0.56	0.88	16.11	0.00	16.11	4.000	No	Yes	2.00
738	14.04	1.95	89.53	2.83	0.56	0.88	17.21	0.00	17.21	4.000	No	Yes	2.00
739	14.06	2.00	90.10	2.84	0.56	0.88	16.74	0.00	16.74	4.000	No	Yes	2.00
740	14.08	2.14	88.65	2.82	0.56	0.88	17.56	0.00	17.56	4.000	No	Yes	2.00
741	14.10	2.37	83.83	2.76	0.55	0.88	20.84	0.00	20.84	4.000	No	Yes	2.00
742	14.12	2.57	79.65	2.71	0.54	0.88	22.95	0.00	22.95	4.000	No	Yes	2.00
743	14.14	2.61	77.85	2.69	0.54	0.88	22.80	0.00	22.80	4.000	No	Yes	2.00
744	14.16	2.60	77.86	2.69	0.55	0.88	21.72	0.00	21.72	4.000	No	Yes	2.00
745	14.18	2.64	78.25	2.69	0.54	0.88	22.72	0.00	22.72	4.000	No	Yes	2.00
746	14.21	2.83	76.59	2.67	0.54	0.88	23.89	0.00	23.89	4.000	Yes	Yes	2.00
747	14.22	3.06	72.71	2.62	0.53	0.88	26.66	0.00	26.66	4.000	Yes	Yes	2.00
748	14.24	3.28	67.49	2.56	0.53	0.88	28.67	58.48	87.15	4.000	Yes	No	2.00
749	14.26	3.39	63.26	2.50	0.53	0.88	29.88	57.90	87.79	4.000	Yes	No	2.00
750	14.28	3.32	61.17	2.48	0.53	0.88	29.24	57.21	86.45	4.000	Yes	No	2.00
751	14.30	3.07	61.61	2.48	0.54	0.88	26.81	56.64	83.44	4.000	Yes	No	2.00
752	14.32	2.73	65.13	2.53	0.55	0.87	23.33	56.45	79.78	4.000	Yes	No	2.00
753	14.34	2.37	73.27	2.63	0.55	0.87	20.17	0.00	20.17	4.000	Yes	Yes	2.00
754	14.37	2.13	83.09	2.75	0.56	0.87	17.45	0.00	17.45	4.000	Yes	Yes	2.00
755	14.38	2.04	89.18	2.83	0.56	0.87	16.88	0.00	16.88	4.000	Yes	Yes	2.00
756	14.40	2.16	89.05	2.83	0.56	0.87	17.92	0.00	17.92	4.000	Yes	Yes	2.00
757	14.42	2.54	81.99	2.74	0.55	0.87	20.48	0.00	20.48	4.000	Yes	Yes	2.00
758	14.44	3.03	73.12	2.63	0.53	0.87	26.66	0.00	26.66	4.000	Yes	Yes	2.00
759	14.46	3.46	65.76	2.53	0.52	0.88	30.83	58.74	89.57	4.000	Yes	No	2.00
760	14.48	3.59	62.71	2.50	0.52	0.88	31.68	58.28	89.96	4.000	Yes	No	2.00
761	14.50	3.52	61.17	2.48	0.53	0.87	30.13	57.46	87.59	0.123	No	No	0.68
762	14.52	3.33	60.29	2.47	0.53	0.87	28.67	56.83	85.50	0.121	No	No	0.66
763	14.54	3.17	57.83	2.44	0.54	0.87	26.62	55.60	82.22	0.118	No	No	0.64
764	14.56	3.11	55.51	2.41	0.54	0.87	25.98	54.75	80.73	0.117	No	No	0.63
765	14.58	3.13	55.56	2.41	0.54	0.87	26.88	55.01	81.89	4.000	Yes	No	2.00
766	14.60	3.21	59.03	2.45	0.54	0.87	27.28	56.11	83.39	4.000	Yes	No	2.00
767	14.62	3.23	64.03	2.51	0.53	0.87	27.91	57.51	85.42	4.000	Yes	No	2.00
768	14.64	3.17	68.08	2.56	0.53	0.87	27.55	58.27	85.82	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	14.66	2.95	71.82	2.61	0.54	0.87	25.72	0.00	25.72	4.000	Yes	Yes	2.00
770	14.68	2.69	76.06	2.66	0.55	0.86	22.28	0.00	22.28	4.000	Yes	Yes	2.00
771	14.70	2.47	81.29	2.73	0.55	0.86	20.55	0.00	20.55	4.000	Yes	Yes	2.00
772	14.72	2.46	84.12	2.76	0.55	0.86	20.17	0.00	20.17	4.000	Yes	Yes	2.00
773	14.74	2.55	84.86	2.77	0.54	0.86	21.87	0.00	21.87	4.000	No	Yes	2.00
774	14.76	2.74	83.71	2.76	0.54	0.86	23.03	0.00	23.03	4.000	No	Yes	2.00
775	14.78	2.94	79.77	2.71	0.54	0.86	24.85	0.00	24.85	4.000	No	Yes	2.00
776	14.80	3.10	77.19	2.68	0.53	0.86	27.24	0.00	27.24	4.000	No	Yes	2.00
777	14.82	3.06	76.41	2.67	0.53	0.86	27.15	0.00	27.15	4.000	No	Yes	2.00
778	14.84	2.80	81.16	2.73	0.54	0.86	23.72	0.00	23.72	4.000	No	Yes	2.00
779	14.86	2.42	87.12	2.80	0.55	0.86	20.31	0.00	20.31	4.000	No	Yes	2.00
780	14.88	2.04	94.86	2.90	0.56	0.86	17.37	0.00	17.37	4.000	No	Yes	2.00
781	14.90	1.92	97.01	2.93	0.57	0.85	14.02	0.00	14.02	4.000	No	Yes	2.00
782	14.92	2.06	91.79	2.86	0.56	0.85	16.94	0.00	16.94	4.000	No	Yes	2.00
783	14.94	2.28	86.23	2.79	0.55	0.86	20.83	0.00	20.83	4.000	No	Yes	2.00
784	14.96	2.17	88.33	2.82	0.55	0.86	19.52	0.00	19.52	4.000	No	Yes	2.00
785	14.98	1.77	99.11	2.95	0.57	0.85	14.13	0.00	14.13	4.000	No	Yes	2.00
786	15.00	1.30	100.00	3.16	0.58	0.85	10.73	0.00	10.73	4.000	No	Yes	2.00
787	15.02	1.04	100.00	3.32	0.59	0.84	7.40	0.00	7.40	4.000	No	Yes	2.00
788	15.04	0.93	100.00	3.41	0.59	0.84	7.32	0.00	7.32	4.000	No	Yes	2.00
789	15.06	0.94	100.00	3.38	0.59	0.84	7.58	0.00	7.58	4.000	No	Yes	2.00
790	15.08	0.93	100.00	3.40	0.59	0.84	7.53	0.00	7.53	4.000	No	Yes	2.00
791	15.10	0.91	100.00	3.42	0.59	0.84	7.13	0.00	7.13	4.000	No	Yes	2.00
792	15.12	0.89	100.00	3.44	0.59	0.84	6.97	0.00	6.97	4.000	No	Yes	2.00
793	15.15	0.88	100.00	3.42	0.59	0.84	6.85	0.00	6.85	4.000	No	Yes	2.00
794	15.16	0.89	100.00	3.38	0.59	0.84	6.94	0.00	6.94	4.000	No	Yes	2.00
795	15.18	0.91	100.00	3.34	0.59	0.84	7.08	0.00	7.08	4.000	No	Yes	2.00
796	15.20	0.93	100.00	3.31	0.59	0.84	7.36	0.00	7.36	4.000	No	Yes	2.00
797	15.22	0.93	100.00	3.30	0.59	0.84	7.39	0.00	7.39	4.000	No	Yes	2.00
798	15.24	0.92	100.00	3.30	0.59	0.84	7.16	0.00	7.16	4.000	No	Yes	2.00
799	15.26	0.92	100.00	3.31	0.59	0.84	7.16	0.00	7.16	4.000	No	Yes	2.00
800	15.28	0.93	100.00	3.31	0.59	0.84	7.23	0.00	7.23	4.000	No	Yes	2.00
801	15.30	0.95	100.00	3.30	0.59	0.84	7.51	0.00	7.51	4.000	No	Yes	2.00
802	15.32	0.95	100.00	3.30	0.59	0.84	7.58	0.00	7.58	4.000	No	Yes	2.00
803	15.34	0.91	100.00	3.35	0.59	0.83	7.26	0.00	7.26	4.000	No	Yes	2.00
804	15.36	0.86	100.00	3.39	0.60	0.83	6.35	0.00	6.35	4.000	No	Yes	2.00
805	15.38	0.85	100.00	3.39	0.60	0.83	6.41	0.00	6.41	4.000	No	Yes	2.00
806	15.40	0.91	100.00	3.32	0.59	0.83	6.89	0.00	6.89	4.000	No	Yes	2.00
807	15.42	1.03	100.00	3.21	0.59	0.83	7.84	0.00	7.84	4.000	No	Yes	2.00
808	15.44	1.18	100.00	3.11	0.58	0.83	9.40	0.00	9.40	4.000	No	Yes	2.00
809	15.46	1.33	100.00	3.04	0.58	0.84	10.52	0.00	10.52	4.000	No	Yes	2.00
810	15.48	1.44	100.00	3.01	0.58	0.84	11.59	0.00	11.59	4.000	No	Yes	2.00
811	15.50	1.54	100.00	2.99	0.57	0.84	12.30	0.00	12.30	4.000	No	Yes	2.00
812	15.52	1.56	100.00	3.01	0.57	0.84	13.03	0.00	13.03	4.000	No	Yes	2.00
813	15.54	1.46	100.00	3.09	0.57	0.84	12.29	0.00	12.29	4.000	No	Yes	2.00
814	15.56	1.31	100.00	3.20	0.58	0.83	10.09	0.00	10.09	4.000	No	Yes	2.00
815	15.58	1.19	100.00	3.29	0.59	0.83	9.26	0.00	9.26	4.000	No	Yes	2.00
816	15.60	1.22	100.00	3.27	0.58	0.83	10.02	0.00	10.02	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.07	2.00	0.00	9.97	0.03	0.00	0.08	2.00	0.00	9.96	0.01	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.19	2.00	0.00	9.91	0.03	0.00	0.20	2.00	0.00	9.90	0.01	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.02	2.00	0.00	9.99	0.70	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.63	2.00	0.00	9.19	0.03	0.00	1.64	2.00	0.00	9.18	0.01	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.01	2.00	0.00	8.99	0.03	0.00
2.02	2.00	0.00	8.99	0.01	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.09	2.00	0.00	8.46	0.03	0.00
3.10	2.00	0.00	8.45	0.01	0.00	3.12	2.00	0.00	8.44	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.21	2.00	0.00	8.40	0.03	0.00
3.22	2.00	0.00	8.39	0.01	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.04	2.00	0.00	7.98	0.02	0.00
4.06	2.00	0.00	7.97	0.02	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.61	2.00	0.00	7.70	0.03	0.00
4.62	2.00	0.00	7.69	0.01	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.51	2.00	0.00	7.25	0.03	0.00	5.52	2.00	0.00	7.24	0.01	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.95	2.00	0.00	7.03	0.03	0.00	5.96	2.00	0.00	7.02	0.01	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.67	2.00	0.00	6.67	0.03	0.00	6.68	2.00	0.00	6.66	0.01	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.05	2.00	0.00	6.48	0.03	0.00
7.06	2.00	0.00	6.47	0.01	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.03	2.00	0.00	4.99	0.03	0.00	10.04	2.00	0.00	4.98	0.01	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.15	2.00	0.00	4.93	0.03	0.00	10.16	2.00	0.00	4.92	0.01	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.91	2.00	0.00	4.55	0.03	0.00	10.92	2.00	0.00	4.54	0.01	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.05	2.00	0.00	4.47	0.03	0.00
11.06	2.00	0.00	4.47	0.01	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.89	2.00	0.00	4.06	0.03	0.00
11.90	2.00	0.00	4.05	0.01	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.20	2.00	0.00	3.40	0.02	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	0.62	0.38	3.23	0.02	0.02	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.82	2.00	0.00	3.09	0.02	0.00	13.84	2.00	0.00	3.08	0.02	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.89	2.00	0.00	3.06	0.03	0.00
13.90	2.00	0.00	3.05	0.01	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.21	2.00	0.00	2.90	0.03	0.00
14.22	2.00	0.00	2.89	0.01	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.37	2.00	0.00	2.82	0.03	0.00
14.38	2.00	0.00	2.81	0.01	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	0.68	0.32	2.75	0.02	0.02	14.52	0.66	0.34	2.74	0.02	0.02
14.54	0.64	0.36	2.73	0.02	0.02	14.56	0.63	0.37	2.72	0.02	0.02
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.80	2.00	0.00	2.60	0.02	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.84	2.00	0.00	2.58	0.02	0.00
14.86	2.00	0.00	2.57	0.02	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.00	2.00	0.00	2.50	0.02	0.00
15.02	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.15	2.00	0.00	2.42	0.03	0.00	15.16	2.00	0.00	2.42	0.01	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00

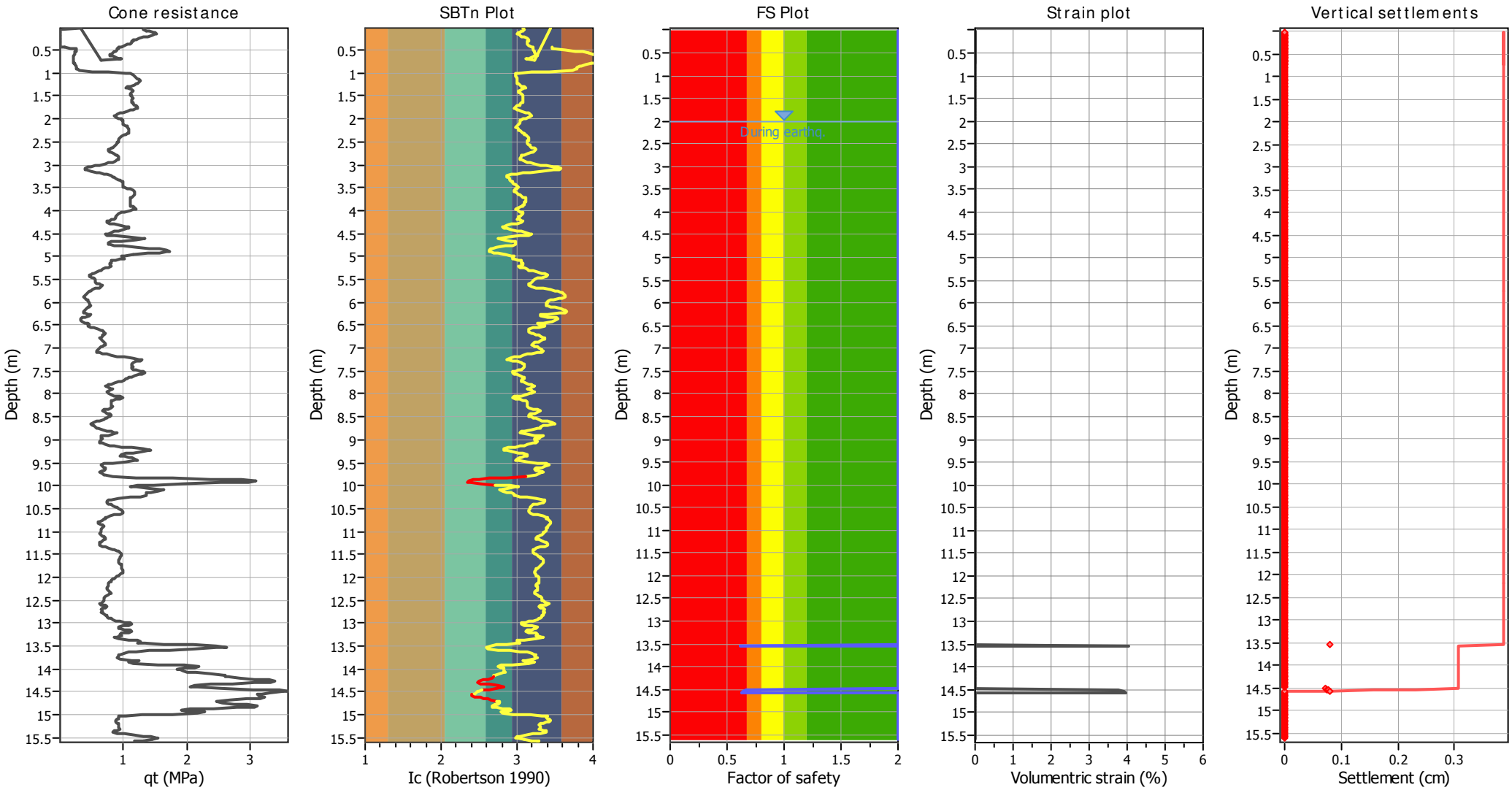
Overall liquefaction potential: 0.10

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.01	15.43	2.00	0.00	1.00	0.00	2.02	15.54	2.00	0.00	1.00	0.00
2.04	15.84	2.00	0.00	1.00	0.00	2.06	16.06	2.00	0.00	1.00	0.00
2.08	15.79	2.00	0.00	1.00	0.00	2.10	15.76	2.00	0.00	1.00	0.00
2.12	15.93	2.00	0.00	1.00	0.00	2.14	16.21	2.00	0.00	1.00	0.00
2.16	16.93	2.00	0.00	1.00	0.00	2.18	16.92	2.00	0.00	1.00	0.00
2.20	16.49	2.00	0.00	1.00	0.00	2.22	16.76	2.00	0.00	1.00	0.00
2.24	16.78	2.00	0.00	1.00	0.00	2.26	16.87	2.00	0.00	1.00	0.00
2.28	16.79	2.00	0.00	1.00	0.00	2.30	16.40	2.00	0.00	1.00	0.00
2.32	15.88	2.00	0.00	1.00	0.00	2.34	15.80	2.00	0.00	1.00	0.00
2.36	15.29	2.00	0.00	1.00	0.00	2.38	14.46	2.00	0.00	1.00	0.00
2.40	14.29	2.00	0.00	1.00	0.00	2.42	13.81	2.00	0.00	1.00	0.00
2.44	13.78	2.00	0.00	1.00	0.00	2.46	13.51	2.00	0.00	1.00	0.00
2.48	13.44	2.00	0.00	1.00	0.00	2.50	13.48	2.00	0.00	1.00	0.00
2.52	13.08	2.00	0.00	1.00	0.00	2.54	12.98	2.00	0.00	1.00	0.00
2.56	12.91	2.00	0.00	1.00	0.00	2.58	12.55	2.00	0.00	1.00	0.00
2.60	12.38	2.00	0.00	1.00	0.00	2.62	11.99	2.00	0.00	1.00	0.00
2.64	11.56	2.00	0.00	1.00	0.00	2.66	11.20	2.00	0.00	1.00	0.00
2.68	10.84	2.00	0.00	1.00	0.00	2.70	11.05	2.00	0.00	1.00	0.00
2.72	11.05	2.00	0.00	1.00	0.00	2.74	11.65	2.00	0.00	1.00	0.00
2.76	12.08	2.00	0.00	1.00	0.00	2.78	12.81	2.00	0.00	1.00	0.00
2.80	12.94	2.00	0.00	1.00	0.00	2.82	12.95	2.00	0.00	1.00	0.00
2.84	13.08	2.00	0.00	1.00	0.00	2.86	13.06	2.00	0.00	1.00	0.00
2.88	13.06	2.00	0.00	1.00	0.00	2.90	12.84	2.00	0.00	1.00	0.00
2.92	12.24	2.00	0.00	1.00	0.00	2.94	11.73	2.00	0.00	1.00	0.00
2.96	10.78	2.00	0.00	1.00	0.00	2.98	9.76	2.00	0.00	1.00	0.00
3.00	9.03	2.00	0.00	1.00	0.00	3.02	7.67	2.00	0.00	1.00	0.00
3.04	6.48	2.00	0.00	1.00	0.00	3.06	5.77	2.00	0.00	1.00	0.00
3.09	5.40	2.00	0.00	1.00	0.00	3.10	5.06	2.00	0.00	1.00	0.00
3.12	5.58	2.00	0.00	1.00	0.00	3.14	6.32	2.00	0.00	1.00	0.00
3.16	8.10	2.00	0.00	1.00	0.00	3.18	8.98	2.00	0.00	1.00	0.00
3.21	8.96	2.00	0.00	1.00	0.00	3.22	10.24	2.00	0.00	1.00	0.00
3.24	11.13	2.00	0.00	1.00	0.00	3.26	11.78	2.00	0.00	1.00	0.00
3.28	11.57	2.00	0.00	1.00	0.00	3.30	12.06	2.00	0.00	1.00	0.00
3.32	12.36	2.00	0.00	1.00	0.00	3.34	12.91	2.00	0.00	1.00	0.00
3.36	13.42	2.00	0.00	1.00	0.00	3.38	13.37	2.00	0.00	1.00	0.00
3.40	13.45	2.00	0.00	1.00	0.00	3.42	13.61	2.00	0.00	1.00	0.00
3.44	13.44	2.00	0.00	1.00	0.00	3.46	13.18	2.00	0.00	1.00	0.00
3.48	13.28	2.00	0.00	1.00	0.00	3.50	13.75	2.00	0.00	1.00	0.00
3.52	14.10	2.00	0.00	1.00	0.00	3.54	14.78	2.00	0.00	1.00	0.00
3.56	15.55	2.00	0.00	1.00	0.00	3.58	15.62	2.00	0.00	1.00	0.00
3.60	15.81	2.00	0.00	1.00	0.00	3.62	15.93	2.00	0.00	1.00	0.00
3.64	15.72	2.00	0.00	1.00	0.00	3.66	15.69	2.00	0.00	1.00	0.00
3.68	15.58	2.00	0.00	1.00	0.00	3.70	14.98	2.00	0.00	1.00	0.00
3.72	14.56	2.00	0.00	1.00	0.00	3.74	14.53	2.00	0.00	1.00	0.00
3.76	14.50	2.00	0.00	1.00	0.00	3.78	14.80	2.00	0.00	1.00	0.00
3.80	14.56	2.00	0.00	1.00	0.00	3.82	14.35	2.00	0.00	1.00	0.00
3.84	14.77	2.00	0.00	1.00	0.00	3.86	14.44	2.00	0.00	1.00	0.00
3.88	14.65	2.00	0.00	1.00	0.00	3.90	14.59	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.92	14.47	2.00	0.00	1.00	0.00	3.94	15.85	2.00	0.00	1.00	0.00
3.96	15.38	2.00	0.00	1.00	0.00	3.98	15.15	2.00	0.00	1.00	0.00
4.00	14.46	2.00	0.00	1.00	0.00	4.02	13.07	2.00	0.00	1.00	0.00
4.04	12.22	2.00	0.00	1.00	0.00	4.06	12.00	2.00	0.00	1.00	0.00
4.08	11.77	2.00	0.00	1.00	0.00	4.10	11.46	2.00	0.00	1.00	0.00
4.12	11.41	2.00	0.00	1.00	0.00	4.14	11.21	2.00	0.00	1.00	0.00
4.16	11.46	2.00	0.00	1.00	0.00	4.18	10.74	2.00	0.00	1.00	0.00
4.20	10.64	2.00	0.00	1.00	0.00	4.22	9.86	2.00	0.00	1.00	0.00
4.24	9.40	2.00	0.00	1.00	0.00	4.26	9.21	2.00	0.00	1.00	0.00
4.28	9.85	2.00	0.00	1.00	0.00	4.30	10.75	2.00	0.00	1.00	0.00
4.32	12.10	2.00	0.00	1.00	0.00	4.34	13.40	2.00	0.00	1.00	0.00
4.36	13.88	2.00	0.00	1.00	0.00	4.38	13.95	2.00	0.00	1.00	0.00
4.40	13.35	2.00	0.00	1.00	0.00	4.42	12.72	2.00	0.00	1.00	0.00
4.44	11.58	2.00	0.00	1.00	0.00	4.46	10.96	2.00	0.00	1.00	0.00
4.48	10.08	2.00	0.00	1.00	0.00	4.50	9.46	2.00	0.00	1.00	0.00
4.52	8.81	2.00	0.00	1.00	0.00	4.54	8.74	2.00	0.00	1.00	0.00
4.56	10.21	2.00	0.00	1.00	0.00	4.58	13.26	2.00	0.00	1.00	0.00
4.61	16.94	2.00	0.00	1.00	0.00	4.62	18.04	2.00	0.00	1.00	0.00
4.64	15.10	2.00	0.00	1.00	0.00	4.66	11.45	2.00	0.00	1.00	0.00
4.68	9.69	2.00	0.00	1.00	0.00	4.70	9.22	2.00	0.00	1.00	0.00
4.72	9.53	2.00	0.00	1.00	0.00	4.74	9.43	2.00	0.00	1.00	0.00
4.76	10.03	2.00	0.00	1.00	0.00	4.78	11.94	2.00	0.00	1.00	0.00
4.80	15.14	2.00	0.00	1.00	0.00	4.82	17.65	2.00	0.00	1.00	0.00
4.84	19.17	2.00	0.00	1.00	0.00	4.86	21.04	2.00	0.00	1.00	0.00
4.88	21.95	2.00	0.00	1.00	0.00	4.90	20.80	2.00	0.00	1.00	0.00
4.92	19.93	2.00	0.00	1.00	0.00	4.94	17.13	2.00	0.00	1.00	0.00
4.96	14.07	2.00	0.00	1.00	0.00	4.98	11.92	2.00	0.00	1.00	0.00
5.00	11.73	2.00	0.00	1.00	0.00	5.02	12.28	2.00	0.00	1.00	0.00
5.04	12.52	2.00	0.00	1.00	0.00	5.06	12.11	2.00	0.00	1.00	0.00
5.08	10.36	2.00	0.00	1.00	0.00	5.10	9.59	2.00	0.00	1.00	0.00
5.12	9.86	2.00	0.00	1.00	0.00	5.14	10.10	2.00	0.00	1.00	0.00
5.16	9.50	2.00	0.00	1.00	0.00	5.18	9.18	2.00	0.00	1.00	0.00
5.20	9.89	2.00	0.00	1.00	0.00	5.22	9.83	2.00	0.00	1.00	0.00
5.24	9.84	2.00	0.00	1.00	0.00	5.26	8.19	2.00	0.00	1.00	0.00
5.28	8.21	2.00	0.00	1.00	0.00	5.30	7.81	2.00	0.00	1.00	0.00
5.32	7.44	2.00	0.00	1.00	0.00	5.34	6.90	2.00	0.00	1.00	0.00
5.36	6.42	2.00	0.00	1.00	0.00	5.38	6.08	2.00	0.00	1.00	0.00
5.40	5.74	2.00	0.00	1.00	0.00	5.42	5.32	2.00	0.00	1.00	0.00
5.44	5.59	2.00	0.00	1.00	0.00	5.46	5.90	2.00	0.00	1.00	0.00
5.48	6.17	2.00	0.00	1.00	0.00	5.51	6.49	2.00	0.00	1.00	0.00
5.52	6.66	2.00	0.00	1.00	0.00	5.54	6.54	2.00	0.00	1.00	0.00
5.56	6.45	2.00	0.00	1.00	0.00	5.58	6.92	2.00	0.00	1.00	0.00
5.60	7.38	2.00	0.00	1.00	0.00	5.62	7.84	2.00	0.00	1.00	0.00
5.64	7.92	2.00	0.00	1.00	0.00	5.66	7.91	2.00	0.00	1.00	0.00
5.68	7.39	2.00	0.00	1.00	0.00	5.70	6.62	2.00	0.00	1.00	0.00
5.72	6.01	2.00	0.00	1.00	0.00	5.74	5.60	2.00	0.00	1.00	0.00
5.76	5.43	2.00	0.00	1.00	0.00	5.78	5.37	2.00	0.00	1.00	0.00
5.80	4.98	2.00	0.00	1.00	0.00	5.82	4.93	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.84	4.62	2.00	0.00	1.00	0.00	5.86	4.45	2.00	0.00	1.00	0.00
5.88	4.45	2.00	0.00	1.00	0.00	5.90	4.34	2.00	0.00	1.00	0.00
5.92	4.57	2.00	0.00	1.00	0.00	5.95	4.84	2.00	0.00	1.00	0.00
5.96	5.14	2.00	0.00	1.00	0.00	5.98	5.10	2.00	0.00	1.00	0.00
6.00	5.34	2.00	0.00	1.00	0.00	6.02	5.34	2.00	0.00	1.00	0.00
6.04	5.63	2.00	0.00	1.00	0.00	6.06	5.49	2.00	0.00	1.00	0.00
6.08	5.51	2.00	0.00	1.00	0.00	6.10	5.56	2.00	0.00	1.00	0.00
6.12	5.16	2.00	0.00	1.00	0.00	6.14	4.72	2.00	0.00	1.00	0.00
6.16	4.66	2.00	0.00	1.00	0.00	6.18	4.58	2.00	0.00	1.00	0.00
6.20	4.20	2.00	0.00	1.00	0.00	6.22	3.90	2.00	0.00	1.00	0.00
6.24	4.38	2.00	0.00	1.00	0.00	6.26	4.97	2.00	0.00	1.00	0.00
6.28	5.76	2.00	0.00	1.00	0.00	6.30	5.73	2.00	0.00	1.00	0.00
6.32	4.56	2.00	0.00	1.00	0.00	6.34	3.67	2.00	0.00	1.00	0.00
6.36	3.59	2.00	0.00	1.00	0.00	6.38	3.96	2.00	0.00	1.00	0.00
6.40	3.70	2.00	0.00	1.00	0.00	6.42	3.72	2.00	0.00	1.00	0.00
6.44	4.49	2.00	0.00	1.00	0.00	6.46	5.63	2.00	0.00	1.00	0.00
6.48	5.36	2.00	0.00	1.00	0.00	6.50	4.67	2.00	0.00	1.00	0.00
6.52	4.70	2.00	0.00	1.00	0.00	6.54	5.54	2.00	0.00	1.00	0.00
6.56	6.22	2.00	0.00	1.00	0.00	6.58	6.90	2.00	0.00	1.00	0.00
6.60	7.37	2.00	0.00	1.00	0.00	6.62	7.65	2.00	0.00	1.00	0.00
6.64	7.86	2.00	0.00	1.00	0.00	6.67	8.18	2.00	0.00	1.00	0.00
6.68	8.05	2.00	0.00	1.00	0.00	6.70	7.84	2.00	0.00	1.00	0.00
6.72	7.78	2.00	0.00	1.00	0.00	6.74	7.41	2.00	0.00	1.00	0.00
6.76	7.33	2.00	0.00	1.00	0.00	6.78	7.06	2.00	0.00	1.00	0.00
6.80	7.00	2.00	0.00	1.00	0.00	6.82	7.49	2.00	0.00	1.00	0.00
6.84	7.40	2.00	0.00	1.00	0.00	6.86	7.86	2.00	0.00	1.00	0.00
6.88	7.87	2.00	0.00	1.00	0.00	6.90	8.02	2.00	0.00	1.00	0.00
6.92	8.07	2.00	0.00	1.00	0.00	6.94	7.72	2.00	0.00	1.00	0.00
6.96	7.54	2.00	0.00	1.00	0.00	6.98	7.15	2.00	0.00	1.00	0.00
7.00	6.93	2.00	0.00	1.00	0.00	7.02	6.77	2.00	0.00	1.00	0.00
7.05	6.51	2.00	0.00	1.00	0.00	7.06	6.40	2.00	0.00	1.00	0.00
7.08	6.29	2.00	0.00	1.00	0.00	7.10	6.67	2.00	0.00	1.00	0.00
7.12	7.61	2.00	0.00	1.00	0.00	7.14	8.34	2.00	0.00	1.00	0.00
7.16	9.02	2.00	0.00	1.00	0.00	7.18	9.82	2.00	0.00	1.00	0.00
7.20	11.05	2.00	0.00	1.00	0.00	7.22	12.68	2.00	0.00	1.00	0.00
7.24	14.47	2.00	0.00	1.00	0.00	7.26	14.33	2.00	0.00	1.00	0.00
7.28	14.16	2.00	0.00	1.00	0.00	7.30	13.03	2.00	0.00	1.00	0.00
7.32	12.64	2.00	0.00	1.00	0.00	7.34	12.45	2.00	0.00	1.00	0.00
7.36	12.34	2.00	0.00	1.00	0.00	7.38	12.55	2.00	0.00	1.00	0.00
7.40	12.48	2.00	0.00	1.00	0.00	7.42	12.47	2.00	0.00	1.00	0.00
7.44	12.28	2.00	0.00	1.00	0.00	7.46	12.39	2.00	0.00	1.00	0.00
7.48	12.95	2.00	0.00	1.00	0.00	7.50	13.70	2.00	0.00	1.00	0.00
7.52	14.48	2.00	0.00	1.00	0.00	7.54	14.41	2.00	0.00	1.00	0.00
7.56	14.22	2.00	0.00	1.00	0.00	7.58	13.59	2.00	0.00	1.00	0.00
7.60	12.66	2.00	0.00	1.00	0.00	7.62	12.08	2.00	0.00	1.00	0.00
7.64	11.72	2.00	0.00	1.00	0.00	7.66	11.31	2.00	0.00	1.00	0.00
7.68	11.00	2.00	0.00	1.00	0.00	7.70	11.06	2.00	0.00	1.00	0.00
7.72	10.48	2.00	0.00	1.00	0.00	7.74	9.66	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.76	9.08	2.00	0.00	1.00	0.00	7.78	8.41	2.00	0.00	1.00	0.00
7.80	8.08	2.00	0.00	1.00	0.00	7.82	7.80	2.00	0.00	1.00	0.00
7.84	7.38	2.00	0.00	1.00	0.00	7.86	7.35	2.00	0.00	1.00	0.00
7.88	9.32	2.00	0.00	1.00	0.00	7.90	8.73	2.00	0.00	1.00	0.00
7.92	8.18	2.00	0.00	1.00	0.00	7.94	7.66	2.00	0.00	1.00	0.00
7.96	7.80	2.00	0.00	1.00	0.00	7.98	8.04	2.00	0.00	1.00	0.00
8.00	8.08	2.00	0.00	1.00	0.00	8.02	8.20	2.00	0.00	1.00	0.00
8.04	8.85	2.00	0.00	1.00	0.00	8.06	9.96	2.00	0.00	1.00	0.00
8.08	10.84	2.00	0.00	1.00	0.00	8.10	10.28	2.00	0.00	1.00	0.00
8.12	8.96	2.00	0.00	1.00	0.00	8.14	8.55	2.00	0.00	1.00	0.00
8.16	8.47	2.00	0.00	1.00	0.00	8.18	8.24	2.00	0.00	1.00	0.00
8.20	8.50	2.00	0.00	1.00	0.00	8.22	8.57	2.00	0.00	1.00	0.00
8.24	8.30	2.00	0.00	1.00	0.00	8.26	8.43	2.00	0.00	1.00	0.00
8.28	8.72	2.00	0.00	1.00	0.00	8.30	8.61	2.00	0.00	1.00	0.00
8.32	8.08	2.00	0.00	1.00	0.00	8.34	7.16	2.00	0.00	1.00	0.00
8.36	6.53	2.00	0.00	1.00	0.00	8.38	6.95	2.00	0.00	1.00	0.00
8.40	7.12	2.00	0.00	1.00	0.00	8.42	7.73	2.00	0.00	1.00	0.00
8.44	8.27	2.00	0.00	1.00	0.00	8.46	8.63	2.00	0.00	1.00	0.00
8.48	8.19	2.00	0.00	1.00	0.00	8.50	7.75	2.00	0.00	1.00	0.00
8.52	7.70	2.00	0.00	1.00	0.00	8.54	7.45	2.00	0.00	1.00	0.00
8.56	7.18	2.00	0.00	1.00	0.00	8.58	6.32	2.00	0.00	1.00	0.00
8.60	5.91	2.00	0.00	1.00	0.00	8.62	5.34	2.00	0.00	1.00	0.00
8.64	4.93	2.00	0.00	1.00	0.00	8.66	4.83	2.00	0.00	1.00	0.00
8.68	5.09	2.00	0.00	1.00	0.00	8.70	5.63	2.00	0.00	1.00	0.00
8.72	5.72	2.00	0.00	1.00	0.00	8.74	5.64	2.00	0.00	1.00	0.00
8.76	5.93	2.00	0.00	1.00	0.00	8.78	6.70	2.00	0.00	1.00	0.00
8.80	7.60	2.00	0.00	1.00	0.00	8.82	8.35	2.00	0.00	1.00	0.00
8.84	8.74	2.00	0.00	1.00	0.00	8.86	8.76	2.00	0.00	1.00	0.00
8.88	9.77	2.00	0.00	1.00	0.00	8.90	6.85	2.00	0.00	1.00	0.00
8.92	6.19	2.00	0.00	1.00	0.00	8.94	6.21	2.00	0.00	1.00	0.00
8.96	7.00	2.00	0.00	1.00	0.00	8.98	6.53	2.00	0.00	1.00	0.00
9.00	6.80	2.00	0.00	1.00	0.00	9.02	6.42	2.00	0.00	1.00	0.00
9.04	6.04	2.00	0.00	1.00	0.00	9.06	5.97	2.00	0.00	1.00	0.00
9.08	6.67	2.00	0.00	1.00	0.00	9.10	7.29	2.00	0.00	1.00	0.00
9.12	7.84	2.00	0.00	1.00	0.00	9.14	8.47	2.00	0.00	1.00	0.00
9.16	9.50	2.00	0.00	1.00	0.00	9.18	11.01	2.00	0.00	1.00	0.00
9.20	13.59	2.00	0.00	1.00	0.00	9.22	14.97	2.00	0.00	1.00	0.00
9.24	14.47	2.00	0.00	1.00	0.00	9.26	12.91	2.00	0.00	1.00	0.00
9.28	11.47	2.00	0.00	1.00	0.00	9.30	10.42	2.00	0.00	1.00	0.00
9.32	9.72	2.00	0.00	1.00	0.00	9.34	8.76	2.00	0.00	1.00	0.00
9.36	10.28	2.00	0.00	1.00	0.00	9.38	11.25	2.00	0.00	1.00	0.00
9.40	11.13	2.00	0.00	1.00	0.00	9.42	11.81	2.00	0.00	1.00	0.00
9.44	12.69	2.00	0.00	1.00	0.00	9.46	12.24	2.00	0.00	1.00	0.00
9.48	10.42	2.00	0.00	1.00	0.00	9.50	8.12	2.00	0.00	1.00	0.00
9.52	6.50	2.00	0.00	1.00	0.00	9.54	6.29	2.00	0.00	1.00	0.00
9.56	6.40	2.00	0.00	1.00	0.00	9.58	6.32	2.00	0.00	1.00	0.00
9.60	6.88	2.00	0.00	1.00	0.00	9.62	7.06	2.00	0.00	1.00	0.00
9.64	7.19	2.00	0.00	1.00	0.00	9.66	7.14	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.68	6.31	2.00	0.00	1.00	0.00	9.70	5.92	2.00	0.00	1.00	0.00
9.72	5.98	2.00	0.00	1.00	0.00	9.74	6.59	2.00	0.00	1.00	0.00
9.76	6.88	2.00	0.00	1.00	0.00	9.78	6.92	2.00	0.00	1.00	0.00
9.80	7.01	2.00	0.00	1.00	0.00	9.82	10.71	2.00	0.00	1.00	0.00
9.84	17.31	2.00	0.00	1.00	0.00	9.86	80.48	2.00	0.00	1.00	0.00
9.88	84.53	2.00	0.00	1.00	0.00	9.90	87.00	2.00	0.00	1.00	0.00
9.92	85.46	2.00	0.00	1.00	0.00	9.94	79.79	2.00	0.00	1.00	0.00
9.96	73.38	2.00	0.00	1.00	0.00	9.98	13.43	2.00	0.00	1.00	0.00
10.00	11.37	2.00	0.00	1.00	0.00	10.03	10.98	2.00	0.00	1.00	0.00
10.04	10.30	2.00	0.00	1.00	0.00	10.06	13.65	2.00	0.00	1.00	0.00
10.08	16.75	2.00	0.00	1.00	0.00	10.10	16.47	2.00	0.00	1.00	0.00
10.12	15.02	2.00	0.00	1.00	0.00	10.15	13.57	2.00	0.00	1.00	0.00
10.16	13.32	2.00	0.00	1.00	0.00	10.18	13.15	2.00	0.00	1.00	0.00
10.20	13.40	2.00	0.00	1.00	0.00	10.22	13.55	2.00	0.00	1.00	0.00
10.24	12.71	2.00	0.00	1.00	0.00	10.26	10.61	2.00	0.00	1.00	0.00
10.28	8.70	2.00	0.00	1.00	0.00	10.30	7.27	2.00	0.00	1.00	0.00
10.32	7.22	2.00	0.00	1.00	0.00	10.34	7.37	2.00	0.00	1.00	0.00
10.36	6.96	2.00	0.00	1.00	0.00	10.38	7.24	2.00	0.00	1.00	0.00
10.40	7.41	2.00	0.00	1.00	0.00	10.42	7.64	2.00	0.00	1.00	0.00
10.44	8.30	2.00	0.00	1.00	0.00	10.46	8.38	2.00	0.00	1.00	0.00
10.48	8.59	2.00	0.00	1.00	0.00	10.50	8.89	2.00	0.00	1.00	0.00
10.52	9.30	2.00	0.00	1.00	0.00	10.54	9.42	2.00	0.00	1.00	0.00
10.56	9.52	2.00	0.00	1.00	0.00	10.58	9.80	2.00	0.00	1.00	0.00
10.60	9.51	2.00	0.00	1.00	0.00	10.62	9.13	2.00	0.00	1.00	0.00
10.64	8.20	2.00	0.00	1.00	0.00	10.66	7.29	2.00	0.00	1.00	0.00
10.68	6.85	2.00	0.00	1.00	0.00	10.70	6.84	2.00	0.00	1.00	0.00
10.72	6.88	2.00	0.00	1.00	0.00	10.74	6.67	2.00	0.00	1.00	0.00
10.76	6.15	2.00	0.00	1.00	0.00	10.78	5.94	2.00	0.00	1.00	0.00
10.80	5.74	2.00	0.00	1.00	0.00	10.82	5.65	2.00	0.00	1.00	0.00
10.84	5.56	2.00	0.00	1.00	0.00	10.86	6.74	2.00	0.00	1.00	0.00
10.88	6.28	2.00	0.00	1.00	0.00	10.91	6.29	2.00	0.00	1.00	0.00
10.92	6.38	2.00	0.00	1.00	0.00	10.94	6.16	2.00	0.00	1.00	0.00
10.96	5.85	2.00	0.00	1.00	0.00	10.98	5.89	2.00	0.00	1.00	0.00
11.00	6.08	2.00	0.00	1.00	0.00	11.02	5.86	2.00	0.00	1.00	0.00
11.05	5.90	2.00	0.00	1.00	0.00	11.06	5.85	2.00	0.00	1.00	0.00
11.08	6.09	2.00	0.00	1.00	0.00	11.10	6.26	2.00	0.00	1.00	0.00
11.12	6.36	2.00	0.00	1.00	0.00	11.14	6.59	2.00	0.00	1.00	0.00
11.16	6.65	2.00	0.00	1.00	0.00	11.18	6.31	2.00	0.00	1.00	0.00
11.20	6.07	2.00	0.00	1.00	0.00	11.22	5.87	2.00	0.00	1.00	0.00
11.24	5.83	2.00	0.00	1.00	0.00	11.26	5.72	2.00	0.00	1.00	0.00
11.28	5.67	2.00	0.00	1.00	0.00	11.30	5.71	2.00	0.00	1.00	0.00
11.32	5.96	2.00	0.00	1.00	0.00	11.34	6.60	2.00	0.00	1.00	0.00
11.36	7.13	2.00	0.00	1.00	0.00	11.38	7.55	2.00	0.00	1.00	0.00
11.40	7.93	2.00	0.00	1.00	0.00	11.42	8.27	2.00	0.00	1.00	0.00
11.44	8.46	2.00	0.00	1.00	0.00	11.46	8.83	2.00	0.00	1.00	0.00
11.48	8.85	2.00	0.00	1.00	0.00	11.50	9.01	2.00	0.00	1.00	0.00
11.52	8.77	2.00	0.00	1.00	0.00	11.54	8.74	2.00	0.00	1.00	0.00
11.56	8.73	2.00	0.00	1.00	0.00	11.58	8.64	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.60	8.70	2.00	0.00	1.00	0.00	11.62	8.33	2.00	0.00	1.00	0.00
11.64	8.38	2.00	0.00	1.00	0.00	11.66	8.37	2.00	0.00	1.00	0.00
11.68	8.38	2.00	0.00	1.00	0.00	11.70	8.65	2.00	0.00	1.00	0.00
11.72	8.70	2.00	0.00	1.00	0.00	11.74	8.90	2.00	0.00	1.00	0.00
11.76	8.81	2.00	0.00	1.00	0.00	11.78	8.70	2.00	0.00	1.00	0.00
11.80	8.71	2.00	0.00	1.00	0.00	11.82	8.87	2.00	0.00	1.00	0.00
11.84	8.92	2.00	0.00	1.00	0.00	11.86	8.89	2.00	0.00	1.00	0.00
11.89	8.96	2.00	0.00	1.00	0.00	11.90	8.81	2.00	0.00	1.00	0.00
11.92	8.56	2.00	0.00	1.00	0.00	11.94	8.57	2.00	0.00	1.00	0.00
11.96	8.31	2.00	0.00	1.00	0.00	11.98	8.01	2.00	0.00	1.00	0.00
12.00	7.72	2.00	0.00	1.00	0.00	12.02	7.40	2.00	0.00	1.00	0.00
12.04	7.41	2.00	0.00	1.00	0.00	12.06	7.22	2.00	0.00	1.00	0.00
12.08	7.11	2.00	0.00	1.00	0.00	12.10	6.85	2.00	0.00	1.00	0.00
12.12	6.77	2.00	0.00	1.00	0.00	12.14	6.78	2.00	0.00	1.00	0.00
12.16	6.82	2.00	0.00	1.00	0.00	12.18	6.73	2.00	0.00	1.00	0.00
12.20	6.69	2.00	0.00	1.00	0.00	12.22	6.48	2.00	0.00	1.00	0.00
12.24	6.50	2.00	0.00	1.00	0.00	12.26	6.53	2.00	0.00	1.00	0.00
12.28	6.51	2.00	0.00	1.00	0.00	12.30	6.61	2.00	0.00	1.00	0.00
12.32	6.85	2.00	0.00	1.00	0.00	12.34	7.20	2.00	0.00	1.00	0.00
12.36	6.89	2.00	0.00	1.00	0.00	12.38	6.56	2.00	0.00	1.00	0.00
12.40	6.33	2.00	0.00	1.00	0.00	12.42	6.04	2.00	0.00	1.00	0.00
12.44	5.95	2.00	0.00	1.00	0.00	12.46	5.93	2.00	0.00	1.00	0.00
12.48	6.01	2.00	0.00	1.00	0.00	12.50	6.03	2.00	0.00	1.00	0.00
12.52	6.11	2.00	0.00	1.00	0.00	12.54	5.65	2.00	0.00	1.00	0.00
12.56	5.49	2.00	0.00	1.00	0.00	12.58	5.22	2.00	0.00	1.00	0.00
12.60	5.58	2.00	0.00	1.00	0.00	12.62	6.17	2.00	0.00	1.00	0.00
12.64	6.54	2.00	0.00	1.00	0.00	12.66	6.21	2.00	0.00	1.00	0.00
12.68	5.59	2.00	0.00	1.00	0.00	12.70	5.51	2.00	0.00	1.00	0.00
12.72	5.67	2.00	0.00	1.00	0.00	12.74	5.71	2.00	0.00	1.00	0.00
12.76	5.64	2.00	0.00	1.00	0.00	12.78	5.46	2.00	0.00	1.00	0.00
12.80	5.50	2.00	0.00	1.00	0.00	12.82	6.62	2.00	0.00	1.00	0.00
12.84	6.15	2.00	0.00	1.00	0.00	12.86	6.39	2.00	0.00	1.00	0.00
12.88	6.65	2.00	0.00	1.00	0.00	12.90	6.72	2.00	0.00	1.00	0.00
12.92	7.02	2.00	0.00	1.00	0.00	12.94	7.47	2.00	0.00	1.00	0.00
12.96	8.09	2.00	0.00	1.00	0.00	12.98	8.92	2.00	0.00	1.00	0.00
13.00	9.34	2.00	0.00	1.00	0.00	13.02	10.39	2.00	0.00	1.00	0.00
13.04	9.73	2.00	0.00	1.00	0.00	13.06	8.31	2.00	0.00	1.00	0.00
13.08	7.55	2.00	0.00	1.00	0.00	13.10	7.81	2.00	0.00	1.00	0.00
13.12	8.41	2.00	0.00	1.00	0.00	13.14	8.34	2.00	0.00	1.00	0.00
13.16	9.28	2.00	0.00	1.00	0.00	13.18	10.69	2.00	0.00	1.00	0.00
13.20	9.17	2.00	0.00	1.00	0.00	13.22	7.95	2.00	0.00	1.00	0.00
13.24	8.06	2.00	0.00	1.00	0.00	13.26	8.52	2.00	0.00	1.00	0.00
13.28	8.41	2.00	0.00	1.00	0.00	13.30	7.38	2.00	0.00	1.00	0.00
13.32	6.85	2.00	0.00	1.00	0.00	13.34	7.55	2.00	0.00	1.00	0.00
13.36	9.28	2.00	0.00	1.00	0.00	13.38	10.90	2.00	0.00	1.00	0.00
13.40	11.22	2.00	0.00	1.00	0.00	13.42	10.20	2.00	0.00	1.00	0.00
13.44	9.87	2.00	0.00	1.00	0.00	13.46	14.16	2.00	0.00	1.00	0.00
13.48	18.19	2.00	0.00	1.00	0.00	13.50	22.38	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.52	24.20	2.00	0.00	1.00	0.00	13.54	79.71	0.62	4.02	1.00	0.08
13.56	17.96	2.00	0.00	1.00	0.00	13.58	15.01	2.00	0.00	1.00	0.00
13.60	11.73	2.00	0.00	1.00	0.00	13.62	9.81	2.00	0.00	1.00	0.00
13.64	9.12	2.00	0.00	1.00	0.00	13.66	8.54	2.00	0.00	1.00	0.00
13.68	7.70	2.00	0.00	1.00	0.00	13.70	7.43	2.00	0.00	1.00	0.00
13.72	7.51	2.00	0.00	1.00	0.00	13.74	7.44	2.00	0.00	1.00	0.00
13.76	7.10	2.00	0.00	1.00	0.00	13.78	7.33	2.00	0.00	1.00	0.00
13.80	8.71	2.00	0.00	1.00	0.00	13.82	12.17	2.00	0.00	1.00	0.00
13.84	10.44	2.00	0.00	1.00	0.00	13.86	8.12	2.00	0.00	1.00	0.00
13.89	8.78	2.00	0.00	1.00	0.00	13.90	12.30	2.00	0.00	1.00	0.00
13.92	18.04	2.00	0.00	1.00	0.00	13.94	19.73	2.00	0.00	1.00	0.00
13.96	18.90	2.00	0.00	1.00	0.00	13.98	16.31	2.00	0.00	1.00	0.00
14.00	15.31	2.00	0.00	1.00	0.00	14.02	16.11	2.00	0.00	1.00	0.00
14.04	17.21	2.00	0.00	1.00	0.00	14.06	16.74	2.00	0.00	1.00	0.00
14.08	17.56	2.00	0.00	1.00	0.00	14.10	20.84	2.00	0.00	1.00	0.00
14.12	22.95	2.00	0.00	1.00	0.00	14.14	22.80	2.00	0.00	1.00	0.00
14.16	21.72	2.00	0.00	1.00	0.00	14.18	22.72	2.00	0.00	1.00	0.00
14.21	23.89	2.00	0.00	1.00	0.00	14.22	26.66	2.00	0.00	1.00	0.00
14.24	87.15	2.00	0.00	1.00	0.00	14.26	87.79	2.00	0.00	1.00	0.00
14.28	86.45	2.00	0.00	1.00	0.00	14.30	83.44	2.00	0.00	1.00	0.00
14.32	79.78	2.00	0.00	1.00	0.00	14.34	20.17	2.00	0.00	1.00	0.00
14.37	17.45	2.00	0.00	1.00	0.00	14.38	16.88	2.00	0.00	1.00	0.00
14.40	17.92	2.00	0.00	1.00	0.00	14.42	20.48	2.00	0.00	1.00	0.00
14.44	26.66	2.00	0.00	1.00	0.00	14.46	89.57	2.00	0.00	1.00	0.00
14.48	89.96	2.00	0.00	1.00	0.00	14.50	87.59	0.68	3.67	1.00	0.07
14.52	85.50	0.66	3.76	1.00	0.08	14.54	82.22	0.64	3.90	1.00	0.08
14.56	80.73	0.63	3.97	1.00	0.08	14.58	81.89	2.00	0.00	1.00	0.00
14.60	83.39	2.00	0.00	1.00	0.00	14.62	85.42	2.00	0.00	1.00	0.00
14.64	85.82	2.00	0.00	1.00	0.00	14.66	25.72	2.00	0.00	1.00	0.00
14.68	22.28	2.00	0.00	1.00	0.00	14.70	20.55	2.00	0.00	1.00	0.00
14.72	20.17	2.00	0.00	1.00	0.00	14.74	21.87	2.00	0.00	1.00	0.00
14.76	23.03	2.00	0.00	1.00	0.00	14.78	24.85	2.00	0.00	1.00	0.00
14.80	27.24	2.00	0.00	1.00	0.00	14.82	27.15	2.00	0.00	1.00	0.00
14.84	23.72	2.00	0.00	1.00	0.00	14.86	20.31	2.00	0.00	1.00	0.00
14.88	17.37	2.00	0.00	1.00	0.00	14.90	14.02	2.00	0.00	1.00	0.00
14.92	16.94	2.00	0.00	1.00	0.00	14.94	20.83	2.00	0.00	1.00	0.00
14.96	19.52	2.00	0.00	1.00	0.00	14.98	14.13	2.00	0.00	1.00	0.00
15.00	10.73	2.00	0.00	1.00	0.00	15.02	7.40	2.00	0.00	1.00	0.00
15.04	7.32	2.00	0.00	1.00	0.00	15.06	7.58	2.00	0.00	1.00	0.00
15.08	7.53	2.00	0.00	1.00	0.00	15.10	7.13	2.00	0.00	1.00	0.00
15.12	6.97	2.00	0.00	1.00	0.00	15.15	6.85	2.00	0.00	1.00	0.00
15.16	6.94	2.00	0.00	1.00	0.00	15.18	7.08	2.00	0.00	1.00	0.00
15.20	7.36	2.00	0.00	1.00	0.00	15.22	7.39	2.00	0.00	1.00	0.00
15.24	7.16	2.00	0.00	1.00	0.00	15.26	7.16	2.00	0.00	1.00	0.00
15.28	7.23	2.00	0.00	1.00	0.00	15.30	7.51	2.00	0.00	1.00	0.00
15.32	7.58	2.00	0.00	1.00	0.00	15.34	7.26	2.00	0.00	1.00	0.00
15.36	6.35	2.00	0.00	1.00	0.00	15.38	6.41	2.00	0.00	1.00	0.00
15.40	6.89	2.00	0.00	1.00	0.00	15.42	7.84	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.44	9.40	2.00	0.00	1.00	0.00	15.46	10.52	2.00	0.00	1.00	0.00
15.48	11.59	2.00	0.00	1.00	0.00	15.50	12.30	2.00	0.00	1.00	0.00
15.52	13.03	2.00	0.00	1.00	0.00	15.54	12.29	2.00	0.00	1.00	0.00
15.56	10.09	2.00	0.00	1.00	0.00	15.58	9.26	2.00	0.00	1.00	0.00
15.60	10.02	2.00	0.00	1.00	0.00						

Total estimated settlement: 0.39

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	1.34	22.74	7.72	175.51	3.08	0.08	254.15
0.04	1.33	22.62	7.83	177.15	3.09	0.08	126.30
0.07	1.37	23.21	7.66	177.85	3.08	0.08	74.02
0.08	1.42	24.11	7.42	178.96	3.06	0.08	67.27
0.10	1.47	24.95	7.22	180.03	3.04	0.08	55.65
0.12	1.51	25.64	7.01	179.66	3.02	0.08	47.63
0.14	1.52	25.87	6.83	176.58	3.01	0.08	41.19
0.16	1.50	25.38	6.89	174.77	3.01	0.08	35.37
0.19	1.45	24.55	7.07	173.64	3.03	0.08	28.82
0.20	1.38	23.45	7.47	175.29	3.06	0.08	26.16
0.22	1.32	22.37	7.86	175.89	3.09	0.08	22.69
0.24	1.25	21.21	8.31	176.28	3.13	0.07	19.72
0.26	1.20	20.28	8.63	175.00	3.15	0.07	17.41
0.28	1.17	19.79	8.69	171.89	3.16	0.07	15.78
0.30	1.15	19.50	8.61	167.92	3.15	0.07	14.53
0.32	1.14	19.34	8.46	163.62	3.14	0.07	13.51
0.34	1.13	19.13	8.34	159.46	3.13	0.07	12.59
0.36	1.11	18.67	8.31	155.16	3.13	0.07	11.62
0.38	1.07	18.02	8.43	151.91	3.14	0.07	10.64
0.40	1.02	17.16	8.74	149.90	3.16	0.07	9.63
0.42	0.97	16.42	9.06	148.80	3.19	0.07	8.79
0.44	0.94	15.85	9.33	147.92	3.21	0.07	8.10
0.46	0.92	15.55	9.44	146.71	3.21	0.07	7.61
0.48	0.91	15.36	9.47	145.50	3.22	0.07	7.21
0.50	0.90	15.12	9.51	143.71	3.22	0.07	6.82
0.52	0.88	14.84	9.55	141.80	3.22	0.07	6.44
0.54	0.86	14.52	9.63	139.83	3.23	0.07	6.08
0.56	0.84	14.18	9.76	138.36	3.24	0.07	5.73
0.58	0.81	13.65	10.06	137.30	3.26	0.07	5.33
0.60	0.79	13.31	10.26	136.60	3.27	0.06	5.03
0.62	0.80	13.42	10.16	136.30	3.26	0.07	4.91
0.64	0.85	14.18	9.60	136.12	3.22	0.07	5.03
0.66	0.89	15.00	9.05	135.69	3.19	0.07	5.16
0.68	0.94	15.73	8.56	134.59	3.15	0.07	5.26
0.70	0.97	16.25	8.21	133.40	3.12	0.07	5.28
0.72	0.66	11.00	9.78	107.59	3.24	0.07	3.48
0.02	0.34	5.78	12.90	74.56	3.43	0.05	13.19
0.04	0.01	0.18	1.00	0.18	-1.00	0.01	0.17
0.06	0.02	0.22	1.00	0.22	-1.00	0.01	0.18
0.08	0.01	0.17	1.00	0.17	-1.00	0.01	0.16
0.10	0.01	0.15	1.00	0.15	-1.00	0.01	0.15
0.12	0.01	0.16	26.61	4.33	4.06	0.05	0.18
0.14	0.02	0.21	26.61	5.62	4.06	0.05	0.22
0.16	0.02	0.21	26.61	5.55	4.06	0.05	0.20
0.18	0.01	0.16	26.61	4.14	4.06	0.05	0.14
0.20	0.01	0.11	1.00	0.11	-1.00	0.01	0.13
0.22	0.01	0.11	1.00	0.11	-1.00	0.01	0.12
0.24	0.01	0.09	1.00	0.09	-1.00	0.01	0.11

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.26	0.01	0.11	1.00	0.11	-1.00	0.01	0.12
0.28	0.01	0.13	1.00	0.13	-1.00	0.01	0.14
0.30	0.02	0.16	1.00	0.16	-1.00	0.01	0.16
0.32	0.02	0.13	1.00	0.13	-1.00	0.01	0.14
0.34	0.01	0.11	1.00	0.11	-1.00	0.01	0.13
0.36	0.01	0.06	1.00	0.06	-1.00	0.01	0.07
0.38	0.01	0.05	1.00	0.05	-1.00	0.01	0.06
0.40	0.01	0.01	1.00	0.01	-1.00	-0.07	-0.07
0.42	0.01	0.04	1.00	0.04	-1.00	0.01	0.05
0.44	0.09	1.34	13.26	17.73	3.45	0.05	0.55
0.46	0.17	2.72	13.34	36.22	3.46	0.05	1.10
0.48	0.25	4.15	13.45	55.76	3.46	0.05	1.63
0.50	0.26	4.20	16.83	70.73	3.64	0.05	1.60
0.52	0.26	4.17	19.46	81.12	3.77	0.05	1.54
0.54	0.25	4.04	21.89	88.43	3.87	0.05	1.45
0.56	0.24	3.95	23.77	94.01	3.95	0.05	1.38
0.58	0.24	3.90	25.27	98.61	4.01	0.05	1.32
0.60	0.23	3.71	26.61	98.60	4.06	0.05	1.22
0.62	0.22	3.60	26.61	95.81	4.06	0.05	1.15
0.64	0.22	3.47	26.61	92.19	4.06	0.05	1.08
0.66	0.21	3.40	26.61	90.35	4.06	0.05	1.03
0.68	0.21	3.35	26.61	89.02	4.06	0.05	0.99
0.70	0.21	3.31	26.61	88.00	4.06	0.05	0.96
0.72	0.22	3.40	26.61	90.56	4.06	0.05	0.96
0.74	0.21	3.32	26.61	88.25	4.06	0.05	0.92
0.76	0.21	3.27	26.61	87.02	4.06	0.05	0.88
0.78	0.22	3.39	26.61	90.26	4.06	0.05	0.89
0.80	0.23	3.68	24.58	90.54	3.98	0.05	0.95
0.82	0.24	3.88	22.83	88.48	3.91	0.05	0.98
0.84	0.26	4.09	21.31	87.25	3.85	0.05	1.01
0.86	0.27	4.22	20.69	87.32	3.82	0.05	1.03
0.88	0.27	4.27	20.19	86.14	3.80	0.05	1.02
0.90	0.26	4.15	20.17	83.69	3.80	0.05	0.97
0.92	0.27	4.36	19.45	84.87	3.76	0.05	1.00
0.94	0.30	4.81	18.78	90.40	3.73	0.05	1.08
0.96	0.53	8.61	12.69	109.29	3.42	0.05	1.90
0.98	0.78	12.91	9.15	118.06	3.19	0.07	2.80
1.00	1.05	17.46	6.99	122.13	3.02	0.07	3.72
1.02	1.12	18.76	6.52	122.43	2.98	0.07	3.93
1.04	1.16	19.34	6.45	124.73	2.97	0.07	3.98
1.06	1.18	19.67	6.49	127.61	2.98	0.07	3.98
1.08	1.19	19.90	6.60	131.32	2.99	0.07	3.95
1.10	1.22	20.30	6.65	134.95	2.99	0.07	3.96
1.12	1.24	20.69	6.69	138.50	3.00	0.07	3.97
1.14	1.26	21.01	6.70	140.77	3.00	0.07	3.97
1.16	1.26	21.10	6.72	141.83	3.00	0.07	3.92
1.18	1.26	21.07	6.72	141.67	3.00	0.07	3.85
1.20	1.25	20.84	6.77	141.03	3.00	0.07	3.75

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.22	1.23	20.56	6.82	140.10	3.01	0.07	3.64
1.24	1.21	20.18	6.90	139.29	3.01	0.07	3.52
1.26	1.18	19.67	7.08	139.17	3.03	0.07	3.38
1.28	1.12	18.64	7.50	139.81	3.07	0.07	3.16
1.30	1.06	17.64	7.93	139.92	3.10	0.07	2.94
1.32	1.04	17.25	8.10	139.70	3.11	0.07	2.84
1.34	1.07	17.83	7.84	139.84	3.09	0.07	2.89
1.36	1.13	18.70	7.45	139.22	3.06	0.07	2.99
1.38	1.16	19.31	7.10	137.00	3.03	0.07	3.05
1.40	1.16	19.30	6.95	134.23	3.02	0.07	3.01
1.42	1.14	18.91	7.05	133.39	3.03	0.07	2.91
1.44	1.12	18.51	7.31	135.25	3.05	0.07	2.81
1.46	1.11	18.37	7.50	137.74	3.06	0.07	2.75
1.48	1.12	18.48	7.61	140.69	3.07	0.07	2.73
1.50	1.13	18.72	7.68	143.78	3.08	0.07	2.73
1.52	1.14	18.93	7.73	146.41	3.08	0.07	2.73
1.54	1.15	19.05	7.75	147.52	3.09	0.07	2.71
1.56	1.15	19.09	7.68	146.49	3.08	0.07	2.68
1.58	1.15	18.98	7.66	145.34	3.08	0.07	2.63
1.60	1.14	18.85	7.66	144.31	3.08	0.07	2.59
1.63	1.14	18.78	7.65	143.67	3.08	0.07	2.53
1.64	1.14	18.91	7.54	142.61	3.07	0.07	2.53
1.66	1.16	19.11	7.38	141.03	3.06	0.07	2.53
1.68	1.16	19.20	7.28	139.74	3.05	0.07	2.51
1.70	1.18	19.46	7.09	137.99	3.03	0.07	2.52
1.72	1.20	19.92	6.80	135.54	3.01	0.07	2.55
1.74	1.23	20.34	6.53	132.71	2.98	0.07	2.57
1.76	1.23	20.35	6.41	130.44	2.97	0.07	2.55
1.78	1.21	19.91	6.50	129.40	2.98	0.07	2.47
1.80	1.17	19.28	6.69	128.96	2.99	0.07	2.36
1.82	1.12	18.46	7.00	129.21	3.02	0.07	2.24
1.84	1.06	17.51	7.44	130.26	3.06	0.07	2.10
1.86	1.00	16.45	8.01	131.79	3.11	0.07	1.95
1.88	0.95	15.51	8.52	132.10	3.15	0.07	1.82
1.90	0.90	14.76	8.90	131.45	3.17	0.07	1.72
1.92	0.87	14.24	9.15	130.32	3.19	0.07	1.64
1.94	0.86	13.93	9.17	127.75	3.19	0.07	1.59
1.96	0.88	14.40	8.66	124.69	3.16	0.07	1.63
1.98	0.92	15.04	8.06	121.20	3.11	0.07	1.68
2.01	0.96	15.75	7.61	119.84	3.07	0.07	1.74
2.02	0.98	15.96	7.44	118.75	3.06	0.07	1.75
2.04	0.99	16.17	7.25	117.23	3.04	0.07	1.76
2.06	0.99	16.25	7.12	115.74	3.03	0.07	1.75
2.08	0.99	16.25	7.09	115.17	3.03	0.07	1.74
2.10	1.00	16.25	7.10	115.41	3.03	0.07	1.72
2.12	1.01	16.48	7.03	115.78	3.02	0.07	1.73
2.14	1.04	16.99	6.81	115.67	3.01	0.07	1.77
2.16	1.07	17.43	6.64	115.72	2.99	0.07	1.80

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.18	1.08	17.61	6.63	116.85	2.99	0.07	1.80
2.20	1.08	17.63	6.79	119.71	3.00	0.07	1.79
2.22	1.08	17.65	6.96	122.82	3.02	0.07	1.78
2.24	1.09	17.88	7.03	125.68	3.03	0.07	1.78
2.26	1.10	17.97	7.14	128.35	3.04	0.07	1.78
2.28	1.10	17.90	7.35	131.51	3.05	0.07	1.76
2.30	1.08	17.61	7.61	133.96	3.07	0.07	1.71
2.32	1.06	17.31	7.79	134.84	3.09	0.07	1.67
2.34	1.04	16.96	7.93	134.56	3.10	0.07	1.62
2.36	1.01	16.49	8.15	134.41	3.12	0.07	1.56
2.38	0.99	15.99	8.40	134.37	3.14	0.07	1.50
2.40	0.96	15.50	8.65	134.10	3.16	0.07	1.45
2.42	0.95	15.30	8.68	132.85	3.16	0.07	1.42
2.44	0.93	15.07	8.72	131.37	3.16	0.07	1.38
2.46	0.93	14.99	8.62	129.19	3.15	0.07	1.37
2.48	0.93	14.94	8.48	126.60	3.14	0.07	1.35
2.50	0.92	14.82	8.38	124.08	3.14	0.07	1.33
2.52	0.91	14.67	8.36	122.67	3.13	0.06	1.31
2.54	0.90	14.48	8.45	122.34	3.14	0.06	1.29
2.56	0.89	14.30	8.60	122.90	3.15	0.06	1.27
2.58	0.88	14.09	8.75	123.33	3.16	0.06	1.25
2.60	0.86	13.75	9.00	123.85	3.18	0.06	1.21
2.62	0.84	13.39	9.26	123.98	3.20	0.06	1.18
2.64	0.81	12.95	9.57	123.94	3.22	0.06	1.14
2.66	0.79	12.52	9.85	123.34	3.24	0.06	1.09
2.68	0.78	12.34	9.90	122.11	3.25	0.06	1.07
2.70	0.77	12.30	9.81	120.72	3.24	0.06	1.07
2.72	0.79	12.64	9.43	119.18	3.21	0.06	1.09
2.74	0.82	13.07	9.03	118.00	3.18	0.06	1.13
2.76	0.86	13.78	8.42	115.99	3.14	0.06	1.18
2.78	0.89	14.31	7.92	113.30	3.10	0.06	1.23
2.80	0.91	14.66	7.52	110.33	3.07	0.06	1.25
2.82	0.92	14.79	7.32	108.24	3.05	0.06	1.26
2.84	0.93	14.86	7.24	107.64	3.04	0.06	1.26
2.86	0.93	14.93	7.20	107.49	3.04	0.06	1.26
2.88	0.93	14.86	7.27	108.03	3.05	0.06	1.25
2.90	0.91	14.54	7.48	108.75	3.06	0.06	1.22
2.92	0.88	14.03	7.79	109.24	3.09	0.06	1.18
2.94	0.83	13.22	8.27	109.36	3.13	0.06	1.10
2.96	0.78	12.24	8.89	108.86	3.17	0.06	1.02
2.98	0.71	11.17	9.71	108.52	3.23	0.06	0.93
3.00	0.64	9.94	10.80	107.44	3.31	0.06	0.82
3.02	0.56	8.65	12.13	104.97	3.39	0.06	0.71
3.04	0.49	7.37	13.70	100.95	3.48	0.06	0.61
3.06	0.44	6.48	14.90	96.49	3.54	0.06	0.53
3.09	0.41	5.92	15.64	92.58	3.58	0.06	0.48
3.10	0.40	5.85	15.26	89.24	3.56	0.06	0.48
3.12	0.42	6.22	13.88	86.36	3.49	0.06	0.51

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.14	0.50	7.44	11.20	83.31	3.33	0.06	0.60
3.16	0.58	8.81	8.99	79.22	3.18	0.06	0.71
3.18	0.64	9.88	7.61	75.19	3.07	0.06	0.80
3.21	0.69	10.75	6.66	71.61	2.99	0.06	0.87
3.22	0.74	11.63	5.94	69.13	2.92	0.06	0.94
3.24	0.81	12.79	5.38	68.84	2.87	0.07	1.03
3.26	0.84	13.34	5.45	72.69	2.87	0.07	1.07
3.28	0.87	13.74	5.62	77.23	2.89	0.07	1.10
3.30	0.88	14.00	5.79	81.01	2.91	0.07	1.11
3.32	0.92	14.57	5.75	83.70	2.90	0.07	1.16
3.34	0.95	15.15	5.77	87.42	2.91	0.07	1.20
3.36	0.98	15.59	5.89	91.74	2.92	0.07	1.23
3.38	0.99	15.83	6.06	95.92	2.94	0.07	1.25
3.40	1.00	15.93	6.19	98.68	2.95	0.07	1.25
3.42	1.00	15.98	6.34	101.28	2.96	0.07	1.25
3.44	1.00	15.89	6.56	104.17	2.98	0.07	1.24
3.46	0.99	15.77	6.80	107.23	3.01	0.07	1.23
3.48	1.00	15.92	6.88	109.48	3.01	0.07	1.23
3.50	1.02	16.33	6.83	111.45	3.01	0.07	1.26
3.52	1.06	16.98	6.69	113.65	3.00	0.07	1.31
3.54	1.11	17.77	6.54	116.15	2.98	0.07	1.37
3.56	1.15	18.44	6.42	118.31	2.97	0.07	1.41
3.58	1.18	18.90	6.38	120.64	2.97	0.07	1.45
3.60	1.19	19.09	6.50	124.05	2.98	0.07	1.45
3.62	1.19	19.16	6.71	128.51	3.00	0.07	1.46
3.64	1.19	19.13	6.94	132.74	3.02	0.07	1.45
3.66	1.18	19.00	7.13	135.57	3.03	0.07	1.44
3.68	1.17	18.71	7.36	137.64	3.05	0.07	1.41
3.70	1.14	18.24	7.66	139.78	3.08	0.07	1.37
3.72	1.12	17.82	8.00	142.54	3.11	0.07	1.33
3.74	1.11	17.64	8.20	144.56	3.12	0.07	1.32
3.76	1.11	17.77	8.17	145.23	3.12	0.07	1.32
3.78	1.12	17.81	8.11	144.43	3.11	0.07	1.32
3.80	1.11	17.77	8.05	143.07	3.11	0.07	1.31
3.82	1.12	17.78	7.96	141.62	3.10	0.07	1.31
3.84	1.11	17.75	7.89	140.10	3.10	0.07	1.31
3.86	1.12	17.90	7.77	139.07	3.09	0.07	1.31
3.88	1.12	17.85	7.75	138.40	3.09	0.07	1.31
3.90	1.12	17.89	7.72	138.10	3.08	0.07	1.30
3.92	1.16	18.44	7.30	134.70	3.05	0.07	1.34
3.94	1.18	18.81	6.97	131.03	3.02	0.07	1.36
3.96	1.20	19.13	6.59	126.01	2.99	0.07	1.38
3.98	1.16	18.54	6.67	123.65	2.99	0.07	1.34
4.00	1.11	17.54	6.86	120.32	3.01	0.07	1.26
4.02	1.03	16.27	7.21	117.38	3.04	0.06	1.17
4.04	0.97	15.21	7.54	114.64	3.07	0.06	1.09
4.06	0.94	14.63	7.64	111.77	3.08	0.06	1.04
4.08	0.92	14.27	7.60	108.47	3.07	0.06	1.02

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.10	0.90	14.00	7.44	104.18	3.06	0.06	1.00
4.12	0.89	13.73	7.29	100.13	3.05	0.06	0.98
4.14	0.89	13.72	7.01	96.13	3.02	0.06	0.98
4.16	0.88	13.41	6.92	92.73	3.02	0.06	0.96
4.18	0.86	13.14	6.84	89.86	3.01	0.06	0.94
4.20	0.82	12.42	7.09	88.07	3.03	0.06	0.89
4.22	0.79	11.83	7.30	86.37	3.05	0.06	0.84
4.24	0.75	11.20	7.59	85.03	3.07	0.06	0.80
4.26	0.75	11.18	7.41	82.79	3.06	0.06	0.80
4.28	0.79	11.74	6.85	80.42	3.01	0.06	0.84
4.30	0.86	12.94	6.02	77.95	2.93	0.06	0.93
4.32	0.96	14.26	5.35	76.26	2.86	0.07	1.03
4.34	1.04	15.43	4.94	76.27	2.82	0.07	1.13
4.36	1.09	16.14	4.81	77.70	2.80	0.07	1.18
4.38	1.09	16.17	4.99	80.62	2.82	0.07	1.18
4.40	1.06	15.78	5.35	84.43	2.86	0.07	1.14
4.42	1.00	14.94	5.96	89.02	2.93	0.07	1.07
4.44	0.94	13.93	6.65	92.60	2.99	0.06	0.99
4.46	0.87	12.78	7.45	95.23	3.06	0.06	0.91
4.48	0.82	11.85	8.12	96.27	3.12	0.06	0.85
4.50	0.76	10.92	8.78	95.88	3.17	0.06	0.78
4.52	0.73	10.33	9.12	94.24	3.19	0.06	0.74
4.54	0.75	10.65	8.66	92.21	3.16	0.06	0.76
4.56	0.87	12.52	7.21	90.27	3.04	0.06	0.89
4.58	1.09	15.84	5.48	86.81	2.88	0.07	1.14
4.61	1.30	18.71	4.50	84.24	2.77	0.08	1.38
4.62	1.35	19.39	4.33	83.98	2.74	0.08	1.43
4.64	1.20	17.33	4.94	85.52	2.82	0.07	1.26
4.66	0.98	14.09	5.85	82.49	2.92	0.07	1.01
4.68	0.82	11.66	6.58	76.77	2.99	0.06	0.83
4.70	0.77	10.84	6.55	71.07	2.98	0.06	0.77
4.72	0.77	10.72	6.60	70.77	2.99	0.06	0.77
4.74	0.79	11.04	6.51	71.93	2.98	0.06	0.79
4.76	0.86	12.04	6.12	73.60	2.94	0.06	0.86
4.78	1.01	14.17	5.12	72.58	2.84	0.07	1.03
4.80	1.22	17.00	4.28	72.79	2.74	0.08	1.26
4.82	1.41	19.71	3.78	74.54	2.67	0.08	1.47
4.84	1.57	21.97	3.62	79.47	2.65	0.08	1.65
4.86	1.69	23.55	3.53	83.10	2.63	0.08	1.77
4.88	1.73	24.07	3.57	85.99	2.64	0.08	1.80
4.90	1.69	23.57	3.63	85.57	2.65	0.08	1.76
4.92	1.56	21.77	3.96	86.29	2.70	0.08	1.62
4.94	1.38	19.28	4.43	85.39	2.76	0.08	1.42
4.96	1.17	16.28	5.26	85.63	2.85	0.07	1.18
4.98	1.03	14.25	5.93	84.45	2.92	0.07	1.02
5.00	0.98	13.57	6.23	84.48	2.95	0.06	0.97
5.02	1.00	13.83	6.13	84.77	2.94	0.07	0.99
5.04	1.01	13.97	6.06	84.62	2.94	0.07	1.00

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.06	0.96	13.15	6.39	83.99	2.97	0.06	0.94
5.08	0.88	11.93	6.98	83.27	3.02	0.06	0.85
5.10	0.82	11.01	7.46	82.06	3.06	0.06	0.79
5.12	0.82	10.89	7.40	80.59	3.06	0.06	0.78
5.14	0.82	10.83	7.36	79.75	3.05	0.06	0.77
5.16	0.80	10.54	7.55	79.56	3.07	0.06	0.75
5.18	0.79	10.44	7.54	78.71	3.07	0.06	0.75
5.20	0.80	10.57	7.24	76.48	3.04	0.06	0.75
5.22	0.82	10.81	6.90	74.59	3.01	0.06	0.77
5.24	0.78	10.11	7.29	73.62	3.05	0.06	0.72
5.26	0.73	9.44	7.79	73.48	3.09	0.06	0.67
5.28	0.68	8.61	8.43	72.62	3.14	0.06	0.62
5.30	0.66	8.30	8.70	72.17	3.16	0.06	0.59
5.32	0.62	7.76	9.39	72.86	3.21	0.06	0.55
5.34	0.59	7.19	10.31	74.11	3.27	0.06	0.51
5.36	0.55	6.64	11.13	73.87	3.33	0.06	0.47
5.38	0.52	6.17	11.75	72.50	3.37	0.06	0.44
5.40	0.49	5.72	12.31	70.45	3.40	0.06	0.41
5.42	0.48	5.52	12.51	69.04	3.41	0.06	0.39
5.44	0.48	5.57	12.09	67.36	3.39	0.06	0.40
5.46	0.50	5.90	11.08	65.44	3.32	0.06	0.42
5.48	0.53	6.26	10.18	63.73	3.26	0.06	0.45
5.51	0.55	6.55	9.60	62.85	3.22	0.06	0.47
5.52	0.56	6.69	9.34	62.50	3.21	0.06	0.48
5.54	0.56	6.66	9.35	62.29	3.21	0.06	0.48
5.56	0.57	6.76	9.19	62.14	3.20	0.06	0.48
5.58	0.59	7.09	8.90	63.03	3.17	0.06	0.51
5.60	0.63	7.60	8.60	65.38	3.15	0.06	0.54
5.62	0.66	7.97	8.59	68.46	3.15	0.06	0.57
5.64	0.67	8.14	8.72	71.02	3.16	0.06	0.58
5.66	0.66	7.95	9.17	72.91	3.19	0.06	0.57
5.68	0.62	7.42	10.06	74.64	3.26	0.06	0.53
5.70	0.57	6.65	11.46	76.22	3.35	0.06	0.47
5.72	0.52	5.94	12.97	76.96	3.44	0.06	0.42
5.74	0.49	5.46	14.18	77.45	3.51	0.06	0.39
5.76	0.47	5.21	14.92	77.66	3.54	0.06	0.37
5.78	0.46	4.96	15.60	77.41	3.58	0.06	0.35
5.80	0.44	4.76	16.00	76.19	3.60	0.06	0.34
5.82	0.42	4.46	16.46	73.44	3.62	0.06	0.32
5.84	0.41	4.25	16.55	70.33	3.63	0.06	0.30
5.86	0.39	4.06	16.59	67.29	3.63	0.05	0.29
5.88	0.39	3.94	16.52	65.09	3.63	0.05	0.28
5.90	0.39	3.98	15.92	63.42	3.60	0.05	0.28
5.92	0.40	4.13	15.04	62.12	3.55	0.06	0.30
5.95	0.43	4.43	13.81	61.17	3.48	0.06	0.32
5.96	0.44	4.63	13.05	60.38	3.44	0.06	0.33
5.98	0.45	4.81	12.49	60.11	3.41	0.06	0.34
6.00	0.46	4.88	12.35	60.26	3.40	0.06	0.35

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.02	0.48	5.07	12.14	61.61	3.39	0.06	0.36
6.04	0.48	5.12	12.23	62.59	3.39	0.06	0.37
6.06	0.48	5.16	12.22	63.05	3.39	0.06	0.37
6.08	0.48	5.10	12.43	63.42	3.41	0.06	0.36
6.10	0.47	4.96	12.99	64.40	3.44	0.06	0.35
6.12	0.45	4.64	14.15	65.70	3.50	0.06	0.33
6.14	0.42	4.30	15.41	66.24	3.57	0.06	0.31
6.16	0.41	4.07	16.15	65.70	3.61	0.06	0.29
6.18	0.39	3.87	16.63	64.31	3.63	0.06	0.28
6.20	0.37	3.57	17.20	61.45	3.66	0.05	0.26
6.22	0.37	3.48	16.88	58.80	3.64	0.05	0.25
6.24	0.39	3.76	15.02	56.56	3.55	0.05	0.27
6.26	0.44	4.47	12.29	54.93	3.40	0.06	0.32
6.28	0.48	4.99	10.73	53.54	3.30	0.06	0.36
6.30	0.47	4.83	10.82	52.28	3.31	0.06	0.34
6.32	0.41	4.03	12.44	50.10	3.41	0.06	0.29
6.34	0.35	3.20	14.44	46.16	3.52	0.05	0.23
6.36	0.33	2.96	14.71	43.50	3.53	0.05	0.21
6.38	0.33	2.96	14.18	41.96	3.50	0.05	0.21
6.40	0.34	3.01	13.92	41.86	3.49	0.05	0.21
6.42	0.35	3.19	13.37	42.68	3.46	0.05	0.23
6.44	0.41	3.92	11.45	44.88	3.35	0.06	0.28
6.46	0.46	4.55	10.37	47.16	3.28	0.06	0.32
6.48	0.46	4.63	10.62	49.23	3.29	0.06	0.33
6.50	0.44	4.27	11.73	50.12	3.36	0.06	0.31
6.52	0.44	4.32	11.77	50.88	3.37	0.06	0.31
6.54	0.49	4.90	10.58	51.81	3.29	0.06	0.35
6.56	0.55	5.73	9.28	53.17	3.20	0.06	0.41
6.58	0.60	6.42	8.69	55.79	3.16	0.06	0.46
6.60	0.65	6.95	8.52	59.21	3.15	0.06	0.50
6.62	0.67	7.31	8.65	63.26	3.16	0.06	0.52
6.64	0.70	7.62	8.73	66.51	3.16	0.06	0.54
6.67	0.71	7.75	9.04	70.08	3.19	0.06	0.55
6.68	0.71	7.75	9.44	73.13	3.21	0.06	0.55
6.70	0.70	7.59	9.95	75.53	3.25	0.06	0.54
6.72	0.68	7.34	10.45	76.67	3.28	0.06	0.52
6.74	0.67	7.13	10.88	77.61	3.31	0.06	0.51
6.76	0.65	6.85	11.41	78.21	3.34	0.06	0.49
6.78	0.64	6.69	11.77	78.79	3.37	0.06	0.48
6.80	0.64	6.75	11.69	78.88	3.36	0.06	0.48
6.82	0.65	6.87	11.45	78.61	3.35	0.06	0.49
6.84	0.68	7.18	10.84	77.82	3.31	0.06	0.51
6.86	0.69	7.32	10.42	76.28	3.28	0.06	0.52
6.88	0.71	7.55	9.78	73.85	3.24	0.06	0.54
6.90	0.72	7.62	9.40	71.62	3.21	0.06	0.54
6.92	0.71	7.56	9.23	69.77	3.20	0.06	0.54
6.94	0.70	7.37	9.35	68.89	3.21	0.06	0.53
6.96	0.67	7.01	9.75	68.40	3.24	0.06	0.50

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.98	0.65	6.71	10.20	68.46	3.27	0.06	0.48
7.00	0.63	6.42	10.66	68.39	3.30	0.06	0.46
7.02	0.61	6.17	10.99	67.86	3.32	0.06	0.44
7.05	0.60	5.96	11.22	66.89	3.33	0.06	0.43
7.06	0.58	5.78	11.43	66.06	3.35	0.06	0.41
7.08	0.59	5.83	11.23	65.47	3.33	0.06	0.42
7.10	0.62	6.28	10.35	64.99	3.28	0.06	0.45
7.12	0.69	7.04	9.20	64.79	3.20	0.06	0.50
7.14	0.76	7.91	8.26	65.34	3.13	0.06	0.57
7.16	0.82	8.73	7.70	67.15	3.08	0.06	0.62
7.18	0.90	9.73	7.10	69.09	3.03	0.06	0.70
7.20	1.02	11.10	6.37	70.75	2.97	0.06	0.79
7.22	1.16	12.82	5.66	72.62	2.90	0.07	0.92
7.24	1.26	14.02	5.42	76.05	2.87	0.07	1.00
7.26	1.31	14.58	5.53	80.59	2.88	0.07	1.04
7.28	1.26	14.07	6.08	85.47	2.94	0.07	1.00
7.30	1.21	13.42	6.70	89.96	3.00	0.06	0.96
7.32	1.16	12.77	7.34	93.74	3.05	0.06	0.91
7.34	1.15	12.51	7.75	96.97	3.09	0.06	0.89
7.36	1.14	12.47	7.87	98.16	3.10	0.06	0.89
7.38	1.15	12.47	7.89	98.46	3.10	0.06	0.89
7.40	1.15	12.51	7.79	97.46	3.09	0.06	0.89
7.42	1.15	12.40	7.76	96.22	3.09	0.06	0.89
7.44	1.14	12.35	7.64	94.40	3.08	0.06	0.88
7.46	1.16	12.52	7.41	92.73	3.06	0.06	0.89
7.48	1.20	13.03	7.00	91.19	3.02	0.06	0.93
7.50	1.27	13.79	6.52	89.98	2.98	0.07	0.99
7.52	1.32	14.32	6.21	89.01	2.95	0.07	1.02
7.54	1.33	14.50	6.16	89.37	2.95	0.07	1.04
7.56	1.31	14.16	6.37	90.26	2.97	0.07	1.01
7.58	1.25	13.50	6.78	91.55	3.00	0.07	0.96
7.60	1.19	12.69	7.23	91.72	3.04	0.06	0.91
7.62	1.13	11.99	7.59	90.99	3.07	0.06	0.86
7.64	1.09	11.49	7.78	89.36	3.09	0.06	0.82
7.66	1.06	11.08	7.81	86.60	3.09	0.06	0.79
7.68	1.04	10.84	7.67	83.10	3.08	0.06	0.77
7.70	1.02	10.52	7.44	78.29	3.06	0.06	0.75
7.72	0.98	10.02	7.41	74.22	3.06	0.06	0.72
7.74	0.92	9.29	7.63	70.90	3.08	0.06	0.66
7.76	0.86	8.52	8.16	69.49	3.12	0.06	0.61
7.78	0.81	7.94	8.63	68.53	3.15	0.06	0.57
7.80	0.77	7.46	9.07	67.67	3.19	0.06	0.53
7.82	0.74	7.08	9.41	66.67	3.21	0.06	0.51
7.84	0.72	6.81	9.65	65.68	3.23	0.06	0.49
7.86	0.76	7.35	9.02	66.33	3.18	0.06	0.53
7.88	0.81	7.83	8.59	67.25	3.15	0.06	0.56
7.90	0.83	8.12	8.42	68.42	3.14	0.06	0.58
7.92	0.78	7.51	9.15	68.75	3.19	0.06	0.54

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.94	0.75	7.17	9.55	68.47	3.22	0.06	0.51
7.96	0.75	7.12	9.56	68.02	3.22	0.06	0.51
7.98	0.76	7.26	9.17	66.59	3.19	0.06	0.52
8.00	0.78	7.40	8.75	64.77	3.16	0.06	0.53
8.02	0.80	7.69	8.14	62.60	3.12	0.06	0.55
8.04	0.86	8.36	7.30	61.02	3.05	0.06	0.60
8.06	0.95	9.31	6.42	59.77	2.97	0.06	0.66
8.08	0.99	9.81	6.12	60.06	2.94	0.06	0.70
8.10	0.96	9.44	6.44	60.82	2.97	0.06	0.67
8.12	0.89	8.60	7.15	61.47	3.04	0.06	0.61
8.14	0.83	7.94	7.72	61.33	3.08	0.06	0.57
8.16	0.81	7.68	8.09	62.07	3.11	0.06	0.55
8.18	0.81	7.65	8.32	63.66	3.13	0.06	0.55
8.20	0.82	7.68	8.45	64.88	3.14	0.06	0.55
8.22	0.82	7.70	8.49	65.33	3.14	0.06	0.55
8.24	0.82	7.66	8.48	65.02	3.14	0.06	0.55
8.26	0.82	7.71	8.45	65.15	3.14	0.06	0.55
8.28	0.83	7.81	8.44	65.93	3.14	0.06	0.56
8.30	0.82	7.68	8.67	66.58	3.16	0.06	0.55
8.32	0.77	7.11	9.33	66.37	3.21	0.06	0.51
8.34	0.71	6.36	10.26	65.24	3.27	0.06	0.45
8.36	0.67	5.95	10.79	64.20	3.30	0.06	0.43
8.38	0.67	5.93	10.79	64.01	3.30	0.06	0.42
8.40	0.71	6.36	10.19	64.81	3.26	0.06	0.45
8.42	0.75	6.83	9.66	65.96	3.23	0.06	0.49
8.44	0.80	7.36	9.00	66.20	3.18	0.06	0.53
8.46	0.82	7.50	8.66	64.98	3.16	0.06	0.54
8.48	0.80	7.30	8.69	63.43	3.16	0.06	0.52
8.50	0.77	6.96	9.09	63.33	3.19	0.06	0.50
8.52	0.75	6.70	9.54	63.94	3.22	0.06	0.48
8.54	0.73	6.50	9.86	64.04	3.24	0.06	0.46
8.56	0.69	6.00	10.45	62.74	3.28	0.06	0.43
8.58	0.64	5.45	11.25	61.31	3.33	0.06	0.39
8.60	0.58	4.79	12.42	59.45	3.41	0.06	0.34
8.62	0.54	4.29	13.37	57.29	3.46	0.06	0.31
8.64	0.50	3.89	13.91	54.14	3.49	0.06	0.28
8.66	0.49	3.80	13.62	51.70	3.47	0.06	0.27
8.68	0.52	4.05	12.39	50.14	3.40	0.06	0.29
8.70	0.55	4.37	11.30	49.33	3.34	0.06	0.31
8.72	0.57	4.56	10.82	49.36	3.31	0.06	0.33
8.74	0.58	4.66	10.73	50.06	3.30	0.06	0.33
8.76	0.61	5.01	10.13	50.76	3.26	0.06	0.36
8.78	0.67	5.70	9.01	51.37	3.18	0.06	0.41
8.80	0.75	6.55	7.90	51.72	3.10	0.06	0.47
8.82	0.82	7.26	7.34	53.27	3.05	0.06	0.52
8.84	0.86	7.66	7.15	54.76	3.04	0.06	0.55
8.86	0.90	8.15	7.23	58.92	3.04	0.06	0.58
8.88	0.84	7.47	8.32	62.14	3.13	0.06	0.53

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.90	0.76	6.55	9.61	62.97	3.23	0.06	0.47
8.92	0.64	5.30	11.35	60.18	3.34	0.06	0.38
8.94	0.65	5.35	10.92	58.46	3.31	0.06	0.38
8.96	0.66	5.47	10.43	57.03	3.28	0.06	0.39
8.98	0.68	5.67	9.75	55.32	3.24	0.06	0.41
9.00	0.66	5.46	9.64	52.68	3.23	0.06	0.39
9.02	0.65	5.29	9.65	51.02	3.23	0.06	0.38
9.04	0.62	4.99	10.12	50.52	3.26	0.06	0.36
9.06	0.63	5.07	9.98	50.65	3.25	0.06	0.36
9.08	0.67	5.51	9.30	51.20	3.20	0.06	0.39
9.10	0.73	6.16	8.42	51.86	3.14	0.06	0.44
9.12	0.79	6.78	7.81	52.92	3.09	0.06	0.48
9.14	0.86	7.54	7.20	54.34	3.04	0.06	0.54
9.16	0.97	8.64	6.44	55.67	2.97	0.06	0.62
9.18	1.14	10.42	5.59	58.25	2.89	0.07	0.74
9.20	1.32	12.28	5.04	61.87	2.83	0.07	0.88
9.22	1.43	13.46	4.99	67.11	2.82	0.07	0.96
9.24	1.40	13.20	5.38	70.98	2.87	0.07	0.94
9.26	1.29	11.97	6.10	73.03	2.94	0.07	0.85
9.28	1.16	10.54	6.92	72.99	3.02	0.06	0.75
9.30	1.05	9.43	7.67	72.28	3.08	0.06	0.67
9.32	0.97	8.49	8.36	70.91	3.13	0.06	0.61
9.34	0.96	8.44	8.30	70.00	3.13	0.06	0.60
9.36	1.01	8.96	7.83	70.15	3.09	0.06	0.64
9.38	1.09	9.77	7.38	72.08	3.05	0.06	0.70
9.40	1.14	10.29	7.10	73.07	3.03	0.06	0.73
9.42	1.19	10.77	6.80	73.29	3.01	0.06	0.77
9.44	1.23	11.14	6.58	73.32	2.99	0.06	0.80
9.46	1.18	10.65	7.01	74.70	3.02	0.06	0.76
9.48	1.03	9.06	8.32	75.34	3.13	0.06	0.65
9.50	0.85	7.08	10.32	73.03	3.27	0.06	0.51
9.52	0.71	5.66	12.15	68.74	3.39	0.06	0.40
9.54	0.65	5.07	12.88	65.29	3.43	0.06	0.36
9.56	0.65	5.01	12.69	63.53	3.42	0.06	0.36
9.58	0.67	5.21	11.91	62.05	3.37	0.06	0.37
9.60	0.69	5.43	11.08	60.22	3.32	0.06	0.39
9.62	0.72	5.73	10.08	57.70	3.26	0.06	0.41
9.64	0.73	5.81	9.60	55.78	3.22	0.06	0.41
9.66	0.71	5.55	9.86	54.72	3.24	0.06	0.40
9.68	0.66	5.11	10.67	54.52	3.30	0.06	0.36
9.70	0.63	4.71	11.44	53.89	3.35	0.06	0.34
9.72	0.64	4.80	11.25	54.03	3.33	0.06	0.34
9.74	0.67	5.13	10.57	54.26	3.29	0.06	0.37
9.76	0.70	5.45	10.05	54.80	3.26	0.06	0.39
9.78	0.72	5.59	9.85	55.07	3.24	0.06	0.40
9.80	0.85	6.89	8.11	55.88	3.11	0.06	0.49
9.82	1.19	10.43	5.36	55.85	2.86	0.07	0.75
9.84	1.77	16.27	3.57	58.01	2.64	0.08	1.16

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.86	2.38	22.35	2.77	61.82	2.50	0.08	0.64
9.88	2.86	27.22	2.39	65.02	2.42	0.09	0.66
9.90	3.09	29.44	2.18	64.03	2.36	0.09	0.67
9.92	2.98	28.32	2.11	59.84	2.35	0.09	0.66
9.94	2.54	23.82	2.27	54.16	2.39	0.08	0.64
9.96	1.95	17.89	2.84	50.78	2.51	0.08	0.61
9.98	1.47	13.10	4.07	53.35	2.71	0.07	0.94
10.00	1.22	10.54	5.76	60.71	2.91	0.07	0.75
10.03	1.12	9.48	6.90	65.36	3.01	0.06	0.68
10.04	1.20	10.29	6.62	68.14	2.99	0.06	0.74
10.06	1.40	12.24	5.52	67.61	2.88	0.07	0.87
10.08	1.61	14.30	4.69	67.14	2.79	0.08	1.02
10.10	1.65	14.71	4.47	65.80	2.76	0.08	1.05
10.12	1.54	13.62	4.80	65.43	2.80	0.07	0.97
10.15	1.44	12.53	5.40	67.61	2.87	0.07	0.90
10.16	1.37	11.89	5.97	70.95	2.93	0.07	0.85
10.18	1.37	11.81	6.25	73.88	2.95	0.07	0.84
10.20	1.38	11.87	6.32	75.05	2.96	0.07	0.85
10.22	1.36	11.71	6.56	76.79	2.98	0.07	0.84
10.24	1.27	10.75	7.20	77.37	3.04	0.06	0.77
10.26	1.10	9.11	8.42	76.70	3.14	0.06	0.65
10.28	0.92	7.29	10.09	73.50	3.26	0.06	0.52
10.30	0.80	6.15	11.42	70.24	3.34	0.06	0.44
10.32	0.76	5.70	11.88	67.77	3.37	0.06	0.41
10.34	0.75	5.60	11.82	66.16	3.37	0.06	0.40
10.36	0.75	5.60	11.57	64.77	3.35	0.06	0.40
10.38	0.75	5.61	11.15	62.56	3.33	0.06	0.40
10.40	0.78	5.83	10.35	60.39	3.28	0.06	0.42
10.42	0.81	6.18	9.51	58.81	3.22	0.06	0.44
10.44	0.85	6.50	9.12	59.27	3.19	0.06	0.46
10.46	0.88	6.81	8.90	60.60	3.17	0.06	0.49
10.48	0.90	7.00	8.93	62.50	3.18	0.06	0.50
10.50	0.93	7.30	8.79	64.21	3.17	0.06	0.52
10.52	0.96	7.57	8.64	65.42	3.16	0.06	0.54
10.54	0.99	7.77	8.58	66.67	3.15	0.06	0.56
10.56	1.00	7.94	8.53	67.68	3.15	0.06	0.57
10.58	1.01	7.96	8.62	68.59	3.15	0.06	0.57
10.60	1.00	7.82	8.82	68.98	3.17	0.06	0.56
10.62	0.94	7.28	9.45	68.84	3.21	0.06	0.52
10.64	0.87	6.54	10.38	67.93	3.28	0.06	0.47
10.66	0.79	5.78	11.50	66.46	3.35	0.06	0.41
10.68	0.74	5.33	12.18	64.87	3.39	0.06	0.38
10.70	0.73	5.19	12.27	63.65	3.40	0.06	0.37
10.72	0.72	5.13	12.14	62.27	3.39	0.06	0.37
10.74	0.70	4.89	12.34	60.39	3.40	0.06	0.35
10.76	0.67	4.58	12.67	58.08	3.42	0.06	0.33
10.78	0.64	4.27	13.04	55.69	3.44	0.06	0.31
10.80	0.62	4.11	13.08	53.73	3.44	0.06	0.29

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.82	0.61	3.98	13.16	52.37	3.45	0.06	0.28
10.84	0.64	4.32	12.75	55.03	3.42	0.06	0.31
10.86	0.67	4.54	12.59	57.10	3.42	0.06	0.32
10.88	0.69	4.79	12.31	58.92	3.40	0.06	0.34
10.91	0.68	4.66	12.29	57.29	3.40	0.06	0.33
10.92	0.68	4.63	12.09	55.94	3.39	0.06	0.33
10.94	0.66	4.48	12.17	54.47	3.39	0.06	0.32
10.96	0.65	4.31	12.22	52.69	3.39	0.06	0.31
10.98	0.65	4.28	11.93	51.10	3.38	0.06	0.31
11.00	0.65	4.29	11.60	49.73	3.36	0.06	0.31
11.02	0.65	4.29	11.41	48.90	3.34	0.06	0.31
11.05	0.64	4.21	11.49	48.32	3.35	0.06	0.30
11.06	0.65	4.28	11.24	48.10	3.33	0.06	0.31
11.08	0.66	4.40	10.92	47.98	3.31	0.06	0.31
11.10	0.68	4.56	10.57	48.18	3.29	0.06	0.33
11.12	0.70	4.72	10.22	48.23	3.27	0.06	0.34
11.14	0.71	4.85	9.96	48.27	3.25	0.06	0.35
11.16	0.71	4.83	9.99	48.24	3.25	0.06	0.34
11.18	0.69	4.65	10.45	48.60	3.28	0.06	0.33
11.20	0.67	4.39	11.23	49.30	3.33	0.06	0.31
11.22	0.65	4.23	11.80	49.91	3.37	0.06	0.30
11.24	0.64	4.11	12.14	49.91	3.39	0.06	0.29
11.26	0.63	4.04	12.36	49.94	3.40	0.06	0.29
11.28	0.63	4.00	12.55	50.18	3.41	0.06	0.29
11.30	0.64	4.08	12.49	50.90	3.41	0.06	0.29
11.32	0.67	4.38	11.80	51.67	3.37	0.06	0.31
11.34	0.72	4.84	10.86	52.55	3.31	0.06	0.35
11.36	0.78	5.36	10.07	53.93	3.26	0.06	0.38
11.38	0.83	5.79	9.66	55.92	3.23	0.06	0.41
11.40	0.87	6.15	9.50	58.44	3.22	0.06	0.44
11.42	0.90	6.44	9.45	60.92	3.21	0.06	0.46
11.44	0.93	6.73	9.40	63.29	3.21	0.06	0.48
11.46	0.95	6.91	9.52	65.83	3.22	0.06	0.49
11.48	0.97	7.09	9.67	68.56	3.23	0.06	0.51
11.50	0.97	7.06	10.05	70.93	3.26	0.06	0.50
11.52	0.97	7.02	10.36	72.72	3.28	0.06	0.50
11.54	0.96	6.93	10.65	73.77	3.30	0.06	0.49
11.56	0.96	6.88	10.84	74.53	3.31	0.06	0.49
11.58	0.96	6.86	10.91	74.84	3.31	0.06	0.49
11.60	0.94	6.72	11.14	74.87	3.33	0.06	0.48
11.62	0.93	6.63	11.31	74.96	3.34	0.06	0.47
11.64	0.92	6.52	11.50	75.00	3.35	0.06	0.47
11.66	0.93	6.53	11.51	75.23	3.35	0.06	0.47
11.68	0.94	6.62	11.39	75.40	3.34	0.06	0.47
11.70	0.95	6.72	11.24	75.54	3.33	0.06	0.48
11.72	0.97	6.88	10.99	75.63	3.32	0.06	0.49
11.74	0.98	6.93	10.85	75.20	3.31	0.06	0.50
11.76	0.98	6.92	10.71	74.14	3.30	0.06	0.49

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.78	0.97	6.86	10.55	72.35	3.29	0.06	0.49
11.80	0.97	6.87	10.27	70.58	3.27	0.06	0.49
11.82	0.98	6.96	10.00	69.56	3.25	0.06	0.50
11.84	0.99	7.03	9.83	69.08	3.24	0.06	0.50
11.86	1.00	7.08	9.73	68.84	3.23	0.06	0.51
11.89	1.00	7.03	9.67	68.02	3.23	0.06	0.50
11.90	0.99	6.93	9.69	67.13	3.23	0.06	0.49
11.92	0.97	6.79	9.78	66.42	3.24	0.06	0.49
11.94	0.95	6.63	9.95	65.90	3.25	0.06	0.47
11.96	0.94	6.45	10.09	65.03	3.26	0.06	0.46
11.98	0.91	6.17	10.29	63.49	3.27	0.06	0.44
12.00	0.87	5.87	10.51	61.69	3.29	0.06	0.42
12.02	0.85	5.67	10.56	59.91	3.29	0.06	0.41
12.04	0.83	5.51	10.57	58.26	3.29	0.06	0.39
12.06	0.82	5.42	10.45	56.60	3.28	0.06	0.39
12.08	0.81	5.24	10.50	55.02	3.29	0.06	0.37
12.10	0.79	5.09	10.53	53.61	3.29	0.06	0.36
12.12	0.78	4.99	10.46	52.20	3.28	0.06	0.36
12.14	0.78	4.98	10.26	51.05	3.27	0.06	0.36
12.16	0.78	4.97	10.08	50.06	3.26	0.06	0.35
12.18	0.78	4.93	10.02	49.42	3.25	0.06	0.35
12.20	0.76	4.82	10.18	49.04	3.26	0.06	0.34
12.22	0.76	4.74	10.29	48.77	3.27	0.06	0.34
12.24	0.75	4.69	10.34	48.48	3.28	0.06	0.34
12.26	0.75	4.70	10.25	48.18	3.27	0.06	0.34
12.28	0.76	4.74	10.14	48.04	3.26	0.06	0.34
12.30	0.77	4.84	9.98	48.28	3.25	0.06	0.35
12.32	0.80	5.05	9.65	48.78	3.23	0.06	0.36
12.34	0.81	5.14	9.55	49.08	3.22	0.06	0.37
12.36	0.80	5.04	9.76	49.18	3.24	0.06	0.36
12.38	0.76	4.76	10.22	48.64	3.27	0.06	0.34
12.40	0.73	4.48	10.67	47.79	3.30	0.06	0.32
12.42	0.71	4.29	10.94	46.87	3.31	0.06	0.31
12.44	0.70	4.16	11.12	46.22	3.33	0.06	0.30
12.46	0.70	4.15	11.10	46.01	3.32	0.06	0.30
12.48	0.70	4.17	11.13	46.39	3.33	0.06	0.30
12.50	0.71	4.22	11.14	47.04	3.33	0.06	0.30
12.52	0.69	4.11	11.51	47.25	3.35	0.06	0.29
12.54	0.67	3.93	11.90	46.78	3.37	0.06	0.28
12.56	0.64	3.64	12.63	45.99	3.42	0.06	0.26
12.58	0.64	3.61	12.72	45.93	3.42	0.06	0.26
12.60	0.66	3.82	12.07	46.15	3.38	0.06	0.27
12.62	0.71	4.23	10.94	46.30	3.31	0.06	0.30
12.64	0.74	4.42	10.43	46.09	3.28	0.06	0.32
12.66	0.72	4.23	10.82	45.80	3.31	0.06	0.30
12.68	0.68	3.92	11.54	45.19	3.35	0.06	0.28
12.70	0.66	3.75	11.85	44.49	3.37	0.06	0.27
12.72	0.67	3.80	11.58	43.96	3.35	0.06	0.27

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.74	0.67	3.84	11.33	43.56	3.34	0.06	0.27
12.76	0.67	3.78	11.52	43.52	3.35	0.06	0.27
12.78	0.66	3.70	11.77	43.59	3.37	0.06	0.26
12.80	0.69	4.00	11.53	46.18	3.35	0.06	0.29
12.82	0.72	4.20	11.47	48.25	3.35	0.06	0.30
12.84	0.75	4.48	11.28	50.61	3.34	0.06	0.32
12.86	0.75	4.49	11.29	50.67	3.34	0.06	0.32
12.88	0.78	4.68	10.91	51.06	3.31	0.06	0.33
12.90	0.80	4.89	10.51	51.37	3.29	0.06	0.35
12.92	0.84	5.15	10.12	52.07	3.26	0.06	0.37
12.94	0.89	5.58	9.45	52.69	3.21	0.06	0.40
12.96	0.96	6.17	8.64	53.30	3.15	0.06	0.44
12.98	1.03	6.76	8.02	54.25	3.11	0.06	0.48
13.00	1.12	7.45	7.39	55.10	3.06	0.06	0.53
13.02	1.14	7.66	7.36	56.44	3.05	0.06	0.55
13.04	1.10	7.29	7.96	58.05	3.10	0.06	0.52
13.06	0.99	6.39	9.21	58.82	3.20	0.06	0.46
13.08	0.92	5.80	10.14	58.85	3.26	0.06	0.41
13.10	0.93	5.85	10.00	58.56	3.25	0.06	0.42
13.12	0.96	6.11	9.73	59.42	3.23	0.06	0.44
13.14	1.02	6.57	9.18	60.31	3.20	0.06	0.47
13.16	1.11	7.27	8.31	60.47	3.13	0.06	0.52
13.18	1.14	7.51	8.07	60.59	3.11	0.06	0.54
13.20	1.08	7.07	8.70	61.47	3.16	0.06	0.50
13.22	0.98	6.24	10.00	62.42	3.25	0.06	0.45
13.24	0.96	6.06	10.35	62.68	3.28	0.06	0.43
13.26	0.98	6.22	10.03	62.37	3.25	0.06	0.44
13.28	0.96	6.01	10.31	61.91	3.27	0.06	0.43
13.30	0.90	5.48	11.11	60.94	3.33	0.06	0.39
13.32	0.87	5.22	11.32	59.10	3.34	0.06	0.37
13.34	0.94	5.82	9.91	57.70	3.25	0.06	0.42
13.36	1.10	7.09	7.96	56.42	3.10	0.06	0.51
13.38	1.23	8.21	6.85	56.18	3.01	0.06	0.59
13.40	1.27	8.45	6.80	57.45	3.01	0.06	0.60
13.42	1.22	8.09	7.28	58.87	3.05	0.06	0.58
13.44	1.34	8.99	6.72	60.38	3.00	0.06	0.64
13.46	1.64	11.43	5.38	61.47	2.87	0.07	0.82
13.48	2.11	15.38	4.19	64.46	2.73	0.08	1.09
13.50	2.48	18.51	3.63	67.26	2.65	0.09	1.30
13.52	2.63	19.85	3.33	66.17	2.60	0.09	1.39
13.54	2.47	18.48	3.29	60.76	2.59	0.08	0.61
13.56	2.13	15.59	3.46	53.99	2.62	0.08	1.09
13.58	1.72	12.14	4.34	52.68	2.75	0.08	0.86
13.60	1.42	9.57	5.71	54.69	2.90	0.07	0.68
13.62	1.21	7.85	7.29	57.26	3.05	0.06	0.56
13.64	1.10	6.95	8.34	57.94	3.13	0.06	0.50
13.66	1.02	6.33	9.15	57.91	3.19	0.06	0.45
13.68	0.96	5.81	9.80	56.97	3.24	0.06	0.42

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.70	0.92	5.52	9.99	55.14	3.25	0.06	0.39
13.72	0.92	5.47	9.80	53.59	3.24	0.06	0.39
13.74	0.91	5.38	9.88	53.11	3.24	0.06	0.38
13.76	0.90	5.32	10.11	53.81	3.26	0.06	0.38
13.78	0.95	5.72	9.52	54.44	3.22	0.06	0.41
13.80	1.14	7.18	8.08	58.03	3.11	0.06	0.51
13.82	1.24	8.02	7.71	61.86	3.08	0.06	0.57
13.84	1.21	7.72	8.56	66.07	3.15	0.06	0.55
13.86	1.08	6.71	9.71	65.19	3.23	0.06	0.48
13.89	1.16	7.33	8.74	64.08	3.16	0.06	0.52
13.90	1.54	10.35	6.08	62.86	2.94	0.07	0.74
13.92	1.96	13.67	4.74	64.75	2.79	0.08	0.97
13.94	2.20	15.65	4.33	67.75	2.74	0.08	1.11
13.96	2.13	15.04	4.61	69.31	2.78	0.08	1.07
13.98	1.96	13.63	4.94	67.37	2.82	0.08	0.97
14.00	1.86	12.75	5.08	64.79	2.83	0.07	0.91
14.02	1.89	13.02	4.98	64.87	2.82	0.08	0.93
14.04	1.95	13.42	5.06	67.89	2.83	0.08	0.96
14.06	2.00	13.82	5.12	70.81	2.84	0.08	0.99
14.08	2.14	14.91	4.96	73.98	2.82	0.08	1.06
14.10	2.37	16.83	4.46	75.04	2.76	0.08	1.19
14.12	2.57	18.47	4.06	74.92	2.71	0.09	1.30
14.14	2.61	18.76	3.89	73.03	2.69	0.09	1.32
14.16	2.60	18.67	3.89	72.70	2.69	0.08	1.31
14.18	2.64	18.98	3.93	74.55	2.69	0.09	1.34
14.21	2.83	20.46	3.78	77.37	2.67	0.09	1.44
14.22	3.06	22.34	3.46	77.28	2.62	0.09	1.56
14.24	3.28	24.27	3.07	74.48	2.56	0.09	0.65
14.26	3.39	25.17	2.79	70.09	2.50	0.09	0.65
14.28	3.32	24.66	2.66	65.48	2.48	0.09	0.65
14.30	3.07	22.64	2.68	60.73	2.48	0.09	0.64
14.32	2.73	19.78	2.91	57.51	2.53	0.08	0.62
14.34	2.37	16.76	3.51	58.73	2.63	0.08	1.17
14.37	2.13	14.62	4.38	64.09	2.75	0.08	1.03
14.38	2.04	13.86	5.02	69.58	2.83	0.08	0.99
14.40	2.16	14.77	5.01	73.93	2.83	0.08	1.05
14.42	2.54	17.80	4.28	76.11	2.74	0.08	1.26
14.44	3.03	21.84	3.49	76.29	2.63	0.09	1.53
14.46	3.46	25.39	2.95	74.88	2.53	0.09	0.65
14.48	3.59	26.52	2.75	72.93	2.50	0.09	0.66
14.50	3.52	25.91	2.66	68.81	2.48	0.09	0.65
14.52	3.33	24.41	2.60	63.55	2.47	0.09	0.65
14.54	3.17	23.24	2.46	57.24	2.44	0.08	0.64
14.56	3.11	22.77	2.34	53.24	2.41	0.08	0.64
14.58	3.13	22.95	2.34	53.73	2.41	0.08	0.64
14.60	3.21	23.39	2.53	59.18	2.45	0.09	0.64
14.62	3.23	23.39	2.83	66.30	2.51	0.09	0.64
14.64	3.17	22.77	3.11	70.82	2.56	0.09	0.64

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.66	2.95	20.96	3.39	71.05	2.61	0.09	1.46
14.68	2.69	18.75	3.74	70.06	2.66	0.09	1.31
14.70	2.47	16.97	4.21	71.42	2.73	0.08	1.20
14.72	2.46	16.77	4.49	75.21	2.76	0.08	1.19
14.74	2.55	17.46	4.56	79.62	2.77	0.08	1.24
14.76	2.74	18.84	4.45	83.73	2.76	0.09	1.33
14.78	2.94	20.49	4.07	83.35	2.71	0.09	1.44
14.80	3.10	21.76	3.83	83.44	2.68	0.09	1.53
14.82	3.06	21.44	3.77	80.75	2.67	0.09	1.50
14.84	2.80	19.26	4.20	80.84	2.73	0.09	1.36
14.86	2.42	16.25	4.80	77.95	2.80	0.08	1.16
14.88	2.04	13.35	5.68	75.86	2.90	0.07	0.95
14.90	1.92	12.40	5.95	73.74	2.93	0.07	0.89
14.92	2.06	13.42	5.32	71.32	2.86	0.08	0.96
14.94	2.28	15.11	4.70	71.06	2.79	0.08	1.07
14.96	2.17	14.22	4.93	70.08	2.82	0.08	1.01
14.98	1.77	11.24	6.22	69.87	2.95	0.07	0.80
15.00	1.30	7.71	8.75	67.45	3.16	0.06	0.55
15.02	1.04	5.78	11.05	63.86	3.32	0.06	0.41
15.04	0.93	4.93	12.46	61.45	3.41	0.06	0.35
15.06	0.94	5.04	12.02	60.56	3.38	0.06	0.36
15.08	0.93	4.99	12.27	61.18	3.40	0.06	0.36
15.10	0.91	4.81	12.74	61.25	3.42	0.06	0.34
15.12	0.89	4.61	12.96	59.67	3.44	0.06	0.33
15.15	0.88	4.55	12.59	57.25	3.42	0.06	0.32
15.16	0.89	4.59	11.95	54.85	3.38	0.06	0.33
15.18	0.91	4.75	11.29	53.59	3.34	0.06	0.34
15.20	0.93	4.89	10.81	52.84	3.31	0.06	0.35
15.22	0.93	4.91	10.69	52.46	3.30	0.06	0.35
15.24	0.92	4.85	10.77	52.22	3.30	0.06	0.35
15.26	0.92	4.80	10.91	52.34	3.31	0.06	0.34
15.28	0.93	4.90	10.81	52.91	3.31	0.06	0.35
15.30	0.95	5.02	10.65	53.42	3.30	0.06	0.36
15.32	0.95	5.02	10.73	53.88	3.30	0.06	0.36
15.34	0.91	4.68	11.47	53.64	3.35	0.06	0.33
15.36	0.86	4.33	12.18	52.70	3.39	0.06	0.31
15.38	0.85	4.22	12.22	51.63	3.39	0.06	0.30
15.40	0.91	4.67	10.98	51.28	3.32	0.06	0.33
15.42	1.03	5.56	9.34	51.88	3.21	0.06	0.40
15.44	1.18	6.62	8.08	53.54	3.11	0.06	0.47
15.46	1.33	7.70	7.21	55.52	3.04	0.06	0.55
15.48	1.44	8.51	6.84	58.15	3.01	0.06	0.61
15.50	1.54	9.18	6.60	60.59	2.99	0.06	0.66
15.52	1.56	9.32	6.84	63.74	3.01	0.06	0.67
15.54	1.46	8.63	7.80	67.28	3.09	0.06	0.62
15.56	1.31	7.50	9.27	69.53	3.20	0.06	0.54
15.58	1.19	6.61	10.62	70.20	3.29	0.06	0.47
15.60	1.22	6.82	10.27	70.00	3.27	0.06	0.49

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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LIQUEFACTION ANALYSIS REPORT

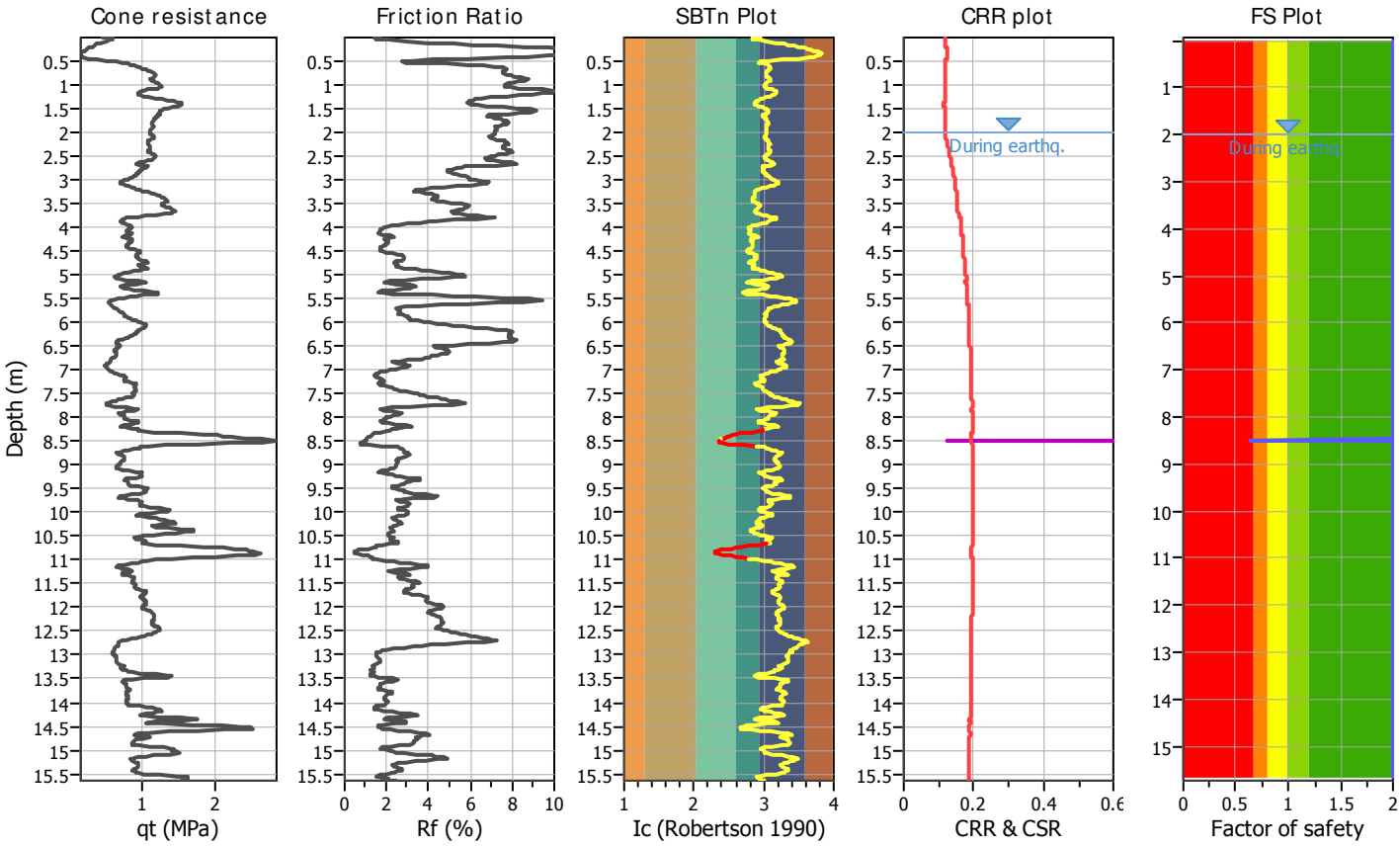
Project title :

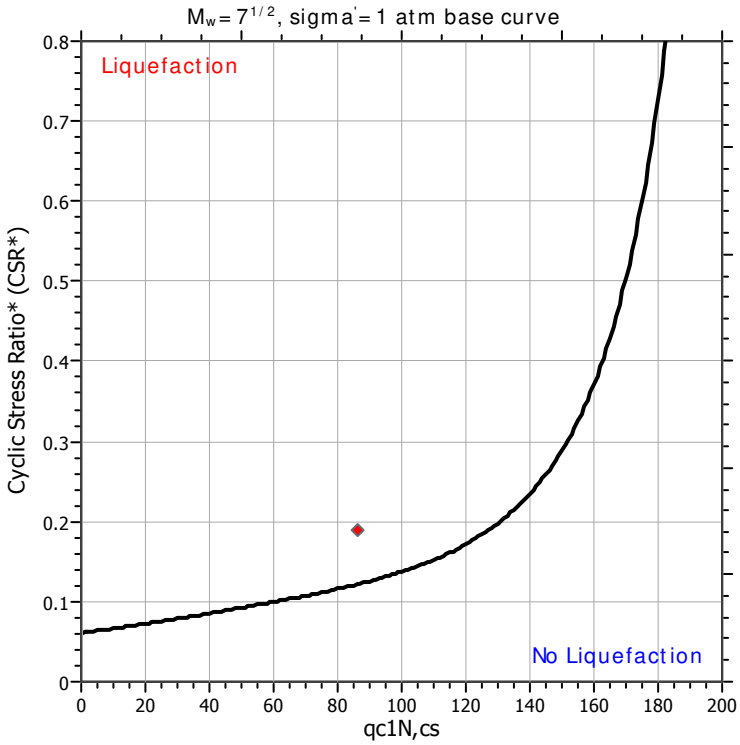
Location :

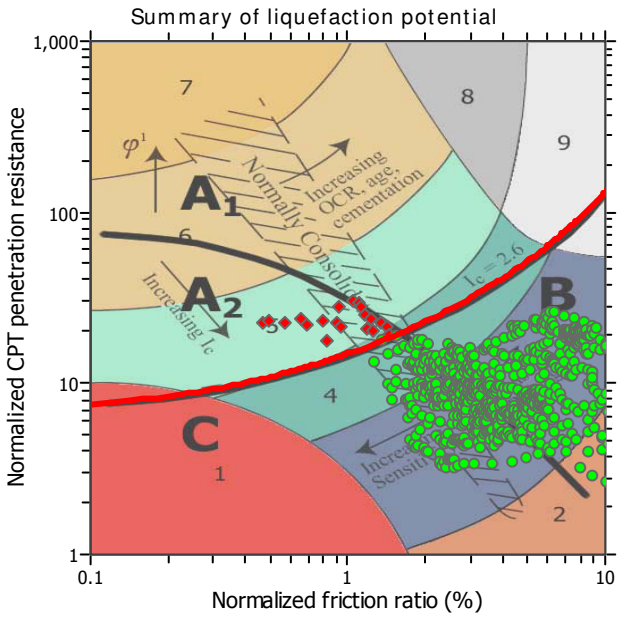
CPT file : Cptu-4

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.50 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.22	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

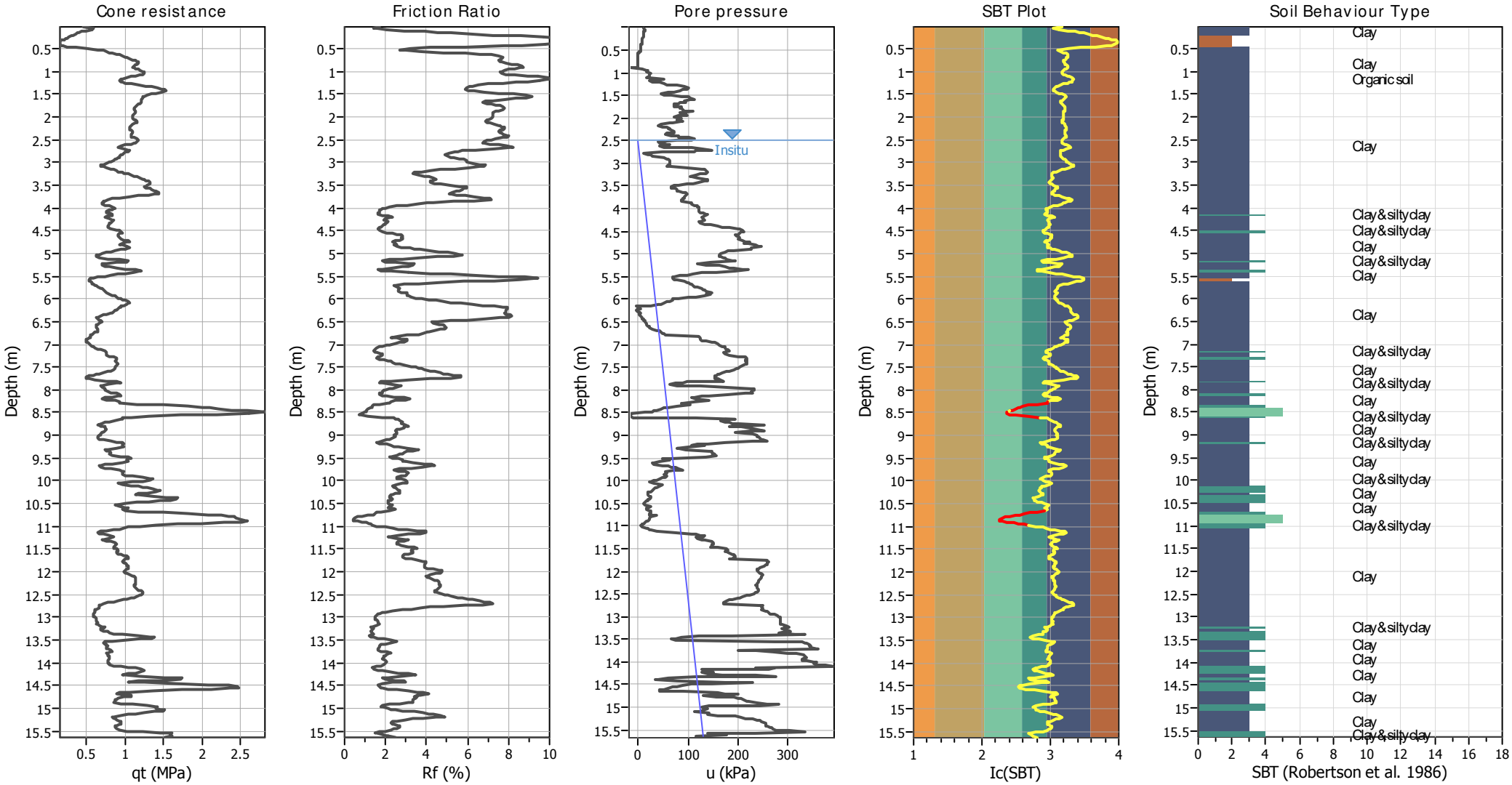






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



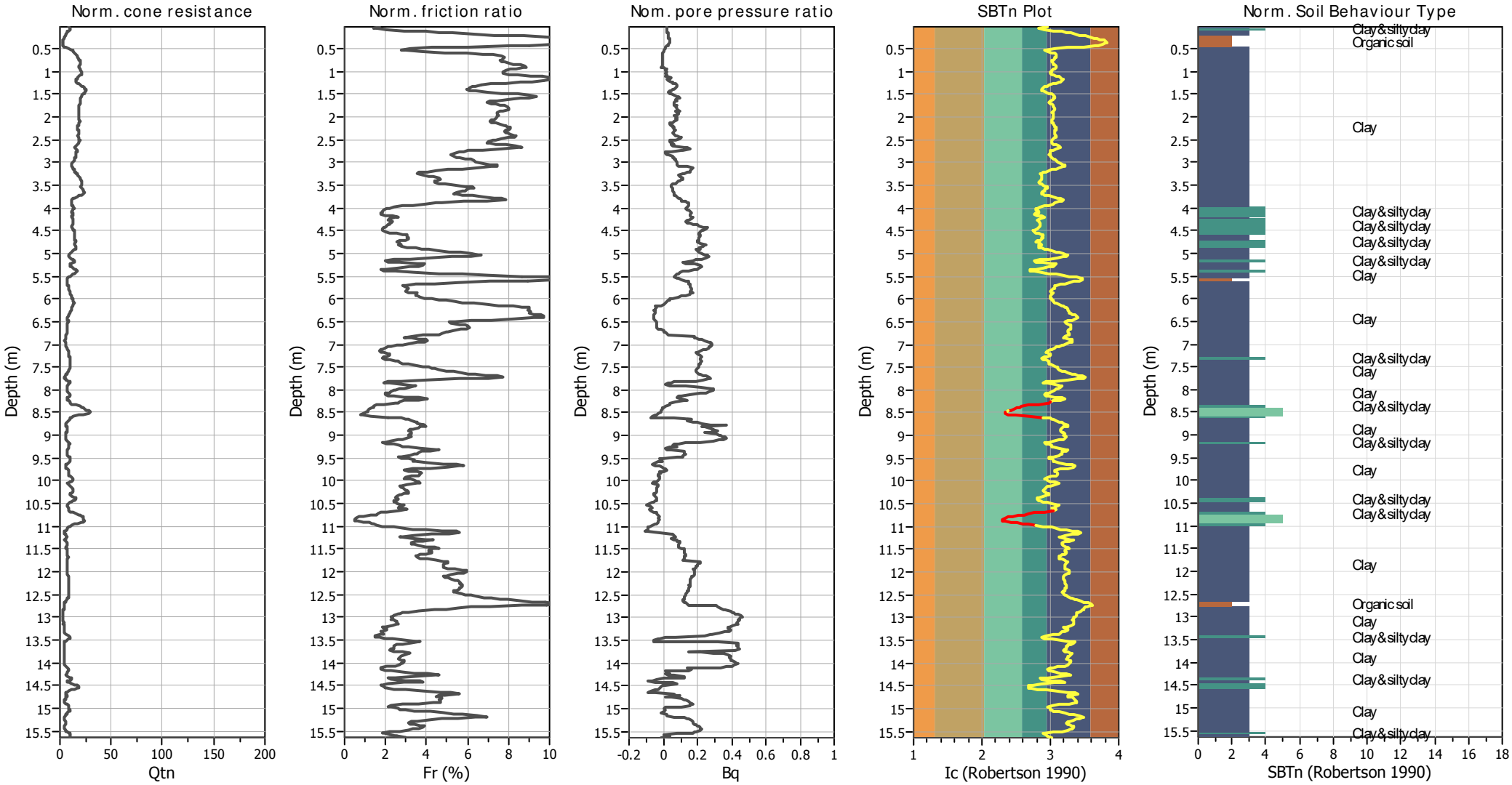
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



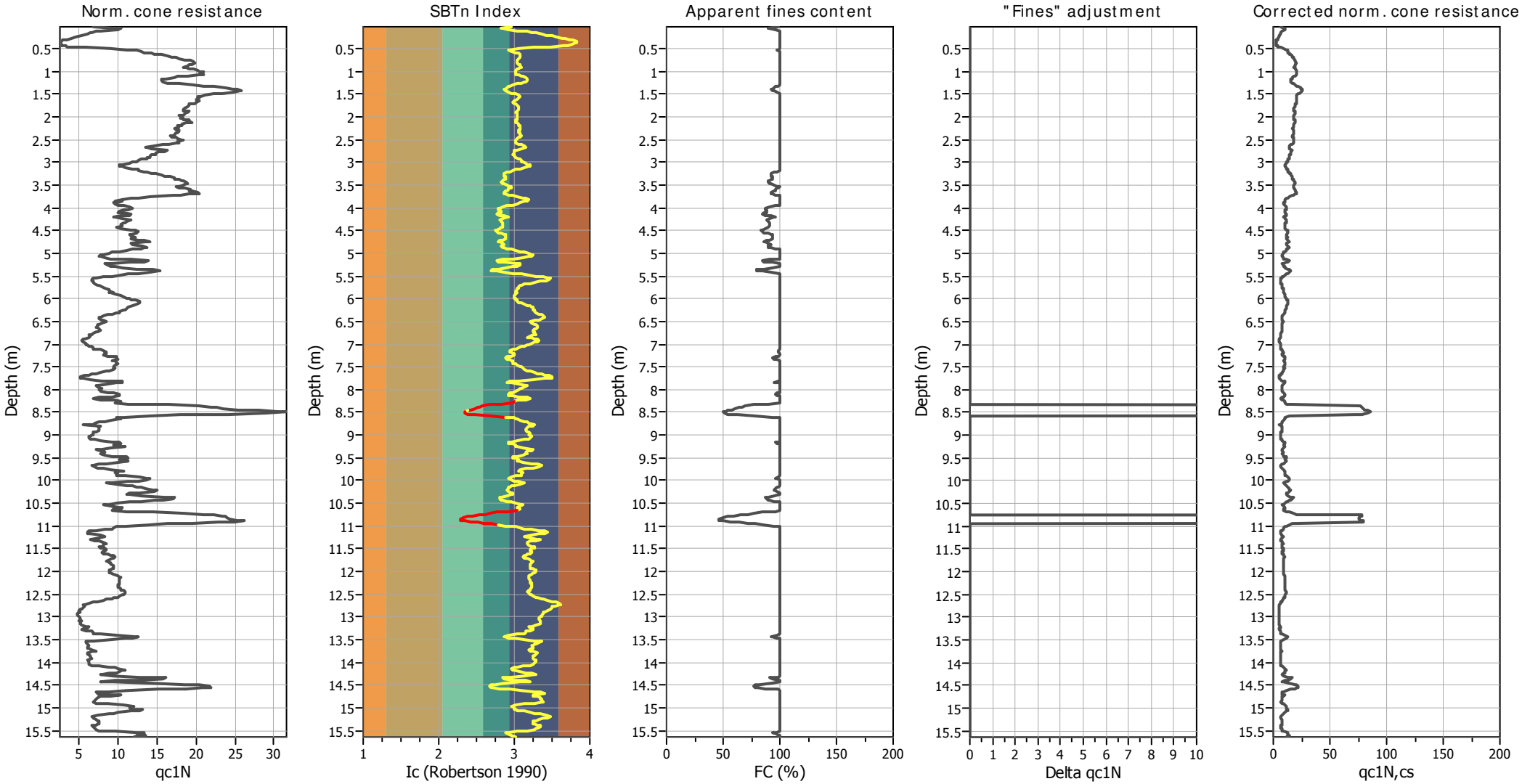
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

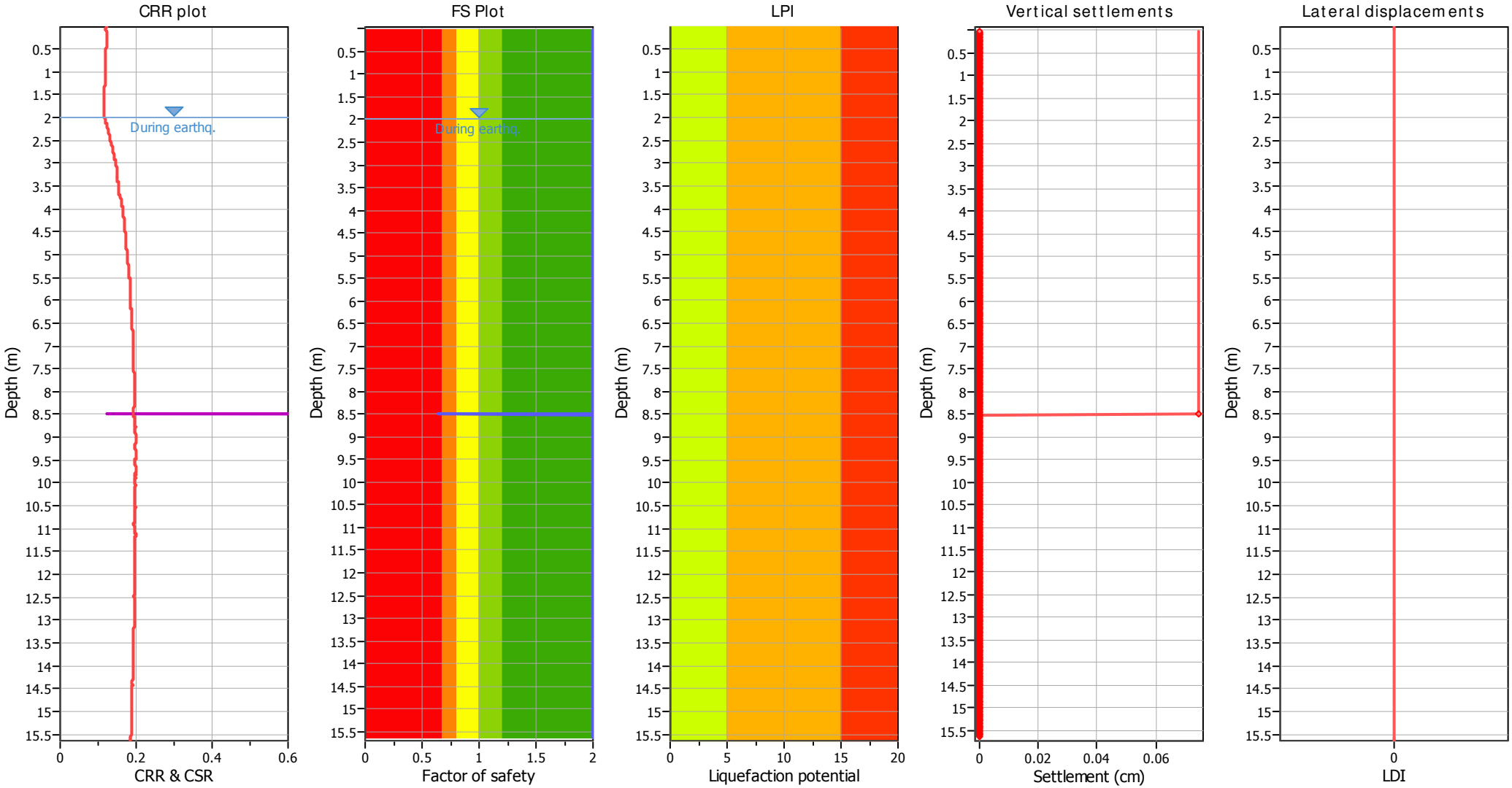
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

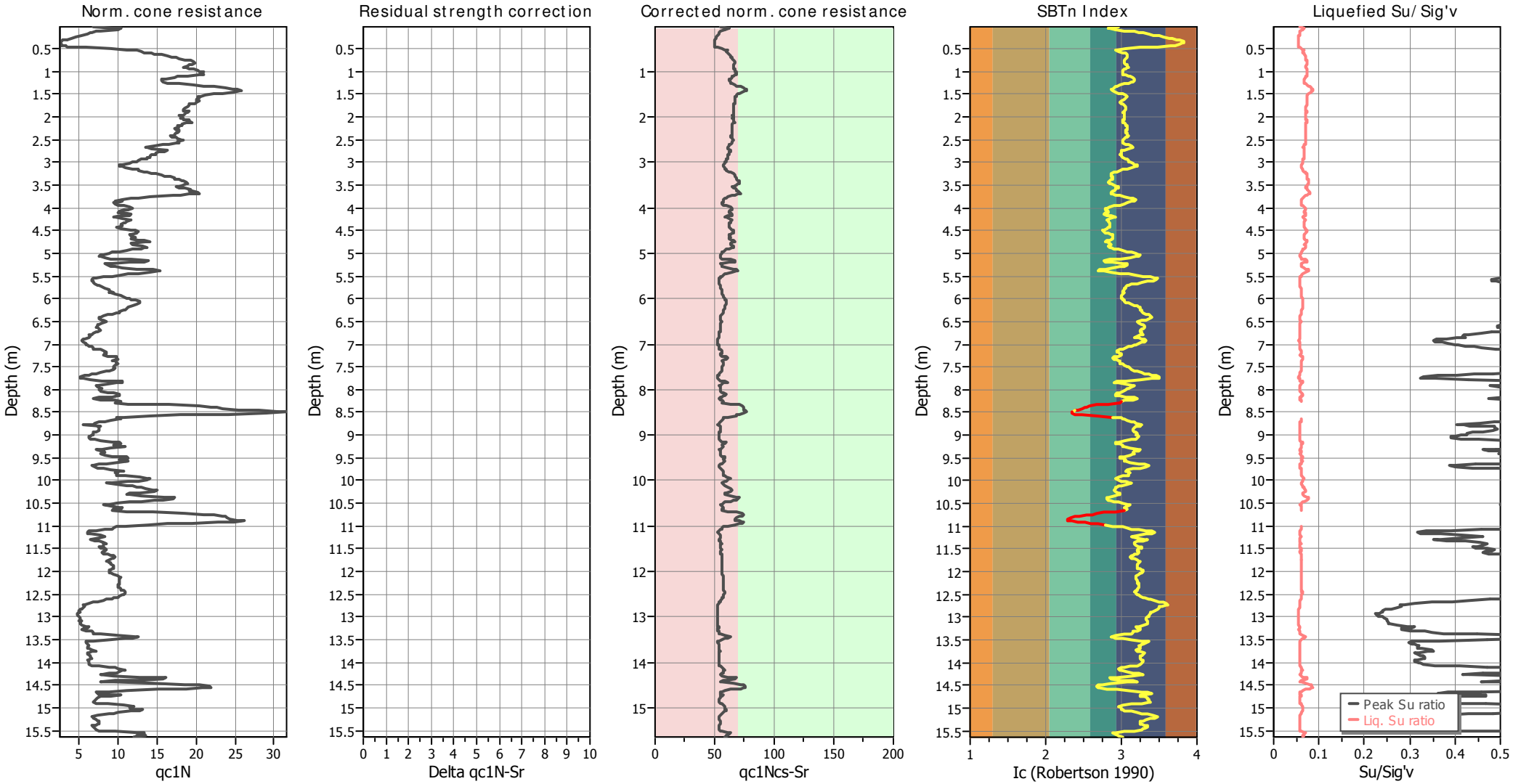
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

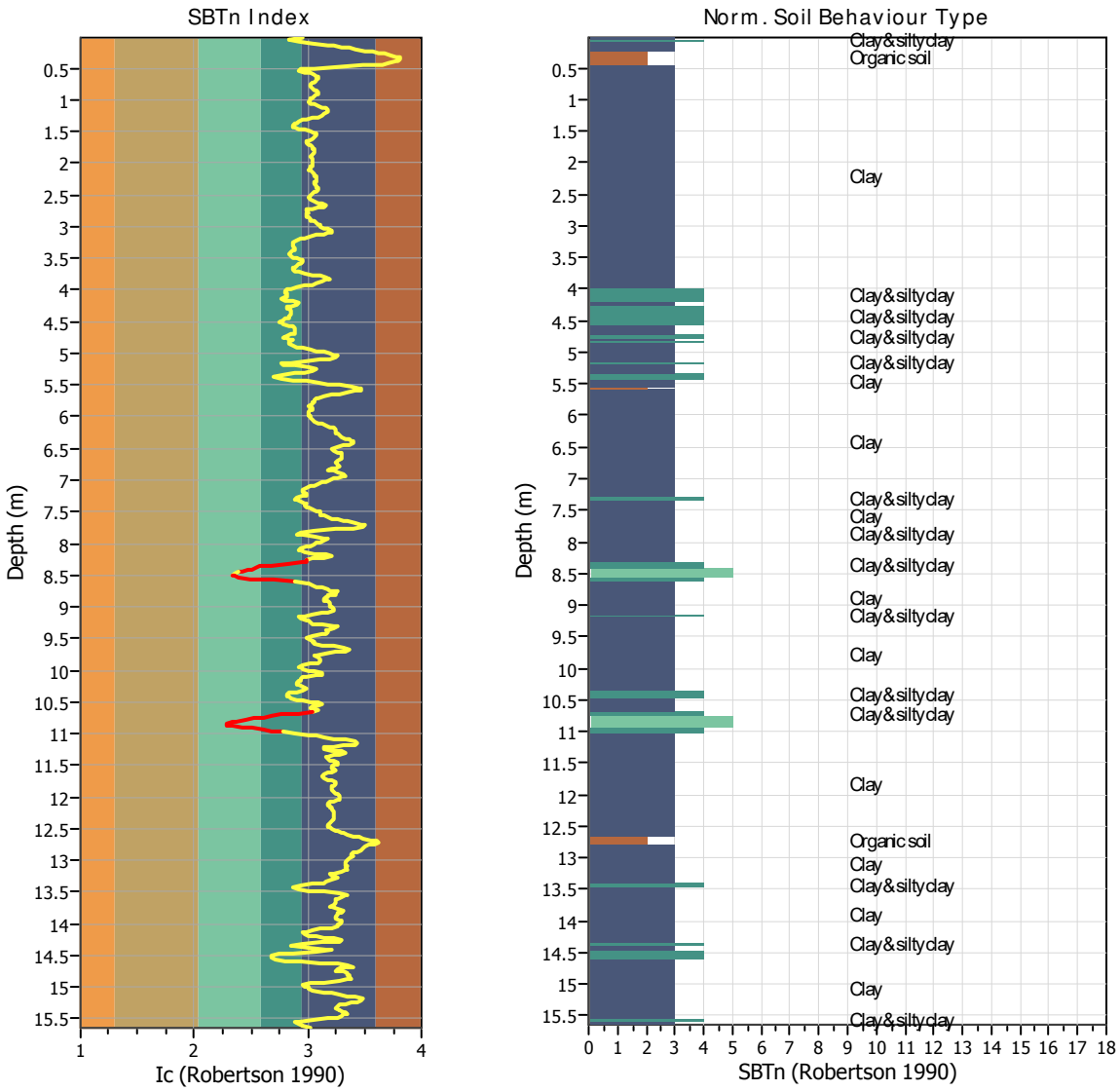
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	782
I_c maximum check value:	3.00	Total points excluded:	34
I_c change ratio value:	0.0100	Exclusion percentage:	4.35%
Minimum number of points in layer:	4	Number of layers detected:	4

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	11	Start depth: 8.28 (m)	3	Clay
		End depth: 8.48 (m)	5	Silty sand & sandy silt
Transition layer 2	6	Start depth: 8.52 (m)	5	Silty sand & sandy silt
		End depth: 8.62 (m)	3	Clay
Transition layer 3	9	Start depth: 10.68 (m)	3	Clay
		End depth: 10.84 (m)	5	Silty sand & sandy silt
Transition layer 4	8	Start depth: 10.87 (m)	5	Silty sand & sandy silt
		End depth: 11.00 (m)	4	Clay & silty clay

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.41	7.62	10.35	55.34	15.05
2	0.04	0.55	8.09	11.97	48.04	15.22
3	0.06	0.62	8.79	12.21	48.34	15.33
4	0.08	0.60	10.55	12.09	53.36	15.58
5	0.10	0.47	15.33	11.28	61.78	15.81
6	0.13	0.43	18.08	10.79	70.92	15.94
7	0.14	0.40	18.14	10.35	75.72	16.01
8	0.16	0.39	19.84	10.04	80.18	16.07
9	0.18	0.36	22.04	9.61	86.05	16.16
10	0.20	0.32	24.65	9.30	91.80	16.24
11	0.22	0.32	26.32	9.11	100.00	16.30
12	0.24	0.27	28.34	8.68	100.00	16.30
13	0.26	0.24	26.79	8.18	100.00	16.25
14	0.28	0.24	25.85	7.75	100.00	16.15
15	0.30	0.21	23.74	7.38	100.00	16.04
16	0.32	0.18	22.60	6.88	100.00	15.90
17	0.34	0.16	19.94	6.51	100.00	15.76
18	0.36	0.15	18.18	6.01	100.00	15.63
19	0.38	0.16	16.86	5.64	100.00	15.53
20	0.40	0.16	15.58	5.27	100.00	15.48
21	0.42	0.17	15.52	4.96	100.00	15.46
22	0.44	0.20	14.62	4.46	100.00	15.46
23	0.46	0.21	14.56	4.09	97.11	15.57
24	0.48	0.35	15.56	4.15	77.66	15.76
25	0.50	0.54	16.41	5.89	62.78	15.96
26	0.52	0.67	17.59	4.28	54.87	16.13
27	0.54	0.74	19.12	2.42	53.54	16.40
28	0.56	0.78	27.97	0.62	56.04	16.75
29	0.58	0.80	39.05	-0.37	59.71	17.12
30	0.60	0.85	50.36	-0.93	62.48	17.41
31	0.62	0.88	58.45	-1.18	63.77	17.63
32	0.64	0.93	67.42	-1.36	64.35	17.79
33	0.66	0.98	74.22	-1.49	64.37	17.92
34	0.68	1.00	77.98	-1.55	64.05	17.99
35	0.70	1.04	80.18	-1.55	63.47	18.04
36	0.72	1.06	81.79	-1.49	62.45	18.08
37	0.74	1.11	83.34	-1.36	61.42	18.12
38	0.76	1.15	85.95	-1.24	60.61	18.16
39	0.78	1.17	88.77	-1.05	60.46	18.20
40	0.80	1.17	90.82	-1.12	60.53	18.23
41	0.82	1.18	92.14	-1.12	61.21	18.26
42	0.84	1.16	95.04	-1.18	62.03	18.28
43	0.86	1.14	96.30	-1.18	63.21	18.29
44	0.88	1.13	97.76	-1.12	64.26	18.29
45	0.90	1.09	96.79	-15.69	64.66	18.29
46	0.92	1.11	96.61	6.26	64.15	18.28
47	0.94	1.15	95.00	17.11	62.75	18.28
48	0.96	1.18	93.88	20.15	61.43	18.28

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.20	94.15	17.54	60.42	18.28
50	1.00	1.22	93.71	25.23	59.54	18.29
51	1.02	1.26	94.38	21.70	59.20	18.31
52	1.04	1.24	95.84	20.71	59.19	18.32
53	1.06	1.25	97.57	22.38	60.12	18.34
54	1.08	1.21	100.47	21.02	61.90	18.36
55	1.10	1.13	101.96	17.11	64.73	18.36
56	1.12	1.06	102.92	19.71	67.29	18.33
57	1.14	1.02	100.75	50.71	69.62	18.31
58	1.16	0.96	99.81	35.09	70.92	18.26
59	1.18	0.93	94.04	20.95	71.62	18.19
60	1.20	0.93	88.53	27.65	70.63	18.13
61	1.22	0.94	84.74	41.60	69.13	18.07
62	1.24	0.95	80.58	51.64	67.35	18.03
63	1.27	0.97	77.50	56.23	64.54	18.00
64	1.28	1.07	75.33	77.12	60.84	18.00
65	1.30	1.17	75.44	91.07	57.49	18.04
66	1.32	1.25	79.60	101.55	55.08	18.11
67	1.34	1.33	82.67	102.36	53.37	18.18
68	1.36	1.42	85.81	98.82	51.83	18.24
69	1.38	1.47	87.09	90.82	50.82	18.28
70	1.40	1.50	89.35	83.45	50.28	18.32
71	1.42	1.54	92.86	71.23	50.47	18.36
72	1.44	1.53	96.05	58.71	51.45	18.41
73	1.46	1.48	100.27	46.50	53.68	18.45
74	1.48	1.40	106.68	50.65	56.53	18.48
75	1.50	1.32	110.46	64.54	59.61	18.51
76	1.52	1.26	114.50	85.31	61.95	18.53
77	1.54	1.23	117.19	102.11	63.38	18.53
78	1.56	1.21	113.81	105.39	63.57	18.52
79	1.58	1.22	110.06	113.39	62.99	18.46
80	1.60	1.20	102.85	102.60	61.89	18.39
81	1.62	1.20	94.73	91.01	60.69	18.31
82	1.64	1.20	89.16	96.09	59.04	18.22
83	1.66	1.22	82.01	83.63	58.07	18.16
84	1.68	1.20	81.59	79.23	57.73	18.14
85	1.70	1.19	83.17	71.98	58.79	18.14
86	1.72	1.14	83.64	70.80	59.84	18.15
87	1.74	1.14	85.89	70.80	60.79	18.16
88	1.76	1.14	87.12	86.30	61.32	18.18
89	1.78	1.13	88.17	83.14	62.00	18.19
90	1.80	1.11	89.13	86.48	62.46	18.19
91	1.82	1.10	87.20	89.34	62.67	18.18
92	1.84	1.10	86.41	91.13	62.56	18.16
93	1.86	1.10	86.49	109.98	61.73	18.15
94	1.88	1.14	83.17	82.27	61.04	18.14
95	1.90	1.13	83.11	85.68	60.43	18.12
96	1.92	1.12	82.35	96.53	60.71	18.11

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	1.11	81.68	97.46	60.98	18.09
98	1.96	1.10	80.04	80.41	61.51	18.07
99	1.98	1.07	79.16	71.11	61.52	18.05
100	2.00	1.09	78.31	86.86	61.65	18.05
101	2.02	1.08	78.98	84.00	61.31	18.05
102	2.04	1.09	79.65	77.62	61.31	18.06
103	2.06	1.10	79.48	89.46	60.51	18.07
104	2.08	1.14	79.15	87.79	59.94	18.07
105	2.10	1.14	80.09	69.75	59.27	18.08
106	2.12	1.16	80.12	61.69	59.72	18.09
107	2.14	1.12	80.23	46.37	60.66	18.08
108	2.16	1.08	80.76	40.24	61.84	18.08
109	2.19	1.08	81.20	47.68	62.90	18.08
110	2.20	1.05	81.72	58.28	63.28	18.08
111	2.22	1.06	82.63	63.17	63.64	18.09
112	2.24	1.07	83.07	60.51	64.01	18.10
113	2.26	1.04	83.68	67.39	64.17	18.10
114	2.28	1.05	82.95	67.08	63.83	18.09
115	2.30	1.08	81.54	72.16	62.96	18.10
116	2.32	1.10	83.18	70.80	62.61	18.11
117	2.34	1.09	83.82	56.79	62.85	18.11
118	2.36	1.08	83.38	54.56	63.23	18.12
119	2.38	1.08	84.52	66.58	63.51	18.13
120	2.40	1.08	85.93	79.23	64.30	18.14
121	2.42	1.04	87.12	79.54	64.67	18.15
122	2.44	1.06	86.95	101.24	64.22	18.15
123	2.46	1.10	85.69	112.40	62.99	18.15
124	2.48	1.12	85.39	106.57	61.32	18.15
125	2.50	1.17	83.60	78.80	60.24	18.14
126	2.52	1.18	81.29	39.12	59.63	18.11
127	2.54	1.14	79.00	41.79	59.34	18.07
128	2.56	1.15	76.33	49.29	59.48	18.04
129	2.58	1.12	75.54	56.73	60.17	18.02
130	2.60	1.07	76.94	64.41	62.10	18.00
131	2.62	1.01	76.36	43.83	64.73	17.98
132	2.64	0.94	75.83	51.15	67.62	17.95
133	2.66	0.87	75.21	108.06	69.41	17.93
134	2.68	0.89	75.33	126.60	69.13	17.91
135	2.70	0.92	72.51	147.74	65.09	17.90
136	2.72	1.06	67.44	116.68	60.97	17.84
137	2.74	1.06	60.18	113.02	58.17	17.76
138	2.76	1.04	57.77	48.23	58.07	17.66
139	2.78	0.99	54.61	11.22	58.32	17.58
140	2.80	0.98	49.36	18.29	58.00	17.49
141	2.82	0.97	46.67	24.67	57.69	17.42
142	2.84	0.94	46.46	28.21	57.96	17.39
143	2.86	0.93	46.85	51.77	58.82	17.39
144	2.88	0.92	47.82	51.83	59.58	17.41

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.91	48.90	57.22	60.37	17.43
146	2.92	0.91	50.19	59.45	61.96	17.46
147	2.94	0.86	51.95	63.86	63.40	17.46
148	2.96	0.84	50.86	64.04	64.80	17.44
149	2.98	0.82	49.08	64.35	65.51	17.40
150	3.00	0.79	47.79	64.41	66.44	17.36
151	3.02	0.76	47.32	62.18	68.86	17.32
152	3.04	0.70	47.41	58.96	71.54	17.30
153	3.06	0.67	47.41	57.90	73.82	17.29
154	3.08	0.67	47.44	63.48	73.52	17.29
155	3.10	0.71	47.96	96.84	71.75	17.31
156	3.12	0.73	47.52	128.02	68.25	17.31
157	3.14	0.79	44.33	134.41	64.10	17.26
158	3.16	0.84	39.55	136.45	60.29	17.18
159	3.18	0.85	36.89	137.76	56.93	17.10
160	3.20	0.90	34.69	139.80	54.39	17.04
161	3.22	0.93	32.82	137.20	51.70	16.99
162	3.24	0.97	31.41	124.18	50.30	17.01
163	3.26	1.01	35.04	117.11	49.56	17.09
164	3.28	1.06	38.03	103.16	49.98	17.23
165	3.30	1.10	44.24	108.00	50.24	17.37
166	3.32	1.14	48.02	119.90	50.57	17.51
167	3.34	1.19	52.57	136.39	50.85	17.60
168	3.36	1.19	55.70	138.13	50.71	17.67
169	3.38	1.23	55.61	138.00	50.25	17.69
170	3.40	1.26	55.23	133.11	49.10	17.69
171	3.42	1.28	53.86	122.50	48.37	17.70
172	3.44	1.31	55.50	109.86	48.06	17.72
173	3.46	1.33	57.81	97.89	48.70	17.78
174	3.48	1.32	62.70	80.72	50.03	17.85
175	3.50	1.28	65.90	72.85	52.13	17.92
176	3.52	1.25	71.58	66.03	54.27	17.98
177	3.54	1.22	74.75	65.96	55.54	18.03
178	3.56	1.26	77.06	73.34	55.40	18.07
179	3.58	1.31	77.12	77.06	54.06	18.09
180	3.60	1.37	77.32	77.43	53.14	18.11
181	3.62	1.35	78.20	81.59	52.44	18.12
182	3.64	1.38	77.88	90.51	51.59	18.12
183	3.66	1.44	75.56	95.29	50.22	18.10
184	3.68	1.45	72.78	97.77	49.92	18.07
185	3.70	1.36	71.46	96.65	51.09	18.03
186	3.72	1.28	71.72	95.04	53.27	18.00
187	3.74	1.22	70.58	93.74	56.83	17.94
188	3.76	1.01	66.71	90.89	61.07	17.85
189	3.78	0.90	63.55	89.52	66.01	17.73
190	3.80	0.83	59.36	88.72	69.53	17.63
191	3.82	0.75	56.02	87.60	72.34	17.51
192	3.84	0.69	50.62	87.04	70.55	17.31

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	0.75	34.59	103.91	67.52	17.08
194	3.88	0.71	31.52	105.70	63.61	16.84
195	3.90	0.68	28.79	107.75	63.23	16.71
196	3.92	0.68	25.51	111.78	60.80	16.59
197	3.94	0.72	22.26	117.23	56.91	16.46
198	3.96	0.76	20.18	119.09	52.45	16.36
199	3.98	0.82	18.45	120.52	48.94	16.29
200	4.00	0.86	17.54	120.52	46.54	16.22
201	4.02	0.85	16.14	120.71	45.81	16.13
202	4.04	0.81	14.82	120.27	45.72	16.01
203	4.06	0.78	13.15	121.82	46.60	15.90
204	4.08	0.73	12.86	124.92	47.33	15.83
205	4.10	0.72	12.80	131.00	47.25	15.83
206	4.12	0.78	13.07	135.90	45.51	15.86
207	4.14	0.84	13.21	137.82	44.41	15.94
208	4.16	0.84	14.88	134.53	46.33	16.05
209	4.18	0.75	17.61	128.52	50.30	16.14
210	4.20	0.68	17.87	128.08	53.39	16.15
211	4.22	0.70	16.67	131.00	52.27	16.11
212	4.25	0.77	15.53	134.35	48.67	16.07
213	4.26	0.84	15.06	132.11	46.72	16.13
214	4.28	0.85	17.99	125.23	47.11	16.20
215	4.30	0.81	18.58	121.88	48.11	16.23
216	4.32	0.81	16.74	123.12	48.69	16.18
217	4.34	0.78	16.18	132.30	48.73	16.12
218	4.36	0.76	16.01	144.14	49.00	16.08
219	4.38	0.76	15.33	159.70	48.77	16.05
220	4.40	0.77	15.13	168.63	48.54	16.00
221	4.42	0.73	13.90	183.76	48.16	15.90
222	4.44	0.72	12.14	200.12	47.70	15.86
223	4.46	0.77	13.67	204.15	46.11	15.92
224	4.48	0.86	15.01	210.60	44.53	16.04
225	4.50	0.91	15.72	211.53	43.44	16.15
226	4.52	0.93	17.01	207.75	44.04	16.27
227	4.55	0.91	19.85	203.04	45.37	16.39
228	4.56	0.92	21.58	201.67	47.58	16.51
229	4.58	0.88	23.78	195.41	49.64	16.60
230	4.60	0.86	26.01	198.88	51.19	16.66
231	4.62	0.87	25.51	200.25	51.06	16.70
232	4.64	0.92	26.04	202.36	50.72	16.71
233	4.66	0.89	26.80	200.99	50.98	16.74
234	4.68	0.88	27.12	200.62	50.84	16.76
235	4.70	0.95	27.42	210.29	49.21	16.76
236	4.72	1.00	25.37	214.01	46.62	16.75
237	4.74	1.06	25.07	224.12	45.46	16.73
238	4.76	1.02	25.10	213.33	46.56	16.69
239	4.78	0.89	24.11	220.33	48.38	16.65
240	4.80	0.89	23.67	236.89	49.70	16.61

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	0.89	23.46	241.79	48.16	16.62
242	4.84	1.00	23.80	246.37	47.77	16.75
243	4.86	1.05	31.19	226.53	48.32	16.92
244	4.88	1.02	34.44	226.84	50.33	17.06
245	4.90	1.00	35.61	222.94	52.69	17.08
246	4.92	0.91	34.82	192.62	55.50	17.08
247	4.94	0.85	36.32	181.09	59.47	17.07
248	4.97	0.78	37.46	174.15	64.02	17.07
249	4.98	0.71	38.31	164.60	68.10	17.06
250	5.01	0.67	37.58	163.79	72.28	17.03
251	5.02	0.62	37.96	163.55	75.16	16.99
252	5.04	0.59	36.61	163.48	77.34	16.94
253	5.06	0.58	34.18	165.47	76.04	16.83
254	5.08	0.60	28.29	170.80	71.91	16.69
255	5.10	0.64	24.36	174.52	65.95	16.54
256	5.12	0.69	21.96	178.49	57.28	16.46
257	5.14	0.90	20.11	189.15	48.81	16.42
258	5.16	1.09	18.82	194.42	43.99	16.40
259	5.19	1.04	18.68	144.58	45.05	16.46
260	5.20	0.89	23.36	120.09	51.30	16.51
261	5.22	0.71	24.51	117.54	59.42	16.55
262	5.24	0.64	24.18	136.70	64.00	16.51
263	5.26	0.67	23.45	162.24	63.55	16.49
264	5.28	0.71	23.10	174.15	60.88	16.50
265	5.30	0.75	23.78	184.13	57.15	16.48
266	5.32	0.82	20.58	193.06	51.32	16.43
267	5.34	0.98	17.80	210.11	44.87	16.36
268	5.36	1.13	17.62	220.21	40.74	16.41
269	5.38	1.22	20.58	193.37	40.45	16.58
270	5.40	1.19	25.62	155.73	44.18	16.87
271	5.42	1.11	36.26	127.53	50.25	17.12
272	5.44	0.99	42.79	108.62	57.60	17.30
273	5.46	0.89	48.07	98.95	64.70	17.39
274	5.48	0.81	51.06	82.15	71.89	17.45
275	5.50	0.72	55.63	72.23	79.88	17.49
276	5.52	0.63	59.82	67.89	87.92	17.49
277	5.54	0.57	57.68	69.37	93.79	17.43
278	5.56	0.54	51.32	71.17	96.39	17.31
279	5.58	0.52	47.69	78.30	95.33	17.16
280	5.60	0.52	39.43	91.20	91.48	16.99
281	5.62	0.54	32.42	97.58	85.27	16.76
282	5.64	0.55	25.39	101.24	79.16	16.52
283	5.66	0.55	20.59	104.22	73.78	16.28
284	5.68	0.56	16.84	108.06	68.70	16.06
285	5.70	0.59	14.34	111.04	64.92	15.93
286	5.72	0.61	14.49	113.95	63.19	15.95
287	5.74	0.63	16.98	118.97	62.84	16.06
288	5.76	0.66	18.54	127.40	62.69	16.17

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	0.67	18.92	130.50	61.43	16.23
290	5.80	0.71	19.01	133.85	60.64	16.26
291	5.82	0.71	19.42	136.14	59.17	16.30
292	5.85	0.76	20.17	146.87	60.09	16.36
293	5.86	0.71	22.37	143.15	60.87	16.43
294	5.88	0.72	23.19	136.52	61.72	16.51
295	5.90	0.78	24.74	145.32	60.06	16.58
296	5.92	0.84	25.53	133.91	58.98	16.67
297	5.94	0.84	27.44	115.19	58.32	16.73
298	5.96	0.87	28.23	101.12	58.78	16.82
299	5.98	0.90	31.92	80.66	58.93	16.93
300	6.00	0.93	35.12	69.50	59.58	17.07
301	6.02	0.96	39.60	68.01	60.26	17.22
302	6.04	1.00	44.87	62.99	60.81	17.37
303	6.06	1.04	50.15	57.10	61.68	17.51
304	6.08	1.05	55.45	50.46	62.77	17.62
305	6.10	1.05	59.55	45.51	64.82	17.71
306	6.12	1.03	64.50	40.11	67.62	17.78
307	6.14	0.97	67.37	25.60	70.27	17.82
308	6.16	0.97	68.87	-2.98	73.16	17.86
309	6.18	0.94	73.99	0.93	74.83	17.90
310	6.20	0.94	75.81	4.34	76.33	17.91
311	6.22	0.92	72.67	-0.06	76.76	17.89
312	6.25	0.90	70.06	-3.60	77.21	17.85
313	6.26	0.89	69.39	-2.48	78.25	17.81
314	6.28	0.85	68.63	2.11	79.03	17.78
315	6.30	0.84	65.90	4.09	79.85	17.73
316	6.32	0.82	62.50	2.48	80.85	17.68
317	6.34	0.77	61.06	1.30	83.24	17.61
318	6.36	0.72	58.72	4.03	86.24	17.54
319	6.38	0.68	55.88	5.27	88.71	17.47
320	6.40	0.65	52.94	6.70	90.18	17.38
321	6.42	0.63	49.02	8.49	89.79	17.29
322	6.44	0.64	44.04	9.80	87.16	17.18
323	6.46	0.66	39.58	11.22	82.82	17.06
324	6.48	0.68	35.13	13.14	78.11	16.95
325	6.50	0.71	31.55	14.76	74.55	16.84
326	6.52	0.71	29.18	15.62	73.72	16.76
327	6.54	0.66	28.88	16.12	75.34	16.72
328	6.56	0.64	29.76	17.42	78.47	16.73
329	6.58	0.62	31.08	20.15	80.31	16.74
330	6.60	0.62	30.38	21.64	81.47	16.74
331	6.62	0.61	30.32	22.07	81.52	16.75
332	6.64	0.63	31.38	23.06	81.37	16.77
333	6.66	0.64	32.14	27.22	80.42	16.79
334	6.68	0.65	31.35	36.02	78.60	16.76
335	6.70	0.66	28.36	41.23	77.57	16.69
336	6.72	0.63	26.57	45.20	77.08	16.59

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	0.61	25.02	47.99	78.09	16.50
338	6.76	0.59	23.06	51.70	78.65	16.39
339	6.78	0.56	20.69	54.56	79.61	16.26
340	6.80	0.53	18.40	55.80	76.82	16.03
341	6.82	0.55	12.19	121.39	74.11	15.84
342	6.84	0.54	12.95	123.06	71.53	15.71
343	6.86	0.53	13.63	124.18	74.68	15.77
344	6.88	0.49	14.65	125.73	78.50	15.82
345	6.90	0.47	15.39	128.70	82.14	15.84
346	6.93	0.46	15.21	135.40	83.07	15.84
347	6.94	0.47	14.86	146.62	81.79	15.81
348	6.96	0.48	13.89	154.68	78.66	15.76
349	6.98	0.51	12.93	160.20	75.72	15.70
350	7.00	0.51	12.19	163.79	72.49	15.62
351	7.03	0.53	10.94	167.02	70.49	15.55
352	7.04	0.53	10.61	169.31	67.38	15.47
353	7.06	0.57	9.76	173.96	64.79	15.44
354	7.08	0.59	9.59	175.64	62.69	15.40
355	7.10	0.58	9.47	176.07	60.30	15.45
356	7.12	0.67	10.41	178.92	57.80	15.50
357	7.14	0.70	10.21	181.90	55.09	15.58
358	7.16	0.74	10.91	171.79	54.91	15.67
359	7.18	0.73	12.61	172.04	55.38	15.77
360	7.20	0.74	13.23	173.78	57.25	15.87
361	7.22	0.72	14.43	174.33	58.22	15.91
362	7.24	0.71	14.11	183.57	58.20	15.93
363	7.26	0.75	13.90	199.69	55.31	15.94
364	7.28	0.85	13.93	214.82	52.47	15.96
365	7.30	0.86	13.85	218.85	50.85	15.99
366	7.32	0.87	14.58	218.41	51.87	16.08
367	7.34	0.85	17.28	215.81	54.25	16.20
368	7.36	0.81	19.00	215.13	56.37	16.31
369	7.38	0.84	19.80	216.62	57.18	16.38
370	7.40	0.87	21.03	217.92	57.10	16.45
371	7.42	0.87	22.17	217.05	57.56	16.53
372	7.44	0.87	23.93	213.89	59.17	16.61
373	7.46	0.85	26.33	208.80	61.46	16.71
374	7.48	0.83	28.82	204.59	63.92	16.79
375	7.50	0.82	30.55	203.04	65.54	16.86
376	7.52	0.83	31.99	200.25	65.96	16.91
377	7.54	0.85	32.52	198.39	66.71	16.96
378	7.56	0.83	34.27	191.75	68.21	16.98
379	7.58	0.79	34.63	183.32	70.92	16.99
380	7.60	0.75	34.92	175.70	74.19	16.97
381	7.62	0.69	33.95	169.19	77.93	16.92
382	7.64	0.64	32.81	163.55	82.06	16.85
383	7.66	0.59	31.37	158.59	85.84	16.79
384	7.68	0.56	31.05	155.86	90.57	16.74

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	0.51	31.31	153.25	95.87	16.69
386	7.72	0.46	29.53	153.19	100.00	16.60
387	7.74	0.46	26.13	154.93	98.04	16.47
388	7.76	0.49	22.44	159.08	89.58	16.34
389	7.78	0.57	19.65	165.03	77.03	16.23
390	7.80	0.71	16.60	172.72	63.00	16.18
391	7.82	0.94	16.20	97.58	54.59	16.13
392	7.85	0.95	15.18	88.16	51.89	16.14
393	7.86	0.89	15.88	74.71	55.49	16.17
394	7.88	0.78	18.78	63.36	62.45	16.23
395	7.91	0.66	19.49	77.37	68.97	16.25
396	7.92	0.64	18.78	124.24	71.29	16.23
397	7.94	0.67	18.67	175.45	68.67	16.20
398	7.97	0.71	17.35	227.53	65.66	16.16
399	7.98	0.71	16.35	234.04	63.82	16.09
400	8.00	0.69	15.18	233.79	62.72	15.99
401	8.02	0.70	13.60	230.56	62.38	15.94
402	8.04	0.70	14.45	225.67	60.35	15.96
403	8.06	0.78	15.21	229.14	57.75	16.03
404	8.08	0.86	15.18	216.49	54.39	16.08
405	8.10	0.92	15.47	181.09	53.21	16.15
406	8.12	0.92	17.38	141.04	53.83	16.24
407	8.14	0.91	18.87	126.66	56.85	16.33
408	8.16	0.83	20.25	113.08	62.46	16.38
409	8.18	0.69	21.48	106.08	70.27	16.41
410	8.20	0.63	23.39	114.94	74.19	16.43
411	8.22	0.71	22.57	141.17	69.25	16.46
412	8.24	0.87	21.48	143.34	61.48	16.46
413	8.26	0.95	20.25	111.59	57.87	16.47
414	8.28	0.91	21.51	89.96	57.58	16.45
415	8.30	0.88	20.25	85.80	56.02	16.43
416	8.32	1.03	18.76	92.31	47.57	16.49
417	8.34	1.52	20.63	104.40	39.36	16.66
418	8.36	1.87	24.44	77.62	34.60	16.89
419	8.38	2.01	28.04	60.82	32.62	17.03
420	8.40	2.09	27.05	51.95	31.30	17.04
421	8.42	2.16	24.32	45.20	29.49	17.01
422	8.45	2.35	24.91	38.00	27.70	17.06
423	8.46	2.61	28.25	31.93	26.12	17.18
424	8.48	2.83	30.33	26.66	24.90	17.28
425	8.50	2.93	29.98	13.76	24.21	17.21
426	8.52	2.69	23.30	-13.21	24.32	16.96
427	8.54	2.24	15.42	-14.51	25.86	16.50
428	8.56	1.66	10.00	-15.93	30.25	16.15
429	8.58	1.31	13.78	-15.93	40.11	16.21
430	8.60	1.00	21.22	-11.22	51.12	16.43
431	8.62	0.91	23.53	114.76	58.17	16.60
432	8.64	0.97	25.06	195.91	59.27	16.66

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	0.95	24.88	173.65	60.67	16.67
434	8.68	0.84	24.85	166.09	63.89	16.60
435	8.70	0.77	22.48	173.22	67.91	16.50
436	8.72	0.71	20.98	182.64	70.89	16.38
437	8.74	0.66	19.84	187.66	73.02	16.29
438	8.76	0.64	18.55	199.32	78.13	16.22
439	8.78	0.51	19.23	252.39	76.84	16.27
440	8.80	0.72	21.95	183.08	76.54	16.36
441	8.82	0.69	22.80	207.25	71.78	16.44
442	8.84	0.71	21.51	224.61	71.46	16.42
443	8.86	0.71	20.81	239.06	69.70	16.35
444	8.88	0.71	18.88	238.75	68.83	16.31
445	8.90	0.72	19.23	252.45	68.91	16.25
446	8.92	0.68	18.15	226.04	71.01	16.23
447	8.94	0.64	18.53	194.30	72.43	16.17
448	8.96	0.65	16.97	230.07	73.21	16.12
449	8.99	0.64	16.45	238.38	72.49	16.07
450	9.00	0.63	16.27	239.86	73.62	16.06
451	9.02	0.60	16.65	239.06	74.85	16.03
452	9.04	0.59	15.71	242.22	75.73	16.00
453	9.06	0.59	15.28	245.26	74.63	15.95
454	9.09	0.61	14.40	247.24	71.72	15.93
455	9.10	0.67	14.43	251.08	67.64	15.96
456	9.12	0.74	15.51	259.52	61.50	16.00
457	9.14	0.88	14.22	230.63	56.39	16.05
458	9.16	0.96	14.81	175.39	53.32	16.12
459	9.18	0.99	17.12	138.56	53.98	16.25
460	9.20	0.96	19.35	117.85	57.47	16.41
461	9.22	0.89	22.90	108.06	59.44	16.53
462	9.24	0.98	23.75	133.91	59.56	16.63
463	9.26	1.04	24.95	101.12	61.44	16.72
464	9.28	0.87	28.76	79.11	66.76	16.75
465	9.30	0.75	28.08	79.29	75.23	16.73
466	9.32	0.69	27.23	96.03	77.53	16.67
467	9.34	0.75	25.97	141.29	75.07	16.61
468	9.36	0.79	23.36	147.37	71.23	16.58
469	9.38	0.80	23.77	147.43	70.18	16.54
470	9.40	0.76	23.25	148.23	70.66	16.50
471	9.42	0.75	21.61	154.43	69.74	16.44
472	9.44	0.80	20.37	147.74	66.86	16.46
473	9.46	0.89	22.86	155.98	60.99	16.51
474	9.48	1.06	22.10	136.45	57.45	16.62
475	9.50	1.10	24.59	66.03	57.18	16.73
476	9.52	1.02	28.96	48.30	60.20	16.82
477	9.54	0.98	29.49	58.83	61.94	16.89
478	9.56	1.06	29.90	62.00	61.14	16.91
479	9.58	1.09	30.01	43.83	62.31	16.95
480	9.60	0.96	32.97	31.18	67.10	16.97

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	0.83	33.73	29.14	75.14	16.94
482	9.64	0.73	32.01	31.68	82.34	16.87
483	9.66	0.67	30.60	47.74	86.75	16.78
484	9.68	0.65	28.93	58.83	87.00	16.70
485	9.70	0.67	26.58	67.14	83.76	16.63
486	9.72	0.71	24.91	73.78	77.30	16.55
487	9.74	0.80	21.84	81.40	69.76	16.46
488	9.76	0.89	18.97	88.16	63.22	16.53
489	9.78	1.05	26.15	72.66	62.90	16.71
490	9.80	0.95	31.46	55.05	64.44	16.87
491	9.82	0.95	30.55	58.28	66.19	16.90
492	9.84	0.98	28.70	57.59	65.71	16.88
493	9.86	0.96	29.76	51.27	65.83	16.89
494	9.88	0.96	31.31	50.34	64.59	16.92
495	9.90	1.07	30.14	56.17	60.18	16.96
496	9.92	1.25	30.02	54.18	55.43	17.04
497	9.94	1.35	34.18	48.61	53.28	17.17
498	9.96	1.39	38.78	42.90	54.05	17.30
499	9.98	1.34	41.57	35.28	55.99	17.34
500	10.01	1.25	39.10	29.57	58.51	17.25
501	10.02	1.12	32.75	24.49	62.45	17.06
502	10.04	0.91	28.67	21.45	66.81	16.84
503	10.06	0.84	25.51	29.51	67.67	16.71
504	10.08	0.97	24.10	49.04	63.30	16.67
505	10.10	1.09	24.89	49.23	58.20	16.74
506	10.12	1.17	26.89	43.77	55.72	16.85
507	10.14	1.24	29.73	37.69	54.78	16.97
508	10.16	1.29	32.27	34.35	54.00	17.08
509	10.18	1.35	34.12	32.11	53.12	17.18
510	10.20	1.43	36.99	29.82	52.24	17.28
511	10.22	1.49	40.01	28.02	52.22	17.36
512	10.24	1.46	41.33	25.05	53.44	17.32
513	10.26	1.27	33.80	20.15	55.64	17.16
514	10.28	1.14	28.52	18.16	57.25	16.93
515	10.30	1.11	25.12	19.65	57.64	16.82
516	10.32	1.14	26.65	20.40	55.80	16.85
517	10.34	1.29	29.43	23.12	51.64	17.00
518	10.36	1.59	32.86	25.05	48.12	17.22
519	10.38	1.73	40.27	24.36	46.54	17.39
520	10.40	1.71	42.91	22.26	46.87	17.41
521	10.42	1.58	34.82	19.71	47.60	17.27
522	10.44	1.46	28.99	17.73	49.18	17.07
523	10.46	1.30	28.67	15.00	51.98	16.91
524	10.48	1.16	25.38	12.65	55.85	16.71
525	10.50	0.99	18.70	10.79	59.94	16.52
526	10.52	0.90	19.99	9.49	65.19	16.41
527	10.54	0.83	22.22	12.09	66.81	16.41
528	10.56	0.91	19.05	24.98	64.09	16.42

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	1.03	19.82	24.86	60.69	16.51
530	10.60	1.06	25.32	19.71	60.58	16.67
531	10.62	1.04	27.17	16.49	62.95	16.72
532	10.64	0.95	24.03	15.31	64.40	16.66
533	10.66	0.94	22.33	21.45	61.15	16.54
534	10.68	1.12	19.40	23.99	52.86	16.55
535	10.70	1.47	20.90	26.41	44.44	16.74
536	10.72	1.87	28.14	24.24	39.31	17.02
537	10.74	2.13	32.85	22.44	35.76	17.17
538	10.76	2.26	27.81	21.82	32.03	17.05
539	10.78	2.37	17.63	38.13	28.45	16.79
540	10.80	2.42	15.75	24.86	25.51	16.48
541	10.82	2.44	13.09	22.50	23.84	16.28
542	10.84	2.48	9.92	23.12	5.00	16.09
543	10.87	2.57	9.66	21.02	5.00	16.19
544	10.88	2.67	15.96	19.96	24.00	16.54
545	10.90	2.54	22.14	16.18	27.13	16.85
546	10.92	2.33	25.48	12.77	31.34	17.00
547	10.95	1.99	27.12	9.80	35.54	16.95
548	10.96	1.67	21.76	8.06	39.69	16.74
549	10.98	1.42	16.78	6.82	44.81	16.50
550	11.00	1.13	17.98	4.90	51.52	16.40
551	11.02	1.01	20.36	8.80	59.33	16.47
552	11.04	0.98	22.88	15.56	64.11	16.57
553	11.06	0.94	24.81	20.52	68.58	16.65
554	11.08	0.86	26.48	23.37	74.88	16.68
555	11.10	0.74	27.18	25.48	83.35	16.67
556	11.12	0.65	27.42	37.51	90.87	16.63
557	11.14	0.62	26.24	73.28	93.42	16.57
558	11.17	0.64	24.25	105.52	90.64	16.50
559	11.18	0.67	22.29	116.18	82.70	16.45
560	11.20	0.80	21.44	124.86	74.83	16.40
561	11.22	0.85	18.97	134.28	68.51	16.32
562	11.24	0.87	16.72	131.68	68.09	16.27
563	11.26	0.79	19.21	115.50	74.17	16.34
564	11.28	0.66	23.48	118.78	81.47	16.40
565	11.30	0.67	21.96	127.09	84.29	16.44
566	11.32	0.73	21.90	133.11	79.73	16.42
567	11.34	0.78	21.29	146.62	74.62	16.44
568	11.36	0.85	21.37	150.90	71.21	16.48
569	11.38	0.88	22.93	150.71	70.52	16.53
570	11.40	0.85	23.81	149.54	71.26	16.58
571	11.42	0.85	24.13	148.48	72.73	16.62
572	11.44	0.85	25.97	146.44	75.66	16.71
573	11.46	0.79	29.78	145.69	78.25	16.80
574	11.48	0.81	31.22	159.21	78.66	16.86
575	11.50	0.88	30.63	176.19	75.78	16.87
576	11.52	0.90	29.17	180.78	73.90	16.86

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	0.88	29.61	177.87	74.37	16.85
578	11.56	0.85	30.22	175.45	75.92	16.86
579	11.58	0.84	30.05	176.19	75.95	16.83
580	11.60	0.86	27.70	182.27	74.08	16.80
581	11.62	0.91	27.15	188.03	71.16	16.79
582	11.64	0.96	28.46	192.93	68.82	16.83
583	11.66	1.00	29.52	194.42	67.31	16.88
584	11.68	1.02	29.64	194.73	67.12	16.92
585	11.70	1.00	30.72	192.00	68.15	16.95
586	11.72	0.98	32.51	187.85	70.70	17.01
587	11.74	0.94	34.94	181.84	73.71	17.07
588	11.76	0.90	37.50	260.07	76.05	17.14
589	11.78	0.92	39.26	260.20	76.77	17.19
590	11.80	0.94	39.79	261.38	76.02	17.22
591	11.82	0.96	39.85	259.89	75.26	17.23
592	11.84	0.97	40.32	258.28	74.29	17.24
593	11.86	0.99	40.14	257.10	73.92	17.26
594	11.88	0.99	40.70	254.06	73.37	17.27
595	11.90	1.01	40.87	252.51	73.52	17.29
596	11.92	1.01	42.39	244.14	74.61	17.32
597	11.94	0.98	44.62	240.61	76.40	17.37
598	11.96	0.97	47.29	239.37	78.43	17.41
599	11.98	0.95	47.67	238.69	79.53	17.43
600	12.00	0.95	47.96	240.24	79.97	17.43
601	12.03	0.95	46.96	240.67	79.31	17.41
602	12.04	0.97	45.56	244.14	77.49	17.40
603	12.06	1.02	45.00	248.11	74.81	17.39
604	12.08	1.06	43.68	248.79	72.92	17.39
605	12.10	1.07	44.56	248.54	71.70	17.40
606	12.12	1.10	45.49	248.17	71.67	17.44
607	12.14	1.10	47.34	246.93	71.94	17.48
608	12.16	1.10	48.98	245.32	72.56	17.51
609	12.18	1.10	50.09	243.77	73.50	17.55
610	12.20	1.09	52.76	242.41	74.17	17.59
611	12.22	1.10	53.40	241.79	74.62	17.60
612	12.24	1.10	52.29	240.67	74.74	17.60
613	12.26	1.09	52.43	239.49	74.61	17.59
614	12.28	1.10	52.17	238.75	75.19	17.59
615	12.30	1.07	52.75	237.14	75.53	17.59
616	12.32	1.08	52.93	236.95	75.89	17.59
617	12.34	1.08	51.90	237.63	75.31	17.59
618	12.36	1.11	52.87	237.32	74.77	17.60
619	12.38	1.12	53.69	237.69	74.15	17.62
620	12.40	1.13	53.04	240.11	73.21	17.62
621	12.42	1.17	52.89	240.42	72.03	17.63
622	12.44	1.19	53.57	240.24	71.45	17.66
623	12.46	1.19	55.59	238.56	71.75	17.69
624	12.48	1.19	57.76	235.40	72.89	17.73

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	1.17	59.25	231.56	74.21	17.76
626	12.52	1.15	60.39	224.86	75.99	17.77
627	12.54	1.11	61.15	218.41	77.73	17.78
628	12.57	1.10	62.32	210.11	80.20	17.78
629	12.58	1.04	63.06	204.65	82.50	17.77
630	12.60	1.00	61.74	199.94	85.81	17.75
631	12.62	0.94	61.47	188.10	88.95	17.71
632	12.64	0.89	60.36	182.46	93.61	17.67
633	12.66	0.81	58.69	176.88	98.32	17.60
634	12.68	0.75	55.40	172.41	100.00	17.52
635	12.70	0.69	52.97	170.92	100.00	17.41
636	12.72	0.62	47.79	170.37	100.00	17.25
637	12.74	0.62	37.25	242.03	100.00	17.06
638	12.76	0.63	32.68	248.79	100.00	16.84
639	12.78	0.63	27.40	248.17	100.00	16.67
640	12.80	0.61	24.30	248.73	98.16	16.51
641	12.82	0.60	21.75	249.10	97.65	16.32
642	12.84	0.56	17.09	247.80	96.32	16.10
643	12.87	0.55	13.87	255.98	93.55	15.85
644	12.88	0.56	11.79	260.32	90.09	15.68
645	12.90	0.57	11.09	262.37	88.73	15.56
646	12.92	0.54	10.33	263.24	88.72	15.48
647	12.94	0.53	9.68	265.47	89.06	15.40
648	12.96	0.53	9.04	273.34	87.27	15.34
649	12.98	0.56	8.86	280.16	86.15	15.32
650	13.00	0.55	9.10	283.01	84.65	15.34
651	13.02	0.57	9.25	284.13	84.13	15.37
652	13.04	0.58	9.57	285.74	83.15	15.40
653	13.06	0.58	9.60	285.99	84.13	15.44
654	13.08	0.56	10.36	285.37	84.42	15.48
655	13.10	0.59	10.48	286.67	84.93	15.52
656	13.12	0.59	10.74	286.42	84.42	15.54
657	13.14	0.59	10.86	286.11	85.26	15.56
658	13.16	0.58	11.10	285.62	84.44	15.56
659	13.18	0.60	10.39	288.53	80.71	15.53
660	13.21	0.67	9.66	297.33	75.42	15.48
661	13.22	0.70	9.11	302.73	72.62	15.46
662	13.24	0.68	9.64	295.47	73.81	15.47
663	13.26	0.64	10.10	289.77	77.45	15.47
664	13.28	0.60	9.49	289.52	77.62	15.45
665	13.30	0.67	9.14	300.12	73.85	15.43
666	13.32	0.74	9.23	305.33	70.04	15.51
667	13.34	0.76	10.78	296.90	69.56	15.66
668	13.36	0.76	12.78	283.32	68.04	15.79
669	13.38	0.86	12.69	315.00	61.66	15.94
670	13.40	1.12	13.74	336.33	53.81	16.10
671	13.42	1.36	16.18	187.66	50.00	16.34
672	13.44	1.40	20.28	121.70	50.49	16.55

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	1.33	23.00	87.04	53.59	16.65
674	13.48	1.23	22.54	75.70	59.26	16.67
675	13.50	1.02	23.41	65.47	68.34	16.60
676	13.52	0.77	22.65	75.26	79.08	16.46
677	13.54	0.67	18.90	273.28	85.88	16.28
678	13.56	0.66	16.09	329.82	84.07	16.10
679	13.58	0.68	14.54	336.52	80.75	15.96
680	13.60	0.69	13.07	337.82	78.11	15.88
681	13.62	0.70	12.96	343.09	76.61	15.85
682	13.64	0.72	13.31	347.24	76.06	15.84
683	13.66	0.70	12.69	344.64	76.52	15.83
684	13.68	0.69	12.87	345.32	76.35	15.82
685	13.70	0.72	12.96	358.15	74.68	15.83
686	13.72	0.75	12.49	359.95	72.41	15.89
687	13.74	0.83	14.22	200.12	73.50	16.00
688	13.76	0.76	17.01	236.70	77.37	16.14
689	13.78	0.71	18.50	271.42	81.58	16.19
690	13.80	0.70	17.18	300.06	82.46	16.15
691	13.82	0.70	15.46	317.48	80.29	16.08
692	13.84	0.73	15.28	330.75	78.52	16.05
693	13.86	0.74	15.75	334.16	77.54	16.06
694	13.88	0.74	15.72	335.21	76.77	16.05
695	13.90	0.75	14.69	337.76	76.43	16.02
696	13.92	0.73	14.58	335.15	76.88	16.01
697	13.94	0.72	15.54	330.01	79.26	16.03
698	13.96	0.69	15.81	328.77	80.37	16.05
699	13.98	0.71	15.57	339.18	80.63	16.07
700	14.00	0.72	16.22	351.52	79.18	16.06
701	14.02	0.73	15.16	357.22	78.69	16.06
702	14.05	0.73	15.34	351.21	77.35	16.05
703	14.06	0.76	15.51	361.25	73.43	16.06
704	14.08	0.87	14.78	376.50	66.54	16.07
705	14.10	1.01	14.14	390.64	60.70	16.09
706	14.12	1.09	14.84	236.95	58.04	16.22
707	14.14	1.14	18.59	273.78	55.93	16.32
708	14.16	1.26	17.54	260.82	57.06	16.52
709	14.18	1.21	24.16	128.21	59.09	16.68
710	14.20	1.17	27.26	141.29	64.11	16.86
711	14.22	1.12	30.31	149.47	68.87	16.95
712	14.24	1.03	32.89	127.03	75.00	17.02
713	14.26	0.92	35.00	138.13	80.62	17.03
714	14.28	0.88	33.36	166.89	78.97	17.05
715	14.30	1.09	33.74	235.09	67.74	17.08
716	14.32	1.47	31.86	277.37	55.06	17.12
717	14.34	1.85	29.34	119.90	49.16	17.19
718	14.36	1.80	35.05	60.38	50.42	17.25
719	14.38	1.47	37.40	40.30	58.59	17.27
720	14.40	1.12	36.22	32.55	69.84	17.12

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	0.90	29.57	78.80	74.21	16.96
722	14.44	1.09	27.55	175.33	63.58	16.96
723	14.46	1.66	30.80	229.70	50.31	17.11
724	14.48	2.14	32.36	147.37	42.82	17.32
725	14.50	2.34	38.45	106.26	39.77	17.50
726	14.52	2.50	43.17	88.65	39.31	17.64
727	14.54	2.52	44.95	79.05	39.59	17.69
728	14.56	2.40	43.31	67.76	41.35	17.67
729	14.58	2.17	43.66	59.33	46.23	17.66
730	14.60	1.75	48.17	50.28	54.46	17.58
731	14.62	1.29	43.05	42.41	65.49	17.42
732	14.64	1.04	35.84	42.53	78.05	17.21
733	14.66	0.85	36.19	88.10	85.72	17.08
734	14.68	0.87	35.66	158.65	89.36	17.09
735	14.70	0.89	38.06	175.51	80.90	17.18
736	14.72	1.21	40.26	199.19	77.31	17.22
737	14.74	1.07	37.65	129.76	76.56	17.19
738	14.76	0.90	34.40	156.48	81.95	17.06
739	14.78	0.88	31.64	191.26	85.29	16.92
740	14.80	0.85	28.68	201.36	85.72	16.85
741	14.82	0.84	29.33	206.51	86.31	16.82
742	14.85	0.84	29.65	211.22	87.26	16.81
743	14.86	0.81	28.13	217.11	87.86	16.78
744	14.88	0.80	27.48	220.64	85.88	16.71
745	14.90	0.86	24.58	239.49	78.78	16.68
746	14.92	1.03	23.64	259.39	68.17	16.69
747	14.94	1.27	24.08	281.84	59.45	16.72
748	14.96	1.41	22.82	245.32	55.98	16.79
749	14.98	1.39	26.22	141.85	56.65	16.89
750	15.00	1.35	30.18	127.22	58.98	17.03
751	15.03	1.40	33.28	137.14	58.74	17.15
752	15.04	1.55	35.25	140.17	59.24	17.32
753	15.06	1.50	44.27	129.82	61.53	17.45
754	15.08	1.37	46.79	123.99	68.08	17.54
755	15.10	1.18	49.51	111.59	74.27	17.53
756	15.12	1.12	48.34	141.54	79.24	17.47
757	15.14	1.06	43.48	142.10	84.61	17.40
758	15.16	0.88	45.27	138.25	91.45	17.32
759	15.18	0.80	43.54	160.88	97.24	17.23
760	15.20	0.81	37.21	195.78	96.64	17.09
761	15.23	0.80	31.90	206.32	92.90	16.94
762	15.24	0.81	29.24	216.18	88.58	16.82
763	15.26	0.86	26.57	229.94	84.10	16.72
764	15.28	0.89	23.79	239.93	79.94	16.61
765	15.30	0.89	21.59	243.58	77.50	16.53
766	15.32	0.90	21.38	248.67	76.46	16.50
767	15.34	0.90	21.65	254.87	77.05	16.52
768	15.36	0.88	22.91	254.68	78.94	16.56

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	0.85	23.81	255.80	82.26	16.59
770	15.40	0.81	24.37	255.80	84.30	16.59
771	15.42	0.82	23.49	258.83	84.53	16.57
772	15.44	0.84	22.82	263.98	82.37	16.52
773	15.46	0.85	21.24	269.19	80.35	16.48
774	15.48	0.86	20.50	271.42	77.84	16.45
775	15.50	0.91	20.89	277.81	71.15	16.49
776	15.52	1.15	20.86	302.73	61.07	16.59
777	15.54	1.48	22.15	333.60	53.53	16.71
778	15.56	1.60	23.96	237.07	51.35	16.90
779	15.58	1.60	30.56	138.56	53.69	17.06
780	15.60	1.49	33.90	146.37	55.33	17.18
781	15.62	1.61	33.84	177.81	55.66	17.22
782	15.64	1.44	39.46	115.25	59.87	17.32

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.30	0.00	0.30	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
2	0.04	0.61	0.00	0.61	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
3	0.06	0.91	0.00	0.91	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
4	0.08	1.22	0.00	1.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
5	0.10	1.54	0.00	1.54	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
6	0.13	2.02	0.00	2.02	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
7	0.14	2.18	0.00	2.18	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
8	0.16	2.50	0.00	2.50	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
9	0.18	2.82	0.00	2.82	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
10	0.20	3.15	0.00	3.15	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
11	0.22	3.47	0.00	3.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
12	0.24	3.80	0.00	3.80	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
13	0.26	4.12	0.00	4.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
14	0.28	4.45	0.00	4.45	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
15	0.30	4.77	0.00	4.77	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
16	0.32	5.09	0.00	5.09	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
17	0.34	5.40	0.00	5.40	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
18	0.36	5.71	0.00	5.71	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
19	0.38	6.03	0.00	6.03	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
20	0.40	6.33	0.00	6.33	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
21	0.42	6.64	0.00	6.64	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
22	0.44	6.95	0.00	6.95	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
23	0.46	7.26	0.00	7.26	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
24	0.48	7.58	0.00	7.58	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
25	0.50	7.90	0.00	7.90	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
26	0.52	8.22	0.00	8.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
27	0.54	8.55	0.00	8.55	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
28	0.56	8.88	0.00	8.88	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
29	0.58	9.23	0.00	9.23	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
30	0.60	9.58	0.00	9.58	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
31	0.62	9.93	0.00	9.93	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
32	0.64	10.28	0.00	10.28	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
33	0.66	10.64	0.00	10.64	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
34	0.68	11.00	0.00	11.00	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
35	0.70	11.36	0.00	11.36	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
36	0.72	11.72	0.00	11.72	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
37	0.74	12.09	0.00	12.09	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
38	0.76	12.45	0.00	12.45	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
39	0.78	12.81	0.00	12.81	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
40	0.80	13.18	0.00	13.18	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
41	0.82	13.54	0.00	13.54	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
42	0.84	13.91	0.00	13.91	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
43	0.86	14.28	0.00	14.28	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
44	0.88	14.64	0.00	14.64	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
45	0.90	15.01	0.00	15.01	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
46	0.92	15.37	0.00	15.37	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
47	0.94	15.74	0.00	15.74	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
48	0.96	16.10	0.00	16.10	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	16.47	0.00	16.47	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
50	1.00	16.84	0.00	16.84	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
51	1.02	17.20	0.00	17.20	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
52	1.04	17.57	0.00	17.57	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
53	1.06	17.93	0.00	17.93	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
54	1.08	18.30	0.00	18.30	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
55	1.10	18.67	0.00	18.67	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
56	1.12	19.04	0.00	19.04	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
57	1.14	19.40	0.00	19.40	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
58	1.16	19.77	0.00	19.77	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
59	1.18	20.13	0.00	20.13	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
60	1.20	20.49	0.00	20.49	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
61	1.22	20.85	0.00	20.85	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
62	1.24	21.22	0.00	21.22	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
63	1.27	21.76	0.00	21.76	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
64	1.28	21.94	0.00	21.94	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
65	1.30	22.30	0.00	22.30	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
66	1.32	22.66	0.00	22.66	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
67	1.34	23.02	0.00	23.02	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
68	1.36	23.39	0.00	23.39	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
69	1.38	23.75	0.00	23.75	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
70	1.40	24.12	0.00	24.12	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
71	1.42	24.49	0.00	24.49	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
72	1.44	24.85	0.00	24.85	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
73	1.46	25.22	0.00	25.22	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
74	1.48	25.59	0.00	25.59	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
75	1.50	25.96	0.00	25.96	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
76	1.52	26.33	0.00	26.33	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
77	1.54	26.70	0.00	26.70	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
78	1.56	27.07	0.00	27.07	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
79	1.58	27.44	0.00	27.44	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
80	1.60	27.81	0.00	27.81	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
81	1.62	28.18	0.00	28.18	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
82	1.64	28.54	0.00	28.54	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
83	1.66	28.91	0.00	28.91	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
84	1.68	29.27	0.00	29.27	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
85	1.70	29.63	0.00	29.63	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
86	1.72	29.99	0.00	29.99	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
87	1.74	30.36	0.00	30.36	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
88	1.76	30.72	0.00	30.72	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
89	1.78	31.08	0.00	31.08	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
90	1.80	31.45	0.00	31.45	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
91	1.82	31.81	0.00	31.81	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
92	1.84	32.18	0.00	32.18	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
93	1.86	32.54	0.00	32.54	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
94	1.88	32.90	0.00	32.90	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
95	1.90	33.26	0.00	33.26	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
96	1.92	33.63	0.00	33.63	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	33.99	0.00	33.99	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
98	1.96	34.35	0.00	34.35	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
99	1.98	34.71	0.00	34.71	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
100	2.00	35.07	0.00	35.07	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
101	2.02	35.43	0.20	35.24	0.98	0.141	1.43	0.098	1.09	1.00	0.118	No
102	2.04	35.79	0.39	35.40	0.98	0.141	1.43	0.099	1.09	1.00	0.118	No
103	2.06	36.15	0.59	35.57	0.98	0.142	1.43	0.100	1.09	1.00	0.119	No
104	2.08	36.52	0.78	35.73	0.98	0.143	1.43	0.100	1.09	1.00	0.119	No
105	2.10	36.88	0.98	35.90	0.98	0.144	1.43	0.100	1.09	1.00	0.120	No
106	2.12	37.24	1.18	36.06	0.98	0.144	1.43	0.101	1.09	1.00	0.121	No
107	2.14	37.60	1.37	36.23	0.98	0.145	1.43	0.101	1.09	1.00	0.121	No
108	2.16	37.96	1.57	36.39	0.98	0.146	1.43	0.102	1.09	1.00	0.122	No
109	2.19	38.51	1.86	36.64	0.98	0.147	1.43	0.103	1.09	1.00	0.123	No
110	2.20	38.69	1.96	36.72	0.98	0.147	1.43	0.103	1.09	1.00	0.124	No
111	2.22	39.05	2.16	36.89	0.98	0.148	1.43	0.103	1.09	1.00	0.124	No
112	2.24	39.41	2.35	37.06	0.97	0.148	1.43	0.104	1.09	1.00	0.125	No
113	2.26	39.77	2.55	37.22	0.97	0.149	1.43	0.104	1.09	1.00	0.126	No
114	2.28	40.13	2.75	37.39	0.97	0.150	1.43	0.105	1.09	1.00	0.126	No
115	2.30	40.50	2.94	37.55	0.97	0.150	1.43	0.105	1.09	1.00	0.127	No
116	2.32	40.86	3.14	37.72	0.97	0.151	1.43	0.106	1.09	1.00	0.127	No
117	2.34	41.22	3.34	37.88	0.97	0.151	1.43	0.106	1.09	1.00	0.128	No
118	2.36	41.58	3.53	38.05	0.97	0.152	1.43	0.106	1.09	1.00	0.128	No
119	2.38	41.94	3.73	38.22	0.97	0.153	1.43	0.107	1.09	1.00	0.129	No
120	2.40	42.31	3.92	38.38	0.97	0.153	1.43	0.107	1.09	1.00	0.130	No
121	2.42	42.67	4.12	38.55	0.97	0.154	1.43	0.108	1.08	1.00	0.130	No
122	2.44	43.03	4.32	38.72	0.97	0.154	1.43	0.108	1.08	1.00	0.131	No
123	2.46	43.40	4.51	38.88	0.97	0.155	1.43	0.108	1.08	1.00	0.131	No
124	2.48	43.76	4.71	39.05	0.97	0.156	1.43	0.109	1.08	1.00	0.132	No
125	2.50	44.12	4.91	39.22	0.97	0.156	1.43	0.109	1.08	1.00	0.132	No
126	2.52	44.48	5.10	39.38	0.97	0.157	1.43	0.110	1.08	1.00	0.132	No
127	2.54	44.85	5.30	39.55	0.97	0.157	1.43	0.110	1.08	1.00	0.133	No
128	2.56	45.21	5.49	39.71	0.97	0.158	1.43	0.110	1.08	1.00	0.134	No
129	2.58	45.57	5.69	39.88	0.97	0.158	1.43	0.111	1.08	1.00	0.134	No
130	2.60	45.93	5.89	40.04	0.97	0.159	1.43	0.111	1.08	1.00	0.135	No
131	2.62	46.29	6.08	40.20	0.97	0.159	1.43	0.112	1.08	1.00	0.136	No
132	2.64	46.65	6.28	40.37	0.97	0.160	1.43	0.112	1.08	1.00	0.137	No
133	2.66	47.00	6.47	40.53	0.97	0.160	1.43	0.112	1.08	1.00	0.138	No
134	2.68	47.36	6.67	40.69	0.97	0.161	1.43	0.113	1.08	1.00	0.138	No
135	2.70	47.72	6.87	40.85	0.97	0.162	1.43	0.113	1.08	1.00	0.138	No
136	2.72	48.08	7.06	41.01	0.97	0.162	1.43	0.113	1.08	1.00	0.138	No
137	2.74	48.43	7.26	41.17	0.97	0.163	1.43	0.114	1.08	1.00	0.139	No
138	2.76	48.79	7.46	41.33	0.97	0.163	1.43	0.114	1.08	1.00	0.139	No
139	2.78	49.14	7.65	41.49	0.97	0.164	1.43	0.114	1.08	1.00	0.140	No
140	2.80	49.49	7.85	41.64	0.97	0.164	1.43	0.115	1.08	1.00	0.140	No
141	2.82	49.84	8.04	41.79	0.96	0.165	1.43	0.115	1.08	1.00	0.141	No
142	2.84	50.18	8.24	41.94	0.96	0.165	1.43	0.115	1.08	1.00	0.142	No
143	2.86	50.53	8.44	42.09	0.96	0.165	1.43	0.116	1.08	1.00	0.142	No
144	2.88	50.88	8.63	42.25	0.96	0.166	1.43	0.116	1.07	1.00	0.143	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	51.23	8.83	42.40	0.96	0.166	1.43	0.117	1.07	1.00	0.143	No
146	2.92	51.58	9.03	42.55	0.96	0.167	1.43	0.117	1.07	1.00	0.144	No
147	2.94	51.93	9.22	42.70	0.96	0.167	1.43	0.117	1.07	1.00	0.144	No
148	2.96	52.27	9.42	42.86	0.96	0.168	1.43	0.117	1.07	1.00	0.145	No
149	2.98	52.62	9.61	43.01	0.96	0.168	1.43	0.118	1.07	1.00	0.145	No
150	3.00	52.97	9.81	43.16	0.96	0.169	1.43	0.118	1.07	1.00	0.146	No
151	3.02	53.32	10.01	43.31	0.96	0.169	1.43	0.118	1.07	1.00	0.146	No
152	3.04	53.66	10.20	43.46	0.96	0.170	1.43	0.119	1.07	1.00	0.147	No
153	3.06	54.01	10.40	43.61	0.96	0.170	1.43	0.119	1.07	1.00	0.148	No
154	3.08	54.35	10.59	43.76	0.96	0.171	1.43	0.119	1.07	1.00	0.148	No
155	3.10	54.70	10.79	43.91	0.96	0.171	1.43	0.120	1.07	1.00	0.148	No
156	3.12	55.05	10.99	44.06	0.96	0.171	1.43	0.120	1.07	1.00	0.149	No
157	3.14	55.39	11.18	44.21	0.96	0.172	1.43	0.120	1.07	1.00	0.149	No
158	3.16	55.74	11.38	44.36	0.96	0.172	1.43	0.121	1.07	1.00	0.149	No
159	3.18	56.08	11.58	44.50	0.96	0.173	1.43	0.121	1.07	1.00	0.149	No
160	3.20	56.42	11.77	44.65	0.96	0.173	1.43	0.121	1.07	1.00	0.150	No
161	3.22	56.76	11.97	44.79	0.96	0.174	1.43	0.121	1.07	1.00	0.150	No
162	3.24	57.10	12.16	44.93	0.96	0.174	1.43	0.122	1.07	1.00	0.150	No
163	3.26	57.44	12.36	45.08	0.96	0.174	1.43	0.122	1.07	1.00	0.150	No
164	3.28	57.78	12.56	45.23	0.96	0.175	1.43	0.122	1.07	1.00	0.151	No
165	3.30	58.13	12.75	45.38	0.96	0.175	1.43	0.123	1.07	1.00	0.151	No
166	3.32	58.48	12.95	45.53	0.96	0.176	1.43	0.123	1.07	1.00	0.151	No
167	3.34	58.83	13.15	45.69	0.96	0.176	1.43	0.123	1.07	1.00	0.151	No
168	3.36	59.19	13.34	45.85	0.95	0.176	1.43	0.123	1.07	1.00	0.151	No
169	3.38	59.54	13.54	46.00	0.95	0.177	1.43	0.124	1.07	1.00	0.152	No
170	3.40	59.90	13.73	46.16	0.95	0.177	1.43	0.124	1.07	1.00	0.152	No
171	3.42	60.25	13.93	46.32	0.95	0.177	1.43	0.124	1.07	1.00	0.152	No
172	3.44	60.60	14.13	46.48	0.95	0.178	1.43	0.124	1.07	1.00	0.152	No
173	3.46	60.96	14.32	46.64	0.95	0.178	1.43	0.125	1.07	1.00	0.153	No
174	3.48	61.32	14.52	46.80	0.95	0.178	1.43	0.125	1.07	1.00	0.153	No
175	3.50	61.67	14.72	46.96	0.95	0.179	1.43	0.125	1.07	1.00	0.153	No
176	3.52	62.03	14.91	47.12	0.95	0.179	1.43	0.125	1.07	1.00	0.154	No
177	3.54	62.39	15.11	47.29	0.95	0.180	1.43	0.126	1.07	1.00	0.154	No
178	3.56	62.76	15.30	47.45	0.95	0.180	1.43	0.126	1.07	1.00	0.154	No
179	3.58	63.12	15.50	47.62	0.95	0.180	1.43	0.126	1.07	1.00	0.155	No
180	3.60	63.48	15.70	47.78	0.95	0.181	1.43	0.126	1.07	1.00	0.155	No
181	3.62	63.84	15.89	47.95	0.95	0.181	1.43	0.127	1.07	1.00	0.155	No
182	3.64	64.20	16.09	48.12	0.95	0.181	1.43	0.127	1.07	1.00	0.155	No
183	3.66	64.57	16.28	48.28	0.95	0.182	1.43	0.127	1.07	1.00	0.155	No
184	3.68	64.93	16.48	48.45	0.95	0.182	1.43	0.127	1.07	1.00	0.156	No
185	3.70	65.29	16.68	48.61	0.95	0.182	1.43	0.127	1.07	1.00	0.156	No
186	3.72	65.65	16.87	48.78	0.95	0.182	1.43	0.128	1.06	1.00	0.157	No
187	3.74	66.01	17.07	48.94	0.95	0.183	1.43	0.128	1.06	1.00	0.158	No
188	3.76	66.36	17.27	49.10	0.95	0.183	1.43	0.128	1.06	1.00	0.159	No
189	3.78	66.72	17.46	49.26	0.95	0.183	1.43	0.128	1.06	1.00	0.160	No
190	3.80	67.07	17.66	49.41	0.95	0.184	1.43	0.129	1.06	1.00	0.161	No
191	3.82	67.42	17.85	49.57	0.95	0.184	1.43	0.129	1.06	1.00	0.161	No
192	3.84	67.77	18.05	49.72	0.95	0.184	1.43	0.129	1.06	1.00	0.162	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	68.11	18.25	49.86	0.95	0.185	1.43	0.129	1.06	1.00	0.162	No
194	3.88	68.45	18.44	50.00	0.94	0.185	1.43	0.129	1.06	1.00	0.163	No
195	3.90	68.78	18.64	50.14	0.94	0.185	1.43	0.130	1.06	1.00	0.163	No
196	3.92	69.11	18.84	50.28	0.94	0.186	1.43	0.130	1.06	1.00	0.163	No
197	3.94	69.44	19.03	50.41	0.94	0.186	1.43	0.130	1.06	1.00	0.163	No
198	3.96	69.77	19.23	50.54	0.94	0.186	1.43	0.130	1.06	1.00	0.164	No
199	3.98	70.09	19.42	50.67	0.94	0.187	1.43	0.131	1.06	1.00	0.164	No
200	4.00	70.42	19.62	50.80	0.94	0.187	1.43	0.131	1.06	1.00	0.164	No
201	4.02	70.74	19.82	50.93	0.94	0.187	1.43	0.131	1.06	1.00	0.164	No
202	4.04	71.06	20.01	51.05	0.94	0.187	1.43	0.131	1.06	1.00	0.165	No
203	4.06	71.38	20.21	51.17	0.94	0.188	1.43	0.131	1.06	1.00	0.165	No
204	4.08	71.70	20.40	51.29	0.94	0.188	1.43	0.132	1.06	1.00	0.166	No
205	4.10	72.01	20.60	51.41	0.94	0.188	1.43	0.132	1.06	1.00	0.166	No
206	4.12	72.33	20.80	51.53	0.94	0.189	1.43	0.132	1.06	1.00	0.166	No
207	4.14	72.65	20.99	51.66	0.94	0.189	1.43	0.132	1.06	1.00	0.166	No
208	4.16	72.97	21.19	51.78	0.94	0.189	1.43	0.133	1.06	1.00	0.167	No
209	4.18	73.29	21.39	51.91	0.94	0.190	1.43	0.133	1.05	1.00	0.167	No
210	4.20	73.62	21.58	52.03	0.94	0.190	1.43	0.133	1.05	1.00	0.168	No
211	4.22	73.94	21.78	52.16	0.94	0.190	1.43	0.133	1.05	1.00	0.168	No
212	4.25	74.42	22.07	52.35	0.94	0.191	1.43	0.133	1.05	1.00	0.168	No
213	4.26	74.58	22.17	52.41	0.94	0.191	1.43	0.134	1.05	1.00	0.168	No
214	4.28	74.91	22.37	52.54	0.94	0.191	1.43	0.134	1.05	1.00	0.168	No
215	4.30	75.23	22.56	52.67	0.94	0.191	1.43	0.134	1.05	1.00	0.169	No
216	4.32	75.55	22.76	52.79	0.94	0.192	1.43	0.134	1.05	1.00	0.169	No
217	4.34	75.88	22.96	52.92	0.94	0.192	1.43	0.134	1.05	1.00	0.169	No
218	4.36	76.20	23.15	53.05	0.94	0.192	1.43	0.134	1.05	1.00	0.170	No
219	4.38	76.52	23.35	53.17	0.93	0.192	1.43	0.135	1.05	1.00	0.170	No
220	4.40	76.84	23.54	53.29	0.93	0.193	1.43	0.135	1.05	1.00	0.170	No
221	4.42	77.16	23.74	53.42	0.93	0.193	1.43	0.135	1.05	1.00	0.171	No
222	4.44	77.47	23.94	53.54	0.93	0.193	1.43	0.135	1.05	1.00	0.171	No
223	4.46	77.79	24.13	53.66	0.93	0.193	1.43	0.135	1.05	1.00	0.171	No
224	4.48	78.11	24.33	53.78	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
225	4.50	78.44	24.53	53.91	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
226	4.52	78.76	24.72	54.04	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
227	4.55	79.25	25.02	54.24	0.93	0.195	1.43	0.136	1.05	1.00	0.172	No
228	4.56	79.42	25.11	54.30	0.93	0.195	1.43	0.136	1.05	1.00	0.172	No
229	4.58	79.75	25.31	54.44	0.93	0.195	1.43	0.136	1.05	1.00	0.172	No
230	4.60	80.08	25.51	54.58	0.93	0.195	1.43	0.137	1.05	1.00	0.172	No
231	4.62	80.42	25.70	54.72	0.93	0.195	1.43	0.137	1.05	1.00	0.172	No
232	4.64	80.75	25.90	54.85	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
233	4.66	81.09	26.09	54.99	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
234	4.68	81.42	26.29	55.13	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
235	4.70	81.76	26.49	55.27	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
236	4.72	82.09	26.68	55.41	0.93	0.197	1.43	0.138	1.05	1.00	0.173	No
237	4.74	82.43	26.88	55.55	0.93	0.197	1.43	0.138	1.05	1.00	0.173	No
238	4.76	82.76	27.08	55.68	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
239	4.78	83.09	27.27	55.82	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
240	4.80	83.43	27.47	55.96	0.93	0.198	1.43	0.138	1.05	1.00	0.175	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	83.76	27.66	56.09	0.93	0.198	1.43	0.138	1.05	1.00	0.175	No
242	4.84	84.09	27.86	56.23	0.93	0.198	1.43	0.139	1.05	1.00	0.175	No
243	4.86	84.43	28.06	56.37	0.93	0.198	1.43	0.139	1.05	1.00	0.175	No
244	4.88	84.77	28.25	56.52	0.92	0.198	1.43	0.139	1.05	1.00	0.175	No
245	4.90	85.11	28.45	56.67	0.92	0.199	1.43	0.139	1.05	1.00	0.175	No
246	4.92	85.46	28.65	56.81	0.92	0.199	1.43	0.139	1.05	1.00	0.176	No
247	4.94	85.80	28.84	56.96	0.92	0.199	1.43	0.139	1.05	1.00	0.176	No
248	4.97	86.31	29.14	57.17	0.92	0.199	1.43	0.139	1.05	1.00	0.177	No
249	4.98	86.48	29.23	57.25	0.92	0.199	1.43	0.140	1.05	1.00	0.177	No
250	5.01	86.99	29.53	57.46	0.92	0.200	1.43	0.140	1.05	1.00	0.178	No
251	5.02	87.16	29.63	57.53	0.92	0.200	1.43	0.140	1.05	1.00	0.178	No
252	5.04	87.50	29.82	57.68	0.92	0.200	1.43	0.140	1.05	1.00	0.178	No
253	5.06	87.84	30.02	57.82	0.92	0.200	1.43	0.140	1.04	1.00	0.179	No
254	5.08	88.17	30.21	57.96	0.92	0.200	1.43	0.140	1.04	1.00	0.179	No
255	5.10	88.50	30.41	58.09	0.92	0.200	1.43	0.140	1.04	1.00	0.179	No
256	5.12	88.83	30.61	58.22	0.92	0.201	1.43	0.140	1.04	1.00	0.179	No
257	5.14	89.16	30.80	58.35	0.92	0.201	1.43	0.141	1.05	1.00	0.178	No
258	5.16	89.49	31.00	58.49	0.92	0.201	1.43	0.141	1.05	1.00	0.178	No
259	5.19	89.98	31.29	58.69	0.92	0.201	1.43	0.141	1.05	1.00	0.178	No
260	5.20	90.15	31.39	58.75	0.92	0.201	1.43	0.141	1.05	1.00	0.179	No
261	5.22	90.48	31.59	58.89	0.92	0.202	1.43	0.141	1.04	1.00	0.180	No
262	5.24	90.81	31.78	59.02	0.92	0.202	1.43	0.141	1.04	1.00	0.180	No
263	5.26	91.14	31.98	59.16	0.92	0.202	1.43	0.141	1.04	1.00	0.180	No
264	5.28	91.47	32.18	59.29	0.92	0.202	1.43	0.141	1.04	1.00	0.180	No
265	5.30	91.80	32.37	59.42	0.92	0.202	1.43	0.142	1.04	1.00	0.180	No
266	5.32	92.12	32.57	59.56	0.92	0.203	1.43	0.142	1.04	1.00	0.180	No
267	5.34	92.45	32.77	59.69	0.92	0.203	1.43	0.142	1.04	1.00	0.180	No
268	5.36	92.78	32.96	59.82	0.91	0.203	1.43	0.142	1.04	1.00	0.180	No
269	5.38	93.11	33.16	59.95	0.91	0.203	1.43	0.142	1.04	1.00	0.180	No
270	5.40	93.45	33.35	60.10	0.91	0.203	1.43	0.142	1.04	1.00	0.180	No
271	5.42	93.79	33.55	60.24	0.91	0.203	1.43	0.142	1.04	1.00	0.180	No
272	5.44	94.14	33.75	60.39	0.91	0.203	1.43	0.142	1.04	1.00	0.180	No
273	5.46	94.49	33.94	60.54	0.91	0.204	1.43	0.143	1.04	1.00	0.181	No
274	5.48	94.83	34.14	60.70	0.91	0.204	1.43	0.143	1.04	1.00	0.182	No
275	5.50	95.18	34.34	60.85	0.91	0.204	1.43	0.143	1.04	1.00	0.182	No
276	5.52	95.53	34.53	61.00	0.91	0.204	1.43	0.143	1.04	1.00	0.183	No
277	5.54	95.88	34.73	61.16	0.91	0.204	1.43	0.143	1.04	1.00	0.183	No
278	5.56	96.23	34.92	61.31	0.91	0.204	1.43	0.143	1.04	1.00	0.183	No
279	5.58	96.57	35.12	61.45	0.91	0.204	1.43	0.143	1.04	1.00	0.184	No
280	5.60	96.91	35.32	61.60	0.91	0.205	1.43	0.143	1.04	1.00	0.184	No
281	5.62	97.25	35.51	61.73	0.91	0.205	1.43	0.143	1.04	1.00	0.184	No
282	5.64	97.58	35.71	61.87	0.91	0.205	1.43	0.143	1.04	1.00	0.184	No
283	5.66	97.90	35.90	62.00	0.91	0.205	1.43	0.144	1.04	1.00	0.184	No
284	5.68	98.22	36.10	62.12	0.91	0.205	1.43	0.144	1.04	1.00	0.184	No
285	5.70	98.54	36.30	62.25	0.91	0.205	1.43	0.144	1.04	1.00	0.184	No
286	5.72	98.86	36.49	62.37	0.91	0.206	1.43	0.144	1.04	1.00	0.185	No
287	5.74	99.18	36.69	62.49	0.91	0.206	1.43	0.144	1.04	1.00	0.185	No
288	5.76	99.51	36.89	62.62	0.91	0.206	1.43	0.144	1.04	1.00	0.185	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	99.83	37.08	62.75	0.91	0.206	1.43	0.144	1.04	1.00	0.185	No
290	5.80	100.16	37.28	62.88	0.91	0.206	1.43	0.144	1.04	1.00	0.185	No
291	5.82	100.48	37.47	63.01	0.90	0.206	1.43	0.144	1.04	1.00	0.185	No
292	5.85	100.97	37.77	63.20	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
293	5.86	101.14	37.87	63.27	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
294	5.88	101.47	38.06	63.41	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
295	5.90	101.80	38.26	63.54	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
296	5.92	102.13	38.46	63.68	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
297	5.94	102.47	38.65	63.82	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
298	5.96	102.80	38.85	63.96	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
299	5.98	103.14	39.04	64.10	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
300	6.00	103.48	39.24	64.24	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
301	6.02	103.83	39.44	64.39	0.90	0.208	1.43	0.145	1.04	1.00	0.185	No
302	6.04	104.18	39.63	64.54	0.90	0.208	1.43	0.145	1.04	1.00	0.185	No
303	6.06	104.53	39.83	64.70	0.90	0.208	1.43	0.145	1.04	1.00	0.185	No
304	6.08	104.88	40.02	64.85	0.90	0.208	1.43	0.146	1.04	1.00	0.185	No
305	6.10	105.23	40.22	65.01	0.90	0.208	1.43	0.146	1.04	1.00	0.185	No
306	6.12	105.59	40.42	65.17	0.90	0.208	1.43	0.146	1.04	1.00	0.186	No
307	6.14	105.94	40.61	65.33	0.90	0.208	1.43	0.146	1.04	1.00	0.186	No
308	6.16	106.30	40.81	65.49	0.90	0.208	1.43	0.146	1.04	1.00	0.186	No
309	6.18	106.66	41.01	65.65	0.90	0.208	1.43	0.146	1.04	1.00	0.186	No
310	6.20	107.02	41.20	65.82	0.90	0.208	1.43	0.146	1.04	1.00	0.187	No
311	6.22	107.38	41.40	65.98	0.90	0.208	1.43	0.146	1.04	1.00	0.187	No
312	6.25	107.91	41.69	66.22	0.90	0.209	1.43	0.146	1.04	1.00	0.187	No
313	6.26	108.09	41.79	66.30	0.89	0.209	1.43	0.146	1.04	1.00	0.187	No
314	6.28	108.45	41.99	66.46	0.89	0.209	1.43	0.146	1.03	1.00	0.187	No
315	6.30	108.80	42.18	66.62	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
316	6.32	109.15	42.38	66.77	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
317	6.34	109.51	42.58	66.93	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
318	6.36	109.86	42.77	67.08	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
319	6.38	110.21	42.97	67.24	0.89	0.209	1.43	0.146	1.03	1.00	0.189	No
320	6.40	110.55	43.16	67.39	0.89	0.209	1.43	0.146	1.03	1.00	0.189	No
321	6.42	110.90	43.36	67.54	0.89	0.209	1.43	0.147	1.03	1.00	0.189	No
322	6.44	111.24	43.56	67.69	0.89	0.209	1.43	0.147	1.03	1.00	0.189	No
323	6.46	111.58	43.75	67.83	0.89	0.209	1.43	0.147	1.03	1.00	0.189	No
324	6.48	111.92	43.95	67.97	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
325	6.50	112.26	44.15	68.11	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
326	6.52	112.59	44.34	68.25	0.89	0.210	1.43	0.147	1.03	1.00	0.189	No
327	6.54	112.93	44.54	68.39	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
328	6.56	113.26	44.73	68.53	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
329	6.58	113.60	44.93	68.67	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
330	6.60	113.93	45.13	68.81	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
331	6.62	114.27	45.32	68.95	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
332	6.64	114.60	45.52	69.09	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
333	6.66	114.94	45.71	69.22	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
334	6.68	115.27	45.91	69.36	0.89	0.210	1.43	0.147	1.03	1.00	0.190	No
335	6.70	115.61	46.11	69.50	0.89	0.211	1.43	0.147	1.03	1.00	0.191	No
336	6.72	115.94	46.30	69.64	0.88	0.211	1.43	0.147	1.03	1.00	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	116.27	46.50	69.77	0.88	0.211	1.43	0.147	1.03	1.00	0.191	No
338	6.76	116.60	46.70	69.90	0.88	0.211	1.43	0.148	1.03	1.00	0.191	No
339	6.78	116.92	46.89	70.03	0.88	0.211	1.43	0.148	1.03	1.00	0.191	No
340	6.80	117.24	47.09	70.16	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
341	6.82	117.56	47.28	70.28	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
342	6.84	117.88	47.48	70.39	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
343	6.86	118.19	47.68	70.51	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
344	6.88	118.51	47.87	70.63	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
345	6.90	118.82	48.07	70.75	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
346	6.93	119.30	48.36	70.94	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
347	6.94	119.46	48.46	71.00	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
348	6.96	119.77	48.66	71.11	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
349	6.98	120.09	48.85	71.23	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
350	7.00	120.40	49.05	71.35	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
351	7.03	120.87	49.34	71.52	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
352	7.04	121.02	49.44	71.58	0.88	0.212	1.43	0.148	1.03	1.00	0.193	No
353	7.06	121.33	49.64	71.69	0.88	0.212	1.43	0.149	1.03	1.00	0.193	No
354	7.08	121.64	49.83	71.80	0.88	0.212	1.43	0.149	1.03	1.00	0.193	No
355	7.10	121.95	50.03	71.91	0.88	0.212	1.43	0.149	1.03	1.00	0.193	No
356	7.12	122.26	50.23	72.03	0.88	0.213	1.43	0.149	1.03	1.00	0.193	No
357	7.14	122.57	50.42	72.14	0.88	0.213	1.43	0.149	1.03	1.00	0.193	No
358	7.16	122.88	50.62	72.26	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
359	7.18	123.20	50.82	72.38	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
360	7.20	123.51	51.01	72.50	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
361	7.22	123.83	51.21	72.62	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
362	7.24	124.15	51.40	72.75	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
363	7.26	124.47	51.60	72.87	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
364	7.28	124.79	51.80	72.99	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
365	7.30	125.11	51.99	73.11	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
366	7.32	125.43	52.19	73.24	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
367	7.34	125.75	52.39	73.37	0.87	0.213	1.43	0.149	1.03	1.00	0.193	No
368	7.36	126.08	52.58	73.50	0.87	0.213	1.43	0.149	1.03	1.00	0.194	No
369	7.38	126.41	52.78	73.63	0.87	0.213	1.43	0.149	1.03	1.00	0.194	No
370	7.40	126.74	52.97	73.76	0.87	0.214	1.43	0.149	1.03	1.00	0.193	No
371	7.42	127.07	53.17	73.90	0.87	0.214	1.43	0.150	1.03	1.00	0.194	No
372	7.44	127.40	53.37	74.03	0.87	0.214	1.43	0.150	1.03	1.00	0.194	No
373	7.46	127.73	53.56	74.17	0.87	0.214	1.43	0.150	1.03	1.00	0.194	No
374	7.48	128.07	53.76	74.31	0.87	0.214	1.43	0.150	1.03	1.00	0.194	No
375	7.50	128.41	53.96	74.45	0.87	0.214	1.43	0.150	1.03	1.00	0.194	No
376	7.52	128.74	54.15	74.59	0.87	0.214	1.43	0.150	1.02	1.00	0.194	No
377	7.54	129.08	54.35	74.74	0.87	0.214	1.43	0.150	1.02	1.00	0.194	No
378	7.56	129.42	54.54	74.88	0.87	0.214	1.43	0.150	1.02	1.00	0.194	No
379	7.58	129.76	54.74	75.02	0.87	0.214	1.43	0.150	1.02	1.00	0.194	No
380	7.60	130.10	54.94	75.17	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
381	7.62	130.44	55.13	75.31	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
382	7.64	130.78	55.33	75.45	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
383	7.66	131.11	55.52	75.59	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
384	7.68	131.45	55.72	75.73	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	131.78	55.92	75.87	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
386	7.72	132.11	56.11	76.00	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
387	7.74	132.44	56.31	76.13	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
388	7.76	132.77	56.51	76.27	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
389	7.78	133.10	56.70	76.39	0.86	0.214	1.43	0.150	1.02	1.00	0.196	No
390	7.80	133.42	56.90	76.52	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
391	7.82	133.74	57.09	76.65	0.86	0.214	1.43	0.150	1.02	1.00	0.195	No
392	7.85	134.23	57.39	76.84	0.86	0.215	1.43	0.150	1.02	1.00	0.195	No
393	7.86	134.39	57.49	76.90	0.86	0.215	1.43	0.150	1.02	1.00	0.195	No
394	7.88	134.71	57.68	77.03	0.86	0.215	1.43	0.150	1.02	1.00	0.195	No
395	7.91	135.20	57.98	77.22	0.86	0.215	1.43	0.150	1.02	1.00	0.196	No
396	7.92	135.36	58.08	77.29	0.86	0.215	1.43	0.150	1.02	1.00	0.196	No
397	7.94	135.69	58.27	77.41	0.86	0.215	1.43	0.150	1.02	1.00	0.196	No
398	7.97	136.17	58.57	77.60	0.86	0.215	1.43	0.150	1.02	1.00	0.196	No
399	7.98	136.33	58.66	77.67	0.86	0.215	1.43	0.150	1.02	1.00	0.196	No
400	8.00	136.65	58.86	77.79	0.86	0.215	1.43	0.150	1.02	1.00	0.196	No
401	8.02	136.97	59.06	77.91	0.85	0.215	1.43	0.150	1.02	1.00	0.196	No
402	8.04	137.29	59.25	78.04	0.85	0.215	1.43	0.150	1.02	1.00	0.196	No
403	8.06	137.61	59.45	78.16	0.85	0.215	1.43	0.150	1.02	1.00	0.196	No
404	8.08	137.93	59.64	78.29	0.85	0.215	1.43	0.150	1.02	1.00	0.196	No
405	8.10	138.25	59.84	78.41	0.85	0.215	1.43	0.151	1.02	1.00	0.196	No
406	8.12	138.58	60.04	78.54	0.85	0.215	1.43	0.151	1.02	1.00	0.196	No
407	8.14	138.91	60.23	78.67	0.85	0.215	1.43	0.151	1.02	1.00	0.196	No
408	8.16	139.23	60.43	78.80	0.85	0.215	1.43	0.151	1.02	1.00	0.196	No
409	8.18	139.56	60.63	78.94	0.85	0.215	1.43	0.151	1.02	1.00	0.197	No
410	8.20	139.89	60.82	79.07	0.85	0.215	1.43	0.151	1.02	1.00	0.197	No
411	8.22	140.22	61.02	79.20	0.85	0.215	1.43	0.151	1.02	1.00	0.197	No
412	8.24	140.55	61.21	79.33	0.85	0.215	1.43	0.151	1.02	1.00	0.196	No
413	8.26	140.88	61.41	79.47	0.85	0.215	1.43	0.151	1.02	1.00	0.196	No
414	8.28	141.21	61.61	79.60	0.85	0.215	1.43	0.151	1.02	1.00	2.000	Yes
415	8.30	141.54	61.80	79.73	0.85	0.215	1.43	0.151	1.02	1.00	2.000	Yes
416	8.32	141.86	62.00	79.87	0.85	0.215	1.43	0.151	1.02	1.00	2.000	Yes
417	8.34	142.20	62.20	80.00	0.85	0.215	1.43	0.151	1.02	1.00	2.000	Yes
418	8.36	142.54	62.39	80.14	0.85	0.215	1.43	0.151	1.02	1.00	2.000	Yes
419	8.38	142.88	62.59	80.29	0.85	0.215	1.43	0.151	1.02	1.00	2.000	Yes
420	8.40	143.22	62.78	80.43	0.85	0.215	1.43	0.151	1.02	1.00	2.000	Yes
421	8.42	143.56	62.98	80.58	0.85	0.215	1.43	0.151	1.02	1.00	2.000	Yes
422	8.45	144.07	63.27	80.79	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
423	8.46	144.24	63.37	80.87	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
424	8.48	144.59	63.57	81.02	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
425	8.50	144.93	63.77	81.17	0.84	0.215	1.43	0.151	1.02	1.00	0.191	No
426	8.52	145.27	63.96	81.31	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
427	8.54	145.60	64.16	81.44	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
428	8.56	145.92	64.35	81.57	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
429	8.58	146.25	64.55	81.70	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
430	8.60	146.58	64.75	81.83	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
431	8.62	146.91	64.94	81.97	0.84	0.215	1.43	0.151	1.02	1.00	2.000	Yes
432	8.64	147.24	65.14	82.10	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	147.57	65.33	82.24	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No
434	8.68	147.91	65.53	82.38	0.84	0.215	1.43	0.151	1.02	1.00	0.197	No
435	8.70	148.24	65.73	82.51	0.84	0.215	1.43	0.151	1.02	1.00	0.198	No
436	8.72	148.56	65.92	82.64	0.84	0.216	1.43	0.151	1.02	1.00	0.198	No
437	8.74	148.89	66.12	82.77	0.84	0.216	1.43	0.151	1.02	1.00	0.198	No
438	8.76	149.21	66.32	82.90	0.84	0.216	1.43	0.151	1.02	1.00	0.198	No
439	8.78	149.54	66.51	83.03	0.84	0.216	1.43	0.151	1.02	1.00	0.198	No
440	8.80	149.87	66.71	83.16	0.84	0.216	1.43	0.151	1.02	1.00	0.198	No
441	8.82	150.20	66.90	83.29	0.84	0.216	1.43	0.151	1.02	1.00	0.198	No
442	8.84	150.52	67.10	83.42	0.84	0.216	1.43	0.151	1.02	1.00	0.198	No
443	8.86	150.85	67.30	83.55	0.83	0.216	1.43	0.151	1.02	1.00	0.198	No
444	8.88	151.18	67.49	83.68	0.83	0.216	1.43	0.151	1.02	1.00	0.198	No
445	8.90	151.50	67.69	83.81	0.83	0.216	1.43	0.151	1.02	1.00	0.198	No
446	8.92	151.83	67.89	83.94	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
447	8.94	152.15	68.08	84.07	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
448	8.96	152.47	68.28	84.20	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
449	8.99	152.96	68.57	84.38	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
450	9.00	153.12	68.67	84.45	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
451	9.02	153.44	68.87	84.57	0.83	0.216	1.43	0.151	1.01	1.00	0.199	No
452	9.04	153.76	69.06	84.69	0.83	0.216	1.43	0.151	1.01	1.00	0.199	No
453	9.06	154.08	69.26	84.82	0.83	0.216	1.43	0.151	1.01	1.00	0.199	No
454	9.09	154.55	69.55	85.00	0.83	0.216	1.43	0.151	1.01	1.00	0.199	No
455	9.10	154.71	69.65	85.06	0.83	0.216	1.43	0.151	1.01	1.00	0.199	No
456	9.12	155.03	69.85	85.19	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
457	9.14	155.35	70.04	85.31	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
458	9.16	155.68	70.24	85.44	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
459	9.18	156.00	70.44	85.57	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
460	9.20	156.33	70.63	85.70	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
461	9.22	156.66	70.83	85.83	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
462	9.24	156.99	71.02	85.97	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
463	9.26	157.33	71.22	86.11	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
464	9.28	157.66	71.42	86.25	0.83	0.216	1.43	0.151	1.01	1.00	0.198	No
465	9.30	158.00	71.61	86.38	0.82	0.216	1.43	0.151	1.01	1.00	0.198	No
466	9.32	158.33	71.81	86.52	0.82	0.216	1.43	0.151	1.01	1.00	0.199	No
467	9.34	158.66	72.01	86.66	0.82	0.216	1.43	0.151	1.01	1.00	0.199	No
468	9.36	158.99	72.20	86.79	0.82	0.216	1.43	0.151	1.01	1.00	0.198	No
469	9.38	159.32	72.40	86.93	0.82	0.216	1.43	0.151	1.01	1.00	0.198	No
470	9.40	159.65	72.59	87.06	0.82	0.216	1.43	0.151	1.01	1.00	0.199	No
471	9.42	159.98	72.79	87.19	0.82	0.216	1.43	0.151	1.01	1.00	0.199	No
472	9.44	160.31	72.99	87.33	0.82	0.216	1.43	0.151	1.01	1.00	0.198	No
473	9.46	160.64	73.18	87.46	0.82	0.216	1.43	0.151	1.01	1.00	0.198	No
474	9.48	160.98	73.38	87.60	0.82	0.216	1.43	0.151	1.01	1.00	0.198	No
475	9.50	161.31	73.58	87.73	0.82	0.216	1.43	0.151	1.01	1.00	0.198	No
476	9.52	161.65	73.77	87.88	0.82	0.216	1.43	0.151	1.01	1.00	0.198	No
477	9.54	161.98	73.97	88.02	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
478	9.56	162.32	74.16	88.16	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
479	9.58	162.66	74.36	88.30	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
480	9.60	163.00	74.56	88.44	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	163.34	74.75	88.59	0.82	0.215	1.43	0.151	1.01	1.00	0.198	No
482	9.64	163.68	74.95	88.73	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
483	9.66	164.01	75.14	88.87	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
484	9.68	164.35	75.34	89.01	0.82	0.215	1.43	0.151	1.01	1.00	0.199	No
485	9.70	164.68	75.54	89.14	0.81	0.215	1.43	0.151	1.01	1.00	0.199	No
486	9.72	165.01	75.73	89.28	0.81	0.215	1.43	0.151	1.01	1.00	0.199	No
487	9.74	165.34	75.93	89.41	0.81	0.215	1.43	0.151	1.01	1.00	0.199	No
488	9.76	165.67	76.13	89.54	0.81	0.215	1.43	0.151	1.01	1.00	0.198	No
489	9.78	166.00	76.32	89.68	0.81	0.215	1.43	0.151	1.01	1.00	0.198	No
490	9.80	166.34	76.52	89.82	0.81	0.215	1.43	0.151	1.01	1.00	0.198	No
491	9.82	166.68	76.71	89.97	0.81	0.215	1.43	0.151	1.01	1.00	0.198	No
492	9.84	167.02	76.91	90.11	0.81	0.215	1.43	0.151	1.01	1.00	0.198	No
493	9.86	167.36	77.11	90.25	0.81	0.215	1.43	0.151	1.01	1.00	0.198	No
494	9.88	167.69	77.30	90.39	0.81	0.215	1.43	0.151	1.01	1.00	0.198	No
495	9.90	168.03	77.50	90.53	0.81	0.215	1.43	0.151	1.01	1.00	0.198	No
496	9.92	168.37	77.70	90.68	0.81	0.215	1.43	0.150	1.01	1.00	0.197	No
497	9.94	168.72	77.89	90.83	0.81	0.215	1.43	0.150	1.01	1.00	0.197	No
498	9.96	169.06	78.09	90.98	0.81	0.215	1.43	0.150	1.01	1.00	0.197	No
499	9.98	169.41	78.28	91.13	0.81	0.215	1.43	0.150	1.01	1.00	0.197	No
500	10.01	169.93	78.58	91.35	0.81	0.215	1.43	0.150	1.01	1.00	0.197	No
501	10.02	170.10	78.68	91.42	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
502	10.04	170.43	78.87	91.56	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
503	10.06	170.77	79.07	91.70	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
504	10.08	171.10	79.26	91.84	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
505	10.10	171.44	79.46	91.98	0.81	0.215	1.43	0.150	1.01	1.00	0.198	No
506	10.12	171.77	79.66	92.12	0.80	0.215	1.43	0.150	1.01	1.00	0.197	No
507	10.14	172.11	79.85	92.26	0.80	0.215	1.43	0.150	1.01	1.00	0.197	No
508	10.16	172.45	80.05	92.40	0.80	0.215	1.43	0.150	1.01	1.00	0.197	No
509	10.18	172.80	80.25	92.55	0.80	0.215	1.43	0.150	1.01	1.00	0.197	No
510	10.20	173.14	80.44	92.70	0.80	0.214	1.43	0.150	1.01	1.00	0.197	No
511	10.22	173.49	80.64	92.85	0.80	0.214	1.43	0.150	1.01	1.00	0.196	No
512	10.24	173.84	80.83	93.00	0.80	0.214	1.43	0.150	1.01	1.00	0.196	No
513	10.26	174.18	81.03	93.15	0.80	0.214	1.43	0.150	1.01	1.00	0.197	No
514	10.28	174.52	81.23	93.29	0.80	0.214	1.43	0.150	1.01	1.00	0.197	No
515	10.30	174.86	81.42	93.43	0.80	0.214	1.43	0.150	1.01	1.00	0.197	No
516	10.32	175.19	81.62	93.57	0.80	0.214	1.43	0.150	1.01	1.00	0.197	No
517	10.34	175.53	81.82	93.72	0.80	0.214	1.43	0.150	1.01	1.00	0.197	No
518	10.36	175.88	82.01	93.87	0.80	0.214	1.43	0.150	1.01	1.00	0.196	No
519	10.38	176.22	82.21	94.02	0.80	0.214	1.43	0.150	1.01	1.00	0.196	No
520	10.40	176.57	82.40	94.17	0.80	0.214	1.43	0.150	1.01	1.00	0.196	No
521	10.42	176.92	82.60	94.32	0.80	0.214	1.43	0.150	1.01	1.00	0.196	No
522	10.44	177.26	82.80	94.46	0.80	0.214	1.43	0.150	1.01	1.00	0.196	No
523	10.46	177.60	82.99	94.61	0.80	0.214	1.43	0.150	1.01	1.00	0.197	No
524	10.48	177.93	83.19	94.74	0.80	0.214	1.43	0.150	1.01	1.00	0.197	No
525	10.50	178.26	83.39	94.88	0.80	0.214	1.43	0.150	1.01	1.00	0.198	No
526	10.52	178.59	83.58	95.01	0.80	0.214	1.43	0.150	1.01	1.00	0.198	No
527	10.54	178.92	83.78	95.14	0.79	0.214	1.43	0.150	1.01	1.00	0.198	No
528	10.56	179.25	83.97	95.27	0.79	0.214	1.43	0.150	1.00	1.00	0.198	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	179.58	84.17	95.41	0.79	0.214	1.43	0.150	1.00	1.00	0.198	No
530	10.60	179.91	84.37	95.54	0.79	0.214	1.43	0.150	1.00	1.00	0.197	No
531	10.62	180.25	84.56	95.68	0.79	0.214	1.43	0.150	1.00	1.00	0.197	No
532	10.64	180.58	84.76	95.82	0.79	0.214	1.43	0.149	1.00	1.00	0.198	No
533	10.66	180.91	84.95	95.95	0.79	0.214	1.43	0.149	1.00	1.00	0.198	No
534	10.68	181.24	85.15	96.09	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
535	10.70	181.58	85.35	96.23	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
536	10.72	181.92	85.54	96.37	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
537	10.74	182.26	85.74	96.52	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
538	10.76	182.60	85.94	96.66	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
539	10.78	182.94	86.13	96.80	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
540	10.80	183.27	86.33	96.94	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
541	10.82	183.59	86.52	97.07	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
542	10.84	183.91	86.72	97.19	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
543	10.87	184.40	87.01	97.38	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
544	10.88	184.56	87.11	97.45	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
545	10.90	184.90	87.31	97.59	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
546	10.92	185.24	87.51	97.74	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
547	10.95	185.75	87.80	97.95	0.79	0.213	1.43	0.149	1.00	1.00	2.000	Yes
548	10.96	185.92	87.90	98.02	0.78	0.213	1.43	0.149	1.00	1.00	2.000	Yes
549	10.98	186.25	88.09	98.15	0.78	0.213	1.43	0.149	1.00	1.00	2.000	Yes
550	11.00	186.57	88.29	98.28	0.78	0.213	1.43	0.149	1.00	1.00	2.000	Yes
551	11.02	186.90	88.49	98.42	0.78	0.213	1.43	0.149	1.00	1.00	0.197	No
552	11.04	187.24	88.68	98.55	0.78	0.213	1.43	0.149	1.00	1.00	0.197	No
553	11.06	187.57	88.88	98.69	0.78	0.213	1.43	0.149	1.00	1.00	0.197	No
554	11.08	187.90	89.07	98.83	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
555	11.10	188.24	89.27	98.96	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
556	11.12	188.57	89.47	99.10	0.78	0.213	1.43	0.149	1.00	1.00	0.198	No
557	11.14	188.90	89.66	99.24	0.78	0.212	1.43	0.149	1.00	1.00	0.198	No
558	11.17	189.39	89.96	99.44	0.78	0.212	1.43	0.149	1.00	1.00	0.198	No
559	11.18	189.56	90.06	99.50	0.78	0.212	1.43	0.149	1.00	1.00	0.198	No
560	11.20	189.89	90.25	99.64	0.78	0.212	1.43	0.149	1.00	1.00	0.198	No
561	11.22	190.21	90.45	99.77	0.78	0.212	1.43	0.149	1.00	1.00	0.198	No
562	11.24	190.54	90.64	99.89	0.78	0.212	1.43	0.149	1.00	1.00	0.197	No
563	11.26	190.87	90.84	100.03	0.78	0.212	1.43	0.149	1.00	1.00	0.198	No
564	11.28	191.19	91.04	100.16	0.78	0.212	1.43	0.149	1.00	1.00	0.198	No
565	11.30	191.52	91.23	100.29	0.78	0.212	1.43	0.148	1.00	1.00	0.198	No
566	11.32	191.85	91.43	100.42	0.78	0.212	1.43	0.148	1.00	1.00	0.198	No
567	11.34	192.18	91.63	100.55	0.78	0.212	1.43	0.148	1.00	1.00	0.198	No
568	11.36	192.51	91.82	100.69	0.78	0.212	1.43	0.148	1.00	1.00	0.197	No
569	11.38	192.84	92.02	100.82	0.77	0.212	1.43	0.148	1.00	1.00	0.197	No
570	11.40	193.17	92.21	100.96	0.77	0.212	1.43	0.148	1.00	1.00	0.197	No
571	11.42	193.50	92.41	101.09	0.77	0.212	1.43	0.148	1.00	1.00	0.197	No
572	11.44	193.84	92.61	101.23	0.77	0.212	1.43	0.148	1.00	1.00	0.197	No
573	11.46	194.17	92.80	101.37	0.77	0.212	1.43	0.148	1.00	1.00	0.197	No
574	11.48	194.51	93.00	101.51	0.77	0.212	1.43	0.148	1.00	1.00	0.197	No
575	11.50	194.85	93.19	101.65	0.77	0.212	1.43	0.148	1.00	1.00	0.197	No
576	11.52	195.19	93.39	101.79	0.77	0.212	1.43	0.148	1.00	1.00	0.197	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	195.52	93.59	101.94	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
578	11.56	195.86	93.78	102.08	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
579	11.58	196.20	93.98	102.22	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
580	11.60	196.53	94.18	102.36	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
581	11.62	196.87	94.37	102.50	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
582	11.64	197.21	94.57	102.64	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
583	11.66	197.54	94.76	102.78	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
584	11.68	197.88	94.96	102.92	0.77	0.211	1.43	0.148	1.00	1.00	0.196	No
585	11.70	198.22	95.16	103.06	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
586	11.72	198.56	95.35	103.21	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
587	11.74	198.90	95.55	103.35	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
588	11.76	199.24	95.75	103.50	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
589	11.78	199.59	95.94	103.65	0.77	0.211	1.43	0.148	1.00	1.00	0.197	No
590	11.80	199.93	96.14	103.79	0.76	0.211	1.43	0.147	1.00	1.00	0.197	No
591	11.82	200.28	96.33	103.94	0.76	0.211	1.43	0.147	1.00	1.00	0.196	No
592	11.84	200.62	96.53	104.09	0.76	0.211	1.43	0.147	1.00	1.00	0.196	No
593	11.86	200.97	96.73	104.24	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
594	11.88	201.31	96.92	104.39	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
595	11.90	201.66	97.12	104.54	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
596	11.92	202.00	97.32	104.69	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
597	11.94	202.35	97.51	104.84	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
598	11.96	202.70	97.71	104.99	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
599	11.98	203.05	97.90	105.15	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
600	12.00	203.40	98.10	105.30	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
601	12.03	203.92	98.39	105.53	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
602	12.04	204.09	98.49	105.60	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
603	12.06	204.44	98.69	105.75	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
604	12.08	204.79	98.88	105.90	0.76	0.210	1.43	0.147	1.00	1.00	0.196	No
605	12.10	205.14	99.08	106.06	0.76	0.210	1.43	0.147	1.00	1.00	0.195	No
606	12.12	205.49	99.28	106.21	0.76	0.209	1.43	0.147	1.00	1.00	0.195	No
607	12.14	205.84	99.47	106.36	0.76	0.209	1.43	0.147	1.00	1.00	0.195	No
608	12.16	206.19	99.67	106.52	0.76	0.209	1.43	0.147	1.00	1.00	0.195	No
609	12.18	206.54	99.87	106.67	0.76	0.209	1.43	0.146	1.00	1.00	0.195	No
610	12.20	206.89	100.06	106.83	0.76	0.209	1.43	0.146	1.00	1.00	0.195	No
611	12.22	207.24	100.26	106.98	0.75	0.209	1.43	0.146	1.00	1.00	0.195	No
612	12.24	207.59	100.45	107.14	0.75	0.209	1.43	0.146	1.00	1.00	0.195	No
613	12.26	207.94	100.65	107.29	0.75	0.209	1.43	0.146	1.00	1.00	0.195	No
614	12.28	208.30	100.85	107.45	0.75	0.209	1.43	0.146	1.00	1.00	0.195	No
615	12.30	208.65	101.04	107.61	0.75	0.209	1.43	0.146	1.00	1.00	0.195	No
616	12.32	209.00	101.24	107.76	0.75	0.209	1.43	0.146	0.99	1.00	0.195	No
617	12.34	209.35	101.44	107.92	0.75	0.209	1.43	0.146	0.99	1.00	0.195	No
618	12.36	209.70	101.63	108.07	0.75	0.209	1.43	0.146	0.99	1.00	0.195	No
619	12.38	210.06	101.83	108.23	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
620	12.40	210.41	102.02	108.39	0.75	0.208	1.43	0.146	0.99	1.00	0.195	No
621	12.42	210.76	102.22	108.54	0.75	0.208	1.43	0.146	0.99	1.00	0.194	No
622	12.44	211.12	102.42	108.70	0.75	0.208	1.43	0.146	0.99	1.00	0.194	No
623	12.46	211.47	102.61	108.86	0.75	0.208	1.43	0.146	0.99	1.00	0.194	No
624	12.48	211.82	102.81	109.01	0.75	0.208	1.43	0.146	0.99	1.00	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	212.18	103.01	109.17	0.75	0.208	1.43	0.146	0.99	1.00	0.194	No
626	12.52	212.53	103.20	109.33	0.75	0.208	1.43	0.146	0.99	1.00	0.194	No
627	12.54	212.89	103.40	109.49	0.75	0.208	1.43	0.145	0.99	1.00	0.194	No
628	12.57	213.42	103.69	109.73	0.75	0.208	1.43	0.145	0.99	1.00	0.194	No
629	12.58	213.60	103.79	109.81	0.75	0.208	1.43	0.145	0.99	1.00	0.194	No
630	12.60	213.96	103.99	109.97	0.75	0.208	1.43	0.145	0.99	1.00	0.194	No
631	12.62	214.31	104.18	110.13	0.75	0.207	1.43	0.145	0.99	1.00	0.194	No
632	12.64	214.66	104.38	110.28	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
633	12.66	215.02	104.57	110.44	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
634	12.68	215.37	104.77	110.59	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
635	12.70	215.71	104.97	110.75	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
636	12.72	216.06	105.16	110.90	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
637	12.74	216.40	105.36	111.04	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
638	12.76	216.74	105.56	111.18	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
639	12.78	217.07	105.75	111.32	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
640	12.80	217.40	105.95	111.45	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
641	12.82	217.73	106.14	111.58	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
642	12.84	218.05	106.34	111.71	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
643	12.87	218.52	106.63	111.89	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
644	12.88	218.68	106.73	111.95	0.74	0.207	1.43	0.145	0.99	1.00	0.195	No
645	12.90	218.99	106.93	112.06	0.74	0.206	1.43	0.145	0.99	1.00	0.195	No
646	12.92	219.30	107.13	112.18	0.74	0.206	1.43	0.144	0.99	1.00	0.195	No
647	12.94	219.61	107.32	112.29	0.74	0.206	1.43	0.144	0.99	1.00	0.195	No
648	12.96	219.92	107.52	112.40	0.74	0.206	1.43	0.144	0.99	1.00	0.195	No
649	12.98	220.22	107.71	112.51	0.74	0.206	1.43	0.144	0.99	1.00	0.195	No
650	13.00	220.53	107.91	112.62	0.74	0.206	1.43	0.144	0.99	1.00	0.195	No
651	13.02	220.84	108.11	112.73	0.74	0.206	1.43	0.144	0.99	1.00	0.195	No
652	13.04	221.15	108.30	112.84	0.74	0.206	1.43	0.144	0.99	1.00	0.194	No
653	13.06	221.45	108.50	112.96	0.74	0.206	1.43	0.144	0.99	1.00	0.194	No
654	13.08	221.76	108.69	113.07	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
655	13.10	222.07	108.89	113.18	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
656	13.12	222.39	109.09	113.30	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
657	13.14	222.70	109.28	113.41	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
658	13.16	223.01	109.48	113.53	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
659	13.18	223.32	109.68	113.64	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
660	13.21	223.78	109.97	113.81	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
661	13.22	223.94	110.07	113.87	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
662	13.24	224.25	110.26	113.98	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
663	13.26	224.56	110.46	114.10	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
664	13.28	224.86	110.66	114.21	0.73	0.206	1.43	0.144	0.99	1.00	0.194	No
665	13.30	225.17	110.85	114.32	0.73	0.205	1.43	0.144	0.99	1.00	0.194	No
666	13.32	225.48	111.05	114.43	0.73	0.205	1.43	0.144	0.99	1.00	0.194	No
667	13.34	225.80	111.25	114.55	0.73	0.205	1.43	0.144	0.99	1.00	0.194	No
668	13.36	226.11	111.44	114.67	0.73	0.205	1.43	0.144	0.99	1.00	0.194	No
669	13.38	226.43	111.64	114.79	0.73	0.205	1.43	0.144	0.99	1.00	0.193	No
670	13.40	226.75	111.83	114.92	0.73	0.205	1.43	0.144	0.99	1.00	0.193	No
671	13.42	227.08	112.03	115.05	0.73	0.205	1.43	0.144	0.99	1.00	0.192	No
672	13.44	227.41	112.23	115.18	0.73	0.205	1.43	0.144	0.99	1.00	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	227.74	112.42	115.32	0.73	0.205	1.43	0.143	0.99	1.00	0.192	No
674	13.48	228.08	112.62	115.46	0.73	0.205	1.43	0.143	0.99	1.00	0.192	No
675	13.50	228.41	112.82	115.59	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
676	13.52	228.74	113.01	115.73	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
677	13.54	229.06	113.21	115.86	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
678	13.56	229.39	113.40	115.98	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
679	13.58	229.71	113.60	116.11	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
680	13.60	230.02	113.80	116.23	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
681	13.62	230.34	113.99	116.35	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
682	13.64	230.66	114.19	116.47	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
683	13.66	230.97	114.38	116.59	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
684	13.68	231.29	114.58	116.71	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
685	13.70	231.61	114.78	116.83	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
686	13.72	231.92	114.97	116.95	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
687	13.74	232.24	115.17	117.07	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
688	13.76	232.57	115.37	117.20	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
689	13.78	232.89	115.56	117.33	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
690	13.80	233.21	115.76	117.46	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
691	13.82	233.54	115.95	117.58	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
692	13.84	233.86	116.15	117.71	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
693	13.86	234.18	116.35	117.83	0.72	0.204	1.43	0.143	0.99	1.00	0.193	No
694	13.88	234.50	116.54	117.96	0.72	0.204	1.43	0.143	0.99	1.00	0.192	No
695	13.90	234.82	116.74	118.08	0.72	0.204	1.43	0.142	0.99	1.00	0.192	No
696	13.92	235.14	116.94	118.20	0.72	0.203	1.43	0.142	0.99	1.00	0.192	No
697	13.94	235.46	117.13	118.33	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
698	13.96	235.78	117.33	118.45	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
699	13.98	236.10	117.52	118.58	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
700	14.00	236.42	117.72	118.70	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
701	14.02	236.74	117.92	118.83	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
702	14.05	237.23	118.21	119.02	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
703	14.06	237.39	118.31	119.08	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
704	14.08	237.71	118.50	119.20	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
705	14.10	238.03	118.70	119.33	0.71	0.203	1.43	0.142	0.99	1.00	0.191	No
706	14.12	238.35	118.90	119.46	0.71	0.203	1.43	0.142	0.99	1.00	0.191	No
707	14.14	238.68	119.09	119.59	0.71	0.203	1.43	0.142	0.99	1.00	0.191	No
708	14.16	239.01	119.29	119.72	0.71	0.203	1.43	0.142	0.99	1.00	0.191	No
709	14.18	239.34	119.49	119.86	0.71	0.203	1.43	0.142	0.99	1.00	0.191	No
710	14.20	239.68	119.68	120.00	0.71	0.202	1.43	0.142	0.99	1.00	0.191	No
711	14.22	240.02	119.88	120.14	0.71	0.202	1.43	0.142	0.99	1.00	0.191	No
712	14.24	240.36	120.07	120.29	0.71	0.202	1.43	0.142	0.99	1.00	0.191	No
713	14.26	240.70	120.27	120.43	0.71	0.202	1.43	0.142	0.99	1.00	0.191	No
714	14.28	241.04	120.47	120.58	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
715	14.30	241.38	120.66	120.72	0.71	0.202	1.43	0.141	0.99	1.00	0.191	No
716	14.32	241.73	120.86	120.87	0.71	0.202	1.43	0.141	0.99	1.00	0.190	No
717	14.34	242.07	121.06	121.02	0.71	0.202	1.43	0.141	0.98	1.00	0.189	No
718	14.36	242.42	121.25	121.16	0.71	0.202	1.43	0.141	0.98	1.00	0.189	No
719	14.38	242.76	121.45	121.31	0.70	0.202	1.43	0.141	0.98	1.00	0.189	No
720	14.40	243.10	121.64	121.46	0.70	0.202	1.43	0.141	0.99	1.00	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	243.44	121.84	121.60	0.70	0.202	1.43	0.141	0.99	1.00	0.191	No
722	14.44	243.78	122.04	121.75	0.70	0.201	1.43	0.141	0.99	1.00	0.190	No
723	14.46	244.12	122.23	121.89	0.70	0.201	1.43	0.141	0.98	1.00	0.189	No
724	14.48	244.47	122.43	122.04	0.70	0.201	1.43	0.141	0.98	1.00	0.188	No
725	14.50	244.82	122.63	122.20	0.70	0.201	1.43	0.141	0.98	1.00	0.187	No
726	14.52	245.17	122.82	122.35	0.70	0.201	1.43	0.141	0.98	1.00	0.187	No
727	14.54	245.53	123.02	122.51	0.70	0.201	1.43	0.141	0.98	1.00	0.187	No
728	14.56	245.88	123.21	122.67	0.70	0.201	1.43	0.141	0.98	1.00	0.187	No
729	14.58	246.23	123.41	122.82	0.70	0.201	1.43	0.141	0.98	1.00	0.187	No
730	14.60	246.58	123.61	122.98	0.70	0.201	1.43	0.140	0.98	1.00	0.188	No
731	14.62	246.93	123.80	123.13	0.70	0.201	1.43	0.140	0.98	1.00	0.189	No
732	14.64	247.28	124.00	123.28	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
733	14.66	247.62	124.19	123.42	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
734	14.68	247.96	124.39	123.57	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
735	14.70	248.30	124.59	123.72	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
736	14.72	248.65	124.78	123.87	0.70	0.200	1.43	0.140	0.98	1.00	0.189	No
737	14.74	248.99	124.98	124.01	0.70	0.200	1.43	0.140	0.98	1.00	0.189	No
738	14.76	249.33	125.18	124.16	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
739	14.78	249.67	125.37	124.30	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
740	14.80	250.01	125.57	124.44	0.70	0.200	1.43	0.140	0.98	1.00	0.190	No
741	14.82	250.35	125.76	124.58	0.69	0.200	1.43	0.140	0.98	1.00	0.189	No
742	14.85	250.85	126.06	124.79	0.69	0.200	1.43	0.140	0.98	1.00	0.189	No
743	14.86	251.02	126.16	124.86	0.69	0.200	1.43	0.140	0.98	1.00	0.189	No
744	14.88	251.35	126.35	125.00	0.69	0.199	1.43	0.140	0.98	1.00	0.189	No
745	14.90	251.69	126.55	125.14	0.69	0.199	1.43	0.140	0.98	1.00	0.189	No
746	14.92	252.02	126.75	125.27	0.69	0.199	1.43	0.139	0.98	1.00	0.189	No
747	14.94	252.35	126.94	125.41	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
748	14.96	252.69	127.14	125.55	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
749	14.98	253.03	127.33	125.69	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
750	15.00	253.37	127.53	125.84	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
751	15.03	253.88	127.82	126.06	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
752	15.04	254.06	127.92	126.13	0.69	0.199	1.43	0.139	0.98	1.00	0.187	No
753	15.06	254.40	128.12	126.29	0.69	0.199	1.43	0.139	0.98	1.00	0.187	No
754	15.08	254.76	128.31	126.44	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
755	15.10	255.11	128.51	126.59	0.69	0.198	1.43	0.139	0.98	1.00	0.188	No
756	15.12	255.46	128.71	126.75	0.69	0.198	1.43	0.139	0.98	1.00	0.188	No
757	15.14	255.80	128.90	126.90	0.69	0.198	1.43	0.139	0.98	1.00	0.188	No
758	15.16	256.15	129.10	127.05	0.69	0.198	1.43	0.139	0.98	1.00	0.188	No
759	15.18	256.49	129.30	127.20	0.69	0.198	1.43	0.139	0.98	1.00	0.188	No
760	15.20	256.84	129.49	127.34	0.69	0.198	1.43	0.139	0.98	1.00	0.188	No
761	15.23	257.34	129.79	127.56	0.69	0.198	1.43	0.138	0.98	1.00	0.188	No
762	15.24	257.51	129.88	127.63	0.69	0.198	1.43	0.138	0.98	1.00	0.188	No
763	15.26	257.85	130.08	127.77	0.69	0.198	1.43	0.138	0.98	1.00	0.188	No
764	15.28	258.18	130.28	127.90	0.68	0.198	1.43	0.138	0.98	1.00	0.188	No
765	15.30	258.51	130.47	128.04	0.68	0.198	1.43	0.138	0.98	1.00	0.188	No
766	15.32	258.84	130.67	128.17	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
767	15.34	259.17	130.87	128.30	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
768	15.36	259.50	131.06	128.44	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	259.83	131.26	128.58	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
770	15.40	260.16	131.45	128.71	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
771	15.42	260.50	131.65	128.85	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
772	15.44	260.83	131.85	128.98	0.68	0.197	1.43	0.138	0.98	1.00	0.187	No
773	15.46	261.16	132.04	129.11	0.68	0.197	1.43	0.138	0.98	1.00	0.187	No
774	15.48	261.49	132.24	129.25	0.68	0.197	1.43	0.138	0.98	1.00	0.187	No
775	15.50	261.82	132.44	129.38	0.68	0.197	1.43	0.138	0.98	1.00	0.187	No
776	15.52	262.15	132.63	129.52	0.68	0.197	1.43	0.138	0.98	1.00	0.187	No
777	15.54	262.48	132.83	129.65	0.68	0.197	1.43	0.138	0.98	1.00	0.186	No
778	15.56	262.82	133.02	129.80	0.68	0.196	1.43	0.138	0.98	1.00	0.186	No
779	15.58	263.16	133.22	129.94	0.68	0.196	1.43	0.137	0.98	1.00	0.186	No
780	15.60	263.50	133.42	130.09	0.68	0.196	1.43	0.137	0.98	1.00	0.186	No
781	15.62	263.85	133.61	130.24	0.68	0.196	1.43	0.137	0.98	1.00	0.185	No
782	15.64	264.19	133.81	130.39	0.68	0.196	1.43	0.137	0.98	1.00	0.186	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.46	99.20	2.95	0.59	1.70	6.95	0.00	6.95	4.000	No	Yes	2.00
2	0.04	0.58	89.80	2.83	0.59	1.70	9.29	0.00	9.29	4.000	No	Yes	2.00
3	0.06	0.59	90.21	2.84	0.58	1.70	10.43	0.00	10.43	4.000	No	Yes	2.00
4	0.08	0.57	96.74	2.92	0.58	1.70	10.05	0.00	10.05	4.000	No	Yes	2.00
5	0.10	0.50	100.00	3.05	0.59	1.70	7.86	0.00	7.86	4.000	No	Yes	2.00
6	0.13	0.44	100.00	3.17	0.59	1.70	7.29	0.00	7.29	4.000	No	Yes	2.00
7	0.14	0.41	100.00	3.23	0.60	1.70	6.72	0.00	6.72	4.000	No	Yes	2.00
8	0.16	0.38	100.00	3.29	0.60	1.70	6.46	0.00	6.46	4.000	No	Yes	2.00
9	0.18	0.36	100.00	3.36	0.60	1.70	6.08	0.00	6.08	4.000	No	Yes	2.00
10	0.20	0.34	100.00	3.42	0.60	1.70	5.44	0.00	5.44	4.000	No	Yes	2.00
11	0.22	0.31	100.00	3.50	0.60	1.70	5.33	0.00	5.33	4.000	No	Yes	2.00
12	0.24	0.28	100.00	3.57	0.60	1.70	4.61	0.00	4.61	4.000	No	Yes	2.00
13	0.26	0.25	100.00	3.63	0.61	1.70	4.09	0.00	4.09	4.000	No	Yes	2.00
14	0.28	0.23	100.00	3.67	0.61	1.70	3.98	0.00	3.98	4.000	No	Yes	2.00
15	0.30	0.21	100.00	3.72	0.61	1.70	3.45	0.00	3.45	4.000	No	Yes	2.00
16	0.32	0.18	100.00	3.78	0.61	1.70	2.97	0.00	2.97	4.000	No	Yes	2.00
17	0.34	0.17	100.00	3.82	0.61	1.70	2.76	0.00	2.76	4.000	No	Yes	2.00
18	0.36	0.16	100.00	3.82	0.61	1.70	2.58	0.00	2.58	4.000	No	Yes	2.00
19	0.38	0.16	100.00	3.80	0.61	1.70	2.63	0.00	2.63	4.000	No	Yes	2.00
20	0.40	0.16	100.00	3.77	0.61	1.70	2.76	0.00	2.76	4.000	No	Yes	2.00
21	0.42	0.18	100.00	3.71	0.61	1.70	2.77	0.00	2.77	4.000	No	Yes	2.00
22	0.44	0.19	100.00	3.66	0.61	1.70	3.29	0.00	3.29	4.000	No	Yes	2.00
23	0.46	0.25	100.00	3.48	0.61	1.70	3.54	0.00	3.54	4.000	No	Yes	2.00
24	0.48	0.37	100.00	3.26	0.60	1.70	5.90	0.00	5.90	4.000	No	Yes	2.00
25	0.50	0.52	100.00	3.06	0.59	1.70	9.10	0.00	9.10	4.000	No	Yes	2.00
26	0.52	0.65	98.61	2.95	0.58	1.70	11.20	0.00	11.20	4.000	No	Yes	2.00
27	0.54	0.73	96.96	2.92	0.57	1.70	12.36	0.00	12.36	4.000	No	Yes	2.00
28	0.56	0.77	100.00	2.96	0.57	1.70	13.07	0.00	13.07	4.000	No	Yes	2.00
29	0.58	0.81	100.00	3.02	0.57	1.70	13.40	0.00	13.40	4.000	No	Yes	2.00
30	0.60	0.84	100.00	3.06	0.57	1.70	14.22	0.00	14.22	4.000	No	Yes	2.00
31	0.62	0.89	100.00	3.08	0.56	1.70	14.73	0.00	14.73	4.000	No	Yes	2.00
32	0.64	0.93	100.00	3.08	0.56	1.70	15.67	0.00	15.67	4.000	No	Yes	2.00
33	0.66	0.97	100.00	3.08	0.56	1.70	16.37	0.00	16.37	4.000	No	Yes	2.00
34	0.68	1.00	100.00	3.08	0.56	1.70	16.84	0.00	16.84	4.000	No	Yes	2.00
35	0.70	1.03	100.00	3.07	0.55	1.70	17.38	0.00	17.38	4.000	No	Yes	2.00
36	0.72	1.07	100.00	3.06	0.55	1.70	17.85	0.00	17.85	4.000	No	Yes	2.00
37	0.74	1.11	100.00	3.04	0.55	1.70	18.65	0.00	18.65	4.000	No	Yes	2.00
38	0.76	1.15	100.00	3.03	0.55	1.70	19.31	0.00	19.31	4.000	No	Yes	2.00
39	0.78	1.17	100.00	3.03	0.55	1.70	19.69	0.00	19.69	4.000	No	Yes	2.00
40	0.80	1.18	100.00	3.03	0.55	1.70	19.69	0.00	19.69	4.000	No	Yes	2.00
41	0.82	1.17	100.00	3.04	0.55	1.70	19.88	0.00	19.88	4.000	No	Yes	2.00
42	0.84	1.16	100.00	3.05	0.55	1.70	19.43	0.00	19.43	4.000	No	Yes	2.00
43	0.86	1.14	100.00	3.07	0.55	1.70	19.16	0.00	19.16	4.000	No	Yes	2.00
44	0.88	1.12	100.00	3.08	0.55	1.70	18.89	0.00	18.89	4.000	No	Yes	2.00
45	0.90	1.11	100.00	3.09	0.55	1.70	18.32	0.00	18.32	4.000	No	Yes	2.00
46	0.92	1.12	100.00	3.08	0.55	1.70	18.69	0.00	18.69	4.000	No	Yes	2.00
47	0.94	1.15	100.00	3.06	0.55	1.70	19.22	0.00	19.22	4.000	No	Yes	2.00
48	0.96	1.18	100.00	3.04	0.55	1.70	19.74	0.00	19.74	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	1.20	100.00	3.03	0.55	1.70	20.19	0.00	20.19	4.000	No	Yes	2.00
50	1.00	1.23	100.00	3.02	0.54	1.70	20.48	0.00	20.48	4.000	No	Yes	2.00
51	1.02	1.25	100.00	3.01	0.54	1.70	21.08	0.00	21.08	4.000	No	Yes	2.00
52	1.04	1.25	100.00	3.01	0.54	1.70	20.88	0.00	20.88	4.000	No	Yes	2.00
53	1.06	1.24	100.00	3.02	0.54	1.70	20.94	0.00	20.94	4.000	No	Yes	2.00
54	1.08	1.20	100.00	3.05	0.54	1.70	20.37	0.00	20.37	4.000	No	Yes	2.00
55	1.10	1.14	100.00	3.09	0.55	1.70	18.99	0.00	18.99	4.000	No	Yes	2.00
56	1.12	1.08	100.00	3.12	0.55	1.70	17.72	0.00	17.72	4.000	No	Yes	2.00
57	1.14	1.02	100.00	3.16	0.56	1.70	17.18	0.00	17.18	4.000	No	Yes	2.00
58	1.16	0.98	100.00	3.17	0.56	1.70	16.14	0.00	16.14	4.000	No	Yes	2.00
59	1.18	0.95	100.00	3.18	0.56	1.70	15.63	0.00	15.63	4.000	No	Yes	2.00
60	1.20	0.94	100.00	3.17	0.56	1.70	15.57	0.00	15.57	4.000	No	Yes	2.00
61	1.22	0.95	100.00	3.15	0.56	1.70	15.85	0.00	15.85	4.000	No	Yes	2.00
62	1.24	0.96	100.00	3.13	0.56	1.70	15.87	0.00	15.87	4.000	No	Yes	2.00
63	1.27	1.01	100.00	3.09	0.56	1.70	16.30	0.00	16.30	4.000	No	Yes	2.00
64	1.28	1.08	100.00	3.03	0.55	1.70	17.87	0.00	17.87	4.000	No	Yes	2.00
65	1.30	1.18	100.00	2.99	0.55	1.70	19.60	0.00	19.60	4.000	No	Yes	2.00
66	1.32	1.27	98.88	2.95	0.54	1.70	20.90	0.00	20.90	4.000	No	Yes	2.00
67	1.34	1.35	96.75	2.92	0.54	1.70	22.32	0.00	22.32	4.000	No	Yes	2.00
68	1.36	1.43	94.78	2.90	0.53	1.70	23.74	0.00	23.74	4.000	No	Yes	2.00
69	1.38	1.48	93.48	2.88	0.53	1.70	24.71	0.00	24.71	4.000	No	Yes	2.00
70	1.40	1.52	92.78	2.87	0.53	1.70	25.22	0.00	25.22	4.000	No	Yes	2.00
71	1.42	1.54	93.02	2.88	0.53	1.70	25.88	0.00	25.88	4.000	No	Yes	2.00
72	1.44	1.53	94.30	2.89	0.53	1.70	25.68	0.00	25.68	4.000	No	Yes	2.00
73	1.46	1.48	97.13	2.93	0.53	1.70	24.83	0.00	24.83	4.000	No	Yes	2.00
74	1.48	1.41	100.00	2.97	0.53	1.70	23.41	0.00	23.41	4.000	No	Yes	2.00
75	1.50	1.34	100.00	3.02	0.54	1.70	22.22	0.00	22.22	4.000	No	Yes	2.00
76	1.52	1.29	100.00	3.05	0.54	1.70	21.14	0.00	21.14	4.000	No	Yes	2.00
77	1.54	1.25	100.00	3.07	0.54	1.70	20.70	0.00	20.70	4.000	No	Yes	2.00
78	1.56	1.24	100.00	3.07	0.54	1.70	20.34	0.00	20.34	4.000	No	Yes	2.00
79	1.58	1.23	100.00	3.07	0.54	1.70	20.39	0.00	20.39	4.000	No	Yes	2.00
80	1.60	1.23	100.00	3.05	0.55	1.70	20.21	0.00	20.21	4.000	No	Yes	2.00
81	1.62	1.22	100.00	3.03	0.55	1.70	20.12	0.00	20.12	4.000	No	Yes	2.00
82	1.64	1.22	100.00	3.01	0.55	1.70	20.05	0.00	20.05	4.000	No	Yes	2.00
83	1.66	1.22	100.00	2.99	0.54	1.70	20.41	0.00	20.41	4.000	No	Yes	2.00
84	1.68	1.22	100.00	2.99	0.55	1.70	20.09	0.00	20.09	4.000	No	Yes	2.00
85	1.70	1.19	100.00	3.00	0.55	1.70	19.96	0.00	19.96	4.000	No	Yes	2.00
86	1.72	1.17	100.00	3.02	0.55	1.70	19.14	0.00	19.14	4.000	No	Yes	2.00
87	1.74	1.16	100.00	3.03	0.55	1.70	19.16	0.00	19.16	4.000	No	Yes	2.00
88	1.76	1.15	100.00	3.04	0.55	1.70	19.07	0.00	19.07	4.000	No	Yes	2.00
89	1.78	1.14	100.00	3.05	0.55	1.70	18.90	0.00	18.90	4.000	No	Yes	2.00
90	1.80	1.13	100.00	3.06	0.55	1.70	18.58	0.00	18.58	4.000	No	Yes	2.00
91	1.82	1.12	100.00	3.06	0.55	1.70	18.49	0.00	18.49	4.000	No	Yes	2.00
92	1.84	1.12	100.00	3.06	0.55	1.70	18.44	0.00	18.44	4.000	No	Yes	2.00
93	1.86	1.13	100.00	3.05	0.55	1.70	18.39	0.00	18.39	4.000	No	Yes	2.00
94	1.88	1.14	100.00	3.04	0.55	1.70	19.18	0.00	19.18	4.000	No	Yes	2.00
95	1.90	1.15	100.00	3.03	0.55	1.70	19.03	0.00	19.03	4.000	No	Yes	2.00
96	1.92	1.14	100.00	3.03	0.55	1.70	18.80	0.00	18.80	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	1.13	100.00	3.04	0.55	1.70	18.61	0.00	18.61	4.000	No	Yes	2.00
98	1.96	1.11	100.00	3.04	0.55	1.70	18.38	0.00	18.38	4.000	No	Yes	2.00
99	1.98	1.10	100.00	3.04	0.55	1.70	17.88	0.00	17.88	4.000	No	Yes	2.00
100	2.00	1.09	100.00	3.05	0.55	1.70	18.29	0.00	18.29	4.000	No	Yes	2.00
101	2.02	1.10	100.00	3.04	0.55	1.70	18.09	0.00	18.09	4.000	No	Yes	2.00
102	2.04	1.11	100.00	3.04	0.55	1.70	18.36	0.00	18.36	4.000	No	Yes	2.00
103	2.06	1.13	100.00	3.03	0.55	1.70	18.43	0.00	18.43	4.000	No	Yes	2.00
104	2.08	1.14	100.00	3.02	0.55	1.70	19.14	0.00	19.14	4.000	No	Yes	2.00
105	2.10	1.16	100.00	3.01	0.55	1.70	19.21	0.00	19.21	4.000	No	Yes	2.00
106	2.12	1.15	100.00	3.02	0.55	1.70	19.51	0.00	19.51	4.000	No	Yes	2.00
107	2.14	1.13	100.00	3.03	0.55	1.70	18.81	0.00	18.81	4.000	No	Yes	2.00
108	2.16	1.10	100.00	3.05	0.55	1.70	18.16	0.00	18.16	4.000	No	Yes	2.00
109	2.19	1.08	100.00	3.06	0.55	1.70	18.19	0.00	18.19	4.000	No	Yes	2.00
110	2.20	1.08	100.00	3.07	0.55	1.70	17.65	0.00	17.65	4.000	No	Yes	2.00
111	2.22	1.07	100.00	3.07	0.55	1.69	17.78	0.00	17.78	4.000	No	Yes	2.00
112	2.24	1.07	100.00	3.08	0.55	1.69	17.79	0.00	17.79	4.000	No	Yes	2.00
113	2.26	1.07	100.00	3.08	0.56	1.68	17.19	0.00	17.19	4.000	No	Yes	2.00
114	2.28	1.07	100.00	3.08	0.55	1.67	17.39	0.00	17.39	4.000	No	Yes	2.00
115	2.30	1.09	100.00	3.06	0.55	1.66	17.75	0.00	17.75	4.000	No	Yes	2.00
116	2.32	1.10	100.00	3.06	0.55	1.65	17.87	0.00	17.87	4.000	No	Yes	2.00
117	2.34	1.10	100.00	3.06	0.55	1.65	17.67	0.00	17.67	4.000	No	Yes	2.00
118	2.36	1.09	100.00	3.07	0.55	1.64	17.48	0.00	17.48	4.000	No	Yes	2.00
119	2.38	1.09	100.00	3.07	0.55	1.63	17.36	0.00	17.36	4.000	No	Yes	2.00
120	2.40	1.08	100.00	3.08	0.56	1.62	17.27	0.00	17.27	4.000	No	Yes	2.00
121	2.42	1.08	100.00	3.09	0.56	1.62	16.67	0.00	16.67	4.000	No	Yes	2.00
122	2.44	1.09	100.00	3.08	0.56	1.61	16.86	0.00	16.86	4.000	No	Yes	2.00
123	2.46	1.12	100.00	3.07	0.55	1.60	17.42	0.00	17.42	4.000	No	Yes	2.00
124	2.48	1.15	100.00	3.04	0.55	1.59	17.57	0.00	17.57	4.000	No	Yes	2.00
125	2.50	1.17	100.00	3.03	0.55	1.58	18.29	0.00	18.29	4.000	No	Yes	2.00
126	2.52	1.17	100.00	3.02	0.55	1.58	18.31	0.00	18.31	4.000	No	Yes	2.00
127	2.54	1.16	100.00	3.01	0.55	1.58	17.73	0.00	17.73	4.000	No	Yes	2.00
128	2.56	1.15	100.00	3.01	0.55	1.57	17.89	0.00	17.89	4.000	No	Yes	2.00
129	2.58	1.12	100.00	3.02	0.55	1.57	17.41	0.00	17.41	4.000	No	Yes	2.00
130	2.60	1.08	100.00	3.05	0.56	1.57	16.57	0.00	16.57	4.000	No	Yes	2.00
131	2.62	1.02	100.00	3.09	0.56	1.57	15.70	0.00	15.70	4.000	No	Yes	2.00
132	2.64	0.95	100.00	3.13	0.56	1.58	14.69	0.00	14.69	4.000	No	Yes	2.00
133	2.66	0.92	100.00	3.15	0.57	1.58	13.51	0.00	13.51	4.000	No	Yes	2.00
134	2.68	0.92	100.00	3.15	0.57	1.57	13.75	0.00	13.75	4.000	No	Yes	2.00
135	2.70	0.98	100.00	3.09	0.57	1.57	14.29	0.00	14.29	4.000	No	Yes	2.00
136	2.72	1.04	100.00	3.04	0.56	1.56	16.32	0.00	16.32	4.000	No	Yes	2.00
137	2.74	1.07	100.00	3.00	0.56	1.55	16.28	0.00	16.28	4.000	No	Yes	2.00
138	2.76	1.04	100.00	2.99	0.56	1.55	15.89	0.00	15.89	4.000	No	Yes	2.00
139	2.78	1.01	100.00	3.00	0.56	1.55	15.16	0.00	15.16	4.000	No	Yes	2.00
140	2.80	0.98	100.00	2.99	0.56	1.55	14.93	0.00	14.93	4.000	No	Yes	2.00
141	2.82	0.97	100.00	2.99	0.56	1.55	14.84	0.00	14.84	4.000	No	Yes	2.00
142	2.84	0.95	100.00	2.99	0.57	1.55	14.32	0.00	14.32	4.000	No	Yes	2.00
143	2.86	0.94	100.00	3.01	0.57	1.55	14.18	0.00	14.18	4.000	No	Yes	2.00
144	2.88	0.93	100.00	3.02	0.57	1.54	14.02	0.00	14.02	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.92	100.00	3.03	0.57	1.54	13.77	0.00	13.77	4.000	No	Yes	2.00
146	2.92	0.90	100.00	3.05	0.57	1.54	13.78	0.00	13.78	4.000	No	Yes	2.00
147	2.94	0.88	100.00	3.07	0.57	1.54	13.00	0.00	13.00	4.000	No	Yes	2.00
148	2.96	0.85	100.00	3.09	0.57	1.54	12.68	0.00	12.68	4.000	No	Yes	2.00
149	2.98	0.83	100.00	3.10	0.57	1.54	12.46	0.00	12.46	4.000	No	Yes	2.00
150	3.00	0.80	100.00	3.11	0.57	1.54	11.95	0.00	11.95	4.000	No	Yes	2.00
151	3.02	0.76	100.00	3.15	0.58	1.53	11.56	0.00	11.56	4.000	No	Yes	2.00
152	3.04	0.72	100.00	3.18	0.58	1.54	10.55	0.00	10.55	4.000	No	Yes	2.00
153	3.06	0.69	100.00	3.21	0.58	1.53	10.14	0.00	10.14	4.000	No	Yes	2.00
154	3.08	0.70	100.00	3.21	0.58	1.53	10.15	0.00	10.15	4.000	No	Yes	2.00
155	3.10	0.72	100.00	3.18	0.58	1.53	10.63	0.00	10.63	4.000	No	Yes	2.00
156	3.12	0.77	100.00	3.14	0.58	1.52	10.97	0.00	10.97	4.000	No	Yes	2.00
157	3.14	0.81	100.00	3.08	0.58	1.52	11.87	0.00	11.87	4.000	No	Yes	2.00
158	3.16	0.85	100.00	3.03	0.57	1.51	12.53	0.00	12.53	4.000	No	Yes	2.00
159	3.18	0.89	100.00	2.98	0.57	1.51	12.61	0.00	12.61	4.000	No	Yes	2.00
160	3.20	0.92	98.03	2.94	0.57	1.50	13.37	0.00	13.37	4.000	No	Yes	2.00
161	3.22	0.96	94.62	2.90	0.57	1.50	13.81	0.00	13.81	4.000	No	Yes	2.00
162	3.24	1.00	92.81	2.87	0.57	1.50	14.37	0.00	14.37	4.000	No	Yes	2.00
163	3.26	1.04	91.82	2.86	0.57	1.49	14.93	0.00	14.93	4.000	No	Yes	2.00
164	3.28	1.08	92.38	2.87	0.56	1.49	15.60	0.00	15.60	4.000	No	Yes	2.00
165	3.30	1.12	92.72	2.87	0.56	1.48	16.05	0.00	16.05	4.000	No	Yes	2.00
166	3.32	1.17	93.16	2.88	0.56	1.48	16.63	0.00	16.63	4.000	No	Yes	2.00
167	3.34	1.20	93.52	2.88	0.56	1.47	17.23	0.00	17.23	4.000	No	Yes	2.00
168	3.36	1.23	93.34	2.88	0.56	1.47	17.21	0.00	17.21	4.000	No	Yes	2.00
169	3.38	1.25	92.73	2.87	0.56	1.47	17.74	0.00	17.74	4.000	No	Yes	2.00
170	3.40	1.28	91.22	2.85	0.55	1.46	18.16	0.00	18.16	4.000	No	Yes	2.00
171	3.42	1.31	90.25	2.84	0.55	1.46	18.47	0.00	18.47	4.000	No	Yes	2.00
172	3.44	1.33	89.82	2.84	0.55	1.46	18.75	0.00	18.75	4.000	No	Yes	2.00
173	3.46	1.34	90.69	2.85	0.55	1.45	19.00	0.00	19.00	4.000	No	Yes	2.00
174	3.48	1.32	92.44	2.87	0.55	1.45	18.84	0.00	18.84	4.000	No	Yes	2.00
175	3.50	1.30	95.17	2.90	0.55	1.45	18.31	0.00	18.31	4.000	No	Yes	2.00
176	3.52	1.27	97.87	2.94	0.55	1.45	17.87	0.00	17.87	4.000	No	Yes	2.00
177	3.54	1.26	99.44	2.96	0.55	1.44	17.43	0.00	17.43	4.000	No	Yes	2.00
178	3.56	1.28	99.27	2.95	0.55	1.44	17.86	0.00	17.86	4.000	No	Yes	2.00
179	3.58	1.32	97.62	2.93	0.55	1.44	18.51	0.00	18.51	4.000	No	Yes	2.00
180	3.60	1.36	96.46	2.92	0.55	1.43	19.31	0.00	19.31	4.000	No	Yes	2.00
181	3.62	1.38	95.56	2.91	0.55	1.43	19.12	0.00	19.12	4.000	No	Yes	2.00
182	3.64	1.41	94.47	2.89	0.55	1.43	19.46	0.00	19.46	4.000	No	Yes	2.00
183	3.66	1.44	92.70	2.87	0.55	1.42	20.18	0.00	20.18	4.000	No	Yes	2.00
184	3.68	1.44	92.30	2.87	0.55	1.42	20.36	0.00	20.36	4.000	No	Yes	2.00
185	3.70	1.38	93.83	2.89	0.55	1.42	19.05	0.00	19.05	4.000	No	Yes	2.00
186	3.72	1.30	96.62	2.92	0.55	1.42	17.95	0.00	17.95	4.000	No	Yes	2.00
187	3.74	1.19	100.00	2.98	0.56	1.42	17.09	0.00	17.09	4.000	No	Yes	2.00
188	3.76	1.06	100.00	3.04	0.57	1.43	14.18	0.00	14.18	4.000	No	Yes	2.00
189	3.78	0.93	100.00	3.11	0.57	1.43	12.67	0.00	12.67	4.000	No	Yes	2.00
190	3.80	0.84	100.00	3.15	0.58	1.43	11.72	0.00	11.72	4.000	No	Yes	2.00
191	3.82	0.77	100.00	3.19	0.58	1.43	10.62	0.00	10.62	4.000	No	Yes	2.00
192	3.84	0.75	100.00	3.17	0.58	1.43	9.73	0.00	9.73	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	0.73	100.00	3.13	0.58	1.43	10.58	0.00	10.58	4.000	No	Yes	2.00
194	3.88	0.73	100.00	3.07	0.58	1.43	9.95	0.00	9.95	4.000	No	Yes	2.00
195	3.90	0.71	100.00	3.07	0.58	1.43	9.53	0.00	9.53	4.000	No	Yes	2.00
196	3.92	0.71	100.00	3.03	0.58	1.43	9.58	0.00	9.58	4.000	No	Yes	2.00
197	3.94	0.74	100.00	2.98	0.58	1.42	10.10	0.00	10.10	4.000	No	Yes	2.00
198	3.96	0.79	95.58	2.91	0.58	1.42	10.68	0.00	10.68	4.000	No	Yes	2.00
199	3.98	0.84	91.01	2.85	0.58	1.42	11.50	0.00	11.50	4.000	No	Yes	2.00
200	4.00	0.87	87.76	2.81	0.58	1.41	11.96	0.00	11.96	4.000	No	Yes	2.00
201	4.02	0.86	86.74	2.80	0.58	1.41	11.86	0.00	11.86	4.000	No	Yes	2.00
202	4.04	0.84	86.62	2.80	0.58	1.41	11.23	0.00	11.23	4.000	No	Yes	2.00
203	4.06	0.79	87.84	2.81	0.58	1.41	10.82	0.00	10.82	4.000	No	Yes	2.00
204	4.08	0.77	88.84	2.82	0.58	1.41	10.14	0.00	10.14	4.000	No	Yes	2.00
205	4.10	0.77	88.73	2.82	0.59	1.41	10.01	0.00	10.01	4.000	No	Yes	2.00
206	4.12	0.81	86.33	2.79	0.58	1.41	10.80	0.00	10.80	4.000	No	Yes	2.00
207	4.14	0.85	84.78	2.77	0.58	1.40	11.65	0.00	11.65	4.000	No	Yes	2.00
208	4.16	0.83	87.46	2.81	0.58	1.40	11.57	0.00	11.57	4.000	No	Yes	2.00
209	4.18	0.78	92.80	2.87	0.58	1.40	10.30	0.00	10.30	4.000	No	Yes	2.00
210	4.20	0.74	96.77	2.92	0.59	1.40	9.47	0.00	9.47	4.000	No	Yes	2.00
211	4.22	0.74	95.35	2.90	0.58	1.40	9.65	0.00	9.65	4.000	No	Yes	2.00
212	4.25	0.80	90.65	2.85	0.58	1.39	10.61	0.00	10.61	4.000	No	Yes	2.00
213	4.26	0.85	88.00	2.81	0.58	1.39	11.55	0.00	11.55	4.000	No	Yes	2.00
214	4.28	0.86	88.54	2.82	0.58	1.39	11.66	0.00	11.66	4.000	No	Yes	2.00
215	4.30	0.85	89.89	2.84	0.58	1.39	11.05	0.00	11.05	4.000	No	Yes	2.00
216	4.32	0.82	90.67	2.85	0.58	1.39	11.03	0.00	11.03	4.000	No	Yes	2.00
217	4.34	0.81	90.72	2.85	0.58	1.39	10.69	0.00	10.69	4.000	No	Yes	2.00
218	4.36	0.80	91.08	2.85	0.58	1.39	10.35	0.00	10.35	4.000	No	Yes	2.00
219	4.38	0.80	90.78	2.85	0.58	1.38	10.37	0.00	10.37	4.000	No	Yes	2.00
220	4.40	0.79	90.47	2.84	0.58	1.38	10.55	0.00	10.55	4.000	No	Yes	2.00
221	4.42	0.78	89.96	2.84	0.59	1.38	9.94	0.00	9.94	4.000	No	Yes	2.00
222	4.44	0.78	89.34	2.83	0.59	1.38	9.78	0.00	9.78	4.000	No	Yes	2.00
223	4.46	0.82	87.16	2.80	0.58	1.38	10.47	0.00	10.47	4.000	No	Yes	2.00
224	4.48	0.89	84.94	2.77	0.58	1.37	11.60	0.00	11.60	4.000	No	Yes	2.00
225	4.50	0.94	83.40	2.75	0.58	1.37	12.31	0.00	12.31	4.000	No	Yes	2.00
226	4.52	0.96	84.25	2.77	0.58	1.37	12.56	0.00	12.56	4.000	No	Yes	2.00
227	4.55	0.96	86.13	2.79	0.58	1.36	12.27	0.00	12.27	4.000	No	Yes	2.00
228	4.56	0.94	89.18	2.83	0.58	1.36	12.38	0.00	12.38	4.000	No	Yes	2.00
229	4.58	0.92	91.94	2.86	0.58	1.36	11.77	0.00	11.77	4.000	No	Yes	2.00
230	4.60	0.91	93.96	2.89	0.58	1.36	11.49	0.00	11.49	4.000	No	Yes	2.00
231	4.62	0.92	93.79	2.88	0.58	1.36	11.66	0.00	11.66	4.000	No	Yes	2.00
232	4.64	0.93	93.36	2.88	0.58	1.35	12.29	0.00	12.29	4.000	No	Yes	2.00
233	4.66	0.94	93.69	2.88	0.58	1.35	11.96	0.00	11.96	4.000	No	Yes	2.00
234	4.68	0.95	93.51	2.88	0.58	1.35	11.71	0.00	11.71	4.000	No	Yes	2.00
235	4.70	0.98	91.37	2.85	0.57	1.35	12.67	0.00	12.67	4.000	No	Yes	2.00
236	4.72	1.05	87.86	2.81	0.57	1.35	13.30	0.00	13.30	4.000	No	Yes	2.00
237	4.74	1.07	86.26	2.79	0.57	1.34	14.07	0.00	14.07	4.000	No	Yes	2.00
238	4.76	1.03	87.78	2.81	0.57	1.34	13.53	0.00	13.53	4.000	No	Yes	2.00
239	4.78	0.98	90.25	2.84	0.58	1.34	11.76	0.00	11.76	4.000	No	Yes	2.00
240	4.80	0.94	92.02	2.86	0.58	1.34	11.81	0.00	11.81	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	0.98	89.96	2.84	0.58	1.34	11.83	0.00	11.83	4.000	No	Yes	2.00
242	4.84	1.03	89.44	2.83	0.57	1.34	13.18	0.00	13.18	4.000	No	Yes	2.00
243	4.86	1.07	90.17	2.84	0.57	1.33	13.74	0.00	13.74	4.000	No	Yes	2.00
244	4.88	1.06	92.84	2.87	0.57	1.33	13.34	0.00	13.34	4.000	No	Yes	2.00
245	4.90	1.02	95.89	2.91	0.57	1.33	13.06	0.00	13.06	4.000	No	Yes	2.00
246	4.92	0.96	99.39	2.95	0.57	1.33	11.94	0.00	11.94	4.000	No	Yes	2.00
247	4.94	0.88	100.00	3.01	0.58	1.33	11.14	0.00	11.14	4.000	No	Yes	2.00
248	4.97	0.82	100.00	3.08	0.58	1.33	10.28	0.00	10.28	4.000	No	Yes	2.00
249	4.98	0.76	100.00	3.14	0.58	1.33	9.32	0.00	9.32	4.000	No	Yes	2.00
250	5.01	0.70	100.00	3.19	0.59	1.33	8.83	0.00	8.83	4.000	No	Yes	2.00
251	5.02	0.66	100.00	3.23	0.59	1.33	8.16	0.00	8.16	4.000	No	Yes	2.00
252	5.04	0.63	100.00	3.25	0.59	1.33	7.77	0.00	7.77	4.000	No	Yes	2.00
253	5.06	0.62	100.00	3.24	0.59	1.33	7.58	0.00	7.58	4.000	No	Yes	2.00
254	5.08	0.64	100.00	3.19	0.59	1.33	7.83	0.00	7.83	4.000	No	Yes	2.00
255	5.10	0.68	100.00	3.11	0.59	1.32	8.34	0.00	8.34	4.000	No	Yes	2.00
256	5.12	0.78	100.00	2.98	0.59	1.32	9.00	0.00	9.00	4.000	No	Yes	2.00
257	5.14	0.93	90.83	2.85	0.58	1.31	11.64	0.00	11.64	4.000	No	Yes	2.00
258	5.16	1.04	84.18	2.76	0.57	1.31	14.00	0.00	14.00	4.000	No	Yes	2.00
259	5.19	1.03	85.68	2.78	0.57	1.31	13.35	0.00	13.35	4.000	No	Yes	2.00
260	5.20	0.90	94.11	2.89	0.58	1.31	11.45	0.00	11.45	4.000	No	Yes	2.00
261	5.22	0.77	100.00	3.01	0.59	1.31	9.20	0.00	9.20	4.000	No	Yes	2.00
262	5.24	0.70	100.00	3.08	0.59	1.31	8.33	0.00	8.33	4.000	No	Yes	2.00
263	5.26	0.71	100.00	3.07	0.59	1.31	8.69	0.00	8.69	4.000	No	Yes	2.00
264	5.28	0.75	100.00	3.04	0.59	1.31	9.11	0.00	9.11	4.000	No	Yes	2.00
265	5.30	0.80	100.00	2.98	0.58	1.30	9.67	0.00	9.67	4.000	No	Yes	2.00
266	5.32	0.89	94.12	2.89	0.58	1.30	10.53	0.00	10.53	4.000	No	Yes	2.00
267	5.34	1.02	85.43	2.78	0.58	1.30	12.48	0.00	12.48	4.000	No	Yes	2.00
268	5.36	1.15	79.43	2.71	0.57	1.29	14.45	0.00	14.45	4.000	No	Yes	2.00
269	5.38	1.22	78.99	2.70	0.57	1.29	15.47	0.00	15.47	4.000	No	Yes	2.00
270	5.40	1.20	84.45	2.77	0.57	1.29	15.14	0.00	15.14	4.000	No	Yes	2.00
271	5.42	1.12	92.73	2.87	0.57	1.29	14.04	0.00	14.04	4.000	No	Yes	2.00
272	5.44	1.02	100.00	2.99	0.57	1.29	12.54	0.00	12.54	4.000	No	Yes	2.00
273	5.46	0.92	100.00	3.09	0.58	1.29	11.32	0.00	11.32	4.000	No	Yes	2.00
274	5.48	0.83	100.00	3.19	0.58	1.29	10.32	0.00	10.32	4.000	No	Yes	2.00
275	5.50	0.74	100.00	3.29	0.59	1.29	9.21	0.00	9.21	4.000	No	Yes	2.00
276	5.52	0.66	100.00	3.38	0.59	1.29	8.07	0.00	8.07	4.000	No	Yes	2.00
277	5.54	0.60	100.00	3.45	0.59	1.29	7.29	0.00	7.29	4.000	No	Yes	2.00
278	5.56	0.56	100.00	3.47	0.59	1.29	6.86	0.00	6.86	4.000	No	Yes	2.00
279	5.58	0.54	100.00	3.46	0.60	1.29	6.59	0.00	6.59	4.000	No	Yes	2.00
280	5.60	0.54	100.00	3.42	0.60	1.29	6.58	0.00	6.58	4.000	No	Yes	2.00
281	5.62	0.55	100.00	3.35	0.59	1.28	6.83	0.00	6.83	4.000	No	Yes	2.00
282	5.64	0.57	100.00	3.28	0.59	1.28	6.93	0.00	6.93	4.000	No	Yes	2.00
283	5.66	0.58	100.00	3.21	0.59	1.28	7.01	0.00	7.01	4.000	No	Yes	2.00
284	5.68	0.59	100.00	3.14	0.59	1.28	7.11	0.00	7.11	4.000	No	Yes	2.00
285	5.70	0.61	100.00	3.09	0.59	1.28	7.47	0.00	7.47	4.000	No	Yes	2.00
286	5.72	0.63	100.00	3.07	0.59	1.27	7.66	0.00	7.66	4.000	No	Yes	2.00
287	5.74	0.66	100.00	3.06	0.59	1.27	7.90	0.00	7.90	4.000	No	Yes	2.00
288	5.76	0.68	100.00	3.06	0.59	1.27	8.31	0.00	8.31	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	0.71	100.00	3.04	0.59	1.27	8.42	0.00	8.42	4.000	No	Yes	2.00
290	5.80	0.72	100.00	3.03	0.59	1.27	8.85	0.00	8.85	4.000	No	Yes	2.00
291	5.82	0.75	100.00	3.01	0.59	1.26	8.88	0.00	8.88	4.000	No	Yes	2.00
292	5.85	0.76	100.00	3.02	0.58	1.26	9.43	0.00	9.43	4.000	No	Yes	2.00
293	5.86	0.76	100.00	3.03	0.59	1.26	8.87	0.00	8.87	4.000	No	Yes	2.00
294	5.88	0.77	100.00	3.05	0.59	1.26	9.00	0.00	9.00	4.000	No	Yes	2.00
295	5.90	0.81	100.00	3.02	0.58	1.26	9.63	0.00	9.63	4.000	No	Yes	2.00
296	5.92	0.84	100.00	3.01	0.58	1.25	10.36	0.00	10.36	4.000	No	Yes	2.00
297	5.94	0.87	100.00	3.00	0.58	1.25	10.38	0.00	10.38	4.000	No	Yes	2.00
298	5.96	0.89	100.00	3.00	0.58	1.25	10.70	0.00	10.70	4.000	No	Yes	2.00
299	5.98	0.92	100.00	3.01	0.58	1.25	11.09	0.00	11.09	4.000	No	Yes	2.00
300	6.00	0.94	100.00	3.02	0.58	1.25	11.44	0.00	11.44	4.000	No	Yes	2.00
301	6.02	0.97	100.00	3.03	0.58	1.24	11.78	0.00	11.78	4.000	No	Yes	2.00
302	6.04	1.01	100.00	3.03	0.57	1.24	12.20	0.00	12.20	4.000	No	Yes	2.00
303	6.06	1.04	100.00	3.05	0.57	1.24	12.75	0.00	12.75	4.000	No	Yes	2.00
304	6.08	1.06	100.00	3.06	0.57	1.24	12.82	0.00	12.82	4.000	No	Yes	2.00
305	6.10	1.05	100.00	3.09	0.57	1.24	12.83	0.00	12.83	4.000	No	Yes	2.00
306	6.12	1.02	100.00	3.13	0.57	1.24	12.51	0.00	12.51	4.000	No	Yes	2.00
307	6.14	0.99	100.00	3.16	0.58	1.23	11.79	0.00	11.79	4.000	No	Yes	2.00
308	6.16	0.96	100.00	3.20	0.58	1.23	11.80	0.00	11.80	4.000	No	Yes	2.00
309	6.18	0.95	100.00	3.22	0.58	1.23	11.38	0.00	11.38	4.000	No	Yes	2.00
310	6.20	0.93	100.00	3.24	0.58	1.23	11.36	0.00	11.36	4.000	No	Yes	2.00
311	6.22	0.92	100.00	3.25	0.58	1.23	11.12	0.00	11.12	4.000	No	Yes	2.00
312	6.25	0.90	100.00	3.25	0.58	1.23	10.88	0.00	10.88	4.000	No	Yes	2.00
313	6.26	0.88	100.00	3.27	0.58	1.23	10.74	0.00	10.74	4.000	No	Yes	2.00
314	6.28	0.86	100.00	3.28	0.58	1.23	10.26	0.00	10.26	4.000	No	Yes	2.00
315	6.30	0.84	100.00	3.29	0.58	1.22	10.19	0.00	10.19	4.000	No	Yes	2.00
316	6.32	0.81	100.00	3.30	0.58	1.22	9.88	0.00	9.88	4.000	No	Yes	2.00
317	6.34	0.77	100.00	3.33	0.59	1.22	9.30	0.00	9.30	4.000	No	Yes	2.00
318	6.36	0.72	100.00	3.36	0.59	1.22	8.63	0.00	8.63	4.000	No	Yes	2.00
319	6.38	0.68	100.00	3.39	0.59	1.22	8.19	0.00	8.19	4.000	No	Yes	2.00
320	6.40	0.65	100.00	3.41	0.59	1.22	7.85	0.00	7.85	4.000	No	Yes	2.00
321	6.42	0.64	100.00	3.40	0.59	1.22	7.54	0.00	7.54	4.000	No	Yes	2.00
322	6.44	0.64	100.00	3.37	0.59	1.22	7.64	0.00	7.64	4.000	No	Yes	2.00
323	6.46	0.66	100.00	3.32	0.59	1.22	7.94	0.00	7.94	4.000	No	Yes	2.00
324	6.48	0.69	100.00	3.26	0.59	1.21	8.17	0.00	8.17	4.000	No	Yes	2.00
325	6.50	0.70	100.00	3.22	0.59	1.21	8.51	0.00	8.51	4.000	No	Yes	2.00
326	6.52	0.70	100.00	3.21	0.59	1.21	8.52	0.00	8.52	4.000	No	Yes	2.00
327	6.54	0.68	100.00	3.23	0.59	1.21	7.92	0.00	7.92	4.000	No	Yes	2.00
328	6.56	0.65	100.00	3.27	0.59	1.21	7.65	0.00	7.65	4.000	No	Yes	2.00
329	6.58	0.63	100.00	3.29	0.59	1.21	7.45	0.00	7.45	4.000	No	Yes	2.00
330	6.60	0.62	100.00	3.30	0.59	1.21	7.37	0.00	7.37	4.000	No	Yes	2.00
331	6.62	0.62	100.00	3.31	0.59	1.21	7.28	0.00	7.28	4.000	No	Yes	2.00
332	6.64	0.63	100.00	3.30	0.59	1.20	7.46	0.00	7.46	4.000	No	Yes	2.00
333	6.66	0.64	100.00	3.29	0.59	1.20	7.56	0.00	7.56	4.000	No	Yes	2.00
334	6.68	0.66	100.00	3.27	0.59	1.20	7.69	0.00	7.69	4.000	No	Yes	2.00
335	6.70	0.65	100.00	3.26	0.59	1.20	7.84	0.00	7.84	4.000	No	Yes	2.00
336	6.72	0.64	100.00	3.25	0.59	1.20	7.41	0.00	7.41	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	0.62	100.00	3.26	0.59	1.20	7.25	0.00	7.25	4.000	No	Yes	2.00
338	6.76	0.60	100.00	3.27	0.59	1.20	6.93	0.00	6.93	4.000	No	Yes	2.00
339	6.78	0.57	100.00	3.28	0.60	1.20	6.61	0.00	6.61	4.000	No	Yes	2.00
340	6.80	0.56	100.00	3.25	0.60	1.20	6.24	0.00	6.24	4.000	No	Yes	2.00
341	6.82	0.56	100.00	3.21	0.60	1.19	6.44	0.00	6.44	4.000	No	Yes	2.00
342	6.84	0.56	100.00	3.18	0.60	1.19	6.33	0.00	6.33	4.000	No	Yes	2.00
343	6.86	0.54	100.00	3.22	0.60	1.19	6.24	0.00	6.24	4.000	No	Yes	2.00
344	6.88	0.52	100.00	3.27	0.60	1.19	5.77	0.00	5.77	4.000	No	Yes	2.00
345	6.90	0.50	100.00	3.31	0.60	1.19	5.50	0.00	5.50	4.000	No	Yes	2.00
346	6.93	0.49	100.00	3.32	0.60	1.19	5.41	0.00	5.41	4.000	No	Yes	2.00
347	6.94	0.50	100.00	3.31	0.60	1.19	5.52	0.00	5.52	4.000	No	Yes	2.00
348	6.96	0.52	100.00	3.27	0.60	1.19	5.60	0.00	5.60	4.000	No	Yes	2.00
349	6.98	0.53	100.00	3.23	0.60	1.19	5.93	0.00	5.93	4.000	No	Yes	2.00
350	7.00	0.55	100.00	3.19	0.60	1.19	5.98	0.00	5.98	4.000	No	Yes	2.00
351	7.03	0.56	100.00	3.17	0.60	1.18	6.13	0.00	6.13	4.000	No	Yes	2.00
352	7.04	0.58	100.00	3.13	0.60	1.18	6.21	0.00	6.21	4.000	No	Yes	2.00
353	7.06	0.60	100.00	3.09	0.60	1.18	6.60	0.00	6.60	4.000	No	Yes	2.00
354	7.08	0.61	100.00	3.06	0.59	1.18	6.83	0.00	6.83	4.000	No	Yes	2.00
355	7.10	0.65	100.00	3.03	0.60	1.18	6.80	0.00	6.80	4.000	No	Yes	2.00
356	7.12	0.69	100.00	2.99	0.59	1.18	7.76	0.00	7.76	4.000	No	Yes	2.00
357	7.14	0.74	98.89	2.95	0.59	1.18	8.15	0.00	8.15	4.000	No	Yes	2.00
358	7.16	0.76	98.66	2.95	0.59	1.17	8.58	0.00	8.58	4.000	No	Yes	2.00
359	7.18	0.77	99.25	2.95	0.59	1.17	8.42	0.00	8.42	4.000	No	Yes	2.00
360	7.20	0.76	100.00	2.98	0.59	1.17	8.60	0.00	8.60	4.000	No	Yes	2.00
361	7.22	0.76	100.00	3.00	0.59	1.17	8.28	0.00	8.28	4.000	No	Yes	2.00
362	7.24	0.76	100.00	3.00	0.59	1.17	8.18	0.00	8.18	4.000	No	Yes	2.00
363	7.26	0.81	99.16	2.95	0.59	1.17	8.69	0.00	8.69	4.000	No	Yes	2.00
364	7.28	0.86	95.60	2.91	0.58	1.17	9.76	0.00	9.76	4.000	No	Yes	2.00
365	7.30	0.90	93.52	2.88	0.58	1.17	9.89	0.00	9.89	4.000	No	Yes	2.00
366	7.32	0.90	94.84	2.90	0.58	1.16	9.98	0.00	9.98	4.000	No	Yes	2.00
367	7.34	0.89	97.85	2.94	0.58	1.16	9.77	0.00	9.77	4.000	No	Yes	2.00
368	7.36	0.88	100.00	2.97	0.59	1.16	9.30	0.00	9.30	4.000	No	Yes	2.00
369	7.38	0.88	100.00	2.98	0.58	1.16	9.58	0.00	9.58	4.000	No	Yes	2.00
370	7.40	0.90	100.00	2.98	0.58	1.16	9.90	0.00	9.90	4.000	No	Yes	2.00
371	7.42	0.91	100.00	2.99	0.58	1.16	9.89	0.00	9.89	4.000	No	Yes	2.00
372	7.44	0.91	100.00	3.01	0.58	1.16	9.96	0.00	9.96	4.000	No	Yes	2.00
373	7.46	0.89	100.00	3.04	0.58	1.16	9.70	0.00	9.70	4.000	No	Yes	2.00
374	7.48	0.88	100.00	3.08	0.58	1.15	9.44	0.00	9.44	4.000	No	Yes	2.00
375	7.50	0.87	100.00	3.10	0.58	1.15	9.38	0.00	9.38	4.000	No	Yes	2.00
376	7.52	0.88	100.00	3.11	0.58	1.15	9.47	0.00	9.47	4.000	No	Yes	2.00
377	7.54	0.88	100.00	3.12	0.58	1.15	9.64	0.00	9.64	4.000	No	Yes	2.00
378	7.56	0.86	100.00	3.14	0.58	1.15	9.40	0.00	9.40	4.000	No	Yes	2.00
379	7.58	0.83	100.00	3.17	0.59	1.15	8.96	0.00	8.96	4.000	No	Yes	2.00
380	7.60	0.78	100.00	3.22	0.59	1.15	8.52	0.00	8.52	4.000	No	Yes	2.00
381	7.62	0.73	100.00	3.26	0.59	1.15	7.85	0.00	7.85	4.000	No	Yes	2.00
382	7.64	0.67	100.00	3.31	0.59	1.15	7.24	0.00	7.24	4.000	No	Yes	2.00
383	7.66	0.63	100.00	3.36	0.60	1.15	6.70	0.00	6.70	4.000	No	Yes	2.00
384	7.68	0.59	100.00	3.41	0.60	1.15	6.38	0.00	6.38	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	0.54	100.00	3.47	0.60	1.15	5.74	0.00	5.74	4.000	No	Yes	2.00
386	7.72	0.51	100.00	3.51	0.60	1.15	5.20	0.00	5.20	4.000	No	Yes	2.00
387	7.74	0.50	100.00	3.49	0.60	1.14	5.22	0.00	5.22	4.000	No	Yes	2.00
388	7.76	0.54	100.00	3.40	0.60	1.14	5.50	0.00	5.50	4.000	No	Yes	2.00
389	7.78	0.62	100.00	3.25	0.60	1.14	6.42	0.00	6.42	4.000	No	Yes	2.00
390	7.80	0.77	100.00	3.07	0.59	1.14	7.93	0.00	7.93	4.000	No	Yes	2.00
391	7.82	0.89	98.27	2.94	0.58	1.13	10.57	0.00	10.57	4.000	No	Yes	2.00
392	7.85	0.94	94.86	2.90	0.58	1.13	10.63	0.00	10.63	4.000	No	Yes	2.00
393	7.86	0.89	99.38	2.95	0.58	1.13	9.90	0.00	9.90	4.000	No	Yes	2.00
394	7.88	0.79	100.00	3.06	0.59	1.13	8.69	0.00	8.69	4.000	No	Yes	2.00
395	7.91	0.71	100.00	3.15	0.59	1.13	7.40	0.00	7.40	4.000	No	Yes	2.00
396	7.92	0.68	100.00	3.18	0.59	1.13	7.18	0.00	7.18	4.000	No	Yes	2.00
397	7.94	0.71	100.00	3.14	0.59	1.13	7.47	0.00	7.47	4.000	No	Yes	2.00
398	7.97	0.74	100.00	3.10	0.59	1.13	7.86	0.00	7.86	4.000	No	Yes	2.00
399	7.98	0.75	100.00	3.08	0.59	1.13	7.93	0.00	7.93	4.000	No	Yes	2.00
400	8.00	0.75	100.00	3.06	0.59	1.13	7.65	0.00	7.65	4.000	No	Yes	2.00
401	8.02	0.74	100.00	3.06	0.59	1.13	7.77	0.00	7.77	4.000	No	Yes	2.00
402	8.04	0.77	100.00	3.03	0.59	1.13	7.79	0.00	7.79	4.000	No	Yes	2.00
403	8.06	0.83	100.00	2.99	0.59	1.12	8.68	0.00	8.68	4.000	No	Yes	2.00
404	8.08	0.90	98.02	2.94	0.58	1.12	9.52	0.00	9.52	4.000	No	Yes	2.00
405	8.10	0.93	96.55	2.92	0.58	1.12	10.16	0.00	10.16	4.000	No	Yes	2.00
406	8.12	0.94	97.33	2.93	0.58	1.12	10.12	0.00	10.12	4.000	No	Yes	2.00
407	8.14	0.91	100.00	2.98	0.58	1.12	10.04	0.00	10.04	4.000	No	Yes	2.00
408	8.16	0.83	100.00	3.06	0.59	1.12	9.19	0.00	9.19	4.000	No	Yes	2.00
409	8.18	0.74	100.00	3.16	0.59	1.12	7.57	0.00	7.57	4.000	No	Yes	2.00
410	8.20	0.70	100.00	3.22	0.59	1.12	6.93	0.00	6.93	4.000	No	Yes	2.00
411	8.22	0.76	100.00	3.15	0.59	1.12	7.81	0.00	7.81	4.000	No	Yes	2.00
412	8.24	0.87	100.00	3.04	0.58	1.11	9.55	0.00	9.55	4.000	No	Yes	2.00
413	8.26	0.93	100.00	2.99	0.58	1.11	10.45	0.00	10.45	4.000	No	Yes	2.00
414	8.28	0.93	100.00	2.99	0.58	1.11	9.95	0.00	9.95	4.000	Yes	Yes	2.00
415	8.30	0.96	100.00	2.96	0.58	1.11	9.67	0.00	9.67	4.000	Yes	Yes	2.00
416	8.32	1.16	89.16	2.83	0.58	1.11	11.29	0.00	11.29	4.000	Yes	Yes	2.00
417	8.34	1.49	77.35	2.68	0.56	1.10	16.60	0.00	16.60	4.000	Yes	Yes	2.00
418	8.36	1.82	69.75	2.58	0.55	1.10	20.39	56.51	76.89	4.000	Yes	No	2.00
419	8.38	2.01	66.40	2.54	0.55	1.10	21.87	56.30	78.17	4.000	Yes	No	2.00
420	8.40	2.10	64.10	2.51	0.55	1.10	22.68	56.04	78.72	4.000	Yes	No	2.00
421	8.42	2.21	60.84	2.47	0.55	1.10	23.46	55.50	78.96	4.000	Yes	No	2.00
422	8.45	2.38	57.49	2.43	0.54	1.10	25.42	55.17	80.58	4.000	Yes	No	2.00
423	8.46	2.60	54.42	2.39	0.54	1.09	28.13	54.99	83.13	4.000	Yes	No	2.00
424	8.48	2.80	51.99	2.36	0.53	1.09	30.54	54.83	85.38	4.000	Yes	No	2.00
425	8.50	2.82	50.57	2.34	0.53	1.09	31.58	54.59	86.17	0.122	No	No	0.64
426	8.52	2.62	50.80	2.35	0.54	1.09	28.93	53.97	82.90	4.000	Yes	No	2.00
427	8.54	2.19	53.91	2.39	0.55	1.09	24.16	53.75	77.91	4.000	Yes	No	2.00
428	8.56	1.73	62.22	2.49	0.57	1.09	17.93	54.27	72.19	4.000	Yes	No	2.00
429	8.58	1.32	78.49	2.69	0.57	1.09	14.10	0.00	14.10	4.000	Yes	Yes	2.00
430	8.60	1.08	93.87	2.89	0.58	1.09	10.75	0.00	10.75	4.000	Yes	Yes	2.00
431	8.62	0.98	100.00	3.00	0.58	1.09	9.86	0.00	9.86	4.000	Yes	Yes	2.00
432	8.64	0.97	100.00	3.01	0.58	1.09	10.43	0.00	10.43	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	0.95	100.00	3.03	0.58	1.09	10.18	0.00	10.18	4.000	No	Yes	2.00
434	8.68	0.89	100.00	3.08	0.59	1.09	9.06	0.00	9.06	4.000	No	Yes	2.00
435	8.70	0.81	100.00	3.13	0.59	1.09	8.26	0.00	8.26	4.000	No	Yes	2.00
436	8.72	0.75	100.00	3.17	0.59	1.09	7.62	0.00	7.62	4.000	No	Yes	2.00
437	8.74	0.71	100.00	3.20	0.59	1.09	7.08	0.00	7.08	4.000	No	Yes	2.00
438	8.76	0.65	100.00	3.26	0.59	1.09	6.88	0.00	6.88	4.000	No	Yes	2.00
439	8.78	0.67	100.00	3.25	0.60	1.09	5.47	0.00	5.47	4.000	No	Yes	2.00
440	8.80	0.69	100.00	3.24	0.59	1.09	7.76	0.00	7.76	4.000	No	Yes	2.00
441	8.82	0.75	100.00	3.18	0.59	1.09	7.44	0.00	7.44	4.000	No	Yes	2.00
442	8.84	0.75	100.00	3.18	0.59	1.08	7.63	0.00	7.63	4.000	No	Yes	2.00
443	8.86	0.76	100.00	3.16	0.59	1.08	7.64	0.00	7.64	4.000	No	Yes	2.00
444	8.88	0.76	100.00	3.15	0.59	1.08	7.64	0.00	7.64	4.000	No	Yes	2.00
445	8.90	0.75	100.00	3.15	0.59	1.08	7.66	0.00	7.66	4.000	No	Yes	2.00
446	8.92	0.73	100.00	3.17	0.59	1.08	7.29	0.00	7.29	4.000	No	Yes	2.00
447	8.94	0.70	100.00	3.19	0.59	1.08	6.83	0.00	6.83	4.000	No	Yes	2.00
448	8.96	0.68	100.00	3.20	0.59	1.08	6.87	0.00	6.87	4.000	No	Yes	2.00
449	8.99	0.68	100.00	3.19	0.60	1.08	6.77	0.00	6.77	4.000	No	Yes	2.00
450	9.00	0.67	100.00	3.21	0.60	1.08	6.72	0.00	6.72	4.000	No	Yes	2.00
451	9.02	0.66	100.00	3.22	0.60	1.08	6.40	0.00	6.40	4.000	No	Yes	2.00
452	9.04	0.64	100.00	3.23	0.60	1.08	6.25	0.00	6.25	4.000	No	Yes	2.00
453	9.06	0.65	100.00	3.22	0.60	1.08	6.30	0.00	6.30	4.000	No	Yes	2.00
454	9.09	0.67	100.00	3.18	0.60	1.07	6.46	0.00	6.46	4.000	No	Yes	2.00
455	9.10	0.72	100.00	3.13	0.59	1.07	7.08	0.00	7.08	4.000	No	Yes	2.00
456	9.12	0.81	100.00	3.04	0.59	1.07	7.86	0.00	7.86	4.000	No	Yes	2.00
457	9.14	0.90	100.00	2.97	0.59	1.07	9.25	0.00	9.25	4.000	No	Yes	2.00
458	9.16	0.98	96.69	2.92	0.58	1.07	10.12	0.00	10.12	4.000	No	Yes	2.00
459	9.18	1.00	97.51	2.93	0.58	1.07	10.42	0.00	10.42	4.000	No	Yes	2.00
460	9.20	0.97	100.00	2.98	0.58	1.07	10.08	0.00	10.08	4.000	No	Yes	2.00
461	9.22	0.97	100.00	3.01	0.58	1.07	9.41	0.00	9.41	4.000	No	Yes	2.00
462	9.24	0.99	100.00	3.02	0.58	1.07	10.25	0.00	10.25	4.000	No	Yes	2.00
463	9.26	0.98	100.00	3.04	0.58	1.06	10.88	0.00	10.88	4.000	No	Yes	2.00
464	9.28	0.90	100.00	3.12	0.59	1.06	9.13	0.00	9.13	4.000	No	Yes	2.00
465	9.30	0.79	100.00	3.23	0.59	1.06	7.89	0.00	7.89	4.000	No	Yes	2.00
466	9.32	0.75	100.00	3.26	0.59	1.06	7.20	0.00	7.20	4.000	No	Yes	2.00
467	9.34	0.77	100.00	3.23	0.59	1.06	7.83	0.00	7.83	4.000	No	Yes	2.00
468	9.36	0.81	100.00	3.18	0.59	1.06	8.25	0.00	8.25	4.000	No	Yes	2.00
469	9.38	0.81	100.00	3.16	0.59	1.06	8.33	0.00	8.33	4.000	No	Yes	2.00
470	9.40	0.80	100.00	3.17	0.59	1.06	7.97	0.00	7.97	4.000	No	Yes	2.00
471	9.42	0.80	100.00	3.16	0.59	1.06	7.83	0.00	7.83	4.000	No	Yes	2.00
472	9.44	0.84	100.00	3.12	0.59	1.06	8.33	0.00	8.33	4.000	No	Yes	2.00
473	9.46	0.95	100.00	3.04	0.59	1.06	9.24	0.00	9.24	4.000	No	Yes	2.00
474	9.48	1.04	100.00	2.98	0.58	1.05	11.06	0.00	11.06	4.000	No	Yes	2.00
475	9.50	1.08	100.00	2.98	0.58	1.05	11.40	0.00	11.40	4.000	No	Yes	2.00
476	9.52	1.04	100.00	3.03	0.58	1.05	10.59	0.00	10.59	4.000	No	Yes	2.00
477	9.54	1.03	100.00	3.05	0.58	1.05	10.21	0.00	10.21	4.000	No	Yes	2.00
478	9.56	1.05	100.00	3.04	0.58	1.05	10.97	0.00	10.97	4.000	No	Yes	2.00
479	9.58	1.04	100.00	3.06	0.58	1.05	11.26	0.00	11.26	4.000	No	Yes	2.00
480	9.60	0.97	100.00	3.12	0.58	1.05	9.95	0.00	9.95	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	0.85	100.00	3.23	0.59	1.05	8.61	0.00	8.61	4.000	No	Yes	2.00
482	9.64	0.75	100.00	3.32	0.59	1.05	7.51	0.00	7.51	4.000	No	Yes	2.00
483	9.66	0.69	100.00	3.37	0.59	1.05	6.88	0.00	6.88	4.000	No	Yes	2.00
484	9.68	0.68	100.00	3.37	0.60	1.05	6.73	0.00	6.73	4.000	No	Yes	2.00
485	9.70	0.69	100.00	3.33	0.59	1.05	6.96	0.00	6.96	4.000	No	Yes	2.00
486	9.72	0.74	100.00	3.25	0.59	1.04	7.37	0.00	7.37	4.000	No	Yes	2.00
487	9.74	0.82	100.00	3.16	0.59	1.04	8.24	0.00	8.24	4.000	No	Yes	2.00
488	9.76	0.93	100.00	3.07	0.59	1.04	9.11	0.00	9.11	4.000	No	Yes	2.00
489	9.78	0.98	100.00	3.06	0.58	1.04	10.76	0.00	10.76	4.000	No	Yes	2.00
490	9.80	1.00	100.00	3.09	0.58	1.04	9.78	0.00	9.78	4.000	No	Yes	2.00
491	9.82	0.97	100.00	3.11	0.58	1.04	9.73	0.00	9.73	4.000	No	Yes	2.00
492	9.84	0.98	100.00	3.10	0.58	1.04	10.09	0.00	10.09	4.000	No	Yes	2.00
493	9.86	0.98	100.00	3.10	0.58	1.04	9.87	0.00	9.87	4.000	No	Yes	2.00
494	9.88	1.01	100.00	3.09	0.58	1.04	9.77	0.00	9.77	4.000	No	Yes	2.00
495	9.90	1.10	100.00	3.02	0.58	1.04	10.98	0.00	10.98	4.000	No	Yes	2.00
496	9.92	1.23	99.31	2.95	0.57	1.03	12.72	0.00	12.72	4.000	No	Yes	2.00
497	9.94	1.34	96.63	2.92	0.57	1.03	13.76	0.00	13.76	4.000	No	Yes	2.00
498	9.96	1.37	97.60	2.93	0.57	1.03	14.14	0.00	14.14	4.000	No	Yes	2.00
499	9.98	1.33	99.99	2.96	0.57	1.03	13.64	0.00	13.64	4.000	No	Yes	2.00
500	10.01	1.24	100.00	3.00	0.57	1.03	12.66	0.00	12.66	4.000	No	Yes	2.00
501	10.02	1.10	100.00	3.06	0.58	1.03	11.33	0.00	11.33	4.000	No	Yes	2.00
502	10.04	0.96	100.00	3.12	0.59	1.03	9.26	0.00	9.26	4.000	No	Yes	2.00
503	10.06	0.91	100.00	3.13	0.59	1.03	8.50	0.00	8.50	4.000	No	Yes	2.00
504	10.08	0.98	100.00	3.07	0.58	1.03	9.84	0.00	9.84	4.000	No	Yes	2.00
505	10.10	1.09	100.00	3.00	0.58	1.03	11.09	0.00	11.09	4.000	No	Yes	2.00
506	10.12	1.18	99.67	2.96	0.58	1.03	11.87	0.00	11.87	4.000	No	Yes	2.00
507	10.14	1.24	98.50	2.94	0.57	1.02	12.52	0.00	12.52	4.000	No	Yes	2.00
508	10.16	1.30	97.54	2.93	0.57	1.02	12.98	0.00	12.98	4.000	No	Yes	2.00
509	10.18	1.36	96.43	2.92	0.57	1.02	13.63	0.00	13.63	4.000	No	Yes	2.00
510	10.20	1.43	95.31	2.90	0.57	1.02	14.39	0.00	14.39	4.000	No	Yes	2.00
511	10.22	1.46	95.29	2.90	0.56	1.02	14.96	0.00	14.96	4.000	No	Yes	2.00
512	10.24	1.41	96.84	2.92	0.57	1.02	14.68	0.00	14.68	4.000	No	Yes	2.00
513	10.26	1.29	99.57	2.96	0.57	1.02	12.76	0.00	12.76	4.000	No	Yes	2.00
514	10.28	1.18	100.00	2.98	0.58	1.02	11.44	0.00	11.44	4.000	No	Yes	2.00
515	10.30	1.14	100.00	2.99	0.58	1.02	11.18	0.00	11.18	4.000	No	Yes	2.00
516	10.32	1.19	99.76	2.96	0.58	1.02	11.46	0.00	11.46	4.000	No	Yes	2.00
517	10.34	1.35	94.54	2.89	0.57	1.02	12.94	0.00	12.94	4.000	No	Yes	2.00
518	10.36	1.54	89.91	2.84	0.56	1.01	15.91	0.00	15.91	4.000	No	Yes	2.00
519	10.38	1.68	87.75	2.81	0.56	1.01	17.31	0.00	17.31	4.000	No	Yes	2.00
520	10.40	1.68	88.20	2.82	0.56	1.01	17.07	0.00	17.07	4.000	No	Yes	2.00
521	10.42	1.59	89.21	2.83	0.56	1.01	15.82	0.00	15.82	4.000	No	Yes	2.00
522	10.44	1.45	91.33	2.85	0.57	1.01	14.61	0.00	14.61	4.000	No	Yes	2.00
523	10.46	1.31	94.98	2.90	0.57	1.01	12.98	0.00	12.98	4.000	No	Yes	2.00
524	10.48	1.15	99.83	2.96	0.58	1.01	11.55	0.00	11.55	4.000	No	Yes	2.00
525	10.50	1.02	100.00	3.02	0.58	1.01	9.81	0.00	9.81	4.000	No	Yes	2.00
526	10.52	0.90	100.00	3.10	0.59	1.01	8.91	0.00	8.91	4.000	No	Yes	2.00
527	10.54	0.88	100.00	3.12	0.59	1.01	8.21	0.00	8.21	4.000	No	Yes	2.00
528	10.56	0.93	100.00	3.08	0.59	1.01	9.05	0.00	9.05	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	1.00	100.00	3.03	0.58	1.01	10.21	0.00	10.21	4.000	No	Yes	2.00
530	10.60	1.05	100.00	3.03	0.58	1.01	10.53	0.00	10.53	4.000	No	Yes	2.00
531	10.62	1.02	100.00	3.06	0.58	1.00	10.32	0.00	10.32	4.000	No	Yes	2.00
532	10.64	0.98	100.00	3.09	0.58	1.00	9.38	0.00	9.38	4.000	No	Yes	2.00
533	10.66	1.01	100.00	3.04	0.58	1.00	9.32	0.00	9.32	4.000	No	Yes	2.00
534	10.68	1.18	96.09	2.91	0.58	1.00	11.10	0.00	11.10	4.000	Yes	Yes	2.00
535	10.70	1.49	84.83	2.77	0.57	1.00	14.50	0.00	14.50	4.000	Yes	Yes	2.00
536	10.72	1.83	77.26	2.68	0.56	1.00	18.49	0.00	18.49	4.000	Yes	Yes	2.00
537	10.74	2.09	71.66	2.61	0.55	1.00	21.01	0.00	21.01	4.000	Yes	Yes	2.00
538	10.76	2.26	65.38	2.53	0.55	1.00	22.29	56.21	78.50	4.000	Yes	No	2.00
539	10.78	2.36	58.91	2.45	0.55	1.00	23.33	54.97	78.30	4.000	Yes	No	2.00
540	10.80	2.42	53.21	2.38	0.55	1.00	23.85	53.44	77.29	4.000	Yes	No	2.00
541	10.82	2.45	49.80	2.34	0.56	1.00	23.97	52.28	76.26	4.000	Yes	No	2.00
542	10.84	2.50	46.46	2.29	0.56	1.00	24.33	51.04	75.37	4.000	Yes	No	2.00
543	10.87	2.58	46.18	2.29	0.56	0.99	25.22	51.14	76.36	4.000	Yes	No	2.00
544	10.88	2.60	50.13	2.34	0.55	0.99	26.20	52.99	79.19	4.000	Yes	No	2.00
545	10.90	2.52	56.41	2.42	0.55	0.99	24.94	54.73	79.67	4.000	Yes	No	2.00
546	10.92	2.29	64.17	2.51	0.55	0.99	22.84	56.10	78.94	4.000	Yes	No	2.00
547	10.95	2.00	71.30	2.60	0.56	0.99	19.46	0.00	19.46	4.000	Yes	Yes	2.00
548	10.96	1.70	77.84	2.69	0.57	0.99	16.32	0.00	16.32	4.000	Yes	Yes	2.00
549	10.98	1.41	85.35	2.78	0.57	0.99	13.91	0.00	13.91	4.000	Yes	Yes	2.00
550	11.00	1.19	94.39	2.89	0.58	0.99	10.99	0.00	10.99	4.000	Yes	Yes	2.00
551	11.02	1.04	100.00	3.01	0.58	0.99	9.88	0.00	9.88	4.000	No	Yes	2.00
552	11.04	0.98	100.00	3.08	0.58	0.99	9.52	0.00	9.52	4.000	No	Yes	2.00
553	11.06	0.93	100.00	3.14	0.59	0.99	9.20	0.00	9.20	4.000	No	Yes	2.00
554	11.08	0.85	100.00	3.22	0.59	0.99	8.34	0.00	8.34	4.000	No	Yes	2.00
555	11.10	0.76	100.00	3.33	0.59	0.99	7.19	0.00	7.19	4.000	No	Yes	2.00
556	11.12	0.68	100.00	3.41	0.60	0.98	6.35	0.00	6.35	4.000	No	Yes	2.00
557	11.14	0.65	100.00	3.44	0.60	0.98	6.04	0.00	6.04	4.000	No	Yes	2.00
558	11.17	0.66	100.00	3.41	0.60	0.98	6.18	0.00	6.18	4.000	No	Yes	2.00
559	11.18	0.73	100.00	3.32	0.60	0.98	6.52	0.00	6.52	4.000	No	Yes	2.00
560	11.20	0.80	100.00	3.22	0.59	0.98	7.74	0.00	7.74	4.000	No	Yes	2.00
561	11.22	0.87	100.00	3.14	0.59	0.98	8.26	0.00	8.26	4.000	No	Yes	2.00
562	11.24	0.86	100.00	3.14	0.59	0.98	8.38	0.00	8.38	4.000	No	Yes	2.00
563	11.26	0.80	100.00	3.22	0.59	0.98	7.65	0.00	7.65	4.000	No	Yes	2.00
564	11.28	0.73	100.00	3.30	0.60	0.98	6.40	0.00	6.40	4.000	No	Yes	2.00
565	11.30	0.71	100.00	3.34	0.60	0.98	6.46	0.00	6.46	4.000	No	Yes	2.00
566	11.32	0.75	100.00	3.28	0.59	0.98	7.02	0.00	7.02	4.000	No	Yes	2.00
567	11.34	0.82	100.00	3.22	0.59	0.98	7.56	0.00	7.56	4.000	No	Yes	2.00
568	11.36	0.87	100.00	3.18	0.59	0.98	8.16	0.00	8.16	4.000	No	Yes	2.00
569	11.38	0.89	100.00	3.17	0.59	0.98	8.48	0.00	8.48	4.000	No	Yes	2.00
570	11.40	0.89	100.00	3.18	0.59	0.97	8.15	0.00	8.15	4.000	No	Yes	2.00
571	11.42	0.88	100.00	3.20	0.59	0.97	8.17	0.00	8.17	4.000	No	Yes	2.00
572	11.44	0.86	100.00	3.23	0.59	0.97	8.20	0.00	8.20	4.000	No	Yes	2.00
573	11.46	0.85	100.00	3.27	0.59	0.97	7.57	0.00	7.57	4.000	No	Yes	2.00
574	11.48	0.86	100.00	3.27	0.59	0.97	7.80	0.00	7.80	4.000	No	Yes	2.00
575	11.50	0.90	100.00	3.24	0.59	0.97	8.40	0.00	8.40	4.000	No	Yes	2.00
576	11.52	0.92	100.00	3.21	0.59	0.97	8.61	0.00	8.61	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	0.91	100.00	3.22	0.59	0.97	8.43	0.00	8.43	4.000	No	Yes	2.00
578	11.56	0.89	100.00	3.24	0.59	0.97	8.17	0.00	8.17	4.000	No	Yes	2.00
579	11.58	0.89	100.00	3.24	0.59	0.97	8.05	0.00	8.05	4.000	No	Yes	2.00
580	11.60	0.91	100.00	3.21	0.59	0.97	8.24	0.00	8.24	4.000	No	Yes	2.00
581	11.62	0.95	100.00	3.18	0.59	0.97	8.64	0.00	8.64	4.000	No	Yes	2.00
582	11.64	1.00	100.00	3.15	0.59	0.97	9.17	0.00	9.17	4.000	No	Yes	2.00
583	11.66	1.03	100.00	3.13	0.58	0.97	9.55	0.00	9.55	4.000	No	Yes	2.00
584	11.68	1.05	100.00	3.12	0.58	0.96	9.69	0.00	9.69	4.000	No	Yes	2.00
585	11.70	1.04	100.00	3.14	0.58	0.96	9.54	0.00	9.54	4.000	No	Yes	2.00
586	11.72	1.01	100.00	3.17	0.58	0.96	9.33	0.00	9.33	4.000	No	Yes	2.00
587	11.74	0.98	100.00	3.21	0.59	0.96	8.94	0.00	8.94	4.000	No	Yes	2.00
588	11.76	0.97	100.00	3.24	0.59	0.96	8.58	0.00	8.58	4.000	No	Yes	2.00
589	11.78	0.97	100.00	3.25	0.59	0.96	8.70	0.00	8.70	4.000	No	Yes	2.00
590	11.80	0.99	100.00	3.24	0.59	0.96	8.87	0.00	8.87	4.000	No	Yes	2.00
591	11.82	1.01	100.00	3.23	0.59	0.96	9.12	0.00	9.12	4.000	No	Yes	2.00
592	11.84	1.03	100.00	3.22	0.59	0.96	9.15	0.00	9.15	4.000	No	Yes	2.00
593	11.86	1.04	100.00	3.21	0.58	0.96	9.38	0.00	9.38	4.000	No	Yes	2.00
594	11.88	1.05	100.00	3.20	0.58	0.96	9.39	0.00	9.39	4.000	No	Yes	2.00
595	11.90	1.05	100.00	3.21	0.58	0.96	9.49	0.00	9.49	4.000	No	Yes	2.00
596	11.92	1.05	100.00	3.22	0.58	0.96	9.52	0.00	9.52	4.000	No	Yes	2.00
597	11.94	1.03	100.00	3.24	0.59	0.95	9.19	0.00	9.19	4.000	No	Yes	2.00
598	11.96	1.01	100.00	3.27	0.59	0.95	9.14	0.00	9.14	4.000	No	Yes	2.00
599	11.98	1.01	100.00	3.28	0.59	0.95	8.96	0.00	8.96	4.000	No	Yes	2.00
600	12.00	1.00	100.00	3.29	0.59	0.95	8.93	0.00	8.93	4.000	No	Yes	2.00
601	12.03	1.01	100.00	3.28	0.59	0.95	8.92	0.00	8.92	4.000	No	Yes	2.00
602	12.04	1.03	100.00	3.26	0.59	0.95	9.12	0.00	9.12	4.000	No	Yes	2.00
603	12.06	1.07	100.00	3.22	0.58	0.95	9.54	0.00	9.54	4.000	No	Yes	2.00
604	12.08	1.10	100.00	3.20	0.58	0.95	9.97	0.00	9.97	4.000	No	Yes	2.00
605	12.10	1.13	100.00	3.18	0.58	0.95	10.02	0.00	10.02	4.000	No	Yes	2.00
606	12.12	1.14	100.00	3.18	0.58	0.95	10.25	0.00	10.25	4.000	No	Yes	2.00
607	12.14	1.15	100.00	3.19	0.58	0.95	10.30	0.00	10.30	4.000	No	Yes	2.00
608	12.16	1.15	100.00	3.19	0.58	0.95	10.25	0.00	10.25	4.000	No	Yes	2.00
609	12.18	1.15	100.00	3.21	0.58	0.95	10.28	0.00	10.28	4.000	No	Yes	2.00
610	12.20	1.15	100.00	3.22	0.58	0.94	10.20	0.00	10.20	4.000	No	Yes	2.00
611	12.22	1.14	100.00	3.22	0.58	0.94	10.22	0.00	10.22	4.000	No	Yes	2.00
612	12.24	1.14	100.00	3.22	0.58	0.94	10.20	0.00	10.20	4.000	No	Yes	2.00
613	12.26	1.14	100.00	3.22	0.58	0.94	10.13	0.00	10.13	4.000	No	Yes	2.00
614	12.28	1.13	100.00	3.23	0.58	0.94	10.20	0.00	10.20	4.000	No	Yes	2.00
615	12.30	1.13	100.00	3.23	0.58	0.94	9.94	0.00	9.94	4.000	No	Yes	2.00
616	12.32	1.12	100.00	3.24	0.58	0.94	9.99	0.00	9.99	4.000	No	Yes	2.00
617	12.34	1.14	100.00	3.23	0.58	0.94	10.00	0.00	10.00	4.000	No	Yes	2.00
618	12.36	1.15	100.00	3.22	0.58	0.94	10.26	0.00	10.26	4.000	No	Yes	2.00
619	12.38	1.17	100.00	3.21	0.58	0.94	10.34	0.00	10.34	4.000	No	Yes	2.00
620	12.40	1.19	100.00	3.20	0.58	0.94	10.43	0.00	10.43	4.000	No	Yes	2.00
621	12.42	1.21	100.00	3.19	0.58	0.94	10.80	0.00	10.80	4.000	No	Yes	2.00
622	12.44	1.23	100.00	3.18	0.58	0.94	11.02	0.00	11.02	4.000	No	Yes	2.00
623	12.46	1.24	100.00	3.18	0.58	0.94	10.98	0.00	10.98	4.000	No	Yes	2.00
624	12.48	1.23	100.00	3.20	0.58	0.93	10.99	0.00	10.99	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	1.22	100.00	3.22	0.58	0.93	10.77	0.00	10.77	4.000	No	Yes	2.00
626	12.52	1.19	100.00	3.24	0.58	0.93	10.57	0.00	10.57	4.000	No	Yes	2.00
627	12.54	1.16	100.00	3.26	0.58	0.93	10.25	0.00	10.25	4.000	No	Yes	2.00
628	12.57	1.12	100.00	3.29	0.58	0.93	10.07	0.00	10.07	4.000	No	Yes	2.00
629	12.58	1.09	100.00	3.32	0.58	0.93	9.52	0.00	9.52	4.000	No	Yes	2.00
630	12.60	1.03	100.00	3.36	0.59	0.93	9.20	0.00	9.20	4.000	No	Yes	2.00
631	12.62	0.98	100.00	3.39	0.59	0.93	8.59	0.00	8.59	4.000	No	Yes	2.00
632	12.64	0.92	100.00	3.44	0.59	0.93	8.14	0.00	8.14	4.000	No	Yes	2.00
633	12.66	0.85	100.00	3.49	0.59	0.93	7.39	0.00	7.39	4.000	No	Yes	2.00
634	12.68	0.78	100.00	3.55	0.59	0.93	6.82	0.00	6.82	4.000	No	Yes	2.00
635	12.70	0.72	100.00	3.61	0.60	0.92	6.28	0.00	6.28	4.000	No	Yes	2.00
636	12.72	0.68	100.00	3.62	0.60	0.92	5.67	0.00	5.67	4.000	No	Yes	2.00
637	12.74	0.67	100.00	3.60	0.60	0.92	5.64	0.00	5.64	4.000	No	Yes	2.00
638	12.76	0.68	100.00	3.54	0.60	0.92	5.76	0.00	5.76	4.000	No	Yes	2.00
639	12.78	0.67	100.00	3.51	0.60	0.92	5.70	0.00	5.70	4.000	No	Yes	2.00
640	12.80	0.66	100.00	3.49	0.60	0.92	5.55	0.00	5.55	4.000	No	Yes	2.00
641	12.82	0.64	100.00	3.49	0.60	0.92	5.41	0.00	5.41	4.000	No	Yes	2.00
642	12.84	0.62	100.00	3.47	0.60	0.92	5.10	0.00	5.10	4.000	No	Yes	2.00
643	12.87	0.61	100.00	3.44	0.60	0.92	5.01	0.00	5.01	4.000	No	Yes	2.00
644	12.88	0.61	100.00	3.40	0.60	0.92	5.07	0.00	5.07	4.000	No	Yes	2.00
645	12.90	0.61	100.00	3.39	0.60	0.92	5.15	0.00	5.15	4.000	No	Yes	2.00
646	12.92	0.60	100.00	3.39	0.60	0.92	4.89	0.00	4.89	4.000	No	Yes	2.00
647	12.94	0.59	100.00	3.39	0.60	0.92	4.82	0.00	4.82	4.000	No	Yes	2.00
648	12.96	0.60	100.00	3.37	0.60	0.92	4.82	0.00	4.82	4.000	No	Yes	2.00
649	12.98	0.60	100.00	3.36	0.60	0.92	5.03	0.00	5.03	4.000	No	Yes	2.00
650	13.00	0.61	100.00	3.34	0.60	0.91	4.94	0.00	4.94	4.000	No	Yes	2.00
651	13.02	0.62	100.00	3.34	0.60	0.91	5.15	0.00	5.15	4.000	No	Yes	2.00
652	13.04	0.63	100.00	3.32	0.60	0.91	5.23	0.00	5.23	4.000	No	Yes	2.00
653	13.06	0.63	100.00	3.34	0.60	0.91	5.23	0.00	5.23	4.000	No	Yes	2.00
654	13.08	0.63	100.00	3.34	0.60	0.91	5.09	0.00	5.09	4.000	No	Yes	2.00
655	13.10	0.64	100.00	3.35	0.60	0.91	5.29	0.00	5.29	4.000	No	Yes	2.00
656	13.12	0.64	100.00	3.34	0.60	0.91	5.27	0.00	5.27	4.000	No	Yes	2.00
657	13.14	0.64	100.00	3.35	0.60	0.91	5.27	0.00	5.27	4.000	No	Yes	2.00
658	13.16	0.65	100.00	3.34	0.60	0.91	5.19	0.00	5.19	4.000	No	Yes	2.00
659	13.18	0.67	100.00	3.30	0.60	0.91	5.41	0.00	5.41	4.000	No	Yes	2.00
660	13.21	0.72	100.00	3.23	0.60	0.91	5.98	0.00	5.98	4.000	No	Yes	2.00
661	13.22	0.74	100.00	3.20	0.60	0.91	6.28	0.00	6.28	4.000	No	Yes	2.00
662	13.24	0.73	100.00	3.21	0.60	0.91	6.10	0.00	6.10	4.000	No	Yes	2.00
663	13.26	0.70	100.00	3.26	0.60	0.91	5.71	0.00	5.71	4.000	No	Yes	2.00
664	13.28	0.69	100.00	3.26	0.60	0.91	5.35	0.00	5.35	4.000	No	Yes	2.00
665	13.30	0.73	100.00	3.21	0.60	0.91	5.98	0.00	5.98	4.000	No	Yes	2.00
666	13.32	0.78	100.00	3.16	0.60	0.91	6.60	0.00	6.60	4.000	No	Yes	2.00
667	13.34	0.81	100.00	3.16	0.60	0.91	6.76	0.00	6.76	4.000	No	Yes	2.00
668	13.36	0.85	100.00	3.13	0.60	0.91	6.80	0.00	6.80	4.000	No	Yes	2.00
669	13.38	0.98	100.00	3.05	0.59	0.91	7.73	0.00	7.73	4.000	No	Yes	2.00
670	13.40	1.17	97.30	2.93	0.58	0.91	10.00	0.00	10.00	4.000	No	Yes	2.00
671	13.42	1.34	92.41	2.87	0.58	0.91	12.19	0.00	12.19	4.000	No	Yes	2.00
672	13.44	1.39	93.05	2.88	0.57	0.91	12.57	0.00	12.57	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	1.34	97.02	2.93	0.58	0.91	11.94	0.00	11.94	4.000	No	Yes	2.00
674	13.48	1.21	100.00	3.01	0.58	0.91	11.00	0.00	11.00	4.000	No	Yes	2.00
675	13.50	1.02	100.00	3.14	0.59	0.90	9.11	0.00	9.11	4.000	No	Yes	2.00
676	13.52	0.85	100.00	3.28	0.59	0.90	6.84	0.00	6.84	4.000	No	Yes	2.00
677	13.54	0.75	100.00	3.36	0.60	0.90	5.93	0.00	5.93	4.000	No	Yes	2.00
678	13.56	0.73	100.00	3.34	0.60	0.90	5.89	0.00	5.89	4.000	No	Yes	2.00
679	13.58	0.74	100.00	3.30	0.60	0.90	6.07	0.00	6.07	4.000	No	Yes	2.00
680	13.60	0.76	100.00	3.26	0.60	0.90	6.09	0.00	6.09	4.000	No	Yes	2.00
681	13.62	0.77	100.00	3.25	0.60	0.90	6.24	0.00	6.24	4.000	No	Yes	2.00
682	13.64	0.78	100.00	3.24	0.60	0.90	6.34	0.00	6.34	4.000	No	Yes	2.00
683	13.66	0.77	100.00	3.24	0.60	0.90	6.20	0.00	6.20	4.000	No	Yes	2.00
684	13.68	0.77	100.00	3.24	0.60	0.90	6.10	0.00	6.10	4.000	No	Yes	2.00
685	13.70	0.79	100.00	3.22	0.60	0.90	6.33	0.00	6.33	4.000	No	Yes	2.00
686	13.72	0.83	100.00	3.19	0.60	0.90	6.67	0.00	6.67	4.000	No	Yes	2.00
687	13.74	0.83	100.00	3.21	0.59	0.90	7.31	0.00	7.31	4.000	No	Yes	2.00
688	13.76	0.82	100.00	3.26	0.60	0.89	6.74	0.00	6.74	4.000	No	Yes	2.00
689	13.78	0.78	100.00	3.31	0.60	0.89	6.30	0.00	6.30	4.000	No	Yes	2.00
690	13.80	0.76	100.00	3.32	0.60	0.89	6.17	0.00	6.17	4.000	No	Yes	2.00
691	13.82	0.78	100.00	3.29	0.60	0.89	6.19	0.00	6.19	4.000	No	Yes	2.00
692	13.84	0.79	100.00	3.27	0.60	0.89	6.47	0.00	6.47	4.000	No	Yes	2.00
693	13.86	0.80	100.00	3.26	0.60	0.89	6.48	0.00	6.48	4.000	No	Yes	2.00
694	13.88	0.81	100.00	3.25	0.60	0.89	6.50	0.00	6.50	4.000	No	Yes	2.00
695	13.90	0.81	100.00	3.24	0.60	0.89	6.63	0.00	6.63	4.000	No	Yes	2.00
696	13.92	0.80	100.00	3.25	0.60	0.89	6.45	0.00	6.45	4.000	No	Yes	2.00
697	13.94	0.78	100.00	3.28	0.60	0.89	6.35	0.00	6.35	4.000	No	Yes	2.00
698	13.96	0.78	100.00	3.29	0.60	0.89	6.07	0.00	6.07	4.000	No	Yes	2.00
699	13.98	0.78	100.00	3.29	0.60	0.89	6.24	0.00	6.24	4.000	No	Yes	2.00
700	14.00	0.79	100.00	3.28	0.60	0.89	6.32	0.00	6.32	4.000	No	Yes	2.00
701	14.02	0.80	100.00	3.27	0.60	0.89	6.37	0.00	6.37	4.000	No	Yes	2.00
702	14.05	0.81	100.00	3.25	0.60	0.89	6.35	0.00	6.35	4.000	No	Yes	2.00
703	14.06	0.86	100.00	3.21	0.60	0.89	6.64	0.00	6.64	4.000	No	Yes	2.00
704	14.08	0.95	100.00	3.11	0.59	0.89	7.59	0.00	7.59	4.000	No	Yes	2.00
705	14.10	1.06	100.00	3.03	0.59	0.89	8.82	0.00	8.82	4.000	No	Yes	2.00
706	14.12	1.14	100.00	2.99	0.58	0.89	9.57	0.00	9.57	4.000	No	Yes	2.00
707	14.14	1.21	99.92	2.96	0.58	0.89	9.96	0.00	9.96	4.000	No	Yes	2.00
708	14.16	1.25	100.00	2.98	0.58	0.89	11.01	0.00	11.01	4.000	No	Yes	2.00
709	14.18	1.25	100.00	3.01	0.58	0.89	10.62	0.00	10.62	4.000	No	Yes	2.00
710	14.20	1.20	100.00	3.08	0.58	0.89	10.20	0.00	10.20	4.000	No	Yes	2.00
711	14.22	1.13	100.00	3.15	0.58	0.88	9.79	0.00	9.79	4.000	No	Yes	2.00
712	14.24	1.05	100.00	3.23	0.59	0.88	8.97	0.00	8.97	4.000	No	Yes	2.00
713	14.26	0.97	100.00	3.29	0.59	0.88	8.00	0.00	8.00	4.000	No	Yes	2.00
714	14.28	1.00	100.00	3.27	0.59	0.88	7.70	0.00	7.70	4.000	No	Yes	2.00
715	14.30	1.19	100.00	3.13	0.58	0.88	9.51	0.00	9.51	4.000	No	Yes	2.00
716	14.32	1.51	98.86	2.95	0.57	0.88	12.83	0.00	12.83	4.000	No	Yes	2.00
717	14.34	1.74	91.30	2.85	0.56	0.89	16.14	0.00	16.14	4.000	No	Yes	2.00
718	14.36	1.72	92.95	2.87	0.56	0.88	15.75	0.00	15.75	4.000	No	Yes	2.00
719	14.38	1.47	100.00	3.00	0.57	0.88	12.78	0.00	12.78	4.000	No	Yes	2.00
720	14.40	1.17	100.00	3.16	0.58	0.88	9.72	0.00	9.72	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	1.06	100.00	3.22	0.59	0.88	7.76	0.00	7.76	4.000	No	Yes	2.00
722	14.44	1.25	100.00	3.07	0.58	0.88	9.47	0.00	9.47	4.000	No	Yes	2.00
723	14.46	1.67	92.81	2.87	0.57	0.88	14.41	0.00	14.41	4.000	No	Yes	2.00
724	14.48	2.08	82.50	2.74	0.56	0.88	18.61	0.00	18.61	4.000	No	Yes	2.00
725	14.50	2.35	77.97	2.69	0.55	0.88	20.39	0.00	20.39	4.000	No	Yes	2.00
726	14.52	2.47	77.27	2.68	0.55	0.88	21.75	0.00	21.75	4.000	No	Yes	2.00
727	14.54	2.49	77.69	2.68	0.55	0.88	21.94	0.00	21.94	4.000	No	Yes	2.00
728	14.56	2.38	80.34	2.72	0.55	0.88	20.88	0.00	20.88	4.000	No	Yes	2.00
729	14.58	2.12	87.32	2.80	0.55	0.88	18.83	0.00	18.83	4.000	No	Yes	2.00
730	14.60	1.75	98.12	2.94	0.56	0.88	15.17	0.00	15.17	4.000	No	Yes	2.00
731	14.62	1.37	100.00	3.10	0.58	0.87	11.16	0.00	11.16	4.000	No	Yes	2.00
732	14.64	1.07	100.00	3.26	0.59	0.87	8.92	0.00	8.92	4.000	No	Yes	2.00
733	14.66	0.94	100.00	3.35	0.59	0.87	7.27	0.00	7.27	4.000	No	Yes	2.00
734	14.68	0.90	100.00	3.40	0.59	0.87	7.46	0.00	7.46	4.000	No	Yes	2.00
735	14.70	1.02	100.00	3.30	0.59	0.87	7.65	0.00	7.65	4.000	No	Yes	2.00
736	14.72	1.09	100.00	3.25	0.58	0.87	10.36	0.00	10.36	4.000	No	Yes	2.00
737	14.74	1.09	100.00	3.25	0.59	0.87	9.18	0.00	9.18	4.000	No	Yes	2.00
738	14.76	0.98	100.00	3.31	0.59	0.87	7.73	0.00	7.73	4.000	No	Yes	2.00
739	14.78	0.91	100.00	3.35	0.59	0.87	7.50	0.00	7.50	4.000	No	Yes	2.00
740	14.80	0.89	100.00	3.35	0.59	0.87	7.22	0.00	7.22	4.000	No	Yes	2.00
741	14.82	0.88	100.00	3.36	0.59	0.86	7.14	0.00	7.14	4.000	No	Yes	2.00
742	14.85	0.87	100.00	3.37	0.59	0.86	7.13	0.00	7.13	4.000	No	Yes	2.00
743	14.86	0.86	100.00	3.38	0.59	0.86	6.88	0.00	6.88	4.000	No	Yes	2.00
744	14.88	0.87	100.00	3.36	0.60	0.86	6.79	0.00	6.79	4.000	No	Yes	2.00
745	14.90	0.94	100.00	3.27	0.59	0.86	7.29	0.00	7.29	4.000	No	Yes	2.00
746	14.92	1.10	100.00	3.14	0.59	0.86	8.78	0.00	8.78	4.000	No	Yes	2.00
747	14.94	1.29	100.00	3.01	0.58	0.86	10.83	0.00	10.83	4.000	No	Yes	2.00
748	14.96	1.40	99.98	2.96	0.57	0.86	12.03	0.00	12.03	4.000	No	Yes	2.00
749	14.98	1.42	100.00	2.97	0.58	0.86	11.82	0.00	11.82	4.000	No	Yes	2.00
750	15.00	1.41	100.00	3.01	0.58	0.86	11.51	0.00	11.51	4.000	No	Yes	2.00
751	15.03	1.46	100.00	3.00	0.57	0.86	11.92	0.00	11.92	4.000	No	Yes	2.00
752	15.04	1.51	100.00	3.01	0.57	0.86	13.18	0.00	13.18	4.000	No	Yes	2.00
753	15.06	1.50	100.00	3.04	0.57	0.86	12.80	0.00	12.80	4.000	No	Yes	2.00
754	15.08	1.38	100.00	3.14	0.58	0.86	11.67	0.00	11.67	4.000	No	Yes	2.00
755	15.10	1.25	100.00	3.22	0.58	0.86	10.02	0.00	10.02	4.000	No	Yes	2.00
756	15.12	1.15	100.00	3.28	0.58	0.86	9.49	0.00	9.49	4.000	No	Yes	2.00
757	15.14	1.05	100.00	3.34	0.59	0.86	8.94	0.00	8.94	4.000	No	Yes	2.00
758	15.16	0.94	100.00	3.42	0.59	0.86	7.44	0.00	7.44	4.000	No	Yes	2.00
759	15.18	0.86	100.00	3.48	0.60	0.85	6.76	0.00	6.76	4.000	No	Yes	2.00
760	15.20	0.84	100.00	3.48	0.60	0.85	6.81	0.00	6.81	4.000	No	Yes	2.00
761	15.23	0.85	100.00	3.44	0.60	0.85	6.77	0.00	6.77	4.000	No	Yes	2.00
762	15.24	0.87	100.00	3.39	0.59	0.85	6.84	0.00	6.84	4.000	No	Yes	2.00
763	15.26	0.90	100.00	3.34	0.59	0.85	7.25	0.00	7.25	4.000	No	Yes	2.00
764	15.28	0.93	100.00	3.29	0.59	0.85	7.46	0.00	7.46	4.000	No	Yes	2.00
765	15.30	0.94	100.00	3.26	0.59	0.85	7.51	0.00	7.51	4.000	No	Yes	2.00
766	15.32	0.95	100.00	3.24	0.59	0.85	7.58	0.00	7.58	4.000	No	Yes	2.00
767	15.34	0.95	100.00	3.25	0.59	0.85	7.60	0.00	7.60	4.000	No	Yes	2.00
768	15.36	0.93	100.00	3.27	0.59	0.85	7.42	0.00	7.42	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	0.90	100.00	3.31	0.59	0.85	7.15	0.00	7.15	4.000	No	Yes	2.00
770	15.40	0.88	100.00	3.34	0.60	0.85	6.74	0.00	6.74	4.000	No	Yes	2.00
771	15.42	0.87	100.00	3.34	0.59	0.85	6.84	0.00	6.84	4.000	No	Yes	2.00
772	15.44	0.89	100.00	3.32	0.59	0.85	6.98	0.00	6.98	4.000	No	Yes	2.00
773	15.46	0.90	100.00	3.29	0.59	0.85	7.11	0.00	7.11	4.000	No	Yes	2.00
774	15.48	0.93	100.00	3.26	0.59	0.85	7.19	0.00	7.19	4.000	No	Yes	2.00
775	15.50	1.03	100.00	3.18	0.59	0.85	7.62	0.00	7.62	4.000	No	Yes	2.00
776	15.52	1.24	100.00	3.04	0.58	0.85	9.59	0.00	9.59	4.000	No	Yes	2.00
777	15.54	1.47	96.95	2.92	0.57	0.85	12.42	0.00	12.42	4.000	No	Yes	2.00
778	15.56	1.61	94.16	2.89	0.57	0.85	13.44	0.00	13.44	4.000	No	Yes	2.00
779	15.58	1.60	97.15	2.93	0.57	0.85	13.42	0.00	13.42	4.000	No	Yes	2.00
780	15.60	1.60	99.18	2.95	0.57	0.85	12.47	0.00	12.47	4.000	No	Yes	2.00
781	15.62	1.61	99.59	2.96	0.57	0.85	13.52	0.00	13.52	4.000	No	Yes	2.00
782	15.64	1.53	100.00	3.02	0.57	0.85	12.04	0.00	12.04	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.13	2.00	0.00	9.94	0.03	0.00
0.14	2.00	0.00	9.93	0.01	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.27	2.00	0.00	9.37	0.03	0.00	1.28	2.00	0.00	9.36	0.01	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.19	2.00	0.00	8.91	0.03	0.00	2.20	2.00	0.00	8.90	0.01	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.04	2.00	0.00	7.98	0.02	0.00
4.06	2.00	0.00	7.97	0.02	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.25	2.00	0.00	7.88	0.03	0.00
4.26	2.00	0.00	7.87	0.01	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.55	2.00	0.00	7.73	0.03	0.00	4.56	2.00	0.00	7.72	0.01	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.97	2.00	0.00	7.52	0.03	0.00
4.98	2.00	0.00	7.51	0.01	0.00	5.01	2.00	0.00	7.50	0.03	0.00
5.02	2.00	0.00	7.49	0.01	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.19	2.00	0.00	7.41	0.03	0.00	5.20	2.00	0.00	7.40	0.01	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.85	2.00	0.00	7.08	0.03	0.00
5.86	2.00	0.00	7.07	0.01	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.25	2.00	0.00	6.88	0.03	0.00
6.26	2.00	0.00	6.87	0.01	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.93	2.00	0.00	6.54	0.03	0.00
6.94	2.00	0.00	6.53	0.01	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.03	2.00	0.00	6.49	0.03	0.00	7.04	2.00	0.00	6.48	0.01	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.85	2.00	0.00	6.08	0.03	0.00
7.86	2.00	0.00	6.07	0.01	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.91	2.00	0.00	6.05	0.03	0.00	7.92	2.00	0.00	6.04	0.01	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.97	2.00	0.00	6.02	0.03	0.00
7.98	2.00	0.00	6.01	0.01	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.45	2.00	0.00	5.78	0.03	0.00
8.46	2.00	0.00	5.77	0.01	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	0.64	0.36	5.75	0.02	0.04	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.99	2.00	0.00	5.51	0.03	0.00	9.00	2.00	0.00	5.50	0.01	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.09	2.00	0.00	5.46	0.03	0.00
9.10	2.00	0.00	5.45	0.01	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.01	2.00	0.00	5.00	0.03	0.00
10.02	2.00	0.00	4.99	0.01	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.87	2.00	0.00	4.57	0.03	0.00	10.88	2.00	0.00	4.56	0.01	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.95	2.00	0.00	4.53	0.03	0.00	10.96	2.00	0.00	4.52	0.01	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.17	2.00	0.00	4.42	0.03	0.00
11.18	2.00	0.00	4.41	0.01	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.03	2.00	0.00	3.99	0.03	0.00	12.04	2.00	0.00	3.98	0.01	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.57	2.00	0.00	3.72	0.03	0.00
12.58	2.00	0.00	3.71	0.01	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.87	2.00	0.00	3.57	0.03	0.00	12.88	2.00	0.00	3.56	0.01	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.21	2.00	0.00	3.40	0.03	0.00
13.22	2.00	0.00	3.39	0.01	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.82	2.00	0.00	3.09	0.02	0.00	13.84	2.00	0.00	3.08	0.02	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.05	2.00	0.00	2.98	0.03	0.00
14.06	2.00	0.00	2.97	0.01	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.80	2.00	0.00	2.60	0.02	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.85	2.00	0.00	2.58	0.03	0.00
14.86	2.00	0.00	2.57	0.01	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.00	2.00	0.00	2.50	0.02	0.00
15.03	2.00	0.00	2.49	0.03	0.00	15.04	2.00	0.00	2.48	0.01	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.23	2.00	0.00	2.38	0.03	0.00	15.24	2.00	0.00	2.38	0.01	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00
15.62	2.00	0.00	2.19	0.02	0.00	15.64	2.00	0.00	2.18	0.02	0.00

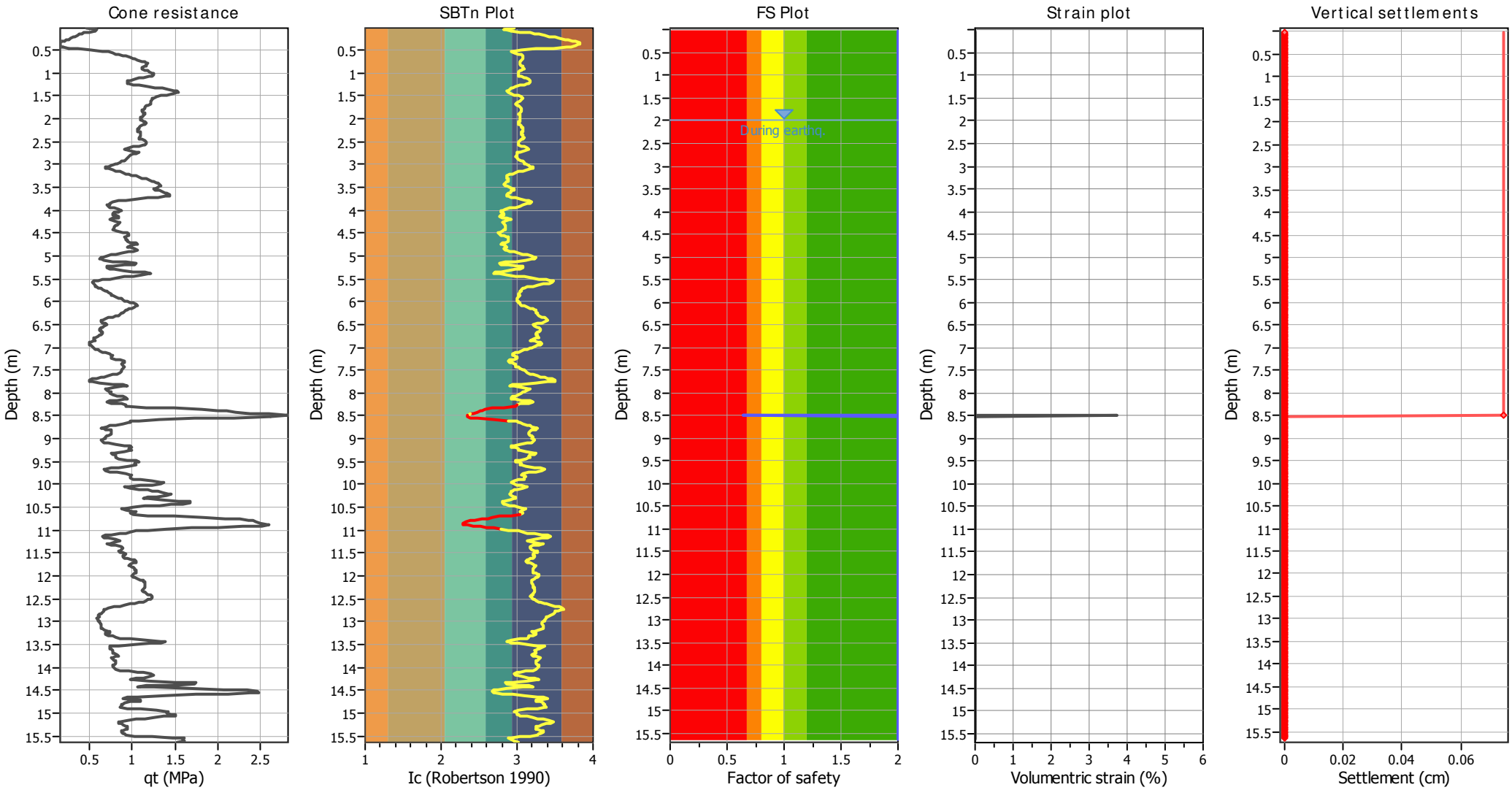
Overall liquefaction potential: 0.04

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.00	18.29	2.00	0.00	1.00	0.00	2.02	18.09	2.00	0.00	1.00	0.00
2.04	18.36	2.00	0.00	1.00	0.00	2.06	18.43	2.00	0.00	1.00	0.00
2.08	19.14	2.00	0.00	1.00	0.00	2.10	19.21	2.00	0.00	1.00	0.00
2.12	19.51	2.00	0.00	1.00	0.00	2.14	18.81	2.00	0.00	1.00	0.00
2.16	18.16	2.00	0.00	1.00	0.00	2.19	18.19	2.00	0.00	1.00	0.00
2.20	17.65	2.00	0.00	1.00	0.00	2.22	17.78	2.00	0.00	1.00	0.00
2.24	17.79	2.00	0.00	1.00	0.00	2.26	17.19	2.00	0.00	1.00	0.00
2.28	17.39	2.00	0.00	1.00	0.00	2.30	17.75	2.00	0.00	1.00	0.00
2.32	17.87	2.00	0.00	1.00	0.00	2.34	17.67	2.00	0.00	1.00	0.00
2.36	17.48	2.00	0.00	1.00	0.00	2.38	17.36	2.00	0.00	1.00	0.00
2.40	17.27	2.00	0.00	1.00	0.00	2.42	16.67	2.00	0.00	1.00	0.00
2.44	16.86	2.00	0.00	1.00	0.00	2.46	17.42	2.00	0.00	1.00	0.00
2.48	17.57	2.00	0.00	1.00	0.00	2.50	18.29	2.00	0.00	1.00	0.00
2.52	18.31	2.00	0.00	1.00	0.00	2.54	17.73	2.00	0.00	1.00	0.00
2.56	17.89	2.00	0.00	1.00	0.00	2.58	17.41	2.00	0.00	1.00	0.00
2.60	16.57	2.00	0.00	1.00	0.00	2.62	15.70	2.00	0.00	1.00	0.00
2.64	14.69	2.00	0.00	1.00	0.00	2.66	13.51	2.00	0.00	1.00	0.00
2.68	13.75	2.00	0.00	1.00	0.00	2.70	14.29	2.00	0.00	1.00	0.00
2.72	16.32	2.00	0.00	1.00	0.00	2.74	16.28	2.00	0.00	1.00	0.00
2.76	15.89	2.00	0.00	1.00	0.00	2.78	15.16	2.00	0.00	1.00	0.00
2.80	14.93	2.00	0.00	1.00	0.00	2.82	14.84	2.00	0.00	1.00	0.00
2.84	14.32	2.00	0.00	1.00	0.00	2.86	14.18	2.00	0.00	1.00	0.00
2.88	14.02	2.00	0.00	1.00	0.00	2.90	13.77	2.00	0.00	1.00	0.00
2.92	13.78	2.00	0.00	1.00	0.00	2.94	13.00	2.00	0.00	1.00	0.00
2.96	12.68	2.00	0.00	1.00	0.00	2.98	12.46	2.00	0.00	1.00	0.00
3.00	11.95	2.00	0.00	1.00	0.00	3.02	11.56	2.00	0.00	1.00	0.00
3.04	10.55	2.00	0.00	1.00	0.00	3.06	10.14	2.00	0.00	1.00	0.00
3.08	10.15	2.00	0.00	1.00	0.00	3.10	10.63	2.00	0.00	1.00	0.00
3.12	10.97	2.00	0.00	1.00	0.00	3.14	11.87	2.00	0.00	1.00	0.00
3.16	12.53	2.00	0.00	1.00	0.00	3.18	12.61	2.00	0.00	1.00	0.00
3.20	13.37	2.00	0.00	1.00	0.00	3.22	13.81	2.00	0.00	1.00	0.00
3.24	14.37	2.00	0.00	1.00	0.00	3.26	14.93	2.00	0.00	1.00	0.00
3.28	15.60	2.00	0.00	1.00	0.00	3.30	16.05	2.00	0.00	1.00	0.00
3.32	16.63	2.00	0.00	1.00	0.00	3.34	17.23	2.00	0.00	1.00	0.00
3.36	17.21	2.00	0.00	1.00	0.00	3.38	17.74	2.00	0.00	1.00	0.00
3.40	18.16	2.00	0.00	1.00	0.00	3.42	18.47	2.00	0.00	1.00	0.00
3.44	18.75	2.00	0.00	1.00	0.00	3.46	19.00	2.00	0.00	1.00	0.00
3.48	18.84	2.00	0.00	1.00	0.00	3.50	18.31	2.00	0.00	1.00	0.00
3.52	17.87	2.00	0.00	1.00	0.00	3.54	17.43	2.00	0.00	1.00	0.00
3.56	17.86	2.00	0.00	1.00	0.00	3.58	18.51	2.00	0.00	1.00	0.00
3.60	19.31	2.00	0.00	1.00	0.00	3.62	19.12	2.00	0.00	1.00	0.00
3.64	19.46	2.00	0.00	1.00	0.00	3.66	20.18	2.00	0.00	1.00	0.00
3.68	20.36	2.00	0.00	1.00	0.00	3.70	19.05	2.00	0.00	1.00	0.00
3.72	17.95	2.00	0.00	1.00	0.00	3.74	17.09	2.00	0.00	1.00	0.00
3.76	14.18	2.00	0.00	1.00	0.00	3.78	12.67	2.00	0.00	1.00	0.00
3.80	11.72	2.00	0.00	1.00	0.00	3.82	10.62	2.00	0.00	1.00	0.00
3.84	9.73	2.00	0.00	1.00	0.00	3.86	10.58	2.00	0.00	1.00	0.00
3.88	9.95	2.00	0.00	1.00	0.00	3.90	9.53	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.92	9.58	2.00	0.00	1.00	0.00	3.94	10.10	2.00	0.00	1.00	0.00
3.96	10.68	2.00	0.00	1.00	0.00	3.98	11.50	2.00	0.00	1.00	0.00
4.00	11.96	2.00	0.00	1.00	0.00	4.02	11.86	2.00	0.00	1.00	0.00
4.04	11.23	2.00	0.00	1.00	0.00	4.06	10.82	2.00	0.00	1.00	0.00
4.08	10.14	2.00	0.00	1.00	0.00	4.10	10.01	2.00	0.00	1.00	0.00
4.12	10.80	2.00	0.00	1.00	0.00	4.14	11.65	2.00	0.00	1.00	0.00
4.16	11.57	2.00	0.00	1.00	0.00	4.18	10.30	2.00	0.00	1.00	0.00
4.20	9.47	2.00	0.00	1.00	0.00	4.22	9.65	2.00	0.00	1.00	0.00
4.25	10.61	2.00	0.00	1.00	0.00	4.26	11.55	2.00	0.00	1.00	0.00
4.28	11.66	2.00	0.00	1.00	0.00	4.30	11.05	2.00	0.00	1.00	0.00
4.32	11.03	2.00	0.00	1.00	0.00	4.34	10.69	2.00	0.00	1.00	0.00
4.36	10.35	2.00	0.00	1.00	0.00	4.38	10.37	2.00	0.00	1.00	0.00
4.40	10.55	2.00	0.00	1.00	0.00	4.42	9.94	2.00	0.00	1.00	0.00
4.44	9.78	2.00	0.00	1.00	0.00	4.46	10.47	2.00	0.00	1.00	0.00
4.48	11.60	2.00	0.00	1.00	0.00	4.50	12.31	2.00	0.00	1.00	0.00
4.52	12.56	2.00	0.00	1.00	0.00	4.55	12.27	2.00	0.00	1.00	0.00
4.56	12.38	2.00	0.00	1.00	0.00	4.58	11.77	2.00	0.00	1.00	0.00
4.60	11.49	2.00	0.00	1.00	0.00	4.62	11.66	2.00	0.00	1.00	0.00
4.64	12.29	2.00	0.00	1.00	0.00	4.66	11.96	2.00	0.00	1.00	0.00
4.68	11.71	2.00	0.00	1.00	0.00	4.70	12.67	2.00	0.00	1.00	0.00
4.72	13.30	2.00	0.00	1.00	0.00	4.74	14.07	2.00	0.00	1.00	0.00
4.76	13.53	2.00	0.00	1.00	0.00	4.78	11.76	2.00	0.00	1.00	0.00
4.80	11.81	2.00	0.00	1.00	0.00	4.82	11.83	2.00	0.00	1.00	0.00
4.84	13.18	2.00	0.00	1.00	0.00	4.86	13.74	2.00	0.00	1.00	0.00
4.88	13.34	2.00	0.00	1.00	0.00	4.90	13.06	2.00	0.00	1.00	0.00
4.92	11.94	2.00	0.00	1.00	0.00	4.94	11.14	2.00	0.00	1.00	0.00
4.97	10.28	2.00	0.00	1.00	0.00	4.98	9.32	2.00	0.00	1.00	0.00
5.01	8.83	2.00	0.00	1.00	0.00	5.02	8.16	2.00	0.00	1.00	0.00
5.04	7.77	2.00	0.00	1.00	0.00	5.06	7.58	2.00	0.00	1.00	0.00
5.08	7.83	2.00	0.00	1.00	0.00	5.10	8.34	2.00	0.00	1.00	0.00
5.12	9.00	2.00	0.00	1.00	0.00	5.14	11.64	2.00	0.00	1.00	0.00
5.16	14.00	2.00	0.00	1.00	0.00	5.19	13.35	2.00	0.00	1.00	0.00
5.20	11.45	2.00	0.00	1.00	0.00	5.22	9.20	2.00	0.00	1.00	0.00
5.24	8.33	2.00	0.00	1.00	0.00	5.26	8.69	2.00	0.00	1.00	0.00
5.28	9.11	2.00	0.00	1.00	0.00	5.30	9.67	2.00	0.00	1.00	0.00
5.32	10.53	2.00	0.00	1.00	0.00	5.34	12.48	2.00	0.00	1.00	0.00
5.36	14.45	2.00	0.00	1.00	0.00	5.38	15.47	2.00	0.00	1.00	0.00
5.40	15.14	2.00	0.00	1.00	0.00	5.42	14.04	2.00	0.00	1.00	0.00
5.44	12.54	2.00	0.00	1.00	0.00	5.46	11.32	2.00	0.00	1.00	0.00
5.48	10.32	2.00	0.00	1.00	0.00	5.50	9.21	2.00	0.00	1.00	0.00
5.52	8.07	2.00	0.00	1.00	0.00	5.54	7.29	2.00	0.00	1.00	0.00
5.56	6.86	2.00	0.00	1.00	0.00	5.58	6.59	2.00	0.00	1.00	0.00
5.60	6.58	2.00	0.00	1.00	0.00	5.62	6.83	2.00	0.00	1.00	0.00
5.64	6.93	2.00	0.00	1.00	0.00	5.66	7.01	2.00	0.00	1.00	0.00
5.68	7.11	2.00	0.00	1.00	0.00	5.70	7.47	2.00	0.00	1.00	0.00
5.72	7.66	2.00	0.00	1.00	0.00	5.74	7.90	2.00	0.00	1.00	0.00
5.76	8.31	2.00	0.00	1.00	0.00	5.78	8.42	2.00	0.00	1.00	0.00
5.80	8.85	2.00	0.00	1.00	0.00	5.82	8.88	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.85	9.43	2.00	0.00	1.00	0.00	5.86	8.87	2.00	0.00	1.00	0.00
5.88	9.00	2.00	0.00	1.00	0.00	5.90	9.63	2.00	0.00	1.00	0.00
5.92	10.36	2.00	0.00	1.00	0.00	5.94	10.38	2.00	0.00	1.00	0.00
5.96	10.70	2.00	0.00	1.00	0.00	5.98	11.09	2.00	0.00	1.00	0.00
6.00	11.44	2.00	0.00	1.00	0.00	6.02	11.78	2.00	0.00	1.00	0.00
6.04	12.20	2.00	0.00	1.00	0.00	6.06	12.75	2.00	0.00	1.00	0.00
6.08	12.82	2.00	0.00	1.00	0.00	6.10	12.83	2.00	0.00	1.00	0.00
6.12	12.51	2.00	0.00	1.00	0.00	6.14	11.79	2.00	0.00	1.00	0.00
6.16	11.80	2.00	0.00	1.00	0.00	6.18	11.38	2.00	0.00	1.00	0.00
6.20	11.36	2.00	0.00	1.00	0.00	6.22	11.12	2.00	0.00	1.00	0.00
6.25	10.88	2.00	0.00	1.00	0.00	6.26	10.74	2.00	0.00	1.00	0.00
6.28	10.26	2.00	0.00	1.00	0.00	6.30	10.19	2.00	0.00	1.00	0.00
6.32	9.88	2.00	0.00	1.00	0.00	6.34	9.30	2.00	0.00	1.00	0.00
6.36	8.63	2.00	0.00	1.00	0.00	6.38	8.19	2.00	0.00	1.00	0.00
6.40	7.85	2.00	0.00	1.00	0.00	6.42	7.54	2.00	0.00	1.00	0.00
6.44	7.64	2.00	0.00	1.00	0.00	6.46	7.94	2.00	0.00	1.00	0.00
6.48	8.17	2.00	0.00	1.00	0.00	6.50	8.51	2.00	0.00	1.00	0.00
6.52	8.52	2.00	0.00	1.00	0.00	6.54	7.92	2.00	0.00	1.00	0.00
6.56	7.65	2.00	0.00	1.00	0.00	6.58	7.45	2.00	0.00	1.00	0.00
6.60	7.37	2.00	0.00	1.00	0.00	6.62	7.28	2.00	0.00	1.00	0.00
6.64	7.46	2.00	0.00	1.00	0.00	6.66	7.56	2.00	0.00	1.00	0.00
6.68	7.69	2.00	0.00	1.00	0.00	6.70	7.84	2.00	0.00	1.00	0.00
6.72	7.41	2.00	0.00	1.00	0.00	6.74	7.25	2.00	0.00	1.00	0.00
6.76	6.93	2.00	0.00	1.00	0.00	6.78	6.61	2.00	0.00	1.00	0.00
6.80	6.24	2.00	0.00	1.00	0.00	6.82	6.44	2.00	0.00	1.00	0.00
6.84	6.33	2.00	0.00	1.00	0.00	6.86	6.24	2.00	0.00	1.00	0.00
6.88	5.77	2.00	0.00	1.00	0.00	6.90	5.50	2.00	0.00	1.00	0.00
6.93	5.41	2.00	0.00	1.00	0.00	6.94	5.52	2.00	0.00	1.00	0.00
6.96	5.60	2.00	0.00	1.00	0.00	6.98	5.93	2.00	0.00	1.00	0.00
7.00	5.98	2.00	0.00	1.00	0.00	7.03	6.13	2.00	0.00	1.00	0.00
7.04	6.21	2.00	0.00	1.00	0.00	7.06	6.60	2.00	0.00	1.00	0.00
7.08	6.83	2.00	0.00	1.00	0.00	7.10	6.80	2.00	0.00	1.00	0.00
7.12	7.76	2.00	0.00	1.00	0.00	7.14	8.15	2.00	0.00	1.00	0.00
7.16	8.58	2.00	0.00	1.00	0.00	7.18	8.42	2.00	0.00	1.00	0.00
7.20	8.60	2.00	0.00	1.00	0.00	7.22	8.28	2.00	0.00	1.00	0.00
7.24	8.18	2.00	0.00	1.00	0.00	7.26	8.69	2.00	0.00	1.00	0.00
7.28	9.76	2.00	0.00	1.00	0.00	7.30	9.89	2.00	0.00	1.00	0.00
7.32	9.98	2.00	0.00	1.00	0.00	7.34	9.77	2.00	0.00	1.00	0.00
7.36	9.30	2.00	0.00	1.00	0.00	7.38	9.58	2.00	0.00	1.00	0.00
7.40	9.90	2.00	0.00	1.00	0.00	7.42	9.89	2.00	0.00	1.00	0.00
7.44	9.96	2.00	0.00	1.00	0.00	7.46	9.70	2.00	0.00	1.00	0.00
7.48	9.44	2.00	0.00	1.00	0.00	7.50	9.38	2.00	0.00	1.00	0.00
7.52	9.47	2.00	0.00	1.00	0.00	7.54	9.64	2.00	0.00	1.00	0.00
7.56	9.40	2.00	0.00	1.00	0.00	7.58	8.96	2.00	0.00	1.00	0.00
7.60	8.52	2.00	0.00	1.00	0.00	7.62	7.85	2.00	0.00	1.00	0.00
7.64	7.24	2.00	0.00	1.00	0.00	7.66	6.70	2.00	0.00	1.00	0.00
7.68	6.38	2.00	0.00	1.00	0.00	7.70	5.74	2.00	0.00	1.00	0.00
7.72	5.20	2.00	0.00	1.00	0.00	7.74	5.22	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.76	5.50	2.00	0.00	1.00	0.00	7.78	6.42	2.00	0.00	1.00	0.00
7.80	7.93	2.00	0.00	1.00	0.00	7.82	10.57	2.00	0.00	1.00	0.00
7.85	10.63	2.00	0.00	1.00	0.00	7.86	9.90	2.00	0.00	1.00	0.00
7.88	8.69	2.00	0.00	1.00	0.00	7.91	7.40	2.00	0.00	1.00	0.00
7.92	7.18	2.00	0.00	1.00	0.00	7.94	7.47	2.00	0.00	1.00	0.00
7.97	7.86	2.00	0.00	1.00	0.00	7.98	7.93	2.00	0.00	1.00	0.00
8.00	7.65	2.00	0.00	1.00	0.00	8.02	7.77	2.00	0.00	1.00	0.00
8.04	7.79	2.00	0.00	1.00	0.00	8.06	8.68	2.00	0.00	1.00	0.00
8.08	9.52	2.00	0.00	1.00	0.00	8.10	10.16	2.00	0.00	1.00	0.00
8.12	10.12	2.00	0.00	1.00	0.00	8.14	10.04	2.00	0.00	1.00	0.00
8.16	9.19	2.00	0.00	1.00	0.00	8.18	7.57	2.00	0.00	1.00	0.00
8.20	6.93	2.00	0.00	1.00	0.00	8.22	7.81	2.00	0.00	1.00	0.00
8.24	9.55	2.00	0.00	1.00	0.00	8.26	10.45	2.00	0.00	1.00	0.00
8.28	9.95	2.00	0.00	1.00	0.00	8.30	9.67	2.00	0.00	1.00	0.00
8.32	11.29	2.00	0.00	1.00	0.00	8.34	16.60	2.00	0.00	1.00	0.00
8.36	76.89	2.00	0.00	1.00	0.00	8.38	78.17	2.00	0.00	1.00	0.00
8.40	78.72	2.00	0.00	1.00	0.00	8.42	78.96	2.00	0.00	1.00	0.00
8.45	80.58	2.00	0.00	1.00	0.00	8.46	83.13	2.00	0.00	1.00	0.00
8.48	85.38	2.00	0.00	1.00	0.00	8.50	86.17	0.64	3.73	1.00	0.07
8.52	82.90	2.00	0.00	1.00	0.00	8.54	77.91	2.00	0.00	1.00	0.00
8.56	72.19	2.00	0.00	1.00	0.00	8.58	14.10	2.00	0.00	1.00	0.00
8.60	10.75	2.00	0.00	1.00	0.00	8.62	9.86	2.00	0.00	1.00	0.00
8.64	10.43	2.00	0.00	1.00	0.00	8.66	10.18	2.00	0.00	1.00	0.00
8.68	9.06	2.00	0.00	1.00	0.00	8.70	8.26	2.00	0.00	1.00	0.00
8.72	7.62	2.00	0.00	1.00	0.00	8.74	7.08	2.00	0.00	1.00	0.00
8.76	6.88	2.00	0.00	1.00	0.00	8.78	5.47	2.00	0.00	1.00	0.00
8.80	7.76	2.00	0.00	1.00	0.00	8.82	7.44	2.00	0.00	1.00	0.00
8.84	7.63	2.00	0.00	1.00	0.00	8.86	7.64	2.00	0.00	1.00	0.00
8.88	7.64	2.00	0.00	1.00	0.00	8.90	7.66	2.00	0.00	1.00	0.00
8.92	7.29	2.00	0.00	1.00	0.00	8.94	6.83	2.00	0.00	1.00	0.00
8.96	6.87	2.00	0.00	1.00	0.00	8.99	6.77	2.00	0.00	1.00	0.00
9.00	6.72	2.00	0.00	1.00	0.00	9.02	6.40	2.00	0.00	1.00	0.00
9.04	6.25	2.00	0.00	1.00	0.00	9.06	6.30	2.00	0.00	1.00	0.00
9.09	6.46	2.00	0.00	1.00	0.00	9.10	7.08	2.00	0.00	1.00	0.00
9.12	7.86	2.00	0.00	1.00	0.00	9.14	9.25	2.00	0.00	1.00	0.00
9.16	10.12	2.00	0.00	1.00	0.00	9.18	10.42	2.00	0.00	1.00	0.00
9.20	10.08	2.00	0.00	1.00	0.00	9.22	9.41	2.00	0.00	1.00	0.00
9.24	10.25	2.00	0.00	1.00	0.00	9.26	10.88	2.00	0.00	1.00	0.00
9.28	9.13	2.00	0.00	1.00	0.00	9.30	7.89	2.00	0.00	1.00	0.00
9.32	7.20	2.00	0.00	1.00	0.00	9.34	7.83	2.00	0.00	1.00	0.00
9.36	8.25	2.00	0.00	1.00	0.00	9.38	8.33	2.00	0.00	1.00	0.00
9.40	7.97	2.00	0.00	1.00	0.00	9.42	7.83	2.00	0.00	1.00	0.00
9.44	8.33	2.00	0.00	1.00	0.00	9.46	9.24	2.00	0.00	1.00	0.00
9.48	11.06	2.00	0.00	1.00	0.00	9.50	11.40	2.00	0.00	1.00	0.00
9.52	10.59	2.00	0.00	1.00	0.00	9.54	10.21	2.00	0.00	1.00	0.00
9.56	10.97	2.00	0.00	1.00	0.00	9.58	11.26	2.00	0.00	1.00	0.00
9.60	9.95	2.00	0.00	1.00	0.00	9.62	8.61	2.00	0.00	1.00	0.00
9.64	7.51	2.00	0.00	1.00	0.00	9.66	6.88	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.68	6.73	2.00	0.00	1.00	0.00	9.70	6.96	2.00	0.00	1.00	0.00
9.72	7.37	2.00	0.00	1.00	0.00	9.74	8.24	2.00	0.00	1.00	0.00
9.76	9.11	2.00	0.00	1.00	0.00	9.78	10.76	2.00	0.00	1.00	0.00
9.80	9.78	2.00	0.00	1.00	0.00	9.82	9.73	2.00	0.00	1.00	0.00
9.84	10.09	2.00	0.00	1.00	0.00	9.86	9.87	2.00	0.00	1.00	0.00
9.88	9.77	2.00	0.00	1.00	0.00	9.90	10.98	2.00	0.00	1.00	0.00
9.92	12.72	2.00	0.00	1.00	0.00	9.94	13.76	2.00	0.00	1.00	0.00
9.96	14.14	2.00	0.00	1.00	0.00	9.98	13.64	2.00	0.00	1.00	0.00
10.01	12.66	2.00	0.00	1.00	0.00	10.02	11.33	2.00	0.00	1.00	0.00
10.04	9.26	2.00	0.00	1.00	0.00	10.06	8.50	2.00	0.00	1.00	0.00
10.08	9.84	2.00	0.00	1.00	0.00	10.10	11.09	2.00	0.00	1.00	0.00
10.12	11.87	2.00	0.00	1.00	0.00	10.14	12.52	2.00	0.00	1.00	0.00
10.16	12.98	2.00	0.00	1.00	0.00	10.18	13.63	2.00	0.00	1.00	0.00
10.20	14.39	2.00	0.00	1.00	0.00	10.22	14.96	2.00	0.00	1.00	0.00
10.24	14.68	2.00	0.00	1.00	0.00	10.26	12.76	2.00	0.00	1.00	0.00
10.28	11.44	2.00	0.00	1.00	0.00	10.30	11.18	2.00	0.00	1.00	0.00
10.32	11.46	2.00	0.00	1.00	0.00	10.34	12.94	2.00	0.00	1.00	0.00
10.36	15.91	2.00	0.00	1.00	0.00	10.38	17.31	2.00	0.00	1.00	0.00
10.40	17.07	2.00	0.00	1.00	0.00	10.42	15.82	2.00	0.00	1.00	0.00
10.44	14.61	2.00	0.00	1.00	0.00	10.46	12.98	2.00	0.00	1.00	0.00
10.48	11.55	2.00	0.00	1.00	0.00	10.50	9.81	2.00	0.00	1.00	0.00
10.52	8.91	2.00	0.00	1.00	0.00	10.54	8.21	2.00	0.00	1.00	0.00
10.56	9.05	2.00	0.00	1.00	0.00	10.58	10.21	2.00	0.00	1.00	0.00
10.60	10.53	2.00	0.00	1.00	0.00	10.62	10.32	2.00	0.00	1.00	0.00
10.64	9.38	2.00	0.00	1.00	0.00	10.66	9.32	2.00	0.00	1.00	0.00
10.68	11.10	2.00	0.00	1.00	0.00	10.70	14.50	2.00	0.00	1.00	0.00
10.72	18.49	2.00	0.00	1.00	0.00	10.74	21.01	2.00	0.00	1.00	0.00
10.76	78.50	2.00	0.00	1.00	0.00	10.78	78.30	2.00	0.00	1.00	0.00
10.80	77.29	2.00	0.00	1.00	0.00	10.82	76.26	2.00	0.00	1.00	0.00
10.84	75.37	2.00	0.00	1.00	0.00	10.87	76.36	2.00	0.00	1.00	0.00
10.88	79.19	2.00	0.00	1.00	0.00	10.90	79.67	2.00	0.00	1.00	0.00
10.92	78.94	2.00	0.00	1.00	0.00	10.95	19.46	2.00	0.00	1.00	0.00
10.96	16.32	2.00	0.00	1.00	0.00	10.98	13.91	2.00	0.00	1.00	0.00
11.00	10.99	2.00	0.00	1.00	0.00	11.02	9.88	2.00	0.00	1.00	0.00
11.04	9.52	2.00	0.00	1.00	0.00	11.06	9.20	2.00	0.00	1.00	0.00
11.08	8.34	2.00	0.00	1.00	0.00	11.10	7.19	2.00	0.00	1.00	0.00
11.12	6.35	2.00	0.00	1.00	0.00	11.14	6.04	2.00	0.00	1.00	0.00
11.17	6.18	2.00	0.00	1.00	0.00	11.18	6.52	2.00	0.00	1.00	0.00
11.20	7.74	2.00	0.00	1.00	0.00	11.22	8.26	2.00	0.00	1.00	0.00
11.24	8.38	2.00	0.00	1.00	0.00	11.26	7.65	2.00	0.00	1.00	0.00
11.28	6.40	2.00	0.00	1.00	0.00	11.30	6.46	2.00	0.00	1.00	0.00
11.32	7.02	2.00	0.00	1.00	0.00	11.34	7.56	2.00	0.00	1.00	0.00
11.36	8.16	2.00	0.00	1.00	0.00	11.38	8.48	2.00	0.00	1.00	0.00
11.40	8.15	2.00	0.00	1.00	0.00	11.42	8.17	2.00	0.00	1.00	0.00
11.44	8.20	2.00	0.00	1.00	0.00	11.46	7.57	2.00	0.00	1.00	0.00
11.48	7.80	2.00	0.00	1.00	0.00	11.50	8.40	2.00	0.00	1.00	0.00
11.52	8.61	2.00	0.00	1.00	0.00	11.54	8.43	2.00	0.00	1.00	0.00
11.56	8.17	2.00	0.00	1.00	0.00	11.58	8.05	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.60	8.24	2.00	0.00	1.00	0.00	11.62	8.64	2.00	0.00	1.00	0.00
11.64	9.17	2.00	0.00	1.00	0.00	11.66	9.55	2.00	0.00	1.00	0.00
11.68	9.69	2.00	0.00	1.00	0.00	11.70	9.54	2.00	0.00	1.00	0.00
11.72	9.33	2.00	0.00	1.00	0.00	11.74	8.94	2.00	0.00	1.00	0.00
11.76	8.58	2.00	0.00	1.00	0.00	11.78	8.70	2.00	0.00	1.00	0.00
11.80	8.87	2.00	0.00	1.00	0.00	11.82	9.12	2.00	0.00	1.00	0.00
11.84	9.15	2.00	0.00	1.00	0.00	11.86	9.38	2.00	0.00	1.00	0.00
11.88	9.39	2.00	0.00	1.00	0.00	11.90	9.49	2.00	0.00	1.00	0.00
11.92	9.52	2.00	0.00	1.00	0.00	11.94	9.19	2.00	0.00	1.00	0.00
11.96	9.14	2.00	0.00	1.00	0.00	11.98	8.96	2.00	0.00	1.00	0.00
12.00	8.93	2.00	0.00	1.00	0.00	12.03	8.92	2.00	0.00	1.00	0.00
12.04	9.12	2.00	0.00	1.00	0.00	12.06	9.54	2.00	0.00	1.00	0.00
12.08	9.97	2.00	0.00	1.00	0.00	12.10	10.02	2.00	0.00	1.00	0.00
12.12	10.25	2.00	0.00	1.00	0.00	12.14	10.30	2.00	0.00	1.00	0.00
12.16	10.25	2.00	0.00	1.00	0.00	12.18	10.28	2.00	0.00	1.00	0.00
12.20	10.20	2.00	0.00	1.00	0.00	12.22	10.22	2.00	0.00	1.00	0.00
12.24	10.20	2.00	0.00	1.00	0.00	12.26	10.13	2.00	0.00	1.00	0.00
12.28	10.20	2.00	0.00	1.00	0.00	12.30	9.94	2.00	0.00	1.00	0.00
12.32	9.99	2.00	0.00	1.00	0.00	12.34	10.00	2.00	0.00	1.00	0.00
12.36	10.26	2.00	0.00	1.00	0.00	12.38	10.34	2.00	0.00	1.00	0.00
12.40	10.43	2.00	0.00	1.00	0.00	12.42	10.80	2.00	0.00	1.00	0.00
12.44	11.02	2.00	0.00	1.00	0.00	12.46	10.98	2.00	0.00	1.00	0.00
12.48	10.99	2.00	0.00	1.00	0.00	12.50	10.77	2.00	0.00	1.00	0.00
12.52	10.57	2.00	0.00	1.00	0.00	12.54	10.25	2.00	0.00	1.00	0.00
12.57	10.07	2.00	0.00	1.00	0.00	12.58	9.52	2.00	0.00	1.00	0.00
12.60	9.20	2.00	0.00	1.00	0.00	12.62	8.59	2.00	0.00	1.00	0.00
12.64	8.14	2.00	0.00	1.00	0.00	12.66	7.39	2.00	0.00	1.00	0.00
12.68	6.82	2.00	0.00	1.00	0.00	12.70	6.28	2.00	0.00	1.00	0.00
12.72	5.67	2.00	0.00	1.00	0.00	12.74	5.64	2.00	0.00	1.00	0.00
12.76	5.76	2.00	0.00	1.00	0.00	12.78	5.70	2.00	0.00	1.00	0.00
12.80	5.55	2.00	0.00	1.00	0.00	12.82	5.41	2.00	0.00	1.00	0.00
12.84	5.10	2.00	0.00	1.00	0.00	12.87	5.01	2.00	0.00	1.00	0.00
12.88	5.07	2.00	0.00	1.00	0.00	12.90	5.15	2.00	0.00	1.00	0.00
12.92	4.89	2.00	0.00	1.00	0.00	12.94	4.82	2.00	0.00	1.00	0.00
12.96	4.82	2.00	0.00	1.00	0.00	12.98	5.03	2.00	0.00	1.00	0.00
13.00	4.94	2.00	0.00	1.00	0.00	13.02	5.15	2.00	0.00	1.00	0.00
13.04	5.23	2.00	0.00	1.00	0.00	13.06	5.23	2.00	0.00	1.00	0.00
13.08	5.09	2.00	0.00	1.00	0.00	13.10	5.29	2.00	0.00	1.00	0.00
13.12	5.27	2.00	0.00	1.00	0.00	13.14	5.27	2.00	0.00	1.00	0.00
13.16	5.19	2.00	0.00	1.00	0.00	13.18	5.41	2.00	0.00	1.00	0.00
13.21	5.98	2.00	0.00	1.00	0.00	13.22	6.28	2.00	0.00	1.00	0.00
13.24	6.10	2.00	0.00	1.00	0.00	13.26	5.71	2.00	0.00	1.00	0.00
13.28	5.35	2.00	0.00	1.00	0.00	13.30	5.98	2.00	0.00	1.00	0.00
13.32	6.60	2.00	0.00	1.00	0.00	13.34	6.76	2.00	0.00	1.00	0.00
13.36	6.80	2.00	0.00	1.00	0.00	13.38	7.73	2.00	0.00	1.00	0.00
13.40	10.00	2.00	0.00	1.00	0.00	13.42	12.19	2.00	0.00	1.00	0.00
13.44	12.57	2.00	0.00	1.00	0.00	13.46	11.94	2.00	0.00	1.00	0.00
13.48	11.00	2.00	0.00	1.00	0.00	13.50	9.11	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.52	6.84	2.00	0.00	1.00	0.00	13.54	5.93	2.00	0.00	1.00	0.00
13.56	5.89	2.00	0.00	1.00	0.00	13.58	6.07	2.00	0.00	1.00	0.00
13.60	6.09	2.00	0.00	1.00	0.00	13.62	6.24	2.00	0.00	1.00	0.00
13.64	6.34	2.00	0.00	1.00	0.00	13.66	6.20	2.00	0.00	1.00	0.00
13.68	6.10	2.00	0.00	1.00	0.00	13.70	6.33	2.00	0.00	1.00	0.00
13.72	6.67	2.00	0.00	1.00	0.00	13.74	7.31	2.00	0.00	1.00	0.00
13.76	6.74	2.00	0.00	1.00	0.00	13.78	6.30	2.00	0.00	1.00	0.00
13.80	6.17	2.00	0.00	1.00	0.00	13.82	6.19	2.00	0.00	1.00	0.00
13.84	6.47	2.00	0.00	1.00	0.00	13.86	6.48	2.00	0.00	1.00	0.00
13.88	6.50	2.00	0.00	1.00	0.00	13.90	6.63	2.00	0.00	1.00	0.00
13.92	6.45	2.00	0.00	1.00	0.00	13.94	6.35	2.00	0.00	1.00	0.00
13.96	6.07	2.00	0.00	1.00	0.00	13.98	6.24	2.00	0.00	1.00	0.00
14.00	6.32	2.00	0.00	1.00	0.00	14.02	6.37	2.00	0.00	1.00	0.00
14.05	6.35	2.00	0.00	1.00	0.00	14.06	6.64	2.00	0.00	1.00	0.00
14.08	7.59	2.00	0.00	1.00	0.00	14.10	8.82	2.00	0.00	1.00	0.00
14.12	9.57	2.00	0.00	1.00	0.00	14.14	9.96	2.00	0.00	1.00	0.00
14.16	11.01	2.00	0.00	1.00	0.00	14.18	10.62	2.00	0.00	1.00	0.00
14.20	10.20	2.00	0.00	1.00	0.00	14.22	9.79	2.00	0.00	1.00	0.00
14.24	8.97	2.00	0.00	1.00	0.00	14.26	8.00	2.00	0.00	1.00	0.00
14.28	7.70	2.00	0.00	1.00	0.00	14.30	9.51	2.00	0.00	1.00	0.00
14.32	12.83	2.00	0.00	1.00	0.00	14.34	16.14	2.00	0.00	1.00	0.00
14.36	15.75	2.00	0.00	1.00	0.00	14.38	12.78	2.00	0.00	1.00	0.00
14.40	9.72	2.00	0.00	1.00	0.00	14.42	7.76	2.00	0.00	1.00	0.00
14.44	9.47	2.00	0.00	1.00	0.00	14.46	14.41	2.00	0.00	1.00	0.00
14.48	18.61	2.00	0.00	1.00	0.00	14.50	20.39	2.00	0.00	1.00	0.00
14.52	21.75	2.00	0.00	1.00	0.00	14.54	21.94	2.00	0.00	1.00	0.00
14.56	20.88	2.00	0.00	1.00	0.00	14.58	18.83	2.00	0.00	1.00	0.00
14.60	15.17	2.00	0.00	1.00	0.00	14.62	11.16	2.00	0.00	1.00	0.00
14.64	8.92	2.00	0.00	1.00	0.00	14.66	7.27	2.00	0.00	1.00	0.00
14.68	7.46	2.00	0.00	1.00	0.00	14.70	7.65	2.00	0.00	1.00	0.00
14.72	10.36	2.00	0.00	1.00	0.00	14.74	9.18	2.00	0.00	1.00	0.00
14.76	7.73	2.00	0.00	1.00	0.00	14.78	7.50	2.00	0.00	1.00	0.00
14.80	7.22	2.00	0.00	1.00	0.00	14.82	7.14	2.00	0.00	1.00	0.00
14.85	7.13	2.00	0.00	1.00	0.00	14.86	6.88	2.00	0.00	1.00	0.00
14.88	6.79	2.00	0.00	1.00	0.00	14.90	7.29	2.00	0.00	1.00	0.00
14.92	8.78	2.00	0.00	1.00	0.00	14.94	10.83	2.00	0.00	1.00	0.00
14.96	12.03	2.00	0.00	1.00	0.00	14.98	11.82	2.00	0.00	1.00	0.00
15.00	11.51	2.00	0.00	1.00	0.00	15.03	11.92	2.00	0.00	1.00	0.00
15.04	13.18	2.00	0.00	1.00	0.00	15.06	12.80	2.00	0.00	1.00	0.00
15.08	11.67	2.00	0.00	1.00	0.00	15.10	10.02	2.00	0.00	1.00	0.00
15.12	9.49	2.00	0.00	1.00	0.00	15.14	8.94	2.00	0.00	1.00	0.00
15.16	7.44	2.00	0.00	1.00	0.00	15.18	6.76	2.00	0.00	1.00	0.00
15.20	6.81	2.00	0.00	1.00	0.00	15.23	6.77	2.00	0.00	1.00	0.00
15.24	6.84	2.00	0.00	1.00	0.00	15.26	7.25	2.00	0.00	1.00	0.00
15.28	7.46	2.00	0.00	1.00	0.00	15.30	7.51	2.00	0.00	1.00	0.00
15.32	7.58	2.00	0.00	1.00	0.00	15.34	7.60	2.00	0.00	1.00	0.00
15.36	7.42	2.00	0.00	1.00	0.00	15.38	7.15	2.00	0.00	1.00	0.00
15.40	6.74	2.00	0.00	1.00	0.00	15.42	6.84	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.44	6.98	2.00	0.00	1.00	0.00	15.46	7.11	2.00	0.00	1.00	0.00
15.48	7.19	2.00	0.00	1.00	0.00	15.50	7.62	2.00	0.00	1.00	0.00
15.52	9.59	2.00	0.00	1.00	0.00	15.54	12.42	2.00	0.00	1.00	0.00
15.56	13.44	2.00	0.00	1.00	0.00	15.58	13.42	2.00	0.00	1.00	0.00
15.60	12.47	2.00	0.00	1.00	0.00	15.62	13.52	2.00	0.00	1.00	0.00
15.64	12.04	2.00	0.00	1.00	0.00						

Total estimated settlement: 0.07

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.46	7.86	6.23	49.00	2.95	0.06	109.76
0.04	0.58	9.83	5.09	50.03	2.83	0.07	68.24
0.06	0.59	10.08	5.14	51.77	2.84	0.07	46.45
0.08	0.57	9.59	5.91	56.72	2.92	0.06	32.93
0.10	0.50	8.52	7.29	62.17	3.05	0.06	23.26
0.13	0.44	7.39	8.88	65.61	3.17	0.06	15.38
0.14	0.41	6.91	9.74	67.32	3.23	0.06	13.33
0.16	0.38	6.50	10.55	68.57	3.29	0.06	10.92
0.18	0.36	6.06	11.64	70.53	3.36	0.06	9.02
0.20	0.34	5.67	12.73	72.14	3.42	0.06	7.57
0.22	0.31	5.17	14.12	72.96	3.50	0.06	6.25
0.24	0.28	4.70	15.34	72.12	3.57	0.06	5.20
0.26	0.25	4.24	16.56	70.19	3.63	0.05	4.32
0.28	0.23	3.84	17.47	67.10	3.67	0.05	3.63
0.30	0.21	3.46	18.51	63.99	3.72	0.05	3.05
0.32	0.18	3.04	19.74	59.97	3.78	0.05	2.51
0.34	0.17	2.74	20.66	56.52	3.82	0.05	2.13
0.36	0.16	2.61	20.70	54.10	3.82	0.05	1.92
0.38	0.16	2.61	20.24	52.79	3.80	0.05	1.82
0.40	0.16	2.67	19.62	52.33	3.77	0.05	1.77
0.42	0.18	2.88	18.32	52.82	3.71	0.05	1.82
0.44	0.19	3.14	17.12	53.73	3.66	0.05	1.90
0.46	0.25	4.19	13.74	57.58	3.48	0.05	2.42
0.48	0.37	6.15	10.09	62.07	3.26	0.06	3.41
0.50	0.52	8.74	7.46	65.20	3.06	0.06	4.65
0.52	0.65	10.91	6.15	67.13	2.95	0.06	5.58
0.54	0.73	12.24	5.94	72.72	2.92	0.07	6.01
0.56	0.77	12.97	6.34	82.26	2.96	0.06	6.13
0.58	0.81	13.59	6.95	94.38	3.02	0.07	6.19
0.60	0.84	14.14	7.41	104.82	3.06	0.07	6.20
0.62	0.89	14.90	7.63	113.70	3.08	0.07	6.30
0.64	0.93	15.61	7.73	120.73	3.08	0.07	6.38
0.66	0.97	16.32	7.74	126.24	3.08	0.07	6.44
0.68	1.00	16.89	7.68	129.76	3.08	0.07	6.45
0.70	1.03	17.39	7.58	131.83	3.07	0.07	6.43
0.72	1.07	18.00	7.41	133.30	3.06	0.07	6.45
0.74	1.11	18.64	7.23	134.85	3.04	0.07	6.48
0.76	1.15	19.26	7.10	136.68	3.03	0.07	6.50
0.78	1.17	19.60	7.07	138.61	3.03	0.07	6.43
0.80	1.18	19.79	7.08	140.19	3.03	0.07	6.31
0.82	1.17	19.69	7.20	141.77	3.04	0.07	6.11
0.84	1.16	19.51	7.34	143.13	3.05	0.07	5.89
0.86	1.14	19.17	7.54	144.48	3.07	0.07	5.64
0.88	1.12	18.77	7.72	144.85	3.08	0.07	5.39
0.90	1.11	18.61	7.78	144.89	3.09	0.07	5.21
0.92	1.12	18.74	7.70	144.25	3.08	0.07	5.12
0.94	1.15	19.25	7.46	143.61	3.06	0.07	5.14
0.96	1.18	19.77	7.24	143.03	3.04	0.07	5.16

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	1.20	20.20	7.07	142.71	3.03	0.07	5.15
1.00	1.23	20.64	6.92	142.83	3.02	0.07	5.15
1.02	1.25	20.87	6.86	143.24	3.01	0.07	5.10
1.04	1.25	21.02	6.86	144.20	3.01	0.07	5.03
1.06	1.24	20.77	7.02	145.73	3.02	0.07	4.87
1.08	1.20	20.12	7.32	147.21	3.05	0.07	4.62
1.10	1.14	19.03	7.80	148.36	3.09	0.07	4.28
1.12	1.08	17.98	8.24	148.15	3.12	0.07	3.97
1.14	1.02	17.03	8.65	147.27	3.16	0.07	3.69
1.16	0.98	16.32	8.88	144.87	3.17	0.07	3.47
1.18	0.95	15.74	9.00	141.73	3.18	0.07	3.29
1.20	0.94	15.65	8.83	138.12	3.17	0.07	3.21
1.22	0.95	15.75	8.56	134.91	3.15	0.07	3.17
1.24	0.96	16.03	8.25	132.25	3.13	0.07	3.17
1.27	1.01	16.74	7.76	130.00	3.09	0.07	3.23
1.28	1.08	18.04	7.14	128.75	3.03	0.07	3.46
1.30	1.18	19.64	6.58	129.23	2.99	0.07	3.70
1.32	1.27	21.17	6.19	131.00	2.95	0.08	3.92
1.34	1.35	22.57	5.92	133.51	2.92	0.08	4.12
1.36	1.43	23.84	5.67	135.19	2.90	0.08	4.28
1.38	1.48	24.79	5.51	136.69	2.88	0.08	4.38
1.40	1.52	25.47	5.43	138.35	2.87	0.09	4.44
1.42	1.54	25.76	5.46	140.65	2.88	0.09	4.42
1.44	1.53	25.58	5.61	143.58	2.89	0.08	4.32
1.46	1.48	24.71	5.96	147.39	2.93	0.08	4.12
1.48	1.41	23.54	6.42	151.23	2.97	0.08	3.87
1.50	1.34	22.34	6.93	154.79	3.02	0.08	3.61
1.52	1.29	21.47	7.32	157.24	3.05	0.07	3.43
1.54	1.25	20.88	7.57	157.95	3.07	0.07	3.28
1.56	1.24	20.65	7.60	156.91	3.07	0.07	3.20
1.58	1.23	20.48	7.50	153.59	3.07	0.07	3.14
1.60	1.23	20.38	7.31	149.07	3.05	0.07	3.08
1.62	1.22	20.24	7.11	143.96	3.03	0.07	3.02
1.64	1.22	20.28	6.84	138.67	3.01	0.07	2.99
1.66	1.22	20.25	6.68	135.23	2.99	0.07	2.94
1.68	1.22	20.19	6.62	133.64	2.99	0.07	2.90
1.70	1.19	19.74	6.79	134.12	3.00	0.07	2.80
1.72	1.17	19.41	6.97	135.27	3.02	0.07	2.72
1.74	1.16	19.12	7.13	136.31	3.03	0.07	2.65
1.76	1.15	19.05	7.22	137.48	3.04	0.07	2.61
1.78	1.14	18.86	7.33	138.30	3.05	0.07	2.55
1.80	1.13	18.67	7.41	138.31	3.06	0.07	2.49
1.82	1.12	18.51	7.45	137.85	3.06	0.07	2.45
1.84	1.12	18.47	7.43	137.17	3.06	0.07	2.41
1.86	1.13	18.69	7.29	136.15	3.05	0.07	2.41
1.88	1.14	18.87	7.17	135.30	3.04	0.07	2.41
1.90	1.15	18.99	7.07	134.21	3.03	0.07	2.40
1.92	1.14	18.81	7.12	133.82	3.03	0.07	2.35

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	1.13	18.58	7.16	133.00	3.04	0.07	2.30
1.96	1.11	18.23	7.25	132.15	3.04	0.07	2.23
1.98	1.10	18.10	7.25	131.24	3.04	0.07	2.19
2.00	1.09	18.00	7.27	130.96	3.05	0.07	2.16
2.02	1.10	18.17	7.22	131.10	3.04	0.07	2.15
2.04	1.11	18.21	7.22	131.41	3.04	0.07	2.14
2.06	1.13	18.56	7.08	131.46	3.03	0.07	2.16
2.08	1.14	18.84	6.99	131.57	3.02	0.07	2.17
2.10	1.16	19.16	6.87	131.73	3.01	0.07	2.18
2.12	1.15	19.00	6.95	132.03	3.02	0.07	2.14
2.14	1.13	18.61	7.11	132.22	3.03	0.07	2.08
2.16	1.10	18.14	7.30	132.49	3.05	0.07	2.01
2.19	1.08	17.75	7.48	132.85	3.06	0.07	1.94
2.20	1.08	17.66	7.55	133.33	3.07	0.07	1.92
2.22	1.07	17.58	7.61	133.81	3.07	0.07	1.89
2.24	1.07	17.50	7.67	134.30	3.08	0.07	1.87
2.26	1.07	17.45	7.70	134.37	3.08	0.07	1.84
2.28	1.07	17.53	7.64	133.99	3.08	0.07	1.84
2.30	1.09	17.86	7.50	133.90	3.06	0.07	1.85
2.32	1.10	18.04	7.44	134.15	3.06	0.07	1.86
2.34	1.10	18.01	7.48	134.62	3.06	0.07	1.84
2.36	1.09	17.90	7.54	134.96	3.07	0.07	1.81
2.38	1.09	17.86	7.59	135.49	3.07	0.07	1.79
2.40	1.08	17.66	7.72	136.42	3.08	0.07	1.75
2.42	1.08	17.60	7.79	137.02	3.09	0.07	1.73
2.44	1.09	17.77	7.71	136.99	3.08	0.07	1.73
2.46	1.12	18.22	7.50	136.61	3.07	0.07	1.76
2.48	1.15	18.81	7.22	135.79	3.04	0.07	1.81
2.50	1.17	19.14	7.04	134.64	3.03	0.07	1.82
2.52	1.17	19.17	6.93	132.95	3.02	0.07	1.82
2.54	1.16	19.02	6.89	131.00	3.01	0.07	1.80
2.56	1.15	18.73	6.91	129.45	3.01	0.07	1.76
2.58	1.12	18.35	7.02	128.90	3.02	0.07	1.72
2.60	1.08	17.54	7.35	128.89	3.05	0.07	1.64
2.62	1.02	16.52	7.80	128.83	3.09	0.07	1.54
2.64	0.95	15.43	8.30	128.07	3.13	0.07	1.43
2.66	0.92	14.81	8.61	127.55	3.15	0.07	1.37
2.68	0.92	14.79	8.56	126.68	3.15	0.07	1.36
2.70	0.98	15.90	7.86	124.98	3.09	0.07	1.46
2.72	1.04	16.88	7.16	120.87	3.04	0.07	1.54
2.74	1.07	17.41	6.69	116.51	3.00	0.07	1.59
2.76	1.04	16.87	6.68	112.63	2.99	0.07	1.53
2.78	1.01	16.27	6.72	109.28	3.00	0.07	1.47
2.80	0.98	15.86	6.66	105.72	2.99	0.07	1.43
2.82	0.97	15.58	6.61	103.04	2.99	0.07	1.40
2.84	0.95	15.35	6.66	102.21	2.99	0.07	1.38
2.86	0.94	15.09	6.80	102.61	3.01	0.07	1.35
2.88	0.93	14.94	6.93	103.44	3.02	0.07	1.33

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.92	14.81	7.06	104.54	3.03	0.07	1.32
2.92	0.90	14.45	7.32	105.87	3.05	0.07	1.28
2.94	0.88	14.06	7.57	106.45	3.07	0.06	1.24
2.96	0.85	13.58	7.81	106.01	3.09	0.06	1.19
2.98	0.83	13.19	7.93	104.60	3.10	0.06	1.16
3.00	0.80	12.77	8.09	103.36	3.11	0.06	1.12
3.02	0.76	12.04	8.52	102.55	3.15	0.06	1.05
3.04	0.72	11.35	8.99	102.07	3.18	0.06	0.99
3.06	0.69	10.83	9.40	101.74	3.21	0.06	0.94
3.08	0.70	10.92	9.34	101.98	3.21	0.06	0.94
3.10	0.72	11.33	9.03	102.30	3.18	0.06	0.98
3.12	0.77	12.10	8.41	101.73	3.14	0.06	1.04
3.14	0.81	12.90	7.69	99.22	3.08	0.06	1.10
3.16	0.85	13.57	7.04	95.60	3.03	0.06	1.16
3.18	0.89	14.18	6.49	92.04	2.98	0.06	1.21
3.20	0.92	14.70	6.08	89.37	2.94	0.07	1.25
3.22	0.96	15.40	5.65	87.03	2.90	0.07	1.30
3.24	1.00	16.01	5.43	86.99	2.87	0.07	1.35
3.26	1.04	16.70	5.32	88.86	2.86	0.07	1.40
3.28	1.08	17.38	5.39	93.62	2.87	0.07	1.46
3.30	1.12	18.10	5.42	98.18	2.87	0.07	1.51
3.32	1.17	18.82	5.48	103.09	2.88	0.07	1.57
3.34	1.20	19.35	5.52	106.81	2.88	0.07	1.61
3.36	1.23	19.86	5.50	109.17	2.88	0.07	1.64
3.38	1.25	20.26	5.43	109.90	2.87	0.08	1.67
3.40	1.28	20.78	5.25	109.11	2.85	0.08	1.71
3.42	1.31	21.19	5.14	108.92	2.84	0.08	1.74
3.44	1.33	21.53	5.09	109.64	2.84	0.08	1.76
3.46	1.34	21.67	5.19	112.46	2.85	0.08	1.77
3.48	1.32	21.48	5.39	115.83	2.87	0.08	1.75
3.50	1.30	21.02	5.72	120.20	2.90	0.07	1.70
3.52	1.27	20.46	6.06	123.92	2.94	0.07	1.65
3.54	1.26	20.31	6.26	127.16	2.96	0.07	1.63
3.56	1.28	20.62	6.24	128.66	2.95	0.07	1.65
3.58	1.32	21.44	6.03	129.20	2.93	0.07	1.72
3.60	1.36	22.01	5.88	129.37	2.92	0.08	1.75
3.62	1.38	22.45	5.77	129.46	2.91	0.08	1.78
3.64	1.41	22.87	5.63	128.83	2.89	0.08	1.81
3.66	1.44	23.44	5.42	127.08	2.87	0.08	1.85
3.68	1.44	23.30	5.38	125.26	2.87	0.08	1.84
3.70	1.38	22.40	5.56	124.45	2.89	0.08	1.76
3.72	1.30	21.06	5.90	124.22	2.92	0.07	1.65
3.74	1.19	19.05	6.47	123.27	2.98	0.07	1.49
3.76	1.06	16.87	7.18	121.07	3.04	0.07	1.31
3.78	0.93	14.66	8.02	117.55	3.11	0.06	1.14
3.80	0.84	13.20	8.63	113.96	3.15	0.06	1.02
3.82	0.77	12.00	9.13	109.59	3.19	0.06	0.93
3.84	0.75	11.56	8.81	101.91	3.17	0.06	0.89

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	0.73	11.32	8.28	93.77	3.13	0.06	0.87
3.88	0.73	11.28	7.61	85.77	3.07	0.06	0.86
3.90	0.71	10.89	7.54	82.10	3.07	0.06	0.83
3.92	0.71	10.97	7.13	78.24	3.03	0.06	0.84
3.94	0.74	11.47	6.48	74.38	2.98	0.06	0.87
3.96	0.79	12.28	5.77	70.86	2.91	0.07	0.93
3.98	0.84	13.06	5.23	68.27	2.85	0.07	0.99
4.00	0.87	13.56	4.87	65.97	2.81	0.07	1.02
4.02	0.86	13.46	4.76	64.01	2.80	0.07	1.01
4.04	0.84	13.00	4.74	61.66	2.80	0.07	0.98
4.06	0.79	12.30	4.87	59.94	2.81	0.07	0.92
4.08	0.77	11.81	4.98	58.85	2.82	0.07	0.88
4.10	0.77	11.83	4.97	58.79	2.82	0.07	0.88
4.12	0.81	12.48	4.71	58.82	2.79	0.07	0.93
4.14	0.85	13.15	4.55	59.87	2.77	0.07	0.98
4.16	0.83	12.95	4.83	62.60	2.81	0.07	0.96
4.18	0.78	12.05	5.43	65.45	2.87	0.07	0.89
4.20	0.74	11.25	5.92	66.58	2.92	0.06	0.83
4.22	0.74	11.40	5.74	65.44	2.90	0.06	0.84
4.25	0.80	12.28	5.19	63.68	2.85	0.07	0.90
4.26	0.85	13.11	4.89	64.13	2.81	0.07	0.96
4.28	0.86	13.28	4.95	65.73	2.82	0.07	0.97
4.30	0.85	13.08	5.10	66.73	2.84	0.07	0.96
4.32	0.82	12.70	5.19	65.87	2.85	0.07	0.93
4.34	0.81	12.42	5.19	64.49	2.85	0.07	0.90
4.36	0.80	12.18	5.23	63.74	2.85	0.07	0.89
4.38	0.80	12.13	5.20	63.09	2.85	0.07	0.88
4.40	0.79	11.98	5.16	61.86	2.84	0.07	0.87
4.42	0.78	11.74	5.11	59.98	2.84	0.07	0.86
4.44	0.78	11.72	5.04	59.03	2.83	0.07	0.86
4.46	0.82	12.36	4.80	59.33	2.80	0.07	0.91
4.48	0.89	13.33	4.57	60.92	2.77	0.07	0.98
4.50	0.94	14.13	4.41	62.37	2.75	0.07	1.05
4.52	0.96	14.42	4.50	64.88	2.77	0.07	1.07
4.55	0.96	14.48	4.69	67.93	2.79	0.07	1.07
4.56	0.94	14.25	5.02	71.54	2.83	0.07	1.04
4.58	0.92	14.00	5.33	74.67	2.86	0.07	1.02
4.60	0.91	13.75	5.57	76.62	2.89	0.07	0.99
4.62	0.92	13.96	5.55	77.49	2.88	0.07	1.01
4.64	0.93	14.12	5.50	77.68	2.88	0.07	1.02
4.66	0.94	14.14	5.54	78.33	2.88	0.07	1.02
4.68	0.95	14.28	5.52	78.80	2.88	0.07	1.03
4.70	0.98	14.76	5.27	77.77	2.85	0.07	1.07
4.72	1.05	15.63	4.88	76.21	2.81	0.07	1.14
4.74	1.07	15.91	4.71	74.87	2.79	0.07	1.17
4.76	1.03	15.32	4.87	74.58	2.81	0.07	1.12
4.78	0.98	14.47	5.14	74.36	2.84	0.07	1.05
4.80	0.94	13.83	5.34	73.88	2.86	0.07	1.00

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	0.98	14.36	5.11	73.35	2.84	0.07	1.05
4.84	1.03	15.12	5.05	76.34	2.83	0.07	1.10
4.86	1.07	15.74	5.13	80.77	2.84	0.07	1.15
4.88	1.06	15.75	5.44	85.65	2.87	0.07	1.14
4.90	1.02	15.05	5.81	87.44	2.91	0.07	1.08
4.92	0.96	14.14	6.26	88.44	2.95	0.06	1.01
4.94	0.88	12.90	6.91	89.14	3.01	0.06	0.92
4.97	0.82	11.74	7.68	90.13	3.08	0.06	0.84
4.98	0.76	10.76	8.38	90.22	3.14	0.06	0.77
5.01	0.70	9.84	9.12	89.74	3.19	0.06	0.70
5.02	0.66	9.20	9.64	88.65	3.23	0.06	0.66
5.04	0.63	8.67	10.03	86.97	3.25	0.06	0.62
5.06	0.62	8.53	9.80	83.59	3.24	0.06	0.61
5.08	0.64	8.77	9.06	79.40	3.19	0.06	0.63
5.10	0.68	9.35	8.01	74.91	3.11	0.06	0.67
5.12	0.78	10.93	6.55	71.54	2.98	0.06	0.78
5.14	0.93	13.07	5.21	68.05	2.85	0.07	0.95
5.16	1.04	14.58	4.49	65.50	2.76	0.07	1.07
5.19	1.03	14.45	4.65	67.12	2.78	0.07	1.06
5.20	0.90	12.67	5.59	70.83	2.89	0.07	0.91
5.22	0.77	10.68	6.90	73.69	3.01	0.06	0.76
5.24	0.70	9.58	7.67	73.52	3.08	0.06	0.68
5.26	0.71	9.59	7.60	72.87	3.07	0.06	0.69
5.28	0.75	10.18	7.14	72.73	3.04	0.06	0.73
5.30	0.80	10.95	6.52	71.44	2.98	0.06	0.78
5.32	0.89	12.26	5.59	68.54	2.89	0.07	0.88
5.34	1.02	13.97	4.62	64.52	2.78	0.07	1.02
5.36	1.15	15.73	4.04	63.49	2.71	0.08	1.17
5.38	1.22	16.70	4.00	66.73	2.70	0.08	1.24
5.40	1.20	16.63	4.52	75.16	2.77	0.08	1.22
5.42	1.12	15.62	5.43	84.77	2.87	0.07	1.13
5.44	1.02	14.14	6.60	93.31	2.99	0.06	1.01
5.46	0.92	12.56	7.79	97.84	3.09	0.06	0.90
5.48	0.83	11.15	9.05	100.90	3.19	0.06	0.80
5.50	0.74	9.78	10.50	102.70	3.29	0.06	0.70
5.52	0.66	8.53	11.99	102.35	3.38	0.06	0.61
5.54	0.60	7.57	13.10	99.26	3.45	0.06	0.54
5.56	0.56	6.98	13.60	94.96	3.47	0.06	0.50
5.58	0.54	6.71	13.40	89.91	3.46	0.06	0.48
5.60	0.54	6.72	12.67	85.07	3.42	0.06	0.48
5.62	0.55	6.87	11.50	78.95	3.35	0.06	0.49
5.64	0.57	7.04	10.37	72.97	3.28	0.06	0.50
5.66	0.58	7.15	9.39	67.17	3.21	0.06	0.51
5.68	0.59	7.37	8.49	62.54	3.14	0.06	0.53
5.70	0.61	7.63	7.83	59.73	3.09	0.06	0.54
5.72	0.63	7.94	7.53	59.86	3.07	0.06	0.57
5.74	0.66	8.29	7.47	61.95	3.06	0.06	0.59
5.76	0.68	8.60	7.45	64.05	3.06	0.06	0.61

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	0.71	8.98	7.24	65.00	3.04	0.06	0.64
5.80	0.72	9.21	7.10	65.39	3.03	0.06	0.66
5.82	0.75	9.62	6.86	65.94	3.01	0.06	0.69
5.85	0.76	9.61	7.01	67.36	3.02	0.06	0.69
5.86	0.76	9.66	7.14	68.97	3.03	0.06	0.69
5.88	0.77	9.72	7.29	70.83	3.05	0.06	0.69
5.90	0.81	10.30	7.01	72.13	3.02	0.06	0.74
5.92	0.84	10.81	6.83	73.79	3.01	0.06	0.77
5.94	0.87	11.18	6.72	75.11	3.00	0.06	0.80
5.96	0.89	11.41	6.79	77.49	3.00	0.06	0.81
5.98	0.92	11.77	6.82	80.26	3.01	0.06	0.84
6.00	0.94	12.16	6.93	84.20	3.02	0.06	0.87
6.02	0.97	12.57	7.04	88.46	3.03	0.06	0.90
6.04	1.01	13.06	7.13	93.15	3.03	0.06	0.93
6.06	1.04	13.44	7.28	97.84	3.05	0.06	0.96
6.08	1.06	13.66	7.46	101.95	3.06	0.06	0.98
6.10	1.05	13.53	7.81	105.73	3.09	0.06	0.97
6.12	1.02	13.08	8.30	108.58	3.13	0.06	0.93
6.14	0.99	12.62	8.76	110.56	3.16	0.06	0.90
6.16	0.96	12.11	9.28	112.40	3.20	0.06	0.87
6.18	0.95	11.91	9.58	114.07	3.22	0.06	0.85
6.20	0.93	11.63	9.85	114.57	3.24	0.06	0.83
6.22	0.92	11.42	9.93	113.39	3.25	0.06	0.82
6.25	0.90	11.14	10.01	111.52	3.25	0.06	0.80
6.26	0.88	10.81	10.20	110.22	3.27	0.06	0.77
6.28	0.86	10.53	10.34	108.88	3.28	0.06	0.75
6.30	0.84	10.18	10.49	106.83	3.29	0.06	0.73
6.32	0.81	9.79	10.68	104.54	3.30	0.06	0.70
6.34	0.77	9.17	11.12	101.98	3.33	0.06	0.66
6.36	0.72	8.51	11.68	99.35	3.36	0.06	0.61
6.38	0.68	7.94	12.14	96.43	3.39	0.06	0.57
6.40	0.65	7.51	12.42	93.32	3.41	0.06	0.54
6.42	0.64	7.30	12.35	90.06	3.40	0.06	0.52
6.44	0.64	7.33	11.85	86.81	3.37	0.06	0.52
6.46	0.66	7.56	11.04	83.52	3.32	0.06	0.54
6.48	0.69	7.90	10.17	80.34	3.26	0.06	0.56
6.50	0.70	8.11	9.53	77.31	3.22	0.06	0.58
6.52	0.70	8.01	9.38	75.16	3.21	0.06	0.57
6.54	0.68	7.68	9.67	74.22	3.23	0.06	0.55
6.56	0.65	7.26	10.24	74.35	3.27	0.06	0.52
6.58	0.63	7.04	10.58	74.49	3.29	0.06	0.50
6.60	0.62	6.90	10.79	74.42	3.30	0.06	0.49
6.62	0.62	6.89	10.80	74.45	3.31	0.06	0.49
6.64	0.63	6.96	10.77	75.03	3.30	0.06	0.50
6.66	0.64	7.12	10.60	75.50	3.29	0.06	0.51
6.68	0.66	7.28	10.26	74.71	3.27	0.06	0.52
6.70	0.65	7.23	10.08	72.84	3.26	0.06	0.52
6.72	0.64	7.06	9.99	70.54	3.25	0.06	0.50

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	0.62	6.72	10.17	68.33	3.26	0.06	0.48
6.76	0.60	6.41	10.27	65.88	3.27	0.06	0.46
6.78	0.57	6.03	10.45	62.99	3.28	0.06	0.43
6.80	0.56	5.90	9.94	58.61	3.25	0.06	0.42
6.82	0.56	5.84	9.45	55.23	3.21	0.06	0.42
6.84	0.56	5.90	8.99	53.05	3.18	0.06	0.42
6.86	0.54	5.65	9.55	53.93	3.22	0.06	0.40
6.88	0.52	5.33	10.25	54.62	3.27	0.06	0.38
6.90	0.50	5.02	10.92	54.83	3.31	0.06	0.36
6.93	0.49	4.94	11.09	54.73	3.32	0.06	0.35
6.94	0.50	4.99	10.85	54.19	3.31	0.06	0.36
6.96	0.52	5.20	10.28	53.48	3.27	0.06	0.37
6.98	0.53	5.39	9.74	52.47	3.23	0.06	0.38
7.00	0.55	5.60	9.16	51.25	3.19	0.06	0.40
7.03	0.56	5.70	8.80	50.14	3.17	0.06	0.41
7.04	0.58	5.94	8.26	49.02	3.13	0.06	0.42
7.06	0.60	6.20	7.81	48.40	3.09	0.06	0.44
7.08	0.61	6.42	7.45	47.82	3.06	0.06	0.46
7.10	0.65	6.85	7.05	48.30	3.03	0.06	0.49
7.12	0.69	7.35	6.63	48.71	2.99	0.06	0.52
7.14	0.74	8.00	6.19	49.55	2.95	0.06	0.57
7.16	0.76	8.24	6.16	50.75	2.95	0.06	0.59
7.18	0.77	8.39	6.24	52.35	2.95	0.06	0.60
7.20	0.76	8.27	6.54	54.12	2.98	0.06	0.59
7.22	0.76	8.18	6.70	54.83	3.00	0.06	0.58
7.24	0.76	8.23	6.70	55.13	3.00	0.06	0.59
7.26	0.81	8.81	6.23	54.87	2.95	0.06	0.63
7.28	0.86	9.47	5.77	54.64	2.91	0.06	0.68
7.30	0.90	9.93	5.52	54.82	2.88	0.07	0.71
7.32	0.90	9.94	5.68	56.46	2.90	0.06	0.71
7.34	0.89	9.73	6.05	58.90	2.94	0.06	0.69
7.36	0.88	9.57	6.40	61.19	2.97	0.06	0.68
7.38	0.88	9.61	6.53	62.74	2.98	0.06	0.69
7.40	0.90	9.82	6.52	64.00	2.98	0.06	0.70
7.42	0.91	9.95	6.59	65.61	2.99	0.06	0.71
7.44	0.91	9.86	6.86	67.62	3.01	0.06	0.70
7.46	0.89	9.67	7.24	70.00	3.04	0.06	0.69
7.48	0.88	9.43	7.66	72.23	3.08	0.06	0.67
7.50	0.87	9.33	7.94	74.04	3.10	0.06	0.67
7.52	0.88	9.39	8.01	75.21	3.11	0.06	0.67
7.54	0.88	9.38	8.14	76.34	3.12	0.06	0.67
7.56	0.86	9.17	8.40	77.01	3.14	0.06	0.65
7.58	0.83	8.72	8.88	77.44	3.17	0.06	0.62
7.60	0.78	8.12	9.46	76.85	3.22	0.06	0.58
7.62	0.73	7.46	10.14	75.62	3.26	0.06	0.53
7.64	0.67	6.76	10.90	73.69	3.31	0.06	0.48
7.66	0.63	6.20	11.60	71.95	3.36	0.06	0.44
7.68	0.59	5.64	12.49	70.40	3.41	0.06	0.40

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	0.54	5.08	13.50	68.54	3.47	0.06	0.36
7.72	0.51	4.64	14.21	66.01	3.51	0.06	0.33
7.74	0.50	4.55	13.92	63.36	3.49	0.06	0.33
7.76	0.54	5.00	12.31	61.56	3.40	0.06	0.36
7.78	0.62	6.00	9.98	59.89	3.25	0.06	0.43
7.80	0.77	7.81	7.50	58.58	3.07	0.06	0.56
7.82	0.89	9.28	6.11	56.71	2.94	0.06	0.66
7.85	0.94	9.90	5.68	56.23	2.90	0.07	0.71
7.86	0.89	9.19	6.25	57.48	2.95	0.06	0.66
7.88	0.79	7.99	7.41	59.19	3.06	0.06	0.57
7.91	0.71	7.02	8.54	59.91	3.15	0.06	0.50
7.92	0.68	6.66	8.94	59.61	3.18	0.06	0.48
7.94	0.71	6.95	8.48	58.93	3.14	0.06	0.50
7.97	0.74	7.30	7.96	58.07	3.10	0.06	0.52
7.98	0.75	7.41	7.64	56.63	3.08	0.06	0.53
8.00	0.75	7.37	7.45	54.94	3.06	0.06	0.53
8.02	0.74	7.31	7.40	54.04	3.06	0.06	0.52
8.04	0.77	7.67	7.05	54.10	3.03	0.06	0.55
8.06	0.83	8.29	6.62	54.88	2.99	0.06	0.59
8.08	0.90	9.10	6.08	55.32	2.94	0.06	0.65
8.10	0.93	9.55	5.89	56.24	2.92	0.06	0.68
8.12	0.94	9.66	5.99	57.83	2.93	0.06	0.69
8.14	0.91	9.24	6.48	59.85	2.98	0.06	0.66
8.16	0.83	8.28	7.41	61.36	3.06	0.06	0.59
8.18	0.74	7.13	8.76	62.53	3.16	0.06	0.51
8.20	0.70	6.65	9.46	62.93	3.22	0.06	0.47
8.22	0.76	7.39	8.58	63.44	3.15	0.06	0.53
8.24	0.87	8.66	7.24	62.71	3.04	0.06	0.62
8.26	0.93	9.38	6.64	62.33	2.99	0.06	0.67
8.28	0.93	9.37	6.59	61.81	2.99	0.06	0.67
8.30	0.96	9.65	6.34	61.18	2.96	0.06	0.69
8.32	1.16	12.00	5.02	60.23	2.83	0.07	0.86
8.34	1.49	15.70	3.85	60.42	2.68	0.08	1.14
8.36	1.82	19.34	3.23	62.50	2.58	0.08	0.62
8.38	2.01	21.39	2.99	64.01	2.54	0.08	0.63
8.40	2.10	22.40	2.84	63.59	2.51	0.08	0.64
8.42	2.21	23.57	2.64	62.12	2.47	0.08	0.64
8.45	2.38	25.39	2.44	62.04	2.43	0.08	0.65
8.46	2.60	27.83	2.28	63.52	2.39	0.08	0.66
8.48	2.80	29.91	2.17	64.77	2.36	0.09	0.67
8.50	2.82	30.11	2.10	63.23	2.34	0.09	0.67
8.52	2.62	27.81	2.11	58.71	2.35	0.08	0.66
8.54	2.19	23.03	2.26	52.00	2.39	0.08	0.64
8.56	1.73	17.93	2.72	48.78	2.49	0.08	0.61
8.58	1.32	13.37	3.95	52.81	2.69	0.07	0.97
8.60	1.08	10.72	5.56	59.62	2.89	0.07	0.77
8.62	0.98	9.58	6.69	64.09	3.00	0.06	0.68
8.64	0.97	9.51	6.87	65.37	3.01	0.06	0.68

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	0.95	9.25	7.11	65.77	3.03	0.06	0.66
8.68	0.89	8.45	7.65	64.66	3.08	0.06	0.60
8.70	0.81	7.53	8.35	62.90	3.13	0.06	0.54
8.72	0.75	6.84	8.87	60.68	3.17	0.06	0.49
8.74	0.71	6.36	9.25	58.88	3.20	0.06	0.45
8.76	0.65	5.65	10.18	57.49	3.26	0.06	0.40
8.78	0.67	5.88	9.94	58.47	3.25	0.06	0.42
8.80	0.69	6.08	9.89	60.12	3.24	0.06	0.43
8.82	0.75	6.81	9.03	61.54	3.18	0.06	0.49
8.84	0.75	6.81	8.97	61.10	3.18	0.06	0.49
8.86	0.76	6.90	8.66	59.74	3.16	0.06	0.49
8.88	0.76	6.92	8.51	58.90	3.15	0.06	0.49
8.90	0.75	6.78	8.52	57.79	3.15	0.06	0.48
8.92	0.73	6.45	8.90	57.41	3.17	0.06	0.46
8.94	0.70	6.15	9.15	56.30	3.19	0.06	0.44
8.96	0.68	5.97	9.29	55.48	3.20	0.06	0.43
8.99	0.68	5.96	9.16	54.56	3.19	0.06	0.43
9.00	0.67	5.80	9.36	54.28	3.21	0.06	0.41
9.02	0.66	5.61	9.58	53.79	3.22	0.06	0.40
9.04	0.64	5.46	9.74	53.23	3.23	0.06	0.39
9.06	0.65	5.49	9.54	52.34	3.22	0.06	0.39
9.09	0.67	5.77	9.02	52.05	3.18	0.06	0.41
9.10	0.72	6.33	8.30	52.52	3.13	0.06	0.45
9.12	0.81	7.29	7.25	52.81	3.04	0.06	0.52
9.14	0.90	8.29	6.40	53.08	2.97	0.06	0.59
9.16	0.98	9.10	5.91	53.74	2.92	0.06	0.65
9.18	1.00	9.30	6.01	55.89	2.93	0.06	0.66
9.20	0.97	8.99	6.58	59.12	2.98	0.06	0.64
9.22	0.97	8.92	6.90	61.57	3.01	0.06	0.64
9.24	0.99	9.18	6.92	63.56	3.02	0.06	0.66
9.26	0.98	9.05	7.24	65.52	3.04	0.06	0.65
9.28	0.90	8.18	8.15	66.65	3.12	0.06	0.58
9.30	0.79	6.88	9.65	66.44	3.23	0.06	0.49
9.32	0.75	6.47	10.07	65.15	3.26	0.06	0.46
9.34	0.77	6.64	9.62	63.86	3.23	0.06	0.47
9.36	0.81	7.06	8.93	63.09	3.18	0.06	0.50
9.38	0.81	7.11	8.75	62.20	3.16	0.06	0.51
9.40	0.80	6.96	8.83	61.48	3.17	0.06	0.50
9.42	0.80	6.95	8.67	60.30	3.16	0.06	0.50
9.44	0.84	7.39	8.17	60.38	3.12	0.06	0.53
9.46	0.95	8.50	7.16	60.86	3.04	0.06	0.61
9.48	1.04	9.49	6.57	62.41	2.98	0.06	0.68
9.50	1.08	9.88	6.53	64.50	2.98	0.06	0.71
9.52	1.04	9.52	7.03	66.91	3.03	0.06	0.68
9.54	1.03	9.36	7.32	68.54	3.05	0.06	0.67
9.56	1.05	9.58	7.19	68.86	3.04	0.06	0.68
9.58	1.04	9.46	7.38	69.87	3.06	0.06	0.68
9.60	0.97	8.62	8.21	70.71	3.12	0.06	0.62

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	0.85	7.30	9.63	70.36	3.23	0.06	0.52
9.64	0.75	6.25	10.95	68.44	3.32	0.06	0.45
9.66	0.69	5.62	11.77	66.11	3.37	0.06	0.40
9.68	0.68	5.44	11.82	64.35	3.37	0.06	0.39
9.70	0.69	5.63	11.22	63.10	3.33	0.06	0.40
9.72	0.74	6.16	10.03	61.72	3.25	0.06	0.44
9.74	0.82	6.91	8.67	59.91	3.16	0.06	0.49
9.76	0.93	8.07	7.54	60.82	3.07	0.06	0.58
9.78	0.98	8.57	7.48	64.15	3.06	0.06	0.61
9.80	1.00	8.75	7.75	67.82	3.09	0.06	0.63
9.82	0.97	8.50	8.05	68.46	3.11	0.06	0.61
9.84	0.98	8.52	7.97	67.92	3.10	0.06	0.61
9.86	0.98	8.53	7.99	68.11	3.10	0.06	0.61
9.88	1.01	8.82	7.77	68.60	3.09	0.06	0.63
9.90	1.10	9.79	7.03	68.82	3.02	0.06	0.70
9.92	1.23	11.15	6.24	69.63	2.95	0.07	0.80
9.94	1.34	12.21	5.90	72.05	2.92	0.07	0.87
9.96	1.37	12.51	6.02	75.32	2.93	0.07	0.89
9.98	1.33	12.11	6.34	76.71	2.96	0.07	0.86
10.01	1.24	11.12	6.75	75.02	3.00	0.06	0.79
10.02	1.10	9.61	7.41	71.22	3.06	0.06	0.69
10.04	0.96	8.18	8.16	66.76	3.12	0.06	0.58
10.06	0.91	7.69	8.31	63.86	3.13	0.06	0.55
10.08	0.98	8.32	7.55	62.85	3.07	0.06	0.59
10.10	1.09	9.47	6.70	63.43	3.00	0.06	0.68
10.12	1.18	10.37	6.29	65.22	2.96	0.06	0.74
10.14	1.24	10.99	6.14	67.48	2.94	0.07	0.79
10.16	1.30	11.57	6.02	69.60	2.93	0.07	0.83
10.18	1.36	12.19	5.88	71.63	2.92	0.07	0.87
10.20	1.43	12.85	5.74	73.70	2.90	0.07	0.92
10.22	1.46	13.19	5.73	75.61	2.90	0.07	0.94
10.24	1.41	12.62	5.93	74.79	2.92	0.07	0.90
10.26	1.29	11.41	6.28	71.64	2.96	0.06	0.81
10.28	1.18	10.21	6.54	66.80	2.98	0.06	0.73
10.30	1.14	9.77	6.61	64.50	2.99	0.06	0.70
10.32	1.19	10.27	6.30	64.74	2.96	0.06	0.73
10.34	1.35	11.86	5.64	66.93	2.89	0.07	0.85
10.36	1.54	13.82	5.10	70.54	2.84	0.07	0.99
10.38	1.68	15.20	4.86	73.95	2.81	0.08	1.09
10.40	1.68	15.16	4.91	74.48	2.82	0.08	1.08
10.42	1.59	14.23	5.02	71.50	2.83	0.07	1.02
10.44	1.45	12.84	5.26	67.58	2.85	0.07	0.92
10.46	1.31	11.39	5.70	64.90	2.90	0.07	0.81
10.48	1.15	9.77	6.31	61.68	2.96	0.06	0.70
10.50	1.02	8.39	6.99	58.62	3.02	0.06	0.60
10.52	0.90	7.26	7.88	57.20	3.10	0.06	0.52
10.54	0.88	7.01	8.16	57.18	3.12	0.06	0.50
10.56	0.93	7.45	7.69	57.27	3.08	0.06	0.53

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	1.00	8.23	7.11	58.52	3.03	0.06	0.59
10.60	1.05	8.64	7.09	61.29	3.03	0.06	0.62
10.62	1.02	8.35	7.49	62.57	3.06	0.06	0.60
10.64	0.98	7.94	7.74	61.47	3.09	0.06	0.57
10.66	1.01	8.20	7.19	58.94	3.04	0.06	0.59
10.68	1.18	9.91	5.83	57.82	2.91	0.07	0.71
10.70	1.49	12.97	4.56	59.12	2.77	0.07	0.93
10.72	1.83	16.28	3.84	62.50	2.68	0.08	1.16
10.74	2.09	18.87	3.38	63.73	2.61	0.08	1.35
10.76	2.26	20.49	2.92	59.90	2.53	0.08	0.63
10.78	2.36	21.43	2.52	54.07	2.45	0.08	0.63
10.80	2.42	22.00	2.22	48.91	2.38	0.08	0.63
10.82	2.45	22.32	2.07	46.12	2.34	0.08	0.64
10.84	2.50	22.78	1.00	22.78	2.29	0.07	0.64
10.87	2.58	23.50	1.00	23.50	2.29	0.07	0.64
10.88	2.60	23.69	2.08	49.29	2.34	0.08	0.64
10.90	2.52	22.86	2.39	54.53	2.42	0.08	0.64
10.92	2.29	20.58	2.84	58.52	2.51	0.08	0.63
10.95	2.00	17.67	3.35	59.19	2.60	0.08	1.26
10.96	1.70	14.69	3.89	57.18	2.69	0.08	1.05
10.98	1.41	11.86	4.61	54.68	2.78	0.07	0.85
11.00	1.19	9.71	5.62	54.59	2.89	0.07	0.69
11.02	1.04	8.26	6.88	56.83	3.01	0.06	0.59
11.04	0.98	7.67	7.69	58.99	3.08	0.06	0.55
11.06	0.93	7.17	8.47	60.67	3.14	0.06	0.51
11.08	0.85	6.40	9.59	61.33	3.22	0.06	0.46
11.10	0.76	5.46	11.14	60.84	3.33	0.06	0.39
11.12	0.68	4.73	12.55	59.36	3.41	0.06	0.34
11.14	0.65	4.44	13.03	57.94	3.44	0.06	0.32
11.17	0.66	4.54	12.51	56.83	3.41	0.06	0.32
11.18	0.73	5.14	11.02	56.63	3.32	0.06	0.37
11.20	0.80	5.84	9.58	55.90	3.22	0.06	0.42
11.22	0.87	6.45	8.45	54.54	3.14	0.06	0.46
11.24	0.86	6.41	8.38	53.72	3.14	0.06	0.46
11.26	0.80	5.79	9.46	54.73	3.22	0.06	0.41
11.28	0.73	5.15	10.79	55.55	3.30	0.06	0.37
11.30	0.71	4.95	11.31	55.99	3.34	0.06	0.35
11.32	0.75	5.34	10.47	55.93	3.28	0.06	0.38
11.34	0.82	5.91	9.54	56.38	3.22	0.06	0.42
11.36	0.87	6.39	8.93	57.10	3.18	0.06	0.46
11.38	0.89	6.58	8.81	57.99	3.17	0.06	0.47
11.40	0.89	6.58	8.94	58.80	3.18	0.06	0.47
11.42	0.88	6.48	9.20	59.61	3.20	0.06	0.46
11.44	0.86	6.28	9.73	61.10	3.23	0.06	0.45
11.46	0.85	6.16	10.20	62.85	3.27	0.06	0.44
11.48	0.86	6.24	10.27	64.12	3.27	0.06	0.45
11.50	0.90	6.60	9.75	64.33	3.24	0.06	0.47
11.52	0.92	6.81	9.41	64.07	3.21	0.06	0.49

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	0.91	6.72	9.50	63.85	3.22	0.06	0.48
11.56	0.89	6.53	9.78	63.87	3.24	0.06	0.47
11.58	0.89	6.47	9.78	63.27	3.24	0.06	0.46
11.60	0.91	6.62	9.44	62.57	3.21	0.06	0.47
11.62	0.95	6.99	8.92	62.40	3.18	0.06	0.50
11.64	1.00	7.42	8.51	63.15	3.15	0.06	0.53
11.66	1.03	7.76	8.24	63.99	3.13	0.06	0.55
11.68	1.05	7.87	8.21	64.64	3.12	0.06	0.56
11.70	1.04	7.79	8.39	65.38	3.14	0.06	0.56
11.72	1.01	7.53	8.84	66.60	3.17	0.06	0.54
11.74	0.98	7.26	9.38	68.08	3.21	0.06	0.52
11.76	0.97	7.09	9.80	69.51	3.24	0.06	0.51
11.78	0.97	7.11	9.93	70.62	3.25	0.06	0.51
11.80	0.99	7.28	9.79	71.29	3.24	0.06	0.52
11.82	1.01	7.42	9.66	71.63	3.23	0.06	0.53
11.84	1.03	7.57	9.48	71.81	3.22	0.06	0.54
11.86	1.04	7.65	9.41	72.04	3.21	0.06	0.55
11.88	1.05	7.75	9.32	72.21	3.20	0.06	0.55
11.90	1.05	7.78	9.34	72.71	3.21	0.06	0.56
11.92	1.05	7.70	9.54	73.49	3.22	0.06	0.55
11.94	1.03	7.58	9.86	74.73	3.24	0.06	0.54
11.96	1.01	7.39	10.23	75.60	3.27	0.06	0.53
11.98	1.01	7.30	10.43	76.14	3.28	0.06	0.52
12.00	1.00	7.22	10.52	75.94	3.29	0.06	0.52
12.03	1.01	7.26	10.39	75.50	3.28	0.06	0.52
12.04	1.03	7.46	10.06	75.10	3.26	0.06	0.53
12.06	1.07	7.80	9.58	74.69	3.22	0.06	0.56
12.08	1.10	8.08	9.24	74.67	3.20	0.06	0.58
12.10	1.13	8.30	9.02	74.90	3.18	0.06	0.59
12.12	1.14	8.40	9.01	75.73	3.18	0.06	0.60
12.14	1.15	8.46	9.06	76.69	3.19	0.06	0.60
12.16	1.15	8.46	9.17	77.62	3.19	0.06	0.60
12.18	1.15	8.42	9.34	78.68	3.21	0.06	0.60
12.20	1.15	8.41	9.46	79.52	3.22	0.06	0.60
12.22	1.14	8.37	9.54	79.89	3.22	0.06	0.60
12.24	1.14	8.34	9.56	79.75	3.22	0.06	0.60
12.26	1.14	8.33	9.54	79.45	3.22	0.06	0.59
12.28	1.13	8.24	9.64	79.42	3.23	0.06	0.59
12.30	1.13	8.18	9.71	79.43	3.23	0.06	0.58
12.32	1.12	8.11	9.77	79.26	3.24	0.06	0.58
12.34	1.14	8.21	9.66	79.33	3.23	0.06	0.59
12.36	1.15	8.31	9.57	79.53	3.22	0.06	0.59
12.38	1.17	8.44	9.46	79.83	3.21	0.06	0.60
12.40	1.19	8.61	9.29	79.92	3.20	0.06	0.61
12.42	1.21	8.81	9.08	80.00	3.19	0.06	0.63
12.44	1.23	8.98	8.97	80.58	3.18	0.06	0.64
12.46	1.24	9.03	9.03	81.54	3.18	0.06	0.65
12.48	1.23	8.94	9.23	82.54	3.20	0.06	0.64

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	1.22	8.80	9.47	83.30	3.22	0.06	0.63
12.52	1.19	8.55	9.79	83.67	3.24	0.06	0.61
12.54	1.16	8.31	10.10	83.94	3.26	0.06	0.59
12.57	1.12	7.95	10.56	83.93	3.29	0.06	0.57
12.58	1.09	7.61	10.98	83.55	3.32	0.06	0.54
12.60	1.03	7.12	11.60	82.60	3.36	0.06	0.51
12.62	0.98	6.67	12.19	81.28	3.39	0.06	0.48
12.64	0.92	6.08	13.07	79.46	3.44	0.06	0.43
12.66	0.85	5.51	13.97	76.98	3.49	0.06	0.39
12.68	0.78	4.91	15.06	73.94	3.55	0.06	0.35
12.70	0.72	4.36	16.10	70.24	3.61	0.06	0.31
12.72	0.68	4.03	16.41	66.08	3.62	0.06	0.29
12.74	0.67	3.91	15.94	62.26	3.60	0.06	0.28
12.76	0.68	3.96	14.83	58.71	3.54	0.06	0.28
12.78	0.67	3.93	14.24	55.95	3.51	0.06	0.28
12.80	0.66	3.81	13.94	53.15	3.49	0.06	0.27
12.82	0.64	3.62	13.84	50.10	3.49	0.06	0.26
12.84	0.62	3.45	13.59	46.88	3.47	0.06	0.25
12.87	0.61	3.35	13.06	43.69	3.44	0.06	0.24
12.88	0.61	3.37	12.40	41.81	3.40	0.06	0.24
12.90	0.61	3.33	12.15	40.47	3.39	0.06	0.24
12.92	0.60	3.25	12.14	39.52	3.39	0.06	0.23
12.94	0.59	3.15	12.21	38.50	3.39	0.06	0.23
12.96	0.60	3.20	11.87	38.04	3.37	0.06	0.23
12.98	0.60	3.25	11.66	37.89	3.36	0.06	0.23
13.00	0.61	3.35	11.38	38.18	3.34	0.06	0.24
13.02	0.62	3.42	11.28	38.58	3.34	0.06	0.24
13.04	0.63	3.51	11.10	38.93	3.32	0.06	0.25
13.06	0.63	3.48	11.28	39.32	3.34	0.06	0.25
13.08	0.63	3.50	11.34	39.70	3.34	0.06	0.25
13.10	0.64	3.51	11.43	40.14	3.35	0.06	0.25
13.12	0.64	3.57	11.34	40.42	3.34	0.06	0.25
13.14	0.64	3.53	11.49	40.57	3.35	0.06	0.25
13.16	0.65	3.57	11.34	40.51	3.34	0.06	0.26
13.18	0.67	3.80	10.65	40.44	3.30	0.06	0.27
13.21	0.72	4.14	9.68	40.10	3.23	0.06	0.30
13.22	0.74	4.36	9.18	40.03	3.20	0.06	0.31
13.24	0.73	4.27	9.40	40.10	3.21	0.06	0.30
13.26	0.70	3.97	10.05	39.87	3.26	0.06	0.28
13.28	0.69	3.93	10.08	39.60	3.26	0.06	0.28
13.30	0.73	4.21	9.40	39.58	3.21	0.06	0.30
13.32	0.78	4.65	8.72	40.57	3.16	0.06	0.33
13.34	0.81	4.89	8.64	42.28	3.16	0.06	0.35
13.36	0.85	5.25	8.37	43.92	3.13	0.06	0.37
13.38	0.98	6.27	7.27	45.58	3.05	0.06	0.45
13.40	1.17	7.87	5.99	47.13	2.93	0.06	0.56
13.42	1.34	9.25	5.39	49.86	2.87	0.07	0.66
13.44	1.39	9.71	5.46	53.03	2.88	0.07	0.69

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	1.34	9.27	5.95	55.16	2.93	0.07	0.66
13.48	1.21	8.16	6.87	56.11	3.01	0.06	0.58
13.50	1.02	6.58	8.42	55.45	3.14	0.06	0.47
13.52	0.85	5.13	10.35	53.05	3.28	0.06	0.37
13.54	0.75	4.28	11.61	49.64	3.36	0.06	0.31
13.56	0.73	4.18	11.27	47.09	3.34	0.06	0.30
13.58	0.74	4.26	10.66	45.36	3.30	0.06	0.30
13.60	0.76	4.37	10.17	44.46	3.26	0.06	0.31
13.62	0.77	4.46	9.90	44.12	3.25	0.06	0.32
13.64	0.78	4.49	9.80	44.02	3.24	0.06	0.32
13.66	0.77	4.44	9.88	43.91	3.24	0.06	0.32
13.68	0.77	4.44	9.85	43.77	3.24	0.06	0.32
13.70	0.79	4.59	9.55	43.86	3.22	0.06	0.33
13.72	0.83	4.88	9.14	44.64	3.19	0.06	0.35
13.74	0.83	4.94	9.34	46.11	3.21	0.06	0.35
13.76	0.82	4.77	10.04	47.89	3.26	0.06	0.34
13.78	0.78	4.47	10.81	48.36	3.31	0.06	0.32
13.80	0.76	4.34	10.97	47.68	3.32	0.06	0.31
13.82	0.78	4.43	10.57	46.80	3.29	0.06	0.32
13.84	0.79	4.54	10.25	46.48	3.27	0.06	0.32
13.86	0.80	4.64	10.07	46.68	3.26	0.06	0.33
13.88	0.81	4.69	9.93	46.54	3.25	0.06	0.33
13.90	0.81	4.67	9.87	46.12	3.24	0.06	0.33
13.92	0.80	4.62	9.95	45.99	3.25	0.06	0.33
13.94	0.78	4.44	10.38	46.09	3.28	0.06	0.32
13.96	0.78	4.37	10.59	46.30	3.29	0.06	0.31
13.98	0.78	4.37	10.64	46.49	3.29	0.06	0.31
14.00	0.79	4.48	10.37	46.43	3.28	0.06	0.32
14.02	0.80	4.51	10.28	46.39	3.27	0.06	0.32
14.05	0.81	4.61	10.04	46.27	3.25	0.06	0.33
14.06	0.86	4.99	9.33	46.57	3.21	0.06	0.36
14.08	0.95	5.76	8.11	46.74	3.11	0.06	0.41
14.10	1.06	6.58	7.11	46.82	3.03	0.06	0.47
14.12	1.14	7.24	6.67	48.32	2.99	0.06	0.52
14.14	1.21	7.83	6.33	49.55	2.96	0.06	0.56
14.16	1.25	8.09	6.51	52.67	2.98	0.06	0.58
14.18	1.25	8.09	6.84	55.35	3.01	0.06	0.58
14.20	1.20	7.65	7.69	58.87	3.08	0.06	0.55
14.22	1.13	7.15	8.52	60.90	3.15	0.06	0.51
14.24	1.05	6.48	9.61	62.22	3.23	0.06	0.46
14.26	0.97	5.84	10.63	62.15	3.29	0.06	0.42
14.28	1.00	6.06	10.33	62.59	3.27	0.06	0.43
14.30	1.19	7.59	8.32	63.12	3.13	0.06	0.54
14.32	1.51	10.10	6.19	62.48	2.95	0.07	0.72
14.34	1.74	11.88	5.26	62.48	2.85	0.07	0.85
14.36	1.72	11.73	5.45	63.95	2.87	0.07	0.84
14.38	1.47	9.75	6.76	65.89	3.00	0.06	0.70
14.40	1.17	7.35	8.69	63.86	3.16	0.06	0.52

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	1.06	6.42	9.47	60.80	3.22	0.06	0.46
14.44	1.25	7.93	7.60	60.29	3.07	0.06	0.57
14.46	1.67	11.22	5.44	60.97	2.87	0.07	0.80
14.48	2.08	14.58	4.33	63.09	2.74	0.08	1.03
14.50	2.35	16.79	3.90	65.55	2.69	0.08	1.18
14.52	2.47	17.77	3.84	68.25	2.68	0.08	1.25
14.54	2.49	17.87	3.88	69.31	2.68	0.08	1.26
14.56	2.38	16.91	4.12	69.67	2.72	0.08	1.19
14.58	2.12	14.73	4.82	70.96	2.80	0.08	1.05
14.60	1.75	11.75	6.09	71.53	2.94	0.07	0.84
14.62	1.37	8.77	7.93	69.57	3.10	0.06	0.63
14.64	1.07	6.43	10.16	65.33	3.26	0.06	0.46
14.66	0.94	5.38	11.58	62.26	3.35	0.06	0.38
14.68	0.90	5.06	12.26	62.06	3.40	0.06	0.36
14.70	1.02	6.04	10.69	64.53	3.30	0.06	0.43
14.72	1.09	6.53	10.03	65.53	3.25	0.06	0.47
14.74	1.09	6.54	9.89	64.74	3.25	0.06	0.47
14.76	0.98	5.68	10.88	61.80	3.31	0.06	0.41
14.78	0.91	5.13	11.50	58.97	3.35	0.06	0.37
14.80	0.89	4.97	11.58	57.57	3.35	0.06	0.36
14.82	0.88	4.87	11.69	56.92	3.36	0.06	0.35
14.85	0.87	4.77	11.87	56.57	3.37	0.06	0.34
14.86	0.86	4.67	11.98	55.97	3.38	0.06	0.33
14.88	0.87	4.73	11.61	54.92	3.36	0.06	0.34
14.90	0.94	5.32	10.30	54.74	3.27	0.06	0.38
14.92	1.10	6.54	8.39	54.94	3.14	0.06	0.47
14.94	1.29	7.95	6.90	54.90	3.01	0.06	0.57
14.96	1.40	8.79	6.33	55.68	2.96	0.06	0.63
14.98	1.42	8.91	6.44	57.39	2.97	0.06	0.64
15.00	1.41	8.82	6.83	60.17	3.01	0.06	0.63
15.03	1.46	9.20	6.79	62.46	3.00	0.06	0.66
15.04	1.51	9.59	6.87	65.88	3.01	0.07	0.68
15.06	1.50	9.50	7.25	68.91	3.04	0.06	0.68
15.08	1.38	8.55	8.38	71.60	3.14	0.06	0.61
15.10	1.25	7.57	9.48	71.71	3.22	0.06	0.54
15.12	1.15	6.76	10.38	70.22	3.28	0.06	0.48
15.14	1.05	6.01	11.37	68.33	3.34	0.06	0.43
15.16	0.94	5.20	12.66	65.90	3.42	0.06	0.37
15.18	0.86	4.60	13.76	63.27	3.48	0.06	0.33
15.20	0.84	4.43	13.65	60.45	3.48	0.06	0.32
15.23	0.85	4.47	12.93	57.86	3.44	0.06	0.32
15.24	0.87	4.62	12.12	56.00	3.39	0.06	0.33
15.26	0.90	4.84	11.28	54.59	3.34	0.06	0.35
15.28	0.93	5.05	10.51	53.05	3.29	0.06	0.36
15.30	0.94	5.15	10.06	51.84	3.26	0.06	0.37
15.32	0.95	5.20	9.87	51.31	3.24	0.06	0.37
15.34	0.95	5.17	9.98	51.61	3.25	0.06	0.37
15.36	0.93	5.04	10.33	52.07	3.27	0.06	0.36

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	0.90	4.79	10.94	52.36	3.31	0.06	0.34
15.40	0.88	4.61	11.32	52.20	3.34	0.06	0.33
15.42	0.87	4.57	11.36	51.86	3.34	0.06	0.33
15.44	0.89	4.68	10.96	51.26	3.32	0.06	0.33
15.46	0.90	4.78	10.58	50.64	3.29	0.06	0.34
15.48	0.93	4.97	10.12	50.37	3.26	0.06	0.36
15.50	1.03	5.72	8.92	51.00	3.18	0.06	0.41
15.52	1.24	7.28	7.17	52.22	3.04	0.06	0.52
15.54	1.47	8.96	5.94	53.22	2.92	0.07	0.64
15.56	1.61	9.99	5.60	55.90	2.89	0.07	0.71
15.58	1.60	9.91	5.97	59.09	2.93	0.07	0.71
15.60	1.60	9.89	6.23	61.60	2.95	0.06	0.71
15.62	1.61	9.93	6.28	62.39	2.96	0.07	0.71
15.64	1.53	9.32	6.97	65.01	3.02	0.06	0.67

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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LIQUEFACTION ANALYSIS REPORT

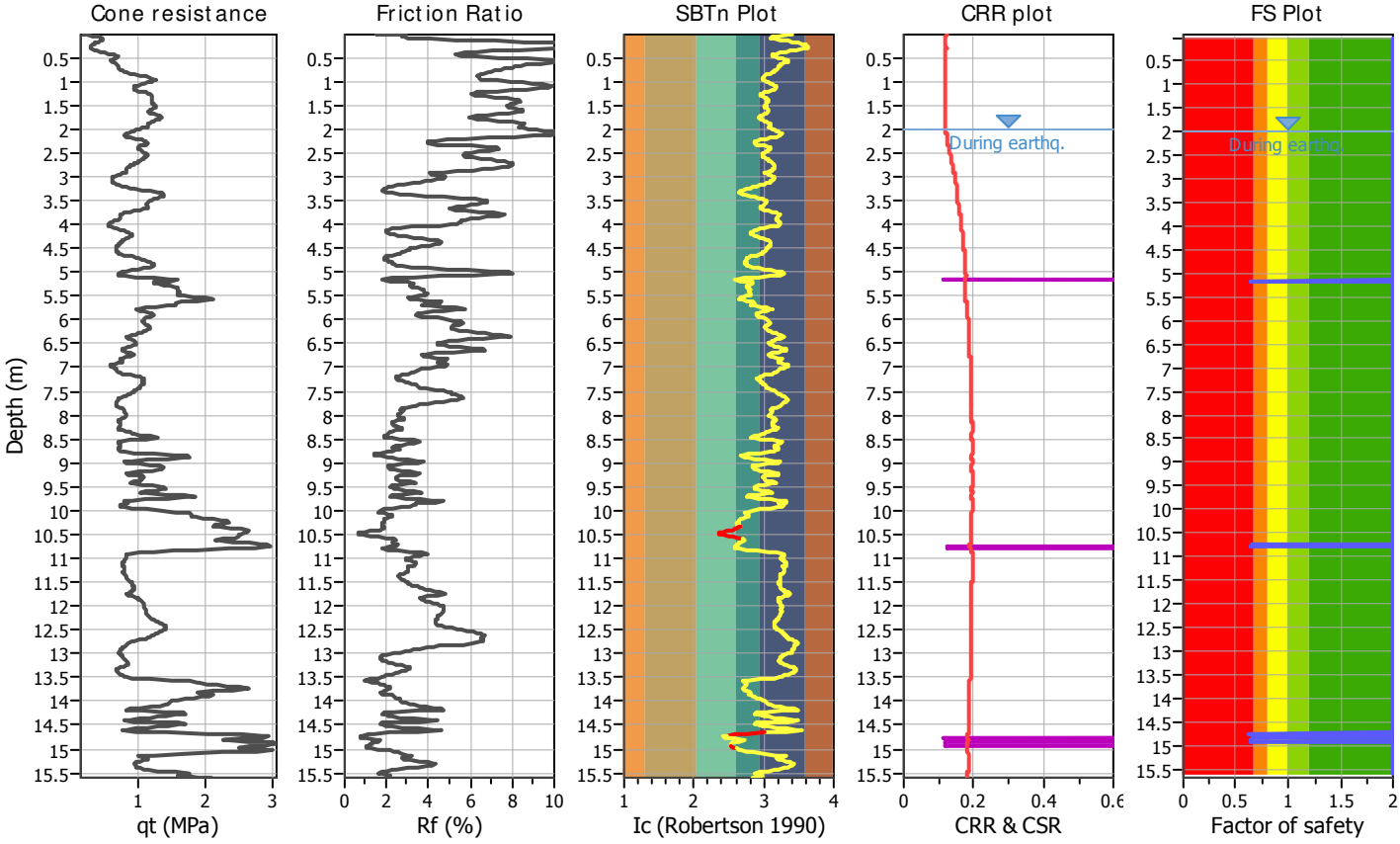
Project title :

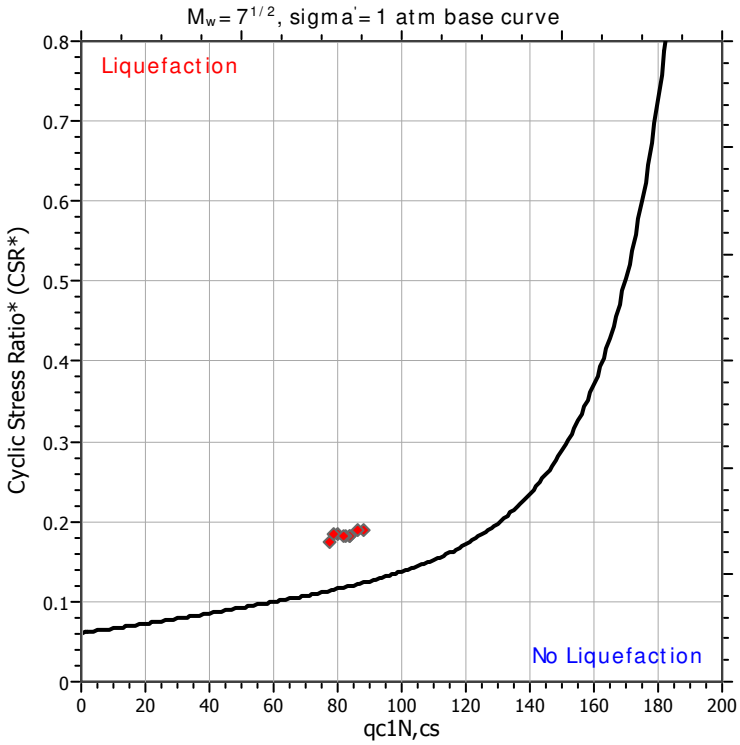
Location :

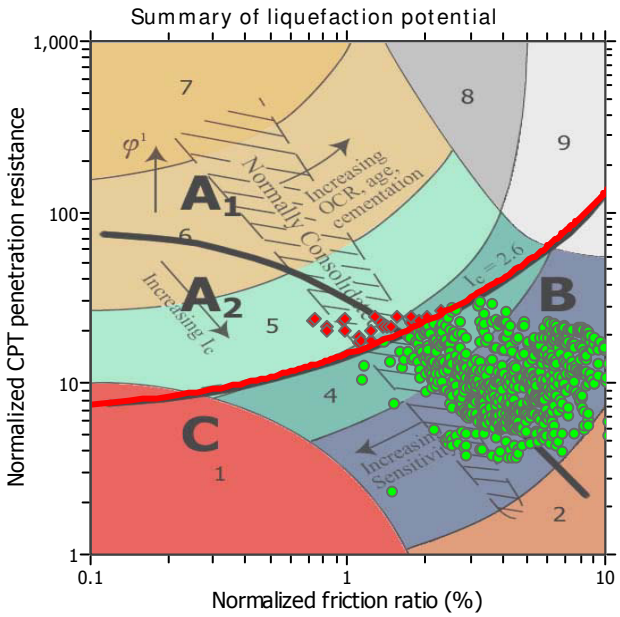
CPT file : Cptu-5

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.50 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.22	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

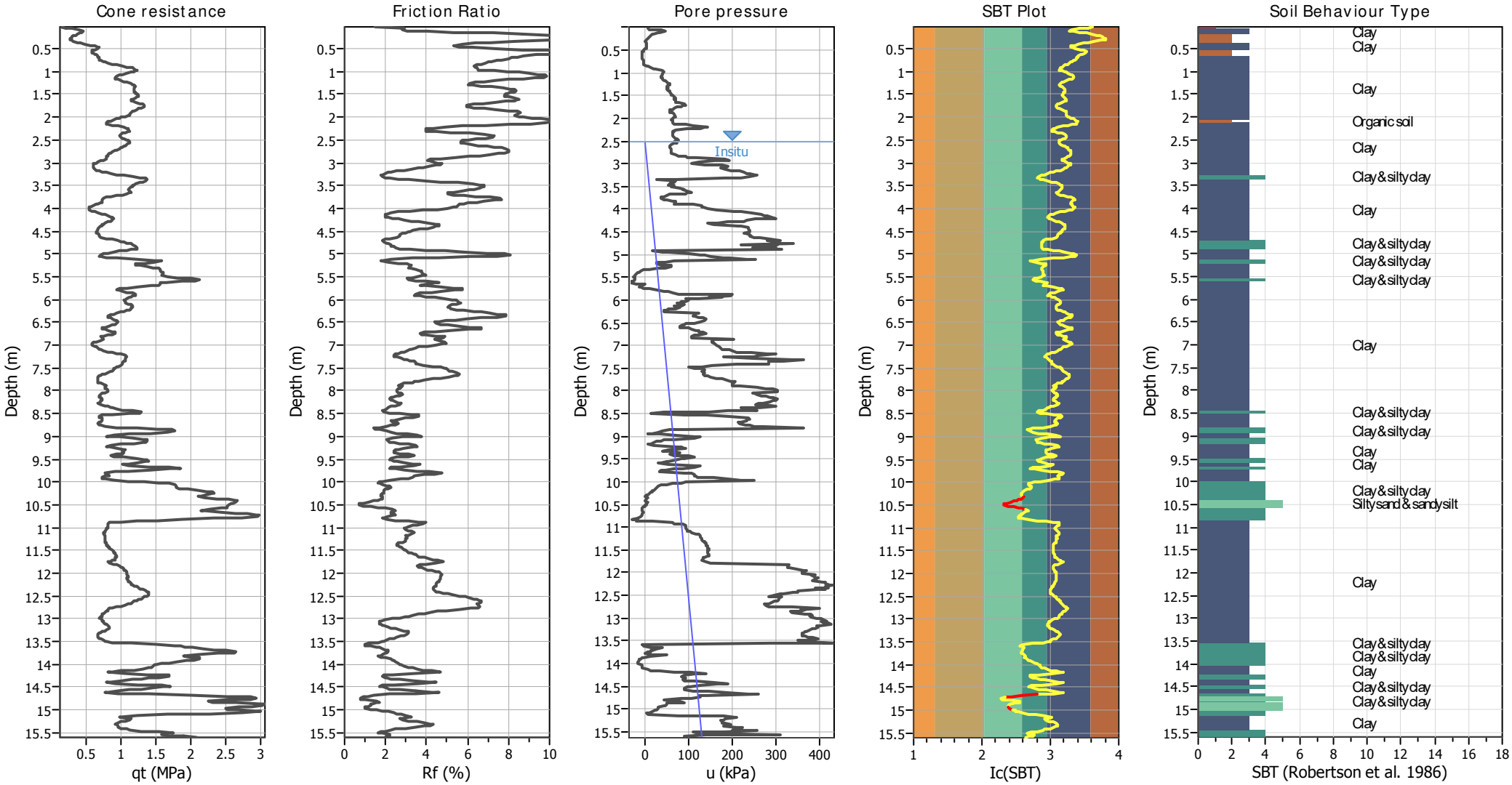






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



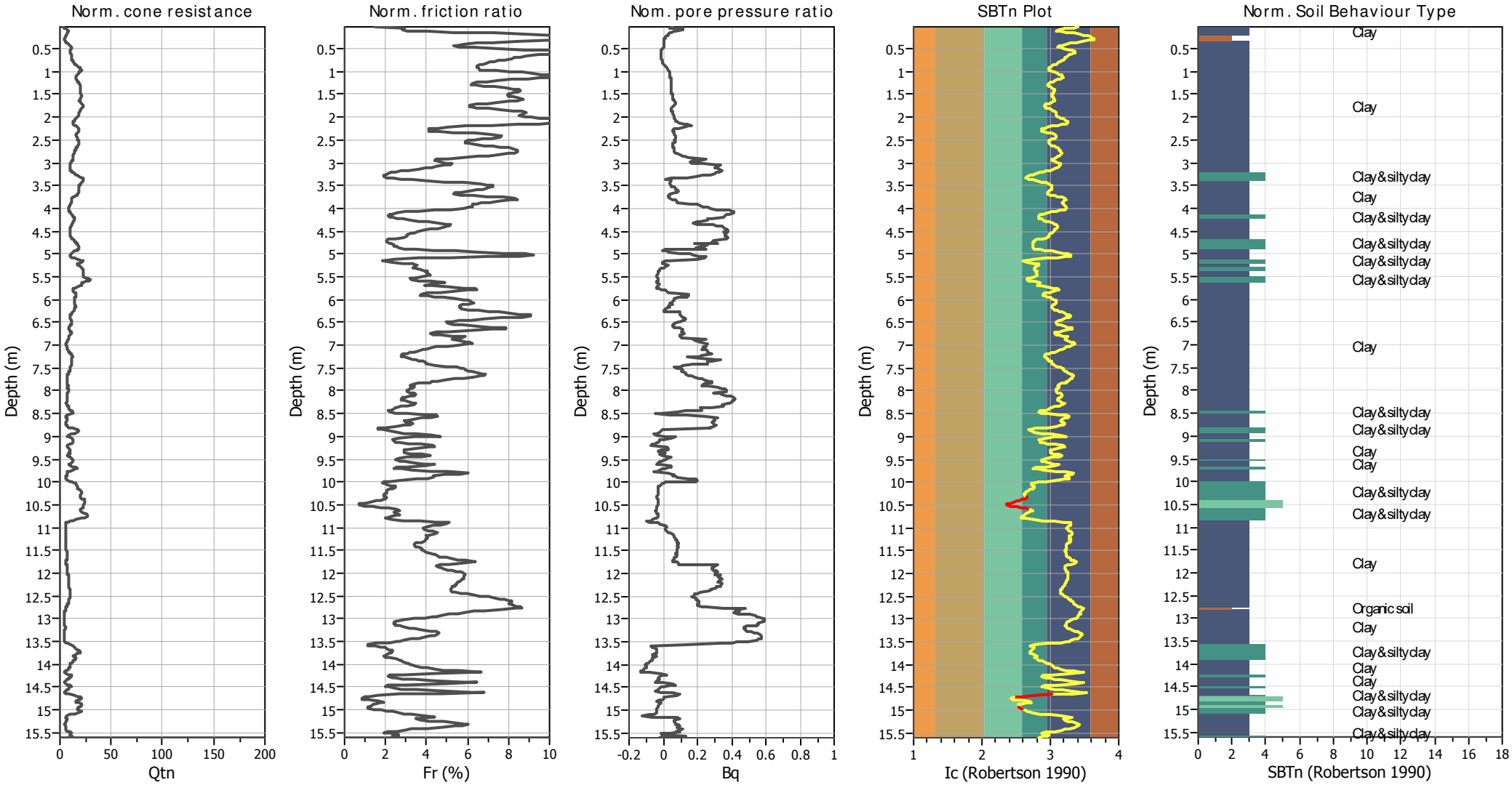
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



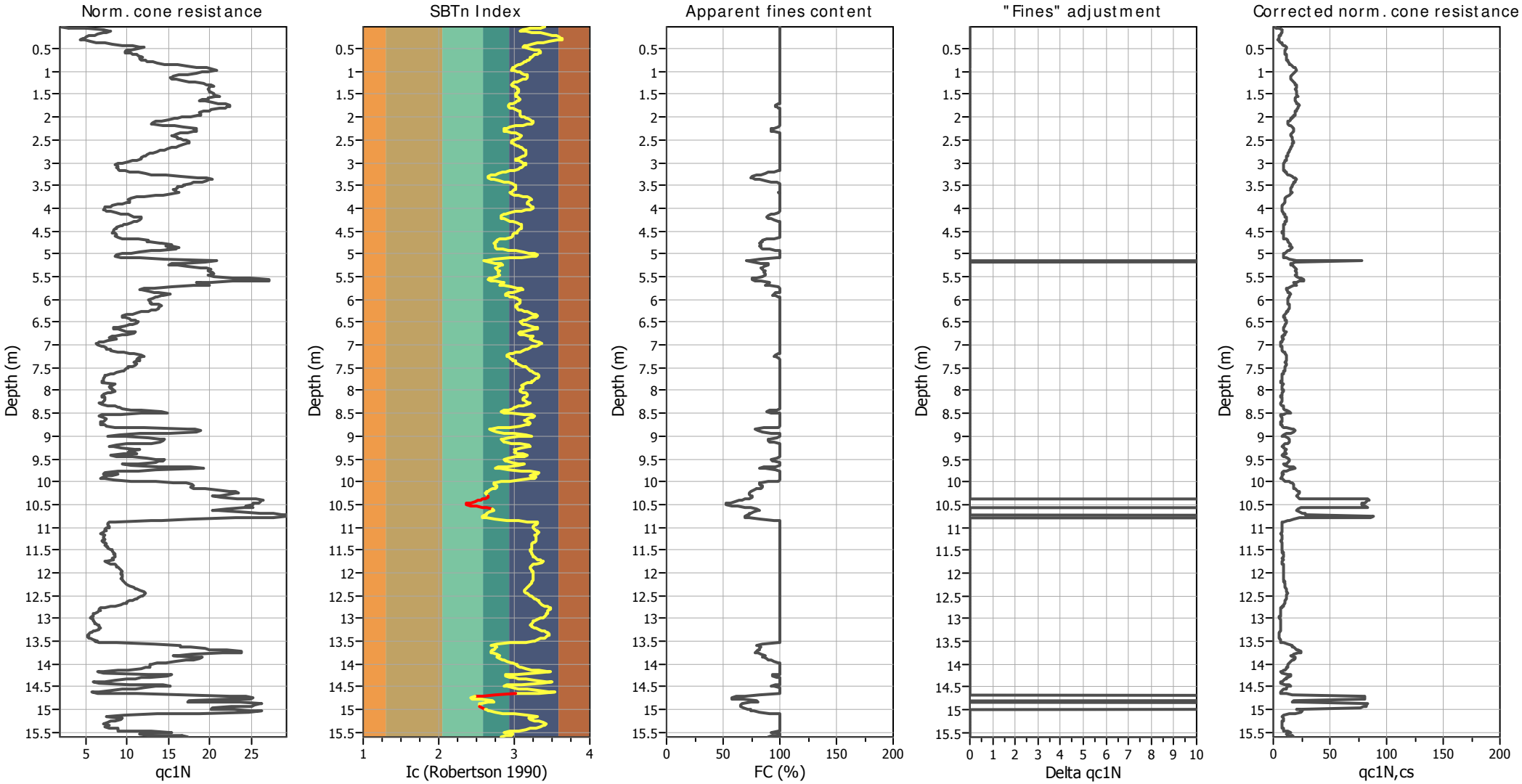
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

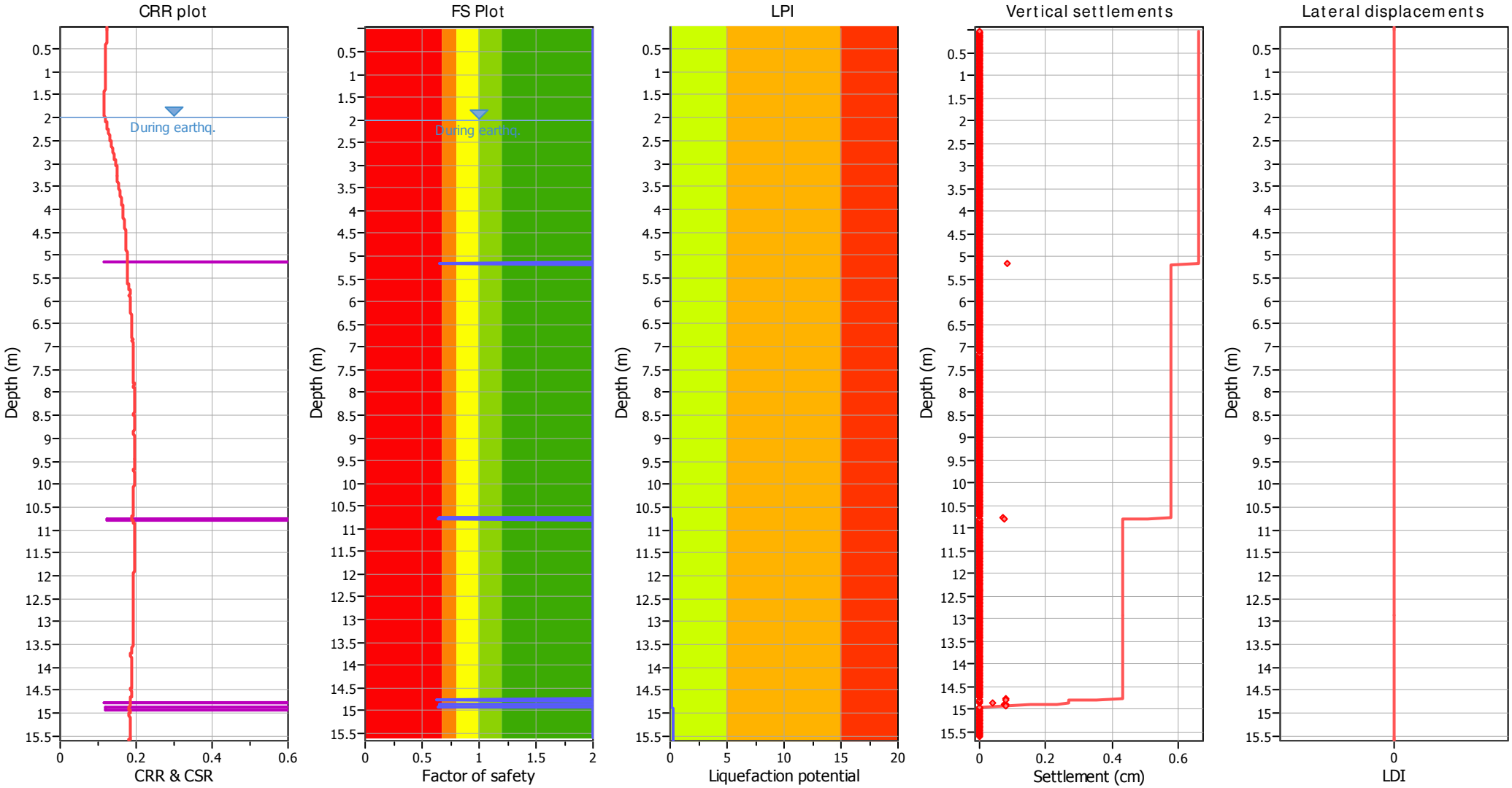
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

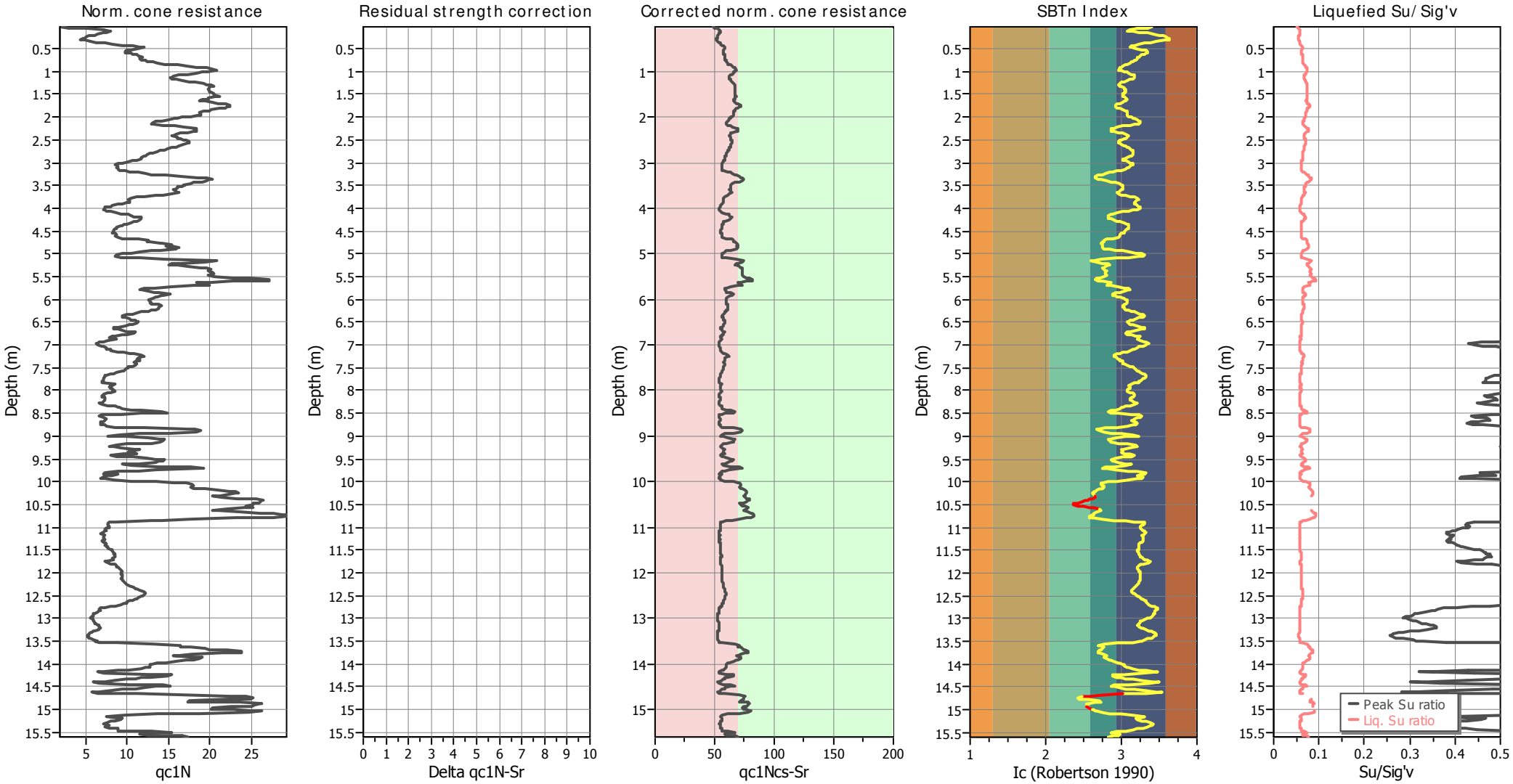
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

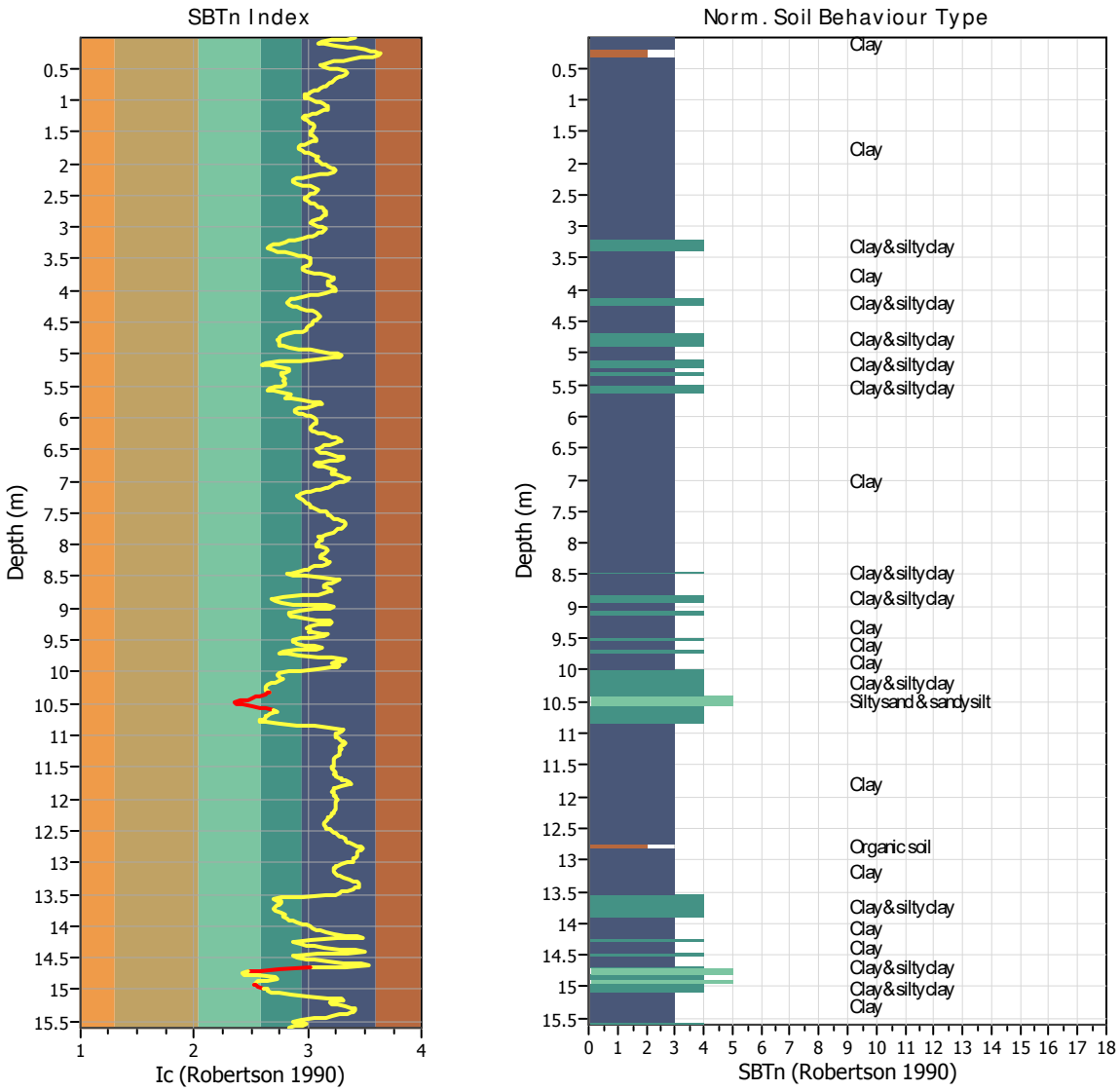
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	780
I_c maximum check value:	3.00	Total points excluded:	23
I_c change ratio value:	0.0100	Exclusion percentage:	2.95%
Minimum number of points in layer:	4	Number of layers detected:	4

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	8	Start depth: 10.34 (m)	4	Clay & silty clay
		End depth: 10.48 (m)	5	Silty sand & sandy silt
Transition layer 2	7	Start depth: 10.50 (m)	5	Silty sand & sandy silt
		End depth: 10.62 (m)	4	Clay & silty clay
Transition layer 3	4	Start depth: 14.68 (m)	4	Clay & silty clay
		End depth: 14.74 (m)	5	Silty sand & sandy silt
Transition layer 4	4	Start depth: 14.94 (m)	5	Silty sand & sandy silt
		End depth: 15.00 (m)	4	Clay & silty clay

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.11	0.33	7.01	90.49	13.73
2	0.04	0.18	5.42	8.00	85.16	14.56
3	0.06	0.30	8.50	36.14	74.32	15.00
4	0.08	0.43	11.64	45.88	66.90	15.46
5	0.11	0.47	14.60	33.48	64.47	15.75
6	0.12	0.48	16.41	29.63	69.25	16.08
7	0.14	0.44	25.76	19.65	75.74	16.35
8	0.16	0.43	30.15	15.81	84.87	16.58
9	0.18	0.38	34.99	12.52	91.38	16.68
10	0.20	0.36	36.07	10.73	98.84	16.72
11	0.22	0.32	37.60	8.06	100.00	16.71
12	0.24	0.30	37.25	4.96	100.00	16.69
13	0.26	0.29	35.99	3.53	100.00	16.62
14	0.28	0.28	33.38	1.49	100.00	16.55
15	0.30	0.25	32.94	0.19	100.00	16.47
16	0.32	0.28	28.73	0.50	100.00	16.41
17	0.34	0.33	27.27	1.12	96.07	16.37
18	0.36	0.37	26.39	0.93	87.91	16.41
19	0.38	0.43	27.36	1.24	81.63	16.47
20	0.40	0.49	28.48	2.17	75.56	16.57
21	0.42	0.57	29.77	3.53	70.68	16.70
22	0.44	0.64	32.91	3.35	67.37	16.84
23	0.46	0.69	37.28	2.17	66.56	17.02
24	0.48	0.72	43.58	0.06	68.47	17.19
25	0.50	0.68	49.39	-3.29	72.77	17.32
26	0.52	0.62	54.64	-5.77	78.30	17.41
27	0.54	0.59	59.65	-6.45	83.10	17.49
28	0.56	0.58	63.85	-7.19	85.60	17.55
29	0.58	0.59	65.23	-7.56	85.59	17.59
30	0.60	0.62	66.02	-6.94	84.02	17.61
31	0.62	0.64	64.33	-6.26	81.33	17.60
32	0.64	0.66	61.14	-6.82	79.13	17.57
33	0.66	0.67	59.15	-7.63	76.57	17.53
34	0.68	0.70	57.28	-7.25	75.51	17.51
35	0.70	0.68	56.37	-7.44	74.58	17.48
36	0.72	0.69	54.56	-5.89	74.29	17.45
37	0.74	0.70	53.88	-5.46	72.74	17.44
38	0.76	0.73	53.45	-5.46	71.34	17.45
39	0.78	0.74	53.74	-5.64	69.71	17.46
40	0.80	0.78	54.44	-4.77	68.28	17.49
41	0.82	0.81	55.27	-3.53	66.61	17.54
42	0.84	0.86	58.49	1.24	64.25	17.61
43	0.86	0.95	61.01	6.45	61.97	17.70
44	0.88	1.02	64.32	11.41	59.68	17.80
45	0.90	1.10	69.74	19.59	58.33	17.91
46	0.92	1.17	76.36	22.75	57.10	18.03
47	0.96	1.24	80.99	39.80	56.48	18.11
48	0.96	1.24	82.45	40.61	56.85	18.18

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.23	89.93	41.10	58.70	18.23
50	1.00	1.18	95.81	40.36	61.12	18.29
51	1.02	1.14	97.78	39.93	63.54	18.31
52	1.04	1.09	99.30	38.69	65.73	18.30
53	1.06	1.03	98.09	35.59	68.08	18.28
54	1.08	0.97	96.39	34.35	70.20	18.23
55	1.10	0.93	93.78	34.28	71.33	18.18
56	1.12	0.92	89.85	38.00	71.58	18.13
57	1.14	0.91	86.45	40.17	70.76	18.08
58	1.16	0.91	81.20	41.29	68.99	18.02
59	1.18	0.95	76.13	44.76	66.29	17.97
60	1.21	0.99	72.94	48.92	63.37	17.93
61	1.22	1.04	71.03	52.26	60.86	17.91
62	1.24	1.08	69.74	54.56	58.42	17.91
63	1.26	1.15	68.82	54.87	56.86	17.92
64	1.28	1.17	71.02	51.15	55.98	17.96
65	1.30	1.20	74.91	50.65	56.22	18.03
66	1.32	1.22	80.53	50.96	57.33	18.12
67	1.34	1.19	87.59	50.77	58.79	18.20
68	1.36	1.19	92.19	50.84	60.53	18.26
69	1.38	1.18	96.93	52.82	61.66	18.32
70	1.40	1.18	101.12	54.99	62.27	18.35
71	1.42	1.19	100.44	57.47	62.36	18.36
72	1.44	1.19	99.88	57.22	61.99	18.35
73	1.46	1.20	97.83	58.09	61.36	18.34
74	1.48	1.22	97.03	60.76	60.77	18.33
75	1.50	1.22	96.62	62.55	60.38	18.33
76	1.52	1.22	97.00	65.16	59.92	18.33
77	1.54	1.26	97.17	68.63	60.02	18.35
78	1.56	1.23	100.24	67.14	60.85	18.36
79	1.58	1.18	101.67	66.58	62.10	18.37
80	1.60	1.18	100.73	68.26	63.17	18.35
81	1.62	1.13	97.97	67.89	63.51	18.32
82	1.64	1.12	95.57	67.82	63.13	18.28
83	1.66	1.16	91.81	75.57	61.55	18.26
84	1.68	1.21	90.49	88.59	59.25	18.24
85	1.70	1.26	87.47	92.13	56.75	18.21
86	1.72	1.31	81.17	87.72	54.61	18.18
87	1.74	1.34	80.02	82.39	53.17	18.14
88	1.76	1.33	78.70	73.09	53.06	18.14
89	1.78	1.32	80.69	67.45	53.70	18.15
90	1.80	1.30	82.68	61.62	54.94	18.17
91	1.82	1.26	84.43	55.11	57.09	18.21
92	1.84	1.20	91.69	55.30	59.38	18.25
93	1.86	1.19	95.76	56.23	61.81	18.30
94	1.88	1.15	99.48	62.24	63.44	18.32
95	1.90	1.12	99.07	65.03	64.33	18.32
96	1.92	1.13	96.58	65.10	64.15	18.29

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.96	1.13	92.78	68.13	63.77	18.26
98	1.96	1.10	91.75	69.00	64.31	18.22
99	1.98	1.05	90.26	66.27	65.85	18.19
100	2.00	0.99	88.15	62.93	67.69	18.15
101	2.02	0.96	88.12	60.14	69.60	18.15
102	2.04	0.94	91.40	61.25	71.55	18.15
103	2.06	0.90	91.84	61.93	73.86	18.14
104	2.08	0.84	89.64	61.50	75.90	18.09
105	2.10	0.80	84.63	61.00	77.07	18.01
106	2.12	0.78	77.77	66.03	76.75	17.92
107	2.14	0.77	72.55	92.75	75.01	17.83
108	2.16	0.79	66.75	109.42	71.30	17.75
109	2.18	0.85	60.86	141.35	65.98	17.67
110	2.20	0.94	54.91	134.72	60.34	17.59
111	2.23	1.01	50.10	127.03	55.28	17.52
112	2.24	1.10	47.02	95.47	52.38	17.45
113	2.26	1.08	44.53	67.70	50.32	17.40
114	2.28	1.11	42.13	62.99	49.97	17.39
115	2.30	1.13	45.73	64.97	50.05	17.42
116	2.32	1.11	47.40	62.62	52.25	17.52
117	2.34	1.06	55.40	61.69	55.68	17.63
118	2.36	1.02	63.31	62.24	59.76	17.76
119	2.38	0.99	69.37	64.04	62.85	17.84
120	2.40	0.96	70.66	64.10	64.74	17.89
121	2.42	0.96	73.71	66.27	64.72	17.91
122	2.44	1.01	73.38	70.92	64.04	17.93
123	2.46	1.01	71.80	72.85	62.23	17.91
124	2.48	1.05	68.46	74.64	60.56	17.86
125	2.50	1.07	63.74	67.02	58.70	17.83
126	2.52	1.09	64.03	65.84	57.29	17.81
127	2.54	1.12	63.86	74.33	56.48	17.81
128	2.56	1.13	63.01	66.77	56.37	17.82
129	2.58	1.11	64.79	58.03	57.13	17.83
130	2.60	1.09	66.49	56.42	58.84	17.86
131	2.62	1.05	70.33	54.68	60.55	17.90
132	2.64	1.05	73.29	54.99	62.27	17.94
133	2.66	1.02	75.31	58.09	63.73	17.97
134	2.68	0.99	76.95	59.95	65.45	17.98
135	2.70	0.96	77.65	58.46	66.77	17.97
136	2.72	0.94	75.80	58.90	68.04	17.95
137	2.74	0.90	73.87	59.45	68.85	17.90
138	2.76	0.88	71.35	59.33	69.79	17.85
139	2.78	0.85	67.98	58.90	69.99	17.78
140	2.80	0.83	63.58	70.24	69.90	17.70
141	2.82	0.81	59.22	76.88	69.04	17.60
142	2.84	0.80	53.80	92.31	67.93	17.50
143	2.86	0.79	48.67	94.61	66.66	17.38
144	2.88	0.77	44.80	114.63	64.26	17.23

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.91	0.77	35.79	184.50	61.69	17.08
146	2.92	0.77	32.92	191.51	59.88	16.93
147	2.94	0.73	31.02	159.45	60.28	16.84
148	2.96	0.70	29.52	122.32	62.05	16.77
149	2.98	0.66	29.23	105.95	64.53	16.73
150	3.00	0.62	29.73	105.33	67.28	16.71
151	3.02	0.58	29.35	135.03	69.67	16.69
152	3.04	0.56	29.00	176.13	69.78	16.64
153	3.06	0.57	26.77	189.96	68.55	16.58
154	3.08	0.58	25.01	183.20	66.74	16.51
155	3.10	0.58	23.81	174.21	65.44	16.45
156	3.12	0.58	22.70	184.38	64.11	16.39
157	3.14	0.59	21.09	195.78	61.81	16.30
158	3.16	0.60	18.27	215.81	58.52	16.21
159	3.18	0.65	17.31	227.96	54.96	16.14
160	3.21	0.69	16.78	232.49	51.49	16.13
161	3.22	0.76	16.93	240.86	48.46	16.16
162	3.24	0.82	16.96	252.63	45.85	16.20
163	3.26	0.87	17.31	255.42	43.05	16.26
164	3.28	0.99	18.19	239.31	40.50	16.37
165	3.30	1.12	20.62	218.78	38.43	16.57
166	3.32	1.26	25.52	183.26	37.66	16.79
167	3.34	1.35	29.44	72.04	38.06	17.03
168	3.36	1.40	35.92	26.29	39.97	17.26
169	3.38	1.38	44.91	69.31	42.46	17.46
170	3.40	1.36	50.74	67.14	46.09	17.67
171	3.42	1.32	63.20	60.14	50.08	17.84
172	3.44	1.25	72.28	54.37	53.77	17.98
173	3.46	1.23	76.18	53.50	57.09	18.05
174	3.48	1.16	80.75	65.59	58.62	18.09
175	3.50	1.18	80.57	61.50	59.86	18.10
176	3.52	1.16	79.69	60.20	60.16	18.08
177	3.54	1.12	78.40	80.97	60.31	18.04
178	3.56	1.12	74.30	90.14	60.14	17.99
179	3.58	1.10	70.70	86.61	59.56	17.94
180	3.60	1.09	68.15	97.40	58.74	17.88
181	3.62	1.11	65.13	106.20	57.56	17.83
182	3.64	1.12	61.58	97.40	55.73	17.77
183	3.66	1.14	56.72	93.24	55.01	17.69
184	3.68	1.08	53.90	54.49	55.68	17.63
185	3.70	1.01	53.90	47.68	58.29	17.59
186	3.72	0.95	54.66	41.35	62.19	17.57
187	3.74	0.85	55.77	34.97	66.52	17.55
188	3.76	0.79	56.24	36.64	71.11	17.54
189	3.78	0.74	57.73	41.10	74.35	17.53
190	3.80	0.71	57.18	49.60	75.54	17.51
191	3.82	0.72	54.04	63.48	74.63	17.46
192	3.84	0.73	50.64	70.30	72.52	17.38

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	0.73	46.54	68.75	71.54	17.31
194	3.88	0.70	45.10	66.03	70.91	17.19
195	3.90	0.66	37.94	111.10	71.52	17.08
196	3.92	0.62	36.13	129.94	72.53	16.94
197	3.94	0.57	33.84	130.69	74.17	16.86
198	3.96	0.56	32.11	134.35	75.83	16.76
199	3.98	0.52	29.45	141.60	76.45	16.67
200	4.00	0.51	27.98	144.51	76.41	16.56
201	4.02	0.51	24.94	162.24	73.91	16.44
202	4.05	0.51	20.75	202.36	69.87	16.28
203	4.06	0.53	18.17	221.02	64.89	16.14
204	4.08	0.57	16.59	242.22	59.73	16.04
205	4.10	0.63	15.15	266.34	55.28	15.99
206	4.12	0.67	14.68	268.01	51.63	16.00
207	4.14	0.73	15.86	273.40	49.46	16.04
208	4.16	0.76	15.91	281.53	47.94	16.10
209	4.18	0.78	16.21	288.53	47.12	16.19
210	4.20	0.84	19.20	301.30	47.29	16.31
211	4.22	0.85	21.02	252.63	48.04	16.44
212	4.24	0.85	22.39	231.62	49.78	16.56
213	4.26	0.84	25.97	225.36	51.95	16.66
214	4.28	0.81	27.76	189.52	54.81	16.76
215	4.30	0.78	30.07	167.51	57.73	16.82
216	4.32	0.76	31.63	142.03	60.89	16.88
217	4.34	0.72	34.50	157.78	63.49	16.93
218	4.36	0.70	35.26	212.28	65.00	16.94
219	4.38	0.69	33.39	220.15	65.39	16.91
220	4.40	0.67	32.30	236.33	65.64	16.85
221	4.42	0.64	30.58	236.95	65.52	16.76
222	4.44	0.64	27.12	237.38	64.96	16.66
223	4.46	0.63	24.92	239.49	63.57	16.53
224	4.48	0.62	22.31	241.35	62.20	16.42
225	4.50	0.62	20.32	241.04	61.42	16.33
226	4.52	0.61	20.21	226.22	61.25	16.30
227	4.54	0.61	20.70	230.01	60.64	16.28
228	4.56	0.64	19.15	239.62	59.13	16.25
229	4.58	0.65	18.16	243.52	57.76	16.21
230	4.60	0.64	18.39	240.11	57.69	16.20
231	4.62	0.64	18.86	248.67	57.66	16.21
232	4.64	0.66	18.63	263.30	56.01	16.21
233	4.66	0.70	17.51	286.55	51.43	16.21
234	4.68	0.85	16.99	311.78	46.88	16.23
235	4.70	0.95	17.66	281.71	44.44	16.30
236	4.72	0.93	19.22	299.07	43.86	16.37
237	4.74	0.96	19.77	299.57	43.33	16.45
238	4.76	1.05	21.09	341.17	43.31	16.59
239	4.78	1.07	25.72	218.35	42.53	16.71
240	4.80	1.16	26.16	304.28	43.13	16.81

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	1.11	27.10	277.99	42.64	16.86
242	4.84	1.16	28.65	300.56	42.98	16.94
243	4.86	1.23	31.64	245.82	43.29	16.99
244	4.88	1.13	30.46	313.76	44.65	17.10
245	4.90	1.21	37.50	39.93	48.48	17.20
246	4.93	1.07	43.62	15.44	53.28	17.36
247	4.94	0.98	48.63	39.68	59.84	17.44
248	4.96	0.88	52.20	51.64	65.90	17.51
249	4.98	0.80	57.19	98.45	72.46	17.56
250	5.00	0.72	61.11	126.78	78.01	17.56
251	5.02	0.66	57.63	135.40	80.93	17.50
252	5.04	0.66	52.15	151.21	80.02	17.37
253	5.06	0.66	43.77	180.41	74.79	17.20
254	5.08	0.71	35.44	194.17	65.27	17.04
255	5.10	0.89	30.37	233.97	54.22	16.94
256	5.12	1.12	28.53	251.83	42.63	16.90
257	5.14	1.61	24.54	67.45	36.68	16.92
258	5.16	1.63	27.53	45.38	34.89	17.00
259	5.18	1.51	31.63	24.80	38.80	17.12
260	5.20	1.28	36.82	25.05	43.48	17.19
261	5.22	1.20	36.88	36.33	47.54	17.23
262	5.24	1.17	38.81	60.26	48.25	17.28
263	5.26	1.27	41.56	59.76	47.66	17.38
264	5.29	1.36	44.96	47.37	45.64	17.46
265	5.30	1.49	44.64	28.83	44.18	17.55
266	5.32	1.55	48.95	9.80	43.60	17.65
267	5.34	1.60	55.36	-4.15	44.47	17.76
268	5.36	1.57	59.49	-9.67	45.45	17.84
269	5.38	1.57	59.99	-13.95	45.89	17.87
270	5.40	1.60	59.58	-17.30	45.60	17.87
271	5.42	1.61	59.05	-19.84	45.32	17.89
272	5.44	1.64	62.22	-21.45	45.88	17.92
273	5.46	1.59	64.71	-24.12	46.43	17.93
274	5.48	1.58	62.01	-24.61	46.14	17.91
275	5.50	1.64	58.35	-26.53	43.94	17.89
276	5.52	1.83	58.73	-23.56	41.03	17.90
277	5.54	2.01	59.29	-25.48	38.56	17.99
278	5.56	2.20	66.05	-25.29	37.92	18.11
279	5.58	2.21	75.55	-28.58	39.86	18.19
280	5.60	1.84	74.99	-32.11	43.66	18.20
281	5.62	1.63	74.20	-34.35	48.71	18.15
282	5.64	1.48	76.63	-21.02	49.42	18.05
283	5.66	1.60	59.55	0.00	47.67	17.92
284	5.68	1.61	51.58	-7.87	46.36	17.80
285	5.70	1.45	59.31	-12.77	49.33	17.78
286	5.72	1.25	59.90	-11.47	55.35	17.76
287	5.74	1.07	57.32	-5.64	61.33	17.70
288	5.76	0.97	57.70	10.23	65.81	17.64

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	0.93	56.03	24.80	67.13	17.58
290	5.80	0.94	50.78	43.83	65.31	17.52
291	5.82	1.01	49.40	51.33	61.45	17.46
292	5.84	1.08	45.53	63.05	57.69	17.42
293	5.86	1.12	43.22	76.69	53.23	17.37
294	5.88	1.23	39.55	198.26	51.59	17.35
295	5.90	1.17	42.45	196.71	51.08	17.35
296	5.93	1.15	42.45	147.24	53.41	17.40
297	5.94	1.12	46.50	177.68	55.29	17.45
298	5.96	1.10	49.54	123.43	57.80	17.52
299	5.98	1.07	52.41	93.49	60.48	17.59
300	6.01	1.03	57.01	99.94	62.67	17.64
301	6.02	1.04	58.01	93.99	63.81	17.67
302	6.04	1.04	57.89	84.00	64.01	17.70
303	6.06	1.06	60.79	77.99	64.19	17.72
304	6.08	1.05	60.50	73.78	64.23	17.75
305	6.10	1.07	61.76	90.45	62.90	17.75
306	6.12	1.14	59.65	81.71	61.12	17.75
307	6.14	1.17	58.25	67.39	60.06	17.75
308	6.16	1.15	60.24	78.49	60.00	17.74
309	6.18	1.15	59.21	68.07	60.47	17.75
310	6.20	1.15	59.12	53.44	61.00	17.74
311	6.22	1.12	60.32	48.85	62.74	17.76
312	6.24	1.07	63.55	43.83	65.19	17.80
313	6.26	1.04	67.03	44.08	68.06	17.82
314	6.28	0.97	67.41	122.94	70.62	17.83
315	6.30	0.93	66.68	117.92	73.42	17.81
316	6.32	0.89	67.94	112.90	76.45	17.80
317	6.34	0.83	68.20	110.35	79.70	17.77
318	6.36	0.78	65.95	112.65	81.09	17.72
319	6.38	0.79	61.05	121.57	79.95	17.65
320	6.40	0.82	57.01	132.18	76.04	17.57
321	6.42	0.87	52.26	138.31	72.46	17.51
322	6.44	0.89	49.24	137.01	69.23	17.45
323	6.46	0.92	47.31	135.28	66.80	17.39
324	6.48	0.95	43.94	124.80	64.83	17.34
325	6.50	0.95	42.77	114.14	63.69	17.30
326	6.52	0.95	41.74	91.13	64.59	17.28
327	6.54	0.89	42.85	91.01	66.61	17.29
328	6.56	0.87	44.82	85.24	69.64	17.30
329	6.58	0.83	45.17	79.23	73.37	17.32
330	6.60	0.76	47.51	80.78	77.94	17.34
331	6.62	0.71	50.06	100.93	81.87	17.36
332	6.64	0.71	50.77	105.46	81.96	17.37
333	6.66	0.75	48.04	115.00	78.50	17.32
334	6.68	0.80	42.65	122.50	73.10	17.23
335	6.70	0.85	37.76	121.57	67.22	17.14
336	6.72	0.93	35.59	133.79	63.48	17.09

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	0.93	35.15	140.48	62.34	17.03
338	6.76	0.86	32.20	123.37	64.34	16.97
339	6.78	0.80	32.40	111.53	68.10	16.93
340	6.80	0.74	33.63	105.95	72.67	16.94
341	6.82	0.70	36.09	104.96	76.98	16.98
342	6.84	0.67	37.27	105.77	75.81	16.97
343	6.86	0.76	32.55	202.54	73.85	16.95
344	6.88	0.75	33.73	155.18	73.25	16.91
345	6.90	0.66	33.32	153.32	76.88	16.87
346	6.92	0.62	31.44	156.23	81.46	16.79
347	6.94	0.57	29.71	152.70	84.03	16.72
348	6.96	0.56	29.42	160.20	86.02	16.66
349	6.98	0.55	28.31	164.23	85.72	16.63
350	7.00	0.56	26.96	163.36	82.96	16.57
351	7.02	0.60	24.97	168.63	79.44	16.52
352	7.04	0.61	23.83	171.23	75.33	16.47
353	7.06	0.65	22.68	174.64	73.41	16.45
354	7.09	0.65	23.01	176.07	71.06	16.45
355	7.10	0.69	23.12	194.48	69.64	16.47
356	7.14	0.70	22.80	209.05	66.61	16.50
357	7.15	0.77	23.39	226.35	63.53	16.55
358	7.16	0.84	24.56	243.21	60.03	16.61
359	7.18	0.90	25.15	279.98	57.23	16.66
360	7.20	0.94	24.86	299.07	54.56	16.71
361	7.22	1.03	25.74	260.57	52.74	16.75
362	7.24	1.06	26.88	249.04	52.31	16.80
363	7.26	1.04	27.32	180.78	53.39	16.85
364	7.28	1.01	29.37	246.93	55.25	16.90
365	7.31	0.98	31.75	336.08	56.14	16.97
366	7.32	1.02	32.51	363.24	56.67	17.03
367	7.34	1.01	33.80	316.24	57.56	17.07
368	7.36	0.98	35.85	283.82	59.34	17.10
369	7.38	0.95	35.70	284.31	60.31	17.12
370	7.40	0.99	36.23	283.38	60.43	17.11
371	7.42	0.99	35.50	208.25	60.94	17.14
372	7.44	0.97	37.87	151.46	63.19	17.19
373	7.46	0.94	42.01	128.08	66.60	17.26
374	7.48	0.90	44.70	100.81	69.28	17.32
375	7.50	0.90	45.23	112.46	70.78	17.34
376	7.52	0.89	45.55	132.86	71.56	17.35
377	7.54	0.87	45.87	136.27	72.29	17.34
378	7.56	0.86	45.05	132.36	73.32	17.32
379	7.58	0.84	44.41	127.90	75.13	17.30
380	7.60	0.78	44.85	137.51	77.62	17.27
381	7.62	0.75	43.56	134.28	80.27	17.23
382	7.64	0.72	41.69	132.86	82.25	17.16
383	7.66	0.68	39.66	137.07	83.70	17.09
384	7.68	0.66	37.47	142.84	84.14	17.01

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	0.65	34.57	149.23	83.51	16.92
386	7.72	0.64	31.96	163.05	82.11	16.82
387	7.74	0.64	29.14	175.08	80.38	16.72
388	7.76	0.64	26.36	185.00	78.58	16.61
389	7.78	0.64	24.46	195.97	76.96	16.52
390	7.80	0.63	22.73	205.33	75.86	16.45
391	7.82	0.64	22.35	204.53	75.56	16.42
392	7.84	0.63	22.32	199.57	70.51	16.37
393	7.86	0.78	18.61	199.50	67.71	16.37
394	7.88	0.75	21.52	199.38	65.23	16.39
395	7.90	0.73	22.07	217.67	67.27	16.43
396	7.92	0.72	21.75	258.03	67.15	16.43
397	7.94	0.73	21.02	275.57	66.16	16.42
398	7.96	0.75	21.22	294.61	65.08	16.41
399	7.98	0.75	21.08	302.11	64.40	16.42
400	8.00	0.76	20.90	304.28	63.74	16.41
401	8.02	0.78	20.67	304.53	64.21	16.39
402	8.04	0.73	20.38	247.30	66.13	16.39
403	8.06	0.69	21.25	251.33	69.28	16.36
404	8.08	0.66	20.55	255.92	70.92	16.32
405	8.10	0.65	18.97	265.41	71.17	16.25
406	8.12	0.64	17.86	277.43	70.37	16.16
407	8.14	0.63	16.36	285.68	68.81	16.09
408	8.16	0.67	15.78	293.37	67.36	16.06
409	8.19	0.67	16.48	302.23	66.36	16.07
410	8.20	0.67	16.39	301.36	66.55	16.09
411	8.22	0.67	16.60	293.30	67.44	16.12
412	8.24	0.66	17.68	285.37	69.37	16.16
413	8.26	0.63	18.53	270.49	71.87	16.20
414	8.28	0.62	18.94	260.32	73.17	16.23
415	8.30	0.64	19.33	252.20	71.31	16.25
416	8.32	0.71	19.27	272.04	66.82	16.28
417	8.34	0.79	18.89	300.68	62.86	16.30
418	8.36	0.82	18.74	263.55	60.20	16.30
419	8.38	0.85	18.42	219.34	59.11	16.32
420	8.40	0.87	19.21	238.93	56.81	16.36
421	8.42	0.97	19.68	256.85	53.68	16.43
422	8.44	1.09	20.38	190.20	49.37	16.57
423	8.46	1.31	24.25	147.24	47.35	16.78
424	8.48	1.38	29.70	41.97	49.66	16.93
425	8.50	1.10	31.31	13.58	56.17	16.95
426	8.52	0.86	29.26	89.34	67.31	16.82
427	8.54	0.66	26.60	138.44	76.02	16.65
428	8.56	0.62	24.16	190.82	79.11	16.53
429	8.58	0.67	23.14	235.09	76.81	16.46
430	8.60	0.67	21.94	235.03	73.31	16.42
431	8.62	0.70	20.68	238.69	71.14	16.32
432	8.64	0.69	17.45	234.04	68.93	16.20

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	0.69	16.17	233.23	68.61	16.11
434	8.68	0.67	16.66	219.78	70.19	16.10
435	8.70	0.64	17.60	213.70	72.54	16.14
436	8.72	0.64	18.13	216.49	73.69	16.15
437	8.74	0.64	17.69	228.95	71.90	16.14
438	8.76	0.69	16.64	240.86	69.03	16.11
439	8.78	0.71	15.82	249.47	64.39	16.10
440	8.80	0.81	16.37	270.74	55.10	16.15
441	8.82	1.14	15.73	362.06	45.04	16.38
442	8.84	1.64	21.04	92.44	40.27	16.73
443	8.86	1.73	30.24	56.29	39.54	17.10
444	8.88	1.80	37.48	39.37	41.45	17.33
445	8.90	1.75	40.06	29.57	44.41	17.37
446	8.93	1.44	37.04	15.13	49.95	17.28
447	8.94	1.09	33.64	7.32	58.91	17.10
448	8.96	0.87	32.32	31.56	69.41	16.93
449	8.99	0.72	29.48	69.37	75.59	16.81
450	9.00	0.75	28.02	113.39	72.76	16.76
451	9.02	0.93	27.93	124.86	62.57	16.81
452	9.04	1.21	28.01	112.34	53.91	16.86
453	9.06	1.33	26.34	65.65	49.02	16.91
454	9.08	1.39	28.54	41.91	47.85	16.94
455	9.10	1.37	29.19	34.72	48.40	16.99
456	9.12	1.34	29.57	25.23	49.38	17.02
457	9.14	1.34	31.15	20.71	51.41	17.06
458	9.16	1.24	33.35	13.70	56.28	17.04
459	9.18	0.96	31.44	7.38	63.47	16.96
460	9.20	0.84	29.60	18.23	72.02	16.84
461	9.22	0.75	28.86	71.73	74.53	16.77
462	9.24	0.81	27.87	81.96	72.53	16.76
463	9.26	0.89	28.10	90.14	65.42	16.79
464	9.28	1.07	27.13	91.94	60.06	16.80
465	9.30	1.11	25.87	53.13	58.14	16.77
466	9.32	1.00	25.58	39.68	59.20	16.72
467	9.34	0.97	24.61	61.75	59.85	16.70
468	9.36	1.05	25.05	78.67	58.87	16.73
469	9.38	1.08	26.95	72.23	60.96	16.82
470	9.40	0.93	31.17	54.31	66.76	16.85
471	9.42	0.78	30.03	64.85	71.42	16.83
472	9.44	0.86	27.69	97.89	68.15	16.80
473	9.46	1.04	27.36	112.59	59.83	16.81
474	9.48	1.22	26.75	91.07	53.88	16.89
475	9.50	1.32	29.41	82.64	50.39	16.97
476	9.52	1.42	30.97	69.75	49.75	17.07
477	9.54	1.39	33.11	51.33	50.62	17.16
478	9.56	1.36	36.65	48.48	52.31	17.18
479	9.58	1.31	34.04	37.45	56.51	17.21
480	9.60	1.10	38.61	30.38	62.79	17.19

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	0.92	38.67	53.38	67.58	17.19
482	9.64	1.03	37.41	116.86	63.13	17.21
483	9.66	1.35	37.41	127.77	52.70	17.28
484	9.68	1.73	37.47	114.07	45.47	17.38
485	9.70	1.90	39.90	85.62	42.79	17.48
486	9.72	1.86	44.06	67.58	46.53	17.52
487	9.74	1.33	44.44	44.45	53.19	17.42
488	9.76	1.11	37.00	35.96	64.59	17.27
489	9.78	0.88	38.05	33.17	74.54	17.14
490	9.80	0.72	38.73	88.90	83.75	17.06
491	9.82	0.71	34.95	104.77	81.86	16.98
492	9.84	0.88	30.30	112.71	77.81	16.89
493	9.86	0.81	30.24	111.84	74.51	16.78
494	9.88	0.76	25.58	116.24	77.60	16.67
495	9.90	0.70	24.52	118.16	79.50	16.54
496	9.92	0.67	23.03	156.97	78.56	16.46
497	9.94	0.73	20.77	189.21	73.34	16.42
498	9.96	0.84	20.57	218.23	64.27	16.44
499	9.98	1.03	21.16	250.65	54.54	16.51
500	10.00	1.34	20.36	92.99	47.70	16.68
501	10.03	1.55	26.08	81.46	43.36	16.86
502	10.04	1.71	28.45	62.74	42.25	17.08
503	10.06	1.78	33.46	47.74	42.20	17.23
504	10.08	1.80	37.33	37.14	43.31	17.38
505	10.10	1.80	41.20	27.71	44.38	17.45
506	10.12	1.77	41.14	27.34	44.66	17.47
507	10.14	1.80	39.12	25.36	43.31	17.45
508	10.16	1.95	37.74	22.13	41.05	17.46
509	10.18	2.11	40.06	19.28	38.97	17.53
510	10.20	2.25	43.16	17.11	37.67	17.61
511	10.22	2.33	44.22	15.19	37.10	17.68
512	10.24	2.36	46.27	11.72	36.73	17.68
513	10.26	2.33	43.22	9.67	36.55	17.62
514	10.28	2.25	37.92	6.88	36.66	17.51
515	10.30	2.13	36.22	1.55	37.59	17.45
516	10.32	2.05	38.21	-0.31	38.38	17.47
517	10.34	2.16	40.73	4.46	37.98	17.55
518	10.36	2.36	43.42	3.72	36.43	17.68
519	10.38	2.59	48.52	3.66	34.40	17.72
520	10.40	2.68	42.75	1.49	32.90	17.70
521	10.42	2.66	39.64	0.68	31.22	17.56
522	10.44	2.65	32.46	3.47	29.43	17.34
523	10.46	2.63	22.91	4.84	26.98	17.00
524	10.48	2.57	15.79	3.10	24.88	16.67
525	10.50	2.57	14.97	2.11	25.08	16.62
526	10.52	2.48	20.86	-2.29	27.56	16.92
527	10.54	2.50	31.23	-2.23	30.91	17.31
528	10.56	2.57	42.28	-2.79	33.93	17.62

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	2.47	49.75	-6.01	37.10	17.80
530	10.60	2.26	53.91	-8.25	40.64	17.87
531	10.62	2.07	54.85	-9.18	42.59	17.86
532	10.64	2.14	50.98	-7.63	41.60	17.86
533	10.66	2.42	52.62	-4.59	38.93	17.91
534	10.68	2.67	58.45	-5.83	37.33	18.07
535	10.70	2.84	69.55	-7.01	36.77	18.23
536	10.72	2.95	74.36	-7.56	36.68	18.34
537	10.74	3.00	76.44	-8.43	35.84	18.33
538	10.76	3.00	65.45	-9.61	34.59	18.18
539	10.78	2.84	48.69	-12.15	34.43	17.92
540	10.80	2.38	42.00	-16.92	36.97	17.63
541	10.82	1.82	36.70	-32.24	43.54	17.44
542	10.84	1.46	37.70	-18.29	51.70	17.35
543	10.86	1.33	41.21	-19.40	62.18	17.27
544	10.88	0.88	37.02	16.49	71.59	17.14
545	10.90	0.81	32.10	63.36	81.09	16.96
546	10.92	0.80	31.43	67.08	81.54	16.86
547	10.94	0.79	29.35	86.98	80.36	16.78
548	10.96	0.80	26.39	92.62	78.70	16.72
549	10.98	0.82	26.33	94.23	76.90	16.65
550	11.00	0.81	24.37	93.61	76.28	16.59
551	11.02	0.79	22.64	93.06	76.80	16.54
552	11.04	0.77	23.46	93.12	77.97	16.53
553	11.06	0.77	24.48	94.67	79.68	16.57
554	11.08	0.75	25.51	95.91	80.94	16.62
555	11.10	0.75	26.39	101.18	82.23	16.64
556	11.12	0.74	26.15	106.63	83.13	16.62
557	11.15	0.72	25.07	116.74	82.20	16.58
558	11.16	0.76	23.60	124.24	80.58	16.55
559	11.18	0.77	23.43	124.67	79.22	16.54
560	11.20	0.76	24.04	125.48	79.61	16.54
561	11.22	0.75	23.69	126.04	80.14	16.53
562	11.24	0.75	23.37	128.52	79.79	16.52
563	11.26	0.76	23.37	129.57	79.61	16.52
564	11.28	0.75	23.20	131.12	80.08	16.51
565	11.30	0.73	23.14	134.16	80.08	16.48
566	11.32	0.75	21.73	136.39	78.75	16.44
567	11.34	0.77	20.56	137.14	76.71	16.40
568	11.36	0.78	20.38	138.93	75.65	16.38
569	11.38	0.78	20.71	138.87	75.46	16.40
570	11.40	0.79	21.18	139.31	75.49	16.42
571	11.42	0.80	21.73	141.41	75.55	16.47
572	11.44	0.80	22.99	141.97	75.83	16.53
573	11.46	0.81	24.52	143.27	75.60	16.60
574	11.48	0.85	25.57	144.82	74.93	16.66
575	11.50	0.87	26.39	145.20	74.47	16.71
576	11.52	0.87	27.57	143.40	74.30	16.76

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	0.89	28.53	143.89	74.94	16.81
578	11.56	0.88	29.79	142.22	75.11	16.86
579	11.58	0.90	31.29	143.21	76.00	16.91
580	11.60	0.89	32.49	147.18	75.78	16.95
581	11.62	0.92	32.67	146.00	76.24	16.99
582	11.64	0.91	34.48	143.03	76.70	17.03
583	11.66	0.90	35.60	137.57	78.72	17.08
584	11.68	0.88	38.06	133.11	80.20	17.13
585	11.70	0.89	39.26	133.11	81.47	17.18
586	11.72	0.89	40.84	130.87	84.19	17.20
587	11.74	0.80	41.66	129.08	87.31	17.20
588	11.76	0.78	40.26	139.49	88.68	17.16
589	11.78	0.82	37.68	151.15	85.94	17.10
590	11.80	0.85	35.42	155.18	80.67	17.07
591	11.82	0.91	34.59	330.50	76.98	17.06
592	11.84	0.93	35.44	329.76	74.68	17.09
593	11.86	0.94	36.41	328.58	74.60	17.13
594	11.88	0.95	38.19	327.90	74.49	17.18
595	11.90	0.98	39.75	329.20	74.59	17.25
596	11.93	0.99	42.88	346.19	74.91	17.33
597	11.94	1.00	45.96	363.48	75.52	17.41
598	11.96	1.01	48.24	370.37	76.06	17.47
599	11.98	1.02	49.79	358.83	76.61	17.51
600	12.00	1.01	50.79	365.03	77.32	17.54
601	12.02	1.00	51.73	361.50	77.45	17.55
602	12.04	1.02	51.99	389.40	77.31	17.57
603	12.06	1.03	52.05	379.73	76.84	17.57
604	12.08	1.02	51.55	386.86	76.91	17.57
605	12.10	1.02	51.99	390.39	77.11	17.56
606	12.12	1.01	51.67	397.77	77.14	17.56
607	12.14	1.02	51.37	390.95	77.04	17.55
608	12.16	1.02	51.08	390.33	76.40	17.55
609	12.18	1.05	50.84	382.46	76.08	17.55
610	12.20	1.04	51.37	408.62	75.31	17.56
611	12.22	1.06	50.81	414.07	74.77	17.57
612	12.24	1.08	51.46	415.38	74.14	17.58
613	12.26	1.09	52.33	424.55	73.55	17.60
614	12.28	1.12	53.33	430.63	73.06	17.63
615	12.30	1.13	53.89	414.57	71.79	17.65
616	12.33	1.19	54.24	420.89	71.03	17.67
617	12.34	1.20	55.38	389.40	70.04	17.71
618	12.36	1.23	57.02	412.40	69.54	17.74
619	12.38	1.27	58.60	398.76	68.69	17.79
620	12.40	1.32	61.24	349.60	68.38	17.84
621	12.42	1.33	63.96	350.34	68.50	17.91
622	12.44	1.35	67.59	339.55	69.46	17.97
623	12.46	1.35	72.19	315.75	70.53	18.03
624	12.48	1.33	74.01	309.98	72.02	18.07

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	1.31	76.97	295.29	73.52	18.10
626	12.52	1.29	79.02	284.81	75.43	18.13
627	12.54	1.25	81.68	314.07	77.10	18.15
628	12.56	1.23	81.51	307.50	78.64	18.15
629	12.58	1.21	81.77	306.14	80.03	18.14
630	12.60	1.17	81.86	306.88	81.48	18.13
631	12.62	1.14	80.54	303.66	83.07	18.10
632	12.64	1.10	78.25	296.47	83.83	18.06
633	12.66	1.10	75.11	291.01	84.44	18.01
634	12.68	1.07	71.92	282.95	85.26	17.96
635	12.70	1.02	70.13	272.78	87.42	17.90
636	12.72	0.95	67.02	277.25	90.16	17.82
637	12.74	0.89	61.69	283.14	93.41	17.72
638	12.76	0.82	58.61	337.63	96.04	17.62
639	12.78	0.76	54.10	399.57	97.43	17.48
640	12.81	0.74	44.13	356.35	96.47	17.33
641	12.82	0.75	41.11	368.32	94.39	17.17
642	12.84	0.74	36.54	356.23	93.10	17.05
643	12.86	0.71	32.59	334.04	92.80	16.91
644	12.88	0.69	29.36	337.01	93.12	16.78
645	12.90	0.66	27.02	368.32	92.04	16.66
646	12.92	0.67	23.91	381.84	90.98	16.56
647	12.94	0.66	23.01	383.69	89.84	16.46
648	12.96	0.64	20.93	376.69	90.33	16.36
649	12.98	0.62	19.26	381.84	89.07	16.23
650	13.00	0.63	16.15	394.17	85.55	16.08
651	13.02	0.66	14.16	403.84	81.53	15.95
652	13.04	0.66	13.31	409.30	78.68	15.87
653	13.06	0.67	12.93	416.37	77.26	15.83
654	13.08	0.69	12.75	405.21	76.43	15.84
655	13.10	0.69	13.49	411.04	75.75	15.88
656	13.12	0.72	14.19	420.89	75.21	15.94
657	13.15	0.73	14.37	425.85	74.64	16.01
658	13.16	0.75	15.86	399.13	75.23	16.10
659	13.18	0.75	17.71	392.75	76.14	16.23
660	13.20	0.77	19.61	398.45	77.81	16.32
661	13.22	0.75	20.49	391.32	79.48	16.40
662	13.24	0.74	21.99	383.82	82.94	16.45
663	13.26	0.69	23.13	375.88	86.58	16.49
664	13.29	0.67	23.34	371.23	90.09	16.49
665	13.30	0.65	22.78	366.77	92.28	16.45
666	13.32	0.62	21.55	363.67	93.78	16.38
667	13.34	0.61	20.44	360.82	95.14	16.32
668	13.36	0.59	19.91	361.50	94.66	16.26
669	13.38	0.61	18.48	360.76	94.05	16.21
670	13.40	0.60	17.80	366.83	91.72	16.14
671	13.42	0.62	16.63	373.53	89.66	16.10
672	13.44	0.64	16.25	382.27	85.50	16.06

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	0.68	15.46	396.22	81.02	16.03
674	13.49	0.73	14.52	379.73	78.96	15.99
675	13.50	0.69	14.41	351.02	76.46	15.98
676	13.52	0.76	14.67	372.54	69.60	16.01
677	13.54	0.99	14.00	430.38	55.29	16.10
678	13.56	1.51	13.97	286.30	44.26	16.21
679	13.58	1.85	15.17	-6.76	40.45	16.53
680	13.60	1.88	24.61	-5.70	41.83	16.88
681	13.62	1.87	31.90	-2.67	43.76	17.16
682	13.64	2.01	34.16	11.59	43.63	17.35
683	13.66	2.20	39.23	38.81	42.95	17.53
684	13.68	2.27	46.90	26.84	42.27	17.73
685	13.70	2.51	53.73	17.42	41.58	17.91
686	13.72	2.71	59.27	12.77	40.42	18.01
687	13.74	2.72	57.69	10.91	40.26	17.97
688	13.76	2.45	47.73	4.28	41.56	17.77
689	13.78	2.04	37.12	-1.05	43.76	17.49
690	13.81	1.84	31.88	13.58	46.05	17.27
691	13.82	1.78	31.17	50.34	45.31	17.20
692	13.84	2.03	31.44	11.47	44.58	17.35
693	13.86	2.18	43.16	-3.04	44.77	17.57
694	13.88	2.14	50.86	-7.19	46.60	17.72
695	13.90	2.06	49.16	-9.92	48.31	17.73
696	13.92	1.96	45.09	-13.33	50.08	17.67
697	13.94	1.82	45.94	-15.69	52.38	17.60
698	13.96	1.69	44.47	-17.05	55.34	17.54
699	13.98	1.57	41.57	-16.74	57.74	17.46
700	14.00	1.49	39.87	-16.99	59.46	17.40
701	14.02	1.47	39.67	-6.32	60.62	17.40
702	14.04	1.48	42.13	-8.00	61.73	17.45
703	14.06	1.47	45.99	-8.25	63.46	17.51
704	14.08	1.41	47.25	-7.01	65.72	17.55
705	14.10	1.35	47.57	-6.08	69.65	17.52
706	14.12	1.18	46.26	5.27	74.92	17.45
707	14.15	1.03	42.65	10.91	83.97	17.33
708	14.16	0.83	41.30	31.87	93.08	17.21
709	14.18	0.76	38.90	66.40	97.00	17.12
710	14.20	0.84	36.00	101.74	78.43	17.12
711	14.22	1.47	32.80	139.86	60.49	17.14
712	14.24	1.79	30.19	114.63	51.12	17.17
713	14.26	1.72	32.95	90.70	50.46	17.13
714	14.28	1.50	29.43	81.84	54.22	17.09
715	14.30	1.37	29.11	82.02	58.19	17.00
716	14.32	1.29	28.78	91.63	62.63	16.98
717	14.34	1.17	30.83	88.03	69.10	17.00
718	14.36	1.00	33.68	86.86	78.84	17.05
719	14.38	0.85	36.96	87.85	91.85	17.05
720	14.40	0.69	36.78	112.71	98.43	17.01

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	0.78	33.09	156.73	85.88	16.99
722	14.44	1.20	30.25	188.28	64.77	17.00
723	14.46	1.69	27.61	167.82	52.56	17.04
724	14.48	1.79	29.19	126.66	49.70	17.08
725	14.50	1.57	31.53	102.48	52.18	17.06
726	14.52	1.41	27.11	95.60	57.17	17.02
727	14.54	1.30	29.31	89.46	62.53	16.96
728	14.56	1.12	30.39	88.53	70.88	16.99
729	14.58	0.95	33.26	87.97	82.95	17.01
730	14.60	0.78	36.43	111.10	96.16	17.02
731	14.62	0.69	36.57	146.44	100.00	16.99
732	14.64	0.76	33.41	185.37	83.59	17.02
733	14.66	1.33	30.77	235.52	59.95	17.07
734	14.68	1.98	28.81	258.59	42.91	17.15
735	14.70	2.64	28.40	141.54	34.38	17.18
736	14.72	2.87	26.82	121.33	29.62	17.11
737	14.74	2.97	20.69	124.55	27.50	16.97
738	14.76	2.93	19.20	105.58	28.08	16.92
739	14.78	2.61	24.62	81.34	33.23	17.08
740	14.80	2.07	32.96	41.91	41.10	17.37
741	14.82	2.05	45.97	80.41	41.86	17.53
742	14.85	2.78	38.85	88.96	37.84	17.67
743	14.86	3.08	41.84	56.79	33.12	17.65
744	14.88	3.08	39.38	50.09	32.42	17.66
745	14.90	3.00	38.85	47.92	32.34	17.60
746	14.92	2.95	35.83	46.50	32.02	17.39
747	14.94	2.67	22.36	41.60	32.32	17.16
748	14.97	2.42	22.85	30.87	33.79	17.04
749	14.98	2.40	29.53	29.82	36.20	17.31
750	15.00	2.72	42.04	29.08	37.51	17.68
751	15.02	2.95	55.73	26.60	37.81	18.00
752	15.04	3.10	65.22	24.18	39.24	18.19
753	15.06	2.93	70.73	17.11	42.80	18.19
754	15.08	2.22	60.59	8.87	48.93	17.98
755	15.10	1.64	43.51	3.78	58.56	17.58
756	15.13	1.16	33.16	4.77	70.73	17.23
757	15.14	0.91	34.74	74.77	81.44	17.00
758	15.16	0.90	30.23	180.53	81.93	16.97
759	15.18	1.08	30.99	207.13	75.82	16.97
760	15.20	1.14	31.72	210.73	72.00	17.00
761	15.22	1.12	31.16	182.77	73.41	17.03
762	15.24	1.04	33.89	178.36	77.91	17.07
763	15.26	0.97	36.32	172.10	83.51	17.11
764	15.28	0.92	37.69	175.02	88.35	17.14
765	15.30	0.88	38.54	174.83	91.47	17.18
766	15.32	0.88	41.12	184.13	91.76	17.22
767	15.34	0.94	41.56	196.96	89.52	17.22
768	15.36	0.95	37.40	190.58	88.21	17.15

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	0.89	34.29	180.78	85.53	17.03
770	15.40	0.95	29.89	209.30	79.89	16.92
771	15.42	1.09	26.61	221.82	73.35	16.79
772	15.44	1.08	23.42	205.89	70.11	16.76
773	15.46	1.09	26.46	200.06	62.88	16.83
774	15.48	1.57	27.78	255.36	54.68	16.97
775	15.50	1.87	28.02	179.60	49.98	17.07
776	15.52	1.71	30.36	110.79	52.75	17.14
777	15.54	1.41	34.73	124.05	57.48	17.25
778	15.56	1.54	39.56	309.98	55.60	17.36
779	15.58	2.01	38.04	139.37	50.97	17.43
780	15.60	2.10	44.28	89.27	48.09	17.58

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.27	0.00	0.27	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
2	0.04	0.57	0.00	0.57	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
3	0.06	0.87	0.00	0.87	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
4	0.08	1.17	0.00	1.17	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
5	0.11	1.65	0.00	1.65	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
6	0.12	1.81	0.00	1.81	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
7	0.14	2.14	0.00	2.14	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
8	0.16	2.47	0.00	2.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
9	0.18	2.80	0.00	2.80	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
10	0.20	3.13	0.00	3.13	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
11	0.22	3.47	0.00	3.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
12	0.24	3.80	0.00	3.80	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
13	0.26	4.14	0.00	4.14	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
14	0.28	4.47	0.00	4.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
15	0.30	4.80	0.00	4.80	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
16	0.32	5.12	0.00	5.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
17	0.34	5.45	0.00	5.45	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
18	0.36	5.78	0.00	5.78	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
19	0.38	6.11	0.00	6.11	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
20	0.40	6.44	0.00	6.44	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
21	0.42	6.77	0.00	6.77	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
22	0.44	7.11	0.00	7.11	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
23	0.46	7.45	0.00	7.45	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
24	0.48	7.80	0.00	7.80	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
25	0.50	8.14	0.00	8.14	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
26	0.52	8.49	0.00	8.49	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
27	0.54	8.84	0.00	8.84	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
28	0.56	9.19	0.00	9.19	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
29	0.58	9.54	0.00	9.54	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
30	0.60	9.89	0.00	9.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
31	0.62	10.25	0.00	10.25	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
32	0.64	10.60	0.00	10.60	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
33	0.66	10.95	0.00	10.95	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
34	0.68	11.30	0.00	11.30	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
35	0.70	11.65	0.00	11.65	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
36	0.72	12.00	0.00	12.00	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
37	0.74	12.35	0.00	12.35	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
38	0.76	12.69	0.00	12.69	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
39	0.78	13.04	0.00	13.04	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
40	0.80	13.39	0.00	13.39	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
41	0.82	13.74	0.00	13.74	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
42	0.84	14.10	0.00	14.10	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
43	0.86	14.45	0.00	14.45	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
44	0.88	14.81	0.00	14.81	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
45	0.90	15.17	0.00	15.17	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
46	0.92	15.53	0.00	15.53	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
47	0.96	16.25	0.00	16.25	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
48	0.96	16.25	0.00	16.25	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	16.61	0.00	16.61	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
50	1.00	16.98	0.00	16.98	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
51	1.02	17.35	0.00	17.35	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
52	1.04	17.71	0.00	17.71	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
53	1.06	18.08	0.00	18.08	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
54	1.08	18.44	0.00	18.44	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
55	1.10	18.81	0.00	18.81	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
56	1.12	19.17	0.00	19.17	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
57	1.14	19.53	0.00	19.53	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
58	1.16	19.89	0.00	19.89	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
59	1.18	20.25	0.00	20.25	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
60	1.21	20.79	0.00	20.79	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
61	1.22	20.97	0.00	20.97	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
62	1.24	21.33	0.00	21.33	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
63	1.26	21.68	0.00	21.68	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
64	1.28	22.04	0.00	22.04	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
65	1.30	22.40	0.00	22.40	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
66	1.32	22.77	0.00	22.77	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
67	1.34	23.13	0.00	23.13	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
68	1.36	23.50	0.00	23.50	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
69	1.38	23.86	0.00	23.86	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
70	1.40	24.23	0.00	24.23	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
71	1.42	24.60	0.00	24.60	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
72	1.44	24.96	0.00	24.96	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
73	1.46	25.33	0.00	25.33	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
74	1.48	25.70	0.00	25.70	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
75	1.50	26.06	0.00	26.06	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
76	1.52	26.43	0.00	26.43	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
77	1.54	26.80	0.00	26.80	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
78	1.56	27.16	0.00	27.16	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
79	1.58	27.53	0.00	27.53	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
80	1.60	27.90	0.00	27.90	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
81	1.62	28.26	0.00	28.26	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
82	1.64	28.63	0.00	28.63	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
83	1.66	29.00	0.00	29.00	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
84	1.68	29.36	0.00	29.36	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
85	1.70	29.72	0.00	29.72	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
86	1.72	30.09	0.00	30.09	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
87	1.74	30.45	0.00	30.45	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
88	1.76	30.81	0.00	30.81	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
89	1.78	31.18	0.00	31.18	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
90	1.80	31.54	0.00	31.54	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
91	1.82	31.90	0.00	31.90	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
92	1.84	32.27	0.00	32.27	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
93	1.86	32.64	0.00	32.64	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
94	1.88	33.00	0.00	33.00	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
95	1.90	33.37	0.00	33.37	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
96	1.92	33.73	0.00	33.73	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.96	34.46	0.00	34.46	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
98	1.96	34.46	0.00	34.46	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
99	1.98	34.83	0.00	34.83	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
100	2.00	35.19	0.00	35.19	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
101	2.02	35.55	0.20	35.36	0.98	0.141	1.43	0.098	1.09	1.00	0.119	No
102	2.04	35.92	0.39	35.52	0.98	0.141	1.43	0.099	1.09	1.00	0.119	No
103	2.06	36.28	0.59	35.69	0.98	0.142	1.43	0.099	1.09	1.00	0.120	No
104	2.08	36.64	0.78	35.86	0.98	0.143	1.43	0.100	1.09	1.00	0.121	No
105	2.10	37.00	0.98	36.02	0.98	0.144	1.43	0.100	1.09	1.00	0.122	No
106	2.12	37.36	1.18	36.18	0.98	0.144	1.43	0.101	1.09	1.00	0.123	No
107	2.14	37.72	1.37	36.34	0.98	0.145	1.43	0.101	1.09	1.00	0.123	No
108	2.16	38.07	1.57	36.50	0.98	0.146	1.43	0.102	1.09	1.00	0.124	No
109	2.18	38.42	1.77	36.66	0.98	0.146	1.43	0.102	1.09	1.00	0.124	No
110	2.20	38.78	1.96	36.81	0.98	0.147	1.43	0.103	1.09	1.00	0.124	No
111	2.23	39.30	2.26	37.05	0.98	0.148	1.43	0.104	1.09	1.00	0.125	No
112	2.24	39.48	2.35	37.12	0.97	0.148	1.43	0.104	1.09	1.00	0.125	No
113	2.26	39.82	2.55	37.27	0.97	0.149	1.43	0.104	1.09	1.00	0.125	No
114	2.28	40.17	2.75	37.43	0.97	0.150	1.43	0.105	1.09	1.00	0.126	No
115	2.30	40.52	2.94	37.58	0.97	0.150	1.43	0.105	1.09	1.00	0.126	No
116	2.32	40.87	3.14	37.73	0.97	0.151	1.43	0.106	1.09	1.00	0.127	No
117	2.34	41.22	3.34	37.89	0.97	0.151	1.43	0.106	1.09	1.00	0.128	No
118	2.36	41.58	3.53	38.05	0.97	0.152	1.43	0.106	1.09	1.00	0.129	No
119	2.38	41.94	3.73	38.21	0.97	0.153	1.43	0.107	1.09	1.00	0.129	No
120	2.40	42.29	3.92	38.37	0.97	0.153	1.43	0.107	1.08	1.00	0.130	No
121	2.42	42.65	4.12	38.53	0.97	0.154	1.43	0.108	1.08	1.00	0.131	No
122	2.44	43.01	4.32	38.69	0.97	0.154	1.43	0.108	1.08	1.00	0.131	No
123	2.46	43.37	4.51	38.86	0.97	0.155	1.43	0.108	1.08	1.00	0.132	No
124	2.48	43.73	4.71	39.02	0.97	0.156	1.43	0.109	1.08	1.00	0.132	No
125	2.50	44.08	4.91	39.18	0.97	0.156	1.43	0.109	1.08	1.00	0.132	No
126	2.52	44.44	5.10	39.34	0.97	0.157	1.43	0.110	1.08	1.00	0.133	No
127	2.54	44.79	5.30	39.50	0.97	0.157	1.43	0.110	1.08	1.00	0.133	No
128	2.56	45.15	5.49	39.66	0.97	0.158	1.43	0.110	1.08	1.00	0.134	No
129	2.58	45.51	5.69	39.82	0.97	0.158	1.43	0.111	1.08	1.00	0.134	No
130	2.60	45.86	5.89	39.98	0.97	0.159	1.43	0.111	1.08	1.00	0.135	No
131	2.62	46.22	6.08	40.14	0.97	0.159	1.43	0.112	1.08	1.00	0.136	No
132	2.64	46.58	6.28	40.30	0.97	0.160	1.43	0.112	1.08	1.00	0.136	No
133	2.66	46.94	6.47	40.47	0.97	0.161	1.43	0.112	1.08	1.00	0.137	No
134	2.68	47.30	6.67	40.63	0.97	0.161	1.43	0.113	1.08	1.00	0.137	No
135	2.70	47.66	6.87	40.79	0.97	0.162	1.43	0.113	1.08	1.00	0.138	No
136	2.72	48.02	7.06	40.96	0.97	0.162	1.43	0.113	1.08	1.00	0.139	No
137	2.74	48.38	7.26	41.12	0.97	0.163	1.43	0.114	1.08	1.00	0.139	No
138	2.76	48.73	7.46	41.28	0.97	0.163	1.43	0.114	1.08	1.00	0.140	No
139	2.78	49.09	7.65	41.44	0.97	0.164	1.43	0.114	1.08	1.00	0.141	No
140	2.80	49.44	7.85	41.60	0.97	0.164	1.43	0.115	1.08	1.00	0.141	No
141	2.82	49.80	8.04	41.75	0.96	0.165	1.43	0.115	1.07	1.00	0.142	No
142	2.84	50.15	8.24	41.91	0.96	0.165	1.43	0.116	1.07	1.00	0.142	No
143	2.86	50.49	8.44	42.06	0.96	0.166	1.43	0.116	1.07	1.00	0.143	No
144	2.88	50.84	8.63	42.21	0.96	0.166	1.43	0.116	1.07	1.00	0.143	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.91	51.35	8.93	42.42	0.96	0.167	1.43	0.117	1.07	1.00	0.144	No
146	2.92	51.52	9.03	42.49	0.96	0.167	1.43	0.117	1.07	1.00	0.144	No
147	2.94	51.86	9.22	42.64	0.96	0.167	1.43	0.117	1.07	1.00	0.145	No
148	2.96	52.19	9.42	42.77	0.96	0.168	1.43	0.118	1.07	1.00	0.146	No
149	2.98	52.53	9.61	42.91	0.96	0.168	1.43	0.118	1.07	1.00	0.146	No
150	3.00	52.86	9.81	43.05	0.96	0.169	1.43	0.118	1.07	1.00	0.147	No
151	3.02	53.19	10.01	43.19	0.96	0.169	1.43	0.118	1.07	1.00	0.147	No
152	3.04	53.53	10.20	43.33	0.96	0.170	1.43	0.119	1.07	1.00	0.148	No
153	3.06	53.86	10.40	43.46	0.96	0.170	1.43	0.119	1.07	1.00	0.148	No
154	3.08	54.19	10.59	43.59	0.96	0.171	1.43	0.119	1.07	1.00	0.149	No
155	3.10	54.52	10.79	43.73	0.96	0.171	1.43	0.120	1.07	1.00	0.149	No
156	3.12	54.85	10.99	43.86	0.96	0.172	1.43	0.120	1.07	1.00	0.150	No
157	3.14	55.17	11.18	43.99	0.96	0.172	1.43	0.120	1.07	1.00	0.150	No
158	3.16	55.50	11.38	44.12	0.96	0.172	1.43	0.121	1.07	1.00	0.150	No
159	3.18	55.82	11.58	44.24	0.96	0.173	1.43	0.121	1.07	1.00	0.151	No
160	3.21	56.30	11.87	44.43	0.96	0.174	1.43	0.121	1.07	1.00	0.151	No
161	3.22	56.46	11.97	44.50	0.96	0.174	1.43	0.122	1.07	1.00	0.151	No
162	3.24	56.79	12.16	44.62	0.96	0.174	1.43	0.122	1.07	1.00	0.151	No
163	3.26	57.11	12.36	44.75	0.96	0.175	1.43	0.122	1.07	1.00	0.152	No
164	3.28	57.44	12.56	44.88	0.96	0.175	1.43	0.123	1.07	1.00	0.151	No
165	3.30	57.77	12.75	45.02	0.96	0.175	1.43	0.123	1.07	1.00	0.151	No
166	3.32	58.11	12.95	45.16	0.96	0.176	1.43	0.123	1.07	1.00	0.151	No
167	3.34	58.45	13.15	45.30	0.96	0.176	1.43	0.123	1.07	1.00	0.151	No
168	3.36	58.79	13.34	45.45	0.95	0.177	1.43	0.124	1.07	1.00	0.151	No
169	3.38	59.14	13.54	45.61	0.95	0.177	1.43	0.124	1.07	1.00	0.151	No
170	3.40	59.50	13.73	45.76	0.95	0.177	1.43	0.124	1.07	1.00	0.152	No
171	3.42	59.85	13.93	45.92	0.95	0.178	1.43	0.124	1.07	1.00	0.152	No
172	3.44	60.21	14.13	46.09	0.95	0.178	1.43	0.125	1.07	1.00	0.153	No
173	3.46	60.57	14.32	46.25	0.95	0.178	1.43	0.125	1.07	1.00	0.153	No
174	3.48	60.94	14.52	46.42	0.95	0.179	1.43	0.125	1.07	1.00	0.154	No
175	3.50	61.30	14.72	46.58	0.95	0.179	1.43	0.125	1.07	1.00	0.154	No
176	3.52	61.66	14.91	46.75	0.95	0.180	1.43	0.126	1.07	1.00	0.154	No
177	3.54	62.02	15.11	46.91	0.95	0.180	1.43	0.126	1.07	1.00	0.155	No
178	3.56	62.38	15.30	47.08	0.95	0.180	1.43	0.126	1.07	1.00	0.155	No
179	3.58	62.74	15.50	47.24	0.95	0.181	1.43	0.126	1.07	1.00	0.156	No
180	3.60	63.10	15.70	47.40	0.95	0.181	1.43	0.127	1.07	1.00	0.156	No
181	3.62	63.45	15.89	47.56	0.95	0.181	1.43	0.127	1.07	1.00	0.156	No
182	3.64	63.81	16.09	47.72	0.95	0.182	1.43	0.127	1.07	1.00	0.157	No
183	3.66	64.16	16.28	47.88	0.95	0.182	1.43	0.127	1.07	1.00	0.157	No
184	3.68	64.52	16.48	48.03	0.95	0.182	1.43	0.128	1.06	1.00	0.158	No
185	3.70	64.87	16.68	48.19	0.95	0.183	1.43	0.128	1.06	1.00	0.158	No
186	3.72	65.22	16.87	48.35	0.95	0.183	1.43	0.128	1.06	1.00	0.159	No
187	3.74	65.57	17.07	48.50	0.95	0.183	1.43	0.128	1.06	1.00	0.160	No
188	3.76	65.92	17.27	48.66	0.95	0.184	1.43	0.128	1.06	1.00	0.160	No
189	3.78	66.27	17.46	48.81	0.95	0.184	1.43	0.129	1.06	1.00	0.161	No
190	3.80	66.62	17.66	48.96	0.95	0.184	1.43	0.129	1.06	1.00	0.161	No
191	3.82	66.97	17.85	49.12	0.95	0.184	1.43	0.129	1.06	1.00	0.162	No
192	3.84	67.32	18.05	49.27	0.95	0.185	1.43	0.129	1.06	1.00	0.162	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	67.66	18.25	49.42	0.95	0.185	1.43	0.130	1.06	1.00	0.162	No
194	3.88	68.01	18.44	49.57	0.94	0.185	1.43	0.130	1.06	1.00	0.163	No
195	3.90	68.35	18.64	49.71	0.94	0.186	1.43	0.130	1.06	1.00	0.163	No
196	3.92	68.69	18.84	49.85	0.94	0.186	1.43	0.130	1.06	1.00	0.164	No
197	3.94	69.03	19.03	49.99	0.94	0.186	1.43	0.130	1.06	1.00	0.164	No
198	3.96	69.36	19.23	50.13	0.94	0.187	1.43	0.131	1.06	1.00	0.165	No
199	3.98	69.69	19.42	50.27	0.94	0.187	1.43	0.131	1.06	1.00	0.165	No
200	4.00	70.03	19.62	50.41	0.94	0.187	1.43	0.131	1.06	1.00	0.166	No
201	4.02	70.35	19.82	50.54	0.94	0.188	1.43	0.131	1.06	1.00	0.166	No
202	4.05	70.84	20.11	50.73	0.94	0.188	1.43	0.132	1.06	1.00	0.166	No
203	4.06	71.00	20.21	50.80	0.94	0.188	1.43	0.132	1.06	1.00	0.166	No
204	4.08	71.32	20.40	50.92	0.94	0.188	1.43	0.132	1.06	1.00	0.166	No
205	4.10	71.64	20.60	51.04	0.94	0.189	1.43	0.132	1.06	1.00	0.167	No
206	4.12	71.96	20.80	51.17	0.94	0.189	1.43	0.132	1.06	1.00	0.167	No
207	4.14	72.29	20.99	51.29	0.94	0.189	1.43	0.133	1.06	1.00	0.167	No
208	4.16	72.61	21.19	51.42	0.94	0.190	1.43	0.133	1.06	1.00	0.167	No
209	4.18	72.93	21.39	51.55	0.94	0.190	1.43	0.133	1.06	1.00	0.167	No
210	4.20	73.26	21.58	51.68	0.94	0.190	1.43	0.133	1.06	1.00	0.167	No
211	4.22	73.59	21.78	51.81	0.94	0.191	1.43	0.133	1.06	1.00	0.168	No
212	4.24	73.92	21.97	51.94	0.94	0.191	1.43	0.134	1.06	1.00	0.168	No
213	4.26	74.25	22.17	52.08	0.94	0.191	1.43	0.134	1.06	1.00	0.168	No
214	4.28	74.59	22.37	52.22	0.94	0.191	1.43	0.134	1.05	1.00	0.168	No
215	4.30	74.92	22.56	52.36	0.94	0.192	1.43	0.134	1.05	1.00	0.169	No
216	4.32	75.26	22.76	52.50	0.94	0.192	1.43	0.134	1.05	1.00	0.169	No
217	4.34	75.60	22.96	52.64	0.94	0.192	1.43	0.135	1.05	1.00	0.170	No
218	4.36	75.94	23.15	52.79	0.94	0.192	1.43	0.135	1.05	1.00	0.170	No
219	4.38	76.28	23.35	52.93	0.93	0.193	1.43	0.135	1.05	1.00	0.170	No
220	4.40	76.61	23.54	53.07	0.93	0.193	1.43	0.135	1.05	1.00	0.171	No
221	4.42	76.95	23.74	53.21	0.93	0.193	1.43	0.135	1.05	1.00	0.171	No
222	4.44	77.28	23.94	53.34	0.93	0.193	1.43	0.135	1.05	1.00	0.171	No
223	4.46	77.61	24.13	53.48	0.93	0.194	1.43	0.136	1.05	1.00	0.172	No
224	4.48	77.94	24.33	53.61	0.93	0.194	1.43	0.136	1.05	1.00	0.172	No
225	4.50	78.27	24.53	53.74	0.93	0.194	1.43	0.136	1.05	1.00	0.172	No
226	4.52	78.59	24.72	53.87	0.93	0.194	1.43	0.136	1.05	1.00	0.172	No
227	4.54	78.92	24.92	54.00	0.93	0.195	1.43	0.136	1.05	1.00	0.173	No
228	4.56	79.24	25.11	54.13	0.93	0.195	1.43	0.136	1.05	1.00	0.173	No
229	4.58	79.57	25.31	54.26	0.93	0.195	1.43	0.137	1.05	1.00	0.173	No
230	4.60	79.89	25.51	54.39	0.93	0.195	1.43	0.137	1.05	1.00	0.173	No
231	4.62	80.22	25.70	54.51	0.93	0.196	1.43	0.137	1.05	1.00	0.174	No
232	4.64	80.54	25.90	54.64	0.93	0.196	1.43	0.137	1.05	1.00	0.174	No
233	4.66	80.86	26.09	54.77	0.93	0.196	1.43	0.137	1.05	1.00	0.174	No
234	4.68	81.19	26.29	54.90	0.93	0.196	1.43	0.138	1.05	1.00	0.174	No
235	4.70	81.51	26.49	55.03	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
236	4.72	81.84	26.68	55.16	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
237	4.74	82.17	26.88	55.29	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
238	4.76	82.50	27.08	55.43	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
239	4.78	82.84	27.27	55.56	0.93	0.198	1.43	0.138	1.05	1.00	0.174	No
240	4.80	83.17	27.47	55.70	0.93	0.198	1.43	0.138	1.05	1.00	0.174	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	83.51	27.66	55.85	0.93	0.198	1.43	0.139	1.05	1.00	0.174	No
242	4.84	83.85	27.86	55.99	0.93	0.198	1.43	0.139	1.05	1.00	0.174	No
243	4.86	84.19	28.06	56.13	0.93	0.198	1.43	0.139	1.05	1.00	0.174	No
244	4.88	84.53	28.25	56.28	0.92	0.199	1.43	0.139	1.05	1.00	0.175	No
245	4.90	84.87	28.45	56.43	0.92	0.199	1.43	0.139	1.05	1.00	0.174	No
246	4.93	85.40	28.74	56.65	0.92	0.199	1.43	0.139	1.05	1.00	0.175	No
247	4.94	85.57	28.84	56.73	0.92	0.199	1.43	0.139	1.05	1.00	0.176	No
248	4.96	85.92	29.04	56.88	0.92	0.199	1.43	0.140	1.05	1.00	0.176	No
249	4.98	86.27	29.23	57.04	0.92	0.200	1.43	0.140	1.05	1.00	0.177	No
250	5.00	86.62	29.43	57.19	0.92	0.200	1.43	0.140	1.05	1.00	0.177	No
251	5.02	86.97	29.63	57.35	0.92	0.200	1.43	0.140	1.05	1.00	0.178	No
252	5.04	87.32	29.82	57.50	0.92	0.200	1.43	0.140	1.05	1.00	0.178	No
253	5.06	87.66	30.02	57.65	0.92	0.200	1.43	0.140	1.05	1.00	0.178	No
254	5.08	88.00	30.21	57.79	0.92	0.200	1.43	0.140	1.05	1.00	0.178	No
255	5.10	88.34	30.41	57.93	0.92	0.201	1.43	0.140	1.05	1.00	0.178	No
256	5.12	88.68	30.61	58.07	0.92	0.201	1.43	0.141	1.05	1.00	0.177	No
257	5.14	89.02	30.80	58.22	0.92	0.201	1.43	0.141	1.05	1.00	0.175	No
258	5.16	89.36	31.00	58.36	0.92	0.201	1.43	0.141	1.05	1.00	0.176	No
259	5.18	89.70	31.20	58.51	0.92	0.201	1.43	0.141	1.05	1.00	0.176	No
260	5.20	90.05	31.39	58.65	0.92	0.202	1.43	0.141	1.05	1.00	0.177	No
261	5.22	90.39	31.59	58.80	0.92	0.202	1.43	0.141	1.05	1.00	0.178	No
262	5.24	90.74	31.78	58.95	0.92	0.202	1.43	0.141	1.05	1.00	0.178	No
263	5.26	91.08	31.98	59.10	0.92	0.202	1.43	0.141	1.05	1.00	0.178	No
264	5.29	91.61	32.27	59.33	0.92	0.202	1.43	0.142	1.05	1.00	0.178	No
265	5.30	91.78	32.37	59.41	0.92	0.202	1.43	0.142	1.05	1.00	0.177	No
266	5.32	92.14	32.57	59.57	0.92	0.202	1.43	0.142	1.05	1.00	0.177	No
267	5.34	92.49	32.77	59.73	0.92	0.203	1.43	0.142	1.05	1.00	0.177	No
268	5.36	92.85	32.96	59.89	0.91	0.203	1.43	0.142	1.05	1.00	0.177	No
269	5.38	93.21	33.16	60.05	0.91	0.203	1.43	0.142	1.05	1.00	0.177	No
270	5.40	93.56	33.35	60.21	0.91	0.203	1.43	0.142	1.05	1.00	0.177	No
271	5.42	93.92	33.55	60.37	0.91	0.203	1.43	0.142	1.05	1.00	0.177	No
272	5.44	94.28	33.75	60.53	0.91	0.203	1.43	0.142	1.05	1.00	0.177	No
273	5.46	94.64	33.94	60.69	0.91	0.203	1.43	0.142	1.05	1.00	0.178	No
274	5.48	95.00	34.14	60.86	0.91	0.204	1.43	0.143	1.05	1.00	0.178	No
275	5.50	95.35	34.34	61.02	0.91	0.204	1.43	0.143	1.05	1.00	0.178	No
276	5.52	95.71	34.53	61.18	0.91	0.204	1.43	0.143	1.05	1.00	0.177	No
277	5.54	96.07	34.73	61.34	0.91	0.204	1.43	0.143	1.05	1.00	0.177	No
278	5.56	96.43	34.92	61.51	0.91	0.204	1.43	0.143	1.05	1.00	0.176	No
279	5.58	96.80	35.12	61.68	0.91	0.204	1.43	0.143	1.05	1.00	0.176	No
280	5.60	97.16	35.32	61.85	0.91	0.204	1.43	0.143	1.05	1.00	0.178	No
281	5.62	97.52	35.51	62.01	0.91	0.204	1.43	0.143	1.04	1.00	0.179	No
282	5.64	97.89	35.71	62.18	0.91	0.205	1.43	0.143	1.04	1.00	0.180	No
283	5.66	98.24	35.90	62.34	0.91	0.205	1.43	0.143	1.04	1.00	0.179	No
284	5.68	98.60	36.10	62.50	0.91	0.205	1.43	0.143	1.04	1.00	0.179	No
285	5.70	98.96	36.30	62.66	0.91	0.205	1.43	0.143	1.04	1.00	0.180	No
286	5.72	99.31	36.49	62.82	0.91	0.205	1.43	0.144	1.04	1.00	0.181	No
287	5.74	99.66	36.69	62.98	0.91	0.205	1.43	0.144	1.04	1.00	0.182	No
288	5.76	100.02	36.89	63.13	0.91	0.205	1.43	0.144	1.04	1.00	0.183	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	100.37	37.08	63.29	0.91	0.205	1.43	0.144	1.04	1.00	0.183	No
290	5.80	100.72	37.28	63.44	0.91	0.205	1.43	0.144	1.04	1.00	0.183	No
291	5.82	101.07	37.47	63.59	0.90	0.206	1.43	0.144	1.04	1.00	0.183	No
292	5.84	101.42	37.67	63.75	0.90	0.206	1.43	0.144	1.04	1.00	0.183	No
293	5.86	101.76	37.87	63.90	0.90	0.206	1.43	0.144	1.04	1.00	0.183	No
294	5.88	102.11	38.06	64.05	0.90	0.206	1.43	0.144	1.04	1.00	0.183	No
295	5.90	102.46	38.26	64.20	0.90	0.206	1.43	0.144	1.04	1.00	0.183	No
296	5.93	102.98	38.55	64.43	0.90	0.206	1.43	0.144	1.04	1.00	0.183	No
297	5.94	103.15	38.65	64.50	0.90	0.206	1.43	0.144	1.04	1.00	0.184	No
298	5.96	103.51	38.85	64.66	0.90	0.206	1.43	0.144	1.04	1.00	0.184	No
299	5.98	103.86	39.04	64.81	0.90	0.207	1.43	0.145	1.04	1.00	0.184	No
300	6.01	104.39	39.34	65.05	0.90	0.207	1.43	0.145	1.04	1.00	0.184	No
301	6.02	104.56	39.44	65.13	0.90	0.207	1.43	0.145	1.04	1.00	0.184	No
302	6.04	104.92	39.63	65.28	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
303	6.06	105.27	39.83	65.44	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
304	6.08	105.63	40.02	65.60	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
305	6.10	105.98	40.22	65.76	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
306	6.12	106.34	40.42	65.92	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
307	6.14	106.69	40.61	66.08	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
308	6.16	107.05	40.81	66.24	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
309	6.18	107.40	41.01	66.39	0.90	0.207	1.43	0.145	1.04	1.00	0.185	No
310	6.20	107.76	41.20	66.55	0.90	0.208	1.43	0.145	1.04	1.00	0.185	No
311	6.22	108.11	41.40	66.71	0.90	0.208	1.43	0.145	1.04	1.00	0.185	No
312	6.24	108.47	41.59	66.87	0.90	0.208	1.43	0.145	1.04	1.00	0.186	No
313	6.26	108.82	41.79	67.03	0.89	0.208	1.43	0.145	1.03	1.00	0.186	No
314	6.28	109.18	41.99	67.19	0.89	0.208	1.43	0.145	1.03	1.00	0.186	No
315	6.30	109.54	42.18	67.35	0.89	0.208	1.43	0.146	1.03	1.00	0.187	No
316	6.32	109.89	42.38	67.51	0.89	0.208	1.43	0.146	1.03	1.00	0.187	No
317	6.34	110.25	42.58	67.67	0.89	0.208	1.43	0.146	1.03	1.00	0.187	No
318	6.36	110.60	42.77	67.83	0.89	0.208	1.43	0.146	1.03	1.00	0.188	No
319	6.38	110.95	42.97	67.99	0.89	0.208	1.43	0.146	1.03	1.00	0.188	No
320	6.40	111.31	43.16	68.14	0.89	0.208	1.43	0.146	1.03	1.00	0.188	No
321	6.42	111.66	43.36	68.30	0.89	0.208	1.43	0.146	1.03	1.00	0.187	No
322	6.44	112.01	43.56	68.45	0.89	0.208	1.43	0.146	1.03	1.00	0.188	No
323	6.46	112.35	43.75	68.60	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
324	6.48	112.70	43.95	68.75	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
325	6.50	113.05	44.15	68.90	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
326	6.52	113.39	44.34	69.05	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
327	6.54	113.74	44.54	69.20	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
328	6.56	114.08	44.73	69.35	0.89	0.209	1.43	0.146	1.03	1.00	0.188	No
329	6.58	114.43	44.93	69.50	0.89	0.209	1.43	0.146	1.03	1.00	0.189	No
330	6.60	114.78	45.13	69.65	0.89	0.209	1.43	0.146	1.03	1.00	0.189	No
331	6.62	115.12	45.32	69.80	0.89	0.209	1.43	0.146	1.03	1.00	0.189	No
332	6.64	115.47	45.52	69.95	0.89	0.209	1.43	0.146	1.03	1.00	0.189	No
333	6.66	115.82	45.71	70.10	0.89	0.209	1.43	0.147	1.03	1.00	0.189	No
334	6.68	116.16	45.91	70.25	0.89	0.209	1.43	0.147	1.03	1.00	0.189	No
335	6.70	116.50	46.11	70.40	0.89	0.209	1.43	0.147	1.03	1.00	0.189	No
336	6.72	116.85	46.30	70.54	0.88	0.210	1.43	0.147	1.03	1.00	0.189	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	117.19	46.50	70.69	0.88	0.210	1.43	0.147	1.03	1.00	0.189	No
338	6.76	117.53	46.70	70.83	0.88	0.210	1.43	0.147	1.03	1.00	0.189	No
339	6.78	117.87	46.89	70.97	0.88	0.210	1.43	0.147	1.03	1.00	0.190	No
340	6.80	118.20	47.09	71.12	0.88	0.210	1.43	0.147	1.03	1.00	0.190	No
341	6.82	118.54	47.28	71.26	0.88	0.210	1.43	0.147	1.03	1.00	0.190	No
342	6.84	118.88	47.48	71.40	0.88	0.210	1.43	0.147	1.03	1.00	0.190	No
343	6.86	119.22	47.68	71.55	0.88	0.210	1.43	0.147	1.03	1.00	0.190	No
344	6.88	119.56	47.87	71.69	0.88	0.210	1.43	0.147	1.03	1.00	0.190	No
345	6.90	119.90	48.07	71.83	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
346	6.92	120.23	48.27	71.97	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
347	6.94	120.57	48.46	72.11	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
348	6.96	120.90	48.66	72.24	0.88	0.210	1.43	0.147	1.03	1.00	0.191	No
349	6.98	121.23	48.85	72.38	0.88	0.210	1.43	0.147	1.03	1.00	0.192	No
350	7.00	121.56	49.05	72.51	0.88	0.211	1.43	0.147	1.03	1.00	0.192	No
351	7.02	121.90	49.25	72.65	0.88	0.211	1.43	0.147	1.03	1.00	0.192	No
352	7.04	122.22	49.44	72.78	0.88	0.211	1.43	0.147	1.03	1.00	0.192	No
353	7.06	122.55	49.64	72.92	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
354	7.09	123.05	49.93	73.11	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
355	7.10	123.21	50.03	73.18	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
356	7.14	123.87	50.42	73.45	0.88	0.211	1.43	0.148	1.03	1.00	0.192	No
357	7.15	124.04	50.52	73.52	0.87	0.211	1.43	0.148	1.03	1.00	0.192	No
358	7.16	124.20	50.62	73.58	0.87	0.211	1.43	0.148	1.03	1.00	0.191	No
359	7.18	124.54	50.82	73.72	0.87	0.211	1.43	0.148	1.03	1.00	0.191	No
360	7.20	124.87	51.01	73.86	0.87	0.211	1.43	0.148	1.03	1.00	0.191	No
361	7.22	125.21	51.21	74.00	0.87	0.211	1.43	0.148	1.03	1.00	0.191	No
362	7.24	125.54	51.40	74.14	0.87	0.211	1.43	0.148	1.03	1.00	0.191	No
363	7.26	125.88	51.60	74.28	0.87	0.211	1.43	0.148	1.03	1.00	0.191	No
364	7.28	126.22	51.80	74.42	0.87	0.211	1.43	0.148	1.03	1.00	0.191	No
365	7.31	126.73	52.09	74.64	0.87	0.212	1.43	0.148	1.03	1.00	0.191	No
366	7.32	126.90	52.19	74.71	0.87	0.212	1.43	0.148	1.03	1.00	0.191	No
367	7.34	127.24	52.39	74.85	0.87	0.212	1.43	0.148	1.03	1.00	0.191	No
368	7.36	127.58	52.58	75.00	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
369	7.38	127.92	52.78	75.14	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
370	7.40	128.26	52.97	75.29	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
371	7.42	128.61	53.17	75.44	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
372	7.44	128.95	53.37	75.58	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
373	7.46	129.30	53.56	75.73	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
374	7.48	129.64	53.76	75.88	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
375	7.50	129.99	53.96	76.03	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
376	7.52	130.34	54.15	76.18	0.87	0.212	1.43	0.148	1.02	1.00	0.192	No
377	7.54	130.68	54.35	76.34	0.87	0.212	1.43	0.148	1.02	1.00	0.193	No
378	7.56	131.03	54.54	76.49	0.87	0.212	1.43	0.148	1.02	1.00	0.193	No
379	7.58	131.38	54.74	76.64	0.87	0.212	1.43	0.148	1.02	1.00	0.193	No
380	7.60	131.72	54.94	76.78	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
381	7.62	132.07	55.13	76.93	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
382	7.64	132.41	55.33	77.08	0.86	0.212	1.43	0.148	1.02	1.00	0.193	No
383	7.66	132.75	55.52	77.23	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No
384	7.68	133.09	55.72	77.37	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	133.43	55.92	77.51	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No
386	7.72	133.77	56.11	77.65	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No
387	7.74	134.10	56.31	77.79	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No
388	7.76	134.43	56.51	77.93	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No
389	7.78	134.76	56.70	78.06	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No
390	7.80	135.09	56.90	78.19	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No
391	7.82	135.42	57.09	78.33	0.86	0.212	1.43	0.149	1.02	1.00	0.194	No
392	7.84	135.75	57.29	78.46	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
393	7.86	136.07	57.49	78.59	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
394	7.88	136.40	57.68	78.72	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
395	7.90	136.73	57.88	78.85	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
396	7.92	137.06	58.08	78.98	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
397	7.94	137.39	58.27	79.12	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
398	7.96	137.72	58.47	79.25	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
399	7.98	138.04	58.66	79.38	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
400	8.00	138.37	58.86	79.51	0.86	0.213	1.43	0.149	1.02	1.00	0.194	No
401	8.02	138.70	59.06	79.64	0.85	0.213	1.43	0.149	1.02	1.00	0.194	No
402	8.04	139.03	59.25	79.78	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
403	8.06	139.36	59.45	79.91	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
404	8.08	139.68	59.64	80.04	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
405	8.10	140.01	59.84	80.17	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
406	8.12	140.33	60.04	80.29	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
407	8.14	140.65	60.23	80.42	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
408	8.16	140.97	60.43	80.54	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
409	8.19	141.46	60.72	80.73	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
410	8.20	141.62	60.82	80.79	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
411	8.22	141.94	61.02	80.92	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
412	8.24	142.26	61.21	81.05	0.85	0.213	1.43	0.149	1.02	1.00	0.196	No
413	8.26	142.59	61.41	81.17	0.85	0.213	1.43	0.149	1.02	1.00	0.196	No
414	8.28	142.91	61.61	81.30	0.85	0.213	1.43	0.149	1.02	1.00	0.196	No
415	8.30	143.23	61.80	81.43	0.85	0.213	1.43	0.149	1.02	1.00	0.196	No
416	8.32	143.56	62.00	81.56	0.85	0.213	1.43	0.149	1.02	1.00	0.196	No
417	8.34	143.89	62.20	81.69	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
418	8.36	144.21	62.39	81.82	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
419	8.38	144.54	62.59	81.95	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
420	8.40	144.87	62.78	82.08	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
421	8.42	145.19	62.98	82.21	0.85	0.213	1.43	0.149	1.02	1.00	0.195	No
422	8.44	145.53	63.18	82.35	0.84	0.214	1.43	0.149	1.02	1.00	0.195	No
423	8.46	145.86	63.37	82.49	0.84	0.214	1.43	0.149	1.02	1.00	0.194	No
424	8.48	146.20	63.57	82.63	0.84	0.214	1.43	0.149	1.02	1.00	0.194	No
425	8.50	146.54	63.77	82.77	0.84	0.214	1.43	0.149	1.02	1.00	0.195	No
426	8.52	146.88	63.96	82.91	0.84	0.214	1.43	0.149	1.02	1.00	0.196	No
427	8.54	147.21	64.16	83.05	0.84	0.214	1.43	0.149	1.02	1.00	0.196	No
428	8.56	147.54	64.35	83.19	0.84	0.214	1.43	0.149	1.02	1.00	0.196	No
429	8.58	147.87	64.55	83.32	0.84	0.214	1.43	0.150	1.02	1.00	0.196	No
430	8.60	148.20	64.75	83.45	0.84	0.214	1.43	0.150	1.02	1.00	0.196	No
431	8.62	148.52	64.94	83.58	0.84	0.214	1.43	0.150	1.02	1.00	0.196	No
432	8.64	148.85	65.14	83.71	0.84	0.214	1.43	0.150	1.02	1.00	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	149.17	65.33	83.83	0.84	0.214	1.43	0.150	1.02	1.00	0.196	No
434	8.68	149.49	65.53	83.96	0.84	0.214	1.43	0.150	1.01	1.00	0.196	No
435	8.70	149.81	65.73	84.09	0.84	0.214	1.43	0.150	1.01	1.00	0.197	No
436	8.72	150.14	65.92	84.21	0.84	0.214	1.43	0.150	1.01	1.00	0.197	No
437	8.74	150.46	66.12	84.34	0.84	0.214	1.43	0.150	1.01	1.00	0.197	No
438	8.76	150.78	66.32	84.47	0.84	0.214	1.43	0.150	1.01	1.00	0.197	No
439	8.78	151.10	66.51	84.59	0.84	0.214	1.43	0.150	1.01	1.00	0.197	No
440	8.80	151.43	66.71	84.72	0.84	0.214	1.43	0.150	1.01	1.00	0.196	No
441	8.82	151.75	66.90	84.85	0.84	0.214	1.43	0.150	1.01	1.00	0.196	No
442	8.84	152.09	67.10	84.99	0.84	0.214	1.43	0.150	1.02	1.00	0.194	No
443	8.86	152.43	67.30	85.13	0.83	0.214	1.43	0.150	1.02	1.00	0.194	No
444	8.88	152.78	67.49	85.29	0.83	0.214	1.43	0.150	1.02	1.00	0.193	No
445	8.90	153.13	67.69	85.44	0.83	0.214	1.43	0.150	1.02	1.00	0.193	No
446	8.93	153.64	67.98	85.66	0.83	0.214	1.43	0.150	1.01	1.00	0.194	No
447	8.94	153.81	68.08	85.73	0.83	0.214	1.43	0.150	1.01	1.00	0.195	No
448	8.96	154.15	68.28	85.88	0.83	0.214	1.43	0.150	1.01	1.00	0.196	No
449	8.99	154.66	68.57	86.09	0.83	0.214	1.43	0.150	1.01	1.00	0.197	No
450	9.00	154.83	68.67	86.16	0.83	0.214	1.43	0.150	1.01	1.00	0.197	No
451	9.02	155.16	68.87	86.30	0.83	0.214	1.43	0.150	1.01	1.00	0.196	No
452	9.04	155.50	69.06	86.44	0.83	0.214	1.43	0.150	1.01	1.00	0.195	No
453	9.06	155.84	69.26	86.58	0.83	0.214	1.43	0.150	1.01	1.00	0.195	No
454	9.08	156.18	69.45	86.72	0.83	0.214	1.43	0.150	1.01	1.00	0.195	No
455	9.10	156.52	69.65	86.86	0.83	0.214	1.43	0.150	1.01	1.00	0.195	No
456	9.12	156.86	69.85	87.01	0.83	0.214	1.43	0.150	1.01	1.00	0.195	No
457	9.14	157.20	70.04	87.15	0.83	0.214	1.43	0.150	1.01	1.00	0.195	No
458	9.16	157.54	70.24	87.30	0.83	0.214	1.43	0.150	1.01	1.00	0.195	No
459	9.18	157.88	70.44	87.44	0.83	0.214	1.43	0.150	1.01	1.00	0.196	No
460	9.20	158.21	70.63	87.58	0.83	0.214	1.43	0.150	1.01	1.00	0.197	No
461	9.22	158.55	70.83	87.72	0.83	0.214	1.43	0.150	1.01	1.00	0.197	No
462	9.24	158.88	71.02	87.86	0.83	0.214	1.43	0.150	1.01	1.00	0.197	No
463	9.26	159.22	71.22	88.00	0.83	0.214	1.43	0.149	1.01	1.00	0.196	No
464	9.28	159.56	71.42	88.14	0.83	0.214	1.43	0.149	1.01	1.00	0.196	No
465	9.30	159.89	71.61	88.28	0.82	0.214	1.43	0.149	1.01	1.00	0.196	No
466	9.32	160.23	71.81	88.42	0.82	0.214	1.43	0.149	1.01	1.00	0.196	No
467	9.34	160.56	72.01	88.55	0.82	0.214	1.43	0.149	1.01	1.00	0.196	No
468	9.36	160.89	72.20	88.69	0.82	0.214	1.43	0.149	1.01	1.00	0.196	No
469	9.38	161.23	72.40	88.83	0.82	0.214	1.43	0.149	1.01	1.00	0.196	No
470	9.40	161.57	72.59	88.97	0.82	0.213	1.43	0.149	1.01	1.00	0.196	No
471	9.42	161.90	72.79	89.11	0.82	0.213	1.43	0.149	1.01	1.00	0.197	No
472	9.44	162.24	72.99	89.25	0.82	0.213	1.43	0.149	1.01	1.00	0.197	No
473	9.46	162.58	73.18	89.39	0.82	0.213	1.43	0.149	1.01	1.00	0.196	No
474	9.48	162.91	73.38	89.54	0.82	0.213	1.43	0.149	1.01	1.00	0.196	No
475	9.50	163.25	73.58	89.68	0.82	0.213	1.43	0.149	1.01	1.00	0.195	No
476	9.52	163.60	73.77	89.82	0.82	0.213	1.43	0.149	1.01	1.00	0.195	No
477	9.54	163.94	73.97	89.97	0.82	0.213	1.43	0.149	1.01	1.00	0.195	No
478	9.56	164.28	74.16	90.12	0.82	0.213	1.43	0.149	1.01	1.00	0.195	No
479	9.58	164.63	74.36	90.27	0.82	0.213	1.43	0.149	1.01	1.00	0.195	No
480	9.60	164.97	74.56	90.41	0.82	0.213	1.43	0.149	1.01	1.00	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	165.31	74.75	90.56	0.82	0.213	1.43	0.149	1.01	1.00	0.197	No
482	9.64	165.66	74.95	90.71	0.82	0.213	1.43	0.149	1.01	1.00	0.196	No
483	9.66	166.00	75.14	90.86	0.82	0.213	1.43	0.149	1.01	1.00	0.195	No
484	9.68	166.35	75.34	91.01	0.82	0.213	1.43	0.149	1.01	1.00	0.194	No
485	9.70	166.70	75.54	91.16	0.81	0.213	1.43	0.149	1.01	1.00	0.193	No
486	9.72	167.05	75.73	91.32	0.81	0.213	1.43	0.149	1.01	1.00	0.193	No
487	9.74	167.40	75.93	91.47	0.81	0.213	1.43	0.149	1.01	1.00	0.195	No
488	9.76	167.75	76.13	91.62	0.81	0.213	1.43	0.149	1.01	1.00	0.196	No
489	9.78	168.09	76.32	91.77	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
490	9.80	168.43	76.52	91.91	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
491	9.82	168.77	76.71	92.05	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
492	9.84	169.11	76.91	92.20	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
493	9.86	169.44	77.11	92.34	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
494	9.88	169.78	77.30	92.47	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
495	9.90	170.11	77.50	92.61	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
496	9.92	170.44	77.70	92.74	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
497	9.94	170.76	77.89	92.87	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
498	9.96	171.09	78.09	93.01	0.81	0.213	1.43	0.149	1.01	1.00	0.197	No
499	9.98	171.42	78.28	93.14	0.81	0.213	1.43	0.149	1.01	1.00	0.196	No
500	10.00	171.76	78.48	93.28	0.81	0.213	1.43	0.149	1.01	1.00	0.195	No
501	10.03	172.26	78.77	93.49	0.81	0.213	1.43	0.149	1.01	1.00	0.195	No
502	10.04	172.43	78.87	93.56	0.81	0.213	1.43	0.149	1.01	1.00	0.194	No
503	10.06	172.78	79.07	93.71	0.81	0.213	1.43	0.149	1.01	1.00	0.194	No
504	10.08	173.13	79.26	93.86	0.81	0.213	1.43	0.149	1.01	1.00	0.194	No
505	10.10	173.48	79.46	94.01	0.81	0.213	1.43	0.149	1.01	1.00	0.194	No
506	10.12	173.82	79.66	94.17	0.80	0.212	1.43	0.149	1.01	1.00	0.194	No
507	10.14	174.17	79.85	94.32	0.80	0.212	1.43	0.149	1.01	1.00	0.194	No
508	10.16	174.52	80.05	94.47	0.80	0.212	1.43	0.149	1.01	1.00	0.194	No
509	10.18	174.87	80.25	94.63	0.80	0.212	1.43	0.149	1.01	1.00	0.193	No
510	10.20	175.23	80.44	94.78	0.80	0.212	1.43	0.149	1.01	1.00	0.193	No
511	10.22	175.58	80.64	94.94	0.80	0.212	1.43	0.149	1.01	1.00	0.192	No
512	10.24	175.93	80.83	95.10	0.80	0.212	1.43	0.149	1.01	1.00	0.192	No
513	10.26	176.28	81.03	95.25	0.80	0.212	1.43	0.148	1.01	1.00	0.192	No
514	10.28	176.64	81.23	95.41	0.80	0.212	1.43	0.148	1.01	1.00	0.193	No
515	10.30	176.98	81.42	95.56	0.80	0.212	1.43	0.148	1.01	1.00	0.193	No
516	10.32	177.33	81.62	95.71	0.80	0.212	1.43	0.148	1.01	1.00	0.193	No
517	10.34	177.68	81.82	95.87	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
518	10.36	178.04	82.01	96.03	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
519	10.38	178.39	82.21	96.18	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
520	10.40	178.75	82.40	96.34	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
521	10.42	179.10	82.60	96.50	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
522	10.44	179.44	82.80	96.65	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
523	10.46	179.78	82.99	96.79	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
524	10.48	180.12	83.19	96.93	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
525	10.50	180.45	83.39	97.07	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
526	10.52	180.79	83.58	97.21	0.80	0.212	1.43	0.148	1.00	1.00	2.000	Yes
527	10.54	181.13	83.78	97.36	0.79	0.211	1.43	0.148	1.00	1.00	2.000	Yes
528	10.56	181.49	83.97	97.51	0.79	0.211	1.43	0.148	1.00	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	181.84	84.17	97.67	0.79	0.211	1.43	0.148	1.00	1.00	2.000	Yes
530	10.60	182.20	84.37	97.83	0.79	0.211	1.43	0.148	1.00	1.00	2.000	Yes
531	10.62	182.56	84.56	98.00	0.79	0.211	1.43	0.148	1.00	1.00	2.000	Yes
532	10.64	182.91	84.76	98.16	0.79	0.211	1.43	0.148	1.00	1.00	0.192	No
533	10.66	183.27	84.95	98.32	0.79	0.211	1.43	0.148	1.00	1.00	0.191	No
534	10.68	183.63	85.15	98.48	0.79	0.211	1.43	0.148	1.00	1.00	0.191	No
535	10.70	184.00	85.35	98.65	0.79	0.211	1.43	0.148	1.00	1.00	0.190	No
536	10.72	184.37	85.54	98.82	0.79	0.211	1.43	0.148	1.00	1.00	0.189	No
537	10.74	184.73	85.74	98.99	0.79	0.211	1.43	0.148	1.00	1.00	0.189	No
538	10.76	185.10	85.94	99.16	0.79	0.211	1.43	0.148	1.00	1.00	0.189	No
539	10.78	185.45	86.13	99.32	0.79	0.211	1.43	0.147	1.00	1.00	0.190	No
540	10.80	185.81	86.33	99.48	0.79	0.211	1.43	0.147	1.00	1.00	0.192	No
541	10.82	186.16	86.52	99.63	0.79	0.211	1.43	0.147	1.00	1.00	0.193	No
542	10.84	186.50	86.72	99.78	0.79	0.211	1.43	0.147	1.00	1.00	0.194	No
543	10.86	186.85	86.92	99.93	0.79	0.210	1.43	0.147	1.00	1.00	0.194	No
544	10.88	187.19	87.11	100.08	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
545	10.90	187.53	87.31	100.22	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
546	10.92	187.87	87.51	100.36	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
547	10.94	188.20	87.70	100.50	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
548	10.96	188.54	87.90	100.64	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
549	10.98	188.87	88.09	100.78	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
550	11.00	189.20	88.29	100.91	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
551	11.02	189.53	88.49	101.05	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
552	11.04	189.86	88.68	101.18	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
553	11.06	190.19	88.88	101.32	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
554	11.08	190.53	89.07	101.45	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
555	11.10	190.86	89.27	101.59	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
556	11.12	191.19	89.47	101.73	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
557	11.15	191.69	89.76	101.93	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
558	11.16	191.86	89.86	102.00	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
559	11.18	192.19	90.06	102.13	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
560	11.20	192.52	90.25	102.26	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
561	11.22	192.85	90.45	102.40	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
562	11.24	193.18	90.64	102.53	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
563	11.26	193.51	90.84	102.67	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
564	11.28	193.84	91.04	102.80	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
565	11.30	194.17	91.23	102.93	0.78	0.210	1.43	0.147	1.00	1.00	0.196	No
566	11.32	194.50	91.43	103.07	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
567	11.34	194.82	91.63	103.20	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
568	11.36	195.15	91.82	103.33	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
569	11.38	195.48	92.02	103.46	0.77	0.209	1.43	0.147	1.00	1.00	0.196	No
570	11.40	195.81	92.21	103.59	0.77	0.209	1.43	0.146	1.00	1.00	0.196	No
571	11.42	196.14	92.41	103.73	0.77	0.209	1.43	0.146	1.00	1.00	0.196	No
572	11.44	196.47	92.61	103.86	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
573	11.46	196.80	92.80	104.00	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
574	11.48	197.13	93.00	104.13	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
575	11.50	197.47	93.19	104.27	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
576	11.52	197.80	93.39	104.41	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	198.14	93.59	104.55	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
578	11.56	198.48	93.78	104.69	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
579	11.58	198.81	93.98	104.84	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
580	11.60	199.15	94.18	104.98	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
581	11.62	199.49	94.37	105.12	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
582	11.64	199.83	94.57	105.27	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
583	11.66	200.18	94.76	105.41	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
584	11.68	200.52	94.96	105.56	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
585	11.70	200.86	95.16	105.71	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
586	11.72	201.21	95.35	105.85	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
587	11.74	201.55	95.55	106.00	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
588	11.76	201.89	95.75	106.15	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
589	11.78	202.24	95.94	106.29	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
590	11.80	202.58	96.14	106.44	0.76	0.208	1.43	0.146	1.00	1.00	0.195	No
591	11.82	202.92	96.33	106.58	0.76	0.208	1.43	0.146	1.00	1.00	0.195	No
592	11.84	203.26	96.53	106.73	0.76	0.208	1.43	0.146	1.00	1.00	0.195	No
593	11.86	203.60	96.73	106.88	0.76	0.208	1.43	0.146	1.00	1.00	0.194	No
594	11.88	203.95	96.92	107.02	0.76	0.208	1.43	0.146	1.00	1.00	0.194	No
595	11.90	204.29	97.12	107.17	0.76	0.208	1.43	0.145	1.00	1.00	0.194	No
596	11.93	204.81	97.41	107.40	0.76	0.208	1.43	0.145	1.00	1.00	0.194	No
597	11.94	204.99	97.51	107.47	0.76	0.208	1.43	0.145	1.00	1.00	0.194	No
598	11.96	205.33	97.71	107.63	0.76	0.208	1.43	0.145	1.00	1.00	0.194	No
599	11.98	205.68	97.90	107.78	0.76	0.208	1.43	0.145	0.99	1.00	0.194	No
600	12.00	206.04	98.10	107.94	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
601	12.02	206.39	98.30	108.09	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
602	12.04	206.74	98.49	108.25	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
603	12.06	207.09	98.69	108.40	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
604	12.08	207.44	98.88	108.56	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
605	12.10	207.79	99.08	108.71	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
606	12.12	208.14	99.28	108.87	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
607	12.14	208.49	99.47	109.02	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
608	12.16	208.85	99.67	109.18	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
609	12.18	209.20	99.87	109.33	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
610	12.20	209.55	100.06	109.49	0.76	0.207	1.43	0.145	0.99	1.00	0.193	No
611	12.22	209.90	100.26	109.64	0.75	0.207	1.43	0.145	0.99	1.00	0.193	No
612	12.24	210.25	100.45	109.80	0.75	0.207	1.43	0.145	0.99	1.00	0.193	No
613	12.26	210.60	100.65	109.95	0.75	0.207	1.43	0.145	0.99	1.00	0.193	No
614	12.28	210.96	100.85	110.11	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
615	12.30	211.31	101.04	110.27	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
616	12.33	211.84	101.34	110.50	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
617	12.34	212.02	101.44	110.58	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
618	12.36	212.37	101.63	110.74	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
619	12.38	212.73	101.83	110.90	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No
620	12.40	213.08	102.02	111.06	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No
621	12.42	213.44	102.22	111.22	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No
622	12.44	213.80	102.42	111.38	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No
623	12.46	214.16	102.61	111.55	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No
624	12.48	214.52	102.81	111.71	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	214.88	103.01	111.88	0.75	0.206	1.43	0.144	0.99	1.00	0.192	No
626	12.52	215.25	103.20	112.05	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
627	12.54	215.61	103.40	112.21	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
628	12.56	215.97	103.59	112.38	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
629	12.58	216.34	103.79	112.55	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
630	12.60	216.70	103.99	112.71	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
631	12.62	217.06	104.18	112.88	0.75	0.205	1.43	0.143	0.99	1.00	0.192	No
632	12.64	217.42	104.38	113.04	0.74	0.205	1.43	0.143	0.99	1.00	0.192	No
633	12.66	217.78	104.57	113.21	0.74	0.205	1.43	0.143	0.99	1.00	0.192	No
634	12.68	218.14	104.77	113.37	0.74	0.205	1.43	0.143	0.99	1.00	0.192	No
635	12.70	218.50	104.97	113.53	0.74	0.205	1.43	0.143	0.99	1.00	0.192	No
636	12.72	218.86	105.16	113.69	0.74	0.205	1.43	0.143	0.99	1.00	0.192	No
637	12.74	219.21	105.36	113.85	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
638	12.76	219.56	105.56	114.01	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
639	12.78	219.91	105.75	114.16	0.74	0.204	1.43	0.143	0.99	1.00	0.193	No
640	12.81	220.43	106.05	114.39	0.74	0.204	1.43	0.143	0.99	1.00	0.193	No
641	12.82	220.60	106.14	114.46	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
642	12.84	220.94	106.34	114.60	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
643	12.86	221.28	106.54	114.75	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
644	12.88	221.62	106.73	114.89	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
645	12.90	221.95	106.93	115.02	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
646	12.92	222.28	107.13	115.16	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
647	12.94	222.61	107.32	115.29	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
648	12.96	222.94	107.52	115.42	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
649	12.98	223.26	107.71	115.55	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
650	13.00	223.58	107.91	115.67	0.74	0.204	1.43	0.142	0.99	1.00	0.192	No
651	13.02	223.90	108.11	115.80	0.74	0.204	1.43	0.142	0.99	1.00	0.192	No
652	13.04	224.22	108.30	115.92	0.74	0.203	1.43	0.142	0.99	1.00	0.192	No
653	13.06	224.54	108.50	116.04	0.74	0.203	1.43	0.142	0.99	1.00	0.192	No
654	13.08	224.85	108.69	116.16	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
655	13.10	225.17	108.89	116.28	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
656	13.12	225.49	109.09	116.40	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
657	13.15	225.97	109.38	116.59	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
658	13.16	226.13	109.48	116.65	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
659	13.18	226.46	109.68	116.78	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
660	13.20	226.78	109.87	116.91	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
661	13.22	227.11	110.07	117.04	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
662	13.24	227.44	110.26	117.18	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
663	13.26	227.77	110.46	117.31	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
664	13.29	228.26	110.75	117.51	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
665	13.30	228.43	110.85	117.58	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
666	13.32	228.76	111.05	117.71	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
667	13.34	229.08	111.25	117.84	0.73	0.203	1.43	0.142	0.99	1.00	0.192	No
668	13.36	229.41	111.44	117.97	0.73	0.202	1.43	0.142	0.99	1.00	0.192	No
669	13.38	229.73	111.64	118.10	0.73	0.202	1.43	0.142	0.99	1.00	0.192	No
670	13.40	230.06	111.83	118.22	0.73	0.202	1.43	0.142	0.99	1.00	0.192	No
671	13.42	230.38	112.03	118.35	0.73	0.202	1.43	0.142	0.99	1.00	0.192	No
672	13.44	230.70	112.23	118.47	0.73	0.202	1.43	0.142	0.99	1.00	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	231.02	112.42	118.60	0.73	0.202	1.43	0.142	0.99	1.00	0.191	No
674	13.49	231.50	112.72	118.78	0.73	0.202	1.43	0.141	0.99	1.00	0.191	No
675	13.50	231.66	112.82	118.84	0.72	0.202	1.43	0.141	0.99	1.00	0.191	No
676	13.52	231.98	113.01	118.97	0.72	0.202	1.43	0.141	0.99	1.00	0.191	No
677	13.54	232.30	113.21	119.09	0.72	0.202	1.43	0.141	0.99	1.00	0.191	No
678	13.56	232.63	113.40	119.22	0.72	0.202	1.43	0.141	0.99	1.00	0.190	No
679	13.58	232.96	113.60	119.36	0.72	0.202	1.43	0.141	0.99	1.00	0.189	No
680	13.60	233.29	113.80	119.50	0.72	0.202	1.43	0.141	0.99	1.00	0.189	No
681	13.62	233.64	113.99	119.64	0.72	0.202	1.43	0.141	0.99	1.00	0.189	No
682	13.64	233.98	114.19	119.80	0.72	0.202	1.43	0.141	0.99	1.00	0.188	No
683	13.66	234.33	114.38	119.95	0.72	0.201	1.43	0.141	0.98	1.00	0.187	No
684	13.68	234.69	114.58	120.11	0.72	0.201	1.43	0.141	0.98	1.00	0.187	No
685	13.70	235.05	114.78	120.27	0.72	0.201	1.43	0.141	0.98	1.00	0.186	No
686	13.72	235.41	114.97	120.43	0.72	0.201	1.43	0.141	0.98	1.00	0.186	No
687	13.74	235.77	115.17	120.60	0.72	0.201	1.43	0.141	0.98	1.00	0.186	No
688	13.76	236.12	115.37	120.76	0.72	0.201	1.43	0.141	0.98	1.00	0.186	No
689	13.78	236.47	115.56	120.91	0.72	0.201	1.43	0.141	0.98	1.00	0.188	No
690	13.81	236.99	115.86	121.13	0.72	0.201	1.43	0.141	0.98	1.00	0.188	No
691	13.82	237.16	115.95	121.21	0.72	0.201	1.43	0.141	0.98	1.00	0.188	No
692	13.84	237.51	116.15	121.36	0.72	0.201	1.43	0.140	0.98	1.00	0.187	No
693	13.86	237.86	116.35	121.51	0.72	0.201	1.43	0.140	0.98	1.00	0.187	No
694	13.88	238.21	116.54	121.67	0.72	0.201	1.43	0.140	0.98	1.00	0.187	No
695	13.90	238.57	116.74	121.83	0.72	0.200	1.43	0.140	0.98	1.00	0.187	No
696	13.92	238.92	116.94	121.99	0.72	0.200	1.43	0.140	0.98	1.00	0.187	No
697	13.94	239.27	117.13	122.14	0.71	0.200	1.43	0.140	0.98	1.00	0.187	No
698	13.96	239.63	117.33	122.30	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
699	13.98	239.97	117.52	122.45	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
700	14.00	240.32	117.72	122.60	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
701	14.02	240.67	117.92	122.75	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
702	14.04	241.02	118.11	122.91	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
703	14.06	241.37	118.31	123.06	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
704	14.08	241.72	118.50	123.22	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
705	14.10	242.07	118.70	123.37	0.71	0.200	1.43	0.140	0.98	1.00	0.188	No
706	14.12	242.42	118.90	123.52	0.71	0.199	1.43	0.140	0.98	1.00	0.188	No
707	14.15	242.94	119.19	123.75	0.71	0.199	1.43	0.140	0.98	1.00	0.189	No
708	14.16	243.11	119.29	123.82	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
709	14.18	243.45	119.49	123.97	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
710	14.20	243.80	119.68	124.11	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
711	14.22	244.14	119.88	124.26	0.71	0.199	1.43	0.139	0.98	1.00	0.187	No
712	14.24	244.48	120.07	124.41	0.71	0.199	1.43	0.139	0.98	1.00	0.187	No
713	14.26	244.83	120.27	124.56	0.71	0.199	1.43	0.139	0.98	1.00	0.187	No
714	14.28	245.17	120.47	124.70	0.71	0.199	1.43	0.139	0.98	1.00	0.187	No
715	14.30	245.51	120.66	124.84	0.71	0.199	1.43	0.139	0.98	1.00	0.187	No
716	14.32	245.85	120.86	124.99	0.71	0.199	1.43	0.139	0.98	1.00	0.188	No
717	14.34	246.19	121.06	125.13	0.71	0.199	1.43	0.139	0.98	1.00	0.188	No
718	14.36	246.53	121.25	125.28	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
719	14.38	246.87	121.45	125.42	0.70	0.198	1.43	0.139	0.98	1.00	0.188	No
720	14.40	247.21	121.64	125.57	0.70	0.198	1.43	0.139	0.98	1.00	0.189	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	247.55	121.84	125.71	0.70	0.198	1.43	0.139	0.98	1.00	0.188	No
722	14.44	247.89	122.04	125.85	0.70	0.198	1.43	0.139	0.98	1.00	0.187	No
723	14.46	248.23	122.23	126.00	0.70	0.198	1.43	0.139	0.98	1.00	0.186	No
724	14.48	248.57	122.43	126.14	0.70	0.198	1.43	0.139	0.98	1.00	0.186	No
725	14.50	248.91	122.63	126.29	0.70	0.198	1.43	0.139	0.98	1.00	0.186	No
726	14.52	249.25	122.82	126.43	0.70	0.198	1.43	0.138	0.98	1.00	0.187	No
727	14.54	249.59	123.02	126.57	0.70	0.198	1.43	0.138	0.98	1.00	0.187	No
728	14.56	249.93	123.21	126.72	0.70	0.198	1.43	0.138	0.98	1.00	0.187	No
729	14.58	250.27	123.41	126.86	0.70	0.198	1.43	0.138	0.98	1.00	0.188	No
730	14.60	250.61	123.61	127.01	0.70	0.197	1.43	0.138	0.98	1.00	0.188	No
731	14.62	250.95	123.80	127.15	0.70	0.197	1.43	0.138	0.98	1.00	0.188	No
732	14.64	251.29	124.00	127.29	0.70	0.197	1.43	0.138	0.98	1.00	0.188	No
733	14.66	251.63	124.19	127.44	0.70	0.197	1.43	0.138	0.98	1.00	0.186	No
734	14.68	251.98	124.39	127.59	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes
735	14.70	252.32	124.59	127.73	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes
736	14.72	252.66	124.78	127.88	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes
737	14.74	253.00	124.98	128.02	0.70	0.197	1.43	0.138	0.98	1.00	2.000	Yes
738	14.76	253.34	125.18	128.16	0.70	0.197	1.43	0.138	0.98	1.00	0.184	No
739	14.78	253.68	125.37	128.31	0.70	0.197	1.43	0.138	0.98	1.00	0.184	No
740	14.80	254.03	125.57	128.46	0.70	0.197	1.43	0.138	0.98	1.00	0.185	No
741	14.82	254.38	125.76	128.62	0.69	0.197	1.43	0.138	0.98	1.00	0.185	No
742	14.85	254.91	126.06	128.85	0.69	0.196	1.43	0.137	0.98	1.00	0.183	No
743	14.86	255.09	126.16	128.93	0.69	0.196	1.43	0.137	0.98	1.00	0.182	No
744	14.88	255.44	126.35	129.09	0.69	0.196	1.43	0.137	0.98	1.00	0.182	No
745	14.90	255.79	126.55	129.24	0.69	0.196	1.43	0.137	0.98	1.00	0.182	No
746	14.92	256.14	126.75	129.39	0.69	0.196	1.43	0.137	0.98	1.00	0.183	No
747	14.94	256.48	126.94	129.54	0.69	0.196	1.43	0.137	0.98	1.00	2.000	Yes
748	14.97	256.99	127.24	129.76	0.69	0.196	1.43	0.137	0.98	1.00	2.000	Yes
749	14.98	257.17	127.33	129.83	0.69	0.196	1.43	0.137	0.98	1.00	2.000	Yes
750	15.00	257.52	127.53	129.99	0.69	0.196	1.43	0.137	0.98	1.00	2.000	Yes
751	15.02	257.88	127.73	130.15	0.69	0.196	1.43	0.137	0.98	1.00	0.182	No
752	15.04	258.24	127.92	130.32	0.69	0.196	1.43	0.137	0.98	1.00	0.181	No
753	15.06	258.61	128.12	130.49	0.69	0.195	1.43	0.137	0.98	1.00	0.181	No
754	15.08	258.97	128.31	130.65	0.69	0.195	1.43	0.137	0.98	1.00	0.183	No
755	15.10	259.32	128.51	130.81	0.69	0.195	1.43	0.137	0.98	1.00	0.184	No
756	15.13	259.84	128.81	131.03	0.69	0.195	1.43	0.137	0.98	1.00	0.185	No
757	15.14	260.01	128.90	131.10	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
758	15.16	260.35	129.10	131.25	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
759	15.18	260.68	129.30	131.39	0.69	0.195	1.43	0.136	0.98	1.00	0.185	No
760	15.20	261.03	129.49	131.53	0.69	0.195	1.43	0.136	0.98	1.00	0.185	No
761	15.22	261.37	129.69	131.68	0.69	0.195	1.43	0.136	0.98	1.00	0.185	No
762	15.24	261.71	129.88	131.82	0.69	0.195	1.43	0.136	0.98	1.00	0.185	No
763	15.26	262.05	130.08	131.97	0.69	0.195	1.43	0.136	0.98	1.00	0.185	No
764	15.28	262.39	130.28	132.12	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
765	15.30	262.74	130.47	132.26	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
766	15.32	263.08	130.67	132.41	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
767	15.34	263.42	130.87	132.56	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
768	15.36	263.77	131.06	132.71	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	264.11	131.26	132.85	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
770	15.40	264.45	131.45	132.99	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
771	15.42	264.78	131.65	133.13	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
772	15.44	265.12	131.85	133.27	0.68	0.194	1.43	0.136	0.98	1.00	0.184	No
773	15.46	265.45	132.04	133.41	0.68	0.194	1.43	0.136	0.98	1.00	0.184	No
774	15.48	265.79	132.24	133.55	0.68	0.194	1.43	0.136	0.98	1.00	0.183	No
775	15.50	266.13	132.44	133.70	0.68	0.194	1.43	0.135	0.98	1.00	0.183	No
776	15.52	266.48	132.63	133.85	0.68	0.193	1.43	0.135	0.98	1.00	0.183	No
777	15.54	266.82	132.83	133.99	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No
778	15.56	267.17	133.02	134.15	0.68	0.193	1.43	0.135	0.98	1.00	0.183	No
779	15.58	267.52	133.22	134.30	0.68	0.193	1.43	0.135	0.98	1.00	0.182	No
780	15.60	267.87	133.42	134.45	0.68	0.193	1.43	0.135	0.98	1.00	0.182	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.14	100.00	3.41	0.62	1.70	1.88	0.00	1.88	4.000	No	Yes	2.00
2	0.04	0.22	100.00	3.35	0.61	1.70	2.97	0.00	2.97	4.000	No	Yes	2.00
3	0.06	0.31	100.00	3.22	0.60	1.70	5.06	0.00	5.06	4.000	No	Yes	2.00
4	0.08	0.41	100.00	3.12	0.59	1.70	7.14	0.00	7.14	4.000	No	Yes	2.00
5	0.11	0.47	100.00	3.09	0.59	1.70	7.90	0.00	7.90	4.000	No	Yes	2.00
6	0.12	0.47	100.00	3.15	0.59	1.70	8.09	0.00	8.09	4.000	No	Yes	2.00
7	0.14	0.45	100.00	3.23	0.59	1.70	7.44	0.00	7.44	4.000	No	Yes	2.00
8	0.16	0.42	100.00	3.34	0.59	1.70	7.14	0.00	7.14	4.000	No	Yes	2.00
9	0.18	0.39	100.00	3.42	0.60	1.70	6.39	0.00	6.39	4.000	No	Yes	2.00
10	0.20	0.35	100.00	3.50	0.60	1.70	6.01	0.00	6.01	4.000	No	Yes	2.00
11	0.22	0.33	100.00	3.55	0.60	1.70	5.34	0.00	5.34	4.000	No	Yes	2.00
12	0.24	0.31	100.00	3.60	0.60	1.70	5.12	0.00	5.12	4.000	No	Yes	2.00
13	0.26	0.29	100.00	3.61	0.60	1.70	4.89	0.00	4.89	4.000	No	Yes	2.00
14	0.28	0.28	100.00	3.64	0.60	1.70	4.68	0.00	4.68	4.000	No	Yes	2.00
15	0.30	0.27	100.00	3.63	0.61	1.70	4.27	0.00	4.27	4.000	No	Yes	2.00
16	0.32	0.29	100.00	3.57	0.60	1.70	4.78	0.00	4.78	4.000	No	Yes	2.00
17	0.34	0.33	100.00	3.47	0.60	1.70	5.59	0.00	5.59	4.000	No	Yes	2.00
18	0.36	0.38	100.00	3.38	0.60	1.70	6.29	0.00	6.29	4.000	No	Yes	2.00
19	0.38	0.43	100.00	3.31	0.59	1.70	7.26	0.00	7.26	4.000	No	Yes	2.00
20	0.40	0.50	100.00	3.23	0.59	1.70	8.15	0.00	8.15	4.000	No	Yes	2.00
21	0.42	0.56	100.00	3.17	0.58	1.70	9.50	0.00	9.50	4.000	No	Yes	2.00
22	0.44	0.63	100.00	3.13	0.58	1.70	10.69	0.00	10.69	4.000	No	Yes	2.00
23	0.46	0.68	100.00	3.11	0.58	1.70	11.52	0.00	11.52	4.000	No	Yes	2.00
24	0.48	0.69	100.00	3.14	0.57	1.70	12.00	0.00	12.00	4.000	No	Yes	2.00
25	0.50	0.67	100.00	3.20	0.58	1.70	11.38	0.00	11.38	4.000	No	Yes	2.00
26	0.52	0.63	100.00	3.27	0.58	1.70	10.39	0.00	10.39	4.000	No	Yes	2.00
27	0.54	0.60	100.00	3.32	0.58	1.70	9.93	0.00	9.93	4.000	No	Yes	2.00
28	0.56	0.59	100.00	3.35	0.58	1.70	9.77	0.00	9.77	4.000	No	Yes	2.00
29	0.58	0.59	100.00	3.35	0.58	1.70	9.83	0.00	9.83	4.000	No	Yes	2.00
30	0.60	0.61	100.00	3.34	0.58	1.70	10.42	0.00	10.42	4.000	No	Yes	2.00
31	0.62	0.64	100.00	3.30	0.58	1.70	10.71	0.00	10.71	4.000	No	Yes	2.00
32	0.64	0.66	100.00	3.28	0.58	1.70	11.14	0.00	11.14	4.000	No	Yes	2.00
33	0.66	0.68	100.00	3.25	0.58	1.70	11.27	0.00	11.27	4.000	No	Yes	2.00
34	0.68	0.68	100.00	3.23	0.58	1.70	11.82	0.00	11.82	4.000	No	Yes	2.00
35	0.70	0.69	100.00	3.22	0.58	1.70	11.45	0.00	11.45	4.000	No	Yes	2.00
36	0.72	0.69	100.00	3.22	0.58	1.70	11.51	0.00	11.51	4.000	No	Yes	2.00
37	0.74	0.70	100.00	3.20	0.58	1.70	11.71	0.00	11.71	4.000	No	Yes	2.00
38	0.76	0.72	100.00	3.18	0.57	1.70	12.28	0.00	12.28	4.000	No	Yes	2.00
39	0.78	0.75	100.00	3.16	0.57	1.70	12.48	0.00	12.48	4.000	No	Yes	2.00
40	0.80	0.78	100.00	3.14	0.57	1.70	13.06	0.00	13.06	4.000	No	Yes	2.00
41	0.82	0.82	100.00	3.12	0.57	1.70	13.67	0.00	13.67	4.000	No	Yes	2.00
42	0.84	0.88	100.00	3.08	0.57	1.70	14.47	0.00	14.47	4.000	No	Yes	2.00
43	0.86	0.95	100.00	3.05	0.56	1.70	16.02	0.00	16.02	4.000	No	Yes	2.00
44	0.88	1.03	100.00	3.02	0.56	1.70	17.08	0.00	17.08	4.000	No	Yes	2.00
45	0.90	1.10	100.00	3.00	0.55	1.70	18.44	0.00	18.44	4.000	No	Yes	2.00
46	0.92	1.17	100.00	2.98	0.55	1.70	19.60	0.00	19.60	4.000	No	Yes	2.00
47	0.96	1.22	100.00	2.97	0.54	1.70	20.77	0.00	20.77	4.000	No	Yes	2.00
48	0.96	1.25	100.00	2.98	0.54	1.70	20.88	0.00	20.88	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	1.22	100.00	3.00	0.54	1.70	20.62	0.00	20.62	4.000	No	Yes	2.00
50	1.00	1.19	100.00	3.04	0.55	1.70	19.74	0.00	19.74	4.000	No	Yes	2.00
51	1.02	1.14	100.00	3.07	0.55	1.70	19.09	0.00	19.09	4.000	No	Yes	2.00
52	1.04	1.09	100.00	3.10	0.55	1.70	18.33	0.00	18.33	4.000	No	Yes	2.00
53	1.06	1.04	100.00	3.14	0.56	1.70	17.25	0.00	17.25	4.000	No	Yes	2.00
54	1.08	0.98	100.00	3.16	0.56	1.70	16.26	0.00	16.26	4.000	No	Yes	2.00
55	1.10	0.95	100.00	3.18	0.56	1.70	15.60	0.00	15.60	4.000	No	Yes	2.00
56	1.12	0.93	100.00	3.18	0.56	1.70	15.43	0.00	15.43	4.000	No	Yes	2.00
57	1.14	0.92	100.00	3.17	0.56	1.70	15.19	0.00	15.19	4.000	No	Yes	2.00
58	1.16	0.93	100.00	3.15	0.56	1.70	15.32	0.00	15.32	4.000	No	Yes	2.00
59	1.18	0.96	100.00	3.11	0.56	1.70	15.94	0.00	15.94	4.000	No	Yes	2.00
60	1.21	1.00	100.00	3.07	0.56	1.70	16.64	0.00	16.64	4.000	No	Yes	2.00
61	1.22	1.05	100.00	3.03	0.55	1.70	17.45	0.00	17.45	4.000	No	Yes	2.00
62	1.24	1.10	100.00	3.00	0.55	1.70	18.15	0.00	18.15	4.000	No	Yes	2.00
63	1.26	1.14	100.00	2.98	0.55	1.70	19.23	0.00	19.23	4.000	No	Yes	2.00
64	1.28	1.18	99.99	2.96	0.55	1.70	19.59	0.00	19.59	4.000	No	Yes	2.00
65	1.30	1.20	100.00	2.97	0.55	1.70	20.10	0.00	20.10	4.000	No	Yes	2.00
66	1.32	1.21	100.00	2.98	0.54	1.70	20.42	0.00	20.42	4.000	No	Yes	2.00
67	1.34	1.21	100.00	3.00	0.55	1.70	20.02	0.00	20.02	4.000	No	Yes	2.00
68	1.36	1.20	100.00	3.03	0.55	1.70	20.01	0.00	20.01	4.000	No	Yes	2.00
69	1.38	1.19	100.00	3.05	0.55	1.70	19.76	0.00	19.76	4.000	No	Yes	2.00
70	1.40	1.19	100.00	3.06	0.55	1.70	19.85	0.00	19.85	4.000	No	Yes	2.00
71	1.42	1.20	100.00	3.06	0.55	1.70	19.98	0.00	19.98	4.000	No	Yes	2.00
72	1.44	1.20	100.00	3.05	0.55	1.70	19.92	0.00	19.92	4.000	No	Yes	2.00
73	1.46	1.21	100.00	3.04	0.55	1.70	20.05	0.00	20.05	4.000	No	Yes	2.00
74	1.48	1.22	100.00	3.03	0.54	1.70	20.52	0.00	20.52	4.000	No	Yes	2.00
75	1.50	1.23	100.00	3.03	0.54	1.70	20.42	0.00	20.42	4.000	No	Yes	2.00
76	1.52	1.25	100.00	3.02	0.54	1.70	20.51	0.00	20.51	4.000	No	Yes	2.00
77	1.54	1.25	100.00	3.02	0.54	1.70	21.21	0.00	21.21	4.000	No	Yes	2.00
78	1.56	1.24	100.00	3.03	0.54	1.70	20.66	0.00	20.66	4.000	No	Yes	2.00
79	1.58	1.21	100.00	3.05	0.55	1.70	19.80	0.00	19.80	4.000	No	Yes	2.00
80	1.60	1.18	100.00	3.07	0.55	1.70	19.82	0.00	19.82	4.000	No	Yes	2.00
81	1.62	1.16	100.00	3.07	0.55	1.70	19.00	0.00	19.00	4.000	No	Yes	2.00
82	1.64	1.15	100.00	3.07	0.55	1.70	18.79	0.00	18.79	4.000	No	Yes	2.00
83	1.66	1.18	100.00	3.04	0.55	1.70	19.44	0.00	19.44	4.000	No	Yes	2.00
84	1.68	1.23	100.00	3.01	0.54	1.70	20.29	0.00	20.29	4.000	No	Yes	2.00
85	1.70	1.28	100.00	2.97	0.54	1.70	21.06	0.00	21.06	4.000	No	Yes	2.00
86	1.72	1.32	98.29	2.94	0.54	1.70	21.94	0.00	21.94	4.000	No	Yes	2.00
87	1.74	1.34	96.49	2.92	0.54	1.70	22.46	0.00	22.46	4.000	No	Yes	2.00
88	1.76	1.35	96.36	2.92	0.54	1.70	22.40	0.00	22.40	4.000	No	Yes	2.00
89	1.78	1.33	97.16	2.93	0.54	1.70	22.15	0.00	22.15	4.000	No	Yes	2.00
90	1.80	1.31	98.70	2.95	0.54	1.70	21.83	0.00	21.83	4.000	No	Yes	2.00
91	1.82	1.27	100.00	2.98	0.54	1.70	21.17	0.00	21.17	4.000	No	Yes	2.00
92	1.84	1.23	100.00	3.01	0.55	1.70	20.17	0.00	20.17	4.000	No	Yes	2.00
93	1.86	1.19	100.00	3.05	0.55	1.70	19.96	0.00	19.96	4.000	No	Yes	2.00
94	1.88	1.16	100.00	3.07	0.55	1.70	19.33	0.00	19.33	4.000	No	Yes	2.00
95	1.90	1.14	100.00	3.08	0.55	1.70	18.71	0.00	18.71	4.000	No	Yes	2.00
96	1.92	1.14	100.00	3.08	0.55	1.70	18.88	0.00	18.88	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.96	1.13	100.00	3.08	0.55	1.70	18.92	0.00	18.92	4.000	No	Yes	2.00
98	1.96	1.11	100.00	3.08	0.55	1.70	18.51	0.00	18.51	4.000	No	Yes	2.00
99	1.98	1.06	100.00	3.11	0.55	1.70	17.60	0.00	17.60	4.000	No	Yes	2.00
100	2.00	1.01	100.00	3.13	0.56	1.70	16.69	0.00	16.69	4.000	No	Yes	2.00
101	2.02	0.98	100.00	3.16	0.56	1.70	16.15	0.00	16.15	4.000	No	Yes	2.00
102	2.04	0.95	100.00	3.18	0.56	1.70	15.73	0.00	15.73	4.000	No	Yes	2.00
103	2.06	0.90	100.00	3.21	0.56	1.70	15.08	0.00	15.08	4.000	No	Yes	2.00
104	2.08	0.86	100.00	3.24	0.57	1.70	14.12	0.00	14.12	4.000	No	Yes	2.00
105	2.10	0.82	100.00	3.25	0.57	1.70	13.43	0.00	13.43	4.000	No	Yes	2.00
106	2.12	0.80	100.00	3.25	0.57	1.70	13.05	0.00	13.05	4.000	No	Yes	2.00
107	2.14	0.80	100.00	3.23	0.57	1.70	12.96	0.00	12.96	4.000	No	Yes	2.00
108	2.16	0.83	100.00	3.18	0.57	1.70	13.18	0.00	13.18	4.000	No	Yes	2.00
109	2.18	0.89	100.00	3.11	0.57	1.70	14.31	0.00	14.31	4.000	No	Yes	2.00
110	2.20	0.96	100.00	3.03	0.56	1.70	15.80	0.00	15.80	4.000	No	Yes	2.00
111	2.23	1.04	99.13	2.95	0.56	1.69	16.87	0.00	16.87	4.000	No	Yes	2.00
112	2.24	1.08	95.49	2.91	0.55	1.68	18.32	0.00	18.32	4.000	No	Yes	2.00
113	2.26	1.11	92.83	2.87	0.55	1.68	17.96	0.00	17.96	4.000	No	Yes	2.00
114	2.28	1.12	92.37	2.87	0.55	1.67	18.30	0.00	18.30	4.000	No	Yes	2.00
115	2.30	1.13	92.48	2.87	0.55	1.66	18.45	0.00	18.45	4.000	No	Yes	2.00
116	2.32	1.11	95.32	2.90	0.55	1.65	18.11	0.00	18.11	4.000	No	Yes	2.00
117	2.34	1.08	99.61	2.96	0.56	1.65	17.28	0.00	17.28	4.000	No	Yes	2.00
118	2.36	1.03	100.00	3.02	0.56	1.64	16.47	0.00	16.47	4.000	No	Yes	2.00
119	2.38	1.00	100.00	3.06	0.56	1.64	15.94	0.00	15.94	4.000	No	Yes	2.00
120	2.40	0.98	100.00	3.09	0.56	1.63	15.49	0.00	15.49	4.000	No	Yes	2.00
121	2.42	0.99	100.00	3.09	0.56	1.63	15.41	0.00	15.41	4.000	No	Yes	2.00
122	2.44	1.01	100.00	3.08	0.56	1.61	16.13	0.00	16.13	4.000	No	Yes	2.00
123	2.46	1.04	100.00	3.05	0.56	1.61	16.05	0.00	16.05	4.000	No	Yes	2.00
124	2.48	1.06	100.00	3.03	0.56	1.60	16.52	0.00	16.52	4.000	No	Yes	2.00
125	2.50	1.08	100.00	3.00	0.56	1.59	16.71	0.00	16.71	4.000	No	Yes	2.00
126	2.52	1.11	100.00	2.98	0.56	1.58	17.11	0.00	17.11	4.000	No	Yes	2.00
127	2.54	1.13	100.00	2.97	0.55	1.58	17.48	0.00	17.48	4.000	No	Yes	2.00
128	2.56	1.13	100.00	2.97	0.55	1.58	17.51	0.00	17.51	4.000	No	Yes	2.00
129	2.58	1.12	100.00	2.98	0.56	1.57	17.27	0.00	17.27	4.000	No	Yes	2.00
130	2.60	1.09	100.00	3.01	0.56	1.57	16.87	0.00	16.87	4.000	No	Yes	2.00
131	2.62	1.07	100.00	3.03	0.56	1.57	16.33	0.00	16.33	4.000	No	Yes	2.00
132	2.64	1.05	100.00	3.06	0.56	1.57	16.23	0.00	16.23	4.000	No	Yes	2.00
133	2.66	1.03	100.00	3.08	0.56	1.57	15.86	0.00	15.86	4.000	No	Yes	2.00
134	2.68	1.01	100.00	3.10	0.56	1.57	15.39	0.00	15.39	4.000	No	Yes	2.00
135	2.70	0.98	100.00	3.12	0.56	1.57	14.85	0.00	14.85	4.000	No	Yes	2.00
136	2.72	0.95	100.00	3.13	0.56	1.56	14.59	0.00	14.59	4.000	No	Yes	2.00
137	2.74	0.92	100.00	3.15	0.57	1.56	13.92	0.00	13.92	4.000	No	Yes	2.00
138	2.76	0.89	100.00	3.16	0.57	1.56	13.56	0.00	13.56	4.000	No	Yes	2.00
139	2.78	0.87	100.00	3.16	0.57	1.56	13.09	0.00	13.09	4.000	No	Yes	2.00
140	2.80	0.84	100.00	3.16	0.57	1.56	12.79	0.00	12.79	4.000	No	Yes	2.00
141	2.82	0.83	100.00	3.15	0.57	1.56	12.46	0.00	12.46	4.000	No	Yes	2.00
142	2.84	0.82	100.00	3.13	0.57	1.56	12.30	0.00	12.30	4.000	No	Yes	2.00
143	2.86	0.81	100.00	3.12	0.57	1.56	12.08	0.00	12.08	4.000	No	Yes	2.00
144	2.88	0.80	100.00	3.08	0.58	1.55	11.79	0.00	11.79	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.91	0.80	100.00	3.05	0.58	1.55	11.78	0.00	11.78	4.000	No	Yes	2.00
146	2.92	0.79	100.00	3.02	0.58	1.55	11.77	0.00	11.77	4.000	No	Yes	2.00
147	2.94	0.76	100.00	3.03	0.58	1.55	11.12	0.00	11.12	4.000	No	Yes	2.00
148	2.96	0.72	100.00	3.05	0.58	1.55	10.70	0.00	10.70	4.000	No	Yes	2.00
149	2.98	0.68	100.00	3.09	0.58	1.55	10.15	0.00	10.15	4.000	No	Yes	2.00
150	3.00	0.64	100.00	3.12	0.58	1.55	9.40	0.00	9.40	4.000	No	Yes	2.00
151	3.02	0.61	100.00	3.16	0.59	1.55	8.92	0.00	8.92	4.000	No	Yes	2.00
152	3.04	0.60	100.00	3.16	0.59	1.55	8.54	0.00	8.54	4.000	No	Yes	2.00
153	3.06	0.61	100.00	3.14	0.59	1.54	8.69	0.00	8.69	4.000	No	Yes	2.00
154	3.08	0.61	100.00	3.12	0.59	1.54	8.85	0.00	8.85	4.000	No	Yes	2.00
155	3.10	0.62	100.00	3.10	0.59	1.54	8.80	0.00	8.80	4.000	No	Yes	2.00
156	3.12	0.62	100.00	3.08	0.59	1.54	8.83	0.00	8.83	4.000	No	Yes	2.00
157	3.14	0.63	100.00	3.05	0.59	1.53	8.95	0.00	8.95	4.000	No	Yes	2.00
158	3.16	0.66	100.00	3.00	0.59	1.53	9.10	0.00	9.10	4.000	No	Yes	2.00
159	3.18	0.69	98.73	2.95	0.58	1.53	9.75	0.00	9.75	4.000	No	Yes	2.00
160	3.21	0.75	94.35	2.89	0.58	1.52	10.37	0.00	10.37	4.000	No	Yes	2.00
161	3.22	0.80	90.37	2.84	0.58	1.52	11.35	0.00	11.35	4.000	No	Yes	2.00
162	3.24	0.86	86.80	2.80	0.58	1.51	12.17	0.00	12.17	4.000	No	Yes	2.00
163	3.26	0.94	82.84	2.75	0.58	1.51	12.94	0.00	12.94	4.000	No	Yes	2.00
164	3.28	1.04	79.06	2.70	0.57	1.50	14.71	0.00	14.71	4.000	No	Yes	2.00
165	3.30	1.17	75.91	2.66	0.57	1.49	16.47	0.00	16.47	4.000	No	Yes	2.00
166	3.32	1.27	74.71	2.65	0.56	1.48	18.48	0.00	18.48	4.000	No	Yes	2.00
167	3.34	1.36	75.32	2.65	0.55	1.48	19.61	0.00	19.61	4.000	No	Yes	2.00
168	3.36	1.39	78.27	2.69	0.55	1.47	20.35	0.00	20.35	4.000	No	Yes	2.00
169	3.38	1.39	81.97	2.74	0.55	1.47	19.96	0.00	19.96	4.000	No	Yes	2.00
170	3.40	1.37	87.14	2.80	0.55	1.46	19.66	0.00	19.66	4.000	No	Yes	2.00
171	3.42	1.32	92.52	2.87	0.55	1.46	19.05	0.00	19.05	4.000	No	Yes	2.00
172	3.44	1.28	97.25	2.93	0.55	1.46	17.98	0.00	17.98	4.000	No	Yes	2.00
173	3.46	1.22	100.00	2.98	0.55	1.46	17.76	0.00	17.76	4.000	No	Yes	2.00
174	3.48	1.20	100.00	3.00	0.56	1.46	16.73	0.00	16.73	4.000	No	Yes	2.00
175	3.50	1.18	100.00	3.02	0.56	1.46	16.92	0.00	16.92	4.000	No	Yes	2.00
176	3.52	1.16	100.00	3.02	0.56	1.46	16.61	0.00	16.61	4.000	No	Yes	2.00
177	3.54	1.15	100.00	3.03	0.56	1.46	16.08	0.00	16.08	4.000	No	Yes	2.00
178	3.56	1.13	100.00	3.02	0.56	1.45	16.01	0.00	16.01	4.000	No	Yes	2.00
179	3.58	1.12	100.00	3.02	0.56	1.45	15.79	0.00	15.79	4.000	No	Yes	2.00
180	3.60	1.12	100.00	3.00	0.56	1.45	15.57	0.00	15.57	4.000	No	Yes	2.00
181	3.62	1.13	100.00	2.99	0.56	1.45	15.85	0.00	15.85	4.000	No	Yes	2.00
182	3.64	1.15	99.68	2.96	0.56	1.44	16.01	0.00	16.01	4.000	No	Yes	2.00
183	3.66	1.13	98.79	2.95	0.56	1.44	16.25	0.00	16.25	4.000	No	Yes	2.00
184	3.68	1.09	99.62	2.96	0.56	1.44	15.42	0.00	15.42	4.000	No	Yes	2.00
185	3.70	1.02	100.00	3.00	0.57	1.44	14.43	0.00	14.43	4.000	No	Yes	2.00
186	3.72	0.94	100.00	3.05	0.57	1.44	13.47	0.00	13.47	4.000	No	Yes	2.00
187	3.74	0.87	100.00	3.11	0.57	1.44	12.10	0.00	12.10	4.000	No	Yes	2.00
188	3.76	0.80	100.00	3.18	0.58	1.45	11.20	0.00	11.20	4.000	No	Yes	2.00
189	3.78	0.75	100.00	3.22	0.58	1.45	10.52	0.00	10.52	4.000	No	Yes	2.00
190	3.80	0.73	100.00	3.23	0.58	1.44	10.12	0.00	10.12	4.000	No	Yes	2.00
191	3.82	0.73	100.00	3.22	0.58	1.44	10.23	0.00	10.23	4.000	No	Yes	2.00
192	3.84	0.74	100.00	3.19	0.58	1.44	10.37	0.00	10.37	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	0.74	100.00	3.18	0.58	1.44	10.38	0.00	10.38	4.000	No	Yes	2.00
194	3.88	0.72	100.00	3.17	0.58	1.44	9.98	0.00	9.98	4.000	No	Yes	2.00
195	3.90	0.68	100.00	3.18	0.58	1.44	9.41	0.00	9.41	4.000	No	Yes	2.00
196	3.92	0.65	100.00	3.19	0.59	1.43	8.84	0.00	8.84	4.000	No	Yes	2.00
197	3.94	0.61	100.00	3.21	0.59	1.44	8.14	0.00	8.14	4.000	No	Yes	2.00
198	3.96	0.58	100.00	3.24	0.59	1.43	7.94	0.00	7.94	4.000	No	Yes	2.00
199	3.98	0.56	100.00	3.24	0.59	1.43	7.37	0.00	7.37	4.000	No	Yes	2.00
200	4.00	0.54	100.00	3.24	0.59	1.43	7.23	0.00	7.23	4.000	No	Yes	2.00
201	4.02	0.54	100.00	3.21	0.59	1.43	7.13	0.00	7.13	4.000	No	Yes	2.00
202	4.05	0.56	100.00	3.16	0.59	1.43	7.24	0.00	7.24	4.000	No	Yes	2.00
203	4.06	0.58	100.00	3.09	0.59	1.43	7.52	0.00	7.52	4.000	No	Yes	2.00
204	4.08	0.63	100.00	3.02	0.59	1.42	7.98	0.00	7.98	4.000	No	Yes	2.00
205	4.10	0.67	99.12	2.95	0.59	1.42	8.78	0.00	8.78	4.000	No	Yes	2.00
206	4.12	0.73	94.53	2.89	0.59	1.41	9.33	0.00	9.33	4.000	No	Yes	2.00
207	4.14	0.77	91.69	2.86	0.58	1.41	10.18	0.00	10.18	4.000	No	Yes	2.00
208	4.16	0.81	89.67	2.83	0.58	1.41	10.55	0.00	10.55	4.000	No	Yes	2.00
209	4.18	0.85	88.56	2.82	0.58	1.41	10.87	0.00	10.87	4.000	No	Yes	2.00
210	4.20	0.88	88.78	2.82	0.58	1.40	11.63	0.00	11.63	4.000	No	Yes	2.00
211	4.22	0.90	89.80	2.84	0.58	1.40	11.67	0.00	11.67	4.000	No	Yes	2.00
212	4.24	0.89	92.12	2.86	0.58	1.40	11.69	0.00	11.69	4.000	No	Yes	2.00
213	4.26	0.88	94.94	2.90	0.58	1.39	11.61	0.00	11.61	4.000	No	Yes	2.00
214	4.28	0.85	98.54	2.94	0.58	1.39	11.17	0.00	11.17	4.000	No	Yes	2.00
215	4.30	0.82	100.00	2.99	0.58	1.39	10.76	0.00	10.76	4.000	No	Yes	2.00
216	4.32	0.79	100.00	3.04	0.58	1.39	10.42	0.00	10.42	4.000	No	Yes	2.00
217	4.34	0.76	100.00	3.07	0.58	1.39	9.92	0.00	9.92	4.000	No	Yes	2.00
218	4.36	0.74	100.00	3.09	0.58	1.39	9.55	0.00	9.55	4.000	No	Yes	2.00
219	4.38	0.73	100.00	3.10	0.58	1.39	9.45	0.00	9.45	4.000	No	Yes	2.00
220	4.40	0.71	100.00	3.10	0.59	1.39	9.20	0.00	9.20	4.000	No	Yes	2.00
221	4.42	0.70	100.00	3.10	0.59	1.39	8.77	0.00	8.77	4.000	No	Yes	2.00
222	4.44	0.68	100.00	3.09	0.59	1.38	8.70	0.00	8.70	4.000	No	Yes	2.00
223	4.46	0.67	100.00	3.07	0.59	1.38	8.57	0.00	8.57	4.000	No	Yes	2.00
224	4.48	0.67	100.00	3.05	0.59	1.38	8.41	0.00	8.41	4.000	No	Yes	2.00
225	4.50	0.66	100.00	3.04	0.59	1.38	8.46	0.00	8.46	4.000	No	Yes	2.00
226	4.52	0.66	100.00	3.04	0.59	1.38	8.30	0.00	8.30	4.000	No	Yes	2.00
227	4.54	0.66	100.00	3.03	0.59	1.38	8.26	0.00	8.26	4.000	No	Yes	2.00
228	4.56	0.68	100.00	3.01	0.59	1.37	8.61	0.00	8.61	4.000	No	Yes	2.00
229	4.58	0.69	100.00	2.99	0.59	1.37	8.79	0.00	8.79	4.000	No	Yes	2.00
230	4.60	0.69	100.00	2.99	0.59	1.37	8.66	0.00	8.66	4.000	No	Yes	2.00
231	4.62	0.69	100.00	2.99	0.59	1.37	8.59	0.00	8.59	4.000	No	Yes	2.00
232	4.64	0.72	100.00	2.96	0.59	1.37	8.85	0.00	8.85	4.000	No	Yes	2.00
233	4.66	0.79	94.27	2.89	0.59	1.36	9.42	0.00	9.42	4.000	No	Yes	2.00
234	4.68	0.89	88.23	2.82	0.58	1.36	11.40	0.00	11.40	4.000	No	Yes	2.00
235	4.70	0.97	84.83	2.77	0.58	1.35	12.63	0.00	12.63	4.000	No	Yes	2.00
236	4.72	1.00	84.00	2.76	0.58	1.35	12.36	0.00	12.36	4.000	No	Yes	2.00
237	4.74	1.04	83.23	2.75	0.58	1.35	12.82	0.00	12.82	4.000	No	Yes	2.00
238	4.76	1.09	83.21	2.75	0.57	1.35	13.98	0.00	13.98	4.000	No	Yes	2.00
239	4.78	1.15	82.07	2.74	0.57	1.34	14.20	0.00	14.20	4.000	No	Yes	2.00
240	4.80	1.17	82.94	2.75	0.57	1.34	15.34	0.00	15.34	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	1.20	82.23	2.74	0.57	1.34	14.72	0.00	14.72	4.000	No	Yes	2.00
242	4.84	1.23	82.72	2.75	0.57	1.33	15.31	0.00	15.31	4.000	No	Yes	2.00
243	4.86	1.23	83.17	2.75	0.56	1.33	16.21	0.00	16.21	4.000	No	Yes	2.00
244	4.88	1.23	85.11	2.78	0.57	1.33	14.90	0.00	14.90	4.000	No	Yes	2.00
245	4.90	1.16	90.39	2.84	0.56	1.33	15.85	0.00	15.85	4.000	No	Yes	2.00
246	4.93	1.09	96.63	2.92	0.57	1.33	13.97	0.00	13.97	4.000	No	Yes	2.00
247	4.94	0.98	100.00	3.02	0.57	1.33	12.89	0.00	12.89	4.000	No	Yes	2.00
248	4.96	0.90	100.00	3.11	0.58	1.33	11.54	0.00	11.54	4.000	No	Yes	2.00
249	4.98	0.82	100.00	3.19	0.58	1.33	10.51	0.00	10.51	4.000	No	Yes	2.00
250	5.00	0.75	100.00	3.26	0.58	1.33	9.48	0.00	9.48	4.000	No	Yes	2.00
251	5.02	0.71	100.00	3.30	0.59	1.33	8.65	0.00	8.65	4.000	No	Yes	2.00
252	5.04	0.69	100.00	3.29	0.59	1.33	8.61	0.00	8.61	4.000	No	Yes	2.00
253	5.06	0.71	100.00	3.22	0.59	1.33	8.60	0.00	8.60	4.000	No	Yes	2.00
254	5.08	0.79	100.00	3.10	0.58	1.32	9.31	0.00	9.31	4.000	No	Yes	2.00
255	5.10	0.95	97.80	2.94	0.58	1.32	11.57	0.00	11.57	4.000	No	Yes	2.00
256	5.12	1.24	82.22	2.74	0.57	1.31	14.44	0.00	14.44	4.000	No	Yes	2.00
257	5.14	1.48	73.15	2.63	0.55	1.30	20.59	0.00	20.59	4.000	No	Yes	2.00
258	5.16	1.59	70.23	2.59	0.55	1.30	20.91	56.75	77.66	0.114	No	No	0.65
259	5.18	1.48	76.47	2.67	0.56	1.30	19.35	0.00	19.35	4.000	No	Yes	2.00
260	5.20	1.33	83.45	2.76	0.56	1.30	16.39	0.00	16.39	4.000	No	Yes	2.00
261	5.22	1.22	89.12	2.83	0.56	1.30	15.37	0.00	15.37	4.000	No	Yes	2.00
262	5.24	1.22	90.09	2.84	0.57	1.30	15.03	0.00	15.03	4.000	No	Yes	2.00
263	5.26	1.28	89.28	2.83	0.56	1.29	16.17	0.00	16.17	4.000	No	Yes	2.00
264	5.29	1.38	86.50	2.79	0.56	1.29	17.37	0.00	17.37	4.000	No	Yes	2.00
265	5.30	1.47	84.45	2.77	0.55	1.29	18.87	0.00	18.87	4.000	No	Yes	2.00
266	5.32	1.55	83.62	2.76	0.55	1.28	19.68	0.00	19.68	4.000	No	Yes	2.00
267	5.34	1.57	84.87	2.77	0.55	1.28	20.17	0.00	20.17	4.000	No	Yes	2.00
268	5.36	1.58	86.24	2.79	0.55	1.28	19.84	0.00	19.84	4.000	No	Yes	2.00
269	5.38	1.58	86.85	2.80	0.55	1.28	19.75	0.00	19.75	4.000	No	Yes	2.00
270	5.40	1.59	86.45	2.79	0.55	1.27	20.08	0.00	20.08	4.000	No	Yes	2.00
271	5.42	1.61	86.06	2.79	0.55	1.27	20.28	0.00	20.28	4.000	No	Yes	2.00
272	5.44	1.61	86.84	2.80	0.55	1.27	20.55	0.00	20.55	4.000	No	Yes	2.00
273	5.46	1.60	87.61	2.81	0.55	1.27	19.89	0.00	19.89	4.000	No	Yes	2.00
274	5.48	1.60	87.20	2.80	0.55	1.27	19.78	0.00	19.78	4.000	No	Yes	2.00
275	5.50	1.68	84.11	2.76	0.55	1.27	20.53	0.00	20.53	4.000	No	Yes	2.00
276	5.52	1.82	79.86	2.71	0.54	1.26	22.77	0.00	22.77	4.000	No	Yes	2.00
277	5.54	2.01	76.11	2.66	0.54	1.26	24.87	0.00	24.87	4.000	No	Yes	2.00
278	5.56	2.13	75.11	2.65	0.53	1.25	27.11	0.00	27.11	4.000	No	Yes	2.00
279	5.58	2.08	78.10	2.69	0.53	1.25	27.18	0.00	27.18	4.000	No	Yes	2.00
280	5.60	1.88	83.71	2.76	0.54	1.25	22.77	0.00	22.77	4.000	No	Yes	2.00
281	5.62	1.64	90.70	2.85	0.55	1.26	20.15	0.00	20.15	4.000	No	Yes	2.00
282	5.64	1.56	91.64	2.86	0.55	1.26	18.32	0.00	18.32	4.000	No	Yes	2.00
283	5.66	1.56	89.30	2.83	0.55	1.25	19.76	0.00	19.76	4.000	No	Yes	2.00
284	5.68	1.55	87.51	2.81	0.55	1.25	19.93	0.00	19.93	4.000	No	Yes	2.00
285	5.70	1.44	91.53	2.86	0.55	1.25	17.97	0.00	17.97	4.000	No	Yes	2.00
286	5.72	1.26	99.22	2.95	0.56	1.25	15.48	0.00	15.48	4.000	No	Yes	2.00
287	5.74	1.10	100.00	3.04	0.57	1.26	13.25	0.00	13.25	4.000	No	Yes	2.00
288	5.76	0.99	100.00	3.10	0.57	1.26	12.07	0.00	12.07	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	0.95	100.00	3.12	0.58	1.26	11.50	0.00	11.50	4.000	No	Yes	2.00
290	5.80	0.97	100.00	3.10	0.58	1.25	11.62	0.00	11.62	4.000	No	Yes	2.00
291	5.82	1.02	100.00	3.04	0.57	1.25	12.51	0.00	12.51	4.000	No	Yes	2.00
292	5.84	1.08	100.00	2.99	0.57	1.25	13.28	0.00	13.28	4.000	No	Yes	2.00
293	5.86	1.17	96.56	2.92	0.57	1.25	13.84	0.00	13.84	4.000	No	Yes	2.00
294	5.88	1.21	94.47	2.89	0.56	1.24	15.13	0.00	15.13	4.000	No	Yes	2.00
295	5.90	1.22	93.82	2.89	0.57	1.24	14.31	0.00	14.31	4.000	No	Yes	2.00
296	5.93	1.18	96.79	2.92	0.57	1.24	14.12	0.00	14.12	4.000	No	Yes	2.00
297	5.94	1.15	99.14	2.95	0.57	1.24	13.65	0.00	13.65	4.000	No	Yes	2.00
298	5.96	1.12	100.00	2.99	0.57	1.24	13.50	0.00	13.50	4.000	No	Yes	2.00
299	5.98	1.09	100.00	3.03	0.57	1.24	13.10	0.00	13.10	4.000	No	Yes	2.00
300	6.01	1.07	100.00	3.06	0.57	1.24	12.62	0.00	12.62	4.000	No	Yes	2.00
301	6.02	1.06	100.00	3.08	0.57	1.24	12.64	0.00	12.64	4.000	No	Yes	2.00
302	6.04	1.06	100.00	3.08	0.57	1.23	12.71	0.00	12.71	4.000	No	Yes	2.00
303	6.06	1.07	100.00	3.08	0.57	1.23	12.88	0.00	12.88	4.000	No	Yes	2.00
304	6.08	1.08	100.00	3.08	0.57	1.23	12.78	0.00	12.78	4.000	No	Yes	2.00
305	6.10	1.11	100.00	3.06	0.57	1.23	13.01	0.00	13.01	4.000	No	Yes	2.00
306	6.12	1.14	100.00	3.04	0.57	1.23	13.85	0.00	13.85	4.000	No	Yes	2.00
307	6.14	1.17	100.00	3.02	0.57	1.22	14.10	0.00	14.10	4.000	No	Yes	2.00
308	6.16	1.17	100.00	3.02	0.57	1.22	13.84	0.00	13.84	4.000	No	Yes	2.00
309	6.18	1.16	100.00	3.03	0.57	1.22	13.90	0.00	13.90	4.000	No	Yes	2.00
310	6.20	1.15	100.00	3.04	0.57	1.22	13.80	0.00	13.80	4.000	No	Yes	2.00
311	6.22	1.12	100.00	3.06	0.57	1.22	13.46	0.00	13.46	4.000	No	Yes	2.00
312	6.24	1.09	100.00	3.10	0.57	1.22	12.88	0.00	12.88	4.000	No	Yes	2.00
313	6.26	1.04	100.00	3.14	0.57	1.22	12.54	0.00	12.54	4.000	No	Yes	2.00
314	6.28	1.00	100.00	3.17	0.58	1.22	11.70	0.00	11.70	4.000	No	Yes	2.00
315	6.30	0.95	100.00	3.21	0.58	1.22	11.15	0.00	11.15	4.000	No	Yes	2.00
316	6.32	0.91	100.00	3.24	0.58	1.22	10.63	0.00	10.63	4.000	No	Yes	2.00
317	6.34	0.86	100.00	3.28	0.58	1.21	9.97	0.00	9.97	4.000	No	Yes	2.00
318	6.36	0.82	100.00	3.30	0.58	1.21	9.34	0.00	9.34	4.000	No	Yes	2.00
319	6.38	0.82	100.00	3.29	0.58	1.21	9.49	0.00	9.49	4.000	No	Yes	2.00
320	6.40	0.85	100.00	3.24	0.58	1.21	9.79	0.00	9.79	4.000	No	Yes	2.00
321	6.42	0.89	100.00	3.19	0.58	1.21	10.39	0.00	10.39	4.000	No	Yes	2.00
322	6.44	0.92	100.00	3.15	0.58	1.21	10.56	0.00	10.56	4.000	No	Yes	2.00
323	6.46	0.94	100.00	3.12	0.58	1.20	10.92	0.00	10.92	4.000	No	Yes	2.00
324	6.48	0.96	100.00	3.09	0.58	1.20	11.22	0.00	11.22	4.000	No	Yes	2.00
325	6.50	0.97	100.00	3.08	0.58	1.20	11.31	0.00	11.31	4.000	No	Yes	2.00
326	6.52	0.95	100.00	3.09	0.58	1.20	11.25	0.00	11.25	4.000	No	Yes	2.00
327	6.54	0.92	100.00	3.12	0.58	1.20	10.58	0.00	10.58	4.000	No	Yes	2.00
328	6.56	0.88	100.00	3.16	0.58	1.20	10.28	0.00	10.28	4.000	No	Yes	2.00
329	6.58	0.83	100.00	3.20	0.58	1.20	9.77	0.00	9.77	4.000	No	Yes	2.00
330	6.60	0.78	100.00	3.26	0.59	1.20	8.94	0.00	8.94	4.000	No	Yes	2.00
331	6.62	0.74	100.00	3.31	0.59	1.20	8.38	0.00	8.38	4.000	No	Yes	2.00
332	6.64	0.74	100.00	3.31	0.59	1.20	8.34	0.00	8.34	4.000	No	Yes	2.00
333	6.66	0.77	100.00	3.27	0.59	1.19	8.86	0.00	8.86	4.000	No	Yes	2.00
334	6.68	0.82	100.00	3.20	0.58	1.19	9.35	0.00	9.35	4.000	No	Yes	2.00
335	6.70	0.88	100.00	3.12	0.58	1.19	9.92	0.00	9.92	4.000	No	Yes	2.00
336	6.72	0.93	100.00	3.07	0.58	1.19	10.93	0.00	10.93	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	0.93	100.00	3.06	0.58	1.18	10.84	0.00	10.84	4.000	No	Yes	2.00
338	6.76	0.89	100.00	3.08	0.58	1.18	10.03	0.00	10.03	4.000	No	Yes	2.00
339	6.78	0.82	100.00	3.14	0.58	1.18	9.34	0.00	9.34	4.000	No	Yes	2.00
340	6.80	0.77	100.00	3.20	0.59	1.18	8.61	0.00	8.61	4.000	No	Yes	2.00
341	6.82	0.72	100.00	3.25	0.59	1.18	8.16	0.00	8.16	4.000	No	Yes	2.00
342	6.84	0.74	100.00	3.24	0.59	1.18	7.86	0.00	7.86	4.000	No	Yes	2.00
343	6.86	0.76	100.00	3.21	0.59	1.18	8.80	0.00	8.80	4.000	No	Yes	2.00
344	6.88	0.76	100.00	3.20	0.59	1.18	8.72	0.00	8.72	4.000	No	Yes	2.00
345	6.90	0.71	100.00	3.25	0.59	1.18	7.67	0.00	7.67	4.000	No	Yes	2.00
346	6.92	0.65	100.00	3.30	0.59	1.18	7.22	0.00	7.22	4.000	No	Yes	2.00
347	6.94	0.61	100.00	3.34	0.60	1.18	6.62	0.00	6.62	4.000	No	Yes	2.00
348	6.96	0.59	100.00	3.36	0.60	1.18	6.46	0.00	6.46	4.000	No	Yes	2.00
349	6.98	0.59	100.00	3.35	0.60	1.18	6.33	0.00	6.33	4.000	No	Yes	2.00
350	7.00	0.60	100.00	3.32	0.60	1.17	6.48	0.00	6.48	4.000	No	Yes	2.00
351	7.02	0.62	100.00	3.28	0.59	1.17	6.94	0.00	6.94	4.000	No	Yes	2.00
352	7.04	0.66	100.00	3.23	0.59	1.17	7.08	0.00	7.08	4.000	No	Yes	2.00
353	7.06	0.67	100.00	3.21	0.59	1.17	7.52	0.00	7.52	4.000	No	Yes	2.00
354	7.09	0.70	100.00	3.17	0.59	1.17	7.46	0.00	7.46	4.000	No	Yes	2.00
355	7.10	0.72	100.00	3.16	0.59	1.17	7.94	0.00	7.94	4.000	No	Yes	2.00
356	7.14	0.76	100.00	3.12	0.59	1.16	8.06	0.00	8.06	4.000	No	Yes	2.00
357	7.15	0.82	100.00	3.07	0.59	1.16	8.85	0.00	8.85	4.000	No	Yes	2.00
358	7.16	0.89	100.00	3.02	0.58	1.16	9.62	0.00	9.62	4.000	No	Yes	2.00
359	7.18	0.95	100.00	2.98	0.58	1.16	10.28	0.00	10.28	4.000	No	Yes	2.00
360	7.20	1.01	98.23	2.94	0.58	1.16	10.78	0.00	10.78	4.000	No	Yes	2.00
361	7.22	1.07	95.95	2.91	0.58	1.16	11.74	0.00	11.74	4.000	No	Yes	2.00
362	7.24	1.09	95.40	2.90	0.58	1.15	12.11	0.00	12.11	4.000	No	Yes	2.00
363	7.26	1.08	96.77	2.92	0.58	1.15	11.85	0.00	11.85	4.000	No	Yes	2.00
364	7.28	1.06	99.09	2.95	0.58	1.15	11.44	0.00	11.44	4.000	No	Yes	2.00
365	7.31	1.06	100.00	2.96	0.58	1.15	11.14	0.00	11.14	4.000	No	Yes	2.00
366	7.32	1.07	100.00	2.97	0.58	1.15	11.52	0.00	11.52	4.000	No	Yes	2.00
367	7.34	1.07	100.00	2.99	0.58	1.15	11.46	0.00	11.46	4.000	No	Yes	2.00
368	7.36	1.04	100.00	3.01	0.58	1.15	11.12	0.00	11.12	4.000	No	Yes	2.00
369	7.38	1.03	100.00	3.03	0.58	1.15	10.76	0.00	10.76	4.000	No	Yes	2.00
370	7.40	1.03	100.00	3.03	0.58	1.14	11.13	0.00	11.13	4.000	No	Yes	2.00
371	7.42	1.03	100.00	3.04	0.58	1.14	11.17	0.00	11.17	4.000	No	Yes	2.00
372	7.44	1.00	100.00	3.07	0.58	1.14	10.96	0.00	10.96	4.000	No	Yes	2.00
373	7.46	0.96	100.00	3.12	0.58	1.14	10.57	0.00	10.57	4.000	No	Yes	2.00
374	7.48	0.94	100.00	3.15	0.58	1.14	10.16	0.00	10.16	4.000	No	Yes	2.00
375	7.50	0.92	100.00	3.17	0.58	1.14	10.13	0.00	10.13	4.000	No	Yes	2.00
376	7.52	0.91	100.00	3.18	0.58	1.14	10.01	0.00	10.01	4.000	No	Yes	2.00
377	7.54	0.90	100.00	3.19	0.58	1.14	9.75	0.00	9.75	4.000	No	Yes	2.00
378	7.56	0.88	100.00	3.20	0.58	1.14	9.67	0.00	9.67	4.000	No	Yes	2.00
379	7.58	0.85	100.00	3.23	0.58	1.14	9.39	0.00	9.39	4.000	No	Yes	2.00
380	7.60	0.82	100.00	3.26	0.59	1.13	8.75	0.00	8.75	4.000	No	Yes	2.00
381	7.62	0.78	100.00	3.29	0.59	1.13	8.37	0.00	8.37	4.000	No	Yes	2.00
382	7.64	0.74	100.00	3.31	0.59	1.13	8.01	0.00	8.01	4.000	No	Yes	2.00
383	7.66	0.71	100.00	3.33	0.59	1.13	7.57	0.00	7.57	4.000	No	Yes	2.00
384	7.68	0.69	100.00	3.34	0.59	1.13	7.36	0.00	7.36	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	0.68	100.00	3.33	0.59	1.13	7.30	0.00	7.30	4.000	No	Yes	2.00
386	7.72	0.68	100.00	3.31	0.59	1.13	7.17	0.00	7.17	4.000	No	Yes	2.00
387	7.74	0.68	100.00	3.29	0.59	1.13	7.14	0.00	7.14	4.000	No	Yes	2.00
388	7.76	0.68	100.00	3.27	0.59	1.13	7.16	0.00	7.16	4.000	No	Yes	2.00
389	7.78	0.68	100.00	3.25	0.59	1.13	7.07	0.00	7.07	4.000	No	Yes	2.00
390	7.80	0.68	100.00	3.24	0.59	1.13	7.04	0.00	7.04	4.000	No	Yes	2.00
391	7.82	0.68	100.00	3.23	0.59	1.12	7.11	0.00	7.11	4.000	No	Yes	2.00
392	7.84	0.72	100.00	3.17	0.59	1.12	6.96	0.00	6.96	4.000	No	Yes	2.00
393	7.86	0.76	100.00	3.13	0.59	1.12	8.58	0.00	8.58	4.000	No	Yes	2.00
394	7.88	0.79	100.00	3.10	0.59	1.12	8.26	0.00	8.26	4.000	No	Yes	2.00
395	7.90	0.78	100.00	3.12	0.59	1.12	8.08	0.00	8.08	4.000	No	Yes	2.00
396	7.92	0.78	100.00	3.12	0.59	1.12	7.90	0.00	7.90	4.000	No	Yes	2.00
397	7.94	0.79	100.00	3.11	0.59	1.12	8.09	0.00	8.09	4.000	No	Yes	2.00
398	7.96	0.80	100.00	3.09	0.59	1.12	8.28	0.00	8.28	4.000	No	Yes	2.00
399	7.98	0.81	100.00	3.09	0.59	1.11	8.25	0.00	8.25	4.000	No	Yes	2.00
400	8.00	0.82	100.00	3.08	0.59	1.11	8.37	0.00	8.37	4.000	No	Yes	2.00
401	8.02	0.81	100.00	3.08	0.59	1.11	8.53	0.00	8.53	4.000	No	Yes	2.00
402	8.04	0.79	100.00	3.11	0.59	1.11	8.03	0.00	8.03	4.000	No	Yes	2.00
403	8.06	0.74	100.00	3.15	0.59	1.11	7.58	0.00	7.58	4.000	No	Yes	2.00
404	8.08	0.72	100.00	3.17	0.59	1.11	7.19	0.00	7.19	4.000	No	Yes	2.00
405	8.10	0.70	100.00	3.18	0.59	1.11	7.13	0.00	7.13	4.000	No	Yes	2.00
406	8.12	0.70	100.00	3.17	0.59	1.11	7.00	0.00	7.00	4.000	No	Yes	2.00
407	8.14	0.70	100.00	3.15	0.59	1.11	6.90	0.00	6.90	4.000	No	Yes	2.00
408	8.16	0.72	100.00	3.13	0.59	1.11	7.26	0.00	7.26	4.000	No	Yes	2.00
409	8.19	0.73	100.00	3.11	0.59	1.10	7.36	0.00	7.36	4.000	No	Yes	2.00
410	8.20	0.73	100.00	3.11	0.59	1.10	7.33	0.00	7.33	4.000	No	Yes	2.00
411	8.22	0.73	100.00	3.13	0.59	1.10	7.30	0.00	7.30	4.000	No	Yes	2.00
412	8.24	0.71	100.00	3.15	0.59	1.10	7.20	0.00	7.20	4.000	No	Yes	2.00
413	8.26	0.69	100.00	3.19	0.59	1.10	6.90	0.00	6.90	4.000	No	Yes	2.00
414	8.28	0.68	100.00	3.20	0.60	1.10	6.70	0.00	6.70	4.000	No	Yes	2.00
415	8.30	0.71	100.00	3.18	0.59	1.10	6.99	0.00	6.99	4.000	No	Yes	2.00
416	8.32	0.77	100.00	3.12	0.59	1.10	7.71	0.00	7.71	4.000	No	Yes	2.00
417	8.34	0.83	100.00	3.06	0.59	1.10	8.53	0.00	8.53	4.000	No	Yes	2.00
418	8.36	0.87	100.00	3.03	0.59	1.10	8.82	0.00	8.82	4.000	No	Yes	2.00
419	8.38	0.89	100.00	3.01	0.59	1.09	9.15	0.00	9.15	4.000	No	Yes	2.00
420	8.40	0.94	100.00	2.97	0.58	1.09	9.36	0.00	9.36	4.000	No	Yes	2.00
421	8.42	1.02	97.13	2.93	0.58	1.09	10.42	0.00	10.42	4.000	No	Yes	2.00
422	8.44	1.16	91.58	2.86	0.58	1.09	11.74	0.00	11.74	4.000	No	Yes	2.00
423	8.46	1.29	88.87	2.82	0.57	1.09	14.09	0.00	14.09	4.000	No	Yes	2.00
424	8.48	1.28	91.97	2.86	0.57	1.09	14.84	0.00	14.84	4.000	No	Yes	2.00
425	8.50	1.12	100.00	2.97	0.58	1.09	11.75	0.00	11.75	4.000	No	Yes	2.00
426	8.52	0.89	100.00	3.13	0.59	1.09	9.22	0.00	9.22	4.000	No	Yes	2.00
427	8.54	0.74	100.00	3.24	0.59	1.09	7.05	0.00	7.05	4.000	No	Yes	2.00
428	8.56	0.69	100.00	3.28	0.60	1.09	6.65	0.00	6.65	4.000	No	Yes	2.00
429	8.58	0.70	100.00	3.25	0.59	1.09	7.18	0.00	7.18	4.000	No	Yes	2.00
430	8.60	0.73	100.00	3.20	0.59	1.08	7.20	0.00	7.20	4.000	No	Yes	2.00
431	8.62	0.74	100.00	3.18	0.59	1.08	7.50	0.00	7.50	4.000	No	Yes	2.00
432	8.64	0.74	100.00	3.15	0.59	1.08	7.38	0.00	7.38	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	0.73	100.00	3.14	0.59	1.08	7.37	0.00	7.37	4.000	No	Yes	2.00
434	8.68	0.71	100.00	3.16	0.59	1.08	7.13	0.00	7.13	4.000	No	Yes	2.00
435	8.70	0.69	100.00	3.19	0.60	1.08	6.81	0.00	6.81	4.000	No	Yes	2.00
436	8.72	0.68	100.00	3.21	0.60	1.08	6.78	0.00	6.78	4.000	No	Yes	2.00
437	8.74	0.70	100.00	3.19	0.59	1.08	6.82	0.00	6.82	4.000	No	Yes	2.00
438	8.76	0.73	100.00	3.15	0.59	1.08	7.30	0.00	7.30	4.000	No	Yes	2.00
439	8.78	0.79	100.00	3.08	0.59	1.08	7.53	0.00	7.53	4.000	No	Yes	2.00
440	8.80	0.94	98.90	2.95	0.59	1.07	8.57	0.00	8.57	4.000	No	Yes	2.00
441	8.82	1.24	85.67	2.78	0.58	1.07	12.02	0.00	12.02	4.000	No	Yes	2.00
442	8.84	1.53	78.72	2.70	0.56	1.07	17.29	0.00	17.29	4.000	No	Yes	2.00
443	8.86	1.73	77.61	2.68	0.56	1.07	18.20	0.00	18.20	4.000	No	Yes	2.00
444	8.88	1.77	80.48	2.72	0.56	1.07	18.93	0.00	18.93	4.000	No	Yes	2.00
445	8.90	1.67	84.78	2.77	0.56	1.07	18.37	0.00	18.37	4.000	No	Yes	2.00
446	8.93	1.43	92.35	2.87	0.56	1.07	15.12	0.00	15.12	4.000	No	Yes	2.00
447	8.94	1.14	100.00	3.01	0.58	1.07	11.50	0.00	11.50	4.000	No	Yes	2.00
448	8.96	0.90	100.00	3.15	0.59	1.07	9.15	0.00	9.15	4.000	No	Yes	2.00
449	8.99	0.79	100.00	3.23	0.59	1.07	7.60	0.00	7.60	4.000	No	Yes	2.00
450	9.00	0.82	100.00	3.20	0.59	1.07	7.88	0.00	7.88	4.000	No	Yes	2.00
451	9.02	0.99	100.00	3.06	0.58	1.06	9.73	0.00	9.73	4.000	No	Yes	2.00
452	9.04	1.18	97.42	2.93	0.57	1.06	12.66	0.00	12.66	4.000	No	Yes	2.00
453	9.06	1.32	91.11	2.85	0.57	1.06	13.92	0.00	13.92	4.000	No	Yes	2.00
454	9.08	1.37	89.54	2.83	0.57	1.06	14.52	0.00	14.52	4.000	No	Yes	2.00
455	9.10	1.37	90.28	2.84	0.57	1.06	14.27	0.00	14.27	4.000	No	Yes	2.00
456	9.12	1.36	91.59	2.86	0.57	1.06	14.00	0.00	14.00	4.000	No	Yes	2.00
457	9.14	1.31	94.24	2.89	0.57	1.06	13.99	0.00	13.99	4.000	No	Yes	2.00
458	9.16	1.19	100.00	2.97	0.57	1.06	12.97	0.00	12.97	4.000	No	Yes	2.00
459	9.18	1.02	100.00	3.07	0.58	1.06	10.03	0.00	10.03	4.000	No	Yes	2.00
460	9.20	0.85	100.00	3.19	0.59	1.06	8.71	0.00	8.71	4.000	No	Yes	2.00
461	9.22	0.81	100.00	3.22	0.59	1.05	7.76	0.00	7.76	4.000	No	Yes	2.00
462	9.24	0.83	100.00	3.19	0.59	1.05	8.41	0.00	8.41	4.000	No	Yes	2.00
463	9.26	0.94	100.00	3.10	0.59	1.05	9.29	0.00	9.29	4.000	No	Yes	2.00
464	9.28	1.04	100.00	3.02	0.58	1.05	11.07	0.00	11.07	4.000	No	Yes	2.00
465	9.30	1.07	100.00	2.99	0.58	1.05	11.46	0.00	11.46	4.000	No	Yes	2.00
466	9.32	1.04	100.00	3.01	0.58	1.05	10.35	0.00	10.35	4.000	No	Yes	2.00
467	9.34	1.02	100.00	3.02	0.58	1.05	10.06	0.00	10.06	4.000	No	Yes	2.00
468	9.36	1.05	100.00	3.01	0.58	1.05	10.87	0.00	10.87	4.000	No	Yes	2.00
469	9.38	1.03	100.00	3.04	0.58	1.05	11.13	0.00	11.13	4.000	No	Yes	2.00
470	9.40	0.94	100.00	3.12	0.58	1.05	9.62	0.00	9.62	4.000	No	Yes	2.00
471	9.42	0.87	100.00	3.18	0.59	1.05	8.08	0.00	8.08	4.000	No	Yes	2.00
472	9.44	0.91	100.00	3.14	0.59	1.04	8.81	0.00	8.81	4.000	No	Yes	2.00
473	9.46	1.06	100.00	3.02	0.58	1.04	10.70	0.00	10.70	4.000	No	Yes	2.00
474	9.48	1.21	97.39	2.93	0.57	1.04	12.49	0.00	12.49	4.000	No	Yes	2.00
475	9.50	1.33	92.91	2.87	0.57	1.04	13.54	0.00	13.54	4.000	No	Yes	2.00
476	9.52	1.39	92.08	2.86	0.57	1.04	14.54	0.00	14.54	4.000	No	Yes	2.00
477	9.54	1.40	93.23	2.88	0.57	1.04	14.28	0.00	14.28	4.000	No	Yes	2.00
478	9.56	1.36	95.40	2.91	0.57	1.04	13.87	0.00	13.87	4.000	No	Yes	2.00
479	9.58	1.26	100.00	2.97	0.57	1.04	13.40	0.00	13.40	4.000	No	Yes	2.00
480	9.60	1.12	100.00	3.06	0.58	1.04	11.29	0.00	11.29	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	1.03	100.00	3.13	0.58	1.04	9.35	0.00	9.35	4.000	No	Yes	2.00
482	9.64	1.12	100.00	3.07	0.58	1.03	10.56	0.00	10.56	4.000	No	Yes	2.00
483	9.66	1.40	95.89	2.91	0.57	1.03	13.78	0.00	13.78	4.000	No	Yes	2.00
484	9.68	1.68	86.27	2.79	0.56	1.03	17.62	0.00	17.62	4.000	No	Yes	2.00
485	9.70	1.85	82.46	2.74	0.55	1.03	19.34	0.00	19.34	4.000	No	Yes	2.00
486	9.72	1.71	87.75	2.81	0.55	1.03	18.91	0.00	18.91	4.000	No	Yes	2.00
487	9.74	1.45	96.52	2.92	0.57	1.03	13.55	0.00	13.55	4.000	No	Yes	2.00
488	9.76	1.12	100.00	3.09	0.58	1.03	11.27	0.00	11.27	4.000	No	Yes	2.00
489	9.78	0.92	100.00	3.22	0.59	1.03	8.96	0.00	8.96	4.000	No	Yes	2.00
490	9.80	0.79	100.00	3.33	0.59	1.03	7.35	0.00	7.35	4.000	No	Yes	2.00
491	9.82	0.79	100.00	3.31	0.59	1.03	7.16	0.00	7.16	4.000	No	Yes	2.00
492	9.84	0.82	100.00	3.26	0.59	1.03	8.91	0.00	8.91	4.000	No	Yes	2.00
493	9.86	0.84	100.00	3.22	0.59	1.02	8.18	0.00	8.18	4.000	No	Yes	2.00
494	9.88	0.78	100.00	3.26	0.59	1.02	7.65	0.00	7.65	4.000	No	Yes	2.00
495	9.90	0.74	100.00	3.28	0.59	1.02	7.12	0.00	7.12	4.000	No	Yes	2.00
496	9.92	0.73	100.00	3.27	0.60	1.02	6.73	0.00	6.73	4.000	No	Yes	2.00
497	9.94	0.78	100.00	3.20	0.59	1.02	7.36	0.00	7.36	4.000	No	Yes	2.00
498	9.96	0.91	100.00	3.08	0.59	1.02	8.42	0.00	8.42	4.000	No	Yes	2.00
499	9.98	1.11	98.21	2.94	0.58	1.02	10.41	0.00	10.41	4.000	No	Yes	2.00
500	10.00	1.34	89.34	2.83	0.57	1.02	13.50	0.00	13.50	4.000	No	Yes	2.00
501	10.03	1.55	83.27	2.75	0.57	1.02	15.58	0.00	15.58	4.000	No	Yes	2.00
502	10.04	1.69	81.66	2.73	0.56	1.02	17.18	0.00	17.18	4.000	No	Yes	2.00
503	10.06	1.77	81.60	2.73	0.56	1.02	17.80	0.00	17.80	4.000	No	Yes	2.00
504	10.08	1.80	83.20	2.75	0.56	1.01	18.01	0.00	18.01	4.000	No	Yes	2.00
505	10.10	1.80	84.73	2.77	0.56	1.01	18.04	0.00	18.04	4.000	No	Yes	2.00
506	10.12	1.79	85.13	2.78	0.56	1.01	17.64	0.00	17.64	4.000	No	Yes	2.00
507	10.14	1.84	83.21	2.75	0.56	1.01	17.94	0.00	17.94	4.000	No	Yes	2.00
508	10.16	1.95	79.89	2.71	0.55	1.01	19.41	0.00	19.41	4.000	No	Yes	2.00
509	10.18	2.10	76.73	2.67	0.55	1.01	21.00	0.00	21.00	4.000	No	Yes	2.00
510	10.20	2.23	74.72	2.65	0.55	1.01	22.36	0.00	22.36	4.000	No	Yes	2.00
511	10.22	2.31	73.81	2.64	0.54	1.01	23.19	0.00	23.19	4.000	No	Yes	2.00
512	10.24	2.34	73.22	2.63	0.54	1.01	23.43	0.00	23.43	4.000	No	Yes	2.00
513	10.26	2.31	72.93	2.62	0.54	1.01	23.18	0.00	23.18	4.000	No	Yes	2.00
514	10.28	2.24	73.11	2.63	0.55	1.01	22.30	0.00	22.30	4.000	No	Yes	2.00
515	10.30	2.14	74.59	2.64	0.55	1.00	21.10	0.00	21.10	4.000	No	Yes	2.00
516	10.32	2.11	75.82	2.66	0.55	1.00	20.30	0.00	20.30	4.000	No	Yes	2.00
517	10.34	2.19	75.21	2.65	0.55	1.00	21.42	0.00	21.42	4.000	Yes	Yes	2.00
518	10.36	2.37	72.73	2.62	0.54	1.00	23.31	0.00	23.31	4.000	Yes	Yes	2.00
519	10.38	2.54	69.42	2.58	0.54	1.00	25.57	57.96	83.53	4.000	Yes	No	2.00
520	10.40	2.64	66.88	2.55	0.54	1.00	26.47	57.72	84.19	4.000	Yes	No	2.00
521	10.42	2.66	63.95	2.51	0.54	1.00	26.21	57.02	83.23	4.000	Yes	No	2.00
522	10.44	2.64	60.73	2.47	0.54	1.00	26.10	56.22	82.31	4.000	Yes	No	2.00
523	10.46	2.62	56.10	2.41	0.54	1.00	25.86	54.89	80.75	4.000	Yes	No	2.00
524	10.48	2.59	51.94	2.36	0.55	1.00	25.30	53.41	78.71	4.000	Yes	No	2.00
525	10.50	2.54	52.36	2.37	0.55	1.00	25.23	53.53	78.77	4.000	Yes	No	2.00
526	10.52	2.51	57.22	2.43	0.55	1.00	24.32	54.79	79.11	4.000	Yes	No	2.00
527	10.54	2.51	63.41	2.51	0.54	1.00	24.56	56.42	80.98	4.000	Yes	No	2.00
528	10.56	2.51	68.63	2.57	0.54	0.99	25.20	57.70	82.89	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	2.43	73.81	2.64	0.54	0.99	24.26	0.00	24.26	4.000	Yes	Yes	2.00
530	10.60	2.27	79.28	2.70	0.54	0.99	22.14	0.00	22.14	4.000	Yes	Yes	2.00
531	10.62	2.16	82.16	2.74	0.55	0.99	20.30	0.00	20.30	4.000	Yes	Yes	2.00
532	10.64	2.21	80.72	2.72	0.55	0.99	20.95	0.00	20.95	4.000	No	Yes	2.00
533	10.66	2.41	76.67	2.67	0.54	0.99	23.66	0.00	23.66	4.000	No	Yes	2.00
534	10.68	2.64	74.18	2.64	0.53	0.99	26.06	0.00	26.06	4.000	No	Yes	2.00
535	10.70	2.82	73.28	2.63	0.53	0.99	27.67	0.00	27.67	4.000	No	Yes	2.00
536	10.72	2.93	73.15	2.63	0.53	0.99	28.76	0.00	28.76	4.000	No	Yes	2.00
537	10.74	2.98	71.79	2.61	0.52	0.99	29.26	0.00	29.26	4.000	No	Yes	2.00
538	10.76	2.95	69.74	2.58	0.53	0.99	29.24	59.08	88.32	0.124	No	No	0.66
539	10.78	2.74	69.46	2.58	0.53	0.99	27.65	58.57	86.22	0.122	No	No	0.64
540	10.80	2.34	73.61	2.63	0.54	0.98	23.07	0.00	23.07	4.000	No	Yes	2.00
541	10.82	1.88	83.53	2.76	0.56	0.98	17.62	0.00	17.62	4.000	No	Yes	2.00
542	10.84	1.53	94.62	2.90	0.57	0.98	14.19	0.00	14.19	4.000	No	Yes	2.00
543	10.86	1.23	100.00	3.05	0.57	0.98	12.91	0.00	12.91	4.000	No	Yes	2.00
544	10.88	1.01	100.00	3.18	0.59	0.98	8.54	0.00	8.54	4.000	No	Yes	2.00
545	10.90	0.84	100.00	3.30	0.59	0.98	7.79	0.00	7.79	4.000	No	Yes	2.00
546	10.92	0.81	100.00	3.31	0.59	0.98	7.74	0.00	7.74	4.000	No	Yes	2.00
547	10.94	0.81	100.00	3.29	0.59	0.98	7.63	0.00	7.63	4.000	No	Yes	2.00
548	10.96	0.82	100.00	3.27	0.59	0.98	7.69	0.00	7.69	4.000	No	Yes	2.00
549	10.98	0.83	100.00	3.25	0.59	0.98	7.85	0.00	7.85	4.000	No	Yes	2.00
550	11.00	0.82	100.00	3.24	0.59	0.97	7.82	0.00	7.82	4.000	No	Yes	2.00
551	11.02	0.81	100.00	3.25	0.59	0.97	7.56	0.00	7.56	4.000	No	Yes	2.00
552	11.04	0.79	100.00	3.26	0.59	0.97	7.38	0.00	7.38	4.000	No	Yes	2.00
553	11.06	0.78	100.00	3.28	0.59	0.97	7.42	0.00	7.42	4.000	No	Yes	2.00
554	11.08	0.78	100.00	3.30	0.59	0.97	7.24	0.00	7.24	4.000	No	Yes	2.00
555	11.10	0.77	100.00	3.31	0.59	0.97	7.21	0.00	7.21	4.000	No	Yes	2.00
556	11.12	0.76	100.00	3.32	0.59	0.97	7.12	0.00	7.12	4.000	No	Yes	2.00
557	11.15	0.76	100.00	3.31	0.59	0.97	6.87	0.00	6.87	4.000	No	Yes	2.00
558	11.16	0.77	100.00	3.29	0.59	0.97	7.24	0.00	7.24	4.000	No	Yes	2.00
559	11.18	0.79	100.00	3.28	0.59	0.97	7.36	0.00	7.36	4.000	No	Yes	2.00
560	11.20	0.78	100.00	3.28	0.59	0.97	7.23	0.00	7.23	4.000	No	Yes	2.00
561	11.22	0.78	100.00	3.29	0.59	0.97	7.11	0.00	7.11	4.000	No	Yes	2.00
562	11.24	0.78	100.00	3.28	0.59	0.97	7.17	0.00	7.17	4.000	No	Yes	2.00
563	11.26	0.78	100.00	3.28	0.59	0.97	7.28	0.00	7.28	4.000	No	Yes	2.00
564	11.28	0.78	100.00	3.29	0.59	0.96	7.12	0.00	7.12	4.000	No	Yes	2.00
565	11.30	0.77	100.00	3.29	0.59	0.96	6.99	0.00	6.99	4.000	No	Yes	2.00
566	11.32	0.78	100.00	3.27	0.59	0.96	7.11	0.00	7.11	4.000	No	Yes	2.00
567	11.34	0.79	100.00	3.25	0.59	0.96	7.30	0.00	7.30	4.000	No	Yes	2.00
568	11.36	0.80	100.00	3.23	0.59	0.96	7.41	0.00	7.41	4.000	No	Yes	2.00
569	11.38	0.81	100.00	3.23	0.59	0.96	7.38	0.00	7.38	4.000	No	Yes	2.00
570	11.40	0.81	100.00	3.23	0.59	0.96	7.44	0.00	7.44	4.000	No	Yes	2.00
571	11.42	0.82	100.00	3.23	0.59	0.96	7.55	0.00	7.55	4.000	No	Yes	2.00
572	11.44	0.83	100.00	3.24	0.59	0.96	7.61	0.00	7.61	4.000	No	Yes	2.00
573	11.46	0.85	100.00	3.23	0.59	0.96	7.69	0.00	7.69	4.000	No	Yes	2.00
574	11.48	0.87	100.00	3.22	0.59	0.96	8.03	0.00	8.03	4.000	No	Yes	2.00
575	11.50	0.89	100.00	3.22	0.59	0.96	8.22	0.00	8.22	4.000	No	Yes	2.00
576	11.52	0.90	100.00	3.22	0.59	0.96	8.19	0.00	8.19	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	0.91	100.00	3.22	0.59	0.96	8.40	0.00	8.40	4.000	No	Yes	2.00
578	11.56	0.92	100.00	3.23	0.59	0.95	8.29	0.00	8.29	4.000	No	Yes	2.00
579	11.58	0.92	100.00	3.24	0.59	0.95	8.47	0.00	8.47	4.000	No	Yes	2.00
580	11.60	0.93	100.00	3.24	0.59	0.95	8.38	0.00	8.38	4.000	No	Yes	2.00
581	11.62	0.94	100.00	3.24	0.59	0.95	8.63	0.00	8.63	4.000	No	Yes	2.00
582	11.64	0.94	100.00	3.25	0.59	0.95	8.57	0.00	8.57	4.000	No	Yes	2.00
583	11.66	0.93	100.00	3.27	0.59	0.95	8.48	0.00	8.48	4.000	No	Yes	2.00
584	11.68	0.92	100.00	3.29	0.59	0.95	8.26	0.00	8.26	4.000	No	Yes	2.00
585	11.70	0.92	100.00	3.30	0.59	0.95	8.36	0.00	8.36	4.000	No	Yes	2.00
586	11.72	0.89	100.00	3.34	0.59	0.95	8.37	0.00	8.37	4.000	No	Yes	2.00
587	11.74	0.85	100.00	3.37	0.59	0.95	7.48	0.00	7.48	4.000	No	Yes	2.00
588	11.76	0.83	100.00	3.39	0.59	0.95	7.30	0.00	7.30	4.000	No	Yes	2.00
589	11.78	0.85	100.00	3.36	0.59	0.95	7.68	0.00	7.68	4.000	No	Yes	2.00
590	11.80	0.90	100.00	3.30	0.59	0.95	7.95	0.00	7.95	4.000	No	Yes	2.00
591	11.82	0.95	100.00	3.25	0.59	0.95	8.48	0.00	8.48	4.000	No	Yes	2.00
592	11.84	0.99	100.00	3.22	0.59	0.94	8.68	0.00	8.68	4.000	No	Yes	2.00
593	11.86	1.01	100.00	3.22	0.59	0.94	8.74	0.00	8.74	4.000	No	Yes	2.00
594	11.88	1.02	100.00	3.22	0.59	0.94	8.84	0.00	8.84	4.000	No	Yes	2.00
595	11.90	1.04	100.00	3.22	0.59	0.94	9.10	0.00	9.10	4.000	No	Yes	2.00
596	11.93	1.06	100.00	3.22	0.59	0.94	9.20	0.00	9.20	4.000	No	Yes	2.00
597	11.94	1.07	100.00	3.23	0.59	0.94	9.26	0.00	9.26	4.000	No	Yes	2.00
598	11.96	1.08	100.00	3.24	0.58	0.94	9.38	0.00	9.38	4.000	No	Yes	2.00
599	11.98	1.08	100.00	3.25	0.58	0.94	9.43	0.00	9.43	4.000	No	Yes	2.00
600	12.00	1.08	100.00	3.25	0.58	0.94	9.34	0.00	9.34	4.000	No	Yes	2.00
601	12.02	1.09	100.00	3.26	0.59	0.94	9.29	0.00	9.29	4.000	No	Yes	2.00
602	12.04	1.09	100.00	3.25	0.58	0.94	9.47	0.00	9.47	4.000	No	Yes	2.00
603	12.06	1.10	100.00	3.25	0.58	0.94	9.48	0.00	9.48	4.000	No	Yes	2.00
604	12.08	1.10	100.00	3.25	0.58	0.94	9.47	0.00	9.47	4.000	No	Yes	2.00
605	12.10	1.10	100.00	3.25	0.58	0.94	9.44	0.00	9.44	4.000	No	Yes	2.00
606	12.12	1.10	100.00	3.25	0.58	0.93	9.32	0.00	9.32	4.000	No	Yes	2.00
607	12.14	1.10	100.00	3.25	0.58	0.93	9.44	0.00	9.44	4.000	No	Yes	2.00
608	12.16	1.11	100.00	3.24	0.58	0.93	9.43	0.00	9.43	4.000	No	Yes	2.00
609	12.18	1.12	100.00	3.24	0.58	0.93	9.63	0.00	9.63	4.000	No	Yes	2.00
610	12.20	1.13	100.00	3.23	0.58	0.93	9.57	0.00	9.57	4.000	No	Yes	2.00
611	12.22	1.14	100.00	3.22	0.58	0.93	9.77	0.00	9.77	4.000	No	Yes	2.00
612	12.24	1.16	100.00	3.21	0.58	0.93	9.91	0.00	9.91	4.000	No	Yes	2.00
613	12.26	1.18	100.00	3.21	0.58	0.93	9.96	0.00	9.96	4.000	No	Yes	2.00
614	12.28	1.20	100.00	3.20	0.58	0.93	10.26	0.00	10.26	4.000	No	Yes	2.00
615	12.30	1.23	100.00	3.18	0.58	0.93	10.37	0.00	10.37	4.000	No	Yes	2.00
616	12.33	1.25	100.00	3.17	0.58	0.93	10.86	0.00	10.86	4.000	No	Yes	2.00
617	12.34	1.29	100.00	3.16	0.58	0.93	10.98	0.00	10.98	4.000	No	Yes	2.00
618	12.36	1.31	100.00	3.15	0.58	0.93	11.23	0.00	11.23	4.000	No	Yes	2.00
619	12.38	1.35	100.00	3.14	0.58	0.93	11.57	0.00	11.57	4.000	No	Yes	2.00
620	12.40	1.38	100.00	3.14	0.57	0.93	12.08	0.00	12.08	4.000	No	Yes	2.00
621	12.42	1.40	100.00	3.14	0.57	0.92	12.11	0.00	12.11	4.000	No	Yes	2.00
622	12.44	1.41	100.00	3.15	0.57	0.92	12.28	0.00	12.28	4.000	No	Yes	2.00
623	12.46	1.41	100.00	3.17	0.57	0.92	12.27	0.00	12.27	4.000	No	Yes	2.00
624	12.48	1.39	100.00	3.19	0.57	0.92	12.14	0.00	12.14	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	1.37	100.00	3.21	0.57	0.92	11.96	0.00	11.96	4.000	No	Yes	2.00
626	12.52	1.35	100.00	3.23	0.58	0.92	11.76	0.00	11.76	4.000	No	Yes	2.00
627	12.54	1.32	100.00	3.25	0.58	0.92	11.36	0.00	11.36	4.000	No	Yes	2.00
628	12.56	1.29	100.00	3.27	0.58	0.92	11.16	0.00	11.16	4.000	No	Yes	2.00
629	12.58	1.26	100.00	3.29	0.58	0.92	10.96	0.00	10.96	4.000	No	Yes	2.00
630	12.60	1.23	100.00	3.30	0.58	0.92	10.58	0.00	10.58	4.000	No	Yes	2.00
631	12.62	1.20	100.00	3.32	0.58	0.92	10.32	0.00	10.32	4.000	No	Yes	2.00
632	12.64	1.17	100.00	3.33	0.58	0.92	9.96	0.00	9.96	4.000	No	Yes	2.00
633	12.66	1.15	100.00	3.34	0.58	0.91	9.89	0.00	9.89	4.000	No	Yes	2.00
634	12.68	1.12	100.00	3.35	0.58	0.91	9.63	0.00	9.63	4.000	No	Yes	2.00
635	12.70	1.07	100.00	3.37	0.59	0.91	9.21	0.00	9.21	4.000	No	Yes	2.00
636	12.72	1.01	100.00	3.41	0.59	0.91	8.54	0.00	8.54	4.000	No	Yes	2.00
637	12.74	0.95	100.00	3.44	0.59	0.91	8.00	0.00	8.00	4.000	No	Yes	2.00
638	12.76	0.89	100.00	3.47	0.59	0.91	7.34	0.00	7.34	4.000	No	Yes	2.00
639	12.78	0.85	100.00	3.48	0.59	0.91	6.84	0.00	6.84	4.000	No	Yes	2.00
640	12.81	0.83	100.00	3.47	0.60	0.91	6.63	0.00	6.63	4.000	No	Yes	2.00
641	12.82	0.81	100.00	3.45	0.60	0.91	6.73	0.00	6.73	4.000	No	Yes	2.00
642	12.84	0.80	100.00	3.44	0.60	0.91	6.58	0.00	6.58	4.000	No	Yes	2.00
643	12.86	0.78	100.00	3.43	0.60	0.91	6.37	0.00	6.37	4.000	No	Yes	2.00
644	12.88	0.76	100.00	3.44	0.60	0.90	6.15	0.00	6.15	4.000	No	Yes	2.00
645	12.90	0.74	100.00	3.43	0.60	0.90	5.86	0.00	5.86	4.000	No	Yes	2.00
646	12.92	0.74	100.00	3.41	0.60	0.90	5.98	0.00	5.98	4.000	No	Yes	2.00
647	12.94	0.73	100.00	3.40	0.60	0.90	5.87	0.00	5.87	4.000	No	Yes	2.00
648	12.96	0.71	100.00	3.41	0.60	0.90	5.67	0.00	5.67	4.000	No	Yes	2.00
649	12.98	0.70	100.00	3.39	0.60	0.90	5.49	0.00	5.49	4.000	No	Yes	2.00
650	13.00	0.71	100.00	3.35	0.60	0.90	5.58	0.00	5.58	4.000	No	Yes	2.00
651	13.02	0.73	100.00	3.31	0.60	0.90	5.86	0.00	5.86	4.000	No	Yes	2.00
652	13.04	0.75	100.00	3.27	0.60	0.90	5.86	0.00	5.86	4.000	No	Yes	2.00
653	13.06	0.76	100.00	3.25	0.60	0.90	5.96	0.00	5.96	4.000	No	Yes	2.00
654	13.08	0.77	100.00	3.24	0.60	0.90	6.10	0.00	6.10	4.000	No	Yes	2.00
655	13.10	0.78	100.00	3.23	0.60	0.90	6.14	0.00	6.14	4.000	No	Yes	2.00
656	13.12	0.80	100.00	3.23	0.60	0.90	6.34	0.00	6.34	4.000	No	Yes	2.00
657	13.15	0.82	100.00	3.22	0.60	0.90	6.45	0.00	6.45	4.000	No	Yes	2.00
658	13.16	0.83	100.00	3.23	0.60	0.90	6.68	0.00	6.68	4.000	No	Yes	2.00
659	13.18	0.84	100.00	3.24	0.60	0.90	6.63	0.00	6.63	4.000	No	Yes	2.00
660	13.20	0.84	100.00	3.26	0.59	0.90	6.83	0.00	6.83	4.000	No	Yes	2.00
661	13.22	0.83	100.00	3.28	0.60	0.90	6.65	0.00	6.65	4.000	No	Yes	2.00
662	13.24	0.81	100.00	3.32	0.60	0.89	6.55	0.00	6.55	4.000	No	Yes	2.00
663	13.26	0.78	100.00	3.36	0.60	0.89	6.13	0.00	6.13	4.000	No	Yes	2.00
664	13.29	0.74	100.00	3.40	0.60	0.89	5.88	0.00	5.88	4.000	No	Yes	2.00
665	13.30	0.72	100.00	3.43	0.60	0.89	5.72	0.00	5.72	4.000	No	Yes	2.00
666	13.32	0.70	100.00	3.45	0.60	0.89	5.48	0.00	5.48	4.000	No	Yes	2.00
667	13.34	0.68	100.00	3.46	0.60	0.89	5.34	0.00	5.34	4.000	No	Yes	2.00
668	13.36	0.68	100.00	3.45	0.60	0.89	5.22	0.00	5.22	4.000	No	Yes	2.00
669	13.38	0.67	100.00	3.45	0.60	0.89	5.36	0.00	5.36	4.000	No	Yes	2.00
670	13.40	0.68	100.00	3.42	0.60	0.89	5.26	0.00	5.26	4.000	No	Yes	2.00
671	13.42	0.69	100.00	3.40	0.60	0.89	5.43	0.00	5.43	4.000	No	Yes	2.00
672	13.44	0.72	100.00	3.35	0.60	0.89	5.59	0.00	5.59	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	0.76	100.00	3.30	0.60	0.89	5.99	0.00	5.99	4.000	No	Yes	2.00
674	13.49	0.78	100.00	3.27	0.60	0.89	6.40	0.00	6.40	4.000	No	Yes	2.00
675	13.50	0.80	100.00	3.24	0.60	0.89	6.04	0.00	6.04	4.000	No	Yes	2.00
676	13.52	0.89	100.00	3.16	0.60	0.89	6.69	0.00	6.69	4.000	No	Yes	2.00
677	13.54	1.16	99.14	2.95	0.59	0.89	8.66	0.00	8.66	4.000	No	Yes	2.00
678	13.56	1.50	84.57	2.77	0.57	0.89	13.27	0.00	13.27	4.000	No	Yes	2.00
679	13.58	1.77	78.99	2.70	0.56	0.89	16.31	0.00	16.31	4.000	No	Yes	2.00
680	13.60	1.87	81.05	2.73	0.56	0.89	16.52	0.00	16.52	4.000	No	Yes	2.00
681	13.62	1.92	83.86	2.76	0.56	0.89	16.41	0.00	16.41	4.000	No	Yes	2.00
682	13.64	2.03	83.67	2.76	0.56	0.89	17.71	0.00	17.71	4.000	No	Yes	2.00
683	13.66	2.17	82.69	2.75	0.55	0.89	19.35	0.00	19.35	4.000	No	Yes	2.00
684	13.68	2.33	81.69	2.73	0.55	0.89	20.00	0.00	20.00	4.000	No	Yes	2.00
685	13.70	2.50	80.67	2.72	0.54	0.89	22.09	0.00	22.09	4.000	No	Yes	2.00
686	13.72	2.65	78.95	2.70	0.54	0.89	23.84	0.00	23.84	4.000	No	Yes	2.00
687	13.74	2.63	78.71	2.70	0.54	0.89	23.91	0.00	23.91	4.000	No	Yes	2.00
688	13.76	2.40	80.65	2.72	0.55	0.89	21.47	0.00	21.47	4.000	No	Yes	2.00
689	13.78	2.11	83.86	2.76	0.56	0.89	17.86	0.00	17.86	4.000	No	Yes	2.00
690	13.81	1.89	87.07	2.80	0.56	0.88	16.08	0.00	16.08	4.000	No	Yes	2.00
691	13.82	1.89	86.04	2.79	0.57	0.88	15.53	0.00	15.53	4.000	No	Yes	2.00
692	13.84	2.00	85.02	2.78	0.56	0.88	17.73	0.00	17.73	4.000	No	Yes	2.00
693	13.86	2.12	85.29	2.78	0.55	0.88	19.06	0.00	19.06	4.000	No	Yes	2.00
694	13.88	2.13	87.84	2.81	0.55	0.88	18.69	0.00	18.69	4.000	No	Yes	2.00
695	13.90	2.05	90.16	2.84	0.56	0.88	17.94	0.00	17.94	4.000	No	Yes	2.00
696	13.92	1.94	92.52	2.87	0.56	0.88	17.09	0.00	17.09	4.000	No	Yes	2.00
697	13.94	1.82	95.49	2.91	0.56	0.88	15.81	0.00	15.81	4.000	No	Yes	2.00
698	13.96	1.69	99.19	2.95	0.56	0.88	14.69	0.00	14.69	4.000	No	Yes	2.00
699	13.98	1.58	100.00	2.99	0.57	0.88	13.61	0.00	13.61	4.000	No	Yes	2.00
700	14.00	1.51	100.00	3.01	0.57	0.88	12.89	0.00	12.89	4.000	No	Yes	2.00
701	14.02	1.48	100.00	3.03	0.57	0.88	12.68	0.00	12.68	4.000	No	Yes	2.00
702	14.04	1.47	100.00	3.05	0.57	0.88	12.75	0.00	12.75	4.000	No	Yes	2.00
703	14.06	1.45	100.00	3.07	0.57	0.88	12.68	0.00	12.68	4.000	No	Yes	2.00
704	14.08	1.41	100.00	3.10	0.57	0.87	12.16	0.00	12.16	4.000	No	Yes	2.00
705	14.10	1.31	100.00	3.16	0.58	0.87	11.66	0.00	11.66	4.000	No	Yes	2.00
706	14.12	1.19	100.00	3.22	0.58	0.87	10.14	0.00	10.14	4.000	No	Yes	2.00
707	14.15	1.02	100.00	3.33	0.59	0.87	8.81	0.00	8.81	4.000	No	Yes	2.00
708	14.16	0.88	100.00	3.44	0.59	0.87	7.13	0.00	7.13	4.000	No	Yes	2.00
709	14.18	0.82	100.00	3.48	0.60	0.87	6.48	0.00	6.48	4.000	No	Yes	2.00
710	14.20	1.04	100.00	3.27	0.59	0.87	7.20	0.00	7.20	4.000	No	Yes	2.00
711	14.22	1.39	100.00	3.03	0.57	0.87	12.59	0.00	12.59	4.000	No	Yes	2.00
712	14.24	1.68	93.87	2.89	0.56	0.87	15.44	0.00	15.44	4.000	No	Yes	2.00
713	14.26	1.69	93.01	2.88	0.57	0.87	14.79	0.00	14.79	4.000	No	Yes	2.00
714	14.28	1.55	97.81	2.94	0.57	0.87	12.85	0.00	12.85	4.000	No	Yes	2.00
715	14.30	1.40	100.00	3.00	0.58	0.87	11.76	0.00	11.76	4.000	No	Yes	2.00
716	14.32	1.29	100.00	3.06	0.58	0.87	10.99	0.00	10.99	4.000	No	Yes	2.00
717	14.34	1.17	100.00	3.15	0.58	0.86	9.95	0.00	9.95	4.000	No	Yes	2.00
718	14.36	1.02	100.00	3.27	0.59	0.86	8.51	0.00	8.51	4.000	No	Yes	2.00
719	14.38	0.87	100.00	3.42	0.59	0.86	7.25	0.00	7.25	4.000	No	Yes	2.00
720	14.40	0.80	100.00	3.49	0.60	0.86	5.87	0.00	5.87	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	0.92	100.00	3.36	0.60	0.86	6.60	0.00	6.60	4.000	No	Yes	2.00
722	14.44	1.26	100.00	3.09	0.58	0.86	10.24	0.00	10.24	4.000	No	Yes	2.00
723	14.46	1.59	95.72	2.91	0.57	0.86	14.41	0.00	14.41	4.000	No	Yes	2.00
724	14.48	1.71	92.02	2.86	0.56	0.86	15.24	0.00	15.24	4.000	No	Yes	2.00
725	14.50	1.61	95.23	2.90	0.57	0.86	13.40	0.00	13.40	4.000	No	Yes	2.00
726	14.52	1.45	100.00	2.98	0.57	0.86	12.02	0.00	12.02	4.000	No	Yes	2.00
727	14.54	1.30	100.00	3.06	0.58	0.86	11.06	0.00	11.06	4.000	No	Yes	2.00
728	14.56	1.14	100.00	3.17	0.58	0.86	9.51	0.00	9.51	4.000	No	Yes	2.00
729	14.58	0.97	100.00	3.32	0.59	0.86	8.00	0.00	8.00	4.000	No	Yes	2.00
730	14.60	0.83	100.00	3.47	0.60	0.85	6.54	0.00	6.54	4.000	No	Yes	2.00
731	14.62	0.77	100.00	3.53	0.60	0.85	5.79	0.00	5.79	4.000	No	Yes	2.00
732	14.64	0.96	100.00	3.33	0.60	0.85	6.38	0.00	6.38	4.000	No	Yes	2.00
733	14.66	1.40	100.00	3.02	0.58	0.86	11.25	0.00	11.25	4.000	No	Yes	2.00
734	14.68	2.03	82.62	2.75	0.56	0.86	16.82	0.00	16.82	4.000	Yes	Yes	2.00
735	14.70	2.53	69.39	2.58	0.55	0.86	22.49	57.06	79.55	4.000	Yes	No	2.00
736	14.72	2.85	61.07	2.48	0.55	0.86	24.40	55.82	80.22	4.000	Yes	No	2.00
737	14.74	2.95	57.11	2.43	0.55	0.86	25.30	55.03	80.33	4.000	Yes	No	2.00
738	14.76	2.86	58.22	2.44	0.55	0.86	24.94	55.24	80.17	0.116	No	No	0.63
739	14.78	2.55	67.44	2.56	0.55	0.86	22.14	56.58	78.73	0.115	No	No	0.62
740	14.80	2.26	79.96	2.71	0.56	0.86	17.52	0.00	17.52	4.000	No	Yes	2.00
741	14.82	2.31	81.09	2.73	0.56	0.86	17.30	0.00	17.30	4.000	No	Yes	2.00
742	14.85	2.65	74.98	2.65	0.54	0.86	23.63	0.00	23.63	4.000	No	Yes	2.00
743	14.86	2.99	67.25	2.55	0.54	0.86	26.21	57.72	83.93	0.120	No	No	0.66
744	14.88	3.06	66.05	2.54	0.54	0.86	26.15	57.45	83.60	0.119	No	No	0.65
745	14.90	3.02	65.91	2.54	0.54	0.86	25.42	57.22	82.64	0.118	No	No	0.65
746	14.92	2.88	65.37	2.53	0.54	0.86	24.97	56.97	81.94	0.118	No	No	0.64
747	14.94	2.69	65.89	2.54	0.55	0.86	22.60	56.40	79.00	4.000	Yes	No	2.00
748	14.97	2.50	68.40	2.57	0.56	0.85	20.39	56.26	76.65	4.000	Yes	No	2.00
749	14.98	2.52	72.38	2.62	0.55	0.85	20.19	0.00	20.19	4.000	Yes	Yes	2.00
750	15.00	2.70	74.47	2.64	0.54	0.86	23.02	0.00	23.02	4.000	Yes	Yes	2.00
751	15.02	2.93	74.93	2.65	0.54	0.86	24.96	0.00	24.96	4.000	No	Yes	2.00
752	15.04	3.00	77.15	2.68	0.53	0.86	26.25	0.00	26.25	4.000	No	Yes	2.00
753	15.06	2.75	82.47	2.74	0.53	0.86	24.75	0.00	24.75	4.000	No	Yes	2.00
754	15.08	2.27	90.99	2.85	0.55	0.85	18.66	0.00	18.66	4.000	No	Yes	2.00
755	15.10	1.67	100.00	3.00	0.57	0.85	13.71	0.00	13.71	4.000	No	Yes	2.00
756	15.13	1.24	100.00	3.17	0.58	0.84	9.60	0.00	9.60	4.000	No	Yes	2.00
757	15.14	1.01	100.00	3.30	0.59	0.84	7.56	0.00	7.56	4.000	No	Yes	2.00
758	15.16	0.99	100.00	3.31	0.59	0.84	7.47	0.00	7.47	4.000	No	Yes	2.00
759	15.18	1.08	100.00	3.24	0.59	0.84	8.92	0.00	8.92	4.000	No	Yes	2.00
760	15.20	1.15	100.00	3.19	0.58	0.84	9.50	0.00	9.50	4.000	No	Yes	2.00
761	15.22	1.14	100.00	3.21	0.59	0.84	9.30	0.00	9.30	4.000	No	Yes	2.00
762	15.24	1.08	100.00	3.26	0.59	0.84	8.57	0.00	8.57	4.000	No	Yes	2.00
763	15.26	1.01	100.00	3.33	0.59	0.84	7.98	0.00	7.98	4.000	No	Yes	2.00
764	15.28	0.96	100.00	3.38	0.59	0.84	7.63	0.00	7.63	4.000	No	Yes	2.00
765	15.30	0.93	100.00	3.42	0.59	0.84	7.23	0.00	7.23	4.000	No	Yes	2.00
766	15.32	0.94	100.00	3.42	0.59	0.84	7.28	0.00	7.28	4.000	No	Yes	2.00
767	15.34	0.96	100.00	3.40	0.59	0.83	7.74	0.00	7.74	4.000	No	Yes	2.00
768	15.36	0.96	100.00	3.38	0.59	0.83	7.84	0.00	7.84	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	0.97	100.00	3.35	0.59	0.83	7.29	0.00	7.29	4.000	No	Yes	2.00
770	15.40	1.02	100.00	3.29	0.59	0.83	7.83	0.00	7.83	4.000	No	Yes	2.00
771	15.42	1.08	100.00	3.20	0.59	0.83	8.98	0.00	8.98	4.000	No	Yes	2.00
772	15.44	1.13	100.00	3.16	0.59	0.83	8.92	0.00	8.92	4.000	No	Yes	2.00
773	15.46	1.29	100.00	3.06	0.59	0.83	8.97	0.00	8.97	4.000	No	Yes	2.00
774	15.48	1.55	98.38	2.94	0.57	0.84	12.97	0.00	12.97	4.000	No	Yes	2.00
775	15.50	1.75	92.39	2.87	0.56	0.84	15.47	0.00	15.47	4.000	No	Yes	2.00
776	15.52	1.69	95.96	2.91	0.57	0.84	14.08	0.00	14.08	4.000	No	Yes	2.00
777	15.54	1.59	100.00	2.99	0.58	0.83	11.57	0.00	11.57	4.000	No	Yes	2.00
778	15.56	1.69	99.52	2.96	0.57	0.83	12.65	0.00	12.65	4.000	No	Yes	2.00
779	15.58	1.89	93.67	2.88	0.56	0.84	16.65	0.00	16.65	4.000	No	Yes	2.00
780	15.60	2.09	89.87	2.84	0.56	0.84	17.38	0.00	17.38	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.11	2.00	0.00	9.95	0.03	0.00	0.12	2.00	0.00	9.94	0.01	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.96	2.00	0.00	9.52	0.04	0.00	0.96	2.00	0.00	9.52	0.00	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.21	2.00	0.00	9.40	0.03	0.00
1.22	2.00	0.00	9.39	0.01	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.96	2.00	0.00	9.02	0.04	0.00	1.96	2.00	0.00	9.02	0.00	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.23	2.00	0.00	8.89	0.03	0.00	2.24	2.00	0.00	8.88	0.01	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.91	2.00	0.00	8.55	0.03	0.00	2.92	2.00	0.00	8.54	0.01	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.21	2.00	0.00	8.40	0.03	0.00
3.22	2.00	0.00	8.39	0.01	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.05	2.00	0.00	7.98	0.03	0.00
4.06	2.00	0.00	7.97	0.01	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.93	2.00	0.00	7.54	0.03	0.00
4.94	2.00	0.00	7.53	0.01	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	0.65	0.35	7.42	0.02	0.05
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.29	2.00	0.00	7.36	0.03	0.00
5.30	2.00	0.00	7.35	0.01	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.93	2.00	0.00	7.04	0.03	0.00
5.94	2.00	0.00	7.03	0.01	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.01	2.00	0.00	7.00	0.03	0.00
6.02	2.00	0.00	6.99	0.01	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.09	2.00	0.00	6.46	0.03	0.00
7.10	2.00	0.00	6.45	0.01	0.00	7.14	2.00	0.00	6.43	0.04	0.00
7.15	2.00	0.00	6.43	0.01	0.00	7.16	2.00	0.00	6.42	0.01	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.31	2.00	0.00	6.35	0.03	0.00	7.32	2.00	0.00	6.34	0.01	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.19	2.00	0.00	5.91	0.03	0.00	8.20	2.00	0.00	5.90	0.01	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.93	2.00	0.00	5.54	0.03	0.00
8.94	2.00	0.00	5.53	0.01	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.99	2.00	0.00	5.51	0.03	0.00	9.00	2.00	0.00	5.50	0.01	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.03	2.00	0.00	4.99	0.03	0.00	10.04	2.00	0.00	4.98	0.01	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	0.66	0.34	4.62	0.02	0.03
10.78	0.64	0.36	4.61	0.02	0.03	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.15	2.00	0.00	4.43	0.03	0.00	11.16	2.00	0.00	4.42	0.01	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.93	2.00	0.00	4.04	0.03	0.00
11.94	2.00	0.00	4.03	0.01	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.33	2.00	0.00	3.84	0.03	0.00
12.34	2.00	0.00	3.83	0.01	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.81	2.00	0.00	3.60	0.03	0.00
12.82	2.00	0.00	3.59	0.01	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.15	2.00	0.00	3.43	0.03	0.00	13.16	2.00	0.00	3.42	0.01	0.00
13.18	2.00	0.00	3.41	0.02	0.00	13.20	2.00	0.00	3.40	0.02	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.29	2.00	0.00	3.36	0.03	0.00
13.30	2.00	0.00	3.35	0.01	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.49	2.00	0.00	3.26	0.03	0.00
13.50	2.00	0.00	3.25	0.01	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.81	2.00	0.00	3.10	0.03	0.00
13.82	2.00	0.00	3.09	0.01	0.00	13.84	2.00	0.00	3.08	0.02	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.12	2.00	0.00	2.94	0.02	0.00
14.15	2.00	0.00	2.93	0.03	0.00	14.16	2.00	0.00	2.92	0.01	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	0.63	0.37	2.62	0.02	0.02
14.78	0.62	0.38	2.61	0.02	0.02	14.80	2.00	0.00	2.60	0.02	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.85	2.00	0.00	2.58	0.03	0.00
14.86	0.66	0.34	2.57	0.01	0.01	14.88	0.65	0.35	2.56	0.02	0.02
14.90	0.65	0.35	2.55	0.02	0.02	14.92	0.64	0.36	2.54	0.02	0.02
14.94	2.00	0.00	2.53	0.02	0.00	14.97	2.00	0.00	2.52	0.03	0.00
14.98	2.00	0.00	2.51	0.01	0.00	15.00	2.00	0.00	2.50	0.02	0.00
15.02	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.13	2.00	0.00	2.44	0.03	0.00
15.14	2.00	0.00	2.43	0.01	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00

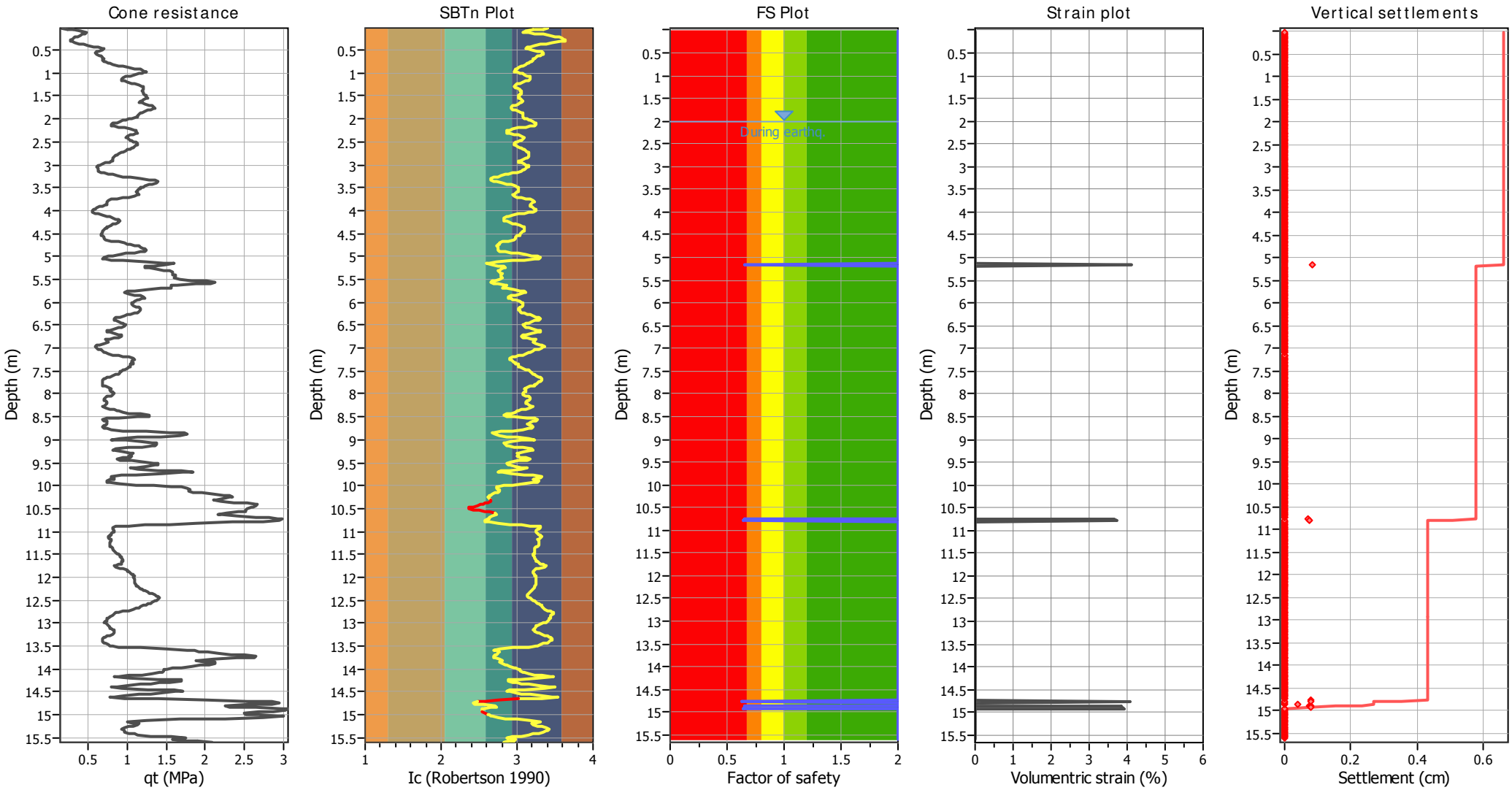
Overall liquefaction potential: 0.22

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.00	16.69	2.00	0.00	1.00	0.00	2.02	16.15	2.00	0.00	1.00	0.00
2.04	15.73	2.00	0.00	1.00	0.00	2.06	15.08	2.00	0.00	1.00	0.00
2.08	14.12	2.00	0.00	1.00	0.00	2.10	13.43	2.00	0.00	1.00	0.00
2.12	13.05	2.00	0.00	1.00	0.00	2.14	12.96	2.00	0.00	1.00	0.00
2.16	13.18	2.00	0.00	1.00	0.00	2.18	14.31	2.00	0.00	1.00	0.00
2.20	15.80	2.00	0.00	1.00	0.00	2.23	16.87	2.00	0.00	1.00	0.00
2.24	18.32	2.00	0.00	1.00	0.00	2.26	17.96	2.00	0.00	1.00	0.00
2.28	18.30	2.00	0.00	1.00	0.00	2.30	18.45	2.00	0.00	1.00	0.00
2.32	18.11	2.00	0.00	1.00	0.00	2.34	17.28	2.00	0.00	1.00	0.00
2.36	16.47	2.00	0.00	1.00	0.00	2.38	15.94	2.00	0.00	1.00	0.00
2.40	15.49	2.00	0.00	1.00	0.00	2.42	15.41	2.00	0.00	1.00	0.00
2.44	16.13	2.00	0.00	1.00	0.00	2.46	16.05	2.00	0.00	1.00	0.00
2.48	16.52	2.00	0.00	1.00	0.00	2.50	16.71	2.00	0.00	1.00	0.00
2.52	17.11	2.00	0.00	1.00	0.00	2.54	17.48	2.00	0.00	1.00	0.00
2.56	17.51	2.00	0.00	1.00	0.00	2.58	17.27	2.00	0.00	1.00	0.00
2.60	16.87	2.00	0.00	1.00	0.00	2.62	16.33	2.00	0.00	1.00	0.00
2.64	16.23	2.00	0.00	1.00	0.00	2.66	15.86	2.00	0.00	1.00	0.00
2.68	15.39	2.00	0.00	1.00	0.00	2.70	14.85	2.00	0.00	1.00	0.00
2.72	14.59	2.00	0.00	1.00	0.00	2.74	13.92	2.00	0.00	1.00	0.00
2.76	13.56	2.00	0.00	1.00	0.00	2.78	13.09	2.00	0.00	1.00	0.00
2.80	12.79	2.00	0.00	1.00	0.00	2.82	12.46	2.00	0.00	1.00	0.00
2.84	12.30	2.00	0.00	1.00	0.00	2.86	12.08	2.00	0.00	1.00	0.00
2.88	11.79	2.00	0.00	1.00	0.00	2.91	11.78	2.00	0.00	1.00	0.00
2.92	11.77	2.00	0.00	1.00	0.00	2.94	11.12	2.00	0.00	1.00	0.00
2.96	10.70	2.00	0.00	1.00	0.00	2.98	10.15	2.00	0.00	1.00	0.00
3.00	9.40	2.00	0.00	1.00	0.00	3.02	8.92	2.00	0.00	1.00	0.00
3.04	8.54	2.00	0.00	1.00	0.00	3.06	8.69	2.00	0.00	1.00	0.00
3.08	8.85	2.00	0.00	1.00	0.00	3.10	8.80	2.00	0.00	1.00	0.00
3.12	8.83	2.00	0.00	1.00	0.00	3.14	8.95	2.00	0.00	1.00	0.00
3.16	9.10	2.00	0.00	1.00	0.00	3.18	9.75	2.00	0.00	1.00	0.00
3.21	10.37	2.00	0.00	1.00	0.00	3.22	11.35	2.00	0.00	1.00	0.00
3.24	12.17	2.00	0.00	1.00	0.00	3.26	12.94	2.00	0.00	1.00	0.00
3.28	14.71	2.00	0.00	1.00	0.00	3.30	16.47	2.00	0.00	1.00	0.00
3.32	18.48	2.00	0.00	1.00	0.00	3.34	19.61	2.00	0.00	1.00	0.00
3.36	20.35	2.00	0.00	1.00	0.00	3.38	19.96	2.00	0.00	1.00	0.00
3.40	19.66	2.00	0.00	1.00	0.00	3.42	19.05	2.00	0.00	1.00	0.00
3.44	17.98	2.00	0.00	1.00	0.00	3.46	17.76	2.00	0.00	1.00	0.00
3.48	16.73	2.00	0.00	1.00	0.00	3.50	16.92	2.00	0.00	1.00	0.00
3.52	16.61	2.00	0.00	1.00	0.00	3.54	16.08	2.00	0.00	1.00	0.00
3.56	16.01	2.00	0.00	1.00	0.00	3.58	15.79	2.00	0.00	1.00	0.00
3.60	15.57	2.00	0.00	1.00	0.00	3.62	15.85	2.00	0.00	1.00	0.00
3.64	16.01	2.00	0.00	1.00	0.00	3.66	16.25	2.00	0.00	1.00	0.00
3.68	15.42	2.00	0.00	1.00	0.00	3.70	14.43	2.00	0.00	1.00	0.00
3.72	13.47	2.00	0.00	1.00	0.00	3.74	12.10	2.00	0.00	1.00	0.00
3.76	11.20	2.00	0.00	1.00	0.00	3.78	10.52	2.00	0.00	1.00	0.00
3.80	10.12	2.00	0.00	1.00	0.00	3.82	10.23	2.00	0.00	1.00	0.00
3.84	10.37	2.00	0.00	1.00	0.00	3.86	10.38	2.00	0.00	1.00	0.00
3.88	9.98	2.00	0.00	1.00	0.00	3.90	9.41	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.92	8.84	2.00	0.00	1.00	0.00	3.94	8.14	2.00	0.00	1.00	0.00
3.96	7.94	2.00	0.00	1.00	0.00	3.98	7.37	2.00	0.00	1.00	0.00
4.00	7.23	2.00	0.00	1.00	0.00	4.02	7.13	2.00	0.00	1.00	0.00
4.05	7.24	2.00	0.00	1.00	0.00	4.06	7.52	2.00	0.00	1.00	0.00
4.08	7.98	2.00	0.00	1.00	0.00	4.10	8.78	2.00	0.00	1.00	0.00
4.12	9.33	2.00	0.00	1.00	0.00	4.14	10.18	2.00	0.00	1.00	0.00
4.16	10.55	2.00	0.00	1.00	0.00	4.18	10.87	2.00	0.00	1.00	0.00
4.20	11.63	2.00	0.00	1.00	0.00	4.22	11.67	2.00	0.00	1.00	0.00
4.24	11.69	2.00	0.00	1.00	0.00	4.26	11.61	2.00	0.00	1.00	0.00
4.28	11.17	2.00	0.00	1.00	0.00	4.30	10.76	2.00	0.00	1.00	0.00
4.32	10.42	2.00	0.00	1.00	0.00	4.34	9.92	2.00	0.00	1.00	0.00
4.36	9.55	2.00	0.00	1.00	0.00	4.38	9.45	2.00	0.00	1.00	0.00
4.40	9.20	2.00	0.00	1.00	0.00	4.42	8.77	2.00	0.00	1.00	0.00
4.44	8.70	2.00	0.00	1.00	0.00	4.46	8.57	2.00	0.00	1.00	0.00
4.48	8.41	2.00	0.00	1.00	0.00	4.50	8.46	2.00	0.00	1.00	0.00
4.52	8.30	2.00	0.00	1.00	0.00	4.54	8.26	2.00	0.00	1.00	0.00
4.56	8.61	2.00	0.00	1.00	0.00	4.58	8.79	2.00	0.00	1.00	0.00
4.60	8.66	2.00	0.00	1.00	0.00	4.62	8.59	2.00	0.00	1.00	0.00
4.64	8.85	2.00	0.00	1.00	0.00	4.66	9.42	2.00	0.00	1.00	0.00
4.68	11.40	2.00	0.00	1.00	0.00	4.70	12.63	2.00	0.00	1.00	0.00
4.72	12.36	2.00	0.00	1.00	0.00	4.74	12.82	2.00	0.00	1.00	0.00
4.76	13.98	2.00	0.00	1.00	0.00	4.78	14.20	2.00	0.00	1.00	0.00
4.80	15.34	2.00	0.00	1.00	0.00	4.82	14.72	2.00	0.00	1.00	0.00
4.84	15.31	2.00	0.00	1.00	0.00	4.86	16.21	2.00	0.00	1.00	0.00
4.88	14.90	2.00	0.00	1.00	0.00	4.90	15.85	2.00	0.00	1.00	0.00
4.93	13.97	2.00	0.00	1.00	0.00	4.94	12.89	2.00	0.00	1.00	0.00
4.96	11.54	2.00	0.00	1.00	0.00	4.98	10.51	2.00	0.00	1.00	0.00
5.00	9.48	2.00	0.00	1.00	0.00	5.02	8.65	2.00	0.00	1.00	0.00
5.04	8.61	2.00	0.00	1.00	0.00	5.06	8.60	2.00	0.00	1.00	0.00
5.08	9.31	2.00	0.00	1.00	0.00	5.10	11.57	2.00	0.00	1.00	0.00
5.12	14.44	2.00	0.00	1.00	0.00	5.14	20.59	2.00	0.00	1.00	0.00
5.16	77.66	0.65	4.12	1.00	0.08	5.18	19.35	2.00	0.00	1.00	0.00
5.20	16.39	2.00	0.00	1.00	0.00	5.22	15.37	2.00	0.00	1.00	0.00
5.24	15.03	2.00	0.00	1.00	0.00	5.26	16.17	2.00	0.00	1.00	0.00
5.29	17.37	2.00	0.00	1.00	0.00	5.30	18.87	2.00	0.00	1.00	0.00
5.32	19.68	2.00	0.00	1.00	0.00	5.34	20.17	2.00	0.00	1.00	0.00
5.36	19.84	2.00	0.00	1.00	0.00	5.38	19.75	2.00	0.00	1.00	0.00
5.40	20.08	2.00	0.00	1.00	0.00	5.42	20.28	2.00	0.00	1.00	0.00
5.44	20.55	2.00	0.00	1.00	0.00	5.46	19.89	2.00	0.00	1.00	0.00
5.48	19.78	2.00	0.00	1.00	0.00	5.50	20.53	2.00	0.00	1.00	0.00
5.52	22.77	2.00	0.00	1.00	0.00	5.54	24.87	2.00	0.00	1.00	0.00
5.56	27.11	2.00	0.00	1.00	0.00	5.58	27.18	2.00	0.00	1.00	0.00
5.60	22.77	2.00	0.00	1.00	0.00	5.62	20.15	2.00	0.00	1.00	0.00
5.64	18.32	2.00	0.00	1.00	0.00	5.66	19.76	2.00	0.00	1.00	0.00
5.68	19.93	2.00	0.00	1.00	0.00	5.70	17.97	2.00	0.00	1.00	0.00
5.72	15.48	2.00	0.00	1.00	0.00	5.74	13.25	2.00	0.00	1.00	0.00
5.76	12.07	2.00	0.00	1.00	0.00	5.78	11.50	2.00	0.00	1.00	0.00
5.80	11.62	2.00	0.00	1.00	0.00	5.82	12.51	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.84	13.28	2.00	0.00	1.00	0.00	5.86	13.84	2.00	0.00	1.00	0.00
5.88	15.13	2.00	0.00	1.00	0.00	5.90	14.31	2.00	0.00	1.00	0.00
5.93	14.12	2.00	0.00	1.00	0.00	5.94	13.65	2.00	0.00	1.00	0.00
5.96	13.50	2.00	0.00	1.00	0.00	5.98	13.10	2.00	0.00	1.00	0.00
6.01	12.62	2.00	0.00	1.00	0.00	6.02	12.64	2.00	0.00	1.00	0.00
6.04	12.71	2.00	0.00	1.00	0.00	6.06	12.88	2.00	0.00	1.00	0.00
6.08	12.78	2.00	0.00	1.00	0.00	6.10	13.01	2.00	0.00	1.00	0.00
6.12	13.85	2.00	0.00	1.00	0.00	6.14	14.10	2.00	0.00	1.00	0.00
6.16	13.84	2.00	0.00	1.00	0.00	6.18	13.90	2.00	0.00	1.00	0.00
6.20	13.80	2.00	0.00	1.00	0.00	6.22	13.46	2.00	0.00	1.00	0.00
6.24	12.88	2.00	0.00	1.00	0.00	6.26	12.54	2.00	0.00	1.00	0.00
6.28	11.70	2.00	0.00	1.00	0.00	6.30	11.15	2.00	0.00	1.00	0.00
6.32	10.63	2.00	0.00	1.00	0.00	6.34	9.97	2.00	0.00	1.00	0.00
6.36	9.34	2.00	0.00	1.00	0.00	6.38	9.49	2.00	0.00	1.00	0.00
6.40	9.79	2.00	0.00	1.00	0.00	6.42	10.39	2.00	0.00	1.00	0.00
6.44	10.56	2.00	0.00	1.00	0.00	6.46	10.92	2.00	0.00	1.00	0.00
6.48	11.22	2.00	0.00	1.00	0.00	6.50	11.31	2.00	0.00	1.00	0.00
6.52	11.25	2.00	0.00	1.00	0.00	6.54	10.58	2.00	0.00	1.00	0.00
6.56	10.28	2.00	0.00	1.00	0.00	6.58	9.77	2.00	0.00	1.00	0.00
6.60	8.94	2.00	0.00	1.00	0.00	6.62	8.38	2.00	0.00	1.00	0.00
6.64	8.34	2.00	0.00	1.00	0.00	6.66	8.86	2.00	0.00	1.00	0.00
6.68	9.35	2.00	0.00	1.00	0.00	6.70	9.92	2.00	0.00	1.00	0.00
6.72	10.93	2.00	0.00	1.00	0.00	6.74	10.84	2.00	0.00	1.00	0.00
6.76	10.03	2.00	0.00	1.00	0.00	6.78	9.34	2.00	0.00	1.00	0.00
6.80	8.61	2.00	0.00	1.00	0.00	6.82	8.16	2.00	0.00	1.00	0.00
6.84	7.86	2.00	0.00	1.00	0.00	6.86	8.80	2.00	0.00	1.00	0.00
6.88	8.72	2.00	0.00	1.00	0.00	6.90	7.67	2.00	0.00	1.00	0.00
6.92	7.22	2.00	0.00	1.00	0.00	6.94	6.62	2.00	0.00	1.00	0.00
6.96	6.46	2.00	0.00	1.00	0.00	6.98	6.33	2.00	0.00	1.00	0.00
7.00	6.48	2.00	0.00	1.00	0.00	7.02	6.94	2.00	0.00	1.00	0.00
7.04	7.08	2.00	0.00	1.00	0.00	7.06	7.52	2.00	0.00	1.00	0.00
7.09	7.46	2.00	0.00	1.00	0.00	7.10	7.94	2.00	0.00	1.00	0.00
7.14	8.06	2.00	0.00	1.00	0.00	7.15	8.85	2.00	0.00	1.00	0.00
7.16	9.62	2.00	0.00	1.00	0.00	7.18	10.28	2.00	0.00	1.00	0.00
7.20	10.78	2.00	0.00	1.00	0.00	7.22	11.74	2.00	0.00	1.00	0.00
7.24	12.11	2.00	0.00	1.00	0.00	7.26	11.85	2.00	0.00	1.00	0.00
7.28	11.44	2.00	0.00	1.00	0.00	7.31	11.14	2.00	0.00	1.00	0.00
7.32	11.52	2.00	0.00	1.00	0.00	7.34	11.46	2.00	0.00	1.00	0.00
7.36	11.12	2.00	0.00	1.00	0.00	7.38	10.76	2.00	0.00	1.00	0.00
7.40	11.13	2.00	0.00	1.00	0.00	7.42	11.17	2.00	0.00	1.00	0.00
7.44	10.96	2.00	0.00	1.00	0.00	7.46	10.57	2.00	0.00	1.00	0.00
7.48	10.16	2.00	0.00	1.00	0.00	7.50	10.13	2.00	0.00	1.00	0.00
7.52	10.01	2.00	0.00	1.00	0.00	7.54	9.75	2.00	0.00	1.00	0.00
7.56	9.67	2.00	0.00	1.00	0.00	7.58	9.39	2.00	0.00	1.00	0.00
7.60	8.75	2.00	0.00	1.00	0.00	7.62	8.37	2.00	0.00	1.00	0.00
7.64	8.01	2.00	0.00	1.00	0.00	7.66	7.57	2.00	0.00	1.00	0.00
7.68	7.36	2.00	0.00	1.00	0.00	7.70	7.30	2.00	0.00	1.00	0.00
7.72	7.17	2.00	0.00	1.00	0.00	7.74	7.14	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.76	7.16	2.00	0.00	1.00	0.00	7.78	7.07	2.00	0.00	1.00	0.00
7.80	7.04	2.00	0.00	1.00	0.00	7.82	7.11	2.00	0.00	1.00	0.00
7.84	6.96	2.00	0.00	1.00	0.00	7.86	8.58	2.00	0.00	1.00	0.00
7.88	8.26	2.00	0.00	1.00	0.00	7.90	8.08	2.00	0.00	1.00	0.00
7.92	7.90	2.00	0.00	1.00	0.00	7.94	8.09	2.00	0.00	1.00	0.00
7.96	8.28	2.00	0.00	1.00	0.00	7.98	8.25	2.00	0.00	1.00	0.00
8.00	8.37	2.00	0.00	1.00	0.00	8.02	8.53	2.00	0.00	1.00	0.00
8.04	8.03	2.00	0.00	1.00	0.00	8.06	7.58	2.00	0.00	1.00	0.00
8.08	7.19	2.00	0.00	1.00	0.00	8.10	7.13	2.00	0.00	1.00	0.00
8.12	7.00	2.00	0.00	1.00	0.00	8.14	6.90	2.00	0.00	1.00	0.00
8.16	7.26	2.00	0.00	1.00	0.00	8.19	7.36	2.00	0.00	1.00	0.00
8.20	7.33	2.00	0.00	1.00	0.00	8.22	7.30	2.00	0.00	1.00	0.00
8.24	7.20	2.00	0.00	1.00	0.00	8.26	6.90	2.00	0.00	1.00	0.00
8.28	6.70	2.00	0.00	1.00	0.00	8.30	6.99	2.00	0.00	1.00	0.00
8.32	7.71	2.00	0.00	1.00	0.00	8.34	8.53	2.00	0.00	1.00	0.00
8.36	8.82	2.00	0.00	1.00	0.00	8.38	9.15	2.00	0.00	1.00	0.00
8.40	9.36	2.00	0.00	1.00	0.00	8.42	10.42	2.00	0.00	1.00	0.00
8.44	11.74	2.00	0.00	1.00	0.00	8.46	14.09	2.00	0.00	1.00	0.00
8.48	14.84	2.00	0.00	1.00	0.00	8.50	11.75	2.00	0.00	1.00	0.00
8.52	9.22	2.00	0.00	1.00	0.00	8.54	7.05	2.00	0.00	1.00	0.00
8.56	6.65	2.00	0.00	1.00	0.00	8.58	7.18	2.00	0.00	1.00	0.00
8.60	7.20	2.00	0.00	1.00	0.00	8.62	7.50	2.00	0.00	1.00	0.00
8.64	7.38	2.00	0.00	1.00	0.00	8.66	7.37	2.00	0.00	1.00	0.00
8.68	7.13	2.00	0.00	1.00	0.00	8.70	6.81	2.00	0.00	1.00	0.00
8.72	6.78	2.00	0.00	1.00	0.00	8.74	6.82	2.00	0.00	1.00	0.00
8.76	7.30	2.00	0.00	1.00	0.00	8.78	7.53	2.00	0.00	1.00	0.00
8.80	8.57	2.00	0.00	1.00	0.00	8.82	12.02	2.00	0.00	1.00	0.00
8.84	17.29	2.00	0.00	1.00	0.00	8.86	18.20	2.00	0.00	1.00	0.00
8.88	18.93	2.00	0.00	1.00	0.00	8.90	18.37	2.00	0.00	1.00	0.00
8.93	15.12	2.00	0.00	1.00	0.00	8.94	11.50	2.00	0.00	1.00	0.00
8.96	9.15	2.00	0.00	1.00	0.00	8.99	7.60	2.00	0.00	1.00	0.00
9.00	7.88	2.00	0.00	1.00	0.00	9.02	9.73	2.00	0.00	1.00	0.00
9.04	12.66	2.00	0.00	1.00	0.00	9.06	13.92	2.00	0.00	1.00	0.00
9.08	14.52	2.00	0.00	1.00	0.00	9.10	14.27	2.00	0.00	1.00	0.00
9.12	14.00	2.00	0.00	1.00	0.00	9.14	13.99	2.00	0.00	1.00	0.00
9.16	12.97	2.00	0.00	1.00	0.00	9.18	10.03	2.00	0.00	1.00	0.00
9.20	8.71	2.00	0.00	1.00	0.00	9.22	7.76	2.00	0.00	1.00	0.00
9.24	8.41	2.00	0.00	1.00	0.00	9.26	9.29	2.00	0.00	1.00	0.00
9.28	11.07	2.00	0.00	1.00	0.00	9.30	11.46	2.00	0.00	1.00	0.00
9.32	10.35	2.00	0.00	1.00	0.00	9.34	10.06	2.00	0.00	1.00	0.00
9.36	10.87	2.00	0.00	1.00	0.00	9.38	11.13	2.00	0.00	1.00	0.00
9.40	9.62	2.00	0.00	1.00	0.00	9.42	8.08	2.00	0.00	1.00	0.00
9.44	8.81	2.00	0.00	1.00	0.00	9.46	10.70	2.00	0.00	1.00	0.00
9.48	12.49	2.00	0.00	1.00	0.00	9.50	13.54	2.00	0.00	1.00	0.00
9.52	14.54	2.00	0.00	1.00	0.00	9.54	14.28	2.00	0.00	1.00	0.00
9.56	13.87	2.00	0.00	1.00	0.00	9.58	13.40	2.00	0.00	1.00	0.00
9.60	11.29	2.00	0.00	1.00	0.00	9.62	9.35	2.00	0.00	1.00	0.00
9.64	10.56	2.00	0.00	1.00	0.00	9.66	13.78	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.68	17.62	2.00	0.00	1.00	0.00	9.70	19.34	2.00	0.00	1.00	0.00
9.72	18.91	2.00	0.00	1.00	0.00	9.74	13.55	2.00	0.00	1.00	0.00
9.76	11.27	2.00	0.00	1.00	0.00	9.78	8.96	2.00	0.00	1.00	0.00
9.80	7.35	2.00	0.00	1.00	0.00	9.82	7.16	2.00	0.00	1.00	0.00
9.84	8.91	2.00	0.00	1.00	0.00	9.86	8.18	2.00	0.00	1.00	0.00
9.88	7.65	2.00	0.00	1.00	0.00	9.90	7.12	2.00	0.00	1.00	0.00
9.92	6.73	2.00	0.00	1.00	0.00	9.94	7.36	2.00	0.00	1.00	0.00
9.96	8.42	2.00	0.00	1.00	0.00	9.98	10.41	2.00	0.00	1.00	0.00
10.00	13.50	2.00	0.00	1.00	0.00	10.03	15.58	2.00	0.00	1.00	0.00
10.04	17.18	2.00	0.00	1.00	0.00	10.06	17.80	2.00	0.00	1.00	0.00
10.08	18.01	2.00	0.00	1.00	0.00	10.10	18.04	2.00	0.00	1.00	0.00
10.12	17.64	2.00	0.00	1.00	0.00	10.14	17.94	2.00	0.00	1.00	0.00
10.16	19.41	2.00	0.00	1.00	0.00	10.18	21.00	2.00	0.00	1.00	0.00
10.20	22.36	2.00	0.00	1.00	0.00	10.22	23.19	2.00	0.00	1.00	0.00
10.24	23.43	2.00	0.00	1.00	0.00	10.26	23.18	2.00	0.00	1.00	0.00
10.28	22.30	2.00	0.00	1.00	0.00	10.30	21.10	2.00	0.00	1.00	0.00
10.32	20.30	2.00	0.00	1.00	0.00	10.34	21.42	2.00	0.00	1.00	0.00
10.36	23.31	2.00	0.00	1.00	0.00	10.38	83.53	2.00	0.00	1.00	0.00
10.40	84.19	2.00	0.00	1.00	0.00	10.42	83.23	2.00	0.00	1.00	0.00
10.44	82.31	2.00	0.00	1.00	0.00	10.46	80.75	2.00	0.00	1.00	0.00
10.48	78.71	2.00	0.00	1.00	0.00	10.50	78.77	2.00	0.00	1.00	0.00
10.52	79.11	2.00	0.00	1.00	0.00	10.54	80.98	2.00	0.00	1.00	0.00
10.56	82.89	2.00	0.00	1.00	0.00	10.58	24.26	2.00	0.00	1.00	0.00
10.60	22.14	2.00	0.00	1.00	0.00	10.62	20.30	2.00	0.00	1.00	0.00
10.64	20.95	2.00	0.00	1.00	0.00	10.66	23.66	2.00	0.00	1.00	0.00
10.68	26.06	2.00	0.00	1.00	0.00	10.70	27.67	2.00	0.00	1.00	0.00
10.72	28.76	2.00	0.00	1.00	0.00	10.74	29.26	2.00	0.00	1.00	0.00
10.76	88.32	0.66	3.64	1.00	0.07	10.78	86.22	0.64	3.73	1.00	0.07
10.80	23.07	2.00	0.00	1.00	0.00	10.82	17.62	2.00	0.00	1.00	0.00
10.84	14.19	2.00	0.00	1.00	0.00	10.86	12.91	2.00	0.00	1.00	0.00
10.88	8.54	2.00	0.00	1.00	0.00	10.90	7.79	2.00	0.00	1.00	0.00
10.92	7.74	2.00	0.00	1.00	0.00	10.94	7.63	2.00	0.00	1.00	0.00
10.96	7.69	2.00	0.00	1.00	0.00	10.98	7.85	2.00	0.00	1.00	0.00
11.00	7.82	2.00	0.00	1.00	0.00	11.02	7.56	2.00	0.00	1.00	0.00
11.04	7.38	2.00	0.00	1.00	0.00	11.06	7.42	2.00	0.00	1.00	0.00
11.08	7.24	2.00	0.00	1.00	0.00	11.10	7.21	2.00	0.00	1.00	0.00
11.12	7.12	2.00	0.00	1.00	0.00	11.15	6.87	2.00	0.00	1.00	0.00
11.16	7.24	2.00	0.00	1.00	0.00	11.18	7.36	2.00	0.00	1.00	0.00
11.20	7.23	2.00	0.00	1.00	0.00	11.22	7.11	2.00	0.00	1.00	0.00
11.24	7.17	2.00	0.00	1.00	0.00	11.26	7.28	2.00	0.00	1.00	0.00
11.28	7.12	2.00	0.00	1.00	0.00	11.30	6.99	2.00	0.00	1.00	0.00
11.32	7.11	2.00	0.00	1.00	0.00	11.34	7.30	2.00	0.00	1.00	0.00
11.36	7.41	2.00	0.00	1.00	0.00	11.38	7.38	2.00	0.00	1.00	0.00
11.40	7.44	2.00	0.00	1.00	0.00	11.42	7.55	2.00	0.00	1.00	0.00
11.44	7.61	2.00	0.00	1.00	0.00	11.46	7.69	2.00	0.00	1.00	0.00
11.48	8.03	2.00	0.00	1.00	0.00	11.50	8.22	2.00	0.00	1.00	0.00
11.52	8.19	2.00	0.00	1.00	0.00	11.54	8.40	2.00	0.00	1.00	0.00
11.56	8.29	2.00	0.00	1.00	0.00	11.58	8.47	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.60	8.38	2.00	0.00	1.00	0.00	11.62	8.63	2.00	0.00	1.00	0.00
11.64	8.57	2.00	0.00	1.00	0.00	11.66	8.48	2.00	0.00	1.00	0.00
11.68	8.26	2.00	0.00	1.00	0.00	11.70	8.36	2.00	0.00	1.00	0.00
11.72	8.37	2.00	0.00	1.00	0.00	11.74	7.48	2.00	0.00	1.00	0.00
11.76	7.30	2.00	0.00	1.00	0.00	11.78	7.68	2.00	0.00	1.00	0.00
11.80	7.95	2.00	0.00	1.00	0.00	11.82	8.48	2.00	0.00	1.00	0.00
11.84	8.68	2.00	0.00	1.00	0.00	11.86	8.74	2.00	0.00	1.00	0.00
11.88	8.84	2.00	0.00	1.00	0.00	11.90	9.10	2.00	0.00	1.00	0.00
11.93	9.20	2.00	0.00	1.00	0.00	11.94	9.26	2.00	0.00	1.00	0.00
11.96	9.38	2.00	0.00	1.00	0.00	11.98	9.43	2.00	0.00	1.00	0.00
12.00	9.34	2.00	0.00	1.00	0.00	12.02	9.29	2.00	0.00	1.00	0.00
12.04	9.47	2.00	0.00	1.00	0.00	12.06	9.48	2.00	0.00	1.00	0.00
12.08	9.47	2.00	0.00	1.00	0.00	12.10	9.44	2.00	0.00	1.00	0.00
12.12	9.32	2.00	0.00	1.00	0.00	12.14	9.44	2.00	0.00	1.00	0.00
12.16	9.43	2.00	0.00	1.00	0.00	12.18	9.63	2.00	0.00	1.00	0.00
12.20	9.57	2.00	0.00	1.00	0.00	12.22	9.77	2.00	0.00	1.00	0.00
12.24	9.91	2.00	0.00	1.00	0.00	12.26	9.96	2.00	0.00	1.00	0.00
12.28	10.26	2.00	0.00	1.00	0.00	12.30	10.37	2.00	0.00	1.00	0.00
12.33	10.86	2.00	0.00	1.00	0.00	12.34	10.98	2.00	0.00	1.00	0.00
12.36	11.23	2.00	0.00	1.00	0.00	12.38	11.57	2.00	0.00	1.00	0.00
12.40	12.08	2.00	0.00	1.00	0.00	12.42	12.11	2.00	0.00	1.00	0.00
12.44	12.28	2.00	0.00	1.00	0.00	12.46	12.27	2.00	0.00	1.00	0.00
12.48	12.14	2.00	0.00	1.00	0.00	12.50	11.96	2.00	0.00	1.00	0.00
12.52	11.76	2.00	0.00	1.00	0.00	12.54	11.36	2.00	0.00	1.00	0.00
12.56	11.16	2.00	0.00	1.00	0.00	12.58	10.96	2.00	0.00	1.00	0.00
12.60	10.58	2.00	0.00	1.00	0.00	12.62	10.32	2.00	0.00	1.00	0.00
12.64	9.96	2.00	0.00	1.00	0.00	12.66	9.89	2.00	0.00	1.00	0.00
12.68	9.63	2.00	0.00	1.00	0.00	12.70	9.21	2.00	0.00	1.00	0.00
12.72	8.54	2.00	0.00	1.00	0.00	12.74	8.00	2.00	0.00	1.00	0.00
12.76	7.34	2.00	0.00	1.00	0.00	12.78	6.84	2.00	0.00	1.00	0.00
12.81	6.63	2.00	0.00	1.00	0.00	12.82	6.73	2.00	0.00	1.00	0.00
12.84	6.58	2.00	0.00	1.00	0.00	12.86	6.37	2.00	0.00	1.00	0.00
12.88	6.15	2.00	0.00	1.00	0.00	12.90	5.86	2.00	0.00	1.00	0.00
12.92	5.98	2.00	0.00	1.00	0.00	12.94	5.87	2.00	0.00	1.00	0.00
12.96	5.67	2.00	0.00	1.00	0.00	12.98	5.49	2.00	0.00	1.00	0.00
13.00	5.58	2.00	0.00	1.00	0.00	13.02	5.86	2.00	0.00	1.00	0.00
13.04	5.86	2.00	0.00	1.00	0.00	13.06	5.96	2.00	0.00	1.00	0.00
13.08	6.10	2.00	0.00	1.00	0.00	13.10	6.14	2.00	0.00	1.00	0.00
13.12	6.34	2.00	0.00	1.00	0.00	13.15	6.45	2.00	0.00	1.00	0.00
13.16	6.68	2.00	0.00	1.00	0.00	13.18	6.63	2.00	0.00	1.00	0.00
13.20	6.83	2.00	0.00	1.00	0.00	13.22	6.65	2.00	0.00	1.00	0.00
13.24	6.55	2.00	0.00	1.00	0.00	13.26	6.13	2.00	0.00	1.00	0.00
13.29	5.88	2.00	0.00	1.00	0.00	13.30	5.72	2.00	0.00	1.00	0.00
13.32	5.48	2.00	0.00	1.00	0.00	13.34	5.34	2.00	0.00	1.00	0.00
13.36	5.22	2.00	0.00	1.00	0.00	13.38	5.36	2.00	0.00	1.00	0.00
13.40	5.26	2.00	0.00	1.00	0.00	13.42	5.43	2.00	0.00	1.00	0.00
13.44	5.59	2.00	0.00	1.00	0.00	13.46	5.99	2.00	0.00	1.00	0.00
13.49	6.40	2.00	0.00	1.00	0.00	13.50	6.04	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.52	6.69	2.00	0.00	1.00	0.00	13.54	8.66	2.00	0.00	1.00	0.00
13.56	13.27	2.00	0.00	1.00	0.00	13.58	16.31	2.00	0.00	1.00	0.00
13.60	16.52	2.00	0.00	1.00	0.00	13.62	16.41	2.00	0.00	1.00	0.00
13.64	17.71	2.00	0.00	1.00	0.00	13.66	19.35	2.00	0.00	1.00	0.00
13.68	20.00	2.00	0.00	1.00	0.00	13.70	22.09	2.00	0.00	1.00	0.00
13.72	23.84	2.00	0.00	1.00	0.00	13.74	23.91	2.00	0.00	1.00	0.00
13.76	21.47	2.00	0.00	1.00	0.00	13.78	17.86	2.00	0.00	1.00	0.00
13.81	16.08	2.00	0.00	1.00	0.00	13.82	15.53	2.00	0.00	1.00	0.00
13.84	17.73	2.00	0.00	1.00	0.00	13.86	19.06	2.00	0.00	1.00	0.00
13.88	18.69	2.00	0.00	1.00	0.00	13.90	17.94	2.00	0.00	1.00	0.00
13.92	17.09	2.00	0.00	1.00	0.00	13.94	15.81	2.00	0.00	1.00	0.00
13.96	14.69	2.00	0.00	1.00	0.00	13.98	13.61	2.00	0.00	1.00	0.00
14.00	12.89	2.00	0.00	1.00	0.00	14.02	12.68	2.00	0.00	1.00	0.00
14.04	12.75	2.00	0.00	1.00	0.00	14.06	12.68	2.00	0.00	1.00	0.00
14.08	12.16	2.00	0.00	1.00	0.00	14.10	11.66	2.00	0.00	1.00	0.00
14.12	10.14	2.00	0.00	1.00	0.00	14.15	8.81	2.00	0.00	1.00	0.00
14.16	7.13	2.00	0.00	1.00	0.00	14.18	6.48	2.00	0.00	1.00	0.00
14.20	7.20	2.00	0.00	1.00	0.00	14.22	12.59	2.00	0.00	1.00	0.00
14.24	15.44	2.00	0.00	1.00	0.00	14.26	14.79	2.00	0.00	1.00	0.00
14.28	12.85	2.00	0.00	1.00	0.00	14.30	11.76	2.00	0.00	1.00	0.00
14.32	10.99	2.00	0.00	1.00	0.00	14.34	9.95	2.00	0.00	1.00	0.00
14.36	8.51	2.00	0.00	1.00	0.00	14.38	7.25	2.00	0.00	1.00	0.00
14.40	5.87	2.00	0.00	1.00	0.00	14.42	6.60	2.00	0.00	1.00	0.00
14.44	10.24	2.00	0.00	1.00	0.00	14.46	14.41	2.00	0.00	1.00	0.00
14.48	15.24	2.00	0.00	1.00	0.00	14.50	13.40	2.00	0.00	1.00	0.00
14.52	12.02	2.00	0.00	1.00	0.00	14.54	11.06	2.00	0.00	1.00	0.00
14.56	9.51	2.00	0.00	1.00	0.00	14.58	8.00	2.00	0.00	1.00	0.00
14.60	6.54	2.00	0.00	1.00	0.00	14.62	5.79	2.00	0.00	1.00	0.00
14.64	6.38	2.00	0.00	1.00	0.00	14.66	11.25	2.00	0.00	1.00	0.00
14.68	16.82	2.00	0.00	1.00	0.00	14.70	79.55	2.00	0.00	1.00	0.00
14.72	80.22	2.00	0.00	1.00	0.00	14.74	80.33	2.00	0.00	1.00	0.00
14.76	80.17	0.63	4.00	1.00	0.08	14.78	78.73	0.62	4.07	1.00	0.08
14.80	17.52	2.00	0.00	1.00	0.00	14.82	17.30	2.00	0.00	1.00	0.00
14.85	23.63	2.00	0.00	1.00	0.00	14.86	83.93	0.66	3.83	1.00	0.04
14.88	83.60	0.65	3.84	1.00	0.08	14.90	82.64	0.65	3.89	1.00	0.08
14.92	81.94	0.64	3.92	1.00	0.08	14.94	79.00	2.00	0.00	1.00	0.00
14.97	76.65	2.00	0.00	1.00	0.00	14.98	20.19	2.00	0.00	1.00	0.00
15.00	23.02	2.00	0.00	1.00	0.00	15.02	24.96	2.00	0.00	1.00	0.00
15.04	26.25	2.00	0.00	1.00	0.00	15.06	24.75	2.00	0.00	1.00	0.00
15.08	18.66	2.00	0.00	1.00	0.00	15.10	13.71	2.00	0.00	1.00	0.00
15.13	9.60	2.00	0.00	1.00	0.00	15.14	7.56	2.00	0.00	1.00	0.00
15.16	7.47	2.00	0.00	1.00	0.00	15.18	8.92	2.00	0.00	1.00	0.00
15.20	9.50	2.00	0.00	1.00	0.00	15.22	9.30	2.00	0.00	1.00	0.00
15.24	8.57	2.00	0.00	1.00	0.00	15.26	7.98	2.00	0.00	1.00	0.00
15.28	7.63	2.00	0.00	1.00	0.00	15.30	7.23	2.00	0.00	1.00	0.00
15.32	7.28	2.00	0.00	1.00	0.00	15.34	7.74	2.00	0.00	1.00	0.00
15.36	7.84	2.00	0.00	1.00	0.00	15.38	7.29	2.00	0.00	1.00	0.00
15.40	7.83	2.00	0.00	1.00	0.00	15.42	8.98	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.44	8.92	2.00	0.00	1.00	0.00	15.46	8.97	2.00	0.00	1.00	0.00
15.48	12.97	2.00	0.00	1.00	0.00	15.50	15.47	2.00	0.00	1.00	0.00
15.52	14.08	2.00	0.00	1.00	0.00	15.54	11.57	2.00	0.00	1.00	0.00
15.56	12.65	2.00	0.00	1.00	0.00	15.58	16.65	2.00	0.00	1.00	0.00
15.60	17.38	2.00	0.00	1.00	0.00						

Total estimated settlement: 0.66

Abbreviations

$Q_{tn,cs}$: Equivalent clean sand normalized cone resistance
FS: Factor of safety against liquefaction
e_v (%): Post-liquefaction volumentric strain
DF: e_v depth weighting factor
Settlement: Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.14	2.29	12.48	28.61	3.41	0.05	35.07
0.04	0.22	3.77	11.48	43.23	3.35	0.05	27.97
0.06	0.31	5.21	9.49	49.44	3.22	0.06	25.29
0.08	0.41	6.90	8.17	56.37	3.12	0.06	24.66
0.11	0.47	7.91	7.75	61.29	3.09	0.06	20.16
0.12	0.47	7.98	8.58	68.46	3.15	0.06	18.53
0.14	0.45	7.70	9.74	74.99	3.23	0.06	15.14
0.16	0.42	7.10	11.42	81.07	3.34	0.06	12.09
0.18	0.39	6.60	12.65	83.44	3.42	0.06	9.90
0.20	0.35	5.97	14.07	84.05	3.50	0.06	8.01
0.22	0.33	5.53	15.06	83.28	3.55	0.06	6.70
0.24	0.31	5.14	15.93	81.84	3.60	0.06	5.68
0.26	0.29	4.90	16.29	79.83	3.61	0.06	4.98
0.28	0.28	4.60	16.83	77.49	3.64	0.06	4.33
0.30	0.27	4.56	16.55	75.40	3.63	0.05	3.99
0.32	0.29	4.86	15.41	74.89	3.57	0.06	3.99
0.34	0.33	5.54	13.54	74.98	3.47	0.06	4.27
0.36	0.38	6.37	11.99	76.40	3.38	0.06	4.63
0.38	0.43	7.23	10.82	78.22	3.31	0.06	4.97
0.40	0.50	8.31	9.71	80.70	3.23	0.06	5.42
0.42	0.56	9.47	8.84	83.66	3.17	0.06	5.87
0.44	0.63	10.60	8.25	87.49	3.13	0.06	6.26
0.46	0.68	11.43	8.11	92.77	3.11	0.06	6.45
0.48	0.69	11.65	8.45	98.45	3.14	0.06	6.28
0.50	0.67	11.26	9.21	103.68	3.20	0.06	5.81
0.52	0.63	10.55	10.21	107.69	3.27	0.06	5.22
0.54	0.60	9.99	11.09	110.85	3.32	0.06	4.75
0.56	0.59	9.79	11.56	113.20	3.35	0.06	4.48
0.58	0.59	9.95	11.56	115.02	3.35	0.06	4.38
0.60	0.61	10.26	11.26	115.62	3.34	0.06	4.36
0.62	0.64	10.70	10.77	115.22	3.30	0.06	4.39
0.64	0.66	10.98	10.36	113.79	3.28	0.06	4.35
0.66	0.68	11.35	9.89	112.30	3.25	0.06	4.36
0.68	0.68	11.45	9.70	111.08	3.23	0.06	4.26
0.70	0.69	11.52	9.53	109.87	3.22	0.06	4.16
0.72	0.69	11.48	9.48	108.87	3.22	0.06	4.02
0.74	0.70	11.76	9.20	108.24	3.20	0.06	4.00
0.76	0.72	12.08	8.95	108.21	3.18	0.06	4.00
0.78	0.75	12.53	8.67	108.62	3.16	0.06	4.04
0.80	0.78	13.00	8.41	109.37	3.14	0.06	4.08
0.82	0.82	13.67	8.12	111.03	3.12	0.07	4.18
0.84	0.88	14.68	7.71	113.23	3.08	0.07	4.37
0.86	0.95	15.84	7.33	116.06	3.05	0.07	4.61
0.88	1.03	17.20	6.94	119.39	3.02	0.07	4.88
0.90	1.10	18.42	6.72	123.75	3.00	0.07	5.10
0.92	1.17	19.69	6.52	128.31	2.98	0.07	5.33
0.96	1.22	20.53	6.42	131.69	2.97	0.07	5.31
0.96	1.25	20.89	6.48	135.31	2.98	0.07	5.40

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	1.22	20.54	6.78	139.25	3.00	0.07	5.19
1.00	1.19	19.93	7.18	143.16	3.04	0.07	4.93
1.02	1.14	19.15	7.59	145.40	3.07	0.07	4.64
1.04	1.09	18.29	7.97	145.78	3.10	0.07	4.34
1.06	1.04	17.32	8.38	145.15	3.14	0.07	4.03
1.08	0.98	16.39	8.75	143.45	3.16	0.07	3.73
1.10	0.95	15.77	8.95	141.20	3.18	0.07	3.52
1.12	0.93	15.41	9.00	138.65	3.18	0.07	3.38
1.14	0.92	15.32	8.85	135.59	3.17	0.07	3.30
1.16	0.93	15.49	8.54	132.29	3.15	0.07	3.27
1.18	0.96	15.99	8.07	129.00	3.11	0.07	3.32
1.21	1.00	16.71	7.56	126.43	3.07	0.07	3.38
1.22	1.05	17.47	7.14	124.72	3.03	0.07	3.50
1.24	1.10	18.34	6.73	123.52	3.00	0.07	3.61
1.26	1.14	19.06	6.48	123.43	2.98	0.07	3.69
1.28	1.18	19.70	6.33	124.82	2.96	0.07	3.76
1.30	1.20	20.10	6.37	128.07	2.97	0.07	3.77
1.32	1.21	20.24	6.55	132.62	2.98	0.07	3.73
1.34	1.21	20.20	6.79	137.23	3.00	0.07	3.67
1.36	1.20	19.97	7.08	141.45	3.03	0.07	3.57
1.38	1.19	19.91	7.27	144.82	3.05	0.07	3.51
1.40	1.19	19.90	7.38	146.84	3.06	0.07	3.45
1.42	1.20	19.96	7.39	147.55	3.06	0.07	3.41
1.44	1.20	20.02	7.33	146.76	3.05	0.07	3.37
1.46	1.21	20.20	7.22	145.94	3.04	0.07	3.35
1.48	1.22	20.37	7.12	145.14	3.03	0.07	3.33
1.50	1.23	20.53	7.06	144.93	3.03	0.07	3.31
1.52	1.25	20.76	6.98	144.96	3.02	0.07	3.30
1.54	1.25	20.84	7.00	145.86	3.02	0.07	3.27
1.56	1.24	20.59	7.14	147.01	3.03	0.07	3.19
1.58	1.21	20.12	7.35	147.85	3.05	0.07	3.07
1.60	1.18	19.55	7.53	147.26	3.07	0.07	2.94
1.62	1.16	19.21	7.59	145.74	3.07	0.07	2.86
1.64	1.15	19.08	7.52	143.56	3.07	0.07	2.80
1.66	1.18	19.54	7.26	141.74	3.04	0.07	2.83
1.68	1.23	20.33	6.87	139.67	3.01	0.07	2.91
1.70	1.28	21.18	6.46	136.79	2.97	0.07	2.99
1.72	1.32	21.90	6.11	133.84	2.94	0.08	3.06
1.74	1.34	22.32	5.88	131.31	2.92	0.08	3.08
1.76	1.35	22.36	5.87	131.17	2.92	0.08	3.05
1.78	1.33	22.12	5.97	131.97	2.93	0.08	2.98
1.80	1.31	21.68	6.17	133.65	2.95	0.08	2.89
1.82	1.27	20.99	6.52	136.74	2.98	0.07	2.76
1.84	1.23	20.34	6.89	140.21	3.01	0.07	2.65
1.86	1.19	19.73	7.30	144.00	3.05	0.07	2.54
1.88	1.16	19.24	7.58	145.76	3.07	0.07	2.45
1.90	1.14	18.88	7.73	145.90	3.08	0.07	2.38
1.92	1.14	18.74	7.70	144.26	3.08	0.07	2.33

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.96	1.13	18.66	7.63	142.46	3.08	0.07	2.28
1.96	1.11	18.23	7.73	140.83	3.08	0.07	2.22
1.98	1.06	17.46	7.99	139.52	3.11	0.07	2.11
2.00	1.01	16.65	8.31	138.38	3.13	0.07	1.99
2.02	0.98	16.01	8.65	138.39	3.16	0.07	1.89
2.04	0.95	15.46	8.99	138.98	3.18	0.07	1.81
2.06	0.90	14.77	9.40	138.87	3.21	0.07	1.71
2.08	0.86	13.99	9.77	136.68	3.24	0.07	1.60
2.10	0.82	13.30	9.98	132.79	3.25	0.07	1.51
2.12	0.80	12.94	9.93	128.40	3.25	0.06	1.45
2.14	0.80	12.90	9.61	123.96	3.23	0.06	1.44
2.16	0.83	13.40	8.95	119.93	3.18	0.07	1.48
2.18	0.89	14.40	8.01	115.44	3.11	0.07	1.58
2.20	0.96	15.68	7.05	110.61	3.03	0.07	1.70
2.23	1.04	17.04	6.22	106.01	2.95	0.07	1.82
2.24	1.08	17.77	5.76	102.31	2.91	0.07	1.89
2.26	1.11	18.27	5.44	99.34	2.87	0.08	1.93
2.28	1.12	18.36	5.38	98.85	2.87	0.08	1.92
2.30	1.13	18.50	5.40	99.83	2.87	0.08	1.92
2.32	1.11	18.22	5.74	104.54	2.90	0.07	1.87
2.34	1.08	17.58	6.29	110.49	2.96	0.07	1.79
2.36	1.03	16.87	6.96	117.34	3.02	0.07	1.70
2.38	1.00	16.29	7.48	121.74	3.06	0.07	1.63
2.40	0.98	15.97	7.80	124.58	3.09	0.07	1.59
2.42	0.99	16.12	7.80	125.70	3.09	0.07	1.59
2.44	1.01	16.42	7.68	126.06	3.08	0.07	1.60
2.46	1.04	16.91	7.37	124.68	3.05	0.07	1.64
2.48	1.06	17.21	7.09	121.98	3.03	0.07	1.65
2.50	1.08	17.66	6.78	119.71	3.00	0.07	1.68
2.52	1.11	18.07	6.55	118.30	2.98	0.07	1.72
2.54	1.13	18.40	6.41	118.03	2.97	0.07	1.74
2.56	1.13	18.48	6.40	118.25	2.97	0.07	1.74
2.58	1.12	18.26	6.52	119.07	2.98	0.07	1.72
2.60	1.09	17.82	6.80	121.27	3.01	0.07	1.67
2.62	1.07	17.45	7.09	123.71	3.03	0.07	1.63
2.64	1.05	17.10	7.38	126.15	3.06	0.07	1.59
2.66	1.03	16.78	7.63	127.92	3.08	0.07	1.55
2.68	1.01	16.28	7.92	128.98	3.10	0.07	1.50
2.70	0.98	15.83	8.15	128.99	3.12	0.07	1.46
2.72	0.95	15.29	8.37	128.00	3.13	0.07	1.40
2.74	0.92	14.82	8.51	126.17	3.15	0.07	1.35
2.76	0.89	14.27	8.68	123.86	3.16	0.07	1.30
2.78	0.87	13.88	8.71	120.92	3.16	0.06	1.26
2.80	0.84	13.50	8.70	117.43	3.16	0.06	1.22
2.82	0.83	13.26	8.55	113.32	3.15	0.06	1.19
2.84	0.82	13.03	8.35	108.85	3.13	0.06	1.17
2.86	0.81	12.83	8.13	104.35	3.12	0.06	1.15
2.88	0.80	12.76	7.72	98.46	3.08	0.06	1.14

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.91	0.80	12.77	7.28	92.95	3.05	0.06	1.13
2.92	0.79	12.58	6.98	87.77	3.02	0.06	1.12
2.94	0.76	12.11	7.04	85.30	3.03	0.06	1.07
2.96	0.72	11.41	7.34	83.77	3.05	0.06	1.01
2.98	0.68	10.71	7.76	83.13	3.09	0.06	0.94
3.00	0.64	10.06	8.24	82.85	3.12	0.06	0.88
3.02	0.61	9.53	8.66	82.52	3.16	0.06	0.83
3.04	0.60	9.37	8.68	81.28	3.16	0.06	0.82
3.06	0.61	9.41	8.46	79.59	3.14	0.06	0.82
3.08	0.61	9.52	8.15	77.50	3.12	0.06	0.82
3.10	0.62	9.57	7.92	75.79	3.10	0.06	0.83
3.12	0.62	9.63	7.69	74.07	3.08	0.06	0.83
3.14	0.63	9.80	7.30	71.57	3.05	0.06	0.84
3.16	0.66	10.22	6.75	68.98	3.00	0.06	0.88
3.18	0.69	10.82	6.17	66.75	2.95	0.06	0.92
3.21	0.75	11.72	5.62	65.88	2.89	0.07	1.00
3.22	0.80	12.70	5.15	65.44	2.84	0.07	1.08
3.24	0.86	13.73	4.76	65.41	2.80	0.07	1.16
3.26	0.94	15.06	4.36	65.62	2.75	0.07	1.27
3.28	1.04	16.73	4.00	66.94	2.70	0.08	1.41
3.30	1.17	18.87	3.72	70.26	2.66	0.08	1.59
3.32	1.27	20.67	3.62	74.88	2.65	0.08	1.73
3.34	1.36	22.06	3.67	81.05	2.65	0.08	1.85
3.36	1.39	22.58	3.93	88.75	2.69	0.08	1.88
3.38	1.39	22.65	4.27	96.81	2.74	0.08	1.88
3.40	1.37	22.21	4.80	106.59	2.80	0.08	1.84
3.42	1.32	21.44	5.40	115.78	2.87	0.08	1.77
3.44	1.28	20.69	5.98	123.70	2.93	0.07	1.70
3.46	1.22	19.79	6.51	128.89	2.98	0.07	1.63
3.48	1.20	19.39	6.77	131.21	3.00	0.07	1.59
3.50	1.18	18.96	6.97	132.19	3.02	0.07	1.55
3.52	1.16	18.74	7.02	131.56	3.02	0.07	1.52
3.54	1.15	18.43	7.05	129.88	3.03	0.07	1.49
3.56	1.13	18.15	7.02	127.42	3.02	0.07	1.47
3.58	1.12	17.99	6.92	124.56	3.02	0.07	1.45
3.60	1.12	17.97	6.79	121.94	3.00	0.07	1.44
3.62	1.13	18.09	6.59	119.26	2.99	0.07	1.45
3.64	1.15	18.39	6.29	115.76	2.96	0.07	1.47
3.66	1.13	18.18	6.18	112.31	2.95	0.07	1.45
3.68	1.09	17.50	6.29	110.00	2.96	0.07	1.39
3.70	1.02	16.32	6.71	109.51	3.00	0.07	1.29
3.72	0.94	14.95	7.36	110.10	3.05	0.07	1.18
3.74	0.87	13.64	8.11	110.56	3.11	0.06	1.07
3.76	0.80	12.45	8.91	110.94	3.18	0.06	0.98
3.78	0.75	11.67	9.49	110.81	3.22	0.06	0.91
3.80	0.73	11.32	9.71	109.91	3.23	0.06	0.88
3.82	0.73	11.31	9.54	107.89	3.22	0.06	0.88
3.84	0.74	11.44	9.16	104.89	3.19	0.06	0.89

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	0.74	11.36	8.99	102.12	3.18	0.06	0.88
3.88	0.72	11.03	8.88	97.91	3.17	0.06	0.85
3.90	0.68	10.48	8.99	94.17	3.18	0.06	0.81
3.92	0.65	9.81	9.17	89.91	3.19	0.06	0.75
3.94	0.61	9.25	9.46	87.46	3.21	0.06	0.71
3.96	0.58	8.67	9.76	84.60	3.24	0.06	0.66
3.98	0.56	8.32	9.87	82.17	3.24	0.06	0.63
4.00	0.54	8.03	9.86	79.22	3.24	0.06	0.61
4.02	0.54	8.06	9.41	75.85	3.21	0.06	0.61
4.05	0.56	8.27	8.69	71.85	3.16	0.06	0.62
4.06	0.58	8.71	7.82	68.18	3.09	0.06	0.66
4.08	0.63	9.42	6.95	65.49	3.02	0.06	0.71
4.10	0.67	10.23	6.22	63.60	2.95	0.06	0.77
4.12	0.73	11.18	5.64	63.05	2.89	0.06	0.84
4.14	0.77	11.93	5.30	63.31	2.86	0.07	0.89
4.16	0.81	12.61	5.07	63.98	2.83	0.07	0.94
4.18	0.85	13.25	4.95	65.63	2.82	0.07	0.99
4.20	0.88	13.71	4.98	68.20	2.82	0.07	1.02
4.22	0.90	14.00	5.09	71.25	2.84	0.07	1.04
4.24	0.89	13.93	5.35	74.56	2.86	0.07	1.03
4.26	0.88	13.66	5.69	77.75	2.90	0.07	1.01
4.28	0.85	13.22	6.14	81.23	2.94	0.06	0.97
4.30	0.82	12.64	6.62	83.67	2.99	0.06	0.93
4.32	0.79	12.09	7.14	86.38	3.04	0.06	0.88
4.34	0.76	11.64	7.59	88.32	3.07	0.06	0.85
4.36	0.74	11.33	7.84	88.91	3.09	0.06	0.83
4.38	0.73	11.13	7.91	88.04	3.10	0.06	0.81
4.40	0.71	10.84	7.95	86.19	3.10	0.06	0.79
4.42	0.70	10.55	7.93	83.69	3.10	0.06	0.76
4.44	0.68	10.29	7.84	80.66	3.09	0.06	0.74
4.46	0.67	10.15	7.60	77.17	3.07	0.06	0.73
4.48	0.67	10.07	7.37	74.15	3.05	0.06	0.72
4.50	0.66	9.95	7.23	71.95	3.04	0.06	0.71
4.52	0.66	9.88	7.20	71.18	3.04	0.06	0.71
4.54	0.66	9.94	7.10	70.59	3.03	0.06	0.71
4.56	0.68	10.15	6.85	69.55	3.01	0.06	0.73
4.58	0.69	10.32	6.62	68.34	2.99	0.06	0.74
4.60	0.69	10.30	6.61	68.13	2.99	0.06	0.74
4.62	0.69	10.34	6.61	68.30	2.99	0.06	0.74
4.64	0.72	10.69	6.34	67.78	2.96	0.06	0.76
4.66	0.79	11.82	5.61	66.31	2.89	0.06	0.85
4.68	0.89	13.21	4.92	64.96	2.82	0.07	0.97
4.70	0.97	14.30	4.56	65.20	2.77	0.07	1.06
4.72	1.00	14.83	4.47	66.33	2.76	0.07	1.10
4.74	1.04	15.40	4.40	67.72	2.75	0.07	1.14
4.76	1.09	16.05	4.40	70.54	2.75	0.07	1.19
4.78	1.15	17.03	4.28	72.94	2.74	0.07	1.26
4.80	1.17	17.28	4.37	75.51	2.75	0.08	1.28

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	1.20	17.78	4.30	76.44	2.74	0.08	1.32
4.84	1.23	18.08	4.35	78.60	2.75	0.08	1.34
4.86	1.23	18.19	4.39	79.91	2.75	0.08	1.35
4.88	1.23	18.21	4.59	83.54	2.78	0.08	1.34
4.90	1.16	17.25	5.16	88.93	2.84	0.07	1.25
4.93	1.09	16.31	5.90	96.25	2.92	0.07	1.17
4.94	0.98	14.57	6.97	101.53	3.02	0.06	1.04
4.96	0.90	13.18	8.00	105.46	3.11	0.06	0.94
4.98	0.82	11.83	9.15	108.30	3.19	0.06	0.85
5.00	0.75	10.70	10.16	108.67	3.26	0.06	0.76
5.02	0.71	9.95	10.69	106.39	3.30	0.06	0.71
5.04	0.69	9.63	10.52	101.31	3.29	0.06	0.69
5.06	0.71	9.95	9.57	95.20	3.22	0.06	0.71
5.08	0.79	11.25	7.89	88.77	3.10	0.06	0.80
5.10	0.95	13.73	6.05	83.05	2.94	0.06	0.98
5.12	1.24	17.68	4.30	75.98	2.74	0.08	1.31
5.14	1.48	20.82	3.50	72.78	2.63	0.08	1.57
5.16	1.59	22.38	3.27	73.16	2.59	0.08	0.64
5.18	1.48	20.94	3.77	78.99	2.67	0.08	1.57
5.20	1.33	18.99	4.42	83.90	2.76	0.08	1.40
5.22	1.22	17.47	5.01	87.58	2.83	0.07	1.27
5.24	1.22	17.44	5.12	89.31	2.84	0.07	1.27
5.26	1.28	18.23	5.03	91.71	2.83	0.08	1.33
5.29	1.38	19.61	4.73	92.78	2.79	0.08	1.43
5.30	1.47	20.90	4.52	94.48	2.77	0.08	1.54
5.32	1.55	21.93	4.44	97.27	2.76	0.08	1.61
5.34	1.57	22.32	4.56	101.83	2.77	0.08	1.64
5.36	1.58	22.37	4.70	105.23	2.79	0.08	1.64
5.38	1.58	22.33	4.77	106.46	2.80	0.08	1.63
5.40	1.59	22.45	4.73	106.11	2.79	0.08	1.64
5.42	1.61	22.73	4.69	106.49	2.79	0.08	1.66
5.44	1.61	22.65	4.77	108.00	2.80	0.08	1.65
5.46	1.60	22.46	4.85	108.90	2.81	0.08	1.64
5.48	1.60	22.40	4.81	107.62	2.80	0.08	1.63
5.50	1.68	23.40	4.49	104.97	2.76	0.08	1.72
5.52	1.82	25.22	4.07	102.78	2.71	0.09	1.87
5.54	2.01	27.65	3.74	103.43	2.66	0.09	2.06
5.56	2.13	29.33	3.66	107.21	2.65	0.09	2.19
5.58	2.08	28.62	3.92	112.06	2.69	0.09	2.12
5.60	1.88	26.08	4.45	115.95	2.76	0.09	1.91
5.62	1.64	22.79	5.19	118.30	2.85	0.08	1.65
5.64	1.56	21.62	5.30	114.54	2.86	0.08	1.56
5.66	1.56	21.43	5.03	107.88	2.83	0.08	1.55
5.68	1.55	21.20	4.84	102.60	2.81	0.08	1.54
5.70	1.44	19.60	5.29	103.60	2.86	0.08	1.42
5.72	1.26	17.08	6.23	106.43	2.95	0.07	1.22
5.74	1.10	14.69	7.22	106.06	3.04	0.07	1.05
5.76	0.99	13.10	7.98	104.63	3.10	0.06	0.94

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	0.95	12.48	8.21	102.54	3.12	0.06	0.89
5.80	0.97	12.68	7.90	100.18	3.10	0.06	0.91
5.82	1.02	13.42	7.24	97.13	3.04	0.06	0.96
5.84	1.08	14.32	6.61	94.71	2.99	0.07	1.02
5.86	1.17	15.48	5.89	91.20	2.92	0.07	1.11
5.88	1.21	15.94	5.63	89.82	2.89	0.07	1.14
5.90	1.22	16.09	5.56	89.38	2.89	0.07	1.16
5.93	1.18	15.52	5.92	91.90	2.92	0.07	1.11
5.94	1.15	15.14	6.22	94.23	2.95	0.07	1.08
5.96	1.12	14.67	6.63	97.25	2.99	0.07	1.05
5.98	1.09	14.17	7.08	100.26	3.03	0.07	1.01
6.01	1.07	13.76	7.44	102.47	3.06	0.06	0.98
6.02	1.06	13.60	7.64	103.90	3.08	0.06	0.97
6.04	1.06	13.66	7.67	104.82	3.08	0.06	0.98
6.06	1.07	13.68	7.70	105.38	3.08	0.06	0.98
6.08	1.08	13.79	7.71	106.32	3.08	0.06	0.98
6.10	1.11	14.16	7.48	105.96	3.06	0.06	1.01
6.12	1.14	14.66	7.18	105.29	3.04	0.07	1.05
6.14	1.17	14.96	7.01	104.78	3.02	0.07	1.07
6.16	1.17	14.95	7.00	104.55	3.02	0.07	1.07
6.18	1.16	14.80	7.07	104.68	3.03	0.07	1.06
6.20	1.15	14.60	7.16	104.59	3.04	0.07	1.04
6.22	1.12	14.16	7.46	105.60	3.06	0.07	1.01
6.24	1.09	13.64	7.88	107.45	3.10	0.06	0.97
6.26	1.04	13.00	8.38	108.91	3.14	0.06	0.93
6.28	1.00	12.38	8.83	109.26	3.17	0.06	0.88
6.30	0.95	11.68	9.33	108.93	3.21	0.06	0.83
6.32	0.91	10.98	9.87	108.43	3.24	0.06	0.78
6.34	0.86	10.26	10.47	107.40	3.28	0.06	0.73
6.36	0.82	9.82	10.72	105.23	3.30	0.06	0.70
6.38	0.82	9.75	10.51	102.54	3.29	0.06	0.70
6.40	0.85	10.17	9.80	99.65	3.24	0.06	0.73
6.42	0.89	10.59	9.15	96.93	3.19	0.06	0.76
6.44	0.92	11.02	8.58	94.52	3.15	0.06	0.79
6.46	0.94	11.31	8.16	92.26	3.12	0.06	0.81
6.48	0.96	11.57	7.81	90.40	3.09	0.06	0.83
6.50	0.97	11.64	7.62	88.69	3.08	0.06	0.83
6.52	0.95	11.35	7.77	88.23	3.09	0.06	0.81
6.54	0.92	10.91	8.12	88.63	3.12	0.06	0.78
6.56	0.88	10.32	8.65	89.28	3.16	0.06	0.74
6.58	0.83	9.67	9.32	90.08	3.20	0.06	0.69
6.60	0.78	8.95	10.14	90.73	3.26	0.06	0.64
6.62	0.74	8.41	10.86	91.42	3.31	0.06	0.60
6.64	0.74	8.40	10.88	91.46	3.31	0.06	0.60
6.66	0.77	8.79	10.25	90.01	3.27	0.06	0.63
6.68	0.82	9.39	9.27	87.03	3.20	0.06	0.67
6.70	0.88	10.18	8.23	83.80	3.12	0.06	0.73
6.72	0.93	10.76	7.58	81.58	3.07	0.06	0.77

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	0.93	10.79	7.39	79.73	3.06	0.06	0.77
6.76	0.89	10.15	7.73	78.49	3.08	0.06	0.73
6.78	0.82	9.26	8.38	77.63	3.14	0.06	0.66
6.80	0.77	8.52	9.19	78.35	3.20	0.06	0.61
6.82	0.72	7.95	9.97	79.24	3.25	0.06	0.57
6.84	0.74	8.10	9.76	79.01	3.24	0.06	0.58
6.86	0.76	8.34	9.40	78.47	3.21	0.06	0.60
6.88	0.76	8.30	9.30	77.18	3.20	0.06	0.59
6.90	0.71	7.66	9.95	76.21	3.25	0.06	0.55
6.92	0.65	6.86	10.79	74.00	3.30	0.06	0.49
6.94	0.61	6.40	11.27	72.13	3.34	0.06	0.46
6.96	0.59	6.07	11.64	70.60	3.36	0.06	0.43
6.98	0.59	6.01	11.58	69.65	3.35	0.06	0.43
7.00	0.60	6.19	11.07	68.54	3.32	0.06	0.44
7.02	0.62	6.48	10.42	67.45	3.28	0.06	0.46
7.04	0.66	6.87	9.67	66.40	3.23	0.06	0.49
7.06	0.67	7.06	9.32	65.84	3.21	0.06	0.50
7.09	0.70	7.39	8.90	65.77	3.17	0.06	0.53
7.10	0.72	7.62	8.65	65.94	3.16	0.06	0.54
7.14	0.76	8.16	8.12	66.27	3.12	0.06	0.58
7.15	0.82	8.83	7.59	67.01	3.07	0.06	0.63
7.16	0.89	9.71	7.00	68.02	3.02	0.06	0.69
7.18	0.95	10.48	6.54	68.54	2.98	0.06	0.75
7.20	1.01	11.28	6.10	68.86	2.94	0.06	0.81
7.22	1.07	11.93	5.82	69.35	2.91	0.07	0.85
7.24	1.09	12.21	5.75	70.15	2.90	0.07	0.87
7.26	1.08	12.08	5.92	71.49	2.92	0.07	0.86
7.28	1.06	11.78	6.22	73.23	2.95	0.06	0.84
7.31	1.06	11.79	6.36	74.95	2.96	0.06	0.84
7.32	1.07	11.85	6.45	76.41	2.97	0.06	0.85
7.34	1.07	11.79	6.59	77.71	2.99	0.06	0.84
7.36	1.04	11.43	6.89	78.69	3.01	0.06	0.82
7.38	1.03	11.27	7.05	79.39	3.03	0.06	0.80
7.40	1.03	11.21	7.07	79.22	3.03	0.06	0.80
7.42	1.03	11.16	7.15	79.83	3.04	0.06	0.80
7.44	1.00	10.81	7.53	81.48	3.07	0.06	0.77
7.46	0.96	10.34	8.12	83.96	3.12	0.06	0.74
7.48	0.94	9.99	8.59	85.78	3.15	0.06	0.71
7.50	0.92	9.77	8.85	86.54	3.17	0.06	0.70
7.52	0.91	9.64	8.99	86.70	3.18	0.06	0.69
7.54	0.90	9.48	9.12	86.48	3.19	0.06	0.68
7.56	0.88	9.23	9.31	85.94	3.20	0.06	0.66
7.58	0.85	8.86	9.63	85.30	3.23	0.06	0.63
7.60	0.82	8.37	10.08	84.39	3.26	0.06	0.60
7.62	0.78	7.86	10.57	83.05	3.29	0.06	0.56
7.64	0.74	7.42	10.94	81.11	3.31	0.06	0.53
7.66	0.71	7.05	11.21	78.99	3.33	0.06	0.50
7.68	0.69	6.80	11.29	76.73	3.34	0.06	0.49

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	0.68	6.67	11.17	74.45	3.33	0.06	0.48
7.72	0.68	6.60	10.91	72.04	3.31	0.06	0.47
7.74	0.68	6.57	10.59	69.59	3.29	0.06	0.47
7.76	0.68	6.56	10.26	67.26	3.27	0.06	0.47
7.78	0.68	6.54	9.97	65.15	3.25	0.06	0.47
7.80	0.68	6.53	9.77	63.77	3.24	0.06	0.47
7.82	0.68	6.48	9.71	62.96	3.23	0.06	0.46
7.84	0.72	7.03	8.81	61.93	3.17	0.06	0.50
7.86	0.76	7.44	8.31	61.82	3.13	0.06	0.53
7.88	0.79	7.85	7.88	61.87	3.10	0.06	0.56
7.90	0.78	7.64	8.24	62.91	3.12	0.06	0.55
7.92	0.78	7.63	8.22	62.69	3.12	0.06	0.54
7.94	0.79	7.76	8.04	62.40	3.11	0.06	0.55
7.96	0.80	7.91	7.86	62.17	3.09	0.06	0.57
7.98	0.81	8.03	7.74	62.13	3.09	0.06	0.57
8.00	0.82	8.12	7.63	61.91	3.08	0.06	0.58
8.02	0.81	7.99	7.71	61.56	3.08	0.06	0.57
8.04	0.79	7.65	8.04	61.54	3.11	0.06	0.55
8.06	0.74	7.12	8.59	61.19	3.15	0.06	0.51
8.08	0.72	6.81	8.88	60.43	3.17	0.06	0.49
8.10	0.70	6.61	8.92	58.99	3.18	0.06	0.47
8.12	0.70	6.52	8.78	57.30	3.17	0.06	0.47
8.14	0.70	6.59	8.51	56.04	3.15	0.06	0.47
8.16	0.72	6.73	8.25	55.53	3.13	0.06	0.48
8.19	0.73	6.88	8.08	55.57	3.11	0.06	0.49
8.20	0.73	6.89	8.11	55.90	3.11	0.06	0.49
8.22	0.73	6.81	8.27	56.32	3.13	0.06	0.49
8.24	0.71	6.63	8.61	57.04	3.15	0.06	0.47
8.26	0.69	6.38	9.05	57.73	3.19	0.06	0.46
8.28	0.68	6.27	9.28	58.23	3.20	0.06	0.45
8.30	0.71	6.56	8.95	58.70	3.18	0.06	0.47
8.32	0.77	7.24	8.16	59.05	3.12	0.06	0.52
8.34	0.83	7.89	7.48	59.03	3.06	0.06	0.56
8.36	0.87	8.36	7.03	58.76	3.03	0.06	0.60
8.38	0.89	8.60	6.85	58.88	3.01	0.06	0.61
8.40	0.94	9.16	6.47	59.25	2.97	0.06	0.65
8.42	1.02	10.05	5.96	59.95	2.93	0.06	0.72
8.44	1.16	11.63	5.29	61.55	2.86	0.07	0.83
8.46	1.29	13.01	4.99	64.89	2.82	0.07	0.93
8.48	1.28	12.90	5.34	68.83	2.86	0.07	0.92
8.50	1.12	11.13	6.37	70.88	2.97	0.06	0.80
8.52	0.89	8.42	8.24	69.44	3.13	0.06	0.60
8.54	0.74	6.74	9.79	65.99	3.24	0.06	0.48
8.56	0.69	6.12	10.36	63.36	3.28	0.06	0.44
8.58	0.70	6.24	9.94	61.99	3.25	0.06	0.45
8.60	0.73	6.57	9.31	61.12	3.20	0.06	0.47
8.62	0.74	6.63	8.92	59.15	3.18	0.06	0.47
8.64	0.74	6.69	8.53	57.01	3.15	0.06	0.48

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	0.73	6.53	8.47	55.33	3.14	0.06	0.47
8.68	0.71	6.31	8.75	55.21	3.16	0.06	0.45
8.70	0.69	6.08	9.17	55.77	3.19	0.06	0.43
8.72	0.68	5.98	9.37	56.03	3.21	0.06	0.43
8.74	0.70	6.16	9.05	55.80	3.19	0.06	0.44
8.76	0.73	6.45	8.54	55.08	3.15	0.06	0.46
8.78	0.79	7.09	7.74	54.84	3.08	0.06	0.51
8.80	0.94	8.83	6.19	54.69	2.95	0.06	0.63
8.82	1.24	12.09	4.65	56.16	2.78	0.07	0.87
8.84	1.53	15.24	3.97	60.52	2.70	0.08	1.10
8.86	1.73	17.40	3.87	67.39	2.68	0.08	1.25
8.88	1.77	17.75	4.13	73.36	2.72	0.08	1.28
8.90	1.67	16.67	4.55	75.89	2.77	0.08	1.20
8.93	1.43	14.06	5.38	75.68	2.87	0.07	1.01
8.94	1.14	10.84	6.81	73.89	3.01	0.06	0.77
8.96	0.90	8.24	8.61	70.94	3.15	0.06	0.59
8.99	0.79	7.03	9.72	68.34	3.23	0.06	0.50
9.00	0.82	7.31	9.21	67.27	3.20	0.06	0.52
9.02	0.99	9.10	7.43	67.61	3.06	0.06	0.65
9.04	1.18	11.17	6.00	67.03	2.93	0.07	0.80
9.06	1.32	12.75	5.24	66.80	2.85	0.07	0.91
9.08	1.37	13.24	5.06	67.00	2.83	0.07	0.95
9.10	1.37	13.23	5.14	68.05	2.84	0.07	0.95
9.12	1.36	13.03	5.29	68.94	2.86	0.07	0.93
9.14	1.31	12.56	5.61	70.40	2.89	0.07	0.90
9.16	1.19	11.15	6.38	71.19	2.97	0.06	0.80
9.18	1.02	9.31	7.58	70.56	3.07	0.06	0.66
9.20	0.85	7.53	9.07	68.36	3.19	0.06	0.54
9.22	0.81	7.02	9.53	66.86	3.22	0.06	0.50
9.24	0.83	7.27	9.17	66.59	3.19	0.06	0.52
9.26	0.94	8.42	7.92	66.66	3.10	0.06	0.60
9.28	1.04	9.45	7.01	66.20	3.02	0.06	0.67
9.30	1.07	9.77	6.69	65.34	2.99	0.06	0.70
9.32	1.04	9.39	6.86	64.44	3.01	0.06	0.67
9.34	1.02	9.20	6.97	64.11	3.02	0.06	0.66
9.36	1.05	9.48	6.81	64.56	3.01	0.06	0.68
9.38	1.03	9.31	7.16	66.66	3.04	0.06	0.67
9.40	0.94	8.33	8.15	67.91	3.12	0.06	0.60
9.42	0.87	7.54	8.97	67.65	3.18	0.06	0.54
9.44	0.91	7.95	8.39	66.72	3.14	0.06	0.57
9.46	1.06	9.48	6.97	66.07	3.02	0.06	0.68
9.48	1.21	11.09	6.00	66.53	2.93	0.07	0.79
9.50	1.33	12.37	5.45	67.40	2.87	0.07	0.88
9.52	1.39	12.95	5.35	69.25	2.86	0.07	0.93
9.54	1.40	13.03	5.48	71.45	2.88	0.07	0.93
9.56	1.36	12.60	5.75	72.45	2.91	0.07	0.90
9.58	1.26	11.56	6.42	74.19	2.97	0.07	0.83
9.60	1.12	10.00	7.47	74.65	3.06	0.06	0.71

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	1.03	9.07	8.29	75.23	3.13	0.06	0.65
9.64	1.12	9.99	7.52	75.15	3.07	0.06	0.71
9.66	1.40	12.85	5.81	74.65	2.91	0.07	0.92
9.68	1.68	15.80	4.71	74.36	2.79	0.08	1.13
9.70	1.85	17.48	4.32	75.54	2.74	0.08	1.25
9.72	1.71	16.04	4.86	78.04	2.81	0.08	1.15
9.74	1.45	13.26	5.89	78.06	2.92	0.07	0.95
9.76	1.12	9.83	7.77	76.43	3.09	0.06	0.70
9.78	0.92	7.74	9.53	73.77	3.22	0.06	0.55
9.80	0.79	6.38	11.21	71.60	3.33	0.06	0.46
9.82	0.79	6.42	10.86	69.74	3.31	0.06	0.46
9.84	0.82	6.71	10.12	67.90	3.26	0.06	0.48
9.86	0.84	6.88	9.52	65.46	3.22	0.06	0.49
9.88	0.78	6.27	10.08	63.16	3.26	0.06	0.45
9.90	0.74	5.80	10.43	60.47	3.28	0.06	0.41
9.92	0.73	5.75	10.26	58.93	3.27	0.06	0.41
9.94	0.78	6.25	9.31	58.19	3.20	0.06	0.45
9.96	0.91	7.55	7.72	58.29	3.08	0.06	0.54
9.98	1.11	9.56	6.10	58.33	2.94	0.06	0.68
10.00	1.34	11.88	5.04	59.85	2.83	0.07	0.85
10.03	1.55	14.01	4.40	61.68	2.75	0.08	1.00
10.04	1.69	15.43	4.24	65.51	2.73	0.08	1.10
10.06	1.77	16.21	4.24	68.71	2.73	0.08	1.16
10.08	1.80	16.46	4.39	72.36	2.75	0.08	1.18
10.10	1.80	16.39	4.55	74.54	2.77	0.08	1.17
10.12	1.79	16.35	4.59	75.00	2.78	0.08	1.17
10.14	1.84	16.79	4.40	73.81	2.75	0.08	1.20
10.16	1.95	17.90	4.08	73.00	2.71	0.08	1.28
10.18	2.10	19.37	3.79	73.49	2.67	0.08	1.38
10.20	2.23	20.62	3.62	74.71	2.65	0.09	1.47
10.22	2.31	21.42	3.55	76.00	2.64	0.09	1.53
10.24	2.34	21.67	3.50	75.87	2.63	0.09	1.55
10.26	2.31	21.35	3.48	74.26	2.62	0.09	1.53
10.28	2.24	20.55	3.49	71.78	2.63	0.08	1.47
10.30	2.14	19.57	3.61	70.71	2.64	0.08	1.40
10.32	2.11	19.26	3.72	71.58	2.66	0.08	1.38
10.34	2.19	19.99	3.66	73.25	2.65	0.08	1.43
10.36	2.37	21.74	3.46	75.27	2.62	0.09	1.55
10.38	2.54	23.42	3.21	75.12	2.58	0.09	0.64
10.40	2.64	24.37	3.03	73.76	2.55	0.09	0.65
10.42	2.66	24.54	2.83	69.42	2.51	0.09	0.65
10.44	2.64	24.33	2.63	63.95	2.47	0.09	0.65
10.46	2.62	24.02	2.37	56.92	2.41	0.08	0.64
10.48	2.59	23.73	2.16	51.33	2.36	0.08	0.64
10.50	2.54	23.20	2.18	50.64	2.37	0.08	0.64
10.52	2.51	22.93	2.43	55.70	2.43	0.08	0.64
10.54	2.51	22.89	2.79	63.96	2.51	0.08	0.64
10.56	2.51	22.84	3.15	71.94	2.57	0.09	0.64

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	2.43	22.00	3.55	78.06	2.64	0.09	1.57
10.60	2.27	20.34	4.02	81.80	2.70	0.09	1.45
10.62	2.16	19.22	4.29	82.50	2.74	0.08	1.37
10.64	2.21	19.72	4.15	81.93	2.72	0.08	1.41
10.66	2.41	21.63	3.79	81.95	2.67	0.09	1.54
10.68	2.64	23.84	3.58	85.34	2.64	0.09	1.70
10.70	2.82	25.51	3.51	89.44	2.63	0.09	1.82
10.72	2.93	26.55	3.50	92.80	2.63	0.09	1.89
10.74	2.98	27.05	3.39	91.66	2.61	0.09	1.92
10.76	2.95	26.68	3.23	86.21	2.58	0.09	0.66
10.78	2.74	24.61	3.21	79.03	2.58	0.09	0.65
10.80	2.34	20.73	3.53	73.23	2.63	0.09	1.47
10.82	1.88	16.25	4.43	71.94	2.76	0.08	1.16
10.84	1.53	12.87	5.65	72.73	2.90	0.07	0.92
10.86	1.23	9.91	7.36	72.98	3.05	0.06	0.71
10.88	1.01	7.86	9.00	70.69	3.18	0.06	0.56
10.90	0.84	6.21	10.72	66.58	3.30	0.06	0.44
10.92	0.81	5.95	10.80	64.30	3.31	0.06	0.43
10.94	0.81	5.93	10.59	62.79	3.29	0.06	0.42
10.96	0.82	5.98	10.28	61.48	3.27	0.06	0.43
10.98	0.83	6.04	9.95	60.16	3.25	0.06	0.43
11.00	0.82	6.00	9.84	59.02	3.24	0.06	0.43
11.02	0.81	5.84	9.94	57.98	3.25	0.06	0.42
11.04	0.79	5.70	10.15	57.83	3.26	0.06	0.41
11.06	0.78	5.59	10.46	58.48	3.28	0.06	0.40
11.08	0.78	5.54	10.69	59.19	3.30	0.06	0.40
11.10	0.77	5.44	10.93	59.48	3.31	0.06	0.39
11.12	0.76	5.33	11.10	59.16	3.32	0.06	0.38
11.15	0.76	5.34	10.93	58.40	3.31	0.06	0.38
11.16	0.77	5.44	10.63	57.77	3.29	0.06	0.39
11.18	0.79	5.55	10.38	57.61	3.28	0.06	0.40
11.20	0.78	5.51	10.45	57.55	3.28	0.06	0.39
11.22	0.78	5.45	10.55	57.43	3.29	0.06	0.39
11.24	0.78	5.46	10.48	57.23	3.28	0.06	0.39
11.26	0.78	5.46	10.45	57.07	3.28	0.06	0.39
11.28	0.78	5.40	10.54	56.89	3.29	0.06	0.39
11.30	0.77	5.35	10.54	56.33	3.29	0.06	0.38
11.32	0.78	5.40	10.29	55.61	3.27	0.06	0.39
11.34	0.79	5.54	9.92	54.93	3.25	0.06	0.40
11.36	0.80	5.62	9.73	54.68	3.23	0.06	0.40
11.38	0.81	5.66	9.69	54.89	3.23	0.06	0.40
11.40	0.81	5.70	9.70	55.33	3.23	0.06	0.41
11.42	0.82	5.77	9.71	56.07	3.23	0.06	0.41
11.44	0.83	5.85	9.76	57.11	3.24	0.06	0.42
11.46	0.85	6.00	9.72	58.35	3.23	0.06	0.43
11.48	0.87	6.20	9.60	59.48	3.22	0.06	0.44
11.50	0.89	6.35	9.51	60.45	3.22	0.06	0.45
11.52	0.90	6.47	9.48	61.34	3.22	0.06	0.46

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	0.91	6.48	9.60	62.24	3.22	0.06	0.46
11.56	0.92	6.57	9.63	63.27	3.23	0.06	0.47
11.58	0.92	6.56	9.79	64.25	3.24	0.06	0.47
11.60	0.93	6.67	9.75	65.05	3.24	0.06	0.48
11.62	0.94	6.70	9.83	65.84	3.24	0.06	0.48
11.64	0.94	6.71	9.92	66.58	3.25	0.06	0.48
11.66	0.93	6.58	10.29	67.67	3.27	0.06	0.47
11.68	0.92	6.50	10.56	68.63	3.29	0.06	0.46
11.70	0.92	6.46	10.79	69.70	3.30	0.06	0.46
11.72	0.89	6.20	11.30	70.05	3.34	0.06	0.44
11.74	0.85	5.86	11.88	69.63	3.37	0.06	0.42
11.76	0.83	5.65	12.14	68.53	3.39	0.06	0.40
11.78	0.85	5.81	11.62	67.50	3.36	0.06	0.41
11.80	0.90	6.29	10.64	66.97	3.30	0.06	0.45
11.82	0.95	6.71	9.97	66.93	3.25	0.06	0.48
11.84	0.99	7.06	9.55	67.48	3.22	0.06	0.50
11.86	1.01	7.17	9.54	68.40	3.22	0.06	0.51
11.88	1.02	7.30	9.52	69.48	3.22	0.06	0.52
11.90	1.04	7.45	9.54	71.06	3.22	0.06	0.53
11.93	1.06	7.59	9.59	72.86	3.22	0.06	0.54
11.94	1.07	7.71	9.70	74.76	3.23	0.06	0.55
11.96	1.08	7.78	9.80	76.24	3.24	0.06	0.56
11.98	1.08	7.80	9.90	77.20	3.25	0.06	0.56
12.00	1.08	7.76	10.03	77.81	3.25	0.06	0.55
12.02	1.09	7.78	10.05	78.23	3.26	0.06	0.56
12.04	1.09	7.83	10.03	78.49	3.25	0.06	0.56
12.06	1.10	7.89	9.94	78.48	3.25	0.06	0.56
12.08	1.10	7.88	9.96	78.42	3.25	0.06	0.56
12.10	1.10	7.83	9.99	78.26	3.25	0.06	0.56
12.12	1.10	7.82	10.00	78.17	3.25	0.06	0.56
12.14	1.10	7.81	9.98	77.94	3.25	0.06	0.56
12.16	1.11	7.89	9.86	77.81	3.24	0.06	0.56
12.18	1.12	7.94	9.81	77.82	3.24	0.06	0.57
12.20	1.13	8.05	9.67	77.83	3.23	0.06	0.58
12.22	1.14	8.15	9.57	78.00	3.22	0.06	0.58
12.24	1.16	8.28	9.46	78.26	3.21	0.06	0.59
12.26	1.18	8.43	9.35	78.85	3.21	0.06	0.60
12.28	1.20	8.57	9.26	79.40	3.20	0.06	0.61
12.30	1.23	8.85	9.03	79.93	3.18	0.06	0.63
12.33	1.25	9.03	8.90	80.40	3.17	0.06	0.65
12.34	1.29	9.30	8.72	81.16	3.16	0.06	0.66
12.36	1.31	9.51	8.64	82.08	3.15	0.06	0.68
12.38	1.35	9.82	8.49	83.34	3.14	0.06	0.70
12.40	1.38	10.05	8.43	84.75	3.14	0.06	0.72
12.42	1.40	10.23	8.45	86.49	3.14	0.06	0.73
12.44	1.41	10.26	8.62	88.47	3.15	0.06	0.73
12.46	1.41	10.24	8.81	90.21	3.17	0.06	0.73
12.48	1.39	10.11	9.08	91.71	3.19	0.06	0.72

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	1.37	9.92	9.34	92.68	3.21	0.06	0.71
12.52	1.35	9.67	9.69	93.68	3.23	0.06	0.69
12.54	1.32	9.42	9.99	94.12	3.25	0.06	0.67
12.56	1.29	9.18	10.27	94.24	3.27	0.06	0.66
12.58	1.26	8.92	10.53	93.92	3.29	0.06	0.64
12.60	1.23	8.65	10.79	93.37	3.30	0.06	0.62
12.62	1.20	8.33	11.09	92.33	3.32	0.06	0.59
12.64	1.17	8.10	11.23	90.91	3.33	0.06	0.58
12.66	1.15	7.86	11.34	89.18	3.34	0.06	0.56
12.68	1.12	7.61	11.49	87.47	3.35	0.06	0.54
12.70	1.07	7.18	11.90	85.41	3.37	0.06	0.51
12.72	1.01	6.67	12.42	82.79	3.41	0.06	0.48
12.74	0.95	6.12	13.03	79.74	3.44	0.06	0.44
12.76	0.89	5.65	13.53	76.53	3.47	0.06	0.40
12.78	0.85	5.26	13.80	72.65	3.48	0.06	0.38
12.81	0.83	5.08	13.62	69.18	3.47	0.06	0.36
12.82	0.81	4.97	13.22	65.75	3.45	0.06	0.36
12.84	0.80	4.88	12.97	63.28	3.44	0.06	0.35
12.86	0.78	4.68	12.92	60.40	3.43	0.06	0.33
12.88	0.76	4.46	12.98	57.82	3.44	0.06	0.32
12.90	0.74	4.36	12.77	55.63	3.43	0.06	0.31
12.92	0.74	4.29	12.57	53.98	3.41	0.06	0.31
12.94	0.73	4.24	12.36	52.33	3.40	0.06	0.30
12.96	0.71	4.08	12.45	50.78	3.41	0.06	0.29
12.98	0.70	3.99	12.21	48.74	3.39	0.06	0.29
13.00	0.71	4.06	11.55	46.93	3.35	0.06	0.29
13.02	0.73	4.19	10.80	45.27	3.31	0.06	0.30
13.04	0.75	4.32	10.28	44.36	3.27	0.06	0.31
13.06	0.76	4.39	10.02	43.94	3.25	0.06	0.31
13.08	0.77	4.47	9.87	44.10	3.24	0.06	0.32
13.10	0.78	4.58	9.74	44.67	3.23	0.06	0.33
13.12	0.80	4.70	9.65	45.36	3.23	0.06	0.34
13.15	0.82	4.85	9.54	46.32	3.22	0.06	0.35
13.16	0.83	4.93	9.65	47.57	3.23	0.06	0.35
13.18	0.84	5.03	9.82	49.33	3.24	0.06	0.36
13.20	0.84	5.01	10.12	50.69	3.26	0.06	0.36
13.22	0.83	4.97	10.42	51.85	3.28	0.06	0.36
13.24	0.81	4.74	11.06	52.45	3.32	0.06	0.34
13.26	0.78	4.49	11.74	52.73	3.36	0.06	0.32
13.29	0.74	4.22	12.40	52.34	3.40	0.06	0.30
13.30	0.72	4.02	12.82	51.47	3.43	0.06	0.29
13.32	0.70	3.84	13.10	50.30	3.45	0.06	0.27
13.34	0.68	3.68	13.36	49.14	3.46	0.06	0.26
13.36	0.68	3.63	13.27	48.24	3.45	0.06	0.26
13.38	0.67	3.61	13.15	47.47	3.45	0.06	0.26
13.40	0.68	3.68	12.71	46.75	3.42	0.06	0.26
13.42	0.69	3.76	12.32	46.30	3.40	0.06	0.27
13.44	0.72	3.99	11.54	46.09	3.35	0.06	0.29

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	0.76	4.29	10.71	45.94	3.30	0.06	0.31
13.49	0.78	4.40	10.33	45.49	3.27	0.06	0.31
13.50	0.80	4.61	9.87	45.49	3.24	0.06	0.33
13.52	0.89	5.32	8.65	45.99	3.16	0.06	0.38
13.54	1.16	7.48	6.22	46.57	2.95	0.06	0.53
13.56	1.50	10.27	4.53	46.54	2.77	0.07	0.73
13.58	1.77	12.50	4.00	49.94	2.70	0.08	0.88
13.60	1.87	13.27	4.19	55.53	2.73	0.08	0.94
13.62	1.92	13.65	4.46	60.89	2.76	0.08	0.97
13.64	2.03	14.53	4.44	64.51	2.76	0.08	1.03
13.66	2.17	15.63	4.34	67.92	2.75	0.08	1.11
13.68	2.33	16.97	4.25	72.08	2.73	0.08	1.20
13.70	2.50	18.32	4.15	76.04	2.72	0.09	1.29
13.72	2.65	19.51	3.99	77.89	2.70	0.09	1.38
13.74	2.63	19.31	3.97	76.65	2.70	0.09	1.36
13.76	2.40	17.45	4.15	72.38	2.72	0.08	1.23
13.78	2.11	15.02	4.46	67.00	2.76	0.08	1.06
13.81	1.89	13.19	4.79	63.23	2.80	0.08	0.94
13.82	1.89	13.18	4.68	61.73	2.79	0.08	0.94
13.84	2.00	14.07	4.58	64.42	2.78	0.08	1.00
13.86	2.12	14.98	4.61	68.97	2.78	0.08	1.06
13.88	2.13	14.97	4.87	72.98	2.81	0.08	1.07
13.90	2.05	14.33	5.13	73.51	2.84	0.08	1.02
13.92	1.94	13.44	5.40	72.59	2.87	0.07	0.96
13.94	1.82	12.46	5.76	71.74	2.91	0.07	0.89
13.96	1.69	11.41	6.23	71.08	2.95	0.07	0.81
13.98	1.58	10.53	6.62	69.72	2.99	0.07	0.75
14.00	1.51	9.93	6.91	68.58	3.01	0.06	0.71
14.02	1.48	9.67	7.10	68.65	3.03	0.06	0.69
14.04	1.47	9.61	7.29	69.99	3.05	0.06	0.69
14.06	1.45	9.44	7.58	71.58	3.07	0.06	0.67
14.08	1.41	9.11	7.97	72.60	3.10	0.06	0.65
14.10	1.31	8.35	8.65	72.27	3.16	0.06	0.60
14.12	1.19	7.36	9.60	70.59	3.22	0.06	0.53
14.15	1.02	6.01	11.26	67.67	3.33	0.06	0.43
14.16	0.88	4.95	12.97	64.19	3.44	0.06	0.35
14.18	0.82	4.51	13.72	61.83	3.48	0.06	0.32
14.20	1.04	6.19	10.23	63.34	3.27	0.06	0.44
14.22	1.39	8.88	7.08	62.84	3.03	0.06	0.63
14.24	1.68	11.13	5.56	61.89	2.89	0.07	0.79
14.26	1.69	11.17	5.46	60.96	2.88	0.07	0.80
14.28	1.55	10.05	6.05	60.83	2.94	0.07	0.72
14.30	1.40	8.92	6.70	59.74	3.00	0.06	0.64
14.32	1.29	8.06	7.44	59.96	3.06	0.06	0.58
14.34	1.17	7.09	8.56	60.67	3.15	0.06	0.51
14.36	1.02	5.97	10.31	61.52	3.27	0.06	0.43
14.38	0.87	4.76	12.74	60.62	3.42	0.06	0.34
14.40	0.80	4.22	13.99	59.08	3.49	0.06	0.30

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	0.92	5.16	11.61	59.95	3.36	0.06	0.37
14.44	1.26	7.72	7.80	60.27	3.09	0.06	0.55
14.46	1.59	10.26	5.79	59.38	2.91	0.07	0.73
14.48	1.71	11.14	5.34	59.53	2.86	0.07	0.80
14.50	1.61	10.39	5.73	59.52	2.90	0.07	0.74
14.52	1.45	9.14	6.53	59.63	2.98	0.06	0.65
14.54	1.30	7.97	7.42	59.17	3.06	0.06	0.57
14.56	1.14	6.78	8.87	60.12	3.17	0.06	0.48
14.58	0.97	5.44	11.07	60.23	3.32	0.06	0.39
14.60	0.83	4.36	13.56	59.17	3.47	0.06	0.31
14.62	0.77	3.93	14.73	57.86	3.53	0.06	0.28
14.64	0.96	5.38	11.18	60.21	3.33	0.06	0.38
14.66	1.40	8.69	6.99	60.73	3.02	0.06	0.62
14.68	2.03	13.54	4.34	58.73	2.75	0.08	0.96
14.70	2.53	17.67	3.21	56.65	2.58	0.08	0.61
14.72	2.85	20.37	2.65	53.97	2.48	0.08	0.62
14.74	2.95	21.20	2.42	51.38	2.43	0.08	0.63
14.76	2.86	20.45	2.48	50.81	2.44	0.08	0.63
14.78	2.55	17.80	3.07	54.57	2.56	0.08	0.61
14.80	2.26	15.22	4.08	62.17	2.71	0.08	1.07
14.82	2.31	15.62	4.19	65.47	2.73	0.08	1.10
14.85	2.65	18.31	3.65	66.74	2.65	0.09	1.28
14.86	2.99	21.13	3.05	64.50	2.55	0.09	0.63
14.88	3.06	21.67	2.97	64.35	2.54	0.09	0.63
14.90	3.02	21.30	2.96	63.03	2.54	0.09	0.63
14.92	2.88	20.25	2.92	59.18	2.53	0.09	0.62
14.94	2.69	18.72	2.96	55.37	2.54	0.08	0.62
14.97	2.50	17.21	3.13	53.92	2.57	0.08	0.61
14.98	2.52	17.22	3.43	59.13	2.62	0.08	1.20
15.00	2.70	18.49	3.60	66.60	2.64	0.09	1.29
15.02	2.93	20.23	3.64	73.66	2.65	0.09	1.41
15.04	3.00	20.64	3.83	79.09	2.68	0.09	1.45
15.06	2.75	18.63	4.32	80.55	2.74	0.09	1.32
15.08	2.27	14.80	5.22	77.31	2.85	0.08	1.06
15.10	1.67	10.42	6.76	70.38	3.00	0.07	0.74
15.13	1.24	7.22	8.85	63.86	3.17	0.06	0.52
15.14	1.01	5.49	10.79	59.23	3.30	0.06	0.39
15.16	0.99	5.39	10.88	58.59	3.31	0.06	0.38
15.18	1.08	6.02	9.76	58.70	3.24	0.06	0.43
15.20	1.15	6.55	9.07	59.37	3.19	0.06	0.47
15.22	1.14	6.43	9.32	59.91	3.21	0.06	0.46
15.24	1.08	5.96	10.14	60.42	3.26	0.06	0.43
15.26	1.01	5.47	11.17	61.06	3.33	0.06	0.39
15.28	0.96	5.07	12.07	61.22	3.38	0.06	0.36
15.30	0.93	4.87	12.66	61.65	3.42	0.06	0.35
15.32	0.94	4.91	12.72	62.40	3.42	0.06	0.35
15.34	0.96	5.09	12.30	62.57	3.40	0.06	0.36
15.36	0.96	5.09	12.05	61.29	3.38	0.06	0.36

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	0.97	5.12	11.55	59.07	3.35	0.06	0.37
15.40	1.02	5.46	10.50	57.32	3.29	0.06	0.39
15.42	1.08	5.94	9.31	55.31	3.20	0.06	0.42
15.44	1.13	6.26	8.74	54.69	3.16	0.06	0.45
15.46	1.29	7.42	7.48	55.54	3.06	0.06	0.53
15.48	1.55	9.29	6.12	56.92	2.94	0.07	0.66
15.50	1.75	10.72	5.39	57.73	2.87	0.07	0.77
15.52	1.69	10.25	5.82	59.59	2.91	0.07	0.73
15.54	1.59	9.49	6.58	62.46	2.99	0.06	0.68
15.56	1.69	10.24	6.27	64.20	2.96	0.06	0.73
15.58	1.89	11.69	5.54	64.71	2.88	0.07	0.83
15.60	2.09	13.11	5.10	66.81	2.84	0.08	0.94

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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LIQUEFACTION ANALYSIS REPORT

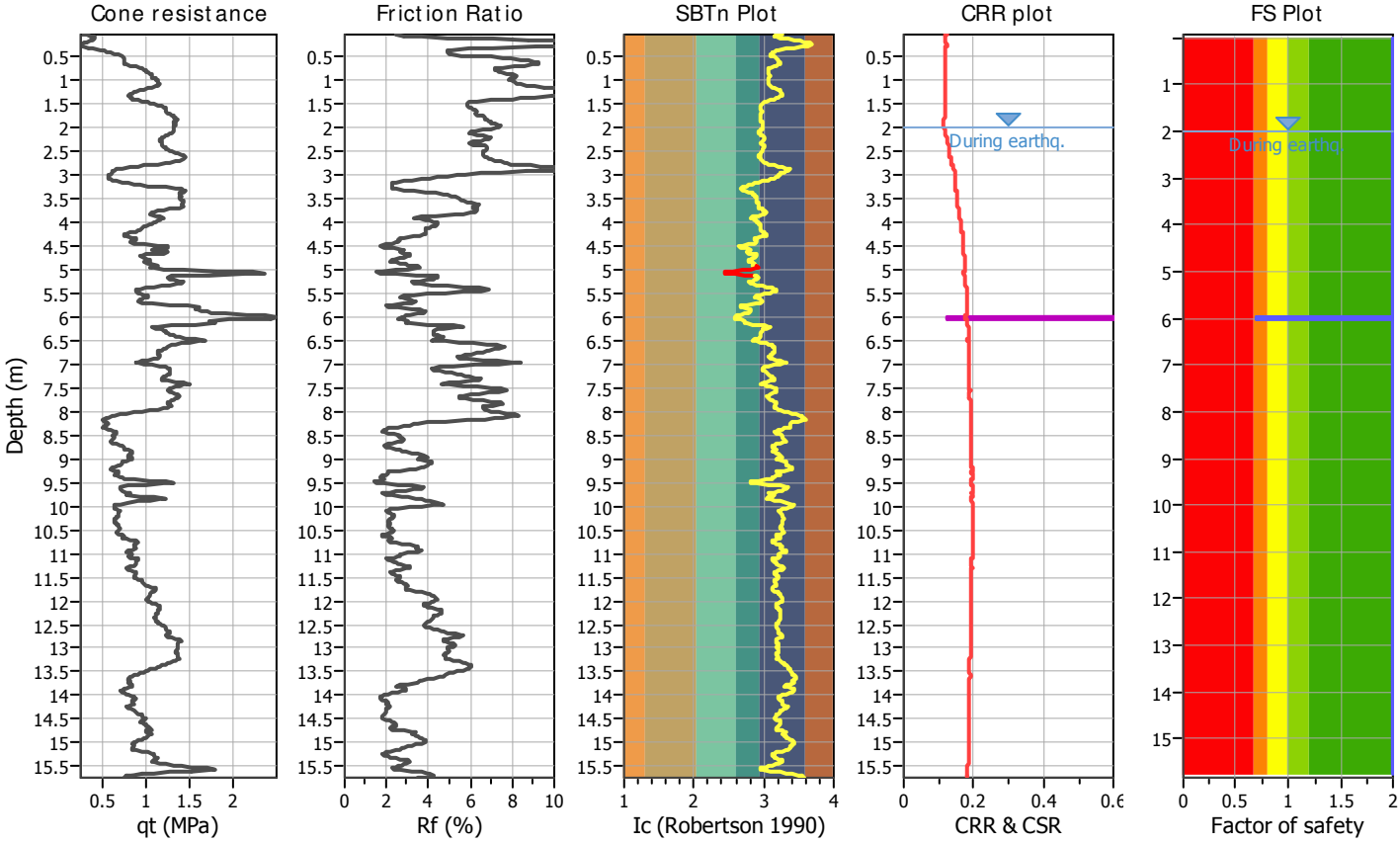
Project title :

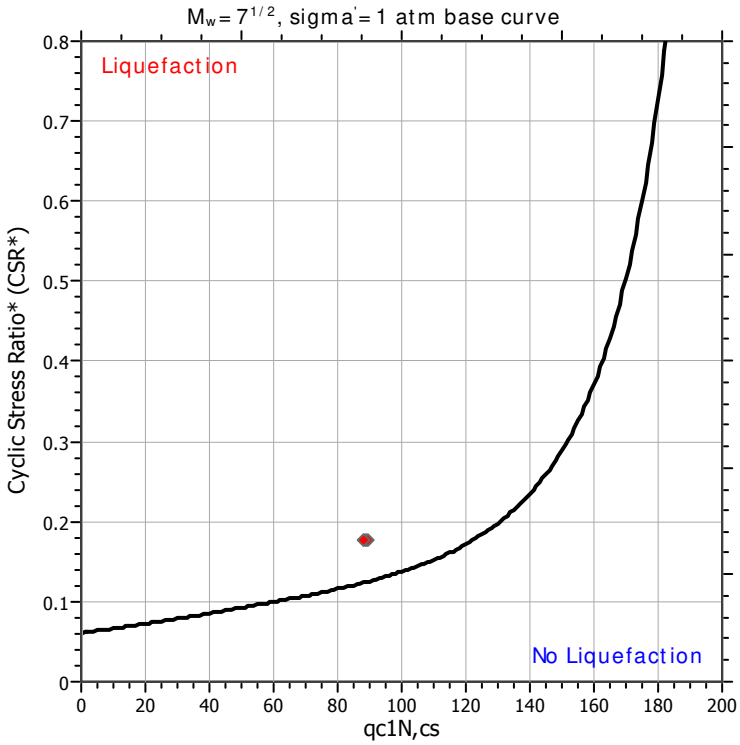
Location :

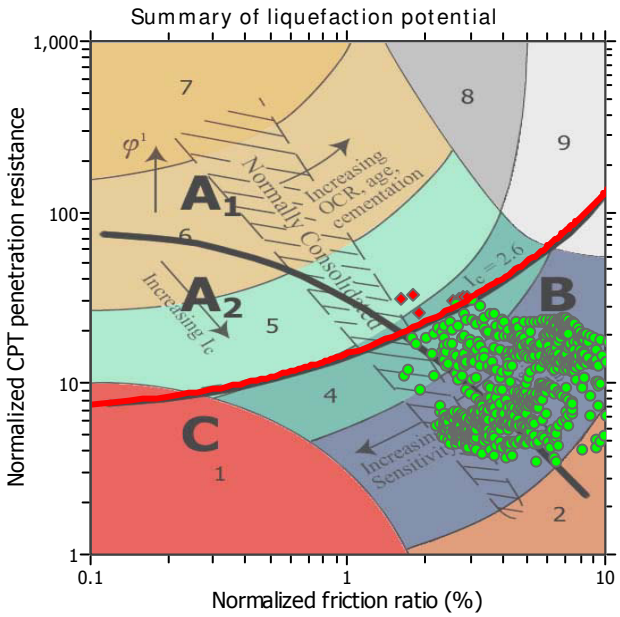
CPT file : Cptu-6

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.50 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.22	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

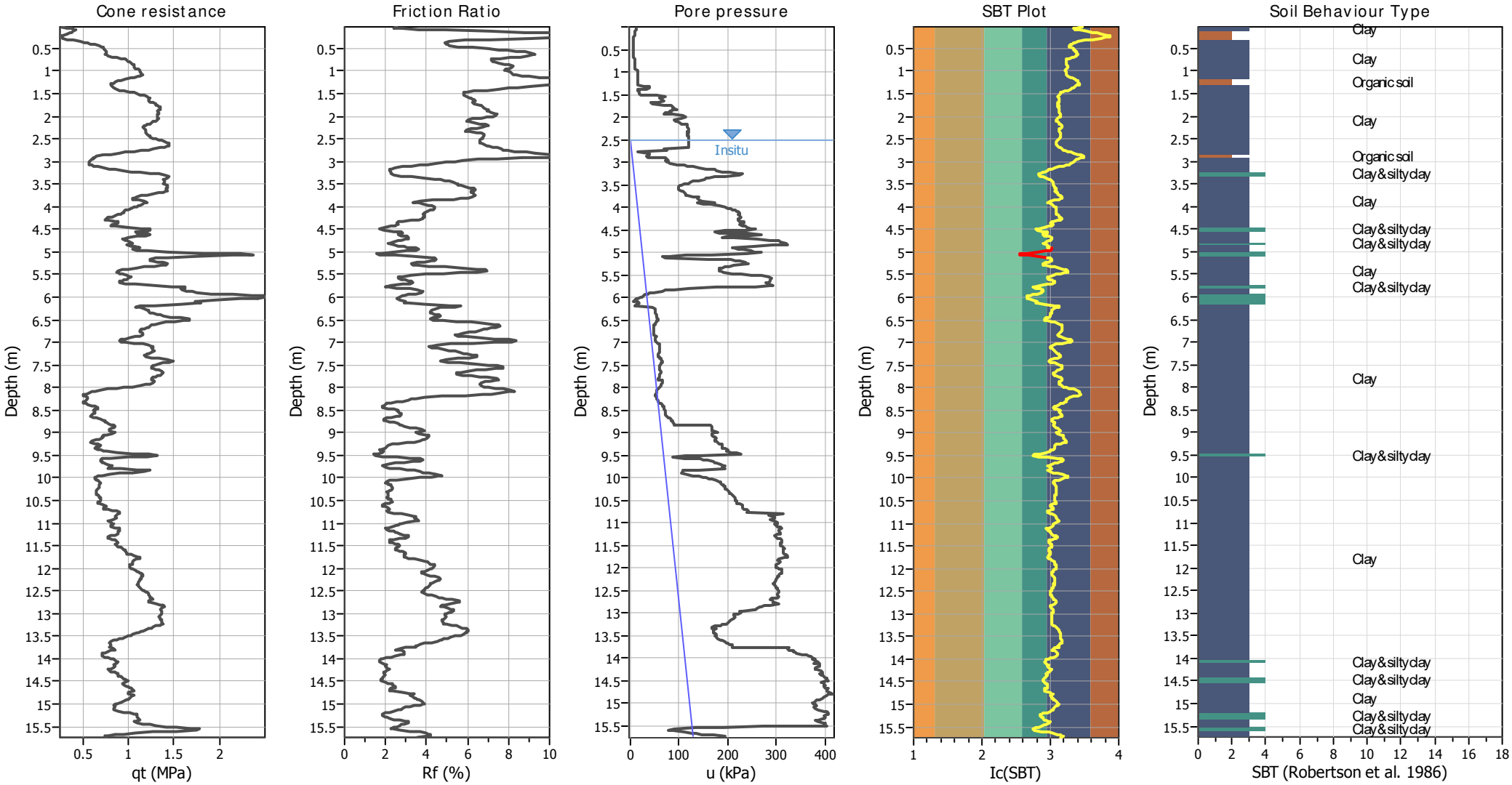






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



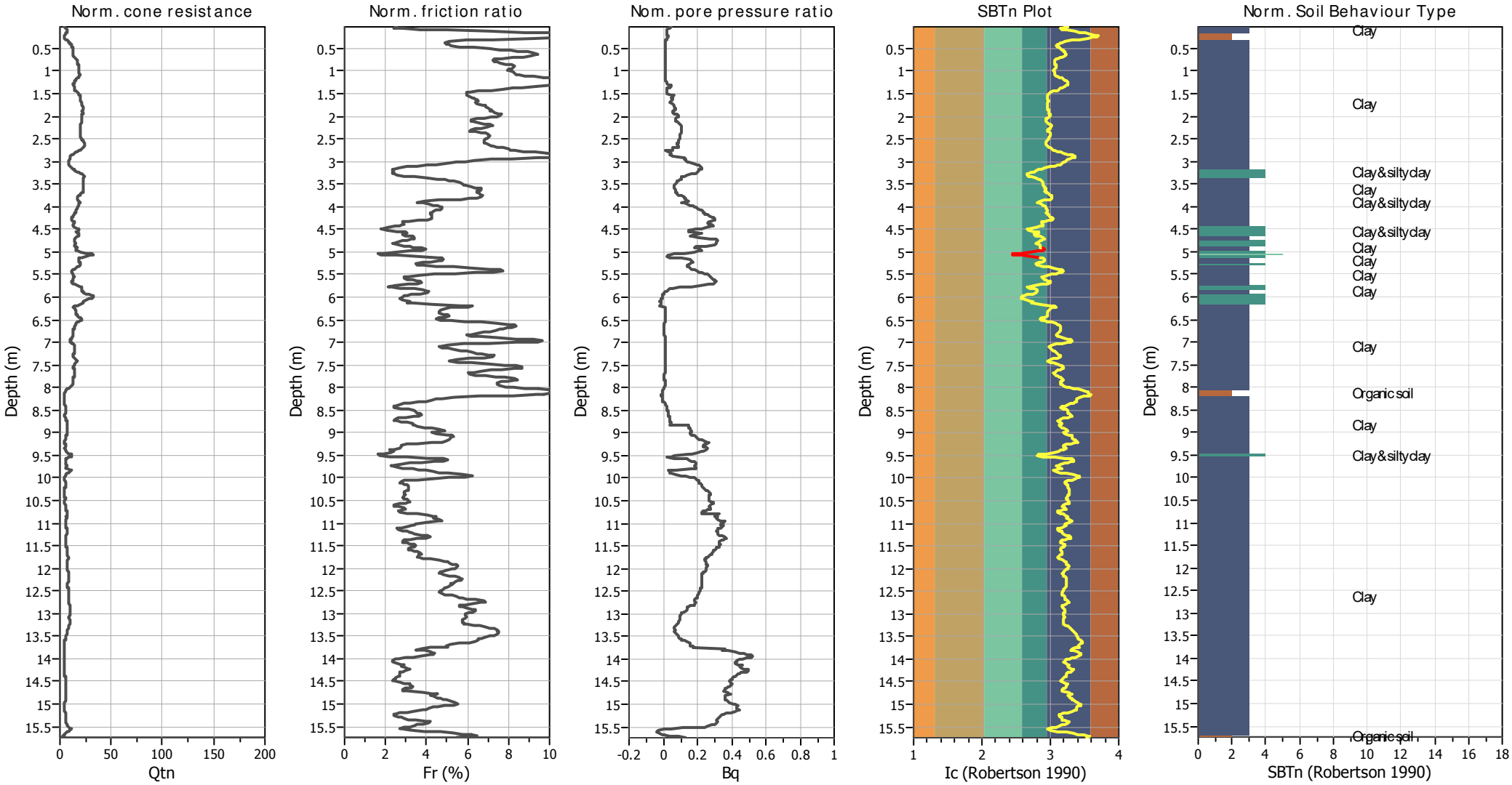
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



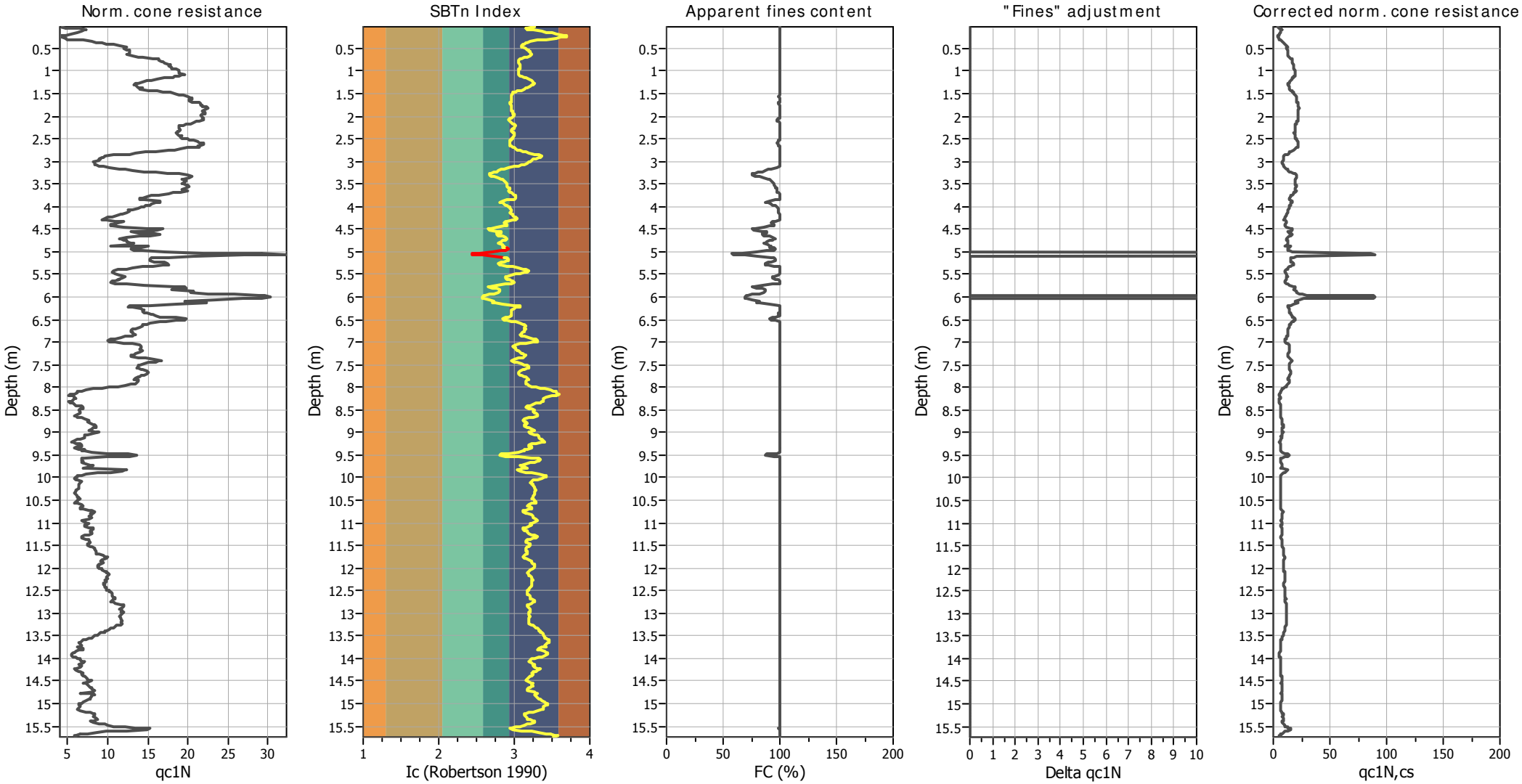
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

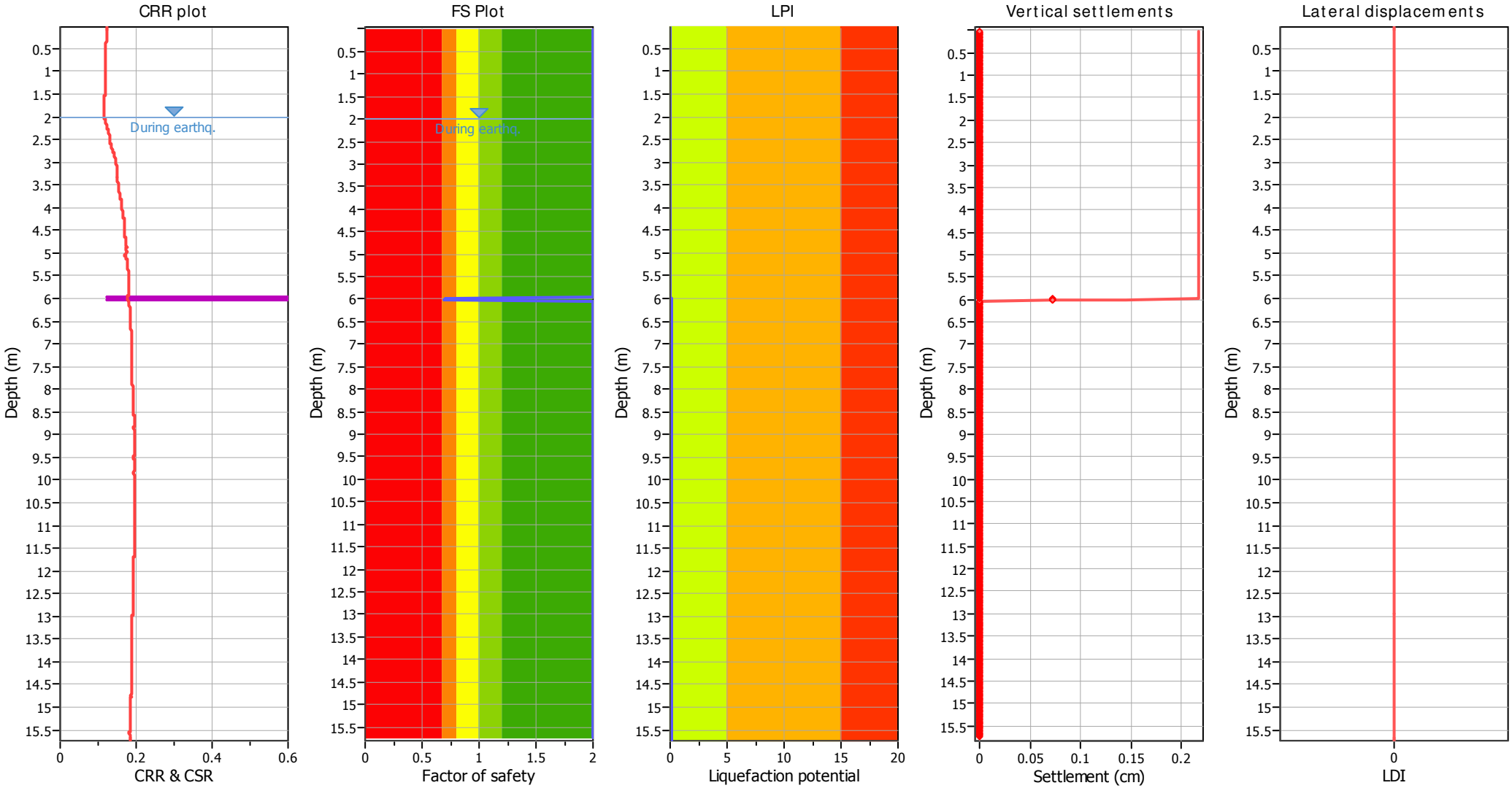
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

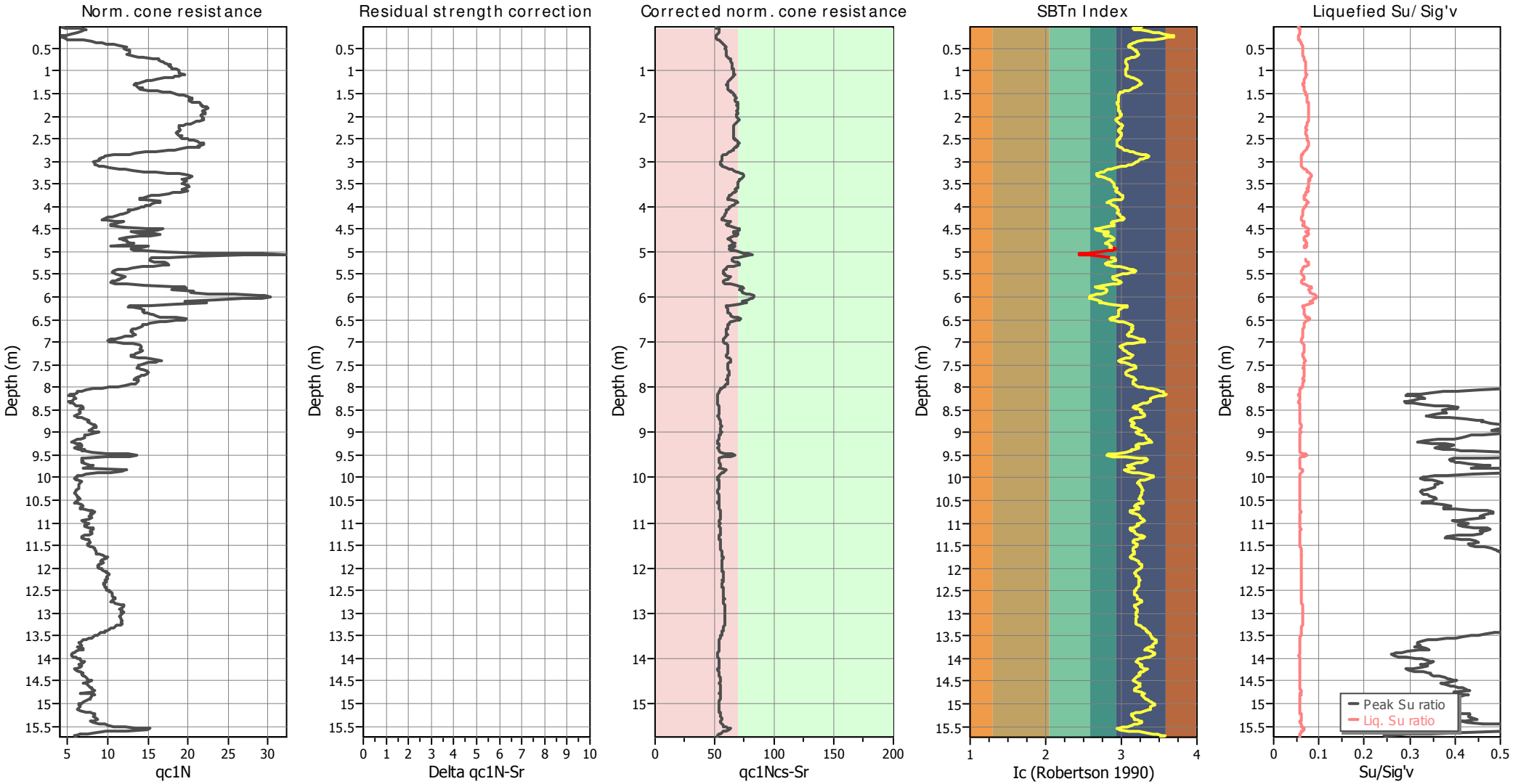
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

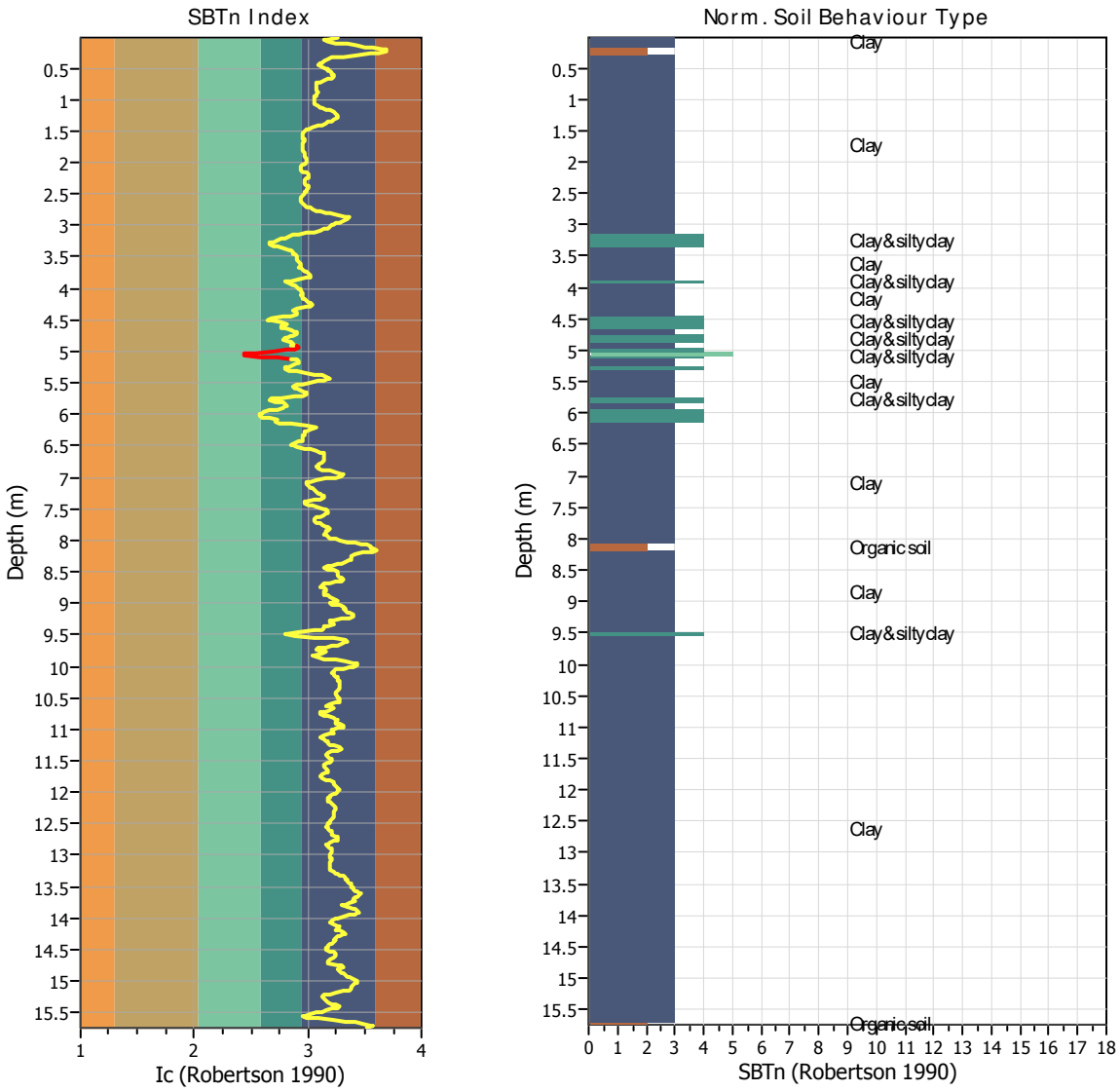
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	787
I_c maximum check value:	3.00	Total points excluded:	11
I_c change ratio value:	0.0100	Exclusion percentage:	1.40%
Minimum number of points in layer:	4	Number of layers detected:	2

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	6	Start depth: 4.94 (m)	3	Clay
		End depth: 5.04 (m)	5	Silty sand & sandy silt
Transition layer 2	5	Start depth: 5.06 (m)	5	Silty sand & sandy silt
		End depth: 5.14 (m)	3	Clay

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.24	6.33	12.46	78.01	14.61
2	0.04	0.28	6.69	12.46	70.62	14.92
3	0.06	0.39	10.11	12.15	69.09	15.30
4	0.08	0.43	14.30	8.56	70.76	15.78
5	0.10	0.42	21.10	8.74	76.40	16.14
6	0.12	0.40	26.43	8.56	85.83	16.48
7	0.15	0.37	37.39	7.94	92.37	16.66
8	0.16	0.37	36.66	7.69	100.00	16.77
9	0.18	0.33	39.21	7.50	100.00	16.75
10	0.20	0.28	39.27	7.19	100.00	16.71
11	0.22	0.24	37.22	6.94	100.00	16.61
12	0.24	0.25	32.59	6.82	100.00	16.47
13	0.26	0.25	28.52	6.63	100.00	16.33
14	0.28	0.28	24.45	6.57	100.00	16.21
15	0.30	0.30	23.02	6.57	92.17	16.20
16	0.32	0.41	23.20	6.57	82.51	16.25
17	0.34	0.47	23.76	6.82	74.42	16.34
18	0.36	0.51	24.29	6.88	70.96	16.43
19	0.38	0.55	26.90	6.82	69.10	16.54
20	0.41	0.58	29.22	7.01	67.62	16.67
21	0.42	0.63	31.57	7.01	66.19	16.80
22	0.44	0.68	35.14	7.44	64.66	16.94
23	0.46	0.74	38.87	7.44	65.19	17.10
24	0.48	0.72	45.26	7.25	67.11	17.25
25	0.50	0.72	51.59	7.01	69.58	17.39
26	0.52	0.74	56.11	6.88	70.87	17.49
27	0.54	0.75	59.21	6.82	71.71	17.58
28	0.56	0.75	64.05	6.82	72.65	17.65
29	0.58	0.76	66.84	6.76	73.71	17.72
30	0.60	0.76	69.68	6.76	74.53	17.75
31	0.62	0.75	70.06	6.82	75.30	17.76
32	0.64	0.74	69.74	6.88	74.90	17.76
33	0.66	0.78	69.51	7.01	73.39	17.78
34	0.68	0.83	71.03	7.25	71.25	17.82
35	0.70	0.86	72.29	7.63	68.42	17.84
36	0.72	0.93	69.27	8.12	65.69	17.84
37	0.74	0.97	68.01	8.43	63.67	17.84
38	0.76	0.97	69.62	8.56	63.09	17.86
39	0.78	0.99	71.96	8.74	63.09	17.90
40	0.80	1.01	73.83	8.93	63.02	17.94
41	0.82	1.02	75.71	9.18	63.06	17.99
42	0.84	1.05	81.33	9.55	63.52	18.06
43	0.86	1.06	86.46	9.73	63.89	18.12
44	0.88	1.06	87.69	9.98	64.33	18.14
45	0.90	1.05	86.28	10.11	64.27	18.15
46	0.92	1.07	87.33	10.35	64.03	18.14
47	0.94	1.07	86.25	14.51	63.41	18.16
48	0.96	1.10	87.98	14.57	62.58	18.17

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.99	1.13	87.34	14.76	62.11	18.18
50	1.00	1.12	88.13	14.88	62.14	18.20
51	1.02	1.12	91.35	14.88	62.70	18.22
52	1.05	1.12	93.31	15.00	62.70	18.26
53	1.07	1.17	95.47	15.19	62.72	18.28
54	1.08	1.15	96.12	14.94	62.99	18.30
55	1.10	1.13	97.17	14.26	64.28	18.31
56	1.12	1.10	100.21	14.38	65.69	18.32
57	1.14	1.08	102.06	14.45	67.63	18.33
58	1.16	1.02	103.34	14.51	70.00	18.33
59	1.18	0.96	104.40	14.57	72.67	18.32
60	1.20	0.92	103.31	14.63	74.79	18.29
61	1.22	0.89	100.37	14.82	75.99	18.24
62	1.24	0.86	96.00	15.00	76.83	18.18
63	1.26	0.83	91.40	15.19	77.62	18.12
64	1.28	0.80	89.49	15.44	78.24	18.07
65	1.30	0.79	86.44	26.10	77.65	18.01
66	1.32	0.80	79.37	38.87	75.75	17.95
67	1.34	0.82	74.19	37.57	73.35	17.87
68	1.36	0.82	70.05	32.05	71.07	17.82
69	1.38	0.86	68.05	16.06	69.85	17.77
70	1.40	0.83	64.71	15.87	67.78	17.74
71	1.42	0.90	62.65	16.49	65.19	17.71
72	1.44	0.96	60.66	17.54	61.70	17.69
73	1.46	1.01	58.78	18.29	59.16	17.70
74	1.48	1.06	60.77	17.98	57.80	17.74
75	1.50	1.09	64.49	22.07	56.93	17.80
76	1.52	1.12	65.65	53.38	56.20	17.86
77	1.54	1.16	67.73	71.79	55.61	17.91
78	1.56	1.19	71.92	60.45	55.38	17.97
79	1.58	1.21	74.08	59.58	55.54	18.02
80	1.60	1.22	76.60	66.77	55.59	18.05
81	1.62	1.22	76.74	66.89	55.96	18.06
82	1.64	1.20	76.89	67.89	56.35	18.07
83	1.66	1.20	78.26	55.42	56.46	18.07
84	1.68	1.23	77.70	41.41	55.67	18.08
85	1.70	1.28	77.41	44.45	55.10	18.11
86	1.72	1.29	82.94	68.26	55.05	18.16
87	1.74	1.29	86.19	82.64	55.62	18.21
88	1.76	1.30	88.77	86.92	55.91	18.24
89	1.78	1.30	89.23	88.41	55.73	18.27
90	1.80	1.34	90.14	87.91	55.59	18.29
91	1.82	1.34	92.77	94.67	55.74	18.31
92	1.84	1.33	94.67	90.95	56.12	18.32
93	1.86	1.32	92.56	80.78	56.56	18.31
94	1.88	1.30	92.06	82.64	56.55	18.29
95	1.90	1.30	90.79	71.73	56.79	18.31
96	1.92	1.32	95.90	68.26	57.05	18.34

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	1.32	98.97	85.93	57.60	18.37
98	1.96	1.30	99.06	107.38	58.08	18.38
99	1.98	1.29	98.85	114.32	57.96	18.36
100	2.00	1.30	95.04	115.00	57.60	18.34
101	2.02	1.30	93.58	104.84	56.62	18.30
102	2.04	1.31	87.69	89.09	55.74	18.24
103	2.06	1.30	82.35	90.82	54.51	18.18
104	2.08	1.31	78.51	92.75	53.93	18.12
105	2.10	1.28	76.28	95.60	54.08	18.09
106	2.12	1.25	77.78	102.29	54.80	18.09
107	2.14	1.24	78.27	104.53	55.93	18.10
108	2.16	1.21	80.97	116.24	57.18	18.12
109	2.18	1.18	83.45	116.55	58.49	18.14
110	2.20	1.16	83.63	117.48	59.35	18.13
111	2.22	1.14	81.52	117.98	59.39	18.11
112	2.24	1.14	78.20	119.16	58.94	18.06
113	2.26	1.15	75.57	119.34	58.12	18.02
114	2.28	1.15	73.25	119.22	56.93	17.98
115	2.30	1.17	68.32	118.72	56.13	17.95
116	2.32	1.17	69.52	117.42	56.03	17.95
117	2.35	1.16	72.86	117.67	56.81	17.99
118	2.36	1.16	75.91	118.29	57.83	18.04
119	2.38	1.16	79.92	118.04	58.42	18.08
120	2.40	1.17	81.30	117.85	58.63	18.12
121	2.42	1.20	83.37	118.16	58.26	18.15
122	2.44	1.22	84.22	118.41	58.05	18.17
123	2.46	1.22	85.07	118.41	57.72	18.18
124	2.48	1.23	83.98	118.47	57.12	18.19
125	2.50	1.29	86.27	118.41	56.39	18.22
126	2.52	1.31	88.49	118.78	55.67	18.25
127	2.54	1.34	89.81	119.53	55.20	18.29
128	2.56	1.38	92.91	120.02	54.64	18.32
129	2.58	1.41	94.09	119.22	54.29	18.36
130	2.60	1.43	97.13	119.59	54.19	18.39
131	2.62	1.44	98.74	120.09	54.54	18.41
132	2.64	1.41	99.97	120.15	55.12	18.42
133	2.66	1.40	100.52	119.71	55.53	18.43
134	2.68	1.41	100.49	117.92	56.65	18.42
135	2.70	1.31	100.67	70.06	58.07	18.40
136	2.72	1.26	98.59	73.34	59.96	18.35
137	2.74	1.21	94.13	71.61	61.25	18.30
138	2.76	1.15	90.88	14.88	63.22	18.23
139	2.78	1.05	87.42	37.14	66.13	18.16
140	2.80	0.96	86.33	40.05	69.70	18.10
141	2.82	0.88	83.72	39.99	72.95	18.04
142	2.84	0.83	81.26	37.88	77.81	17.97
143	2.86	0.69	79.91	31.93	83.23	17.89
144	2.88	0.62	75.75	36.52	86.62	17.75

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.62	60.94	70.86	85.69	17.57
146	2.92	0.60	52.12	74.95	82.52	17.38
147	2.95	0.59	47.11	76.32	79.41	17.18
148	2.96	0.60	36.71	71.54	76.80	17.02
149	2.98	0.58	34.10	73.84	74.87	16.83
150	3.00	0.54	30.67	78.49	74.22	16.71
151	3.02	0.55	27.10	81.65	73.10	16.59
152	3.04	0.54	25.25	96.16	70.83	16.49
153	3.06	0.55	23.55	110.04	68.58	16.40
154	3.08	0.56	21.47	117.98	65.65	16.33
155	3.10	0.59	20.16	130.01	62.15	16.25
156	3.12	0.62	18.28	139.49	57.99	16.19
157	3.14	0.68	17.37	155.98	53.49	16.18
158	3.16	0.77	17.81	172.16	49.91	16.21
159	3.18	0.82	18.43	175.26	47.66	16.32
160	3.20	0.88	20.89	188.78	45.81	16.45
161	3.22	0.98	22.94	204.28	43.89	16.61
162	3.24	1.09	25.52	220.21	41.75	16.76
163	3.26	1.19	27.81	231.06	39.91	16.89
164	3.28	1.29	29.77	223.00	38.66	17.02
165	3.30	1.38	33.44	195.16	38.54	17.18
166	3.32	1.41	39.06	174.46	39.95	17.38
167	3.34	1.42	48.15	160.38	42.27	17.56
168	3.36	1.40	54.36	154.62	45.18	17.73
169	3.38	1.35	62.01	151.95	47.65	17.84
170	3.40	1.34	66.32	139.49	49.07	17.92
171	3.42	1.38	67.49	128.08	49.66	17.98
172	3.44	1.39	71.35	121.64	50.19	18.02
173	3.46	1.37	74.67	118.41	51.25	18.07
174	3.48	1.35	76.37	109.98	51.87	18.09
175	3.50	1.37	76.60	105.70	51.85	18.11
176	3.52	1.39	76.80	101.30	51.66	18.13
177	3.54	1.41	80.88	100.06	51.78	18.17
178	3.56	1.42	84.04	99.07	52.47	18.22
179	3.58	1.41	87.32	99.94	53.21	18.26
180	3.60	1.40	89.69	100.00	54.25	18.29
181	3.62	1.37	91.95	105.02	54.33	18.30
182	3.64	1.41	88.90	106.94	53.95	18.29
183	3.66	1.42	87.52	110.66	53.56	18.26
184	3.68	1.36	85.21	110.97	54.28	18.23
185	3.70	1.29	83.21	112.46	55.33	18.17
186	3.72	1.26	79.02	113.33	56.67	18.11
187	3.74	1.17	75.74	117.42	57.96	18.04
188	3.76	1.10	72.51	129.51	59.41	17.97
189	3.78	1.07	69.44	139.12	60.15	17.88
190	3.80	1.02	63.54	139.06	60.19	17.80
191	3.82	1.00	59.44	140.48	59.52	17.70
192	3.84	1.01	54.90	140.98	57.96	17.62

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	1.04	51.35	146.19	52.80	17.48
194	3.88	1.19	37.38	173.96	48.75	17.37
195	3.90	1.19	39.49	139.06	46.47	17.31
196	3.92	1.15	43.30	148.54	48.19	17.36
197	3.94	1.12	44.48	164.48	49.87	17.42
198	3.96	1.11	46.53	183.32	51.32	17.45
199	3.98	1.07	47.87	195.04	52.49	17.47
200	4.01	1.05	48.23	201.36	53.63	17.48
201	4.02	1.03	48.05	206.82	54.21	17.45
202	4.04	1.00	45.82	210.85	54.89	17.40
203	4.06	0.95	43.13	215.25	55.47	17.31
204	4.08	0.91	40.14	218.97	55.45	17.23
205	4.10	0.92	37.79	220.09	55.31	17.17
206	4.12	0.90	37.35	223.31	54.87	17.13
207	4.15	0.90	36.45	224.05	55.26	17.09
208	4.16	0.86	34.72	222.07	55.66	17.05
209	4.18	0.85	34.66	225.29	56.64	17.01
210	4.20	0.81	33.72	223.68	57.62	16.95
211	4.22	0.76	30.73	226.04	58.89	16.88
212	4.24	0.74	30.44	224.05	59.96	16.80
213	4.26	0.71	28.51	222.19	60.92	16.74
214	4.28	0.68	27.30	222.57	60.16	16.67
215	4.30	0.72	25.34	225.29	57.25	16.63
216	4.32	0.81	24.37	232.05	52.62	16.59
217	4.34	0.88	22.62	233.35	50.46	16.56
218	4.36	0.83	22.67	227.59	50.33	16.53
219	4.38	0.79	22.47	224.55	51.86	16.48
220	4.40	0.76	21.21	229.88	52.26	16.42
221	4.42	0.76	19.63	236.02	51.74	16.35
222	4.44	0.77	18.98	238.50	49.33	16.34
223	4.46	0.89	19.34	247.12	44.77	16.38
224	4.48	1.11	19.63	257.22	39.79	16.46
225	4.50	1.27	19.84	238.87	37.96	16.57
226	4.52	1.21	23.47	195.60	39.43	16.70
227	4.54	1.12	27.16	173.16	44.19	16.83
228	4.56	0.96	30.36	183.94	47.23	16.91
229	4.58	1.04	30.94	240.24	47.16	16.97
230	4.60	1.17	31.38	270.68	44.50	17.03
231	4.62	1.25	32.32	228.27	44.05	17.09
232	4.64	1.16	35.14	199.13	45.50	17.10
233	4.66	1.06	33.08	187.04	48.89	17.06
234	4.68	0.94	32.38	210.97	51.26	16.95
235	4.70	0.87	28.69	260.88	52.64	16.87
236	4.72	0.88	28.05	287.85	52.06	16.80
237	4.74	0.90	27.67	304.22	50.46	16.76
238	4.76	0.94	25.18	308.74	49.12	16.72
239	4.78	0.94	24.56	308.49	47.26	16.66
240	4.80	0.99	23.04	319.03	45.80	16.62

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	1.01	22.04	322.26	45.12	16.60
242	4.84	0.97	22.86	292.81	48.38	16.63
243	4.86	0.78	26.53	255.42	48.68	16.79
244	4.88	1.16	31.54	210.35	49.56	16.95
245	4.90	1.09	34.58	213.14	48.80	17.11
246	4.92	1.01	37.34	222.19	51.87	17.17
247	4.94	0.99	39.27	230.94	53.11	17.20
248	4.96	1.03	38.16	247.74	51.63	17.20
249	4.98	1.11	35.99	253.19	47.33	17.20
250	5.00	1.33	35.23	269.50	40.65	17.20
251	5.02	1.71	32.39	238.31	32.77	17.24
252	5.04	2.30	30.89	167.39	28.02	17.36
253	5.06	2.57	39.83	115.07	28.41	17.59
254	5.08	2.15	52.43	80.91	34.05	17.83
255	5.10	1.63	64.94	64.60	42.02	17.88
256	5.12	1.38	58.90	73.16	49.44	17.85
257	5.14	1.22	58.58	158.46	52.17	17.74
258	5.16	1.20	53.69	207.75	53.38	17.69
259	5.18	1.20	54.65	214.51	53.12	17.67
260	5.20	1.20	55.18	224.74	52.42	17.67
261	5.22	1.25	52.13	235.28	50.21	17.62
262	5.24	1.34	46.94	239.93	47.68	17.58
263	5.26	1.38	47.32	241.91	45.68	17.54
264	5.28	1.40	44.72	212.28	46.03	17.55
265	5.30	1.34	48.55	202.29	48.04	17.58
266	5.32	1.24	53.47	194.36	51.91	17.65
267	5.34	1.14	57.05	187.41	56.91	17.71
268	5.36	1.03	62.15	182.33	61.85	17.76
269	5.38	0.98	65.37	181.46	66.86	17.79
270	5.40	0.89	66.45	183.20	70.16	17.76
271	5.42	0.84	61.82	186.73	72.05	17.69
272	5.44	0.83	57.57	192.44	71.14	17.59
273	5.46	0.84	51.56	210.54	68.08	17.46
274	5.48	0.87	43.10	226.10	64.27	17.30
275	5.50	0.88	37.23	248.17	59.66	17.12
276	5.52	0.91	30.85	268.88	55.33	16.97
277	5.54	0.98	28.36	285.00	51.97	16.85
278	5.56	0.97	26.27	289.71	50.56	16.78
279	5.58	0.95	25.95	291.01	51.18	16.75
280	5.60	0.91	26.86	287.97	52.55	16.78
281	5.62	0.91	28.94	288.34	54.48	16.82
282	5.64	0.87	29.70	286.48	56.08	16.85
283	5.66	0.85	29.67	282.89	57.80	16.86
284	5.68	0.83	30.35	276.81	58.14	16.89
285	5.70	0.88	31.73	283.88	55.82	16.91
286	5.72	1.00	29.91	291.94	50.90	16.93
287	5.74	1.17	28.83	287.66	43.97	16.96
288	5.76	1.50	28.80	258.71	39.48	17.04

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	1.61	31.61	177.50	38.32	17.23
290	5.80	1.62	41.54	118.29	40.77	17.45
291	5.82	1.56	50.69	90.82	44.62	17.66
292	5.84	1.48	57.78	71.48	46.10	17.82
293	5.86	1.71	63.06	65.34	46.55	17.92
294	5.88	1.68	64.90	48.30	46.01	18.00
295	5.90	1.68	67.74	39.55	45.25	18.03
296	5.92	1.87	66.02	34.97	42.44	18.07
297	5.94	2.15	66.54	31.37	38.61	18.13
298	5.96	2.42	69.59	28.02	36.13	18.19
299	5.98	2.49	70.67	24.49	34.70	18.22
300	6.00	2.55	69.15	20.52	34.21	18.19
301	6.02	2.45	63.05	15.13	34.14	18.08
302	6.04	2.26	55.26	11.97	35.41	17.94
303	6.06	1.96	51.24	9.18	38.56	17.81
304	6.08	1.65	52.50	6.14	42.12	17.76
305	6.10	1.64	53.38	15.00	42.45	17.73
306	6.12	1.88	49.10	17.61	41.16	17.76
307	6.14	1.87	53.44	15.69	42.68	17.83
308	6.16	1.55	63.72	12.77	48.91	17.91
309	6.18	1.27	69.32	9.67	58.19	17.92
310	6.20	1.06	68.12	12.28	63.62	17.82
311	6.22	1.05	54.29	45.01	64.13	17.69
312	6.24	1.10	51.91	49.97	60.32	17.59
313	6.26	1.19	52.18	50.65	58.06	17.60
314	6.28	1.20	52.17	50.59	56.54	17.60
315	6.30	1.22	50.85	51.02	56.39	17.60
316	6.32	1.21	52.41	50.96	56.12	17.60
317	6.34	1.23	51.56	51.77	55.91	17.62
318	6.36	1.26	52.84	52.32	55.35	17.67
319	6.38	1.31	57.59	52.63	55.45	17.76
320	6.40	1.33	63.07	52.57	55.57	17.84
321	6.42	1.36	64.56	52.88	55.51	17.91
322	6.44	1.40	66.91	53.56	53.36	17.96
323	6.46	1.59	67.14	56.23	50.85	18.01
324	6.48	1.70	69.22	56.91	49.04	18.06
325	6.50	1.69	71.94	56.54	49.79	18.11
326	6.52	1.60	76.69	54.87	52.55	18.17
327	6.54	1.49	82.37	53.01	56.28	18.21
328	6.56	1.41	86.68	51.52	60.36	18.26
329	6.59	1.31	91.51	49.85	63.81	18.29
330	6.60	1.27	94.18	49.16	66.72	18.31
331	6.62	1.24	96.29	48.67	68.05	18.32
332	6.64	1.24	94.76	48.61	68.76	18.30
333	6.66	1.21	91.25	48.42	68.47	18.25
334	6.68	1.21	86.12	48.17	68.49	18.18
335	6.70	1.16	81.02	47.68	68.46	18.11
336	6.72	1.13	76.91	47.06	68.80	18.05

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	1.12	75.36	46.93	68.62	18.00
338	6.76	1.12	72.49	47.55	67.87	17.96
339	6.78	1.13	68.74	48.36	66.83	17.91
340	6.80	1.14	66.77	48.79	65.47	17.87
341	6.82	1.16	64.43	48.98	64.56	17.84
342	6.84	1.15	62.02	48.73	63.93	17.80
343	6.86	1.14	60.51	53.13	65.41	17.78
344	6.88	1.06	64.02	52.26	67.99	17.80
345	6.90	1.02	66.51	52.01	72.38	17.84
346	6.92	0.95	71.20	52.08	76.57	17.87
347	6.94	0.90	73.81	52.01	80.46	17.90
348	6.96	0.88	75.45	52.20	82.41	17.91
349	6.98	0.89	75.71	53.32	81.17	17.91
350	7.00	0.95	72.55	54.74	76.68	17.89
351	7.02	1.05	66.04	56.79	70.14	17.83
352	7.04	1.16	59.65	58.77	64.02	17.76
353	7.06	1.23	55.02	59.95	59.71	17.69
354	7.08	1.26	51.95	59.83	57.74	17.64
355	7.10	1.25	52.06	59.21	57.24	17.63
356	7.12	1.26	53.35	58.90	57.94	17.67
357	7.14	1.25	56.84	58.83	59.14	17.73
358	7.16	1.24	60.74	59.02	60.28	17.81
359	7.18	1.28	65.45	59.64	61.35	17.89
360	7.20	1.28	69.76	59.89	62.30	17.95
361	7.22	1.25	71.14	58.83	63.86	17.96
362	7.25	1.19	69.70	57.53	65.21	17.97
363	7.26	1.20	72.19	57.16	66.38	17.98
364	7.28	1.19	73.80	57.47	67.68	18.01
365	7.30	1.15	76.91	57.41	68.96	18.04
366	7.32	1.15	78.11	59.14	68.50	18.05
367	7.34	1.23	75.59	60.94	66.01	18.05
368	7.36	1.32	74.03	62.49	62.00	18.05
369	7.38	1.43	71.57	63.79	58.27	18.03
370	7.40	1.50	67.09	64.66	56.20	18.01
371	7.42	1.48	69.08	64.79	56.14	18.02
372	7.44	1.44	71.63	64.35	58.43	18.05
373	7.46	1.36	76.17	62.55	61.74	18.12
374	7.48	1.32	85.69	61.56	65.41	18.19
375	7.50	1.27	90.24	60.57	68.49	18.26
376	7.52	1.25	94.54	59.52	70.53	18.31
377	7.54	1.25	98.97	59.45	71.74	18.34
378	7.56	1.23	98.38	59.76	71.68	18.34
379	7.58	1.25	94.48	60.38	70.50	18.30
380	7.60	1.28	88.97	60.76	68.37	18.26
381	7.62	1.32	84.75	61.19	66.08	18.22
382	7.64	1.37	83.11	61.81	64.12	18.18
383	7.66	1.37	78.10	62.06	62.65	18.13
384	7.68	1.37	74.87	61.93	61.87	18.09

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	1.37	73.67	61.31	62.20	18.08
386	7.72	1.34	76.89	60.51	63.70	18.11
387	7.74	1.31	82.08	59.70	65.80	18.16
388	7.76	1.28	85.30	59.08	67.75	18.20
389	7.78	1.27	88.44	58.71	69.66	18.25
390	7.80	1.24	93.42	58.28	71.50	18.29
391	7.82	1.23	97.75	57.90	71.96	18.31
392	7.84	1.27	93.22	64.91	71.39	18.31
393	7.86	1.27	91.99	64.97	69.97	18.28
394	7.88	1.28	88.33	64.91	69.38	18.24
395	7.90	1.26	84.20	64.79	69.00	18.19
396	7.92	1.24	81.21	64.23	69.61	18.14
397	7.94	1.19	80.33	63.55	70.89	18.08
398	7.96	1.12	75.58	62.12	72.98	18.01
399	7.98	1.04	70.57	60.38	75.95	17.91
400	8.00	0.94	67.58	58.71	79.90	17.81
401	8.02	0.85	63.59	57.04	84.97	17.71
402	8.04	0.76	59.79	55.36	90.54	17.60
403	8.06	0.68	56.03	53.94	96.32	17.50
404	8.08	0.63	54.30	53.32	100.00	17.38
405	8.10	0.58	48.80	52.70	100.00	17.26
406	8.12	0.57	42.79	52.51	100.00	17.11
407	8.14	0.54	38.36	52.08	100.00	16.96
408	8.16	0.48	34.85	51.52	100.00	16.80
409	8.18	0.48	29.87	52.14	100.00	16.63
410	8.20	0.52	24.33	53.38	98.13	16.45
411	8.22	0.55	21.37	54.18	91.08	16.30
412	8.24	0.55	19.26	54.99	88.21	16.18
413	8.26	0.54	18.00	55.05	87.58	16.08
414	8.28	0.52	16.71	55.86	87.94	15.97
415	8.30	0.51	14.84	56.35	88.23	15.83
416	8.32	0.49	12.70	57.78	87.23	15.68
417	8.34	0.49	11.56	60.63	84.35	15.56
418	8.36	0.52	10.88	62.80	80.74	15.52
419	8.39	0.54	10.94	64.54	77.31	15.52
420	8.40	0.57	11.15	66.58	73.83	15.57
421	8.42	0.63	11.62	68.94	70.60	15.63
422	8.44	0.66	11.94	70.06	69.10	15.72
423	8.46	0.66	13.44	69.99	71.67	15.86
424	8.48	0.61	16.34	69.56	75.32	15.96
425	8.50	0.60	16.20	70.37	78.06	16.01
426	8.52	0.61	15.99	71.61	77.74	16.01
427	8.54	0.62	16.32	72.10	77.73	16.05
428	8.56	0.62	17.58	72.60	78.09	16.08
429	8.58	0.62	17.55	73.22	79.56	16.10
430	8.60	0.59	17.32	73.09	81.30	16.04
431	8.63	0.55	15.56	74.09	82.03	15.97
432	8.64	0.57	14.80	75.51	80.98	15.87

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	0.58	13.75	78.18	76.74	15.82
434	8.68	0.63	12.93	81.22	72.27	15.79
435	8.70	0.68	12.93	82.64	68.48	15.83
436	8.72	0.72	14.25	84.56	66.83	15.90
437	8.74	0.73	14.87	86.24	66.60	15.99
438	8.76	0.74	15.72	86.73	68.28	16.10
439	8.78	0.72	18.71	86.48	69.75	16.23
440	8.80	0.75	20.58	88.47	70.39	16.36
441	8.82	0.79	21.93	89.46	68.93	16.43
442	8.84	0.81	21.96	164.85	68.09	16.53
443	8.86	0.83	25.24	166.40	68.68	16.62
444	8.88	0.81	27.35	166.58	70.62	16.72
445	8.90	0.80	28.82	167.33	73.08	16.77
446	8.92	0.76	29.17	166.77	75.90	16.81
447	8.95	0.74	31.57	168.63	77.83	16.84
448	8.96	0.75	31.89	171.23	76.87	16.86
449	8.98	0.81	29.93	178.43	73.26	16.83
450	9.00	0.85	27.62	174.21	72.22	16.81
451	9.02	0.79	30.52	166.03	74.38	16.81
452	9.04	0.72	30.60	167.27	79.29	16.82
453	9.06	0.69	30.28	168.51	82.06	16.79
454	9.08	0.69	29.81	170.99	83.00	16.76
455	9.10	0.68	28.93	173.22	82.59	16.75
456	9.12	0.70	29.31	176.63	83.25	16.70
457	9.14	0.64	26.91	173.90	84.47	16.63
458	9.16	0.61	24.62	172.54	86.88	16.50
459	9.18	0.57	21.87	172.10	89.09	16.36
460	9.20	0.53	20.14	175.45	89.51	16.23
461	9.23	0.54	17.91	180.78	87.01	16.12
462	9.24	0.58	16.30	183.51	80.86	16.03
463	9.26	0.64	15.13	188.41	75.58	15.98
464	9.28	0.66	14.69	189.71	72.34	15.93
465	9.30	0.66	14.05	188.90	72.82	15.89
466	9.32	0.61	13.87	188.10	74.77	15.82
467	9.34	0.57	12.55	189.46	75.07	15.74
468	9.36	0.62	11.73	195.60	71.55	15.70
469	9.38	0.69	11.85	200.25	68.70	15.69
470	9.40	0.66	12.00	197.21	68.09	15.80
471	9.42	0.69	14.58	199.13	67.30	15.95
472	9.44	0.80	16.57	206.01	61.90	16.13
473	9.46	0.99	17.18	217.30	53.62	16.27
474	9.48	1.23	17.33	226.78	47.41	16.37
475	9.50	1.35	18.65	144.33	46.27	16.52
476	9.52	1.26	23.19	113.89	51.47	16.66
477	9.54	0.96	26.44	85.74	62.33	16.70
478	9.56	0.71	25.92	111.22	74.77	16.65
479	9.58	0.67	25.33	143.71	83.01	16.62
480	9.60	0.67	27.47	150.53	84.49	16.62

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	0.66	26.91	159.52	83.58	16.60
482	9.64	0.68	23.72	170.61	81.04	16.50
483	9.66	0.68	20.41	173.59	77.99	16.35
484	9.68	0.68	18.04	177.87	74.18	16.20
485	9.70	0.72	15.69	186.79	69.77	16.10
486	9.72	0.78	15.22	190.70	65.30	16.03
487	9.74	0.81	14.58	193.49	64.04	16.03
488	9.76	0.78	15.25	190.76	67.35	16.09
489	9.78	0.68	18.12	188.72	70.29	16.16
490	9.80	0.75	18.36	194.85	66.81	16.65
491	9.82	1.24	38.17	139.74	62.96	17.06
492	9.84	1.22	43.41	107.63	61.34	17.38
493	9.86	1.18	45.29	108.93	64.48	17.37
494	9.88	1.04	39.86	107.75	69.12	17.27
495	9.90	0.87	36.79	105.58	75.97	17.11
496	9.92	0.74	34.74	116.55	83.82	16.99
497	9.95	0.67	33.54	127.59	90.09	16.89
498	9.96	0.63	31.72	140.24	92.23	16.78
499	9.98	0.62	27.73	149.47	92.41	16.64
500	10.00	0.60	23.60	156.85	90.17	16.45
501	10.02	0.59	19.44	160.57	86.97	16.23
502	10.04	0.60	15.83	168.69	82.27	16.04
503	10.06	0.63	14.31	176.88	77.10	15.91
504	10.08	0.67	13.49	181.90	74.72	15.88
505	10.10	0.66	14.25	184.13	73.81	15.89
506	10.12	0.66	14.37	186.61	75.12	15.92
507	10.14	0.65	14.92	189.15	75.92	15.95
508	10.16	0.65	15.28	190.02	77.10	15.98
509	10.18	0.64	15.60	190.27	77.72	16.00
510	10.20	0.64	16.01	193.74	77.99	16.02
511	10.22	0.65	16.07	195.78	77.87	16.01
512	10.24	0.64	15.22	195.91	78.85	15.99
513	10.26	0.60	15.19	196.53	79.51	15.93
514	10.28	0.60	14.05	199.07	79.95	15.88
515	10.30	0.61	13.61	201.12	79.13	15.82
516	10.32	0.60	13.11	203.22	79.09	15.81
517	10.34	0.60	13.55	204.65	79.03	15.82
518	10.36	0.62	14.13	206.94	79.09	15.86
519	10.38	0.62	14.43	209.61	78.00	15.89
520	10.40	0.64	14.16	211.66	77.31	15.90
521	10.42	0.64	14.37	213.39	76.22	15.90
522	10.44	0.65	14.16	214.69	76.21	15.93
523	10.46	0.66	15.25	215.50	76.08	15.97
524	10.48	0.66	15.66	216.68	77.32	16.02
525	10.50	0.64	16.30	216.74	78.00	16.03
526	10.52	0.64	15.78	217.79	79.23	16.00
527	10.54	0.62	14.96	218.35	79.97	15.95
528	10.56	0.59	14.28	218.91	79.50	15.88

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	0.63	13.52	224.05	76.12	15.84
530	10.60	0.69	12.88	230.56	72.01	15.84
531	10.62	0.72	13.52	230.75	70.55	15.89
532	10.64	0.70	14.87	230.69	72.25	15.98
533	10.66	0.68	16.10	229.51	74.77	16.04
534	10.68	0.67	16.13	230.19	75.29	16.08
535	10.70	0.71	16.86	234.16	72.90	16.14
536	10.72	0.79	17.59	240.36	69.37	16.21
537	10.74	0.84	18.00	242.16	66.52	16.27
538	10.76	0.87	18.56	242.47	66.49	16.35
539	10.78	0.85	21.34	239.24	68.75	16.49
540	10.80	0.82	25.63	312.71	71.52	16.63
541	10.82	0.84	27.18	286.79	74.74	16.75
542	10.84	0.78	29.59	283.08	76.75	16.81
543	10.86	0.79	30.64	294.17	77.54	16.85
544	10.88	0.83	30.14	297.09	76.64	16.86
545	10.90	0.83	30.11	294.92	76.38	16.84
546	10.92	0.79	29.32	289.15	79.56	16.82
547	10.94	0.70	29.64	285.99	82.16	16.77
548	10.96	0.71	27.48	295.91	82.24	16.68
549	10.98	0.74	23.93	301.18	78.27	16.59
550	11.00	0.78	22.43	302.48	74.68	16.51
551	11.02	0.79	21.99	302.67	74.00	16.48
552	11.04	0.75	22.17	297.27	74.49	16.44
553	11.06	0.73	20.15	299.88	74.98	16.36
554	11.08	0.74	18.54	301.24	72.63	16.29
555	11.10	0.79	17.86	307.19	69.18	16.26
556	11.12	0.85	18.15	311.66	66.21	16.27
557	11.14	0.86	17.83	310.91	66.41	16.33
558	11.16	0.82	20.47	306.51	68.15	16.38
559	11.18	0.82	21.26	305.21	70.27	16.45
560	11.20	0.82	21.73	304.77	70.92	16.50
561	11.22	0.83	23.31	306.94	71.08	16.55
562	11.24	0.84	23.69	307.13	72.16	16.59
563	11.26	0.81	24.66	303.04	75.04	16.63
564	11.28	0.74	26.21	296.78	78.86	16.62
565	11.30	0.71	24.77	296.34	81.35	16.57
566	11.32	0.70	22.40	298.64	80.61	16.48
567	11.34	0.72	20.94	302.48	77.45	16.40
568	11.36	0.76	19.71	308.93	73.71	16.35
569	11.38	0.81	19.06	312.46	70.71	16.32
570	11.40	0.82	18.65	311.53	69.53	16.34
571	11.42	0.82	20.00	310.97	69.40	16.38
572	11.44	0.84	20.73	311.10	70.63	16.44
573	11.46	0.81	22.02	309.30	72.05	16.48
574	11.48	0.79	22.43	308.18	73.92	16.52
575	11.50	0.79	23.40	307.01	74.10	16.55
576	11.52	0.82	23.87	311.22	72.92	16.57

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	0.85	23.02	314.38	70.64	16.58
578	11.56	0.89	22.96	316.24	69.17	16.58
579	11.58	0.89	23.45	315.31	68.83	16.61
580	11.60	0.89	24.69	314.76	69.24	16.66
581	11.62	0.91	25.80	314.76	69.99	16.72
582	11.64	0.91	27.64	313.14	70.68	16.79
583	11.66	0.91	29.02	312.90	71.30	16.84
584	11.68	0.92	29.75	314.82	70.99	16.88
585	11.70	0.95	30.13	316.43	69.28	16.92
586	11.72	1.02	30.69	320.33	67.77	16.96
587	11.74	1.04	32.27	321.95	66.41	17.01
588	11.76	1.07	32.86	321.70	66.54	17.06
589	11.78	1.06	34.65	317.79	67.40	17.12
590	11.80	1.05	37.34	305.58	69.83	17.18
591	11.82	1.00	39.54	302.11	72.68	17.25
592	11.84	0.98	42.12	305.64	74.69	17.29
593	11.86	0.99	42.91	309.05	75.01	17.33
594	11.88	1.01	43.14	308.12	75.52	17.35
595	11.90	0.97	44.64	304.77	76.41	17.36
596	11.92	0.96	44.11	300.50	78.25	17.36
597	11.94	0.94	45.05	298.70	78.55	17.36
598	11.96	0.96	43.96	299.13	78.75	17.35
599	11.98	0.95	43.99	299.13	78.17	17.35
600	12.00	0.96	44.23	301.61	77.53	17.36
601	12.02	1.00	44.49	306.51	76.29	17.36
602	12.04	1.01	43.49	310.48	74.62	17.35
603	12.06	1.04	42.29	310.73	73.12	17.34
604	12.08	1.06	41.85	310.73	72.02	17.34
605	12.10	1.07	42.85	311.41	71.52	17.36
606	12.12	1.09	44.05	310.23	71.46	17.40
607	12.14	1.10	45.66	309.42	71.85	17.44
608	12.16	1.10	47.71	306.20	72.95	17.50
609	12.18	1.09	51.13	304.77	74.36	17.55
610	12.20	1.08	52.69	302.67	75.39	17.59
611	12.22	1.08	53.24	302.23	75.92	17.60
612	12.24	1.07	53.01	300.19	76.16	17.60
613	12.26	1.06	52.07	298.57	76.38	17.58
614	12.28	1.06	50.92	297.95	76.02	17.55
615	12.30	1.07	48.99	298.76	75.67	17.51
616	12.32	1.05	47.29	297.02	75.45	17.47
617	12.34	1.04	46.35	295.66	75.24	17.44
618	12.36	1.06	45.82	294.54	75.57	17.44
619	12.38	1.03	46.82	296.22	75.24	17.44
620	12.40	1.06	45.91	297.83	75.06	17.43
621	12.42	1.06	45.06	299.01	73.97	17.42
622	12.44	1.08	44.77	299.50	73.34	17.41
623	12.46	1.08	44.74	300.62	72.84	17.41
624	12.48	1.09	44.94	302.05	72.22	17.42

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	1.12	44.85	303.72	71.53	17.42
626	12.52	1.12	44.27	304.71	70.80	17.44
627	12.54	1.15	46.08	305.83	70.42	17.46
628	12.56	1.16	46.93	305.33	70.68	17.51
629	12.58	1.16	49.65	302.42	71.34	17.56
630	12.60	1.17	52.14	301.74	72.54	17.62
631	12.62	1.17	55.75	302.29	73.22	17.68
632	12.64	1.18	57.62	303.78	73.59	17.74
633	12.66	1.20	59.56	303.10	73.56	17.78
634	12.68	1.22	61.64	290.27	74.52	17.84
635	12.70	1.19	66.50	286.98	76.16	17.89
636	12.72	1.17	68.90	289.27	78.25	17.93
637	12.74	1.15	70.31	291.88	78.56	17.94
638	12.76	1.19	68.31	293.18	77.68	17.94
639	12.78	1.22	67.14	295.66	74.87	17.93
640	12.80	1.31	66.47	304.77	72.47	17.93
641	12.82	1.34	65.36	288.47	70.62	17.93
642	12.84	1.34	64.86	273.71	70.31	17.93
643	12.86	1.35	67.30	267.76	71.01	17.95
644	12.88	1.32	69.26	265.28	72.36	17.98
645	12.90	1.29	70.05	259.27	73.66	18.00
646	12.92	1.30	72.51	256.85	74.19	18.02
647	12.94	1.32	72.68	255.42	74.14	18.03
648	12.96	1.31	71.92	229.76	73.37	18.02
649	12.98	1.34	69.28	224.74	73.04	17.99
650	13.00	1.32	68.38	228.21	72.40	17.96
651	13.02	1.32	65.94	220.95	72.55	17.94
652	13.04	1.31	65.91	212.52	72.81	17.93
653	13.06	1.30	67.05	211.53	73.50	17.93
654	13.08	1.28	66.67	216.62	73.43	17.93
655	13.10	1.31	65.59	214.82	73.09	17.92
656	13.12	1.31	65.29	211.72	72.44	17.91
657	13.14	1.32	64.65	211.10	72.22	17.91
658	13.16	1.33	64.65	205.64	72.37	17.91
659	13.19	1.31	65.61	203.66	72.50	17.92
660	13.20	1.33	65.96	203.16	72.55	17.93
661	13.22	1.34	66.37	200.25	72.40	17.95
662	13.24	1.35	68.48	197.27	73.03	17.97
663	13.26	1.32	70.12	188.22	74.85	17.99
664	13.28	1.26	71.91	185.99	76.94	18.00
665	13.30	1.24	71.91	173.90	78.63	18.00
666	13.32	1.23	71.96	167.58	80.08	18.00
667	13.34	1.18	72.70	168.88	81.61	17.99
668	13.36	1.15	72.75	175.02	83.13	17.97
669	13.38	1.13	69.24	169.87	84.12	17.93
670	13.40	1.10	68.21	169.00	84.50	17.89
671	13.42	1.10	66.13	170.68	85.61	17.85
672	13.44	1.05	64.55	169.50	86.74	17.81

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	1.01	61.88	174.77	87.92	17.74
674	13.48	0.99	57.51	175.51	88.48	17.66
675	13.50	0.96	53.91	174.02	88.86	17.58
676	13.52	0.93	50.71	176.13	89.33	17.49
677	13.54	0.91	46.79	177.62	90.05	17.40
678	13.56	0.87	43.83	177.25	91.02	17.30
679	13.58	0.84	41.31	178.12	92.97	17.22
680	13.60	0.80	39.58	184.62	94.63	17.14
681	13.62	0.77	37.00	189.77	95.36	17.06
682	13.64	0.77	34.27	195.66	95.16	16.97
683	13.66	0.75	31.34	198.45	93.28	16.87
684	13.68	0.77	28.71	200.87	91.63	16.80
685	13.70	0.77	28.39	202.17	90.24	16.77
686	13.72	0.77	29.00	208.68	90.34	16.75
687	13.74	0.75	27.16	210.23	91.50	16.72
688	13.76	0.73	26.98	210.66	86.60	16.57
689	13.78	0.81	18.43	325.48	83.11	16.50
690	13.80	0.80	22.07	323.00	81.02	16.44
691	13.82	0.74	23.09	326.53	85.39	16.49
692	13.84	0.70	22.62	333.97	89.30	16.46
693	13.86	0.67	21.10	335.21	91.57	16.41
694	13.88	0.65	21.16	336.76	93.55	16.36
695	13.90	0.63	20.78	341.29	93.97	16.34
696	13.92	0.64	19.78	353.01	93.42	16.27
697	13.94	0.63	17.79	362.86	90.57	16.19
698	13.96	0.66	16.53	368.38	86.91	16.10
699	13.98	0.70	15.36	371.73	82.81	16.05
700	14.00	0.73	15.10	373.84	78.67	16.02
701	14.02	0.77	14.36	378.98	76.05	16.00
702	14.04	0.77	14.19	374.58	74.41	16.00
703	14.06	0.78	14.77	380.41	73.34	16.02
704	14.08	0.82	14.77	384.75	73.08	16.05
705	14.11	0.81	15.45	376.69	74.99	16.12
706	14.12	0.75	17.50	378.55	77.72	16.15
707	14.14	0.75	16.83	387.60	79.10	16.18
708	14.16	0.78	16.97	389.15	77.76	16.19
709	14.18	0.80	17.21	389.15	77.16	16.20
710	14.20	0.78	17.47	384.38	79.25	16.22
711	14.22	0.72	18.00	378.74	82.14	16.19
712	14.24	0.69	16.51	378.86	84.19	16.14
713	14.26	0.70	16.07	383.38	82.46	16.09
714	14.28	0.74	15.77	391.51	80.01	16.10
715	14.30	0.77	16.19	392.37	77.39	16.15
716	14.32	0.81	17.59	394.17	76.32	16.19
717	14.34	0.80	16.95	393.74	75.77	16.21
718	14.36	0.80	16.89	390.14	76.22	16.22
719	14.38	0.81	18.09	391.82	75.38	16.23
720	14.40	0.84	17.33	395.91	73.96	16.25

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	0.87	17.30	398.26	72.13	16.25
722	14.44	0.88	17.62	400.99	71.24	16.25
723	14.46	0.88	17.15	403.60	70.62	16.25
724	14.48	0.89	16.80	404.15	69.61	16.27
725	14.50	0.94	18.18	405.46	69.58	16.30
726	14.52	0.91	18.65	400.87	72.17	16.38
727	14.54	0.83	20.85	390.70	75.04	16.43
728	14.56	0.85	21.23	397.46	76.90	16.50
729	14.58	0.88	22.66	398.88	76.10	16.56
730	14.60	0.90	23.90	396.96	76.42	16.65
731	14.62	0.90	26.44	399.63	75.61	16.68
732	14.64	0.94	23.95	397.64	74.66	16.68
733	14.66	0.95	23.75	400.43	72.49	16.61
734	14.68	0.95	21.79	405.64	71.08	16.59
735	14.70	0.99	22.23	404.65	70.71	16.61
736	14.72	0.98	24.86	404.03	71.41	16.69
737	14.74	0.98	26.59	402.85	78.49	16.84
738	14.76	0.78	34.25	408.31	80.67	16.96
739	14.79	0.98	34.36	415.75	81.97	17.04
740	14.80	0.99	33.28	413.95	77.95	17.06
741	14.82	0.97	34.07	406.26	78.61	17.05
742	14.84	0.95	33.90	402.73	79.86	17.06
743	14.86	0.95	34.42	397.46	81.13	17.08
744	14.88	0.93	36.27	396.40	81.94	17.10
745	14.90	0.93	35.74	393.74	83.04	17.11
746	14.92	0.91	35.59	388.10	84.61	17.10
747	14.94	0.87	36.12	382.77	86.99	17.08
748	14.96	0.84	34.98	378.67	89.61	17.05
749	14.99	0.81	34.36	376.63	92.29	17.00
750	15.00	0.76	33.48	373.65	93.45	16.94
751	15.02	0.77	30.76	378.24	93.02	16.89
752	15.04	0.79	29.64	381.03	90.92	16.81
753	15.06	0.78	27.30	381.65	89.05	16.74
754	15.08	0.78	25.22	377.31	88.25	16.66
755	15.10	0.77	24.54	377.87	87.75	16.59
756	15.12	0.76	22.76	379.29	87.86	16.52
757	15.14	0.75	21.64	379.60	86.39	16.48
758	15.16	0.79	21.88	386.36	82.33	16.46
759	15.18	0.88	20.65	396.47	77.09	16.47
760	15.20	0.94	20.41	405.02	72.19	16.46
761	15.22	0.99	20.03	407.44	69.08	16.45
762	15.24	1.02	19.41	407.94	67.57	16.46
763	15.26	1.02	20.06	403.22	67.85	16.49
764	15.28	1.00	21.47	397.33	69.11	16.55
765	15.30	1.00	22.78	398.20	69.98	16.62
766	15.32	1.03	24.16	399.63	70.28	16.71
767	15.34	1.06	26.97	396.34	71.32	16.84
768	15.36	1.05	30.58	394.73	73.43	16.94

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	1.02	32.28	387.29	77.21	17.02
770	15.40	0.95	34.36	380.10	78.94	17.05
771	15.42	1.00	33.98	386.86	77.79	17.08
772	15.44	1.09	33.95	396.78	73.78	17.11
773	15.46	1.16	34.36	399.69	70.45	17.14
774	15.48	1.21	35.15	398.26	67.54	17.19
775	15.50	1.31	36.29	404.71	64.05	17.25
776	15.52	1.49	36.96	271.23	60.16	17.31
777	15.54	1.63	37.84	191.32	56.14	17.40
778	15.56	1.85	41.56	136.08	55.02	17.52
779	15.58	1.81	47.74	88.84	57.82	17.62
780	15.60	1.51	50.44	76.88	65.40	17.62
781	15.62	1.20	48.04	87.60	75.13	17.51
782	15.64	1.05	42.85	110.11	83.96	17.35
783	15.66	0.92	38.48	124.98	90.99	17.18
784	15.68	0.81	35.76	133.35	97.92	17.04
785	15.70	0.74	33.24	147.55	100.00	16.91
786	15.72	0.71	29.87	171.54	100.00	16.83
787	15.74	0.73	25.15	193.92	100.00	16.66

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.29	0.00	0.29	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
2	0.04	0.59	0.00	0.59	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
3	0.06	0.90	0.00	0.90	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
4	0.08	1.21	0.00	1.21	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
5	0.10	1.53	0.00	1.53	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
6	0.12	1.86	0.00	1.86	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
7	0.15	2.36	0.00	2.36	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
8	0.16	2.53	0.00	2.53	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
9	0.18	2.87	0.00	2.87	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
10	0.20	3.20	0.00	3.20	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
11	0.22	3.53	0.00	3.53	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
12	0.24	3.86	0.00	3.86	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
13	0.26	4.19	0.00	4.19	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
14	0.28	4.51	0.00	4.51	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
15	0.30	4.84	0.00	4.84	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
16	0.32	5.16	0.00	5.16	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
17	0.34	5.49	0.00	5.49	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
18	0.36	5.82	0.00	5.82	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
19	0.38	6.15	0.00	6.15	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
20	0.41	6.65	0.00	6.65	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
21	0.42	6.82	0.00	6.82	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
22	0.44	7.16	0.00	7.16	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
23	0.46	7.50	0.00	7.50	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
24	0.48	7.84	0.00	7.84	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
25	0.50	8.19	0.00	8.19	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
26	0.52	8.54	0.00	8.54	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
27	0.54	8.89	0.00	8.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
28	0.56	9.25	0.00	9.25	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
29	0.58	9.60	0.00	9.60	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
30	0.60	9.95	0.00	9.95	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
31	0.62	10.31	0.00	10.31	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
32	0.64	10.67	0.00	10.67	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
33	0.66	11.02	0.00	11.02	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
34	0.68	11.38	0.00	11.38	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
35	0.70	11.73	0.00	11.73	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
36	0.72	12.09	0.00	12.09	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
37	0.74	12.45	0.00	12.45	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
38	0.76	12.80	0.00	12.80	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
39	0.78	13.16	0.00	13.16	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
40	0.80	13.52	0.00	13.52	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
41	0.82	13.88	0.00	13.88	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
42	0.84	14.24	0.00	14.24	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
43	0.86	14.61	0.00	14.61	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
44	0.88	14.97	0.00	14.97	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
45	0.90	15.33	0.00	15.33	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
46	0.92	15.69	0.00	15.69	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
47	0.94	16.06	0.00	16.06	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
48	0.96	16.42	0.00	16.42	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.99	16.97	0.00	16.97	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
50	1.00	17.15	0.00	17.15	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
51	1.02	17.51	0.00	17.51	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
52	1.05	18.06	0.00	18.06	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
53	1.07	18.43	0.00	18.43	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
54	1.08	18.61	0.00	18.61	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
55	1.10	18.97	0.00	18.97	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
56	1.12	19.34	0.00	19.34	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
57	1.14	19.71	0.00	19.71	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
58	1.16	20.07	0.00	20.07	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
59	1.18	20.44	0.00	20.44	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
60	1.20	20.81	0.00	20.81	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
61	1.22	21.17	0.00	21.17	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
62	1.24	21.53	0.00	21.53	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
63	1.26	21.90	0.00	21.90	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
64	1.28	22.26	0.00	22.26	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
65	1.30	22.62	0.00	22.62	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
66	1.32	22.98	0.00	22.98	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
67	1.34	23.34	0.00	23.34	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
68	1.36	23.69	0.00	23.69	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
69	1.38	24.05	0.00	24.05	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
70	1.40	24.40	0.00	24.40	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
71	1.42	24.76	0.00	24.76	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
72	1.44	25.11	0.00	25.11	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
73	1.46	25.46	0.00	25.46	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
74	1.48	25.82	0.00	25.82	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
75	1.50	26.17	0.00	26.17	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
76	1.52	26.53	0.00	26.53	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
77	1.54	26.89	0.00	26.89	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
78	1.56	27.25	0.00	27.25	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
79	1.58	27.61	0.00	27.61	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
80	1.60	27.97	0.00	27.97	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
81	1.62	28.33	0.00	28.33	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
82	1.64	28.69	0.00	28.69	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
83	1.66	29.05	0.00	29.05	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
84	1.68	29.42	0.00	29.42	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
85	1.70	29.78	0.00	29.78	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
86	1.72	30.14	0.00	30.14	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
87	1.74	30.51	0.00	30.51	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
88	1.76	30.87	0.00	30.87	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
89	1.78	31.24	0.00	31.24	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
90	1.80	31.60	0.00	31.60	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
91	1.82	31.97	0.00	31.97	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
92	1.84	32.33	0.00	32.33	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
93	1.86	32.70	0.00	32.70	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
94	1.88	33.07	0.00	33.07	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
95	1.90	33.43	0.00	33.43	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
96	1.92	33.80	0.00	33.80	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	34.17	0.00	34.17	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
98	1.96	34.53	0.00	34.53	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
99	1.98	34.90	0.00	34.90	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
100	2.00	35.27	0.00	35.27	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
101	2.02	35.63	0.20	35.44	0.98	0.141	1.43	0.098	1.10	1.00	0.117	No
102	2.04	36.00	0.39	35.61	0.98	0.141	1.43	0.099	1.10	1.00	0.117	No
103	2.06	36.36	0.59	35.77	0.98	0.142	1.43	0.099	1.10	1.00	0.118	No
104	2.08	36.73	0.78	35.94	0.98	0.143	1.43	0.100	1.10	1.00	0.118	No
105	2.10	37.09	0.98	36.11	0.98	0.144	1.43	0.100	1.10	1.00	0.119	No
106	2.12	37.45	1.18	36.27	0.98	0.144	1.43	0.101	1.09	1.00	0.120	No
107	2.14	37.81	1.37	36.44	0.98	0.145	1.43	0.101	1.09	1.00	0.121	No
108	2.16	38.17	1.57	36.60	0.98	0.146	1.43	0.102	1.09	1.00	0.122	No
109	2.18	38.54	1.77	36.77	0.98	0.146	1.43	0.102	1.09	1.00	0.122	No
110	2.20	38.90	1.96	36.94	0.98	0.147	1.43	0.103	1.09	1.00	0.123	No
111	2.22	39.26	2.16	37.10	0.98	0.148	1.43	0.103	1.09	1.00	0.124	No
112	2.24	39.62	2.35	37.27	0.97	0.148	1.43	0.104	1.09	1.00	0.124	No
113	2.26	39.98	2.55	37.43	0.97	0.149	1.43	0.104	1.09	1.00	0.125	No
114	2.28	40.34	2.75	37.60	0.97	0.149	1.43	0.105	1.09	1.00	0.126	No
115	2.30	40.70	2.94	37.76	0.97	0.150	1.43	0.105	1.09	1.00	0.126	No
116	2.32	41.06	3.14	37.92	0.97	0.151	1.43	0.106	1.09	1.00	0.127	No
117	2.35	41.60	3.43	38.17	0.97	0.152	1.43	0.106	1.09	1.00	0.128	No
118	2.36	41.78	3.53	38.25	0.97	0.152	1.43	0.106	1.09	1.00	0.128	No
119	2.38	42.14	3.73	38.41	0.97	0.153	1.43	0.107	1.09	1.00	0.128	No
120	2.40	42.50	3.92	38.58	0.97	0.153	1.43	0.107	1.09	1.00	0.129	No
121	2.42	42.87	4.12	38.75	0.97	0.154	1.43	0.108	1.09	1.00	0.129	No
122	2.44	43.23	4.32	38.91	0.97	0.154	1.43	0.108	1.09	1.00	0.130	No
123	2.46	43.59	4.51	39.08	0.97	0.155	1.43	0.108	1.09	1.00	0.130	No
124	2.48	43.96	4.71	39.25	0.97	0.155	1.43	0.109	1.09	1.00	0.131	No
125	2.50	44.32	4.91	39.42	0.97	0.156	1.43	0.109	1.09	1.00	0.131	No
126	2.52	44.69	5.10	39.59	0.97	0.157	1.43	0.110	1.09	1.00	0.132	No
127	2.54	45.05	5.30	39.76	0.97	0.157	1.43	0.110	1.09	1.00	0.132	No
128	2.56	45.42	5.49	39.93	0.97	0.158	1.43	0.110	1.09	1.00	0.132	No
129	2.58	45.79	5.69	40.10	0.97	0.158	1.43	0.111	1.09	1.00	0.133	No
130	2.60	46.15	5.89	40.27	0.97	0.159	1.43	0.111	1.09	1.00	0.133	No
131	2.62	46.52	6.08	40.44	0.97	0.159	1.43	0.111	1.09	1.00	0.133	No
132	2.64	46.89	6.28	40.61	0.97	0.160	1.43	0.112	1.08	1.00	0.134	No
133	2.66	47.26	6.47	40.79	0.97	0.160	1.43	0.112	1.08	1.00	0.135	No
134	2.68	47.63	6.67	40.96	0.97	0.161	1.43	0.113	1.08	1.00	0.135	No
135	2.70	48.00	6.87	41.13	0.97	0.161	1.43	0.113	1.08	1.00	0.136	No
136	2.72	48.36	7.06	41.30	0.97	0.162	1.43	0.113	1.08	1.00	0.137	No
137	2.74	48.73	7.26	41.47	0.97	0.162	1.43	0.114	1.08	1.00	0.138	No
138	2.76	49.09	7.46	41.64	0.97	0.163	1.43	0.114	1.08	1.00	0.138	No
139	2.78	49.46	7.65	41.80	0.97	0.163	1.43	0.114	1.08	1.00	0.140	No
140	2.80	49.82	7.85	41.97	0.97	0.164	1.43	0.115	1.08	1.00	0.140	No
141	2.82	50.18	8.04	42.14	0.96	0.164	1.43	0.115	1.07	1.00	0.141	No
142	2.84	50.54	8.24	42.30	0.96	0.165	1.43	0.115	1.07	1.00	0.142	No
143	2.86	50.90	8.44	42.46	0.96	0.165	1.43	0.116	1.07	1.00	0.143	No
144	2.88	51.25	8.63	42.62	0.96	0.166	1.43	0.116	1.07	1.00	0.144	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	51.60	8.83	42.77	0.96	0.166	1.43	0.116	1.07	1.00	0.144	No
146	2.92	51.95	9.03	42.93	0.96	0.167	1.43	0.117	1.07	1.00	0.145	No
147	2.95	52.47	9.32	43.15	0.96	0.167	1.43	0.117	1.07	1.00	0.146	No
148	2.96	52.64	9.42	43.22	0.96	0.168	1.43	0.117	1.07	1.00	0.146	No
149	2.98	52.97	9.61	43.36	0.96	0.168	1.43	0.118	1.07	1.00	0.146	No
150	3.00	53.31	9.81	43.50	0.96	0.169	1.43	0.118	1.07	1.00	0.147	No
151	3.02	53.64	10.01	43.63	0.96	0.169	1.43	0.118	1.07	1.00	0.147	No
152	3.04	53.97	10.20	43.77	0.96	0.169	1.43	0.119	1.07	1.00	0.148	No
153	3.06	54.30	10.40	43.90	0.96	0.170	1.43	0.119	1.07	1.00	0.148	No
154	3.08	54.62	10.59	44.03	0.96	0.170	1.43	0.119	1.07	1.00	0.149	No
155	3.10	54.95	10.79	44.16	0.96	0.171	1.43	0.120	1.07	1.00	0.149	No
156	3.12	55.27	10.99	44.29	0.96	0.171	1.43	0.120	1.07	1.00	0.149	No
157	3.14	55.60	11.18	44.41	0.96	0.172	1.43	0.120	1.07	1.00	0.149	No
158	3.16	55.92	11.38	44.54	0.96	0.172	1.43	0.120	1.07	1.00	0.150	No
159	3.18	56.25	11.58	44.67	0.96	0.173	1.43	0.121	1.07	1.00	0.150	No
160	3.20	56.58	11.77	44.80	0.96	0.173	1.43	0.121	1.07	1.00	0.150	No
161	3.22	56.91	11.97	44.94	0.96	0.173	1.43	0.121	1.07	1.00	0.150	No
162	3.24	57.24	12.16	45.08	0.96	0.174	1.43	0.122	1.07	1.00	0.150	No
163	3.26	57.58	12.36	45.22	0.96	0.174	1.43	0.122	1.07	1.00	0.150	No
164	3.28	57.92	12.56	45.36	0.96	0.175	1.43	0.122	1.07	1.00	0.150	No
165	3.30	58.26	12.75	45.51	0.96	0.175	1.43	0.123	1.07	1.00	0.150	No
166	3.32	58.61	12.95	45.66	0.96	0.175	1.43	0.123	1.07	1.00	0.150	No
167	3.34	58.96	13.15	45.82	0.96	0.176	1.43	0.123	1.07	1.00	0.150	No
168	3.36	59.32	13.34	45.98	0.95	0.176	1.43	0.123	1.07	1.00	0.150	No
169	3.38	59.67	13.54	46.14	0.95	0.177	1.43	0.124	1.07	1.00	0.151	No
170	3.40	60.03	13.73	46.30	0.95	0.177	1.43	0.124	1.07	1.00	0.151	No
171	3.42	60.39	13.93	46.46	0.95	0.177	1.43	0.124	1.07	1.00	0.151	No
172	3.44	60.75	14.13	46.63	0.95	0.178	1.43	0.124	1.07	1.00	0.152	No
173	3.46	61.11	14.32	46.79	0.95	0.178	1.43	0.125	1.07	1.00	0.152	No
174	3.48	61.48	14.52	46.96	0.95	0.178	1.43	0.125	1.07	1.00	0.153	No
175	3.50	61.84	14.72	47.12	0.95	0.179	1.43	0.125	1.07	1.00	0.153	No
176	3.52	62.20	14.91	47.29	0.95	0.179	1.43	0.125	1.07	1.00	0.153	No
177	3.54	62.56	15.11	47.46	0.95	0.179	1.43	0.126	1.07	1.00	0.153	No
178	3.56	62.93	15.30	47.63	0.95	0.180	1.43	0.126	1.07	1.00	0.154	No
179	3.58	63.29	15.50	47.79	0.95	0.180	1.43	0.126	1.07	1.00	0.154	No
180	3.60	63.66	15.70	47.96	0.95	0.180	1.43	0.126	1.07	1.00	0.154	No
181	3.62	64.03	15.89	48.13	0.95	0.181	1.43	0.126	1.07	1.00	0.155	No
182	3.64	64.39	16.09	48.30	0.95	0.181	1.43	0.127	1.07	1.00	0.155	No
183	3.66	64.76	16.28	48.47	0.95	0.181	1.43	0.127	1.07	1.00	0.155	No
184	3.68	65.12	16.48	48.64	0.95	0.182	1.43	0.127	1.07	1.00	0.156	No
185	3.70	65.49	16.68	48.81	0.95	0.182	1.43	0.127	1.07	1.00	0.157	No
186	3.72	65.85	16.87	48.97	0.95	0.182	1.43	0.128	1.06	1.00	0.157	No
187	3.74	66.21	17.07	49.14	0.95	0.183	1.43	0.128	1.06	1.00	0.158	No
188	3.76	66.57	17.27	49.30	0.95	0.183	1.43	0.128	1.06	1.00	0.159	No
189	3.78	66.93	17.46	49.46	0.95	0.183	1.43	0.128	1.06	1.00	0.159	No
190	3.80	67.28	17.66	49.62	0.95	0.184	1.43	0.128	1.06	1.00	0.160	No
191	3.82	67.64	17.85	49.78	0.95	0.184	1.43	0.129	1.06	1.00	0.160	No
192	3.84	67.99	18.05	49.94	0.95	0.184	1.43	0.129	1.06	1.00	0.160	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	68.34	18.25	50.09	0.95	0.184	1.43	0.129	1.06	1.00	0.161	No
194	3.88	68.68	18.44	50.24	0.94	0.185	1.43	0.129	1.06	1.00	0.160	No
195	3.90	69.03	18.64	50.39	0.94	0.185	1.43	0.130	1.06	1.00	0.161	No
196	3.92	69.38	18.84	50.54	0.94	0.185	1.43	0.130	1.06	1.00	0.161	No
197	3.94	69.73	19.03	50.69	0.94	0.186	1.43	0.130	1.06	1.00	0.161	No
198	3.96	70.08	19.23	50.85	0.94	0.186	1.43	0.130	1.06	1.00	0.162	No
199	3.98	70.42	19.42	51.00	0.94	0.186	1.43	0.130	1.06	1.00	0.162	No
200	4.01	70.95	19.72	51.23	0.94	0.187	1.43	0.131	1.06	1.00	0.163	No
201	4.02	71.12	19.82	51.31	0.94	0.187	1.43	0.131	1.06	1.00	0.163	No
202	4.04	71.47	20.01	51.46	0.94	0.187	1.43	0.131	1.06	1.00	0.163	No
203	4.06	71.82	20.21	51.61	0.94	0.187	1.43	0.131	1.06	1.00	0.164	No
204	4.08	72.16	20.40	51.76	0.94	0.188	1.43	0.131	1.06	1.00	0.164	No
205	4.10	72.51	20.60	51.90	0.94	0.188	1.43	0.132	1.06	1.00	0.165	No
206	4.12	72.85	20.80	52.05	0.94	0.188	1.43	0.132	1.06	1.00	0.165	No
207	4.15	73.36	21.09	52.27	0.94	0.189	1.43	0.132	1.06	1.00	0.165	No
208	4.16	73.53	21.19	52.34	0.94	0.189	1.43	0.132	1.06	1.00	0.166	No
209	4.18	73.87	21.39	52.49	0.94	0.189	1.43	0.132	1.05	1.00	0.166	No
210	4.20	74.21	21.58	52.63	0.94	0.189	1.43	0.132	1.05	1.00	0.167	No
211	4.22	74.55	21.78	52.77	0.94	0.190	1.43	0.133	1.05	1.00	0.167	No
212	4.24	74.88	21.97	52.91	0.94	0.190	1.43	0.133	1.05	1.00	0.167	No
213	4.26	75.22	22.17	53.05	0.94	0.190	1.43	0.133	1.05	1.00	0.168	No
214	4.28	75.55	22.37	53.19	0.94	0.190	1.43	0.133	1.05	1.00	0.168	No
215	4.30	75.89	22.56	53.32	0.94	0.191	1.43	0.133	1.05	1.00	0.168	No
216	4.32	76.22	22.76	53.46	0.94	0.191	1.43	0.134	1.05	1.00	0.168	No
217	4.34	76.55	22.96	53.59	0.94	0.191	1.43	0.134	1.05	1.00	0.168	No
218	4.36	76.88	23.15	53.73	0.94	0.191	1.43	0.134	1.05	1.00	0.169	No
219	4.38	77.21	23.35	53.86	0.93	0.192	1.43	0.134	1.05	1.00	0.169	No
220	4.40	77.54	23.54	53.99	0.93	0.192	1.43	0.134	1.05	1.00	0.170	No
221	4.42	77.86	23.74	54.12	0.93	0.192	1.43	0.135	1.05	1.00	0.170	No
222	4.44	78.19	23.94	54.25	0.93	0.192	1.43	0.135	1.05	1.00	0.170	No
223	4.46	78.52	24.13	54.39	0.93	0.193	1.43	0.135	1.05	1.00	0.170	No
224	4.48	78.85	24.33	54.52	0.93	0.193	1.43	0.135	1.05	1.00	0.170	No
225	4.50	79.18	24.53	54.65	0.93	0.193	1.43	0.135	1.05	1.00	0.169	No
226	4.52	79.51	24.72	54.79	0.93	0.193	1.43	0.135	1.05	1.00	0.170	No
227	4.54	79.85	24.92	54.93	0.93	0.194	1.43	0.136	1.05	1.00	0.170	No
228	4.56	80.19	25.11	55.07	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
229	4.58	80.53	25.31	55.22	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
230	4.60	80.87	25.51	55.36	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
231	4.62	81.21	25.70	55.51	0.93	0.195	1.43	0.136	1.05	1.00	0.170	No
232	4.64	81.55	25.90	55.65	0.93	0.195	1.43	0.136	1.05	1.00	0.171	No
233	4.66	81.89	26.09	55.80	0.93	0.195	1.43	0.137	1.05	1.00	0.172	No
234	4.68	82.23	26.29	55.94	0.93	0.195	1.43	0.137	1.05	1.00	0.172	No
235	4.70	82.57	26.49	56.08	0.93	0.195	1.43	0.137	1.05	1.00	0.173	No
236	4.72	82.90	26.68	56.22	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
237	4.74	83.24	26.88	56.36	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
238	4.76	83.57	27.08	56.50	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
239	4.78	83.91	27.27	56.64	0.93	0.196	1.43	0.137	1.05	1.00	0.174	No
240	4.80	84.24	27.47	56.77	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	84.57	27.66	56.91	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
242	4.84	84.90	27.86	57.04	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
243	4.86	85.24	28.06	57.18	0.93	0.197	1.43	0.138	1.05	1.00	0.175	No
244	4.88	85.58	28.25	57.33	0.92	0.197	1.43	0.138	1.05	1.00	0.174	No
245	4.90	85.92	28.45	57.47	0.92	0.198	1.43	0.138	1.05	1.00	0.174	No
246	4.92	86.27	28.65	57.62	0.92	0.198	1.43	0.138	1.05	1.00	0.175	No
247	4.94	86.61	28.84	57.77	0.92	0.198	1.43	0.139	1.05	1.00	2.000	Yes
248	4.96	86.95	29.04	57.92	0.92	0.198	1.43	0.139	1.05	1.00	2.000	Yes
249	4.98	87.30	29.23	58.06	0.92	0.198	1.43	0.139	1.05	1.00	2.000	Yes
250	5.00	87.64	29.43	58.21	0.92	0.199	1.43	0.139	1.05	1.00	2.000	Yes
251	5.02	87.99	29.63	58.36	0.92	0.199	1.43	0.139	1.05	1.00	2.000	Yes
252	5.04	88.33	29.82	58.51	0.92	0.199	1.43	0.139	1.05	1.00	2.000	Yes
253	5.06	88.68	30.02	58.67	0.92	0.199	1.43	0.139	1.05	1.00	2.000	Yes
254	5.08	89.04	30.21	58.83	0.92	0.199	1.43	0.139	1.05	1.00	2.000	Yes
255	5.10	89.40	30.41	58.99	0.92	0.199	1.43	0.140	1.05	1.00	2.000	Yes
256	5.12	89.76	30.61	59.15	0.92	0.200	1.43	0.140	1.05	1.00	2.000	Yes
257	5.14	90.11	30.80	59.31	0.92	0.200	1.43	0.140	1.05	1.00	2.000	Yes
258	5.16	90.46	31.00	59.47	0.92	0.200	1.43	0.140	1.05	1.00	0.176	No
259	5.18	90.82	31.20	59.62	0.92	0.200	1.43	0.140	1.05	1.00	0.176	No
260	5.20	91.17	31.39	59.78	0.92	0.200	1.43	0.140	1.05	1.00	0.177	No
261	5.22	91.52	31.59	59.94	0.92	0.200	1.43	0.140	1.05	1.00	0.177	No
262	5.24	91.88	31.78	60.09	0.92	0.201	1.43	0.140	1.05	1.00	0.176	No
263	5.26	92.23	31.98	60.25	0.92	0.201	1.43	0.140	1.05	1.00	0.176	No
264	5.28	92.58	32.18	60.40	0.92	0.201	1.43	0.141	1.05	1.00	0.176	No
265	5.30	92.93	32.37	60.56	0.92	0.201	1.43	0.141	1.04	1.00	0.177	No
266	5.32	93.28	32.57	60.71	0.92	0.201	1.43	0.141	1.04	1.00	0.177	No
267	5.34	93.64	32.77	60.87	0.92	0.201	1.43	0.141	1.04	1.00	0.178	No
268	5.36	93.99	32.96	61.03	0.91	0.201	1.43	0.141	1.04	1.00	0.179	No
269	5.38	94.35	33.16	61.19	0.91	0.202	1.43	0.141	1.04	1.00	0.179	No
270	5.40	94.70	33.35	61.35	0.91	0.202	1.43	0.141	1.04	1.00	0.180	No
271	5.42	95.06	33.55	61.51	0.91	0.202	1.43	0.141	1.04	1.00	0.180	No
272	5.44	95.41	33.75	61.66	0.91	0.202	1.43	0.141	1.04	1.00	0.180	No
273	5.46	95.76	33.94	61.81	0.91	0.202	1.43	0.141	1.04	1.00	0.180	No
274	5.48	96.10	34.14	61.96	0.91	0.202	1.43	0.142	1.04	1.00	0.180	No
275	5.50	96.45	34.34	62.11	0.91	0.202	1.43	0.142	1.04	1.00	0.181	No
276	5.52	96.79	34.53	62.25	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
277	5.54	97.12	34.73	62.39	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
278	5.56	97.46	34.92	62.53	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
279	5.58	97.79	35.12	62.67	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
280	5.60	98.13	35.32	62.81	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
281	5.62	98.46	35.51	62.95	0.91	0.203	1.43	0.142	1.04	1.00	0.181	No
282	5.64	98.80	35.71	63.09	0.91	0.203	1.43	0.142	1.04	1.00	0.182	No
283	5.66	99.14	35.90	63.23	0.91	0.204	1.43	0.143	1.04	1.00	0.182	No
284	5.68	99.48	36.10	63.38	0.91	0.204	1.43	0.143	1.04	1.00	0.182	No
285	5.70	99.81	36.30	63.52	0.91	0.204	1.43	0.143	1.04	1.00	0.182	No
286	5.72	100.15	36.49	63.66	0.91	0.204	1.43	0.143	1.04	1.00	0.182	No
287	5.74	100.49	36.69	63.80	0.91	0.204	1.43	0.143	1.04	1.00	0.182	No
288	5.76	100.83	36.89	63.95	0.91	0.204	1.43	0.143	1.04	1.00	0.180	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	101.18	37.08	64.10	0.91	0.204	1.43	0.143	1.04	1.00	0.180	No
290	5.80	101.53	37.28	64.25	0.91	0.205	1.43	0.143	1.04	1.00	0.180	No
291	5.82	101.88	37.47	64.41	0.90	0.205	1.43	0.143	1.04	1.00	0.180	No
292	5.84	102.24	37.67	64.57	0.90	0.205	1.43	0.143	1.04	1.00	0.181	No
293	5.86	102.60	37.87	64.73	0.90	0.205	1.43	0.143	1.04	1.00	0.180	No
294	5.88	102.96	38.06	64.89	0.90	0.205	1.43	0.143	1.04	1.00	0.180	No
295	5.90	103.32	38.26	65.06	0.90	0.205	1.43	0.144	1.04	1.00	0.180	No
296	5.92	103.68	38.46	65.22	0.90	0.205	1.43	0.144	1.04	1.00	0.180	No
297	5.94	104.04	38.65	65.39	0.90	0.205	1.43	0.144	1.04	1.00	0.178	No
298	5.96	104.40	38.85	65.56	0.90	0.205	1.43	0.144	1.04	1.00	0.177	No
299	5.98	104.77	39.04	65.72	0.90	0.205	1.43	0.144	1.04	1.00	0.177	No
300	6.00	105.13	39.24	65.89	0.90	0.206	1.43	0.144	1.04	1.00	0.177	No
301	6.02	105.49	39.44	66.06	0.90	0.206	1.43	0.144	1.04	1.00	0.178	No
302	6.04	105.85	39.63	66.22	0.90	0.206	1.43	0.144	1.04	1.00	0.179	No
303	6.06	106.21	39.83	66.38	0.90	0.206	1.43	0.144	1.04	1.00	0.180	No
304	6.08	106.56	40.02	66.54	0.90	0.206	1.43	0.144	1.04	1.00	0.182	No
305	6.10	106.92	40.22	66.70	0.90	0.206	1.43	0.144	1.04	1.00	0.182	No
306	6.12	107.27	40.42	66.86	0.90	0.206	1.43	0.144	1.04	1.00	0.181	No
307	6.14	107.63	40.61	67.02	0.90	0.206	1.43	0.144	1.04	1.00	0.181	No
308	6.16	107.99	40.81	67.18	0.90	0.206	1.43	0.144	1.04	1.00	0.182	No
309	6.18	108.35	41.01	67.34	0.90	0.206	1.43	0.144	1.04	1.00	0.184	No
310	6.20	108.70	41.20	67.50	0.90	0.206	1.43	0.144	1.03	1.00	0.185	No
311	6.22	109.06	41.40	67.66	0.90	0.206	1.43	0.145	1.03	1.00	0.185	No
312	6.24	109.41	41.59	67.81	0.90	0.207	1.43	0.145	1.03	1.00	0.185	No
313	6.26	109.76	41.79	67.97	0.89	0.207	1.43	0.145	1.03	1.00	0.184	No
314	6.28	110.11	41.99	68.13	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
315	6.30	110.46	42.18	68.28	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
316	6.32	110.82	42.38	68.44	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
317	6.34	111.17	42.58	68.59	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
318	6.36	111.52	42.77	68.75	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
319	6.38	111.88	42.97	68.91	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
320	6.40	112.23	43.16	69.07	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
321	6.42	112.59	43.36	69.23	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
322	6.44	112.95	43.56	69.40	0.89	0.207	1.43	0.145	1.03	1.00	0.185	No
323	6.46	113.31	43.75	69.56	0.89	0.207	1.43	0.145	1.03	1.00	0.184	No
324	6.48	113.67	43.95	69.72	0.89	0.208	1.43	0.145	1.03	1.00	0.184	No
325	6.50	114.04	44.15	69.89	0.89	0.208	1.43	0.145	1.03	1.00	0.184	No
326	6.52	114.40	44.34	70.06	0.89	0.208	1.43	0.145	1.03	1.00	0.184	No
327	6.54	114.76	44.54	70.23	0.89	0.208	1.43	0.145	1.03	1.00	0.185	No
328	6.56	115.13	44.73	70.39	0.89	0.208	1.43	0.145	1.03	1.00	0.185	No
329	6.59	115.68	45.03	70.65	0.89	0.208	1.43	0.145	1.03	1.00	0.186	No
330	6.60	115.86	45.13	70.73	0.89	0.208	1.43	0.145	1.03	1.00	0.186	No
331	6.62	116.23	45.32	70.90	0.89	0.208	1.43	0.146	1.03	1.00	0.186	No
332	6.64	116.59	45.52	71.07	0.89	0.208	1.43	0.146	1.03	1.00	0.186	No
333	6.66	116.96	45.71	71.24	0.89	0.208	1.43	0.146	1.03	1.00	0.186	No
334	6.68	117.32	45.91	71.41	0.89	0.208	1.43	0.146	1.03	1.00	0.187	No
335	6.70	117.68	46.11	71.58	0.89	0.208	1.43	0.146	1.03	1.00	0.187	No
336	6.72	118.04	46.30	71.74	0.88	0.208	1.43	0.146	1.03	1.00	0.187	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	118.40	46.50	71.90	0.88	0.208	1.43	0.146	1.03	1.00	0.187	No
338	6.76	118.76	46.70	72.07	0.88	0.208	1.43	0.146	1.03	1.00	0.187	No
339	6.78	119.12	46.89	72.23	0.88	0.208	1.43	0.146	1.03	1.00	0.187	No
340	6.80	119.48	47.09	72.39	0.88	0.208	1.43	0.146	1.03	1.00	0.187	No
341	6.82	119.84	47.28	72.55	0.88	0.208	1.43	0.146	1.03	1.00	0.187	No
342	6.84	120.19	47.48	72.71	0.88	0.208	1.43	0.146	1.03	1.00	0.187	No
343	6.86	120.55	47.68	72.87	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
344	6.88	120.90	47.87	73.03	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
345	6.90	121.26	48.07	73.19	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
346	6.92	121.62	48.27	73.35	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
347	6.94	121.98	48.46	73.51	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
348	6.96	122.33	48.66	73.68	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
349	6.98	122.69	48.85	73.84	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
350	7.00	123.05	49.05	74.00	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
351	7.02	123.41	49.25	74.16	0.88	0.209	1.43	0.146	1.03	1.00	0.189	No
352	7.04	123.76	49.44	74.32	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
353	7.06	124.12	49.64	74.48	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
354	7.08	124.47	49.83	74.63	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
355	7.10	124.82	50.03	74.79	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
356	7.12	125.17	50.23	74.95	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
357	7.14	125.53	50.42	75.11	0.88	0.209	1.43	0.146	1.03	1.00	0.188	No
358	7.16	125.88	50.62	75.27	0.87	0.209	1.43	0.146	1.03	1.00	0.188	No
359	7.18	126.24	50.82	75.43	0.87	0.209	1.43	0.146	1.03	1.00	0.188	No
360	7.20	126.60	51.01	75.59	0.87	0.209	1.43	0.146	1.03	1.00	0.188	No
361	7.22	126.96	51.21	75.75	0.87	0.209	1.43	0.147	1.02	1.00	0.189	No
362	7.25	127.50	51.50	76.00	0.87	0.209	1.43	0.147	1.02	1.00	0.189	No
363	7.26	127.68	51.60	76.08	0.87	0.209	1.43	0.147	1.02	1.00	0.189	No
364	7.28	128.04	51.80	76.24	0.87	0.209	1.43	0.147	1.02	1.00	0.189	No
365	7.30	128.40	51.99	76.41	0.87	0.209	1.43	0.147	1.02	1.00	0.189	No
366	7.32	128.76	52.19	76.57	0.87	0.209	1.43	0.147	1.02	1.00	0.189	No
367	7.34	129.12	52.39	76.74	0.87	0.209	1.43	0.147	1.02	1.00	0.189	No
368	7.36	129.48	52.58	76.90	0.87	0.209	1.43	0.147	1.02	1.00	0.189	No
369	7.38	129.84	52.78	77.07	0.87	0.210	1.43	0.147	1.02	1.00	0.188	No
370	7.40	130.20	52.97	77.23	0.87	0.210	1.43	0.147	1.02	1.00	0.188	No
371	7.42	130.56	53.17	77.39	0.87	0.210	1.43	0.147	1.02	1.00	0.188	No
372	7.44	130.93	53.37	77.56	0.87	0.210	1.43	0.147	1.02	1.00	0.188	No
373	7.46	131.29	53.56	77.73	0.87	0.210	1.43	0.147	1.02	1.00	0.189	No
374	7.48	131.65	53.76	77.89	0.87	0.210	1.43	0.147	1.02	1.00	0.189	No
375	7.50	132.02	53.96	78.06	0.87	0.210	1.43	0.147	1.02	1.00	0.189	No
376	7.52	132.38	54.15	78.23	0.87	0.210	1.43	0.147	1.02	1.00	0.189	No
377	7.54	132.75	54.35	78.40	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
378	7.56	133.12	54.54	78.57	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
379	7.58	133.48	54.74	78.74	0.87	0.210	1.43	0.147	1.02	1.00	0.190	No
380	7.60	133.85	54.94	78.91	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
381	7.62	134.21	55.13	79.08	0.86	0.210	1.43	0.147	1.02	1.00	0.189	No
382	7.64	134.58	55.33	79.25	0.86	0.210	1.43	0.147	1.02	1.00	0.189	No
383	7.66	134.94	55.52	79.41	0.86	0.210	1.43	0.147	1.02	1.00	0.189	No
384	7.68	135.30	55.72	79.58	0.86	0.210	1.43	0.147	1.02	1.00	0.189	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	135.66	55.92	79.75	0.86	0.210	1.43	0.147	1.02	1.00	0.189	No
386	7.72	136.02	56.11	79.91	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
387	7.74	136.39	56.31	80.08	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
388	7.76	136.75	56.51	80.25	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
389	7.78	137.12	56.70	80.41	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
390	7.80	137.48	56.90	80.58	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
391	7.82	137.85	57.09	80.75	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
392	7.84	138.22	57.29	80.92	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
393	7.86	138.58	57.49	81.09	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
394	7.88	138.95	57.68	81.26	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
395	7.90	139.31	57.88	81.43	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
396	7.92	139.67	58.08	81.60	0.86	0.210	1.43	0.147	1.02	1.00	0.190	No
397	7.94	140.03	58.27	81.76	0.86	0.210	1.43	0.147	1.02	1.00	0.191	No
398	7.96	140.39	58.47	81.93	0.86	0.210	1.43	0.147	1.02	1.00	0.191	No
399	7.98	140.75	58.66	82.09	0.86	0.210	1.43	0.147	1.02	1.00	0.191	No
400	8.00	141.11	58.86	82.25	0.86	0.210	1.43	0.147	1.02	1.00	0.192	No
401	8.02	141.46	59.06	82.41	0.85	0.210	1.43	0.147	1.02	1.00	0.192	No
402	8.04	141.81	59.25	82.56	0.85	0.210	1.43	0.147	1.02	1.00	0.192	No
403	8.06	142.16	59.45	82.72	0.85	0.210	1.43	0.147	1.02	1.00	0.193	No
404	8.08	142.51	59.64	82.87	0.85	0.210	1.43	0.147	1.02	1.00	0.193	No
405	8.10	142.86	59.84	83.02	0.85	0.210	1.43	0.147	1.02	1.00	0.193	No
406	8.12	143.20	60.04	83.16	0.85	0.210	1.43	0.147	1.02	1.00	0.193	No
407	8.14	143.54	60.23	83.31	0.85	0.210	1.43	0.147	1.02	1.00	0.193	No
408	8.16	143.87	60.43	83.44	0.85	0.210	1.43	0.147	1.02	1.00	0.193	No
409	8.18	144.21	60.63	83.58	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
410	8.20	144.54	60.82	83.71	0.85	0.210	1.43	0.147	1.01	1.00	0.193	No
411	8.22	144.86	61.02	83.84	0.85	0.210	1.43	0.147	1.01	1.00	0.193	No
412	8.24	145.19	61.21	83.97	0.85	0.210	1.43	0.147	1.01	1.00	0.193	No
413	8.26	145.51	61.41	84.10	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
414	8.28	145.83	61.61	84.22	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
415	8.30	146.14	61.80	84.34	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
416	8.32	146.46	62.00	84.46	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
417	8.34	146.77	62.20	84.57	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
418	8.36	147.08	62.39	84.69	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
419	8.39	147.54	62.69	84.86	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
420	8.40	147.70	62.78	84.92	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
421	8.42	148.01	62.98	85.03	0.85	0.210	1.43	0.147	1.01	1.00	0.194	No
422	8.44	148.33	63.18	85.15	0.84	0.210	1.43	0.147	1.01	1.00	0.194	No
423	8.46	148.64	63.37	85.27	0.84	0.210	1.43	0.147	1.01	1.00	0.194	No
424	8.48	148.96	63.57	85.39	0.84	0.211	1.43	0.147	1.01	1.00	0.194	No
425	8.50	149.28	63.77	85.52	0.84	0.211	1.43	0.147	1.01	1.00	0.194	No
426	8.52	149.60	63.96	85.64	0.84	0.211	1.43	0.147	1.01	1.00	0.194	No
427	8.54	149.92	64.16	85.77	0.84	0.211	1.43	0.147	1.01	1.00	0.194	No
428	8.56	150.25	64.35	85.89	0.84	0.211	1.43	0.147	1.01	1.00	0.194	No
429	8.58	150.57	64.55	86.02	0.84	0.211	1.43	0.147	1.01	1.00	0.194	No
430	8.60	150.89	64.75	86.14	0.84	0.211	1.43	0.147	1.01	1.00	0.194	No
431	8.63	151.37	65.04	86.33	0.84	0.211	1.43	0.148	1.01	1.00	0.195	No
432	8.64	151.53	65.14	86.39	0.84	0.211	1.43	0.148	1.01	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	151.84	65.33	86.51	0.84	0.211	1.43	0.148	1.01	1.00	0.195	No
434	8.68	152.16	65.53	86.63	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
435	8.70	152.48	65.73	86.75	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
436	8.72	152.79	65.92	86.87	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
437	8.74	153.11	66.12	86.99	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
438	8.76	153.44	66.32	87.12	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
439	8.78	153.76	66.51	87.25	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
440	8.80	154.09	66.71	87.38	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
441	8.82	154.42	66.90	87.51	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
442	8.84	154.75	67.10	87.65	0.84	0.211	1.43	0.148	1.01	1.00	0.194	No
443	8.86	155.08	67.30	87.78	0.83	0.211	1.43	0.148	1.01	1.00	0.194	No
444	8.88	155.41	67.49	87.92	0.83	0.211	1.43	0.148	1.01	1.00	0.194	No
445	8.90	155.75	67.69	88.06	0.83	0.211	1.43	0.148	1.01	1.00	0.194	No
446	8.92	156.08	67.89	88.20	0.83	0.211	1.43	0.148	1.01	1.00	0.194	No
447	8.95	156.59	68.18	88.41	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
448	8.96	156.76	68.28	88.48	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
449	8.98	157.09	68.47	88.62	0.83	0.211	1.43	0.148	1.01	1.00	0.194	No
450	9.00	157.43	68.67	88.76	0.83	0.211	1.43	0.148	1.01	1.00	0.194	No
451	9.02	157.77	68.87	88.90	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
452	9.04	158.10	69.06	89.04	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
453	9.06	158.44	69.26	89.18	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
454	9.08	158.77	69.45	89.32	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
455	9.10	159.11	69.65	89.46	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
456	9.12	159.44	69.85	89.60	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
457	9.14	159.78	70.04	89.73	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
458	9.16	160.11	70.24	89.87	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
459	9.18	160.43	70.44	90.00	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
460	9.20	160.76	70.63	90.13	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
461	9.23	161.24	70.93	90.32	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
462	9.24	161.40	71.02	90.38	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
463	9.26	161.72	71.22	90.50	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
464	9.28	162.04	71.42	90.62	0.83	0.211	1.43	0.148	1.01	1.00	0.195	No
465	9.30	162.36	71.61	90.74	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
466	9.32	162.67	71.81	90.86	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
467	9.34	162.99	72.01	90.98	0.82	0.211	1.43	0.148	1.01	1.00	0.196	No
468	9.36	163.30	72.20	91.10	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
469	9.38	163.62	72.40	91.22	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
470	9.40	163.93	72.59	91.34	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
471	9.42	164.25	72.79	91.46	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
472	9.44	164.57	72.99	91.59	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
473	9.46	164.90	73.18	91.72	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
474	9.48	165.23	73.38	91.85	0.82	0.211	1.43	0.148	1.01	1.00	0.194	No
475	9.50	165.56	73.58	91.98	0.82	0.211	1.43	0.148	1.01	1.00	0.194	No
476	9.52	165.89	73.77	92.12	0.82	0.211	1.43	0.148	1.01	1.00	0.194	No
477	9.54	166.22	73.97	92.26	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
478	9.56	166.56	74.16	92.39	0.82	0.211	1.43	0.148	1.01	1.00	0.195	No
479	9.58	166.89	74.36	92.53	0.82	0.211	1.43	0.148	1.01	1.00	0.196	No
480	9.60	167.22	74.56	92.67	0.82	0.211	1.43	0.148	1.01	1.00	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	167.55	74.75	92.80	0.82	0.211	1.43	0.148	1.01	1.00	0.196	No
482	9.64	167.88	74.95	92.94	0.82	0.211	1.43	0.148	1.01	1.00	0.196	No
483	9.66	168.21	75.14	93.07	0.82	0.211	1.43	0.148	1.01	1.00	0.196	No
484	9.68	168.54	75.34	93.19	0.82	0.211	1.43	0.148	1.01	1.00	0.196	No
485	9.70	168.86	75.54	93.32	0.81	0.211	1.43	0.148	1.01	1.00	0.195	No
486	9.72	169.18	75.73	93.44	0.81	0.211	1.43	0.148	1.01	1.00	0.195	No
487	9.74	169.50	75.93	93.57	0.81	0.211	1.43	0.148	1.01	1.00	0.195	No
488	9.76	169.82	76.13	93.69	0.81	0.211	1.43	0.148	1.01	1.00	0.195	No
489	9.78	170.14	76.32	93.82	0.81	0.211	1.43	0.148	1.01	1.00	0.196	No
490	9.80	170.48	76.52	93.96	0.81	0.211	1.43	0.148	1.01	1.00	0.195	No
491	9.82	170.82	76.71	94.10	0.81	0.211	1.43	0.148	1.01	1.00	0.194	No
492	9.84	171.17	76.91	94.25	0.81	0.211	1.43	0.148	1.01	1.00	0.194	No
493	9.86	171.51	77.11	94.41	0.81	0.211	1.43	0.148	1.01	1.00	0.194	No
494	9.88	171.86	77.30	94.56	0.81	0.211	1.43	0.147	1.01	1.00	0.195	No
495	9.90	172.20	77.50	94.70	0.81	0.211	1.43	0.147	1.01	1.00	0.195	No
496	9.92	172.54	77.70	94.84	0.81	0.211	1.43	0.147	1.01	1.00	0.195	No
497	9.95	173.05	77.99	95.06	0.81	0.211	1.43	0.147	1.01	1.00	0.196	No
498	9.96	173.21	78.09	95.13	0.81	0.211	1.43	0.147	1.00	1.00	0.196	No
499	9.98	173.55	78.28	95.26	0.81	0.211	1.43	0.147	1.00	1.00	0.196	No
500	10.00	173.88	78.48	95.40	0.81	0.211	1.43	0.147	1.00	1.00	0.196	No
501	10.02	174.20	78.68	95.52	0.81	0.211	1.43	0.147	1.00	1.00	0.196	No
502	10.04	174.52	78.87	95.65	0.81	0.211	1.43	0.147	1.00	1.00	0.196	No
503	10.06	174.84	79.07	95.77	0.81	0.211	1.43	0.147	1.00	1.00	0.196	No
504	10.08	175.16	79.26	95.89	0.81	0.211	1.43	0.147	1.00	1.00	0.196	No
505	10.10	175.48	79.46	96.01	0.81	0.210	1.43	0.147	1.00	1.00	0.196	No
506	10.12	175.79	79.66	96.14	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
507	10.14	176.11	79.85	96.26	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
508	10.16	176.43	80.05	96.38	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
509	10.18	176.75	80.25	96.51	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
510	10.20	177.07	80.44	96.63	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
511	10.22	177.39	80.64	96.76	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
512	10.24	177.71	80.83	96.88	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
513	10.26	178.03	81.03	97.00	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
514	10.28	178.35	81.23	97.12	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
515	10.30	178.67	81.42	97.24	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
516	10.32	178.98	81.62	97.36	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
517	10.34	179.30	81.82	97.48	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
518	10.36	179.62	82.01	97.60	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
519	10.38	179.93	82.21	97.73	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
520	10.40	180.25	82.40	97.85	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
521	10.42	180.57	82.60	97.97	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
522	10.44	180.89	82.80	98.09	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
523	10.46	181.21	82.99	98.21	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
524	10.48	181.53	83.19	98.34	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
525	10.50	181.85	83.39	98.46	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
526	10.52	182.17	83.58	98.59	0.80	0.210	1.43	0.147	1.00	1.00	0.196	No
527	10.54	182.49	83.78	98.71	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
528	10.56	182.80	83.97	98.83	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	183.12	84.17	98.95	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
530	10.60	183.44	84.37	99.07	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
531	10.62	183.76	84.56	99.19	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
532	10.64	184.08	84.76	99.32	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
533	10.66	184.40	84.95	99.44	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
534	10.68	184.72	85.15	99.57	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
535	10.70	185.04	85.35	99.69	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
536	10.72	185.37	85.54	99.82	0.79	0.210	1.43	0.147	1.00	1.00	0.196	No
537	10.74	185.69	85.74	99.95	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
538	10.76	186.02	85.94	100.08	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
539	10.78	186.35	86.13	100.22	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
540	10.80	186.68	86.33	100.35	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
541	10.82	187.01	86.52	100.49	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
542	10.84	187.35	86.72	100.63	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
543	10.86	187.69	86.92	100.77	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
544	10.88	188.03	87.11	100.91	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
545	10.90	188.36	87.31	101.05	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
546	10.92	188.70	87.51	101.19	0.79	0.210	1.43	0.147	1.00	1.00	0.195	No
547	10.94	189.03	87.70	101.33	0.79	0.209	1.43	0.147	1.00	1.00	0.196	No
548	10.96	189.37	87.90	101.47	0.78	0.209	1.43	0.147	1.00	1.00	0.196	No
549	10.98	189.70	88.09	101.61	0.78	0.209	1.43	0.147	1.00	1.00	0.195	No
550	11.00	190.03	88.29	101.74	0.78	0.209	1.43	0.147	1.00	1.00	0.195	No
551	11.02	190.36	88.49	101.87	0.78	0.209	1.43	0.147	1.00	1.00	0.195	No
552	11.04	190.69	88.68	102.01	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
553	11.06	191.02	88.88	102.14	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
554	11.08	191.34	89.07	102.27	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
555	11.10	191.67	89.27	102.40	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
556	11.12	191.99	89.47	102.52	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
557	11.14	192.32	89.66	102.65	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
558	11.16	192.65	89.86	102.79	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
559	11.18	192.97	90.06	102.92	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
560	11.20	193.30	90.25	103.05	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
561	11.22	193.64	90.45	103.19	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
562	11.24	193.97	90.64	103.32	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
563	11.26	194.30	90.84	103.46	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
564	11.28	194.63	91.04	103.60	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
565	11.30	194.96	91.23	103.73	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
566	11.32	195.29	91.43	103.86	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
567	11.34	195.62	91.63	104.00	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
568	11.36	195.95	91.82	104.13	0.78	0.209	1.43	0.146	1.00	1.00	0.195	No
569	11.38	196.28	92.02	104.26	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
570	11.40	196.60	92.21	104.39	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
571	11.42	196.93	92.41	104.52	0.77	0.209	1.43	0.146	1.00	1.00	0.195	No
572	11.44	197.26	92.61	104.65	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
573	11.46	197.59	92.80	104.79	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
574	11.48	197.92	93.00	104.92	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
575	11.50	198.25	93.19	105.05	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
576	11.52	198.58	93.39	105.19	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	198.91	93.59	105.32	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
578	11.56	199.24	93.78	105.46	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
579	11.58	199.58	93.98	105.60	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
580	11.60	199.91	94.18	105.73	0.77	0.208	1.43	0.146	1.00	1.00	0.195	No
581	11.62	200.24	94.37	105.87	0.77	0.208	1.43	0.146	1.00	1.00	0.194	No
582	11.64	200.58	94.57	106.01	0.77	0.208	1.43	0.146	1.00	1.00	0.194	No
583	11.66	200.92	94.76	106.15	0.77	0.208	1.43	0.146	1.00	1.00	0.194	No
584	11.68	201.25	94.96	106.29	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
585	11.70	201.59	95.16	106.44	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
586	11.72	201.93	95.35	106.58	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
587	11.74	202.27	95.55	106.72	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
588	11.76	202.61	95.75	106.87	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
589	11.78	202.96	95.94	107.01	0.77	0.208	1.43	0.145	1.00	1.00	0.194	No
590	11.80	203.30	96.14	107.16	0.76	0.207	1.43	0.145	1.00	1.00	0.194	No
591	11.82	203.64	96.33	107.31	0.76	0.207	1.43	0.145	1.00	1.00	0.194	No
592	11.84	203.99	96.53	107.46	0.76	0.207	1.43	0.145	1.00	1.00	0.194	No
593	11.86	204.34	96.73	107.61	0.76	0.207	1.43	0.145	1.00	1.00	0.194	No
594	11.88	204.68	96.92	107.76	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
595	11.90	205.03	97.12	107.91	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
596	11.92	205.38	97.32	108.06	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
597	11.94	205.72	97.51	108.21	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
598	11.96	206.07	97.71	108.36	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
599	11.98	206.42	97.90	108.52	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
600	12.00	206.77	98.10	108.67	0.76	0.207	1.43	0.145	0.99	1.00	0.194	No
601	12.02	207.11	98.30	108.82	0.76	0.207	1.43	0.145	0.99	1.00	0.193	No
602	12.04	207.46	98.49	108.97	0.76	0.207	1.43	0.145	0.99	1.00	0.193	No
603	12.06	207.81	98.69	109.12	0.76	0.207	1.43	0.145	0.99	1.00	0.193	No
604	12.08	208.15	98.88	109.27	0.76	0.207	1.43	0.145	0.99	1.00	0.193	No
605	12.10	208.50	99.08	109.42	0.76	0.206	1.43	0.145	0.99	1.00	0.193	No
606	12.12	208.85	99.28	109.57	0.76	0.206	1.43	0.144	0.99	1.00	0.193	No
607	12.14	209.20	99.47	109.72	0.76	0.206	1.43	0.144	0.99	1.00	0.193	No
608	12.16	209.55	99.67	109.88	0.76	0.206	1.43	0.144	0.99	1.00	0.193	No
609	12.18	209.90	99.87	110.03	0.76	0.206	1.43	0.144	0.99	1.00	0.193	No
610	12.20	210.25	100.06	110.19	0.76	0.206	1.43	0.144	0.99	1.00	0.193	No
611	12.22	210.60	100.26	110.34	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
612	12.24	210.95	100.45	110.50	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
613	12.26	211.31	100.65	110.66	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
614	12.28	211.66	100.85	110.81	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
615	12.30	212.01	101.04	110.96	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
616	12.32	212.36	101.24	111.12	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
617	12.34	212.71	101.44	111.27	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
618	12.36	213.05	101.63	111.42	0.75	0.206	1.43	0.144	0.99	1.00	0.193	No
619	12.38	213.40	101.83	111.58	0.75	0.205	1.43	0.144	0.99	1.00	0.193	No
620	12.40	213.75	102.02	111.73	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
621	12.42	214.10	102.22	111.88	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
622	12.44	214.45	102.42	112.03	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
623	12.46	214.80	102.61	112.18	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No
624	12.48	215.15	102.81	112.34	0.75	0.205	1.43	0.144	0.99	1.00	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	215.49	103.01	112.49	0.75	0.205	1.43	0.143	0.99	1.00	0.192	No
626	12.52	215.84	103.20	112.64	0.75	0.205	1.43	0.143	0.99	1.00	0.192	No
627	12.54	216.19	103.40	112.79	0.75	0.205	1.43	0.143	0.99	1.00	0.192	No
628	12.56	216.54	103.59	112.95	0.75	0.205	1.43	0.143	0.99	1.00	0.192	No
629	12.58	216.89	103.79	113.10	0.75	0.205	1.43	0.143	0.99	1.00	0.192	No
630	12.60	217.25	103.99	113.26	0.75	0.205	1.43	0.143	0.99	1.00	0.192	No
631	12.62	217.60	104.18	113.42	0.75	0.205	1.43	0.143	0.99	1.00	0.192	No
632	12.64	217.95	104.38	113.57	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
633	12.66	218.31	104.57	113.73	0.74	0.204	1.43	0.143	0.99	1.00	0.192	No
634	12.68	218.67	104.77	113.89	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
635	12.70	219.02	104.97	114.06	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
636	12.72	219.38	105.16	114.22	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
637	12.74	219.74	105.36	114.38	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
638	12.76	220.10	105.56	114.54	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
639	12.78	220.46	105.75	114.71	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
640	12.80	220.82	105.95	114.87	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
641	12.82	221.18	106.14	115.03	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
642	12.84	221.53	106.34	115.19	0.74	0.204	1.43	0.143	0.99	1.00	0.191	No
643	12.86	221.89	106.54	115.36	0.74	0.203	1.43	0.142	0.99	1.00	0.191	No
644	12.88	222.25	106.73	115.52	0.74	0.203	1.43	0.142	0.99	1.00	0.191	No
645	12.90	222.61	106.93	115.68	0.74	0.203	1.43	0.142	0.99	1.00	0.191	No
646	12.92	222.97	107.13	115.85	0.74	0.203	1.43	0.142	0.99	1.00	0.191	No
647	12.94	223.33	107.32	116.01	0.74	0.203	1.43	0.142	0.99	1.00	0.190	No
648	12.96	223.69	107.52	116.18	0.74	0.203	1.43	0.142	0.99	1.00	0.190	No
649	12.98	224.05	107.71	116.34	0.74	0.203	1.43	0.142	0.99	1.00	0.190	No
650	13.00	224.41	107.91	116.50	0.74	0.203	1.43	0.142	0.99	1.00	0.190	No
651	13.02	224.77	108.11	116.67	0.74	0.203	1.43	0.142	0.99	1.00	0.190	No
652	13.04	225.13	108.30	116.83	0.74	0.203	1.43	0.142	0.99	1.00	0.190	No
653	13.06	225.49	108.50	116.99	0.74	0.203	1.43	0.142	0.99	1.00	0.190	No
654	13.08	225.85	108.69	117.15	0.73	0.203	1.43	0.142	0.99	1.00	0.190	No
655	13.10	226.21	108.89	117.31	0.73	0.202	1.43	0.142	0.99	1.00	0.190	No
656	13.12	226.56	109.09	117.48	0.73	0.202	1.43	0.142	0.99	1.00	0.190	No
657	13.14	226.92	109.28	117.64	0.73	0.202	1.43	0.142	0.99	1.00	0.190	No
658	13.16	227.28	109.48	117.80	0.73	0.202	1.43	0.142	0.99	1.00	0.190	No
659	13.19	227.82	109.77	118.04	0.73	0.202	1.43	0.141	0.99	1.00	0.190	No
660	13.20	228.00	109.87	118.12	0.73	0.202	1.43	0.141	0.99	1.00	0.190	No
661	13.22	228.36	110.07	118.29	0.73	0.202	1.43	0.141	0.99	1.00	0.190	No
662	13.24	228.72	110.26	118.45	0.73	0.202	1.43	0.141	0.99	1.00	0.190	No
663	13.26	229.08	110.46	118.61	0.73	0.202	1.43	0.141	0.99	1.00	0.190	No
664	13.28	229.44	110.66	118.78	0.73	0.202	1.43	0.141	0.99	1.00	0.190	No
665	13.30	229.80	110.85	118.94	0.73	0.202	1.43	0.141	0.99	1.00	0.190	No
666	13.32	230.16	111.05	119.11	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No
667	13.34	230.51	111.25	119.27	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No
668	13.36	230.87	111.44	119.43	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No
669	13.38	231.23	111.64	119.60	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No
670	13.40	231.59	111.83	119.76	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No
671	13.42	231.95	112.03	119.92	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No
672	13.44	232.30	112.23	120.08	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	232.66	112.42	120.24	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No
674	13.48	233.01	112.62	120.39	0.73	0.201	1.43	0.141	0.99	1.00	0.190	No
675	13.50	233.36	112.82	120.55	0.72	0.201	1.43	0.140	0.99	1.00	0.190	No
676	13.52	233.71	113.01	120.70	0.72	0.201	1.43	0.140	0.99	1.00	0.190	No
677	13.54	234.06	113.21	120.85	0.72	0.201	1.43	0.140	0.99	1.00	0.190	No
678	13.56	234.41	113.40	121.00	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
679	13.58	234.75	113.60	121.15	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
680	13.60	235.09	113.80	121.30	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
681	13.62	235.44	113.99	121.44	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
682	13.64	235.78	114.19	121.59	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
683	13.66	236.11	114.38	121.73	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
684	13.68	236.45	114.58	121.87	0.72	0.200	1.43	0.140	0.99	1.00	0.190	No
685	13.70	236.78	114.78	122.01	0.72	0.200	1.43	0.140	0.99	1.00	0.189	No
686	13.72	237.12	114.97	122.15	0.72	0.200	1.43	0.140	0.99	1.00	0.189	No
687	13.74	237.45	115.17	122.28	0.72	0.200	1.43	0.140	0.99	1.00	0.189	No
688	13.76	237.78	115.37	122.42	0.72	0.200	1.43	0.140	0.99	1.00	0.189	No
689	13.78	238.11	115.56	122.55	0.72	0.200	1.43	0.140	0.98	1.00	0.189	No
690	13.80	238.44	115.76	122.69	0.72	0.200	1.43	0.140	0.98	1.00	0.189	No
691	13.82	238.77	115.95	122.82	0.72	0.199	1.43	0.140	0.98	1.00	0.189	No
692	13.84	239.10	116.15	122.95	0.72	0.199	1.43	0.140	0.98	1.00	0.189	No
693	13.86	239.43	116.35	123.08	0.72	0.199	1.43	0.140	0.98	1.00	0.189	No
694	13.88	239.76	116.54	123.22	0.72	0.199	1.43	0.139	0.98	1.00	0.189	No
695	13.90	240.08	116.74	123.35	0.72	0.199	1.43	0.139	0.98	1.00	0.189	No
696	13.92	240.41	116.94	123.47	0.72	0.199	1.43	0.139	0.98	1.00	0.189	No
697	13.94	240.73	117.13	123.60	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
698	13.96	241.06	117.33	123.73	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
699	13.98	241.38	117.52	123.85	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
700	14.00	241.70	117.72	123.98	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
701	14.02	242.02	117.92	124.10	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
702	14.04	242.34	118.11	124.22	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
703	14.06	242.66	118.31	124.35	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
704	14.08	242.98	118.50	124.47	0.71	0.199	1.43	0.139	0.98	1.00	0.188	No
705	14.11	243.46	118.80	124.66	0.71	0.199	1.43	0.139	0.98	1.00	0.188	No
706	14.12	243.62	118.90	124.73	0.71	0.199	1.43	0.139	0.98	1.00	0.189	No
707	14.14	243.95	119.09	124.85	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
708	14.16	244.27	119.29	124.98	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
709	14.18	244.60	119.49	125.11	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
710	14.20	244.92	119.68	125.24	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
711	14.22	245.24	119.88	125.36	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
712	14.24	245.57	120.07	125.49	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
713	14.26	245.89	120.27	125.62	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
714	14.28	246.21	120.47	125.74	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
715	14.30	246.53	120.66	125.87	0.71	0.198	1.43	0.139	0.98	1.00	0.188	No
716	14.32	246.86	120.86	126.00	0.71	0.198	1.43	0.138	0.98	1.00	0.188	No
717	14.34	247.18	121.06	126.13	0.71	0.198	1.43	0.138	0.98	1.00	0.188	No
718	14.36	247.51	121.25	126.25	0.71	0.198	1.43	0.138	0.98	1.00	0.188	No
719	14.38	247.83	121.45	126.38	0.70	0.198	1.43	0.138	0.98	1.00	0.188	No
720	14.40	248.15	121.64	126.51	0.70	0.198	1.43	0.138	0.98	1.00	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	248.48	121.84	126.64	0.70	0.198	1.43	0.138	0.98	1.00	0.188	No
722	14.44	248.81	122.04	126.77	0.70	0.197	1.43	0.138	0.98	1.00	0.188	No
723	14.46	249.13	122.23	126.90	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
724	14.48	249.46	122.43	127.03	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
725	14.50	249.78	122.63	127.16	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
726	14.52	250.11	122.82	127.29	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
727	14.54	250.44	123.02	127.42	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
728	14.56	250.77	123.21	127.55	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
729	14.58	251.10	123.41	127.69	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
730	14.60	251.43	123.61	127.83	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
731	14.62	251.77	123.80	127.96	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
732	14.64	252.10	124.00	128.10	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
733	14.66	252.43	124.19	128.24	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
734	14.68	252.76	124.39	128.37	0.70	0.197	1.43	0.138	0.98	1.00	0.187	No
735	14.70	253.09	124.59	128.51	0.70	0.196	1.43	0.138	0.98	1.00	0.187	No
736	14.72	253.43	124.78	128.65	0.70	0.196	1.43	0.137	0.98	1.00	0.187	No
737	14.74	253.77	124.98	128.79	0.70	0.196	1.43	0.137	0.98	1.00	0.187	No
738	14.76	254.10	125.18	128.93	0.70	0.196	1.43	0.137	0.98	1.00	0.187	No
739	14.79	254.62	125.47	129.15	0.70	0.196	1.43	0.137	0.98	1.00	0.186	No
740	14.80	254.79	125.57	129.22	0.70	0.196	1.43	0.137	0.98	1.00	0.186	No
741	14.82	255.13	125.76	129.36	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
742	14.84	255.47	125.96	129.51	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
743	14.86	255.81	126.16	129.65	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
744	14.88	256.15	126.35	129.80	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
745	14.90	256.49	126.55	129.95	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
746	14.92	256.84	126.75	130.09	0.69	0.196	1.43	0.137	0.98	1.00	0.186	No
747	14.94	257.18	126.94	130.24	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
748	14.96	257.52	127.14	130.38	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
749	14.99	258.03	127.43	130.60	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
750	15.00	258.20	127.53	130.67	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
751	15.02	258.54	127.73	130.81	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
752	15.04	258.87	127.92	130.95	0.69	0.195	1.43	0.137	0.98	1.00	0.186	No
753	15.06	259.21	128.12	131.09	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
754	15.08	259.54	128.31	131.23	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
755	15.10	259.87	128.51	131.36	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
756	15.12	260.20	128.71	131.50	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
757	15.14	260.53	128.90	131.63	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
758	15.16	260.86	129.10	131.76	0.69	0.195	1.43	0.136	0.98	1.00	0.186	No
759	15.18	261.19	129.30	131.90	0.69	0.195	1.43	0.136	0.98	1.00	0.185	No
760	15.20	261.52	129.49	132.03	0.69	0.194	1.43	0.136	0.98	1.00	0.185	No
761	15.22	261.85	129.69	132.16	0.69	0.194	1.43	0.136	0.98	1.00	0.185	No
762	15.24	262.18	129.88	132.29	0.69	0.194	1.43	0.136	0.98	1.00	0.185	No
763	15.26	262.51	130.08	132.43	0.69	0.194	1.43	0.136	0.98	1.00	0.185	No
764	15.28	262.84	130.28	132.56	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
765	15.30	263.17	130.47	132.70	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
766	15.32	263.51	130.67	132.84	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
767	15.34	263.84	130.87	132.98	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
768	15.36	264.18	131.06	133.12	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	264.52	131.26	133.26	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
770	15.40	264.86	131.45	133.41	0.68	0.194	1.43	0.136	0.98	1.00	0.185	No
771	15.42	265.20	131.65	133.55	0.68	0.194	1.43	0.135	0.98	1.00	0.184	No
772	15.44	265.55	131.85	133.70	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No
773	15.46	265.89	132.04	133.85	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No
774	15.48	266.23	132.24	133.99	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No
775	15.50	266.58	132.44	134.14	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No
776	15.52	266.92	132.63	134.29	0.68	0.193	1.43	0.135	0.98	1.00	0.183	No
777	15.54	267.27	132.83	134.45	0.68	0.193	1.43	0.135	0.98	1.00	0.183	No
778	15.56	267.62	133.02	134.60	0.68	0.193	1.43	0.135	0.98	1.00	0.182	No
779	15.58	267.98	133.22	134.76	0.68	0.193	1.43	0.135	0.98	1.00	0.182	No
780	15.60	268.33	133.42	134.91	0.68	0.193	1.43	0.135	0.98	1.00	0.183	No
781	15.62	268.68	133.61	135.07	0.68	0.193	1.43	0.135	0.98	1.00	0.183	No
782	15.64	269.02	133.81	135.22	0.68	0.193	1.43	0.135	0.98	1.00	0.184	No
783	15.66	269.37	134.00	135.36	0.68	0.192	1.43	0.135	0.98	1.00	0.184	No
784	15.68	269.71	134.20	135.51	0.68	0.192	1.43	0.135	0.98	1.00	0.184	No
785	15.70	270.05	134.40	135.65	0.68	0.192	1.43	0.135	0.98	1.00	0.184	No
786	15.72	270.38	134.59	135.79	0.68	0.192	1.43	0.135	0.98	1.00	0.184	No
787	15.74	270.72	134.79	135.93	0.67	0.192	1.43	0.135	0.98	1.00	0.184	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.26	100.00	3.26	0.61	1.70	4.00	0.00	4.00	4.000	No	Yes	2.00
2	0.04	0.32	100.00	3.17	0.60	1.70	4.76	0.00	4.76	4.000	No	Yes	2.00
3	0.06	0.37	100.00	3.15	0.60	1.70	6.58	0.00	6.58	4.000	No	Yes	2.00
4	0.08	0.42	100.00	3.17	0.59	1.70	7.22	0.00	7.22	4.000	No	Yes	2.00
5	0.10	0.42	100.00	3.24	0.59	1.70	7.03	0.00	7.03	4.000	No	Yes	2.00
6	0.12	0.40	100.00	3.36	0.60	1.70	6.77	0.00	6.77	4.000	No	Yes	2.00
7	0.15	0.38	100.00	3.43	0.60	1.70	6.24	0.00	6.24	4.000	No	Yes	2.00
8	0.16	0.36	100.00	3.51	0.60	1.70	6.16	0.00	6.16	4.000	No	Yes	2.00
9	0.18	0.33	100.00	3.57	0.60	1.70	5.49	0.00	5.49	4.000	No	Yes	2.00
10	0.20	0.29	100.00	3.65	0.60	1.70	4.70	0.00	4.70	4.000	No	Yes	2.00
11	0.22	0.26	100.00	3.69	0.61	1.70	4.11	0.00	4.11	4.000	No	Yes	2.00
12	0.24	0.25	100.00	3.69	0.61	1.70	4.23	0.00	4.23	4.000	No	Yes	2.00
13	0.26	0.26	100.00	3.62	0.61	1.70	4.17	0.00	4.17	4.000	No	Yes	2.00
14	0.28	0.28	100.00	3.56	0.60	1.70	4.72	0.00	4.72	4.000	No	Yes	2.00
15	0.30	0.33	100.00	3.43	0.60	1.70	4.95	0.00	4.95	4.000	No	Yes	2.00
16	0.32	0.39	100.00	3.32	0.59	1.70	6.95	0.00	6.95	4.000	No	Yes	2.00
17	0.34	0.47	100.00	3.22	0.59	1.70	7.91	0.00	7.91	4.000	No	Yes	2.00
18	0.36	0.51	100.00	3.17	0.59	1.70	8.62	0.00	8.62	4.000	No	Yes	2.00
19	0.38	0.55	100.00	3.15	0.59	1.70	9.28	0.00	9.28	4.000	No	Yes	2.00
20	0.41	0.59	100.00	3.13	0.58	1.70	9.80	0.00	9.80	4.000	No	Yes	2.00
21	0.42	0.64	100.00	3.11	0.58	1.70	10.65	0.00	10.65	4.000	No	Yes	2.00
22	0.44	0.69	100.00	3.09	0.58	1.70	11.46	0.00	11.46	4.000	No	Yes	2.00
23	0.46	0.72	100.00	3.10	0.57	1.70	12.35	0.00	12.35	4.000	No	Yes	2.00
24	0.48	0.73	100.00	3.12	0.57	1.70	12.15	0.00	12.15	4.000	No	Yes	2.00
25	0.50	0.73	100.00	3.16	0.57	1.70	12.05	0.00	12.05	4.000	No	Yes	2.00
26	0.52	0.74	100.00	3.17	0.57	1.70	12.41	0.00	12.41	4.000	No	Yes	2.00
27	0.54	0.75	100.00	3.18	0.57	1.70	12.65	0.00	12.65	4.000	No	Yes	2.00
28	0.56	0.76	100.00	3.20	0.57	1.70	12.67	0.00	12.67	4.000	No	Yes	2.00
29	0.58	0.76	100.00	3.21	0.57	1.70	12.71	0.00	12.71	4.000	No	Yes	2.00
30	0.60	0.76	100.00	3.22	0.57	1.70	12.80	0.00	12.80	4.000	No	Yes	2.00
31	0.62	0.75	100.00	3.23	0.57	1.70	12.58	0.00	12.58	4.000	No	Yes	2.00
32	0.64	0.76	100.00	3.22	0.57	1.70	12.39	0.00	12.39	4.000	No	Yes	2.00
33	0.66	0.78	100.00	3.21	0.57	1.70	13.11	0.00	13.11	4.000	No	Yes	2.00
34	0.68	0.82	100.00	3.18	0.57	1.70	13.87	0.00	13.87	4.000	No	Yes	2.00
35	0.70	0.88	100.00	3.14	0.57	1.70	14.43	0.00	14.43	4.000	No	Yes	2.00
36	0.72	0.92	100.00	3.10	0.56	1.70	15.67	0.00	15.67	4.000	No	Yes	2.00
37	0.74	0.96	100.00	3.07	0.56	1.70	16.27	0.00	16.27	4.000	No	Yes	2.00
38	0.76	0.98	100.00	3.07	0.56	1.70	16.30	0.00	16.30	4.000	No	Yes	2.00
39	0.78	0.99	100.00	3.07	0.56	1.70	16.63	0.00	16.63	4.000	No	Yes	2.00
40	0.80	1.01	100.00	3.07	0.56	1.70	16.93	0.00	16.93	4.000	No	Yes	2.00
41	0.82	1.03	100.00	3.07	0.56	1.70	17.07	0.00	17.07	4.000	No	Yes	2.00
42	0.84	1.04	100.00	3.07	0.55	1.70	17.62	0.00	17.62	4.000	No	Yes	2.00
43	0.86	1.06	100.00	3.08	0.55	1.70	17.72	0.00	17.72	4.000	No	Yes	2.00
44	0.88	1.06	100.00	3.08	0.55	1.70	17.86	0.00	17.86	4.000	No	Yes	2.00
45	0.90	1.06	100.00	3.08	0.55	1.70	17.61	0.00	17.61	4.000	No	Yes	2.00
46	0.92	1.07	100.00	3.08	0.55	1.70	17.90	0.00	17.90	4.000	No	Yes	2.00
47	0.94	1.08	100.00	3.07	0.55	1.70	18.01	0.00	18.01	4.000	No	Yes	2.00
48	0.96	1.11	100.00	3.06	0.55	1.70	18.54	0.00	18.54	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.99	1.12	100.00	3.05	0.55	1.70	18.95	0.00	18.95	4.000	No	Yes	2.00
50	1.00	1.13	100.00	3.05	0.55	1.70	18.83	0.00	18.83	4.000	No	Yes	2.00
51	1.02	1.13	100.00	3.06	0.55	1.70	18.86	0.00	18.86	4.000	No	Yes	2.00
52	1.05	1.14	100.00	3.06	0.55	1.70	18.85	0.00	18.85	4.000	No	Yes	2.00
53	1.07	1.15	100.00	3.06	0.55	1.70	19.59	0.00	19.59	4.000	No	Yes	2.00
54	1.08	1.15	100.00	3.07	0.55	1.70	19.32	0.00	19.32	4.000	No	Yes	2.00
55	1.10	1.13	100.00	3.08	0.55	1.70	18.89	0.00	18.89	4.000	No	Yes	2.00
56	1.12	1.10	100.00	3.10	0.55	1.70	18.41	0.00	18.41	4.000	No	Yes	2.00
57	1.14	1.07	100.00	3.13	0.55	1.70	18.13	0.00	18.13	4.000	No	Yes	2.00
58	1.16	1.02	100.00	3.16	0.56	1.70	17.13	0.00	17.13	4.000	No	Yes	2.00
59	1.18	0.97	100.00	3.20	0.56	1.70	16.13	0.00	16.13	4.000	No	Yes	2.00
60	1.20	0.93	100.00	3.22	0.56	1.70	15.46	0.00	15.46	4.000	No	Yes	2.00
61	1.22	0.89	100.00	3.24	0.56	1.70	14.87	0.00	14.87	4.000	No	Yes	2.00
62	1.24	0.86	100.00	3.25	0.57	1.70	14.43	0.00	14.43	4.000	No	Yes	2.00
63	1.26	0.83	100.00	3.26	0.57	1.70	13.87	0.00	13.87	4.000	No	Yes	2.00
64	1.28	0.81	100.00	3.27	0.57	1.70	13.43	0.00	13.43	4.000	No	Yes	2.00
65	1.30	0.80	100.00	3.26	0.57	1.70	13.22	0.00	13.22	4.000	No	Yes	2.00
66	1.32	0.81	100.00	3.23	0.57	1.70	13.38	0.00	13.38	4.000	No	Yes	2.00
67	1.34	0.82	100.00	3.20	0.57	1.70	13.70	0.00	13.70	4.000	No	Yes	2.00
68	1.36	0.84	100.00	3.18	0.57	1.70	13.82	0.00	13.82	4.000	No	Yes	2.00
69	1.38	0.84	100.00	3.16	0.57	1.70	14.41	0.00	14.41	4.000	No	Yes	2.00
70	1.40	0.87	100.00	3.13	0.57	1.70	13.96	0.00	13.96	4.000	No	Yes	2.00
71	1.42	0.90	100.00	3.10	0.56	1.70	15.04	0.00	15.04	4.000	No	Yes	2.00
72	1.44	0.96	100.00	3.05	0.56	1.70	16.11	0.00	16.11	4.000	No	Yes	2.00
73	1.46	1.01	100.00	3.01	0.56	1.70	16.92	0.00	16.92	4.000	No	Yes	2.00
74	1.48	1.06	100.00	2.99	0.55	1.70	17.73	0.00	17.73	4.000	No	Yes	2.00
75	1.50	1.10	100.00	2.98	0.55	1.70	18.28	0.00	18.28	4.000	No	Yes	2.00
76	1.52	1.14	100.00	2.97	0.55	1.70	18.87	0.00	18.87	4.000	No	Yes	2.00
77	1.54	1.17	99.54	2.96	0.55	1.70	19.49	0.00	19.49	4.000	No	Yes	2.00
78	1.56	1.20	99.25	2.95	0.55	1.70	20.00	0.00	20.00	4.000	No	Yes	2.00
79	1.58	1.22	99.45	2.96	0.54	1.70	20.32	0.00	20.32	4.000	No	Yes	2.00
80	1.60	1.23	99.50	2.96	0.54	1.70	20.46	0.00	20.46	4.000	No	Yes	2.00
81	1.62	1.23	99.96	2.96	0.54	1.70	20.55	0.00	20.55	4.000	No	Yes	2.00
82	1.64	1.22	100.00	2.97	0.55	1.70	20.12	0.00	20.12	4.000	No	Yes	2.00
83	1.66	1.22	100.00	2.97	0.55	1.70	20.14	0.00	20.14	4.000	No	Yes	2.00
84	1.68	1.25	99.60	2.96	0.54	1.70	20.61	0.00	20.61	4.000	No	Yes	2.00
85	1.70	1.28	98.90	2.95	0.54	1.70	21.46	0.00	21.46	4.000	No	Yes	2.00
86	1.72	1.30	98.84	2.95	0.54	1.70	21.60	0.00	21.60	4.000	No	Yes	2.00
87	1.74	1.31	99.55	2.96	0.54	1.70	21.65	0.00	21.65	4.000	No	Yes	2.00
88	1.76	1.31	99.90	2.96	0.54	1.70	21.82	0.00	21.82	4.000	No	Yes	2.00
89	1.78	1.33	99.67	2.96	0.54	1.70	21.84	0.00	21.84	4.000	No	Yes	2.00
90	1.80	1.35	99.50	2.96	0.54	1.70	22.43	0.00	22.43	4.000	No	Yes	2.00
91	1.82	1.35	99.69	2.96	0.54	1.70	22.52	0.00	22.52	4.000	No	Yes	2.00
92	1.84	1.35	100.00	2.96	0.54	1.70	22.24	0.00	22.24	4.000	No	Yes	2.00
93	1.86	1.33	100.00	2.97	0.54	1.70	22.14	0.00	22.14	4.000	No	Yes	2.00
94	1.88	1.32	100.00	2.97	0.54	1.70	21.78	0.00	21.78	4.000	No	Yes	2.00
95	1.90	1.32	100.00	2.97	0.54	1.70	21.88	0.00	21.88	4.000	No	Yes	2.00
96	1.92	1.33	100.00	2.98	0.54	1.70	22.20	0.00	22.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	1.33	100.00	2.99	0.54	1.70	22.17	0.00	22.17	4.000	No	Yes	2.00
98	1.96	1.32	100.00	2.99	0.54	1.70	21.82	0.00	21.82	4.000	No	Yes	2.00
99	1.98	1.32	100.00	2.99	0.54	1.70	21.63	0.00	21.63	4.000	No	Yes	2.00
100	2.00	1.32	100.00	2.99	0.54	1.70	21.85	0.00	21.85	4.000	No	Yes	2.00
101	2.02	1.33	100.00	2.97	0.54	1.70	21.80	0.00	21.80	4.000	No	Yes	2.00
102	2.04	1.32	99.70	2.96	0.54	1.70	22.02	0.00	22.02	4.000	No	Yes	2.00
103	2.06	1.33	98.18	2.94	0.54	1.70	21.86	0.00	21.86	4.000	No	Yes	2.00
104	2.08	1.32	97.45	2.93	0.54	1.70	22.00	0.00	22.00	4.000	No	Yes	2.00
105	2.10	1.30	97.63	2.93	0.54	1.70	21.50	0.00	21.50	4.000	No	Yes	2.00
106	2.12	1.28	98.53	2.94	0.54	1.70	21.00	0.00	21.00	4.000	No	Yes	2.00
107	2.14	1.25	99.92	2.96	0.54	1.70	20.79	0.00	20.79	4.000	No	Yes	2.00
108	2.16	1.23	100.00	2.98	0.54	1.70	20.29	0.00	20.29	4.000	No	Yes	2.00
109	2.18	1.21	100.00	3.00	0.55	1.70	19.74	0.00	19.74	4.000	No	Yes	2.00
110	2.20	1.18	100.00	3.01	0.55	1.69	19.39	0.00	19.39	4.000	No	Yes	2.00
111	2.22	1.17	100.00	3.01	0.55	1.68	18.97	0.00	18.97	4.000	No	Yes	2.00
112	2.24	1.17	100.00	3.01	0.55	1.68	18.87	0.00	18.87	4.000	No	Yes	2.00
113	2.26	1.17	100.00	2.99	0.55	1.67	18.84	0.00	18.84	4.000	No	Yes	2.00
114	2.28	1.18	100.00	2.98	0.55	1.66	18.85	0.00	18.85	4.000	No	Yes	2.00
115	2.30	1.19	100.00	2.96	0.55	1.65	19.03	0.00	19.03	4.000	No	Yes	2.00
116	2.32	1.19	100.00	2.96	0.55	1.64	18.93	0.00	18.93	4.000	No	Yes	2.00
117	2.35	1.19	100.00	2.97	0.55	1.63	18.66	0.00	18.66	4.000	No	Yes	2.00
118	2.36	1.18	100.00	2.99	0.55	1.63	18.67	0.00	18.67	4.000	No	Yes	2.00
119	2.38	1.19	100.00	3.00	0.55	1.62	18.55	0.00	18.55	4.000	No	Yes	2.00
120	2.40	1.20	100.00	3.00	0.55	1.61	18.62	0.00	18.62	4.000	No	Yes	2.00
121	2.42	1.22	100.00	3.00	0.55	1.60	18.97	0.00	18.97	4.000	No	Yes	2.00
122	2.44	1.24	100.00	2.99	0.55	1.60	19.22	0.00	19.22	4.000	No	Yes	2.00
123	2.46	1.25	100.00	2.99	0.55	1.59	19.06	0.00	19.06	4.000	No	Yes	2.00
124	2.48	1.27	100.00	2.98	0.55	1.58	19.23	0.00	19.23	4.000	No	Yes	2.00
125	2.50	1.30	100.00	2.97	0.55	1.57	19.97	0.00	19.97	4.000	No	Yes	2.00
126	2.52	1.34	99.60	2.96	0.55	1.57	20.22	0.00	20.22	4.000	No	Yes	2.00
127	2.54	1.37	99.02	2.95	0.54	1.56	20.70	0.00	20.70	4.000	No	Yes	2.00
128	2.56	1.40	98.34	2.94	0.54	1.56	21.25	0.00	21.25	4.000	No	Yes	2.00
129	2.58	1.43	97.90	2.94	0.54	1.55	21.52	0.00	21.52	4.000	No	Yes	2.00
130	2.60	1.45	97.77	2.93	0.54	1.55	21.90	0.00	21.90	4.000	No	Yes	2.00
131	2.62	1.45	98.21	2.94	0.54	1.54	21.91	0.00	21.91	4.000	No	Yes	2.00
132	2.64	1.44	98.92	2.95	0.54	1.54	21.46	0.00	21.46	4.000	No	Yes	2.00
133	2.66	1.43	99.43	2.96	0.54	1.54	21.25	0.00	21.25	4.000	No	Yes	2.00
134	2.68	1.39	100.00	2.97	0.54	1.54	21.36	0.00	21.36	4.000	No	Yes	2.00
135	2.70	1.34	100.00	2.99	0.55	1.54	19.92	0.00	19.92	4.000	No	Yes	2.00
136	2.72	1.27	100.00	3.02	0.55	1.54	19.12	0.00	19.12	4.000	No	Yes	2.00
137	2.74	1.22	100.00	3.04	0.55	1.54	18.33	0.00	18.33	4.000	No	Yes	2.00
138	2.76	1.14	100.00	3.07	0.55	1.54	17.53	0.00	17.53	4.000	No	Yes	2.00
139	2.78	1.06	100.00	3.11	0.56	1.54	15.92	0.00	15.92	4.000	No	Yes	2.00
140	2.80	0.97	100.00	3.16	0.56	1.55	14.66	0.00	14.66	4.000	No	Yes	2.00
141	2.82	0.90	100.00	3.20	0.57	1.55	13.50	0.00	13.50	4.000	No	Yes	2.00
142	2.84	0.81	100.00	3.26	0.57	1.55	12.71	0.00	12.71	4.000	No	Yes	2.00
143	2.86	0.72	100.00	3.33	0.58	1.55	10.64	0.00	10.64	4.000	No	Yes	2.00
144	2.88	0.66	100.00	3.37	0.58	1.56	9.57	0.00	9.57	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.63	100.00	3.35	0.58	1.55	9.51	0.00	9.51	4.000	No	Yes	2.00
146	2.92	0.62	100.00	3.32	0.59	1.55	9.19	0.00	9.19	4.000	No	Yes	2.00
147	2.95	0.61	100.00	3.28	0.59	1.55	8.97	0.00	8.97	4.000	No	Yes	2.00
148	2.96	0.60	100.00	3.25	0.59	1.55	9.10	0.00	9.10	4.000	No	Yes	2.00
149	2.98	0.59	100.00	3.22	0.59	1.55	8.85	0.00	8.85	4.000	No	Yes	2.00
150	3.00	0.57	100.00	3.22	0.59	1.55	8.26	0.00	8.26	4.000	No	Yes	2.00
151	3.02	0.56	100.00	3.20	0.59	1.54	8.32	0.00	8.32	4.000	No	Yes	2.00
152	3.04	0.57	100.00	3.17	0.59	1.54	8.28	0.00	8.28	4.000	No	Yes	2.00
153	3.06	0.58	100.00	3.14	0.59	1.54	8.36	0.00	8.36	4.000	No	Yes	2.00
154	3.08	0.59	100.00	3.10	0.59	1.53	8.55	0.00	8.55	4.000	No	Yes	2.00
155	3.10	0.62	100.00	3.05	0.59	1.53	8.94	0.00	8.94	4.000	No	Yes	2.00
156	3.12	0.66	100.00	2.99	0.58	1.53	9.36	0.00	9.36	4.000	No	Yes	2.00
157	3.14	0.72	96.90	2.92	0.58	1.52	10.25	0.00	10.25	4.000	No	Yes	2.00
158	3.16	0.79	92.29	2.87	0.58	1.51	11.49	0.00	11.49	4.000	No	Yes	2.00
159	3.18	0.86	89.28	2.83	0.58	1.51	12.20	0.00	12.20	4.000	No	Yes	2.00
160	3.20	0.93	86.74	2.80	0.57	1.51	13.07	0.00	13.07	4.000	No	Yes	2.00
161	3.22	1.02	84.04	2.76	0.57	1.50	14.54	0.00	14.54	4.000	No	Yes	2.00
162	3.24	1.13	80.93	2.72	0.57	1.49	16.01	0.00	16.01	4.000	No	Yes	2.00
163	3.26	1.24	78.18	2.69	0.56	1.48	17.43	0.00	17.43	4.000	No	Yes	2.00
164	3.28	1.33	76.25	2.67	0.56	1.48	18.86	0.00	18.86	4.000	No	Yes	2.00
165	3.30	1.40	76.08	2.66	0.55	1.47	20.06	0.00	20.06	4.000	No	Yes	2.00
166	3.32	1.44	78.24	2.69	0.55	1.47	20.46	0.00	20.46	4.000	No	Yes	2.00
167	3.34	1.44	81.70	2.73	0.55	1.46	20.54	0.00	20.54	4.000	No	Yes	2.00
168	3.36	1.42	85.86	2.79	0.55	1.46	20.12	0.00	20.12	4.000	No	Yes	2.00
169	3.38	1.39	89.27	2.83	0.55	1.46	19.48	0.00	19.48	4.000	No	Yes	2.00
170	3.40	1.39	91.18	2.85	0.55	1.46	19.32	0.00	19.32	4.000	No	Yes	2.00
171	3.42	1.40	91.96	2.86	0.55	1.45	19.75	0.00	19.75	4.000	No	Yes	2.00
172	3.44	1.40	92.66	2.87	0.55	1.45	19.81	0.00	19.81	4.000	No	Yes	2.00
173	3.46	1.39	94.04	2.89	0.55	1.45	19.56	0.00	19.56	4.000	No	Yes	2.00
174	3.48	1.39	94.83	2.90	0.55	1.44	19.25	0.00	19.25	4.000	No	Yes	2.00
175	3.50	1.39	94.81	2.90	0.55	1.44	19.49	0.00	19.49	4.000	No	Yes	2.00
176	3.52	1.41	94.57	2.89	0.55	1.44	19.79	0.00	19.79	4.000	No	Yes	2.00
177	3.54	1.43	94.72	2.90	0.55	1.43	19.97	0.00	19.97	4.000	No	Yes	2.00
178	3.56	1.43	95.61	2.91	0.55	1.43	20.08	0.00	20.08	4.000	No	Yes	2.00
179	3.58	1.43	96.54	2.92	0.55	1.43	19.86	0.00	19.86	4.000	No	Yes	2.00
180	3.60	1.41	97.84	2.94	0.55	1.43	19.76	0.00	19.76	4.000	No	Yes	2.00
181	3.62	1.42	97.94	2.94	0.55	1.43	19.32	0.00	19.32	4.000	No	Yes	2.00
182	3.64	1.42	97.48	2.93	0.55	1.42	19.80	0.00	19.80	4.000	No	Yes	2.00
183	3.66	1.42	96.99	2.92	0.55	1.42	19.95	0.00	19.95	4.000	No	Yes	2.00
184	3.68	1.38	97.88	2.94	0.55	1.42	19.09	0.00	19.09	4.000	No	Yes	2.00
185	3.70	1.33	99.19	2.95	0.55	1.42	18.14	0.00	18.14	4.000	No	Yes	2.00
186	3.72	1.26	100.00	2.97	0.55	1.42	17.61	0.00	17.61	4.000	No	Yes	2.00
187	3.74	1.20	100.00	2.99	0.56	1.42	16.39	0.00	16.39	4.000	No	Yes	2.00
188	3.76	1.14	100.00	3.01	0.56	1.42	15.47	0.00	15.47	4.000	No	Yes	2.00
189	3.78	1.09	100.00	3.02	0.56	1.42	14.98	0.00	14.98	4.000	No	Yes	2.00
190	3.80	1.06	100.00	3.03	0.57	1.42	14.34	0.00	14.34	4.000	No	Yes	2.00
191	3.82	1.04	100.00	3.02	0.57	1.42	14.07	0.00	14.07	4.000	No	Yes	2.00
192	3.84	1.04	100.00	2.99	0.57	1.42	14.07	0.00	14.07	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	1.11	96.03	2.91	0.57	1.41	14.45	0.00	14.45	4.000	No	Yes	2.00
194	3.88	1.17	90.75	2.85	0.56	1.41	16.53	0.00	16.53	4.000	No	Yes	2.00
195	3.90	1.21	87.66	2.81	0.56	1.40	16.48	0.00	16.48	4.000	No	Yes	2.00
196	3.92	1.18	90.00	2.84	0.56	1.40	15.94	0.00	15.94	4.000	No	Yes	2.00
197	3.94	1.16	92.24	2.87	0.56	1.40	15.49	0.00	15.49	4.000	No	Yes	2.00
198	3.96	1.14	94.12	2.89	0.56	1.40	15.34	0.00	15.34	4.000	No	Yes	2.00
199	3.98	1.12	95.63	2.91	0.57	1.40	14.74	0.00	14.74	4.000	No	Yes	2.00
200	4.01	1.09	97.07	2.93	0.57	1.40	14.53	0.00	14.53	4.000	No	Yes	2.00
201	4.02	1.07	97.80	2.93	0.57	1.40	14.21	0.00	14.21	4.000	No	Yes	2.00
202	4.04	1.04	98.64	2.95	0.57	1.40	13.77	0.00	13.77	4.000	No	Yes	2.00
203	4.06	1.00	99.36	2.95	0.57	1.40	13.11	0.00	13.11	4.000	No	Yes	2.00
204	4.08	0.97	99.33	2.95	0.57	1.39	12.55	0.00	12.55	4.000	No	Yes	2.00
205	4.10	0.96	99.16	2.95	0.57	1.39	12.65	0.00	12.65	4.000	No	Yes	2.00
206	4.12	0.95	98.62	2.95	0.57	1.39	12.39	0.00	12.39	4.000	No	Yes	2.00
207	4.15	0.93	99.09	2.95	0.57	1.39	12.36	0.00	12.36	4.000	No	Yes	2.00
208	4.16	0.92	99.59	2.96	0.58	1.39	11.84	0.00	11.84	4.000	No	Yes	2.00
209	4.18	0.89	100.00	2.97	0.58	1.39	11.61	0.00	11.61	4.000	No	Yes	2.00
210	4.20	0.85	100.00	2.99	0.58	1.39	11.14	0.00	11.14	4.000	No	Yes	2.00
211	4.22	0.82	100.00	3.01	0.58	1.39	10.46	0.00	10.46	4.000	No	Yes	2.00
212	4.24	0.78	100.00	3.02	0.58	1.39	10.06	0.00	10.06	4.000	No	Yes	2.00
213	4.26	0.75	100.00	3.04	0.58	1.39	9.65	0.00	9.65	4.000	No	Yes	2.00
214	4.28	0.75	100.00	3.02	0.58	1.38	9.34	0.00	9.34	4.000	No	Yes	2.00
215	4.30	0.78	100.00	2.98	0.58	1.38	9.81	0.00	9.81	4.000	No	Yes	2.00
216	4.32	0.85	95.80	2.91	0.58	1.38	10.94	0.00	10.94	4.000	No	Yes	2.00
217	4.34	0.89	93.01	2.88	0.58	1.37	11.98	0.00	11.98	4.000	No	Yes	2.00
218	4.36	0.88	92.84	2.87	0.58	1.37	11.25	0.00	11.25	4.000	No	Yes	2.00
219	4.38	0.84	94.83	2.90	0.58	1.37	10.72	0.00	10.72	4.000	No	Yes	2.00
220	4.40	0.82	95.34	2.90	0.58	1.37	10.35	0.00	10.35	4.000	No	Yes	2.00
221	4.42	0.81	94.67	2.90	0.58	1.37	10.31	0.00	10.31	4.000	No	Yes	2.00
222	4.44	0.86	91.53	2.86	0.58	1.37	10.45	0.00	10.45	4.000	No	Yes	2.00
223	4.46	0.98	85.29	2.78	0.58	1.36	12.03	0.00	12.03	4.000	No	Yes	2.00
224	4.48	1.14	78.00	2.69	0.57	1.36	14.86	0.00	14.86	4.000	No	Yes	2.00
225	4.50	1.24	75.17	2.65	0.56	1.35	16.93	0.00	16.93	4.000	No	Yes	2.00
226	4.52	1.24	77.45	2.68	0.57	1.35	16.11	0.00	16.11	4.000	No	Yes	2.00
227	4.54	1.13	84.47	2.77	0.57	1.35	14.85	0.00	14.85	4.000	No	Yes	2.00
228	4.56	1.08	88.70	2.82	0.57	1.35	12.87	0.00	12.87	4.000	No	Yes	2.00
229	4.58	1.10	88.60	2.82	0.57	1.35	13.76	0.00	13.76	4.000	No	Yes	2.00
230	4.60	1.20	84.91	2.77	0.57	1.34	15.47	0.00	15.47	4.000	No	Yes	2.00
231	4.62	1.24	84.27	2.77	0.56	1.34	16.50	0.00	16.50	4.000	No	Yes	2.00
232	4.64	1.20	86.32	2.79	0.57	1.34	15.32	0.00	15.32	4.000	No	Yes	2.00
233	4.66	1.09	90.94	2.85	0.57	1.34	14.04	0.00	14.04	4.000	No	Yes	2.00
234	4.68	1.00	94.06	2.89	0.57	1.34	12.40	0.00	12.40	4.000	No	Yes	2.00
235	4.70	0.95	95.82	2.91	0.58	1.34	11.53	0.00	11.53	4.000	No	Yes	2.00
236	4.72	0.94	95.08	2.90	0.58	1.34	11.64	0.00	11.64	4.000	No	Yes	2.00
237	4.74	0.97	93.01	2.88	0.58	1.34	11.92	0.00	11.92	4.000	No	Yes	2.00
238	4.76	0.99	91.24	2.85	0.58	1.33	12.35	0.00	12.35	4.000	No	Yes	2.00
239	4.78	1.02	88.73	2.82	0.58	1.33	12.31	0.00	12.31	4.000	No	Yes	2.00
240	4.80	1.04	86.73	2.80	0.57	1.33	12.94	0.00	12.94	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	1.05	85.77	2.78	0.57	1.33	13.27	0.00	13.27	4.000	No	Yes	2.00
242	4.84	0.98	90.25	2.84	0.57	1.33	12.76	0.00	12.76	4.000	No	Yes	2.00
243	4.86	1.02	90.66	2.85	0.58	1.33	10.31	0.00	10.31	4.000	No	Yes	2.00
244	4.88	1.06	91.82	2.86	0.57	1.32	15.07	0.00	15.07	4.000	No	Yes	2.00
245	4.90	1.13	90.82	2.85	0.57	1.32	14.14	0.00	14.14	4.000	No	Yes	2.00
246	4.92	1.07	94.84	2.90	0.57	1.32	13.09	0.00	13.09	4.000	No	Yes	2.00
247	4.94	1.05	96.41	2.92	0.57	1.32	12.87	0.00	12.87	4.000	Yes	Yes	2.00
248	4.96	1.09	94.53	2.89	0.57	1.31	13.31	0.00	13.31	4.000	Yes	Yes	2.00
249	4.98	1.21	88.84	2.82	0.57	1.31	14.36	0.00	14.36	4.000	Yes	Yes	2.00
250	5.00	1.44	79.29	2.70	0.56	1.30	17.13	0.00	17.13	4.000	Yes	Yes	2.00
251	5.02	1.83	66.67	2.55	0.55	1.30	21.92	56.36	78.29	4.000	Yes	No	2.00
252	5.04	2.23	58.10	2.44	0.53	1.28	29.17	56.38	85.56	4.000	Yes	No	2.00
253	5.06	2.36	58.84	2.45	0.52	1.28	32.33	57.46	89.79	4.000	Yes	No	2.00
254	5.08	2.13	68.82	2.57	0.53	1.28	27.11	58.29	85.41	4.000	Yes	No	2.00
255	5.10	1.73	81.33	2.73	0.55	1.29	20.67	0.00	20.67	4.000	Yes	Yes	2.00
256	5.12	1.43	91.67	2.86	0.56	1.29	17.63	0.00	17.63	4.000	Yes	Yes	2.00
257	5.14	1.30	95.22	2.90	0.56	1.29	15.50	0.00	15.50	4.000	Yes	Yes	2.00
258	5.16	1.24	96.76	2.92	0.56	1.29	15.28	0.00	15.28	4.000	No	Yes	2.00
259	5.18	1.24	96.43	2.92	0.56	1.29	15.32	0.00	15.32	4.000	No	Yes	2.00
260	5.20	1.26	95.54	2.91	0.56	1.29	15.24	0.00	15.24	4.000	No	Yes	2.00
261	5.22	1.31	92.69	2.87	0.56	1.29	15.86	0.00	15.86	4.000	No	Yes	2.00
262	5.24	1.37	89.32	2.83	0.56	1.28	17.01	0.00	17.01	4.000	No	Yes	2.00
263	5.26	1.42	86.56	2.79	0.56	1.28	17.49	0.00	17.49	4.000	No	Yes	2.00
264	5.28	1.42	87.04	2.80	0.56	1.28	17.68	0.00	17.68	4.000	No	Yes	2.00
265	5.30	1.37	89.80	2.83	0.56	1.28	16.85	0.00	16.85	4.000	No	Yes	2.00
266	5.32	1.28	94.88	2.90	0.56	1.28	15.67	0.00	15.67	4.000	No	Yes	2.00
267	5.34	1.18	100.00	2.98	0.57	1.28	14.42	0.00	14.42	4.000	No	Yes	2.00
268	5.36	1.09	100.00	3.05	0.57	1.28	13.01	0.00	13.01	4.000	No	Yes	2.00
269	5.38	1.00	100.00	3.12	0.57	1.28	12.35	0.00	12.35	4.000	No	Yes	2.00
270	5.40	0.94	100.00	3.16	0.58	1.28	11.24	0.00	11.24	4.000	No	Yes	2.00
271	5.42	0.89	100.00	3.19	0.58	1.28	10.63	0.00	10.63	4.000	No	Yes	2.00
272	5.44	0.88	100.00	3.18	0.58	1.28	10.51	0.00	10.51	4.000	No	Yes	2.00
273	5.46	0.89	100.00	3.14	0.58	1.27	10.60	0.00	10.60	4.000	No	Yes	2.00
274	5.48	0.91	100.00	3.08	0.58	1.27	10.91	0.00	10.91	4.000	No	Yes	2.00
275	5.50	0.94	100.00	3.02	0.58	1.27	10.98	0.00	10.98	4.000	No	Yes	2.00
276	5.52	0.98	99.19	2.95	0.58	1.27	11.44	0.00	11.44	4.000	No	Yes	2.00
277	5.54	1.01	94.96	2.90	0.58	1.27	12.20	0.00	12.20	4.000	No	Yes	2.00
278	5.56	1.03	93.14	2.88	0.58	1.26	12.16	0.00	12.16	4.000	No	Yes	2.00
279	5.58	1.00	93.94	2.89	0.58	1.26	11.89	0.00	11.89	4.000	No	Yes	2.00
280	5.60	0.98	95.71	2.91	0.58	1.26	11.35	0.00	11.35	4.000	No	Yes	2.00
281	5.62	0.96	98.13	2.94	0.58	1.26	11.37	0.00	11.37	4.000	No	Yes	2.00
282	5.64	0.94	100.00	2.96	0.58	1.26	10.85	0.00	10.85	4.000	No	Yes	2.00
283	5.66	0.91	100.00	2.99	0.58	1.26	10.54	0.00	10.54	4.000	No	Yes	2.00
284	5.68	0.91	100.00	2.99	0.58	1.26	10.31	0.00	10.31	4.000	No	Yes	2.00
285	5.70	0.96	99.79	2.96	0.58	1.26	10.91	0.00	10.91	4.000	No	Yes	2.00
286	5.72	1.07	93.59	2.88	0.57	1.25	12.33	0.00	12.33	4.000	No	Yes	2.00
287	5.74	1.28	84.16	2.76	0.57	1.25	14.46	0.00	14.46	4.000	No	Yes	2.00
288	5.76	1.48	77.52	2.68	0.56	1.24	18.41	0.00	18.41	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	1.62	75.73	2.66	0.55	1.24	19.63	0.00	19.63	4.000	No	Yes	2.00
290	5.80	1.62	79.47	2.71	0.55	1.23	19.79	0.00	19.79	4.000	No	Yes	2.00
291	5.82	1.57	85.08	2.78	0.55	1.23	18.95	0.00	18.95	4.000	No	Yes	2.00
292	5.84	1.60	87.15	2.80	0.56	1.23	17.96	0.00	17.96	4.000	No	Yes	2.00
293	5.86	1.63	87.77	2.81	0.55	1.23	20.75	0.00	20.75	4.000	No	Yes	2.00
294	5.88	1.70	87.02	2.80	0.55	1.23	20.30	0.00	20.30	4.000	No	Yes	2.00
295	5.90	1.75	85.97	2.79	0.55	1.23	20.28	0.00	20.28	4.000	No	Yes	2.00
296	5.92	1.91	81.95	2.74	0.54	1.22	22.51	0.00	22.51	4.000	No	Yes	2.00
297	5.94	2.15	76.19	2.66	0.53	1.22	25.79	0.00	25.79	4.000	No	Yes	2.00
298	5.96	2.36	72.26	2.62	0.53	1.21	28.89	0.00	28.89	4.000	No	Yes	2.00
299	5.98	2.49	69.92	2.59	0.52	1.21	29.64	59.24	88.88	0.125	No	No	0.70
300	6.00	2.50	69.10	2.58	0.52	1.21	30.32	59.28	89.59	0.125	No	No	0.71
301	6.02	2.42	68.99	2.57	0.53	1.21	29.18	58.92	88.10	0.124	No	No	0.70
302	6.04	2.22	71.09	2.60	0.53	1.21	26.91	0.00	26.91	4.000	No	Yes	2.00
303	6.06	1.96	76.11	2.66	0.54	1.21	23.37	0.00	23.37	4.000	No	Yes	2.00
304	6.08	1.75	81.48	2.73	0.55	1.21	19.78	0.00	19.78	4.000	No	Yes	2.00
305	6.10	1.73	81.96	2.74	0.55	1.21	19.57	0.00	19.57	4.000	No	Yes	2.00
306	6.12	1.80	80.05	2.71	0.54	1.21	22.40	0.00	22.40	4.000	No	Yes	2.00
307	6.14	1.77	82.30	2.74	0.54	1.20	22.26	0.00	22.26	4.000	No	Yes	2.00
308	6.16	1.57	90.96	2.85	0.55	1.21	18.44	0.00	18.44	4.000	No	Yes	2.00
309	6.18	1.29	100.00	3.00	0.56	1.21	15.19	0.00	15.19	4.000	No	Yes	2.00
310	6.20	1.13	100.00	3.07	0.57	1.21	12.63	0.00	12.63	4.000	No	Yes	2.00
311	6.22	1.08	100.00	3.08	0.57	1.21	12.53	0.00	12.53	4.000	No	Yes	2.00
312	6.24	1.12	100.00	3.03	0.57	1.21	13.15	0.00	13.15	4.000	No	Yes	2.00
313	6.26	1.17	100.00	2.99	0.57	1.21	14.11	0.00	14.11	4.000	No	Yes	2.00
314	6.28	1.21	100.00	2.97	0.57	1.20	14.30	0.00	14.30	4.000	No	Yes	2.00
315	6.30	1.22	100.00	2.97	0.57	1.20	14.46	0.00	14.46	4.000	No	Yes	2.00
316	6.32	1.23	100.00	2.96	0.57	1.20	14.28	0.00	14.28	4.000	No	Yes	2.00
317	6.34	1.24	99.89	2.96	0.57	1.20	14.50	0.00	14.50	4.000	No	Yes	2.00
318	6.36	1.28	99.22	2.95	0.56	1.20	14.90	0.00	14.90	4.000	No	Yes	2.00
319	6.38	1.31	99.33	2.95	0.56	1.19	15.43	0.00	15.43	4.000	No	Yes	2.00
320	6.40	1.35	99.49	2.96	0.56	1.19	15.69	0.00	15.69	4.000	No	Yes	2.00
321	6.42	1.38	99.41	2.96	0.56	1.19	16.03	0.00	16.03	4.000	No	Yes	2.00
322	6.44	1.46	96.74	2.92	0.56	1.19	16.48	0.00	16.48	4.000	No	Yes	2.00
323	6.46	1.58	93.52	2.88	0.55	1.19	18.59	0.00	18.59	4.000	No	Yes	2.00
324	6.48	1.67	91.13	2.85	0.55	1.18	19.86	0.00	19.86	4.000	No	Yes	2.00
325	6.50	1.67	92.13	2.86	0.55	1.18	19.70	0.00	19.70	4.000	No	Yes	2.00
326	6.52	1.60	95.71	2.91	0.55	1.18	18.59	0.00	18.59	4.000	No	Yes	2.00
327	6.54	1.51	100.00	2.97	0.56	1.18	17.35	0.00	17.35	4.000	No	Yes	2.00
328	6.56	1.42	100.00	3.03	0.56	1.18	16.45	0.00	16.45	4.000	No	Yes	2.00
329	6.59	1.34	100.00	3.08	0.56	1.18	15.30	0.00	15.30	4.000	No	Yes	2.00
330	6.60	1.29	100.00	3.12	0.56	1.18	14.83	0.00	14.83	4.000	No	Yes	2.00
331	6.62	1.26	100.00	3.14	0.57	1.18	14.42	0.00	14.42	4.000	No	Yes	2.00
332	6.64	1.24	100.00	3.14	0.57	1.18	14.37	0.00	14.37	4.000	No	Yes	2.00
333	6.66	1.23	100.00	3.14	0.57	1.18	14.04	0.00	14.04	4.000	No	Yes	2.00
334	6.68	1.20	100.00	3.14	0.57	1.17	13.99	0.00	13.99	4.000	No	Yes	2.00
335	6.70	1.17	100.00	3.14	0.57	1.17	13.43	0.00	13.43	4.000	No	Yes	2.00
336	6.72	1.15	100.00	3.15	0.57	1.17	13.07	0.00	13.07	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	1.13	100.00	3.14	0.57	1.17	12.97	0.00	12.97	4.000	No	Yes	2.00
338	6.76	1.13	100.00	3.13	0.57	1.17	12.95	0.00	12.95	4.000	No	Yes	2.00
339	6.78	1.14	100.00	3.12	0.57	1.17	13.03	0.00	13.03	4.000	No	Yes	2.00
340	6.80	1.15	100.00	3.10	0.57	1.17	13.12	0.00	13.12	4.000	No	Yes	2.00
341	6.82	1.16	100.00	3.09	0.57	1.17	13.38	0.00	13.38	4.000	No	Yes	2.00
342	6.84	1.16	100.00	3.08	0.57	1.16	13.21	0.00	13.21	4.000	No	Yes	2.00
343	6.86	1.13	100.00	3.10	0.57	1.16	13.08	0.00	13.08	4.000	No	Yes	2.00
344	6.88	1.08	100.00	3.13	0.57	1.16	12.17	0.00	12.17	4.000	No	Yes	2.00
345	6.90	1.02	100.00	3.19	0.58	1.16	11.65	0.00	11.65	4.000	No	Yes	2.00
346	6.92	0.96	100.00	3.25	0.58	1.16	10.90	0.00	10.90	4.000	No	Yes	2.00
347	6.94	0.92	100.00	3.29	0.58	1.16	10.27	0.00	10.27	4.000	No	Yes	2.00
348	6.96	0.90	100.00	3.32	0.58	1.16	10.03	0.00	10.03	4.000	No	Yes	2.00
349	6.98	0.92	100.00	3.30	0.58	1.16	10.14	0.00	10.14	4.000	No	Yes	2.00
350	7.00	0.97	100.00	3.25	0.58	1.16	10.84	0.00	10.84	4.000	No	Yes	2.00
351	7.02	1.06	100.00	3.16	0.57	1.15	11.94	0.00	11.94	4.000	No	Yes	2.00
352	7.04	1.16	100.00	3.08	0.57	1.15	13.17	0.00	13.17	4.000	No	Yes	2.00
353	7.06	1.23	100.00	3.02	0.57	1.15	13.93	0.00	13.93	4.000	No	Yes	2.00
354	7.08	1.26	100.00	2.99	0.57	1.15	14.24	0.00	14.24	4.000	No	Yes	2.00
355	7.10	1.27	100.00	2.98	0.57	1.15	14.17	0.00	14.17	4.000	No	Yes	2.00
356	7.12	1.27	100.00	2.99	0.57	1.14	14.23	0.00	14.23	4.000	No	Yes	2.00
357	7.14	1.26	100.00	3.01	0.57	1.14	14.11	0.00	14.11	4.000	No	Yes	2.00
358	7.16	1.27	100.00	3.03	0.57	1.14	13.97	0.00	13.97	4.000	No	Yes	2.00
359	7.18	1.28	100.00	3.04	0.57	1.14	14.38	0.00	14.38	4.000	No	Yes	2.00
360	7.20	1.28	100.00	3.06	0.57	1.14	14.34	0.00	14.34	4.000	No	Yes	2.00
361	7.22	1.25	100.00	3.08	0.57	1.14	14.05	0.00	14.05	4.000	No	Yes	2.00
362	7.25	1.23	100.00	3.10	0.57	1.14	13.37	0.00	13.37	4.000	No	Yes	2.00
363	7.26	1.20	100.00	3.11	0.57	1.14	13.44	0.00	13.44	4.000	No	Yes	2.00
364	7.28	1.19	100.00	3.13	0.57	1.13	13.30	0.00	13.30	4.000	No	Yes	2.00
365	7.30	1.18	100.00	3.15	0.57	1.13	12.91	0.00	12.91	4.000	No	Yes	2.00
366	7.32	1.19	100.00	3.14	0.57	1.13	12.89	0.00	12.89	4.000	No	Yes	2.00
367	7.34	1.25	100.00	3.11	0.57	1.13	13.77	0.00	13.77	4.000	No	Yes	2.00
368	7.36	1.34	100.00	3.05	0.56	1.13	14.67	0.00	14.67	4.000	No	Yes	2.00
369	7.38	1.43	100.00	3.00	0.56	1.13	15.89	0.00	15.89	4.000	No	Yes	2.00
370	7.40	1.48	100.00	2.97	0.56	1.12	16.69	0.00	16.69	4.000	No	Yes	2.00
371	7.42	1.49	100.00	2.96	0.56	1.12	16.42	0.00	16.42	4.000	No	Yes	2.00
372	7.44	1.44	100.00	3.00	0.56	1.12	15.96	0.00	15.96	4.000	No	Yes	2.00
373	7.46	1.39	100.00	3.05	0.56	1.12	15.10	0.00	15.10	4.000	No	Yes	2.00
374	7.48	1.33	100.00	3.10	0.57	1.12	14.57	0.00	14.57	4.000	No	Yes	2.00
375	7.50	1.29	100.00	3.14	0.57	1.12	14.03	0.00	14.03	4.000	No	Yes	2.00
376	7.52	1.27	100.00	3.17	0.57	1.12	13.77	0.00	13.77	4.000	No	Yes	2.00
377	7.54	1.25	100.00	3.18	0.57	1.12	13.77	0.00	13.77	4.000	No	Yes	2.00
378	7.56	1.26	100.00	3.18	0.57	1.12	13.58	0.00	13.58	4.000	No	Yes	2.00
379	7.58	1.27	100.00	3.17	0.57	1.12	13.81	0.00	13.81	4.000	No	Yes	2.00
380	7.60	1.30	100.00	3.14	0.57	1.11	14.09	0.00	14.09	4.000	No	Yes	2.00
381	7.62	1.33	100.00	3.11	0.57	1.11	14.43	0.00	14.43	4.000	No	Yes	2.00
382	7.64	1.36	100.00	3.08	0.56	1.11	14.97	0.00	14.97	4.000	No	Yes	2.00
383	7.66	1.38	100.00	3.06	0.56	1.11	15.02	0.00	15.02	4.000	No	Yes	2.00
384	7.68	1.38	100.00	3.05	0.56	1.11	15.03	0.00	15.03	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	1.37	100.00	3.05	0.56	1.11	14.94	0.00	14.94	4.000	No	Yes	2.00
386	7.72	1.35	100.00	3.08	0.56	1.11	14.63	0.00	14.63	4.000	No	Yes	2.00
387	7.74	1.32	100.00	3.10	0.57	1.10	14.24	0.00	14.24	4.000	No	Yes	2.00
388	7.76	1.30	100.00	3.13	0.57	1.10	13.98	0.00	13.98	4.000	No	Yes	2.00
389	7.78	1.28	100.00	3.16	0.57	1.10	13.82	0.00	13.82	4.000	No	Yes	2.00
390	7.80	1.26	100.00	3.18	0.57	1.10	13.46	0.00	13.46	4.000	No	Yes	2.00
391	7.82	1.26	100.00	3.19	0.57	1.10	13.35	0.00	13.35	4.000	No	Yes	2.00
392	7.84	1.27	100.00	3.18	0.57	1.10	13.74	0.00	13.74	4.000	No	Yes	2.00
393	7.86	1.29	100.00	3.16	0.57	1.10	13.80	0.00	13.80	4.000	No	Yes	2.00
394	7.88	1.28	100.00	3.15	0.57	1.10	13.86	0.00	13.86	4.000	No	Yes	2.00
395	7.90	1.27	100.00	3.15	0.57	1.10	13.63	0.00	13.63	4.000	No	Yes	2.00
396	7.92	1.24	100.00	3.16	0.57	1.09	13.39	0.00	13.39	4.000	No	Yes	2.00
397	7.94	1.20	100.00	3.17	0.57	1.09	12.85	0.00	12.85	4.000	No	Yes	2.00
398	7.96	1.13	100.00	3.20	0.57	1.09	12.11	0.00	12.11	4.000	No	Yes	2.00
399	7.98	1.05	100.00	3.24	0.58	1.09	11.25	0.00	11.25	4.000	No	Yes	2.00
400	8.00	0.96	100.00	3.29	0.58	1.09	10.17	0.00	10.17	4.000	No	Yes	2.00
401	8.02	0.86	100.00	3.35	0.59	1.09	9.19	0.00	9.19	4.000	No	Yes	2.00
402	8.04	0.78	100.00	3.41	0.59	1.09	8.21	0.00	8.21	4.000	No	Yes	2.00
403	8.06	0.70	100.00	3.47	0.59	1.09	7.31	0.00	7.31	4.000	No	Yes	2.00
404	8.08	0.64	100.00	3.53	0.60	1.09	6.77	0.00	6.77	4.000	No	Yes	2.00
405	8.10	0.60	100.00	3.55	0.60	1.09	6.23	0.00	6.23	4.000	No	Yes	2.00
406	8.12	0.57	100.00	3.56	0.60	1.09	6.15	0.00	6.15	4.000	No	Yes	2.00
407	8.14	0.54	100.00	3.58	0.60	1.09	5.75	0.00	5.75	4.000	No	Yes	2.00
408	8.16	0.51	100.00	3.60	0.60	1.09	5.19	0.00	5.19	4.000	No	Yes	2.00
409	8.18	0.51	100.00	3.57	0.60	1.08	5.11	0.00	5.11	4.000	No	Yes	2.00
410	8.20	0.53	100.00	3.49	0.60	1.08	5.61	0.00	5.61	4.000	No	Yes	2.00
411	8.22	0.55	100.00	3.42	0.60	1.08	5.85	0.00	5.85	4.000	No	Yes	2.00
412	8.24	0.56	100.00	3.38	0.60	1.08	5.91	0.00	5.91	4.000	No	Yes	2.00
413	8.26	0.55	100.00	3.38	0.60	1.08	5.77	0.00	5.77	4.000	No	Yes	2.00
414	8.28	0.53	100.00	3.38	0.60	1.08	5.57	0.00	5.57	4.000	No	Yes	2.00
415	8.30	0.52	100.00	3.38	0.60	1.08	5.40	0.00	5.40	4.000	No	Yes	2.00
416	8.32	0.51	100.00	3.37	0.60	1.08	5.16	0.00	5.16	4.000	No	Yes	2.00
417	8.34	0.51	100.00	3.34	0.60	1.08	5.24	0.00	5.24	4.000	No	Yes	2.00
418	8.36	0.53	100.00	3.30	0.60	1.08	5.57	0.00	5.57	4.000	No	Yes	2.00
419	8.39	0.56	100.00	3.25	0.60	1.08	5.78	0.00	5.78	4.000	No	Yes	2.00
420	8.40	0.60	100.00	3.21	0.60	1.07	6.07	0.00	6.07	4.000	No	Yes	2.00
421	8.42	0.63	100.00	3.17	0.60	1.07	6.67	0.00	6.67	4.000	No	Yes	2.00
422	8.44	0.66	100.00	3.15	0.59	1.07	6.98	0.00	6.98	4.000	No	Yes	2.00
423	8.46	0.66	100.00	3.18	0.59	1.07	6.98	0.00	6.98	4.000	No	Yes	2.00
424	8.48	0.64	100.00	3.23	0.60	1.07	6.48	0.00	6.48	4.000	No	Yes	2.00
425	8.50	0.62	100.00	3.26	0.60	1.07	6.34	0.00	6.34	4.000	No	Yes	2.00
426	8.52	0.63	100.00	3.26	0.60	1.07	6.44	0.00	6.44	4.000	No	Yes	2.00
427	8.54	0.63	100.00	3.26	0.60	1.07	6.58	0.00	6.58	4.000	No	Yes	2.00
428	8.56	0.63	100.00	3.26	0.60	1.07	6.51	0.00	6.51	4.000	No	Yes	2.00
429	8.58	0.62	100.00	3.28	0.60	1.07	6.51	0.00	6.51	4.000	No	Yes	2.00
430	8.60	0.60	100.00	3.30	0.60	1.07	6.25	0.00	6.25	4.000	No	Yes	2.00
431	8.63	0.59	100.00	3.31	0.60	1.06	5.78	0.00	5.78	4.000	No	Yes	2.00
432	8.64	0.58	100.00	3.30	0.60	1.06	6.01	0.00	6.01	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	0.61	100.00	3.25	0.60	1.06	6.11	0.00	6.11	4.000	No	Yes	2.00
434	8.68	0.65	100.00	3.19	0.60	1.06	6.65	0.00	6.65	4.000	No	Yes	2.00
435	8.70	0.70	100.00	3.14	0.59	1.06	7.17	0.00	7.17	4.000	No	Yes	2.00
436	8.72	0.73	100.00	3.12	0.59	1.06	7.55	0.00	7.55	4.000	No	Yes	2.00
437	8.74	0.75	100.00	3.12	0.59	1.06	7.61	0.00	7.61	4.000	No	Yes	2.00
438	8.76	0.75	100.00	3.14	0.59	1.06	7.71	0.00	7.71	4.000	No	Yes	2.00
439	8.78	0.75	100.00	3.16	0.59	1.06	7.52	0.00	7.52	4.000	No	Yes	2.00
440	8.80	0.77	100.00	3.17	0.59	1.06	7.80	0.00	7.80	4.000	No	Yes	2.00
441	8.82	0.80	100.00	3.15	0.59	1.06	8.24	0.00	8.24	4.000	No	Yes	2.00
442	8.84	0.84	100.00	3.14	0.59	1.05	8.40	0.00	8.40	4.000	No	Yes	2.00
443	8.86	0.85	100.00	3.14	0.59	1.05	8.61	0.00	8.61	4.000	No	Yes	2.00
444	8.88	0.85	100.00	3.17	0.59	1.05	8.46	0.00	8.46	4.000	No	Yes	2.00
445	8.90	0.82	100.00	3.20	0.59	1.05	8.27	0.00	8.27	4.000	No	Yes	2.00
446	8.92	0.80	100.00	3.24	0.59	1.05	7.91	0.00	7.91	4.000	No	Yes	2.00
447	8.95	0.78	100.00	3.26	0.59	1.05	7.67	0.00	7.67	4.000	No	Yes	2.00
448	8.96	0.80	100.00	3.25	0.59	1.05	7.78	0.00	7.78	4.000	No	Yes	2.00
449	8.98	0.84	100.00	3.20	0.59	1.05	8.33	0.00	8.33	4.000	No	Yes	2.00
450	9.00	0.85	100.00	3.19	0.59	1.05	8.83	0.00	8.83	4.000	No	Yes	2.00
451	9.02	0.82	100.00	3.22	0.59	1.05	8.13	0.00	8.13	4.000	No	Yes	2.00
452	9.04	0.77	100.00	3.28	0.59	1.05	7.47	0.00	7.47	4.000	No	Yes	2.00
453	9.06	0.73	100.00	3.31	0.59	1.04	7.12	0.00	7.12	4.000	No	Yes	2.00
454	9.08	0.72	100.00	3.32	0.59	1.04	7.06	0.00	7.06	4.000	No	Yes	2.00
455	9.10	0.72	100.00	3.32	0.59	1.04	7.01	0.00	7.01	4.000	No	Yes	2.00
456	9.12	0.71	100.00	3.33	0.59	1.04	7.16	0.00	7.16	4.000	No	Yes	2.00
457	9.14	0.68	100.00	3.34	0.60	1.04	6.60	0.00	6.60	4.000	No	Yes	2.00
458	9.16	0.64	100.00	3.37	0.60	1.04	6.27	0.00	6.27	4.000	No	Yes	2.00
459	9.18	0.61	100.00	3.39	0.60	1.04	5.85	0.00	5.85	4.000	No	Yes	2.00
460	9.20	0.58	100.00	3.40	0.60	1.04	5.45	0.00	5.45	4.000	No	Yes	2.00
461	9.23	0.59	100.00	3.37	0.60	1.04	5.58	0.00	5.58	4.000	No	Yes	2.00
462	9.24	0.63	100.00	3.30	0.60	1.04	5.95	0.00	5.95	4.000	No	Yes	2.00
463	9.26	0.67	100.00	3.23	0.60	1.04	6.54	0.00	6.54	4.000	No	Yes	2.00
464	9.28	0.69	100.00	3.19	0.60	1.04	6.79	0.00	6.79	4.000	No	Yes	2.00
465	9.30	0.68	100.00	3.20	0.60	1.03	6.74	0.00	6.74	4.000	No	Yes	2.00
466	9.32	0.65	100.00	3.22	0.60	1.03	6.21	0.00	6.21	4.000	No	Yes	2.00
467	9.34	0.64	100.00	3.23	0.60	1.03	5.86	0.00	5.86	4.000	No	Yes	2.00
468	9.36	0.67	100.00	3.18	0.60	1.03	6.31	0.00	6.31	4.000	No	Yes	2.00
469	9.38	0.70	100.00	3.14	0.59	1.03	7.02	0.00	7.02	4.000	No	Yes	2.00
470	9.40	0.72	100.00	3.14	0.60	1.03	6.76	0.00	6.76	4.000	No	Yes	2.00
471	9.42	0.76	100.00	3.12	0.59	1.03	7.01	0.00	7.01	4.000	No	Yes	2.00
472	9.44	0.87	100.00	3.05	0.59	1.03	8.08	0.00	8.08	4.000	No	Yes	2.00
473	9.46	1.05	97.06	2.93	0.58	1.03	10.04	0.00	10.04	4.000	No	Yes	2.00
474	9.48	1.23	88.95	2.82	0.58	1.03	12.45	0.00	12.45	4.000	No	Yes	2.00
475	9.50	1.31	87.39	2.80	0.57	1.03	13.70	0.00	13.70	4.000	No	Yes	2.00
476	9.52	1.21	94.32	2.89	0.57	1.03	12.71	0.00	12.71	4.000	No	Yes	2.00
477	9.54	1.00	100.00	3.06	0.58	1.02	9.74	0.00	9.74	4.000	No	Yes	2.00
478	9.56	0.80	100.00	3.22	0.59	1.02	7.16	0.00	7.16	4.000	No	Yes	2.00
479	9.58	0.71	100.00	3.32	0.60	1.02	6.79	0.00	6.79	4.000	No	Yes	2.00
480	9.60	0.70	100.00	3.34	0.60	1.02	6.74	0.00	6.74	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	0.70	100.00	3.33	0.60	1.02	6.69	0.00	6.69	4.000	No	Yes	2.00
482	9.64	0.71	100.00	3.30	0.59	1.02	6.89	0.00	6.89	4.000	No	Yes	2.00
483	9.66	0.72	100.00	3.26	0.59	1.02	6.89	0.00	6.89	4.000	No	Yes	2.00
484	9.68	0.73	100.00	3.22	0.60	1.02	6.79	0.00	6.79	4.000	No	Yes	2.00
485	9.70	0.76	100.00	3.16	0.59	1.02	7.28	0.00	7.28	4.000	No	Yes	2.00
486	9.72	0.81	100.00	3.10	0.59	1.02	7.85	0.00	7.85	4.000	No	Yes	2.00
487	9.74	0.83	100.00	3.08	0.59	1.02	8.13	0.00	8.13	4.000	No	Yes	2.00
488	9.76	0.79	100.00	3.13	0.59	1.02	7.79	0.00	7.79	4.000	No	Yes	2.00
489	9.78	0.77	100.00	3.16	0.59	1.02	6.84	0.00	6.84	4.000	No	Yes	2.00
490	9.80	0.92	100.00	3.12	0.59	1.01	7.46	0.00	7.46	4.000	No	Yes	2.00
491	9.82	1.10	100.00	3.06	0.57	1.01	12.39	0.00	12.39	4.000	No	Yes	2.00
492	9.84	1.24	100.00	3.04	0.57	1.01	12.22	0.00	12.22	4.000	No	Yes	2.00
493	9.86	1.17	100.00	3.09	0.58	1.01	11.78	0.00	11.78	4.000	No	Yes	2.00
494	9.88	1.05	100.00	3.15	0.58	1.01	10.38	0.00	10.38	4.000	No	Yes	2.00
495	9.90	0.90	100.00	3.24	0.59	1.01	8.68	0.00	8.68	4.000	No	Yes	2.00
496	9.92	0.78	100.00	3.33	0.59	1.01	7.35	0.00	7.35	4.000	No	Yes	2.00
497	9.95	0.71	100.00	3.40	0.60	1.01	6.71	0.00	6.71	4.000	No	Yes	2.00
498	9.96	0.67	100.00	3.43	0.60	1.01	6.26	0.00	6.26	4.000	No	Yes	2.00
499	9.98	0.65	100.00	3.43	0.60	1.01	6.21	0.00	6.21	4.000	No	Yes	2.00
500	10.00	0.64	100.00	3.41	0.60	1.01	5.93	0.00	5.93	4.000	No	Yes	2.00
501	10.02	0.63	100.00	3.37	0.60	1.01	5.88	0.00	5.88	4.000	No	Yes	2.00
502	10.04	0.64	100.00	3.31	0.60	1.00	5.98	0.00	5.98	4.000	No	Yes	2.00
503	10.06	0.67	100.00	3.25	0.60	1.00	6.22	0.00	6.22	4.000	No	Yes	2.00
504	10.08	0.69	100.00	3.22	0.60	1.00	6.64	0.00	6.64	4.000	No	Yes	2.00
505	10.10	0.70	100.00	3.21	0.60	1.00	6.50	0.00	6.50	4.000	No	Yes	2.00
506	10.12	0.69	100.00	3.23	0.60	1.00	6.52	0.00	6.52	4.000	No	Yes	2.00
507	10.14	0.69	100.00	3.24	0.60	1.00	6.40	0.00	6.40	4.000	No	Yes	2.00
508	10.16	0.68	100.00	3.25	0.60	1.00	6.37	0.00	6.37	4.000	No	Yes	2.00
509	10.18	0.68	100.00	3.26	0.60	1.00	6.30	0.00	6.30	4.000	No	Yes	2.00
510	10.20	0.68	100.00	3.26	0.60	1.00	6.34	0.00	6.34	4.000	No	Yes	2.00
511	10.22	0.68	100.00	3.26	0.60	1.00	6.38	0.00	6.38	4.000	No	Yes	2.00
512	10.24	0.67	100.00	3.27	0.60	1.00	6.28	0.00	6.28	4.000	No	Yes	2.00
513	10.26	0.66	100.00	3.28	0.60	1.00	5.95	0.00	5.95	4.000	No	Yes	2.00
514	10.28	0.65	100.00	3.29	0.60	1.00	5.94	0.00	5.94	4.000	No	Yes	2.00
515	10.30	0.64	100.00	3.28	0.60	1.00	5.96	0.00	5.96	4.000	No	Yes	2.00
516	10.32	0.64	100.00	3.28	0.60	0.99	5.91	0.00	5.91	4.000	No	Yes	2.00
517	10.34	0.65	100.00	3.28	0.60	0.99	5.89	0.00	5.89	4.000	No	Yes	2.00
518	10.36	0.65	100.00	3.28	0.60	0.99	6.04	0.00	6.04	4.000	No	Yes	2.00
519	10.38	0.67	100.00	3.26	0.60	0.99	6.06	0.00	6.06	4.000	No	Yes	2.00
520	10.40	0.68	100.00	3.25	0.60	0.99	6.27	0.00	6.27	4.000	No	Yes	2.00
521	10.42	0.69	100.00	3.24	0.60	0.99	6.27	0.00	6.27	4.000	No	Yes	2.00
522	10.44	0.69	100.00	3.24	0.60	0.99	6.35	0.00	6.35	4.000	No	Yes	2.00
523	10.46	0.70	100.00	3.24	0.60	0.99	6.42	0.00	6.42	4.000	No	Yes	2.00
524	10.48	0.70	100.00	3.25	0.60	0.99	6.48	0.00	6.48	4.000	No	Yes	2.00
525	10.50	0.69	100.00	3.26	0.60	0.99	6.23	0.00	6.23	4.000	No	Yes	2.00
526	10.52	0.68	100.00	3.28	0.60	0.99	6.27	0.00	6.27	4.000	No	Yes	2.00
527	10.54	0.66	100.00	3.29	0.60	0.99	6.03	0.00	6.03	4.000	No	Yes	2.00
528	10.56	0.66	100.00	3.28	0.60	0.99	5.78	0.00	5.78	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	0.68	100.00	3.24	0.60	0.99	6.13	0.00	6.13	4.000	No	Yes	2.00
530	10.60	0.73	100.00	3.19	0.60	0.98	6.74	0.00	6.74	4.000	No	Yes	2.00
531	10.62	0.75	100.00	3.17	0.59	0.98	7.00	0.00	7.00	4.000	No	Yes	2.00
532	10.64	0.75	100.00	3.19	0.59	0.98	6.84	0.00	6.84	4.000	No	Yes	2.00
533	10.66	0.73	100.00	3.22	0.60	0.98	6.60	0.00	6.60	4.000	No	Yes	2.00
534	10.68	0.73	100.00	3.23	0.60	0.98	6.48	0.00	6.48	4.000	No	Yes	2.00
535	10.70	0.77	100.00	3.20	0.59	0.98	6.92	0.00	6.92	4.000	No	Yes	2.00
536	10.72	0.83	100.00	3.15	0.59	0.98	7.61	0.00	7.61	4.000	No	Yes	2.00
537	10.74	0.88	100.00	3.11	0.59	0.98	8.09	0.00	8.09	4.000	No	Yes	2.00
538	10.76	0.90	100.00	3.11	0.59	0.98	8.39	0.00	8.39	4.000	No	Yes	2.00
539	10.78	0.90	100.00	3.14	0.59	0.98	8.16	0.00	8.16	4.000	No	Yes	2.00
540	10.80	0.89	100.00	3.18	0.59	0.98	7.90	0.00	7.90	4.000	No	Yes	2.00
541	10.82	0.87	100.00	3.22	0.59	0.98	8.07	0.00	8.07	4.000	No	Yes	2.00
542	10.84	0.86	100.00	3.25	0.59	0.98	7.56	0.00	7.56	4.000	No	Yes	2.00
543	10.86	0.86	100.00	3.26	0.59	0.98	7.60	0.00	7.60	4.000	No	Yes	2.00
544	10.88	0.88	100.00	3.25	0.59	0.97	8.01	0.00	8.01	4.000	No	Yes	2.00
545	10.90	0.88	100.00	3.24	0.59	0.97	7.96	0.00	7.96	4.000	No	Yes	2.00
546	10.92	0.83	100.00	3.28	0.59	0.97	7.60	0.00	7.60	4.000	No	Yes	2.00
547	10.94	0.79	100.00	3.31	0.60	0.97	6.75	0.00	6.75	4.000	No	Yes	2.00
548	10.96	0.78	100.00	3.31	0.60	0.97	6.81	0.00	6.81	4.000	No	Yes	2.00
549	10.98	0.80	100.00	3.27	0.59	0.97	7.10	0.00	7.10	4.000	No	Yes	2.00
550	11.00	0.83	100.00	3.22	0.59	0.97	7.44	0.00	7.44	4.000	No	Yes	2.00
551	11.02	0.83	100.00	3.21	0.59	0.97	7.59	0.00	7.59	4.000	No	Yes	2.00
552	11.04	0.82	100.00	3.22	0.59	0.97	7.19	0.00	7.19	4.000	No	Yes	2.00
553	11.06	0.80	100.00	3.23	0.59	0.97	7.01	0.00	7.01	4.000	No	Yes	2.00
554	11.08	0.81	100.00	3.20	0.59	0.97	7.03	0.00	7.03	4.000	No	Yes	2.00
555	11.10	0.86	100.00	3.15	0.59	0.97	7.56	0.00	7.56	4.000	No	Yes	2.00
556	11.12	0.90	100.00	3.11	0.59	0.97	8.14	0.00	8.14	4.000	No	Yes	2.00
557	11.14	0.91	100.00	3.11	0.59	0.97	8.24	0.00	8.24	4.000	No	Yes	2.00
558	11.16	0.90	100.00	3.14	0.59	0.96	7.84	0.00	7.84	4.000	No	Yes	2.00
559	11.18	0.88	100.00	3.16	0.59	0.96	7.77	0.00	7.77	4.000	No	Yes	2.00
560	11.20	0.88	100.00	3.17	0.59	0.96	7.81	0.00	7.81	4.000	No	Yes	2.00
561	11.22	0.89	100.00	3.18	0.59	0.96	7.91	0.00	7.91	4.000	No	Yes	2.00
562	11.24	0.89	100.00	3.19	0.59	0.96	7.99	0.00	7.99	4.000	No	Yes	2.00
563	11.26	0.86	100.00	3.23	0.59	0.96	7.68	0.00	7.68	4.000	No	Yes	2.00
564	11.28	0.81	100.00	3.27	0.59	0.96	7.06	0.00	7.06	4.000	No	Yes	2.00
565	11.30	0.78	100.00	3.30	0.60	0.96	6.69	0.00	6.69	4.000	No	Yes	2.00
566	11.32	0.77	100.00	3.29	0.60	0.96	6.64	0.00	6.64	4.000	No	Yes	2.00
567	11.34	0.79	100.00	3.26	0.60	0.96	6.80	0.00	6.80	4.000	No	Yes	2.00
568	11.36	0.82	100.00	3.21	0.59	0.96	7.22	0.00	7.22	4.000	No	Yes	2.00
569	11.38	0.86	100.00	3.17	0.59	0.96	7.60	0.00	7.60	4.000	No	Yes	2.00
570	11.40	0.88	100.00	3.15	0.59	0.96	7.70	0.00	7.70	4.000	No	Yes	2.00
571	11.42	0.89	100.00	3.15	0.59	0.96	7.76	0.00	7.76	4.000	No	Yes	2.00
572	11.44	0.88	100.00	3.17	0.59	0.95	7.88	0.00	7.88	4.000	No	Yes	2.00
573	11.46	0.87	100.00	3.19	0.59	0.95	7.60	0.00	7.60	4.000	No	Yes	2.00
574	11.48	0.86	100.00	3.21	0.59	0.95	7.47	0.00	7.47	4.000	No	Yes	2.00
575	11.50	0.86	100.00	3.21	0.59	0.95	7.44	0.00	7.44	4.000	No	Yes	2.00
576	11.52	0.88	100.00	3.20	0.59	0.95	7.73	0.00	7.73	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	0.92	100.00	3.17	0.59	0.95	8.00	0.00	8.00	4.000	No	Yes	2.00
578	11.56	0.94	100.00	3.15	0.59	0.95	8.36	0.00	8.36	4.000	No	Yes	2.00
579	11.58	0.95	100.00	3.15	0.59	0.95	8.35	0.00	8.35	4.000	No	Yes	2.00
580	11.60	0.96	100.00	3.15	0.59	0.95	8.37	0.00	8.37	4.000	No	Yes	2.00
581	11.62	0.97	100.00	3.16	0.59	0.95	8.51	0.00	8.51	4.000	No	Yes	2.00
582	11.64	0.97	100.00	3.17	0.59	0.95	8.48	0.00	8.48	4.000	No	Yes	2.00
583	11.66	0.98	100.00	3.18	0.59	0.95	8.51	0.00	8.51	4.000	No	Yes	2.00
584	11.68	0.99	100.00	3.17	0.59	0.95	8.63	0.00	8.63	4.000	No	Yes	2.00
585	11.70	1.03	100.00	3.15	0.59	0.95	8.88	0.00	8.88	4.000	No	Yes	2.00
586	11.72	1.07	100.00	3.13	0.58	0.95	9.53	0.00	9.53	4.000	No	Yes	2.00
587	11.74	1.11	100.00	3.11	0.58	0.95	9.69	0.00	9.69	4.000	No	Yes	2.00
588	11.76	1.12	100.00	3.11	0.58	0.94	9.93	0.00	9.93	4.000	No	Yes	2.00
589	11.78	1.12	100.00	3.13	0.58	0.94	9.88	0.00	9.88	4.000	No	Yes	2.00
590	11.80	1.10	100.00	3.16	0.58	0.94	9.76	0.00	9.76	4.000	No	Yes	2.00
591	11.82	1.07	100.00	3.20	0.59	0.94	9.27	0.00	9.27	4.000	No	Yes	2.00
592	11.84	1.05	100.00	3.22	0.59	0.94	9.07	0.00	9.07	4.000	No	Yes	2.00
593	11.86	1.06	100.00	3.23	0.59	0.94	9.21	0.00	9.21	4.000	No	Yes	2.00
594	11.88	1.05	100.00	3.23	0.58	0.94	9.39	0.00	9.39	4.000	No	Yes	2.00
595	11.90	1.04	100.00	3.24	0.59	0.94	9.03	0.00	9.03	4.000	No	Yes	2.00
596	11.92	1.02	100.00	3.27	0.59	0.94	8.89	0.00	8.89	4.000	No	Yes	2.00
597	11.94	1.01	100.00	3.27	0.59	0.94	8.69	0.00	8.69	4.000	No	Yes	2.00
598	11.96	1.01	100.00	3.27	0.59	0.94	8.85	0.00	8.85	4.000	No	Yes	2.00
599	11.98	1.02	100.00	3.26	0.59	0.94	8.80	0.00	8.80	4.000	No	Yes	2.00
600	12.00	1.03	100.00	3.26	0.59	0.94	8.90	0.00	8.90	4.000	No	Yes	2.00
601	12.02	1.05	100.00	3.24	0.59	0.93	9.18	0.00	9.18	4.000	No	Yes	2.00
602	12.04	1.08	100.00	3.22	0.58	0.93	9.34	0.00	9.34	4.000	No	Yes	2.00
603	12.06	1.10	100.00	3.20	0.58	0.93	9.56	0.00	9.56	4.000	No	Yes	2.00
604	12.08	1.12	100.00	3.19	0.58	0.93	9.74	0.00	9.74	4.000	No	Yes	2.00
605	12.10	1.13	100.00	3.18	0.58	0.93	9.87	0.00	9.87	4.000	No	Yes	2.00
606	12.12	1.15	100.00	3.18	0.58	0.93	9.99	0.00	9.99	4.000	No	Yes	2.00
607	12.14	1.16	100.00	3.19	0.58	0.93	10.10	0.00	10.10	4.000	No	Yes	2.00
608	12.16	1.16	100.00	3.20	0.58	0.93	10.07	0.00	10.07	4.000	No	Yes	2.00
609	12.18	1.15	100.00	3.22	0.58	0.93	9.95	0.00	9.95	4.000	No	Yes	2.00
610	12.20	1.14	100.00	3.23	0.58	0.93	9.88	0.00	9.88	4.000	No	Yes	2.00
611	12.22	1.14	100.00	3.24	0.58	0.93	9.93	0.00	9.93	4.000	No	Yes	2.00
612	12.24	1.13	100.00	3.24	0.58	0.93	9.82	0.00	9.82	4.000	No	Yes	2.00
613	12.26	1.13	100.00	3.24	0.58	0.93	9.73	0.00	9.73	4.000	No	Yes	2.00
614	12.28	1.12	100.00	3.24	0.58	0.93	9.67	0.00	9.67	4.000	No	Yes	2.00
615	12.30	1.12	100.00	3.23	0.58	0.92	9.73	0.00	9.73	4.000	No	Yes	2.00
616	12.32	1.11	100.00	3.23	0.58	0.92	9.57	0.00	9.57	4.000	No	Yes	2.00
617	12.34	1.11	100.00	3.23	0.58	0.92	9.46	0.00	9.46	4.000	No	Yes	2.00
618	12.36	1.10	100.00	3.23	0.58	0.92	9.61	0.00	9.61	4.000	No	Yes	2.00
619	12.38	1.11	100.00	3.23	0.58	0.92	9.38	0.00	9.38	4.000	No	Yes	2.00
620	12.40	1.11	100.00	3.23	0.58	0.92	9.59	0.00	9.59	4.000	No	Yes	2.00
621	12.42	1.12	100.00	3.21	0.58	0.92	9.64	0.00	9.64	4.000	No	Yes	2.00
622	12.44	1.13	100.00	3.20	0.58	0.92	9.78	0.00	9.78	4.000	No	Yes	2.00
623	12.46	1.14	100.00	3.20	0.58	0.92	9.83	0.00	9.83	4.000	No	Yes	2.00
624	12.48	1.16	100.00	3.19	0.58	0.92	9.90	0.00	9.90	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	1.17	100.00	3.18	0.58	0.92	10.12	0.00	10.12	4.000	No	Yes	2.00
626	12.52	1.19	100.00	3.17	0.58	0.92	10.17	0.00	10.17	4.000	No	Yes	2.00
627	12.54	1.21	100.00	3.17	0.58	0.92	10.41	0.00	10.41	4.000	No	Yes	2.00
628	12.56	1.22	100.00	3.17	0.58	0.92	10.52	0.00	10.52	4.000	No	Yes	2.00
629	12.58	1.22	100.00	3.18	0.58	0.92	10.47	0.00	10.47	4.000	No	Yes	2.00
630	12.60	1.22	100.00	3.19	0.58	0.91	10.52	0.00	10.52	4.000	No	Yes	2.00
631	12.62	1.23	100.00	3.20	0.58	0.91	10.51	0.00	10.51	4.000	No	Yes	2.00
632	12.64	1.24	100.00	3.21	0.58	0.91	10.67	0.00	10.67	4.000	No	Yes	2.00
633	12.66	1.26	100.00	3.21	0.58	0.91	10.84	0.00	10.84	4.000	No	Yes	2.00
634	12.68	1.26	100.00	3.22	0.58	0.91	10.98	0.00	10.98	4.000	No	Yes	2.00
635	12.70	1.25	100.00	3.24	0.58	0.91	10.74	0.00	10.74	4.000	No	Yes	2.00
636	12.72	1.23	100.00	3.27	0.58	0.91	10.53	0.00	10.53	4.000	No	Yes	2.00
637	12.74	1.23	100.00	3.27	0.58	0.91	10.33	0.00	10.33	4.000	No	Yes	2.00
638	12.76	1.24	100.00	3.26	0.58	0.91	10.67	0.00	10.67	4.000	No	Yes	2.00
639	12.78	1.30	100.00	3.22	0.58	0.91	10.90	0.00	10.90	4.000	No	Yes	2.00
640	12.80	1.35	100.00	3.19	0.58	0.91	11.71	0.00	11.71	4.000	No	Yes	2.00
641	12.82	1.39	100.00	3.17	0.57	0.91	11.99	0.00	11.99	4.000	No	Yes	2.00
642	12.84	1.40	100.00	3.17	0.57	0.91	12.02	0.00	12.02	4.000	No	Yes	2.00
643	12.86	1.39	100.00	3.17	0.57	0.91	12.05	0.00	12.05	4.000	No	Yes	2.00
644	12.88	1.37	100.00	3.19	0.58	0.91	11.84	0.00	11.84	4.000	No	Yes	2.00
645	12.90	1.36	100.00	3.21	0.58	0.90	11.50	0.00	11.50	4.000	No	Yes	2.00
646	12.92	1.35	100.00	3.22	0.58	0.90	11.57	0.00	11.57	4.000	No	Yes	2.00
647	12.94	1.36	100.00	3.21	0.58	0.90	11.74	0.00	11.74	4.000	No	Yes	2.00
648	12.96	1.37	100.00	3.20	0.58	0.90	11.71	0.00	11.71	4.000	No	Yes	2.00
649	12.98	1.37	100.00	3.20	0.57	0.90	11.92	0.00	11.92	4.000	No	Yes	2.00
650	13.00	1.37	100.00	3.19	0.58	0.90	11.73	0.00	11.73	4.000	No	Yes	2.00
651	13.02	1.36	100.00	3.19	0.58	0.90	11.75	0.00	11.75	4.000	No	Yes	2.00
652	13.04	1.35	100.00	3.20	0.58	0.90	11.62	0.00	11.62	4.000	No	Yes	2.00
653	13.06	1.34	100.00	3.21	0.58	0.90	11.51	0.00	11.51	4.000	No	Yes	2.00
654	13.08	1.34	100.00	3.21	0.58	0.90	11.38	0.00	11.38	4.000	No	Yes	2.00
655	13.10	1.35	100.00	3.20	0.58	0.90	11.65	0.00	11.65	4.000	No	Yes	2.00
656	13.12	1.36	100.00	3.19	0.58	0.90	11.61	0.00	11.61	4.000	No	Yes	2.00
657	13.14	1.36	100.00	3.19	0.58	0.90	11.66	0.00	11.66	4.000	No	Yes	2.00
658	13.16	1.36	100.00	3.19	0.58	0.90	11.75	0.00	11.75	4.000	No	Yes	2.00
659	13.19	1.36	100.00	3.19	0.58	0.89	11.55	0.00	11.55	4.000	No	Yes	2.00
660	13.20	1.37	100.00	3.19	0.58	0.89	11.70	0.00	11.70	4.000	No	Yes	2.00
661	13.22	1.38	100.00	3.19	0.58	0.89	11.83	0.00	11.83	4.000	No	Yes	2.00
662	13.24	1.37	100.00	3.20	0.58	0.89	11.86	0.00	11.86	4.000	No	Yes	2.00
663	13.26	1.35	100.00	3.22	0.58	0.89	11.61	0.00	11.61	4.000	No	Yes	2.00
664	13.28	1.31	100.00	3.25	0.58	0.89	11.08	0.00	11.08	4.000	No	Yes	2.00
665	13.30	1.28	100.00	3.27	0.58	0.89	10.87	0.00	10.87	4.000	No	Yes	2.00
666	13.32	1.25	100.00	3.29	0.58	0.89	10.79	0.00	10.79	4.000	No	Yes	2.00
667	13.34	1.22	100.00	3.31	0.58	0.89	10.36	0.00	10.36	4.000	No	Yes	2.00
668	13.36	1.19	100.00	3.32	0.58	0.89	10.11	0.00	10.11	4.000	No	Yes	2.00
669	13.38	1.16	100.00	3.34	0.58	0.89	9.88	0.00	9.88	4.000	No	Yes	2.00
670	13.40	1.14	100.00	3.34	0.58	0.89	9.65	0.00	9.65	4.000	No	Yes	2.00
671	13.42	1.12	100.00	3.35	0.58	0.89	9.60	0.00	9.60	4.000	No	Yes	2.00
672	13.44	1.09	100.00	3.37	0.59	0.88	9.14	0.00	9.14	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	1.05	100.00	3.38	0.59	0.88	8.83	0.00	8.83	4.000	No	Yes	2.00
674	13.48	1.02	100.00	3.39	0.59	0.88	8.67	0.00	8.67	4.000	No	Yes	2.00
675	13.50	1.00	100.00	3.39	0.59	0.88	8.36	0.00	8.36	4.000	No	Yes	2.00
676	13.52	0.97	100.00	3.40	0.59	0.88	8.10	0.00	8.10	4.000	No	Yes	2.00
677	13.54	0.94	100.00	3.40	0.59	0.88	7.91	0.00	7.91	4.000	No	Yes	2.00
678	13.56	0.91	100.00	3.41	0.59	0.88	7.55	0.00	7.55	4.000	No	Yes	2.00
679	13.58	0.87	100.00	3.44	0.59	0.88	7.25	0.00	7.25	4.000	No	Yes	2.00
680	13.60	0.84	100.00	3.45	0.59	0.88	6.89	0.00	6.89	4.000	No	Yes	2.00
681	13.62	0.81	100.00	3.46	0.60	0.88	6.67	0.00	6.67	4.000	No	Yes	2.00
682	13.64	0.80	100.00	3.46	0.60	0.88	6.62	0.00	6.62	4.000	No	Yes	2.00
683	13.66	0.80	100.00	3.44	0.60	0.88	6.44	0.00	6.44	4.000	No	Yes	2.00
684	13.68	0.80	100.00	3.42	0.60	0.88	6.63	0.00	6.63	4.000	No	Yes	2.00
685	13.70	0.81	100.00	3.41	0.60	0.87	6.67	0.00	6.67	4.000	No	Yes	2.00
686	13.72	0.81	100.00	3.41	0.60	0.87	6.65	0.00	6.65	4.000	No	Yes	2.00
687	13.74	0.79	100.00	3.42	0.60	0.87	6.49	0.00	6.49	4.000	No	Yes	2.00
688	13.76	0.81	100.00	3.36	0.60	0.87	6.25	0.00	6.25	4.000	No	Yes	2.00
689	13.78	0.84	100.00	3.32	0.59	0.87	6.99	0.00	6.99	4.000	No	Yes	2.00
690	13.80	0.85	100.00	3.30	0.59	0.87	6.89	0.00	6.89	4.000	No	Yes	2.00
691	13.82	0.81	100.00	3.35	0.60	0.87	6.34	0.00	6.34	4.000	No	Yes	2.00
692	13.84	0.77	100.00	3.40	0.60	0.87	6.05	0.00	6.05	4.000	No	Yes	2.00
693	13.86	0.74	100.00	3.42	0.60	0.87	5.73	0.00	5.73	4.000	No	Yes	2.00
694	13.88	0.72	100.00	3.44	0.60	0.87	5.61	0.00	5.61	4.000	No	Yes	2.00
695	13.90	0.71	100.00	3.45	0.60	0.87	5.44	0.00	5.44	4.000	No	Yes	2.00
696	13.92	0.71	100.00	3.44	0.60	0.87	5.51	0.00	5.51	4.000	No	Yes	2.00
697	13.94	0.72	100.00	3.41	0.60	0.87	5.43	0.00	5.43	4.000	No	Yes	2.00
698	13.96	0.74	100.00	3.37	0.60	0.87	5.68	0.00	5.68	4.000	No	Yes	2.00
699	13.98	0.77	100.00	3.32	0.60	0.87	5.95	0.00	5.95	4.000	No	Yes	2.00
700	14.00	0.81	100.00	3.27	0.60	0.87	6.20	0.00	6.20	4.000	No	Yes	2.00
701	14.02	0.83	100.00	3.24	0.60	0.87	6.60	0.00	6.60	4.000	No	Yes	2.00
702	14.04	0.85	100.00	3.22	0.60	0.87	6.62	0.00	6.62	4.000	No	Yes	2.00
703	14.06	0.87	100.00	3.20	0.60	0.87	6.69	0.00	6.69	4.000	No	Yes	2.00
704	14.08	0.88	100.00	3.20	0.59	0.86	7.02	0.00	7.02	4.000	No	Yes	2.00
705	14.11	0.87	100.00	3.23	0.59	0.86	6.88	0.00	6.88	4.000	No	Yes	2.00
706	14.12	0.84	100.00	3.26	0.60	0.86	6.40	0.00	6.40	4.000	No	Yes	2.00
707	14.14	0.83	100.00	3.28	0.60	0.86	6.36	0.00	6.36	4.000	No	Yes	2.00
708	14.16	0.85	100.00	3.26	0.60	0.86	6.60	0.00	6.60	4.000	No	Yes	2.00
709	14.18	0.86	100.00	3.25	0.60	0.86	6.77	0.00	6.77	4.000	No	Yes	2.00
710	14.20	0.84	100.00	3.28	0.60	0.86	6.64	0.00	6.64	4.000	No	Yes	2.00
711	14.22	0.80	100.00	3.31	0.60	0.86	6.07	0.00	6.07	4.000	No	Yes	2.00
712	14.24	0.78	100.00	3.34	0.60	0.86	5.86	0.00	5.86	4.000	No	Yes	2.00
713	14.26	0.79	100.00	3.32	0.60	0.86	5.93	0.00	5.93	4.000	No	Yes	2.00
714	14.28	0.81	100.00	3.29	0.60	0.86	6.30	0.00	6.30	4.000	No	Yes	2.00
715	14.30	0.85	100.00	3.26	0.60	0.86	6.51	0.00	6.51	4.000	No	Yes	2.00
716	14.32	0.87	100.00	3.24	0.59	0.86	6.91	0.00	6.91	4.000	No	Yes	2.00
717	14.34	0.88	100.00	3.24	0.60	0.86	6.79	0.00	6.79	4.000	No	Yes	2.00
718	14.36	0.88	100.00	3.24	0.60	0.86	6.79	0.00	6.79	4.000	No	Yes	2.00
719	14.38	0.90	100.00	3.23	0.59	0.86	6.82	0.00	6.82	4.000	No	Yes	2.00
720	14.40	0.92	100.00	3.21	0.59	0.86	7.13	0.00	7.13	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	0.94	100.00	3.19	0.59	0.86	7.33	0.00	7.33	4.000	No	Yes	2.00
722	14.44	0.96	100.00	3.18	0.59	0.86	7.45	0.00	7.45	4.000	No	Yes	2.00
723	14.46	0.96	100.00	3.17	0.59	0.86	7.44	0.00	7.44	4.000	No	Yes	2.00
724	14.48	0.98	100.00	3.16	0.59	0.86	7.52	0.00	7.52	4.000	No	Yes	2.00
725	14.50	0.99	100.00	3.16	0.59	0.86	7.93	0.00	7.93	4.000	No	Yes	2.00
726	14.52	0.97	100.00	3.19	0.59	0.85	7.66	0.00	7.66	4.000	No	Yes	2.00
727	14.54	0.94	100.00	3.23	0.59	0.85	6.99	0.00	6.99	4.000	No	Yes	2.00
728	14.56	0.93	100.00	3.25	0.59	0.85	7.20	0.00	7.20	4.000	No	Yes	2.00
729	14.58	0.96	100.00	3.24	0.59	0.85	7.42	0.00	7.42	4.000	No	Yes	2.00
730	14.60	0.98	100.00	3.24	0.59	0.85	7.59	0.00	7.59	4.000	No	Yes	2.00
731	14.62	0.99	100.00	3.23	0.59	0.85	7.60	0.00	7.60	4.000	No	Yes	2.00
732	14.64	1.01	100.00	3.22	0.59	0.85	7.87	0.00	7.87	4.000	No	Yes	2.00
733	14.66	1.03	100.00	3.19	0.59	0.85	7.96	0.00	7.96	4.000	No	Yes	2.00
734	14.68	1.04	100.00	3.18	0.59	0.85	8.01	0.00	8.01	4.000	No	Yes	2.00
735	14.70	1.06	100.00	3.17	0.59	0.85	8.27	0.00	8.27	4.000	No	Yes	2.00
736	14.72	1.07	100.00	3.18	0.59	0.85	8.25	0.00	8.25	4.000	No	Yes	2.00
737	14.74	1.00	100.00	3.27	0.59	0.85	8.24	0.00	8.24	4.000	No	Yes	2.00
738	14.76	1.00	100.00	3.30	0.60	0.85	6.52	0.00	6.52	4.000	No	Yes	2.00
739	14.79	1.00	100.00	3.31	0.59	0.85	8.20	0.00	8.20	4.000	No	Yes	2.00
740	14.80	1.06	100.00	3.26	0.59	0.85	8.27	0.00	8.27	4.000	No	Yes	2.00
741	14.82	1.05	100.00	3.27	0.59	0.85	8.08	0.00	8.08	4.000	No	Yes	2.00
742	14.84	1.03	100.00	3.29	0.59	0.85	7.92	0.00	7.92	4.000	No	Yes	2.00
743	14.86	1.02	100.00	3.30	0.59	0.85	7.90	0.00	7.90	4.000	No	Yes	2.00
744	14.88	1.02	100.00	3.31	0.59	0.85	7.78	0.00	7.78	4.000	No	Yes	2.00
745	14.90	1.00	100.00	3.32	0.59	0.84	7.77	0.00	7.77	4.000	No	Yes	2.00
746	14.92	0.98	100.00	3.34	0.59	0.84	7.60	0.00	7.60	4.000	No	Yes	2.00
747	14.94	0.95	100.00	3.37	0.59	0.84	7.23	0.00	7.23	4.000	No	Yes	2.00
748	14.96	0.91	100.00	3.40	0.59	0.84	6.94	0.00	6.94	4.000	No	Yes	2.00
749	14.99	0.88	100.00	3.43	0.60	0.84	6.71	0.00	6.71	4.000	No	Yes	2.00
750	15.00	0.85	100.00	3.44	0.60	0.84	6.31	0.00	6.31	4.000	No	Yes	2.00
751	15.02	0.85	100.00	3.44	0.60	0.84	6.36	0.00	6.36	4.000	No	Yes	2.00
752	15.04	0.85	100.00	3.41	0.60	0.84	6.52	0.00	6.52	4.000	No	Yes	2.00
753	15.06	0.86	100.00	3.39	0.60	0.84	6.46	0.00	6.46	4.000	No	Yes	2.00
754	15.08	0.85	100.00	3.38	0.60	0.84	6.49	0.00	6.49	4.000	No	Yes	2.00
755	15.10	0.85	100.00	3.38	0.60	0.84	6.37	0.00	6.37	4.000	No	Yes	2.00
756	15.12	0.83	100.00	3.38	0.60	0.84	6.26	0.00	6.26	4.000	No	Yes	2.00
757	15.14	0.84	100.00	3.36	0.60	0.84	6.18	0.00	6.18	4.000	No	Yes	2.00
758	15.16	0.88	100.00	3.32	0.60	0.84	6.55	0.00	6.55	4.000	No	Yes	2.00
759	15.18	0.95	100.00	3.25	0.59	0.84	7.24	0.00	7.24	4.000	No	Yes	2.00
760	15.20	1.02	100.00	3.19	0.59	0.84	7.76	0.00	7.76	4.000	No	Yes	2.00
761	15.22	1.06	100.00	3.15	0.59	0.84	8.18	0.00	8.18	4.000	No	Yes	2.00
762	15.24	1.09	100.00	3.13	0.59	0.84	8.40	0.00	8.40	4.000	No	Yes	2.00
763	15.26	1.09	100.00	3.13	0.59	0.84	8.42	0.00	8.42	4.000	No	Yes	2.00
764	15.28	1.09	100.00	3.15	0.59	0.84	8.26	0.00	8.26	4.000	No	Yes	2.00
765	15.30	1.09	100.00	3.16	0.59	0.84	8.26	0.00	8.26	4.000	No	Yes	2.00
766	15.32	1.11	100.00	3.16	0.59	0.83	8.51	0.00	8.51	4.000	No	Yes	2.00
767	15.34	1.13	100.00	3.18	0.59	0.83	8.75	0.00	8.75	4.000	No	Yes	2.00
768	15.36	1.12	100.00	3.21	0.59	0.83	8.62	0.00	8.62	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	1.08	100.00	3.25	0.59	0.83	8.37	0.00	8.37	4.000	No	Yes	2.00
770	15.40	1.07	100.00	3.27	0.59	0.83	7.80	0.00	7.80	4.000	No	Yes	2.00
771	15.42	1.09	100.00	3.26	0.59	0.83	8.21	0.00	8.21	4.000	No	Yes	2.00
772	15.44	1.16	100.00	3.21	0.59	0.83	8.97	0.00	8.97	4.000	No	Yes	2.00
773	15.46	1.24	100.00	3.17	0.58	0.83	9.56	0.00	9.56	4.000	No	Yes	2.00
774	15.48	1.31	100.00	3.13	0.58	0.83	9.96	0.00	9.96	4.000	No	Yes	2.00
775	15.50	1.41	100.00	3.08	0.58	0.83	10.80	0.00	10.80	4.000	No	Yes	2.00
776	15.52	1.53	100.00	3.02	0.57	0.83	12.22	0.00	12.22	4.000	No	Yes	2.00
777	15.54	1.69	100.00	2.96	0.57	0.83	13.38	0.00	13.38	4.000	No	Yes	2.00
778	15.56	1.79	98.80	2.95	0.56	0.84	15.24	0.00	15.24	4.000	No	Yes	2.00
779	15.58	1.74	100.00	2.99	0.56	0.83	14.91	0.00	14.91	4.000	No	Yes	2.00
780	15.60	1.52	100.00	3.10	0.57	0.83	12.39	0.00	12.39	4.000	No	Yes	2.00
781	15.62	1.27	100.00	3.23	0.58	0.83	9.84	0.00	9.84	4.000	No	Yes	2.00
782	15.64	1.08	100.00	3.33	0.59	0.83	8.55	0.00	8.55	4.000	No	Yes	2.00
783	15.66	0.95	100.00	3.41	0.59	0.82	7.52	0.00	7.52	4.000	No	Yes	2.00
784	15.68	0.85	100.00	3.49	0.60	0.82	6.57	0.00	6.57	4.000	No	Yes	2.00
785	15.70	0.78	100.00	3.55	0.60	0.82	6.01	0.00	6.01	4.000	No	Yes	2.00
786	15.72	0.75	100.00	3.57	0.60	0.82	5.73	0.00	5.73	4.000	No	Yes	2.00
787	15.74	0.76	100.00	3.52	0.60	0.82	5.93	0.00	5.93	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.15	2.00	0.00	9.93	0.03	0.00	0.16	2.00	0.00	9.92	0.01	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.41	2.00	0.00	9.80	0.03	0.00
0.42	2.00	0.00	9.79	0.01	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.99	2.00	0.00	9.51	0.03	0.00	1.00	2.00	0.00	9.50	0.01	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.05	2.00	0.00	9.48	0.03	0.00
1.07	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.01	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.35	2.00	0.00	8.82	0.03	0.00	2.36	2.00	0.00	8.82	0.01	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.95	2.00	0.00	8.53	0.03	0.00	2.96	2.00	0.00	8.52	0.01	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.01	2.00	0.00	8.00	0.03	0.00
4.02	2.00	0.00	7.99	0.01	0.00	4.04	2.00	0.00	7.98	0.02	0.00
4.06	2.00	0.00	7.97	0.02	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.15	2.00	0.00	7.93	0.03	0.00	4.16	2.00	0.00	7.92	0.01	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.50	2.00	0.00	7.75	0.02	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.86	2.00	0.00	7.07	0.02	0.00	5.88	2.00	0.00	7.06	0.02	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	0.70	0.30	7.01	0.02	0.04	6.00	0.71	0.29	7.00	0.02	0.04
6.02	0.70	0.30	6.99	0.02	0.04	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.59	2.00	0.00	6.71	0.03	0.00	6.60	2.00	0.00	6.70	0.01	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.25	2.00	0.00	6.38	0.03	0.00
7.26	2.00	0.00	6.37	0.01	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.39	2.00	0.00	5.81	0.03	0.00	8.40	2.00	0.00	5.80	0.01	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	2.00	0.00	5.75	0.02	0.00	8.52	2.00	0.00	5.74	0.02	0.00
8.54	2.00	0.00	5.73	0.02	0.00	8.56	2.00	0.00	5.72	0.02	0.00
8.58	2.00	0.00	5.71	0.02	0.00	8.60	2.00	0.00	5.70	0.02	0.00
8.63	2.00	0.00	5.68	0.03	0.00	8.64	2.00	0.00	5.68	0.01	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.95	2.00	0.00	5.53	0.03	0.00	8.96	2.00	0.00	5.52	0.01	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.23	2.00	0.00	5.39	0.03	0.00	9.24	2.00	0.00	5.38	0.01	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.95	2.00	0.00	5.03	0.03	0.00	9.96	2.00	0.00	5.02	0.01	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.02	2.00	0.00	4.99	0.02	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.92	2.00	0.00	4.04	0.02	0.00
11.94	2.00	0.00	4.03	0.02	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.90	2.00	0.00	3.55	0.02	0.00	12.92	2.00	0.00	3.54	0.02	0.00
12.94	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.02	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.19	2.00	0.00	3.41	0.03	0.00	13.20	2.00	0.00	3.40	0.01	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.80	2.00	0.00	3.10	0.02	0.00
13.82	2.00	0.00	3.09	0.02	0.00	13.84	2.00	0.00	3.08	0.02	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.11	2.00	0.00	2.95	0.03	0.00	14.12	2.00	0.00	2.94	0.01	0.00
14.14	2.00	0.00	2.93	0.02	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.79	2.00	0.00	2.61	0.03	0.00	14.80	2.00	0.00	2.60	0.01	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.84	2.00	0.00	2.58	0.02	0.00
14.86	2.00	0.00	2.57	0.02	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.99	2.00	0.00	2.51	0.03	0.00	15.00	2.00	0.00	2.50	0.01	0.00
15.02	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.16	2.00	0.00	2.42	0.02	0.00
15.18	2.00	0.00	2.41	0.02	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00
15.62	2.00	0.00	2.19	0.02	0.00	15.64	2.00	0.00	2.18	0.02	0.00
15.66	2.00	0.00	2.17	0.02	0.00	15.68	2.00	0.00	2.16	0.02	0.00
15.70	2.00	0.00	2.15	0.02	0.00	15.72	2.00	0.00	2.14	0.02	0.00
15.74	2.00	0.00	2.13	0.02	0.00						

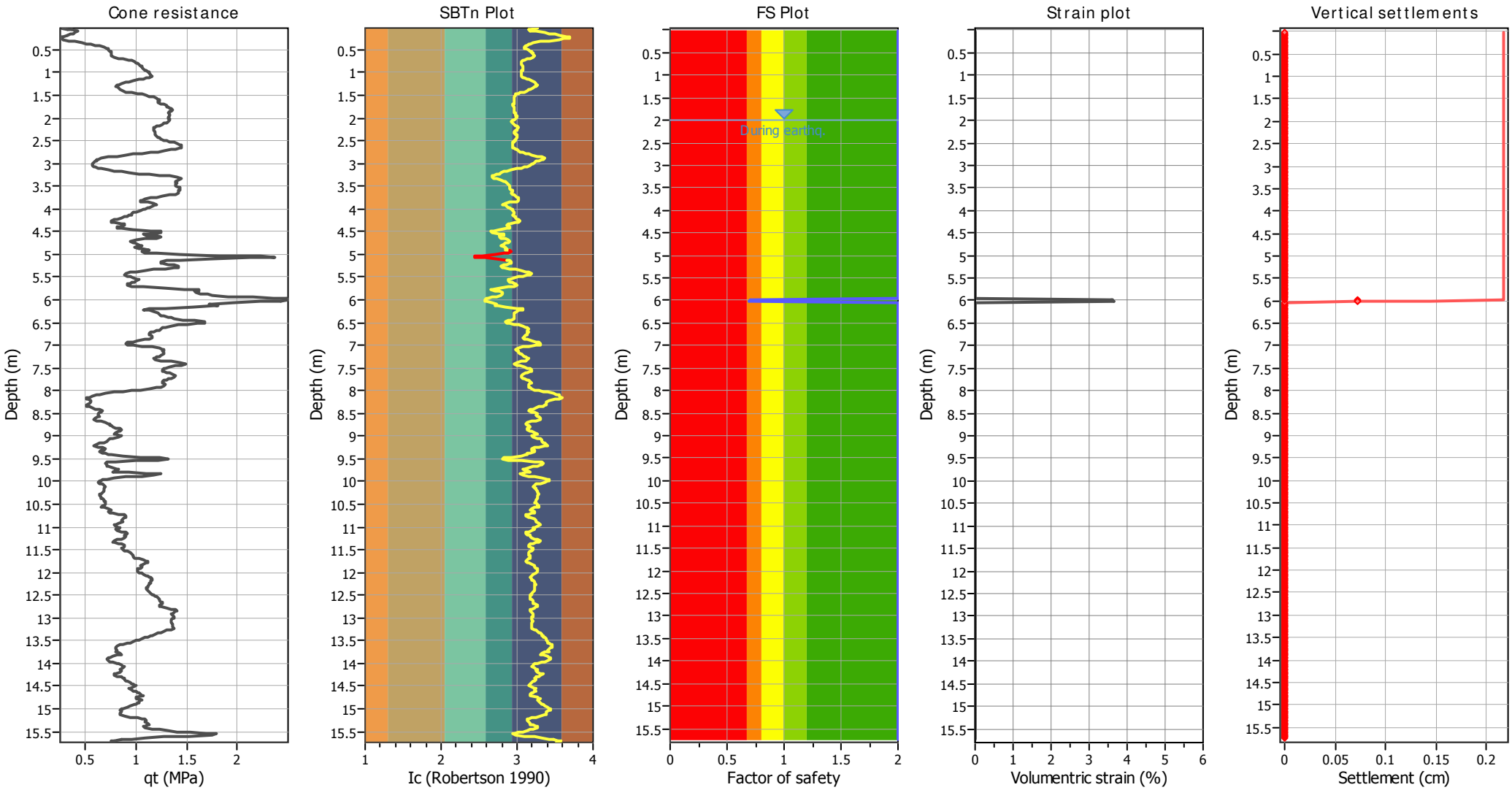
Overall liquefaction potential: 0.12

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.00	21.85	2.00	0.00	1.00	0.00	2.02	21.80	2.00	0.00	1.00	0.00
2.04	22.02	2.00	0.00	1.00	0.00	2.06	21.86	2.00	0.00	1.00	0.00
2.08	22.00	2.00	0.00	1.00	0.00	2.10	21.50	2.00	0.00	1.00	0.00
2.12	21.00	2.00	0.00	1.00	0.00	2.14	20.79	2.00	0.00	1.00	0.00
2.16	20.29	2.00	0.00	1.00	0.00	2.18	19.74	2.00	0.00	1.00	0.00
2.20	19.39	2.00	0.00	1.00	0.00	2.22	18.97	2.00	0.00	1.00	0.00
2.24	18.87	2.00	0.00	1.00	0.00	2.26	18.84	2.00	0.00	1.00	0.00
2.28	18.85	2.00	0.00	1.00	0.00	2.30	19.03	2.00	0.00	1.00	0.00
2.32	18.93	2.00	0.00	1.00	0.00	2.35	18.66	2.00	0.00	1.00	0.00
2.36	18.67	2.00	0.00	1.00	0.00	2.38	18.55	2.00	0.00	1.00	0.00
2.40	18.62	2.00	0.00	1.00	0.00	2.42	18.97	2.00	0.00	1.00	0.00
2.44	19.22	2.00	0.00	1.00	0.00	2.46	19.06	2.00	0.00	1.00	0.00
2.48	19.23	2.00	0.00	1.00	0.00	2.50	19.97	2.00	0.00	1.00	0.00
2.52	20.22	2.00	0.00	1.00	0.00	2.54	20.70	2.00	0.00	1.00	0.00
2.56	21.25	2.00	0.00	1.00	0.00	2.58	21.52	2.00	0.00	1.00	0.00
2.60	21.90	2.00	0.00	1.00	0.00	2.62	21.91	2.00	0.00	1.00	0.00
2.64	21.46	2.00	0.00	1.00	0.00	2.66	21.25	2.00	0.00	1.00	0.00
2.68	21.36	2.00	0.00	1.00	0.00	2.70	19.92	2.00	0.00	1.00	0.00
2.72	19.12	2.00	0.00	1.00	0.00	2.74	18.33	2.00	0.00	1.00	0.00
2.76	17.53	2.00	0.00	1.00	0.00	2.78	15.92	2.00	0.00	1.00	0.00
2.80	14.66	2.00	0.00	1.00	0.00	2.82	13.50	2.00	0.00	1.00	0.00
2.84	12.71	2.00	0.00	1.00	0.00	2.86	10.64	2.00	0.00	1.00	0.00
2.88	9.57	2.00	0.00	1.00	0.00	2.90	9.51	2.00	0.00	1.00	0.00
2.92	9.19	2.00	0.00	1.00	0.00	2.95	8.97	2.00	0.00	1.00	0.00
2.96	9.10	2.00	0.00	1.00	0.00	2.98	8.85	2.00	0.00	1.00	0.00
3.00	8.26	2.00	0.00	1.00	0.00	3.02	8.32	2.00	0.00	1.00	0.00
3.04	8.28	2.00	0.00	1.00	0.00	3.06	8.36	2.00	0.00	1.00	0.00
3.08	8.55	2.00	0.00	1.00	0.00	3.10	8.94	2.00	0.00	1.00	0.00
3.12	9.36	2.00	0.00	1.00	0.00	3.14	10.25	2.00	0.00	1.00	0.00
3.16	11.49	2.00	0.00	1.00	0.00	3.18	12.20	2.00	0.00	1.00	0.00
3.20	13.07	2.00	0.00	1.00	0.00	3.22	14.54	2.00	0.00	1.00	0.00
3.24	16.01	2.00	0.00	1.00	0.00	3.26	17.43	2.00	0.00	1.00	0.00
3.28	18.86	2.00	0.00	1.00	0.00	3.30	20.06	2.00	0.00	1.00	0.00
3.32	20.46	2.00	0.00	1.00	0.00	3.34	20.54	2.00	0.00	1.00	0.00
3.36	20.12	2.00	0.00	1.00	0.00	3.38	19.48	2.00	0.00	1.00	0.00
3.40	19.32	2.00	0.00	1.00	0.00	3.42	19.75	2.00	0.00	1.00	0.00
3.44	19.81	2.00	0.00	1.00	0.00	3.46	19.56	2.00	0.00	1.00	0.00
3.48	19.25	2.00	0.00	1.00	0.00	3.50	19.49	2.00	0.00	1.00	0.00
3.52	19.79	2.00	0.00	1.00	0.00	3.54	19.97	2.00	0.00	1.00	0.00
3.56	20.08	2.00	0.00	1.00	0.00	3.58	19.86	2.00	0.00	1.00	0.00
3.60	19.76	2.00	0.00	1.00	0.00	3.62	19.32	2.00	0.00	1.00	0.00
3.64	19.80	2.00	0.00	1.00	0.00	3.66	19.95	2.00	0.00	1.00	0.00
3.68	19.09	2.00	0.00	1.00	0.00	3.70	18.14	2.00	0.00	1.00	0.00
3.72	17.61	2.00	0.00	1.00	0.00	3.74	16.39	2.00	0.00	1.00	0.00
3.76	15.47	2.00	0.00	1.00	0.00	3.78	14.98	2.00	0.00	1.00	0.00
3.80	14.34	2.00	0.00	1.00	0.00	3.82	14.07	2.00	0.00	1.00	0.00
3.84	14.07	2.00	0.00	1.00	0.00	3.86	14.45	2.00	0.00	1.00	0.00
3.88	16.53	2.00	0.00	1.00	0.00	3.90	16.48	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.92	15.94	2.00	0.00	1.00	0.00	3.94	15.49	2.00	0.00	1.00	0.00
3.96	15.34	2.00	0.00	1.00	0.00	3.98	14.74	2.00	0.00	1.00	0.00
4.01	14.53	2.00	0.00	1.00	0.00	4.02	14.21	2.00	0.00	1.00	0.00
4.04	13.77	2.00	0.00	1.00	0.00	4.06	13.11	2.00	0.00	1.00	0.00
4.08	12.55	2.00	0.00	1.00	0.00	4.10	12.65	2.00	0.00	1.00	0.00
4.12	12.39	2.00	0.00	1.00	0.00	4.15	12.36	2.00	0.00	1.00	0.00
4.16	11.84	2.00	0.00	1.00	0.00	4.18	11.61	2.00	0.00	1.00	0.00
4.20	11.14	2.00	0.00	1.00	0.00	4.22	10.46	2.00	0.00	1.00	0.00
4.24	10.06	2.00	0.00	1.00	0.00	4.26	9.65	2.00	0.00	1.00	0.00
4.28	9.34	2.00	0.00	1.00	0.00	4.30	9.81	2.00	0.00	1.00	0.00
4.32	10.94	2.00	0.00	1.00	0.00	4.34	11.98	2.00	0.00	1.00	0.00
4.36	11.25	2.00	0.00	1.00	0.00	4.38	10.72	2.00	0.00	1.00	0.00
4.40	10.35	2.00	0.00	1.00	0.00	4.42	10.31	2.00	0.00	1.00	0.00
4.44	10.45	2.00	0.00	1.00	0.00	4.46	12.03	2.00	0.00	1.00	0.00
4.48	14.86	2.00	0.00	1.00	0.00	4.50	16.93	2.00	0.00	1.00	0.00
4.52	16.11	2.00	0.00	1.00	0.00	4.54	14.85	2.00	0.00	1.00	0.00
4.56	12.87	2.00	0.00	1.00	0.00	4.58	13.76	2.00	0.00	1.00	0.00
4.60	15.47	2.00	0.00	1.00	0.00	4.62	16.50	2.00	0.00	1.00	0.00
4.64	15.32	2.00	0.00	1.00	0.00	4.66	14.04	2.00	0.00	1.00	0.00
4.68	12.40	2.00	0.00	1.00	0.00	4.70	11.53	2.00	0.00	1.00	0.00
4.72	11.64	2.00	0.00	1.00	0.00	4.74	11.92	2.00	0.00	1.00	0.00
4.76	12.35	2.00	0.00	1.00	0.00	4.78	12.31	2.00	0.00	1.00	0.00
4.80	12.94	2.00	0.00	1.00	0.00	4.82	13.27	2.00	0.00	1.00	0.00
4.84	12.76	2.00	0.00	1.00	0.00	4.86	10.31	2.00	0.00	1.00	0.00
4.88	15.07	2.00	0.00	1.00	0.00	4.90	14.14	2.00	0.00	1.00	0.00
4.92	13.09	2.00	0.00	1.00	0.00	4.94	12.87	2.00	0.00	1.00	0.00
4.96	13.31	2.00	0.00	1.00	0.00	4.98	14.36	2.00	0.00	1.00	0.00
5.00	17.13	2.00	0.00	1.00	0.00	5.02	78.29	2.00	0.00	1.00	0.00
5.04	85.56	2.00	0.00	1.00	0.00	5.06	89.79	2.00	0.00	1.00	0.00
5.08	85.41	2.00	0.00	1.00	0.00	5.10	20.67	2.00	0.00	1.00	0.00
5.12	17.63	2.00	0.00	1.00	0.00	5.14	15.50	2.00	0.00	1.00	0.00
5.16	15.28	2.00	0.00	1.00	0.00	5.18	15.32	2.00	0.00	1.00	0.00
5.20	15.24	2.00	0.00	1.00	0.00	5.22	15.86	2.00	0.00	1.00	0.00
5.24	17.01	2.00	0.00	1.00	0.00	5.26	17.49	2.00	0.00	1.00	0.00
5.28	17.68	2.00	0.00	1.00	0.00	5.30	16.85	2.00	0.00	1.00	0.00
5.32	15.67	2.00	0.00	1.00	0.00	5.34	14.42	2.00	0.00	1.00	0.00
5.36	13.01	2.00	0.00	1.00	0.00	5.38	12.35	2.00	0.00	1.00	0.00
5.40	11.24	2.00	0.00	1.00	0.00	5.42	10.63	2.00	0.00	1.00	0.00
5.44	10.51	2.00	0.00	1.00	0.00	5.46	10.60	2.00	0.00	1.00	0.00
5.48	10.91	2.00	0.00	1.00	0.00	5.50	10.98	2.00	0.00	1.00	0.00
5.52	11.44	2.00	0.00	1.00	0.00	5.54	12.20	2.00	0.00	1.00	0.00
5.56	12.16	2.00	0.00	1.00	0.00	5.58	11.89	2.00	0.00	1.00	0.00
5.60	11.35	2.00	0.00	1.00	0.00	5.62	11.37	2.00	0.00	1.00	0.00
5.64	10.85	2.00	0.00	1.00	0.00	5.66	10.54	2.00	0.00	1.00	0.00
5.68	10.31	2.00	0.00	1.00	0.00	5.70	10.91	2.00	0.00	1.00	0.00
5.72	12.33	2.00	0.00	1.00	0.00	5.74	14.46	2.00	0.00	1.00	0.00
5.76	18.41	2.00	0.00	1.00	0.00	5.78	19.63	2.00	0.00	1.00	0.00
5.80	19.79	2.00	0.00	1.00	0.00	5.82	18.95	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.84	17.96	2.00	0.00	1.00	0.00	5.86	20.75	2.00	0.00	1.00	0.00
5.88	20.30	2.00	0.00	1.00	0.00	5.90	20.28	2.00	0.00	1.00	0.00
5.92	22.51	2.00	0.00	1.00	0.00	5.94	25.79	2.00	0.00	1.00	0.00
5.96	28.89	2.00	0.00	1.00	0.00	5.98	88.88	0.70	3.62	1.00	0.07
6.00	89.59	0.71	3.59	1.00	0.07	6.02	88.10	0.70	3.65	1.00	0.07
6.04	26.91	2.00	0.00	1.00	0.00	6.06	23.37	2.00	0.00	1.00	0.00
6.08	19.78	2.00	0.00	1.00	0.00	6.10	19.57	2.00	0.00	1.00	0.00
6.12	22.40	2.00	0.00	1.00	0.00	6.14	22.26	2.00	0.00	1.00	0.00
6.16	18.44	2.00	0.00	1.00	0.00	6.18	15.19	2.00	0.00	1.00	0.00
6.20	12.63	2.00	0.00	1.00	0.00	6.22	12.53	2.00	0.00	1.00	0.00
6.24	13.15	2.00	0.00	1.00	0.00	6.26	14.11	2.00	0.00	1.00	0.00
6.28	14.30	2.00	0.00	1.00	0.00	6.30	14.46	2.00	0.00	1.00	0.00
6.32	14.28	2.00	0.00	1.00	0.00	6.34	14.50	2.00	0.00	1.00	0.00
6.36	14.90	2.00	0.00	1.00	0.00	6.38	15.43	2.00	0.00	1.00	0.00
6.40	15.69	2.00	0.00	1.00	0.00	6.42	16.03	2.00	0.00	1.00	0.00
6.44	16.48	2.00	0.00	1.00	0.00	6.46	18.59	2.00	0.00	1.00	0.00
6.48	19.86	2.00	0.00	1.00	0.00	6.50	19.70	2.00	0.00	1.00	0.00
6.52	18.59	2.00	0.00	1.00	0.00	6.54	17.35	2.00	0.00	1.00	0.00
6.56	16.45	2.00	0.00	1.00	0.00	6.59	15.30	2.00	0.00	1.00	0.00
6.60	14.83	2.00	0.00	1.00	0.00	6.62	14.42	2.00	0.00	1.00	0.00
6.64	14.37	2.00	0.00	1.00	0.00	6.66	14.04	2.00	0.00	1.00	0.00
6.68	13.99	2.00	0.00	1.00	0.00	6.70	13.43	2.00	0.00	1.00	0.00
6.72	13.07	2.00	0.00	1.00	0.00	6.74	12.97	2.00	0.00	1.00	0.00
6.76	12.95	2.00	0.00	1.00	0.00	6.78	13.03	2.00	0.00	1.00	0.00
6.80	13.12	2.00	0.00	1.00	0.00	6.82	13.38	2.00	0.00	1.00	0.00
6.84	13.21	2.00	0.00	1.00	0.00	6.86	13.08	2.00	0.00	1.00	0.00
6.88	12.17	2.00	0.00	1.00	0.00	6.90	11.65	2.00	0.00	1.00	0.00
6.92	10.90	2.00	0.00	1.00	0.00	6.94	10.27	2.00	0.00	1.00	0.00
6.96	10.03	2.00	0.00	1.00	0.00	6.98	10.14	2.00	0.00	1.00	0.00
7.00	10.84	2.00	0.00	1.00	0.00	7.02	11.94	2.00	0.00	1.00	0.00
7.04	13.17	2.00	0.00	1.00	0.00	7.06	13.93	2.00	0.00	1.00	0.00
7.08	14.24	2.00	0.00	1.00	0.00	7.10	14.17	2.00	0.00	1.00	0.00
7.12	14.23	2.00	0.00	1.00	0.00	7.14	14.11	2.00	0.00	1.00	0.00
7.16	13.97	2.00	0.00	1.00	0.00	7.18	14.38	2.00	0.00	1.00	0.00
7.20	14.34	2.00	0.00	1.00	0.00	7.22	14.05	2.00	0.00	1.00	0.00
7.25	13.37	2.00	0.00	1.00	0.00	7.26	13.44	2.00	0.00	1.00	0.00
7.28	13.30	2.00	0.00	1.00	0.00	7.30	12.91	2.00	0.00	1.00	0.00
7.32	12.89	2.00	0.00	1.00	0.00	7.34	13.77	2.00	0.00	1.00	0.00
7.36	14.67	2.00	0.00	1.00	0.00	7.38	15.89	2.00	0.00	1.00	0.00
7.40	16.69	2.00	0.00	1.00	0.00	7.42	16.42	2.00	0.00	1.00	0.00
7.44	15.96	2.00	0.00	1.00	0.00	7.46	15.10	2.00	0.00	1.00	0.00
7.48	14.57	2.00	0.00	1.00	0.00	7.50	14.03	2.00	0.00	1.00	0.00
7.52	13.77	2.00	0.00	1.00	0.00	7.54	13.77	2.00	0.00	1.00	0.00
7.56	13.58	2.00	0.00	1.00	0.00	7.58	13.81	2.00	0.00	1.00	0.00
7.60	14.09	2.00	0.00	1.00	0.00	7.62	14.43	2.00	0.00	1.00	0.00
7.64	14.97	2.00	0.00	1.00	0.00	7.66	15.02	2.00	0.00	1.00	0.00
7.68	15.03	2.00	0.00	1.00	0.00	7.70	14.94	2.00	0.00	1.00	0.00
7.72	14.63	2.00	0.00	1.00	0.00	7.74	14.24	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.76	13.98	2.00	0.00	1.00	0.00	7.78	13.82	2.00	0.00	1.00	0.00
7.80	13.46	2.00	0.00	1.00	0.00	7.82	13.35	2.00	0.00	1.00	0.00
7.84	13.74	2.00	0.00	1.00	0.00	7.86	13.80	2.00	0.00	1.00	0.00
7.88	13.86	2.00	0.00	1.00	0.00	7.90	13.63	2.00	0.00	1.00	0.00
7.92	13.39	2.00	0.00	1.00	0.00	7.94	12.85	2.00	0.00	1.00	0.00
7.96	12.11	2.00	0.00	1.00	0.00	7.98	11.25	2.00	0.00	1.00	0.00
8.00	10.17	2.00	0.00	1.00	0.00	8.02	9.19	2.00	0.00	1.00	0.00
8.04	8.21	2.00	0.00	1.00	0.00	8.06	7.31	2.00	0.00	1.00	0.00
8.08	6.77	2.00	0.00	1.00	0.00	8.10	6.23	2.00	0.00	1.00	0.00
8.12	6.15	2.00	0.00	1.00	0.00	8.14	5.75	2.00	0.00	1.00	0.00
8.16	5.19	2.00	0.00	1.00	0.00	8.18	5.11	2.00	0.00	1.00	0.00
8.20	5.61	2.00	0.00	1.00	0.00	8.22	5.85	2.00	0.00	1.00	0.00
8.24	5.91	2.00	0.00	1.00	0.00	8.26	5.77	2.00	0.00	1.00	0.00
8.28	5.57	2.00	0.00	1.00	0.00	8.30	5.40	2.00	0.00	1.00	0.00
8.32	5.16	2.00	0.00	1.00	0.00	8.34	5.24	2.00	0.00	1.00	0.00
8.36	5.57	2.00	0.00	1.00	0.00	8.39	5.78	2.00	0.00	1.00	0.00
8.40	6.07	2.00	0.00	1.00	0.00	8.42	6.67	2.00	0.00	1.00	0.00
8.44	6.98	2.00	0.00	1.00	0.00	8.46	6.98	2.00	0.00	1.00	0.00
8.48	6.48	2.00	0.00	1.00	0.00	8.50	6.34	2.00	0.00	1.00	0.00
8.52	6.44	2.00	0.00	1.00	0.00	8.54	6.58	2.00	0.00	1.00	0.00
8.56	6.51	2.00	0.00	1.00	0.00	8.58	6.51	2.00	0.00	1.00	0.00
8.60	6.25	2.00	0.00	1.00	0.00	8.63	5.78	2.00	0.00	1.00	0.00
8.64	6.01	2.00	0.00	1.00	0.00	8.66	6.11	2.00	0.00	1.00	0.00
8.68	6.65	2.00	0.00	1.00	0.00	8.70	7.17	2.00	0.00	1.00	0.00
8.72	7.55	2.00	0.00	1.00	0.00	8.74	7.61	2.00	0.00	1.00	0.00
8.76	7.71	2.00	0.00	1.00	0.00	8.78	7.52	2.00	0.00	1.00	0.00
8.80	7.80	2.00	0.00	1.00	0.00	8.82	8.24	2.00	0.00	1.00	0.00
8.84	8.40	2.00	0.00	1.00	0.00	8.86	8.61	2.00	0.00	1.00	0.00
8.88	8.46	2.00	0.00	1.00	0.00	8.90	8.27	2.00	0.00	1.00	0.00
8.92	7.91	2.00	0.00	1.00	0.00	8.95	7.67	2.00	0.00	1.00	0.00
8.96	7.78	2.00	0.00	1.00	0.00	8.98	8.33	2.00	0.00	1.00	0.00
9.00	8.83	2.00	0.00	1.00	0.00	9.02	8.13	2.00	0.00	1.00	0.00
9.04	7.47	2.00	0.00	1.00	0.00	9.06	7.12	2.00	0.00	1.00	0.00
9.08	7.06	2.00	0.00	1.00	0.00	9.10	7.01	2.00	0.00	1.00	0.00
9.12	7.16	2.00	0.00	1.00	0.00	9.14	6.60	2.00	0.00	1.00	0.00
9.16	6.27	2.00	0.00	1.00	0.00	9.18	5.85	2.00	0.00	1.00	0.00
9.20	5.45	2.00	0.00	1.00	0.00	9.23	5.58	2.00	0.00	1.00	0.00
9.24	5.95	2.00	0.00	1.00	0.00	9.26	6.54	2.00	0.00	1.00	0.00
9.28	6.79	2.00	0.00	1.00	0.00	9.30	6.74	2.00	0.00	1.00	0.00
9.32	6.21	2.00	0.00	1.00	0.00	9.34	5.86	2.00	0.00	1.00	0.00
9.36	6.31	2.00	0.00	1.00	0.00	9.38	7.02	2.00	0.00	1.00	0.00
9.40	6.76	2.00	0.00	1.00	0.00	9.42	7.01	2.00	0.00	1.00	0.00
9.44	8.08	2.00	0.00	1.00	0.00	9.46	10.04	2.00	0.00	1.00	0.00
9.48	12.45	2.00	0.00	1.00	0.00	9.50	13.70	2.00	0.00	1.00	0.00
9.52	12.71	2.00	0.00	1.00	0.00	9.54	9.74	2.00	0.00	1.00	0.00
9.56	7.16	2.00	0.00	1.00	0.00	9.58	6.79	2.00	0.00	1.00	0.00
9.60	6.74	2.00	0.00	1.00	0.00	9.62	6.69	2.00	0.00	1.00	0.00
9.64	6.89	2.00	0.00	1.00	0.00	9.66	6.89	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.68	6.79	2.00	0.00	1.00	0.00	9.70	7.28	2.00	0.00	1.00	0.00
9.72	7.85	2.00	0.00	1.00	0.00	9.74	8.13	2.00	0.00	1.00	0.00
9.76	7.79	2.00	0.00	1.00	0.00	9.78	6.84	2.00	0.00	1.00	0.00
9.80	7.46	2.00	0.00	1.00	0.00	9.82	12.39	2.00	0.00	1.00	0.00
9.84	12.22	2.00	0.00	1.00	0.00	9.86	11.78	2.00	0.00	1.00	0.00
9.88	10.38	2.00	0.00	1.00	0.00	9.90	8.68	2.00	0.00	1.00	0.00
9.92	7.35	2.00	0.00	1.00	0.00	9.95	6.71	2.00	0.00	1.00	0.00
9.96	6.26	2.00	0.00	1.00	0.00	9.98	6.21	2.00	0.00	1.00	0.00
10.00	5.93	2.00	0.00	1.00	0.00	10.02	5.88	2.00	0.00	1.00	0.00
10.04	5.98	2.00	0.00	1.00	0.00	10.06	6.22	2.00	0.00	1.00	0.00
10.08	6.64	2.00	0.00	1.00	0.00	10.10	6.50	2.00	0.00	1.00	0.00
10.12	6.52	2.00	0.00	1.00	0.00	10.14	6.40	2.00	0.00	1.00	0.00
10.16	6.37	2.00	0.00	1.00	0.00	10.18	6.30	2.00	0.00	1.00	0.00
10.20	6.34	2.00	0.00	1.00	0.00	10.22	6.38	2.00	0.00	1.00	0.00
10.24	6.28	2.00	0.00	1.00	0.00	10.26	5.95	2.00	0.00	1.00	0.00
10.28	5.94	2.00	0.00	1.00	0.00	10.30	5.96	2.00	0.00	1.00	0.00
10.32	5.91	2.00	0.00	1.00	0.00	10.34	5.89	2.00	0.00	1.00	0.00
10.36	6.04	2.00	0.00	1.00	0.00	10.38	6.06	2.00	0.00	1.00	0.00
10.40	6.27	2.00	0.00	1.00	0.00	10.42	6.27	2.00	0.00	1.00	0.00
10.44	6.35	2.00	0.00	1.00	0.00	10.46	6.42	2.00	0.00	1.00	0.00
10.48	6.48	2.00	0.00	1.00	0.00	10.50	6.23	2.00	0.00	1.00	0.00
10.52	6.27	2.00	0.00	1.00	0.00	10.54	6.03	2.00	0.00	1.00	0.00
10.56	5.78	2.00	0.00	1.00	0.00	10.58	6.13	2.00	0.00	1.00	0.00
10.60	6.74	2.00	0.00	1.00	0.00	10.62	7.00	2.00	0.00	1.00	0.00
10.64	6.84	2.00	0.00	1.00	0.00	10.66	6.60	2.00	0.00	1.00	0.00
10.68	6.48	2.00	0.00	1.00	0.00	10.70	6.92	2.00	0.00	1.00	0.00
10.72	7.61	2.00	0.00	1.00	0.00	10.74	8.09	2.00	0.00	1.00	0.00
10.76	8.39	2.00	0.00	1.00	0.00	10.78	8.16	2.00	0.00	1.00	0.00
10.80	7.90	2.00	0.00	1.00	0.00	10.82	8.07	2.00	0.00	1.00	0.00
10.84	7.56	2.00	0.00	1.00	0.00	10.86	7.60	2.00	0.00	1.00	0.00
10.88	8.01	2.00	0.00	1.00	0.00	10.90	7.96	2.00	0.00	1.00	0.00
10.92	7.60	2.00	0.00	1.00	0.00	10.94	6.75	2.00	0.00	1.00	0.00
10.96	6.81	2.00	0.00	1.00	0.00	10.98	7.10	2.00	0.00	1.00	0.00
11.00	7.44	2.00	0.00	1.00	0.00	11.02	7.59	2.00	0.00	1.00	0.00
11.04	7.19	2.00	0.00	1.00	0.00	11.06	7.01	2.00	0.00	1.00	0.00
11.08	7.03	2.00	0.00	1.00	0.00	11.10	7.56	2.00	0.00	1.00	0.00
11.12	8.14	2.00	0.00	1.00	0.00	11.14	8.24	2.00	0.00	1.00	0.00
11.16	7.84	2.00	0.00	1.00	0.00	11.18	7.77	2.00	0.00	1.00	0.00
11.20	7.81	2.00	0.00	1.00	0.00	11.22	7.91	2.00	0.00	1.00	0.00
11.24	7.99	2.00	0.00	1.00	0.00	11.26	7.68	2.00	0.00	1.00	0.00
11.28	7.06	2.00	0.00	1.00	0.00	11.30	6.69	2.00	0.00	1.00	0.00
11.32	6.64	2.00	0.00	1.00	0.00	11.34	6.80	2.00	0.00	1.00	0.00
11.36	7.22	2.00	0.00	1.00	0.00	11.38	7.60	2.00	0.00	1.00	0.00
11.40	7.70	2.00	0.00	1.00	0.00	11.42	7.76	2.00	0.00	1.00	0.00
11.44	7.88	2.00	0.00	1.00	0.00	11.46	7.60	2.00	0.00	1.00	0.00
11.48	7.47	2.00	0.00	1.00	0.00	11.50	7.44	2.00	0.00	1.00	0.00
11.52	7.73	2.00	0.00	1.00	0.00	11.54	8.00	2.00	0.00	1.00	0.00
11.56	8.36	2.00	0.00	1.00	0.00	11.58	8.35	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.60	8.37	2.00	0.00	1.00	0.00	11.62	8.51	2.00	0.00	1.00	0.00
11.64	8.48	2.00	0.00	1.00	0.00	11.66	8.51	2.00	0.00	1.00	0.00
11.68	8.63	2.00	0.00	1.00	0.00	11.70	8.88	2.00	0.00	1.00	0.00
11.72	9.53	2.00	0.00	1.00	0.00	11.74	9.69	2.00	0.00	1.00	0.00
11.76	9.93	2.00	0.00	1.00	0.00	11.78	9.88	2.00	0.00	1.00	0.00
11.80	9.76	2.00	0.00	1.00	0.00	11.82	9.27	2.00	0.00	1.00	0.00
11.84	9.07	2.00	0.00	1.00	0.00	11.86	9.21	2.00	0.00	1.00	0.00
11.88	9.39	2.00	0.00	1.00	0.00	11.90	9.03	2.00	0.00	1.00	0.00
11.92	8.89	2.00	0.00	1.00	0.00	11.94	8.69	2.00	0.00	1.00	0.00
11.96	8.85	2.00	0.00	1.00	0.00	11.98	8.80	2.00	0.00	1.00	0.00
12.00	8.90	2.00	0.00	1.00	0.00	12.02	9.18	2.00	0.00	1.00	0.00
12.04	9.34	2.00	0.00	1.00	0.00	12.06	9.56	2.00	0.00	1.00	0.00
12.08	9.74	2.00	0.00	1.00	0.00	12.10	9.87	2.00	0.00	1.00	0.00
12.12	9.99	2.00	0.00	1.00	0.00	12.14	10.10	2.00	0.00	1.00	0.00
12.16	10.07	2.00	0.00	1.00	0.00	12.18	9.95	2.00	0.00	1.00	0.00
12.20	9.88	2.00	0.00	1.00	0.00	12.22	9.93	2.00	0.00	1.00	0.00
12.24	9.82	2.00	0.00	1.00	0.00	12.26	9.73	2.00	0.00	1.00	0.00
12.28	9.67	2.00	0.00	1.00	0.00	12.30	9.73	2.00	0.00	1.00	0.00
12.32	9.57	2.00	0.00	1.00	0.00	12.34	9.46	2.00	0.00	1.00	0.00
12.36	9.61	2.00	0.00	1.00	0.00	12.38	9.38	2.00	0.00	1.00	0.00
12.40	9.59	2.00	0.00	1.00	0.00	12.42	9.64	2.00	0.00	1.00	0.00
12.44	9.78	2.00	0.00	1.00	0.00	12.46	9.83	2.00	0.00	1.00	0.00
12.48	9.90	2.00	0.00	1.00	0.00	12.50	10.12	2.00	0.00	1.00	0.00
12.52	10.17	2.00	0.00	1.00	0.00	12.54	10.41	2.00	0.00	1.00	0.00
12.56	10.52	2.00	0.00	1.00	0.00	12.58	10.47	2.00	0.00	1.00	0.00
12.60	10.52	2.00	0.00	1.00	0.00	12.62	10.51	2.00	0.00	1.00	0.00
12.64	10.67	2.00	0.00	1.00	0.00	12.66	10.84	2.00	0.00	1.00	0.00
12.68	10.98	2.00	0.00	1.00	0.00	12.70	10.74	2.00	0.00	1.00	0.00
12.72	10.53	2.00	0.00	1.00	0.00	12.74	10.33	2.00	0.00	1.00	0.00
12.76	10.67	2.00	0.00	1.00	0.00	12.78	10.90	2.00	0.00	1.00	0.00
12.80	11.71	2.00	0.00	1.00	0.00	12.82	11.99	2.00	0.00	1.00	0.00
12.84	12.02	2.00	0.00	1.00	0.00	12.86	12.05	2.00	0.00	1.00	0.00
12.88	11.84	2.00	0.00	1.00	0.00	12.90	11.50	2.00	0.00	1.00	0.00
12.92	11.57	2.00	0.00	1.00	0.00	12.94	11.74	2.00	0.00	1.00	0.00
12.96	11.71	2.00	0.00	1.00	0.00	12.98	11.92	2.00	0.00	1.00	0.00
13.00	11.73	2.00	0.00	1.00	0.00	13.02	11.75	2.00	0.00	1.00	0.00
13.04	11.62	2.00	0.00	1.00	0.00	13.06	11.51	2.00	0.00	1.00	0.00
13.08	11.38	2.00	0.00	1.00	0.00	13.10	11.65	2.00	0.00	1.00	0.00
13.12	11.61	2.00	0.00	1.00	0.00	13.14	11.66	2.00	0.00	1.00	0.00
13.16	11.75	2.00	0.00	1.00	0.00	13.19	11.55	2.00	0.00	1.00	0.00
13.20	11.70	2.00	0.00	1.00	0.00	13.22	11.83	2.00	0.00	1.00	0.00
13.24	11.86	2.00	0.00	1.00	0.00	13.26	11.61	2.00	0.00	1.00	0.00
13.28	11.08	2.00	0.00	1.00	0.00	13.30	10.87	2.00	0.00	1.00	0.00
13.32	10.79	2.00	0.00	1.00	0.00	13.34	10.36	2.00	0.00	1.00	0.00
13.36	10.11	2.00	0.00	1.00	0.00	13.38	9.88	2.00	0.00	1.00	0.00
13.40	9.65	2.00	0.00	1.00	0.00	13.42	9.60	2.00	0.00	1.00	0.00
13.44	9.14	2.00	0.00	1.00	0.00	13.46	8.83	2.00	0.00	1.00	0.00
13.48	8.67	2.00	0.00	1.00	0.00	13.50	8.36	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.52	8.10	2.00	0.00	1.00	0.00	13.54	7.91	2.00	0.00	1.00	0.00
13.56	7.55	2.00	0.00	1.00	0.00	13.58	7.25	2.00	0.00	1.00	0.00
13.60	6.89	2.00	0.00	1.00	0.00	13.62	6.67	2.00	0.00	1.00	0.00
13.64	6.62	2.00	0.00	1.00	0.00	13.66	6.44	2.00	0.00	1.00	0.00
13.68	6.63	2.00	0.00	1.00	0.00	13.70	6.67	2.00	0.00	1.00	0.00
13.72	6.65	2.00	0.00	1.00	0.00	13.74	6.49	2.00	0.00	1.00	0.00
13.76	6.25	2.00	0.00	1.00	0.00	13.78	6.99	2.00	0.00	1.00	0.00
13.80	6.89	2.00	0.00	1.00	0.00	13.82	6.34	2.00	0.00	1.00	0.00
13.84	6.05	2.00	0.00	1.00	0.00	13.86	5.73	2.00	0.00	1.00	0.00
13.88	5.61	2.00	0.00	1.00	0.00	13.90	5.44	2.00	0.00	1.00	0.00
13.92	5.51	2.00	0.00	1.00	0.00	13.94	5.43	2.00	0.00	1.00	0.00
13.96	5.68	2.00	0.00	1.00	0.00	13.98	5.95	2.00	0.00	1.00	0.00
14.00	6.20	2.00	0.00	1.00	0.00	14.02	6.60	2.00	0.00	1.00	0.00
14.04	6.62	2.00	0.00	1.00	0.00	14.06	6.69	2.00	0.00	1.00	0.00
14.08	7.02	2.00	0.00	1.00	0.00	14.11	6.88	2.00	0.00	1.00	0.00
14.12	6.40	2.00	0.00	1.00	0.00	14.14	6.36	2.00	0.00	1.00	0.00
14.16	6.60	2.00	0.00	1.00	0.00	14.18	6.77	2.00	0.00	1.00	0.00
14.20	6.64	2.00	0.00	1.00	0.00	14.22	6.07	2.00	0.00	1.00	0.00
14.24	5.86	2.00	0.00	1.00	0.00	14.26	5.93	2.00	0.00	1.00	0.00
14.28	6.30	2.00	0.00	1.00	0.00	14.30	6.51	2.00	0.00	1.00	0.00
14.32	6.91	2.00	0.00	1.00	0.00	14.34	6.79	2.00	0.00	1.00	0.00
14.36	6.79	2.00	0.00	1.00	0.00	14.38	6.82	2.00	0.00	1.00	0.00
14.40	7.13	2.00	0.00	1.00	0.00	14.42	7.33	2.00	0.00	1.00	0.00
14.44	7.45	2.00	0.00	1.00	0.00	14.46	7.44	2.00	0.00	1.00	0.00
14.48	7.52	2.00	0.00	1.00	0.00	14.50	7.93	2.00	0.00	1.00	0.00
14.52	7.66	2.00	0.00	1.00	0.00	14.54	6.99	2.00	0.00	1.00	0.00
14.56	7.20	2.00	0.00	1.00	0.00	14.58	7.42	2.00	0.00	1.00	0.00
14.60	7.59	2.00	0.00	1.00	0.00	14.62	7.60	2.00	0.00	1.00	0.00
14.64	7.87	2.00	0.00	1.00	0.00	14.66	7.96	2.00	0.00	1.00	0.00
14.68	8.01	2.00	0.00	1.00	0.00	14.70	8.27	2.00	0.00	1.00	0.00
14.72	8.25	2.00	0.00	1.00	0.00	14.74	8.24	2.00	0.00	1.00	0.00
14.76	6.52	2.00	0.00	1.00	0.00	14.79	8.20	2.00	0.00	1.00	0.00
14.80	8.27	2.00	0.00	1.00	0.00	14.82	8.08	2.00	0.00	1.00	0.00
14.84	7.92	2.00	0.00	1.00	0.00	14.86	7.90	2.00	0.00	1.00	0.00
14.88	7.78	2.00	0.00	1.00	0.00	14.90	7.77	2.00	0.00	1.00	0.00
14.92	7.60	2.00	0.00	1.00	0.00	14.94	7.23	2.00	0.00	1.00	0.00
14.96	6.94	2.00	0.00	1.00	0.00	14.99	6.71	2.00	0.00	1.00	0.00
15.00	6.31	2.00	0.00	1.00	0.00	15.02	6.36	2.00	0.00	1.00	0.00
15.04	6.52	2.00	0.00	1.00	0.00	15.06	6.46	2.00	0.00	1.00	0.00
15.08	6.49	2.00	0.00	1.00	0.00	15.10	6.37	2.00	0.00	1.00	0.00
15.12	6.26	2.00	0.00	1.00	0.00	15.14	6.18	2.00	0.00	1.00	0.00
15.16	6.55	2.00	0.00	1.00	0.00	15.18	7.24	2.00	0.00	1.00	0.00
15.20	7.76	2.00	0.00	1.00	0.00	15.22	8.18	2.00	0.00	1.00	0.00
15.24	8.40	2.00	0.00	1.00	0.00	15.26	8.42	2.00	0.00	1.00	0.00
15.28	8.26	2.00	0.00	1.00	0.00	15.30	8.26	2.00	0.00	1.00	0.00
15.32	8.51	2.00	0.00	1.00	0.00	15.34	8.75	2.00	0.00	1.00	0.00
15.36	8.62	2.00	0.00	1.00	0.00	15.38	8.37	2.00	0.00	1.00	0.00
15.40	7.80	2.00	0.00	1.00	0.00	15.42	8.21	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.44	8.97	2.00	0.00	1.00	0.00	15.46	9.56	2.00	0.00	1.00	0.00
15.48	9.96	2.00	0.00	1.00	0.00	15.50	10.80	2.00	0.00	1.00	0.00
15.52	12.22	2.00	0.00	1.00	0.00	15.54	13.38	2.00	0.00	1.00	0.00
15.56	15.24	2.00	0.00	1.00	0.00	15.58	14.91	2.00	0.00	1.00	0.00
15.60	12.39	2.00	0.00	1.00	0.00	15.62	9.84	2.00	0.00	1.00	0.00
15.64	8.55	2.00	0.00	1.00	0.00	15.66	7.52	2.00	0.00	1.00	0.00
15.68	6.57	2.00	0.00	1.00	0.00	15.70	6.01	2.00	0.00	1.00	0.00
15.72	5.73	2.00	0.00	1.00	0.00	15.74	5.93	2.00	0.00	1.00	0.00

Total estimated settlement: 0.22

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.26	4.35	10.16	44.18	3.26	0.05	62.56
0.04	0.32	5.47	8.83	48.28	3.17	0.06	38.91
0.06	0.37	6.29	8.56	53.83	3.15	0.06	29.48
0.08	0.42	7.05	8.85	62.38	3.17	0.06	24.43
0.10	0.42	7.10	9.86	70.05	3.24	0.06	19.44
0.12	0.40	6.76	11.60	78.46	3.36	0.06	15.24
0.15	0.38	6.46	12.83	82.91	3.43	0.06	11.48
0.16	0.36	6.02	14.19	85.46	3.51	0.06	10.00
0.18	0.33	5.50	15.33	84.27	3.57	0.06	8.06
0.20	0.29	4.80	17.02	81.63	3.65	0.06	6.30
0.22	0.26	4.37	17.87	78.04	3.69	0.05	5.19
0.24	0.25	4.18	17.83	74.53	3.69	0.05	4.55
0.26	0.26	4.38	16.45	72.08	3.62	0.05	4.39
0.28	0.28	4.62	15.19	70.16	3.56	0.06	4.30
0.30	0.33	5.55	12.80	71.04	3.43	0.06	4.82
0.32	0.39	6.63	10.98	72.78	3.32	0.06	5.39
0.34	0.47	7.86	9.50	74.70	3.22	0.06	6.02
0.36	0.51	8.64	8.89	76.80	3.17	0.06	6.24
0.38	0.55	9.27	8.56	79.37	3.15	0.06	6.34
0.41	0.59	9.95	8.30	82.57	3.13	0.06	6.29
0.42	0.64	10.69	8.05	86.02	3.11	0.06	6.59
0.44	0.69	11.54	7.79	89.86	3.09	0.06	6.78
0.46	0.72	12.04	7.88	94.88	3.10	0.06	6.75
0.48	0.73	12.24	8.21	100.46	3.12	0.06	6.56
0.50	0.73	12.25	8.64	105.88	3.16	0.06	6.28
0.52	0.74	12.41	8.87	110.10	3.17	0.06	6.11
0.54	0.75	12.61	9.02	113.77	3.18	0.06	5.96
0.56	0.76	12.71	9.19	116.78	3.20	0.06	5.78
0.58	0.76	12.75	9.38	119.61	3.21	0.06	5.58
0.60	0.76	12.72	9.53	121.14	3.22	0.06	5.37
0.62	0.75	12.60	9.66	121.79	3.23	0.06	5.14
0.64	0.76	12.70	9.59	121.83	3.22	0.06	5.00
0.66	0.78	13.13	9.32	122.41	3.21	0.07	5.01
0.68	0.82	13.82	8.94	123.52	3.18	0.07	5.10
0.70	0.88	14.68	8.44	123.88	3.14	0.07	5.26
0.72	0.92	15.49	7.96	123.33	3.10	0.07	5.38
0.74	0.96	16.11	7.62	122.72	3.07	0.07	5.44
0.76	0.98	16.43	7.52	123.51	3.07	0.07	5.39
0.78	0.99	16.65	7.52	125.14	3.07	0.07	5.31
0.80	1.01	16.90	7.51	126.84	3.07	0.07	5.25
0.82	1.03	17.23	7.51	129.41	3.07	0.07	5.21
0.84	1.04	17.49	7.59	132.77	3.07	0.07	5.16
0.86	1.06	17.75	7.65	135.90	3.08	0.07	5.11
0.88	1.06	17.75	7.73	137.16	3.08	0.07	4.98
0.90	1.06	17.80	7.72	137.39	3.08	0.07	4.88
0.92	1.07	17.85	7.68	137.03	3.08	0.07	4.78
0.94	1.08	18.16	7.57	137.51	3.07	0.07	4.75
0.96	1.11	18.51	7.43	137.55	3.06	0.07	4.74

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.99	1.12	18.78	7.35	138.05	3.05	0.07	4.65
1.00	1.13	18.89	7.36	138.91	3.05	0.07	4.63
1.02	1.13	18.85	7.45	140.41	3.06	0.07	4.52
1.05	1.14	19.10	7.45	142.27	3.06	0.07	4.44
1.07	1.15	19.24	7.45	143.46	3.06	0.07	4.39
1.08	1.15	19.25	7.50	144.41	3.07	0.07	4.35
1.10	1.13	18.85	7.72	145.50	3.08	0.07	4.17
1.12	1.10	18.44	7.96	146.83	3.10	0.07	4.01
1.14	1.07	17.84	8.30	148.10	3.13	0.07	3.80
1.16	1.02	17.06	8.72	148.72	3.16	0.07	3.57
1.18	0.97	16.15	9.19	148.48	3.20	0.07	3.32
1.20	0.93	15.39	9.57	147.26	3.22	0.07	3.11
1.22	0.89	14.81	9.79	144.94	3.24	0.07	2.94
1.24	0.86	14.27	9.94	141.82	3.25	0.07	2.78
1.26	0.83	13.78	10.09	138.92	3.26	0.07	2.64
1.28	0.81	13.37	10.20	136.37	3.27	0.07	2.52
1.30	0.80	13.23	10.09	133.48	3.26	0.07	2.46
1.32	0.81	13.34	9.75	129.97	3.23	0.07	2.44
1.34	0.82	13.54	9.31	126.11	3.20	0.07	2.44
1.36	0.84	13.86	8.91	123.40	3.18	0.07	2.46
1.38	0.84	13.91	8.69	120.91	3.16	0.07	2.43
1.40	0.87	14.30	8.33	119.06	3.13	0.07	2.46
1.42	0.90	14.87	7.88	117.14	3.10	0.07	2.52
1.44	0.96	15.87	7.28	115.55	3.05	0.07	2.66
1.46	1.01	16.77	6.86	114.98	3.01	0.07	2.77
1.48	1.06	17.51	6.63	116.08	2.99	0.07	2.85
1.50	1.10	18.20	6.49	118.07	2.98	0.07	2.92
1.52	1.14	18.84	6.37	120.04	2.97	0.07	2.98
1.54	1.17	19.46	6.27	122.12	2.96	0.07	3.04
1.56	1.20	19.96	6.24	124.47	2.95	0.07	3.08
1.58	1.22	20.27	6.26	126.95	2.96	0.07	3.08
1.60	1.23	20.46	6.27	128.27	2.96	0.07	3.07
1.62	1.23	20.39	6.33	129.07	2.96	0.07	3.02
1.64	1.22	20.26	6.39	129.56	2.97	0.07	2.97
1.66	1.22	20.25	6.41	129.83	2.97	0.07	2.93
1.68	1.25	20.67	6.28	129.89	2.96	0.07	2.95
1.70	1.28	21.17	6.19	131.09	2.95	0.08	2.99
1.72	1.30	21.56	6.18	133.33	2.95	0.08	3.01
1.74	1.31	21.73	6.28	136.37	2.96	0.08	2.99
1.76	1.31	21.83	6.32	138.02	2.96	0.08	2.97
1.78	1.33	22.09	6.29	139.01	2.96	0.08	2.97
1.80	1.35	22.33	6.27	140.01	2.96	0.08	2.97
1.82	1.35	22.46	6.30	141.40	2.96	0.08	2.95
1.84	1.35	22.35	6.36	142.05	2.96	0.08	2.90
1.86	1.33	22.08	6.43	141.92	2.97	0.08	2.84
1.88	1.32	21.93	6.43	140.94	2.97	0.08	2.79
1.90	1.32	21.93	6.47	141.80	2.97	0.08	2.76
1.92	1.33	22.06	6.51	143.55	2.98	0.08	2.74

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	1.33	22.07	6.60	145.64	2.99	0.08	2.71
1.96	1.32	21.92	6.68	146.39	2.99	0.08	2.67
1.98	1.32	21.84	6.66	145.42	2.99	0.08	2.63
2.00	1.32	21.83	6.60	144.04	2.99	0.08	2.60
2.02	1.33	21.93	6.44	141.17	2.97	0.08	2.59
2.04	1.32	21.90	6.30	137.86	2.96	0.08	2.56
2.06	1.33	21.94	6.10	133.80	2.94	0.08	2.54
2.08	1.32	21.77	6.00	130.70	2.93	0.08	2.49
2.10	1.30	21.48	6.03	129.49	2.93	0.08	2.43
2.12	1.28	21.08	6.14	129.52	2.94	0.08	2.37
2.14	1.25	20.69	6.33	130.90	2.96	0.07	2.30
2.16	1.23	20.29	6.53	132.52	2.98	0.07	2.23
2.18	1.21	19.87	6.74	134.01	3.00	0.07	2.17
2.20	1.18	19.48	6.89	134.19	3.01	0.07	2.10
2.22	1.17	19.26	6.89	132.80	3.01	0.07	2.06
2.24	1.17	19.16	6.82	130.63	3.01	0.07	2.03
2.26	1.17	19.20	6.68	128.35	2.99	0.07	2.02
2.28	1.18	19.35	6.49	125.56	2.98	0.07	2.02
2.30	1.19	19.47	6.36	123.80	2.96	0.07	2.01
2.32	1.19	19.50	6.34	123.69	2.96	0.07	2.00
2.35	1.19	19.46	6.47	125.87	2.97	0.07	1.97
2.36	1.18	19.41	6.64	128.79	2.99	0.07	1.95
2.38	1.19	19.47	6.73	131.10	3.00	0.07	1.94
2.40	1.20	19.67	6.77	133.10	3.00	0.07	1.94
2.42	1.22	20.01	6.71	134.22	3.00	0.07	1.96
2.44	1.24	20.26	6.67	135.20	2.99	0.07	1.97
2.46	1.25	20.45	6.62	135.34	2.99	0.07	1.97
2.48	1.27	20.83	6.52	135.84	2.98	0.07	1.99
2.50	1.30	21.35	6.40	136.67	2.97	0.07	2.02
2.52	1.34	21.98	6.28	138.09	2.96	0.07	2.08
2.54	1.37	22.51	6.21	139.73	2.95	0.08	2.12
2.56	1.40	23.06	6.12	141.07	2.94	0.08	2.16
2.58	1.43	23.57	6.06	142.86	2.94	0.08	2.20
2.60	1.45	23.87	6.05	144.28	2.93	0.08	2.22
2.62	1.45	23.89	6.10	145.78	2.94	0.08	2.21
2.64	1.44	23.68	6.19	146.69	2.95	0.08	2.19
2.66	1.43	23.51	6.26	147.17	2.96	0.08	2.16
2.68	1.39	22.89	6.44	147.46	2.97	0.08	2.10
2.70	1.34	22.04	6.67	147.09	2.99	0.07	2.01
2.72	1.27	20.83	6.99	145.60	3.02	0.07	1.89
2.74	1.22	19.87	7.21	143.18	3.04	0.07	1.80
2.76	1.14	18.61	7.54	140.30	3.07	0.07	1.68
2.78	1.06	17.18	8.04	138.08	3.11	0.07	1.55
2.80	0.97	15.67	8.66	135.76	3.16	0.07	1.40
2.82	0.90	14.45	9.24	133.56	3.20	0.07	1.29
2.84	0.81	12.92	10.12	130.74	3.26	0.06	1.15
2.86	0.72	11.43	11.12	127.09	3.33	0.06	1.01
2.88	0.66	10.27	11.75	120.61	3.37	0.06	0.91

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.63	9.78	11.58	113.20	3.35	0.06	0.86
2.92	0.62	9.61	10.99	105.58	3.32	0.06	0.84
2.95	0.61	9.46	10.41	98.55	3.28	0.06	0.83
2.96	0.60	9.35	9.94	92.86	3.25	0.06	0.82
2.98	0.59	9.09	9.59	87.12	3.22	0.06	0.79
3.00	0.57	8.81	9.47	83.46	3.22	0.06	0.77
3.02	0.56	8.63	9.27	79.99	3.20	0.06	0.75
3.04	0.57	8.71	8.86	77.23	3.17	0.06	0.75
3.06	0.58	8.85	8.47	74.96	3.14	0.06	0.76
3.08	0.59	9.16	7.96	72.85	3.10	0.06	0.79
3.10	0.62	9.58	7.36	70.51	3.05	0.06	0.82
3.12	0.66	10.29	6.66	68.55	2.99	0.06	0.88
3.14	0.72	11.33	5.93	67.26	2.92	0.06	0.97
3.16	0.79	12.48	5.37	67.09	2.87	0.07	1.06
3.18	0.86	13.63	5.03	68.59	2.83	0.07	1.16
3.20	0.93	14.88	4.76	70.78	2.80	0.07	1.26
3.22	1.02	16.45	4.48	73.67	2.76	0.07	1.39
3.24	1.13	18.25	4.17	76.19	2.72	0.08	1.53
3.26	1.24	20.02	3.92	78.54	2.69	0.08	1.68
3.28	1.33	21.66	3.75	81.28	2.67	0.08	1.81
3.30	1.40	22.86	3.74	85.44	2.66	0.08	1.90
3.32	1.44	23.51	3.93	92.35	2.69	0.08	1.95
3.34	1.44	23.54	4.25	100.02	2.73	0.08	1.95
3.36	1.42	23.17	4.66	108.08	2.79	0.08	1.91
3.38	1.39	22.70	5.03	114.19	2.83	0.08	1.87
3.40	1.39	22.56	5.25	118.34	2.85	0.08	1.85
3.42	1.40	22.70	5.34	121.14	2.86	0.08	1.86
3.44	1.40	22.81	5.42	123.59	2.87	0.08	1.86
3.46	1.39	22.62	5.58	126.25	2.89	0.08	1.84
3.48	1.39	22.51	5.68	127.80	2.90	0.08	1.82
3.50	1.39	22.62	5.67	128.37	2.90	0.08	1.83
3.52	1.41	22.95	5.65	129.55	2.89	0.08	1.85
3.54	1.43	23.22	5.66	131.55	2.90	0.08	1.86
3.56	1.43	23.29	5.77	134.44	2.91	0.08	1.86
3.58	1.43	23.24	5.89	136.85	2.92	0.08	1.85
3.60	1.41	22.96	6.05	139.03	2.94	0.07	1.82
3.62	1.42	22.98	6.07	139.45	2.94	0.07	1.82
3.64	1.42	23.11	6.01	138.84	2.93	0.08	1.82
3.66	1.42	23.05	5.95	137.06	2.92	0.08	1.81
3.68	1.38	22.39	6.06	135.69	2.94	0.07	1.76
3.70	1.33	21.45	6.23	133.61	2.95	0.07	1.68
3.72	1.26	20.36	6.45	131.22	2.97	0.07	1.59
3.74	1.20	19.29	6.66	128.41	2.99	0.07	1.50
3.76	1.14	18.24	6.90	125.82	3.01	0.07	1.41
3.78	1.09	17.43	7.02	122.40	3.02	0.07	1.35
3.80	1.06	16.88	7.03	118.63	3.03	0.07	1.30
3.82	1.04	16.53	6.92	114.29	3.02	0.07	1.27
3.84	1.04	16.60	6.66	110.50	2.99	0.07	1.27

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	1.11	17.68	5.83	103.02	2.91	0.07	1.35
3.88	1.17	18.71	5.20	97.22	2.85	0.08	1.43
3.90	1.21	19.36	4.85	93.97	2.81	0.08	1.47
3.92	1.18	18.93	5.11	96.78	2.84	0.07	1.43
3.94	1.16	18.53	5.37	99.48	2.87	0.07	1.40
3.96	1.14	18.10	5.59	101.24	2.89	0.07	1.36
3.98	1.12	17.77	5.78	102.65	2.91	0.07	1.34
4.01	1.09	17.34	5.96	103.28	2.93	0.07	1.30
4.02	1.07	16.97	6.05	102.67	2.93	0.07	1.27
4.04	1.04	16.41	6.16	101.03	2.95	0.07	1.22
4.06	1.00	15.74	6.25	98.37	2.95	0.07	1.17
4.08	0.97	15.29	6.25	95.56	2.95	0.06	1.13
4.10	0.96	15.01	6.23	93.47	2.95	0.07	1.11
4.12	0.95	14.96	6.16	92.09	2.95	0.07	1.10
4.15	0.93	14.64	6.22	90.98	2.95	0.06	1.08
4.16	0.92	14.33	6.28	90.00	2.96	0.06	1.05
4.18	0.89	13.82	6.44	89.01	2.97	0.06	1.01
4.20	0.85	13.26	6.60	87.51	2.99	0.06	0.97
4.22	0.82	12.61	6.81	85.87	3.01	0.06	0.92
4.24	0.78	11.99	6.99	83.78	3.02	0.06	0.87
4.26	0.75	11.52	7.15	82.36	3.04	0.06	0.84
4.28	0.75	11.42	7.02	80.23	3.02	0.06	0.83
4.30	0.78	11.99	6.54	78.43	2.98	0.06	0.87
4.32	0.85	13.14	5.80	76.15	2.91	0.07	0.95
4.34	0.89	13.65	5.46	74.51	2.88	0.07	0.99
4.36	0.88	13.53	5.44	73.56	2.87	0.07	0.98
4.38	0.84	12.88	5.68	73.15	2.90	0.07	0.93
4.40	0.82	12.50	5.74	71.74	2.90	0.07	0.90
4.42	0.81	12.36	5.66	69.94	2.90	0.07	0.89
4.44	0.86	12.97	5.29	68.55	2.86	0.07	0.94
4.46	0.98	14.65	4.61	67.49	2.78	0.07	1.08
4.48	1.14	17.01	3.91	66.44	2.69	0.08	1.28
4.50	1.24	18.47	3.66	67.62	2.65	0.08	1.40
4.52	1.24	18.47	3.86	71.24	2.68	0.08	1.39
4.54	1.13	17.03	4.52	77.02	2.77	0.08	1.26
4.56	1.08	16.26	4.97	80.80	2.82	0.07	1.19
4.58	1.10	16.61	4.96	82.33	2.82	0.07	1.21
4.60	1.20	18.00	4.57	82.17	2.77	0.08	1.33
4.62	1.24	18.55	4.50	83.49	2.77	0.08	1.37
4.64	1.20	17.94	4.71	84.52	2.79	0.08	1.32
4.66	1.09	16.38	5.22	85.47	2.85	0.07	1.19
4.68	1.00	14.96	5.58	83.54	2.89	0.07	1.08
4.70	0.95	14.10	5.80	81.78	2.91	0.07	1.01
4.72	0.94	13.96	5.71	79.71	2.90	0.07	1.00
4.74	0.97	14.27	5.46	77.88	2.88	0.07	1.03
4.76	0.99	14.49	5.25	76.09	2.85	0.07	1.05
4.78	1.02	14.82	4.97	73.66	2.82	0.07	1.08
4.80	1.04	15.12	4.76	71.92	2.80	0.07	1.11

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	1.05	15.24	4.66	70.96	2.78	0.07	1.12
4.84	0.98	14.23	5.14	73.16	2.84	0.07	1.03
4.86	1.02	14.86	5.19	77.09	2.85	0.07	1.08
4.88	1.06	15.38	5.32	81.80	2.86	0.07	1.11
4.90	1.13	16.43	5.21	85.52	2.85	0.07	1.19
4.92	1.07	15.66	5.68	88.95	2.90	0.07	1.13
4.94	1.05	15.39	5.87	90.37	2.92	0.07	1.10
4.96	1.09	15.87	5.64	89.49	2.89	0.07	1.14
4.98	1.21	17.43	4.98	86.86	2.82	0.07	1.27
5.00	1.44	20.51	4.02	82.50	2.70	0.08	1.53
5.02	1.83	25.70	3.01	77.39	2.55	0.08	0.65
5.04	2.23	30.99	2.48	76.77	2.44	0.09	0.67
5.06	2.36	32.90	2.52	82.89	2.45	0.09	0.68
5.08	2.13	30.12	3.16	95.30	2.57	0.09	0.67
5.10	1.73	24.85	4.21	104.70	2.73	0.08	1.84
5.12	1.43	20.63	5.30	109.39	2.86	0.08	1.49
5.14	1.30	18.68	5.73	106.92	2.90	0.07	1.34
5.16	1.24	17.90	5.92	105.88	2.92	0.07	1.28
5.18	1.24	17.82	5.88	104.69	2.92	0.07	1.28
5.20	1.26	18.03	5.76	103.95	2.91	0.07	1.29
5.22	1.31	18.62	5.42	100.95	2.87	0.07	1.34
5.24	1.37	19.40	5.04	97.70	2.83	0.08	1.41
5.26	1.42	19.98	4.74	94.66	2.79	0.08	1.46
5.28	1.42	19.87	4.79	95.18	2.80	0.08	1.45
5.30	1.37	19.18	5.09	97.62	2.83	0.08	1.39
5.32	1.28	18.00	5.68	102.31	2.90	0.07	1.29
5.34	1.18	16.48	6.49	106.89	2.98	0.07	1.18
5.36	1.09	15.08	7.31	110.21	3.05	0.06	1.08
5.38	1.00	13.76	8.17	112.36	3.12	0.06	0.98
5.40	0.94	12.78	8.74	111.75	3.16	0.06	0.91
5.42	0.89	12.03	9.08	109.20	3.19	0.06	0.86
5.44	0.88	11.78	8.92	105.05	3.18	0.06	0.84
5.46	0.89	11.92	8.38	99.85	3.14	0.06	0.85
5.48	0.91	12.15	7.72	93.76	3.08	0.06	0.87
5.50	0.94	12.53	6.94	86.94	3.02	0.06	0.89
5.52	0.98	13.09	6.23	81.53	2.95	0.06	0.93
5.54	1.01	13.52	5.69	76.99	2.90	0.07	0.97
5.56	1.03	13.66	5.47	74.80	2.88	0.07	0.98
5.58	1.00	13.33	5.57	74.26	2.89	0.07	0.96
5.60	0.98	13.04	5.79	75.45	2.91	0.07	0.93
5.62	0.96	12.65	6.09	77.06	2.94	0.06	0.90
5.64	0.94	12.30	6.35	78.13	2.96	0.06	0.88
5.66	0.91	11.86	6.63	78.64	2.99	0.06	0.85
5.68	0.91	11.86	6.69	79.32	2.99	0.06	0.85
5.70	0.96	12.57	6.31	79.28	2.96	0.06	0.90
5.72	1.07	14.12	5.53	78.08	2.88	0.07	1.02
5.74	1.28	16.78	4.49	75.36	2.76	0.07	1.23
5.76	1.48	19.29	3.86	74.53	2.68	0.08	1.43

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	1.62	21.12	3.71	78.33	2.66	0.08	1.57
5.80	1.62	21.30	4.04	86.05	2.71	0.08	1.57
5.82	1.57	20.74	4.58	95.08	2.78	0.08	1.51
5.84	1.60	21.14	4.80	101.48	2.80	0.08	1.54
5.86	1.63	21.64	4.87	105.31	2.81	0.08	1.57
5.88	1.70	22.47	4.79	107.57	2.80	0.08	1.63
5.90	1.75	23.08	4.68	107.91	2.79	0.08	1.68
5.92	1.91	25.04	4.27	106.99	2.74	0.09	1.84
5.94	2.15	28.13	3.75	105.43	2.66	0.09	2.08
5.96	2.36	30.68	3.42	105.07	2.62	0.09	2.28
5.98	2.49	32.28	3.25	104.75	2.59	0.09	0.68
6.00	2.50	32.30	3.18	102.85	2.58	0.09	0.68
6.02	2.42	31.19	3.18	99.07	2.57	0.09	0.68
6.04	2.22	28.57	3.33	95.25	2.60	0.09	2.13
6.06	1.96	25.12	3.74	93.97	2.66	0.09	1.86
6.08	1.75	22.45	4.23	94.91	2.73	0.08	1.64
6.10	1.73	22.08	4.27	94.37	2.74	0.08	1.62
6.12	1.80	22.97	4.09	94.02	2.71	0.09	1.69
6.14	1.77	22.60	4.31	97.32	2.74	0.09	1.65
6.16	1.57	20.05	5.22	104.70	2.85	0.08	1.45
6.18	1.29	16.42	6.70	109.92	3.00	0.07	1.17
6.20	1.13	14.11	7.61	107.32	3.07	0.06	1.01
6.22	1.08	13.33	7.69	102.57	3.08	0.06	0.95
6.24	1.12	13.93	7.05	98.19	3.03	0.07	0.99
6.26	1.17	14.61	6.67	97.47	2.99	0.07	1.04
6.28	1.21	15.10	6.42	97.02	2.97	0.07	1.08
6.30	1.22	15.15	6.40	96.98	2.97	0.07	1.08
6.32	1.23	15.21	6.36	96.70	2.96	0.07	1.09
6.34	1.24	15.37	6.32	97.15	2.96	0.07	1.10
6.36	1.28	15.80	6.23	98.46	2.95	0.07	1.13
6.38	1.31	16.25	6.25	101.50	2.95	0.07	1.16
6.40	1.35	16.67	6.27	104.49	2.96	0.07	1.19
6.42	1.38	17.06	6.26	106.77	2.96	0.07	1.22
6.44	1.46	18.17	5.91	107.48	2.92	0.07	1.30
6.46	1.58	19.56	5.52	107.94	2.88	0.08	1.40
6.48	1.67	20.71	5.24	108.55	2.85	0.08	1.49
6.50	1.67	20.72	5.36	110.96	2.86	0.08	1.49
6.52	1.60	19.82	5.79	114.68	2.91	0.07	1.42
6.54	1.51	18.56	6.38	118.46	2.97	0.07	1.33
6.56	1.42	17.27	7.06	121.85	3.03	0.07	1.23
6.59	1.34	16.25	7.64	124.17	3.08	0.07	1.16
6.60	1.29	15.47	8.14	125.95	3.12	0.07	1.11
6.62	1.26	15.09	8.37	126.35	3.14	0.07	1.08
6.64	1.24	14.77	8.50	125.50	3.14	0.07	1.05
6.66	1.23	14.58	8.45	123.21	3.14	0.07	1.04
6.68	1.20	14.21	8.45	120.05	3.14	0.07	1.01
6.70	1.17	13.82	8.45	116.72	3.14	0.07	0.99
6.72	1.15	13.42	8.50	114.09	3.15	0.06	0.96

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	1.13	13.22	8.47	112.02	3.14	0.06	0.94
6.76	1.13	13.19	8.34	110.06	3.13	0.06	0.94
6.78	1.14	13.23	8.16	108.00	3.12	0.06	0.95
6.80	1.15	13.38	7.92	106.05	3.10	0.07	0.96
6.82	1.16	13.43	7.77	104.35	3.09	0.07	0.96
6.84	1.16	13.41	7.66	102.71	3.08	0.07	0.96
6.86	1.13	12.94	7.91	102.42	3.10	0.06	0.92
6.88	1.08	12.34	8.36	103.21	3.13	0.06	0.88
6.90	1.02	11.50	9.14	105.15	3.19	0.06	0.82
6.92	0.96	10.78	9.89	106.61	3.25	0.06	0.77
6.94	0.92	10.16	10.61	107.70	3.29	0.06	0.73
6.96	0.90	9.86	10.97	108.13	3.32	0.06	0.70
6.98	0.92	10.07	10.74	108.06	3.30	0.06	0.72
7.00	0.97	10.78	9.91	106.83	3.25	0.06	0.77
7.02	1.06	11.90	8.74	104.03	3.16	0.06	0.85
7.04	1.16	13.05	7.68	100.17	3.08	0.07	0.93
7.06	1.23	13.90	6.95	96.56	3.02	0.07	0.99
7.08	1.26	14.26	6.62	94.44	2.99	0.07	1.02
7.10	1.27	14.36	6.54	93.89	2.98	0.07	1.03
7.12	1.27	14.30	6.65	95.13	2.99	0.07	1.02
7.14	1.26	14.20	6.85	97.33	3.01	0.07	1.01
7.16	1.27	14.25	7.04	100.32	3.03	0.07	1.02
7.18	1.28	14.32	7.22	103.40	3.04	0.07	1.02
7.20	1.28	14.33	7.38	105.78	3.06	0.07	1.02
7.22	1.25	13.94	7.65	106.62	3.08	0.07	1.00
7.25	1.23	13.57	7.88	106.95	3.10	0.07	0.97
7.26	1.20	13.29	8.08	107.42	3.11	0.07	0.95
7.28	1.19	13.10	8.31	108.85	3.13	0.07	0.94
7.30	1.18	12.88	8.53	109.94	3.15	0.06	0.92
7.32	1.19	13.05	8.45	110.29	3.14	0.06	0.93
7.34	1.25	13.69	8.02	109.80	3.11	0.07	0.98
7.36	1.34	14.79	7.33	108.44	3.05	0.07	1.06
7.38	1.43	15.86	6.71	106.37	3.00	0.07	1.13
7.40	1.48	16.49	6.37	105.02	2.97	0.07	1.18
7.42	1.49	16.50	6.36	104.94	2.96	0.07	1.18
7.44	1.44	15.89	6.74	107.05	3.00	0.07	1.14
7.46	1.39	15.19	7.29	110.70	3.05	0.07	1.08
7.48	1.33	14.46	7.92	114.46	3.10	0.07	1.03
7.50	1.29	13.95	8.45	117.91	3.14	0.07	1.00
7.52	1.27	13.65	8.81	120.22	3.17	0.07	0.97
7.54	1.25	13.47	9.02	121.54	3.18	0.07	0.96
7.56	1.26	13.47	9.01	121.42	3.18	0.07	0.96
7.58	1.27	13.57	8.81	119.49	3.17	0.07	0.97
7.60	1.30	13.87	8.43	116.88	3.14	0.07	0.99
7.62	1.33	14.28	8.03	114.64	3.11	0.07	1.02
7.64	1.36	14.61	7.69	112.37	3.08	0.07	1.04
7.66	1.38	14.81	7.44	110.20	3.06	0.07	1.06
7.68	1.38	14.78	7.31	108.05	3.05	0.07	1.06

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	1.37	14.62	7.37	107.67	3.05	0.07	1.04
7.72	1.35	14.31	7.62	109.10	3.08	0.07	1.02
7.74	1.32	13.95	7.98	111.37	3.10	0.07	1.00
7.76	1.30	13.64	8.32	113.52	3.13	0.07	0.97
7.78	1.28	13.34	8.66	115.52	3.16	0.07	0.95
7.80	1.26	13.10	8.98	117.65	3.18	0.07	0.94
7.82	1.26	13.06	9.06	118.42	3.19	0.07	0.93
7.84	1.27	13.18	8.96	118.12	3.18	0.07	0.94
7.86	1.29	13.36	8.71	116.34	3.16	0.07	0.95
7.88	1.28	13.30	8.61	114.48	3.15	0.07	0.95
7.90	1.27	13.14	8.54	112.20	3.15	0.07	0.94
7.92	1.24	12.76	8.65	110.34	3.16	0.07	0.91
7.94	1.20	12.20	8.87	108.24	3.17	0.06	0.87
7.96	1.13	11.41	9.25	105.52	3.20	0.06	0.82
7.98	1.05	10.44	9.78	102.10	3.24	0.06	0.75
8.00	0.96	9.38	10.50	98.52	3.29	0.06	0.67
8.02	0.86	8.29	11.44	94.79	3.35	0.06	0.59
8.04	0.78	7.25	12.49	90.59	3.41	0.06	0.52
8.06	0.70	6.38	13.59	86.72	3.47	0.06	0.46
8.08	0.64	5.67	14.57	82.58	3.53	0.06	0.40
8.10	0.60	5.25	14.99	78.71	3.55	0.06	0.37
8.12	0.57	4.88	15.22	74.35	3.56	0.06	0.35
8.14	0.54	4.51	15.56	70.20	3.58	0.06	0.32
8.16	0.51	4.14	15.96	66.08	3.60	0.06	0.30
8.18	0.51	4.09	15.35	62.77	3.57	0.06	0.29
8.20	0.53	4.32	13.93	60.16	3.49	0.06	0.31
8.22	0.55	4.60	12.59	57.87	3.42	0.06	0.33
8.24	0.56	4.65	12.05	56.00	3.38	0.06	0.33
8.26	0.55	4.55	11.93	54.24	3.38	0.06	0.32
8.28	0.53	4.36	12.00	52.35	3.38	0.06	0.31
8.30	0.52	4.15	12.05	50.00	3.38	0.06	0.30
8.32	0.51	4.03	11.86	47.79	3.37	0.06	0.29
8.34	0.51	4.09	11.33	46.30	3.34	0.06	0.29
8.36	0.53	4.31	10.66	45.90	3.30	0.06	0.31
8.39	0.56	4.60	10.03	46.09	3.25	0.06	0.33
8.40	0.60	4.99	9.40	46.86	3.21	0.06	0.36
8.42	0.63	5.40	8.82	47.68	3.17	0.06	0.39
8.44	0.66	5.72	8.56	48.94	3.15	0.06	0.41
8.46	0.66	5.65	9.01	50.91	3.18	0.06	0.40
8.48	0.64	5.42	9.67	52.39	3.23	0.06	0.39
8.50	0.62	5.23	10.17	53.12	3.26	0.06	0.37
8.52	0.63	5.26	10.11	53.12	3.26	0.06	0.38
8.54	0.63	5.31	10.11	53.68	3.26	0.06	0.38
8.56	0.63	5.33	10.17	54.25	3.26	0.06	0.38
8.58	0.62	5.21	10.44	54.43	3.28	0.06	0.37
8.60	0.60	4.96	10.76	53.32	3.30	0.06	0.35
8.63	0.59	4.77	10.90	52.02	3.31	0.06	0.34
8.64	0.58	4.73	10.70	50.61	3.30	0.06	0.34

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	0.61	5.03	9.92	49.96	3.25	0.06	0.36
8.68	0.65	5.44	9.12	49.58	3.19	0.06	0.39
8.70	0.70	5.94	8.45	50.16	3.14	0.06	0.42
8.72	0.73	6.27	8.16	51.16	3.12	0.06	0.45
8.74	0.75	6.45	8.12	52.41	3.12	0.06	0.46
8.76	0.75	6.44	8.41	54.17	3.14	0.06	0.46
8.78	0.75	6.50	8.67	56.36	3.16	0.06	0.46
8.80	0.77	6.68	8.79	58.69	3.17	0.06	0.48
8.82	0.80	7.04	8.53	60.02	3.15	0.06	0.50
8.84	0.84	7.37	8.38	61.76	3.14	0.06	0.53
8.86	0.85	7.49	8.48	63.58	3.14	0.06	0.54
8.88	0.85	7.44	8.83	65.67	3.17	0.06	0.53
8.90	0.82	7.19	9.26	66.63	3.20	0.06	0.51
8.92	0.80	6.91	9.77	67.56	3.24	0.06	0.49
8.95	0.78	6.73	10.12	68.17	3.26	0.06	0.48
8.96	0.80	6.89	9.95	68.52	3.25	0.06	0.49
8.98	0.84	7.29	9.30	67.75	3.20	0.06	0.52
9.00	0.85	7.40	9.11	67.40	3.19	0.06	0.53
9.02	0.82	7.09	9.50	67.30	3.22	0.06	0.51
9.04	0.77	6.48	10.39	67.36	3.28	0.06	0.46
9.06	0.73	6.11	10.90	66.63	3.31	0.06	0.44
9.08	0.72	5.95	11.07	65.91	3.32	0.06	0.43
9.10	0.72	5.97	11.00	65.64	3.32	0.06	0.43
9.12	0.71	5.81	11.12	64.58	3.33	0.06	0.41
9.14	0.68	5.55	11.35	62.94	3.34	0.06	0.40
9.16	0.64	5.09	11.80	60.02	3.37	0.06	0.36
9.18	0.61	4.69	12.21	57.27	3.39	0.06	0.33
9.20	0.58	4.45	12.29	54.76	3.40	0.06	0.32
9.23	0.59	4.49	11.82	53.05	3.37	0.06	0.32
9.24	0.63	4.87	10.68	52.00	3.30	0.06	0.35
9.26	0.67	5.28	9.71	51.33	3.23	0.06	0.38
9.28	0.69	5.55	9.13	50.70	3.19	0.06	0.40
9.30	0.68	5.43	9.22	50.07	3.20	0.06	0.39
9.32	0.65	5.11	9.57	48.87	3.22	0.06	0.36
9.34	0.64	4.96	9.62	47.75	3.23	0.06	0.35
9.36	0.67	5.24	8.99	47.15	3.18	0.06	0.37
9.38	0.70	5.55	8.49	47.13	3.14	0.06	0.40
9.40	0.72	5.79	8.38	48.51	3.14	0.06	0.41
9.42	0.76	6.15	8.24	50.68	3.12	0.06	0.44
9.44	0.87	7.27	7.32	53.22	3.05	0.06	0.52
9.46	1.05	9.14	5.96	54.44	2.93	0.06	0.65
9.48	1.23	10.99	4.99	54.91	2.82	0.07	0.79
9.50	1.31	11.82	4.83	57.02	2.80	0.07	0.84
9.52	1.21	10.80	5.62	60.65	2.89	0.07	0.77
9.54	1.00	8.55	7.39	63.14	3.06	0.06	0.61
9.56	0.80	6.55	9.57	62.71	3.22	0.06	0.47
9.58	0.71	5.58	11.08	61.76	3.32	0.06	0.40
9.60	0.70	5.44	11.35	61.79	3.34	0.06	0.39

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	0.70	5.49	11.18	61.39	3.33	0.06	0.39
9.64	0.71	5.55	10.71	59.44	3.30	0.06	0.40
9.66	0.72	5.59	10.15	56.75	3.26	0.06	0.40
9.68	0.73	5.73	9.46	54.19	3.22	0.06	0.41
9.70	0.76	6.06	8.68	52.56	3.16	0.06	0.43
9.72	0.81	6.52	7.90	51.46	3.10	0.06	0.47
9.74	0.83	6.68	7.68	51.33	3.08	0.06	0.48
9.76	0.79	6.34	8.25	52.29	3.13	0.06	0.45
9.78	0.77	6.11	8.77	53.53	3.16	0.06	0.44
9.80	0.92	7.62	8.16	62.13	3.12	0.06	0.54
9.82	1.10	9.37	7.49	70.21	3.06	0.06	0.67
9.84	1.24	10.75	7.22	77.65	3.04	0.06	0.77
9.86	1.17	10.05	7.76	77.91	3.09	0.06	0.72
9.88	1.05	8.85	8.56	75.74	3.15	0.06	0.63
9.90	0.90	7.35	9.79	71.97	3.24	0.06	0.53
9.92	0.78	6.13	11.23	68.85	3.33	0.06	0.44
9.95	0.71	5.33	12.40	66.12	3.40	0.06	0.38
9.96	0.67	4.97	12.81	63.67	3.43	0.06	0.36
9.98	0.65	4.72	12.84	60.66	3.43	0.06	0.34
10.00	0.64	4.60	12.42	57.18	3.41	0.06	0.33
10.02	0.63	4.54	11.81	53.62	3.37	0.06	0.32
10.04	0.64	4.65	10.94	50.82	3.31	0.06	0.33
10.06	0.67	4.91	9.99	49.06	3.25	0.06	0.35
10.08	0.69	5.09	9.56	48.64	3.22	0.06	0.36
10.10	0.70	5.19	9.40	48.74	3.21	0.06	0.37
10.12	0.69	5.11	9.63	49.19	3.23	0.06	0.36
10.14	0.69	5.06	9.78	49.50	3.24	0.06	0.36
10.16	0.68	4.99	9.99	49.85	3.25	0.06	0.36
10.18	0.68	4.97	10.10	50.19	3.26	0.06	0.35
10.20	0.68	4.97	10.15	50.46	3.26	0.06	0.35
10.22	0.68	4.96	10.13	50.29	3.26	0.06	0.35
10.24	0.67	4.83	10.31	49.81	3.27	0.06	0.35
10.26	0.66	4.68	10.43	48.86	3.28	0.06	0.33
10.28	0.65	4.58	10.51	48.10	3.29	0.06	0.33
10.30	0.64	4.56	10.36	47.30	3.28	0.06	0.33
10.32	0.64	4.55	10.35	47.07	3.28	0.06	0.32
10.34	0.65	4.57	10.34	47.28	3.28	0.06	0.33
10.36	0.65	4.62	10.35	47.82	3.28	0.06	0.33
10.38	0.67	4.75	10.15	48.20	3.26	0.06	0.34
10.40	0.68	4.82	10.03	48.37	3.25	0.06	0.34
10.42	0.69	4.92	9.83	48.37	3.24	0.06	0.35
10.44	0.69	4.97	9.83	48.80	3.24	0.06	0.35
10.46	0.70	5.03	9.80	49.34	3.24	0.06	0.36
10.48	0.70	4.99	10.03	50.03	3.25	0.06	0.36
10.50	0.69	4.94	10.15	50.14	3.26	0.06	0.35
10.52	0.68	4.79	10.38	49.67	3.28	0.06	0.34
10.54	0.66	4.63	10.51	48.73	3.29	0.06	0.33
10.56	0.66	4.59	10.43	47.83	3.28	0.06	0.33

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	0.68	4.83	9.81	47.34	3.24	0.06	0.34
10.60	0.73	5.23	9.07	47.45	3.19	0.06	0.37
10.62	0.75	5.46	8.81	48.16	3.17	0.06	0.39
10.64	0.75	5.41	9.12	49.33	3.19	0.06	0.39
10.66	0.73	5.24	9.57	50.10	3.22	0.06	0.37
10.68	0.73	5.26	9.66	50.81	3.23	0.06	0.38
10.70	0.77	5.59	9.23	51.64	3.20	0.06	0.40
10.72	0.83	6.12	8.61	52.70	3.15	0.06	0.44
10.74	0.88	6.61	8.11	53.56	3.11	0.06	0.47
10.76	0.90	6.78	8.10	54.93	3.11	0.06	0.48
10.78	0.90	6.76	8.50	57.42	3.14	0.06	0.48
10.80	0.89	6.68	8.99	59.99	3.18	0.06	0.48
10.82	0.87	6.50	9.56	62.17	3.22	0.06	0.46
10.84	0.86	6.39	9.93	63.38	3.25	0.06	0.46
10.86	0.86	6.37	10.07	64.11	3.26	0.06	0.45
10.88	0.88	6.50	9.91	64.36	3.25	0.06	0.46
10.90	0.88	6.49	9.86	63.97	3.24	0.06	0.46
10.92	0.83	6.07	10.44	63.32	3.28	0.06	0.43
10.94	0.79	5.69	10.92	62.08	3.31	0.06	0.41
10.96	0.78	5.53	10.93	60.42	3.31	0.06	0.39
10.98	0.80	5.76	10.20	58.75	3.27	0.06	0.41
11.00	0.83	6.01	9.55	57.41	3.22	0.06	0.43
11.02	0.83	6.03	9.43	56.88	3.21	0.06	0.43
11.04	0.82	5.88	9.52	56.01	3.22	0.06	0.42
11.06	0.80	5.70	9.61	54.72	3.23	0.06	0.41
11.08	0.81	5.82	9.18	53.43	3.20	0.06	0.42
11.10	0.86	6.19	8.57	53.02	3.15	0.06	0.44
11.12	0.90	6.58	8.05	52.98	3.11	0.06	0.47
11.14	0.91	6.66	8.09	53.90	3.11	0.06	0.48
11.16	0.90	6.54	8.39	54.85	3.14	0.06	0.47
11.18	0.88	6.39	8.77	55.99	3.16	0.06	0.46
11.20	0.88	6.41	8.88	56.87	3.17	0.06	0.46
11.22	0.89	6.47	8.91	57.64	3.18	0.06	0.46
11.24	0.89	6.42	9.10	58.45	3.19	0.06	0.46
11.26	0.86	6.14	9.62	59.01	3.23	0.06	0.44
11.28	0.81	5.70	10.31	58.80	3.27	0.06	0.41
11.30	0.78	5.36	10.77	57.69	3.30	0.06	0.38
11.32	0.77	5.27	10.63	56.07	3.29	0.06	0.38
11.34	0.79	5.45	10.05	54.80	3.26	0.06	0.39
11.36	0.82	5.77	9.38	54.08	3.21	0.06	0.41
11.38	0.86	6.06	8.84	53.57	3.17	0.06	0.43
11.40	0.88	6.23	8.63	53.76	3.15	0.06	0.44
11.42	0.89	6.31	8.61	54.34	3.15	0.06	0.45
11.44	0.88	6.27	8.83	55.37	3.17	0.06	0.45
11.46	0.87	6.17	9.08	56.02	3.19	0.06	0.44
11.48	0.86	6.02	9.41	56.67	3.21	0.06	0.43
11.50	0.86	6.06	9.45	57.23	3.21	0.06	0.43
11.52	0.88	6.23	9.24	57.53	3.20	0.06	0.44

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	0.92	6.52	8.83	57.60	3.17	0.06	0.47
11.56	0.94	6.72	8.57	57.58	3.15	0.06	0.48
11.58	0.95	6.83	8.51	58.13	3.15	0.06	0.49
11.60	0.96	6.87	8.58	58.97	3.15	0.06	0.49
11.62	0.97	6.91	8.71	60.18	3.16	0.06	0.49
11.64	0.97	6.95	8.84	61.39	3.17	0.06	0.50
11.66	0.98	6.98	8.95	62.47	3.18	0.06	0.50
11.68	0.99	7.11	8.89	63.19	3.17	0.06	0.51
11.70	1.03	7.43	8.59	63.81	3.15	0.06	0.53
11.72	1.07	7.76	8.33	64.63	3.13	0.06	0.55
11.74	1.11	8.10	8.09	65.48	3.11	0.06	0.58
11.76	1.12	8.20	8.11	66.52	3.11	0.06	0.59
11.78	1.12	8.21	8.26	67.79	3.13	0.06	0.59
11.80	1.10	7.98	8.69	69.28	3.16	0.06	0.57
11.82	1.07	7.70	9.19	70.82	3.20	0.06	0.55
11.84	1.05	7.53	9.55	71.89	3.22	0.06	0.54
11.86	1.06	7.56	9.61	72.68	3.23	0.06	0.54
11.88	1.05	7.54	9.70	73.17	3.23	0.06	0.54
11.90	1.04	7.43	9.86	73.28	3.24	0.06	0.53
11.92	1.02	7.20	10.20	73.40	3.27	0.06	0.51
11.94	1.01	7.13	10.26	73.14	3.27	0.06	0.51
11.96	1.01	7.10	10.29	73.04	3.27	0.06	0.51
11.98	1.02	7.16	10.19	72.90	3.26	0.06	0.51
12.00	1.03	7.26	10.07	73.09	3.26	0.06	0.52
12.02	1.05	7.43	9.84	73.13	3.24	0.06	0.53
12.04	1.08	7.64	9.54	72.87	3.22	0.06	0.55
12.06	1.10	7.81	9.27	72.40	3.20	0.06	0.56
12.08	1.12	7.97	9.08	72.34	3.19	0.06	0.57
12.10	1.13	8.10	8.99	72.79	3.18	0.06	0.58
12.12	1.15	8.21	8.97	73.66	3.18	0.06	0.59
12.14	1.16	8.26	9.04	74.71	3.19	0.06	0.59
12.16	1.16	8.24	9.24	76.15	3.20	0.06	0.59
12.18	1.15	8.16	9.49	77.48	3.22	0.06	0.58
12.20	1.14	8.11	9.68	78.50	3.23	0.06	0.58
12.22	1.14	8.06	9.78	78.77	3.24	0.06	0.58
12.24	1.13	8.00	9.82	78.55	3.24	0.06	0.57
12.26	1.13	7.91	9.86	77.97	3.24	0.06	0.56
12.28	1.12	7.87	9.79	77.11	3.24	0.06	0.56
12.30	1.12	7.82	9.73	76.06	3.23	0.06	0.56
12.32	1.11	7.74	9.69	75.02	3.23	0.06	0.55
12.34	1.11	7.70	9.65	74.30	3.23	0.06	0.55
12.36	1.10	7.63	9.71	74.10	3.23	0.06	0.54
12.38	1.11	7.67	9.65	74.00	3.23	0.06	0.55
12.40	1.11	7.67	9.62	73.81	3.23	0.06	0.55
12.42	1.12	7.80	9.42	73.46	3.21	0.06	0.56
12.44	1.13	7.87	9.31	73.23	3.20	0.06	0.56
12.46	1.14	7.94	9.22	73.23	3.20	0.06	0.57
12.48	1.16	8.04	9.11	73.28	3.19	0.06	0.57

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	1.17	8.15	8.99	73.22	3.18	0.06	0.58
12.52	1.19	8.30	8.86	73.53	3.17	0.06	0.59
12.54	1.21	8.42	8.79	74.01	3.17	0.06	0.60
12.56	1.22	8.50	8.84	75.16	3.17	0.06	0.61
12.58	1.22	8.53	8.95	76.39	3.18	0.06	0.61
12.60	1.22	8.52	9.17	78.11	3.19	0.06	0.61
12.62	1.23	8.58	9.29	79.67	3.20	0.06	0.61
12.64	1.24	8.67	9.36	81.10	3.21	0.06	0.62
12.66	1.26	8.80	9.35	82.26	3.21	0.06	0.63
12.68	1.26	8.80	9.52	83.84	3.22	0.06	0.63
12.70	1.25	8.69	9.82	85.34	3.24	0.06	0.62
12.72	1.23	8.49	10.20	86.56	3.27	0.06	0.61
12.74	1.23	8.46	10.26	86.79	3.27	0.06	0.60
12.76	1.24	8.57	10.10	86.57	3.26	0.06	0.61
12.78	1.30	9.00	9.59	86.28	3.22	0.06	0.64
12.80	1.35	9.40	9.16	86.03	3.19	0.06	0.67
12.82	1.39	9.72	8.83	85.78	3.17	0.06	0.69
12.84	1.40	9.80	8.77	85.92	3.17	0.06	0.70
12.86	1.39	9.73	8.89	86.53	3.17	0.06	0.69
12.88	1.37	9.55	9.14	87.28	3.19	0.06	0.68
12.90	1.36	9.39	9.37	88.01	3.21	0.06	0.67
12.92	1.35	9.35	9.46	88.51	3.22	0.06	0.67
12.94	1.36	9.39	9.45	88.81	3.21	0.06	0.67
12.96	1.37	9.48	9.32	88.28	3.20	0.06	0.68
12.98	1.37	9.45	9.26	87.48	3.20	0.06	0.67
13.00	1.37	9.45	9.14	86.40	3.19	0.06	0.68
13.02	1.36	9.34	9.17	85.69	3.19	0.06	0.67
13.04	1.35	9.26	9.22	85.35	3.20	0.06	0.66
13.06	1.34	9.14	9.34	85.34	3.21	0.06	0.65
13.08	1.34	9.14	9.33	85.24	3.21	0.06	0.65
13.10	1.35	9.16	9.27	84.90	3.20	0.06	0.65
13.12	1.36	9.24	9.15	84.56	3.19	0.06	0.66
13.14	1.36	9.26	9.11	84.36	3.19	0.06	0.66
13.16	1.36	9.23	9.14	84.35	3.19	0.06	0.66
13.19	1.36	9.23	9.16	84.51	3.19	0.06	0.66
13.20	1.37	9.25	9.17	84.81	3.19	0.06	0.66
13.22	1.38	9.33	9.14	85.32	3.19	0.06	0.67
13.24	1.37	9.29	9.26	85.96	3.20	0.06	0.66
13.26	1.35	9.04	9.58	86.65	3.22	0.06	0.65
13.28	1.31	8.72	9.96	86.87	3.25	0.06	0.62
13.30	1.28	8.46	10.27	86.84	3.27	0.06	0.60
13.32	1.25	8.22	10.54	86.64	3.29	0.06	0.59
13.34	1.22	7.99	10.82	86.43	3.31	0.06	0.57
13.36	1.19	7.71	11.10	85.56	3.32	0.06	0.55
13.38	1.16	7.49	11.28	84.49	3.34	0.06	0.53
13.40	1.14	7.33	11.35	83.16	3.34	0.06	0.52
13.42	1.12	7.09	11.56	82.01	3.35	0.06	0.51
13.44	1.09	6.84	11.77	80.54	3.37	0.06	0.49

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	1.05	6.55	11.99	78.61	3.38	0.06	0.47
13.48	1.02	6.32	12.10	76.41	3.39	0.06	0.45
13.50	1.00	6.09	12.17	74.09	3.39	0.06	0.43
13.52	0.97	5.86	12.26	71.79	3.40	0.06	0.42
13.54	0.94	5.61	12.40	69.50	3.40	0.06	0.40
13.56	0.91	5.35	12.58	67.24	3.41	0.06	0.38
13.58	0.87	5.04	12.95	65.20	3.44	0.06	0.36
13.60	0.84	4.77	13.26	63.28	3.45	0.06	0.34
13.62	0.81	4.59	13.40	61.48	3.46	0.06	0.33
13.64	0.80	4.46	13.37	59.55	3.46	0.06	0.32
13.66	0.80	4.45	13.01	57.86	3.44	0.06	0.32
13.68	0.80	4.46	12.69	56.64	3.42	0.06	0.32
13.70	0.81	4.53	12.43	56.26	3.41	0.06	0.32
13.72	0.81	4.48	12.45	55.81	3.41	0.06	0.32
13.74	0.79	4.36	12.67	55.19	3.42	0.06	0.31
13.76	0.81	4.52	11.75	53.09	3.36	0.06	0.32
13.78	0.84	4.70	11.09	52.12	3.32	0.06	0.34
13.80	0.85	4.78	10.71	51.21	3.30	0.06	0.34
13.82	0.81	4.50	11.52	51.81	3.35	0.06	0.32
13.84	0.77	4.15	12.25	50.86	3.40	0.06	0.30
13.86	0.74	3.93	12.68	49.87	3.42	0.06	0.28
13.88	0.72	3.75	13.06	48.95	3.44	0.06	0.27
13.90	0.71	3.69	13.14	48.46	3.45	0.06	0.26
13.92	0.71	3.64	13.03	47.48	3.44	0.06	0.26
13.94	0.72	3.73	12.49	46.57	3.41	0.06	0.27
13.96	0.74	3.87	11.80	45.63	3.37	0.06	0.28
13.98	0.77	4.10	11.04	45.26	3.32	0.06	0.29
14.00	0.81	4.38	10.28	45.00	3.27	0.06	0.31
14.02	0.83	4.58	9.80	44.87	3.24	0.06	0.33
14.04	0.85	4.73	9.50	44.92	3.22	0.06	0.34
14.06	0.87	4.85	9.31	45.17	3.20	0.06	0.35
14.08	0.88	4.93	9.26	45.65	3.20	0.06	0.35
14.11	0.87	4.83	9.61	46.41	3.23	0.06	0.35
14.12	0.84	4.63	10.10	46.80	3.26	0.06	0.33
14.14	0.83	4.55	10.36	47.14	3.28	0.06	0.33
14.16	0.85	4.67	10.11	47.19	3.26	0.06	0.33
14.18	0.86	4.75	10.00	47.47	3.25	0.06	0.34
14.20	0.84	4.58	10.38	47.54	3.28	0.06	0.33
14.22	0.80	4.30	10.92	46.89	3.31	0.06	0.31
14.24	0.78	4.08	11.30	46.11	3.34	0.06	0.29
14.26	0.79	4.15	10.97	45.56	3.32	0.06	0.30
14.28	0.81	4.35	10.52	45.76	3.29	0.06	0.31
14.30	0.85	4.64	10.04	46.61	3.26	0.06	0.33
14.32	0.87	4.79	9.85	47.13	3.24	0.06	0.34
14.34	0.88	4.86	9.75	47.42	3.24	0.06	0.35
14.36	0.88	4.83	9.83	47.52	3.24	0.06	0.35
14.38	0.90	4.93	9.68	47.73	3.23	0.06	0.35
14.40	0.92	5.10	9.42	48.02	3.21	0.06	0.36

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	0.94	5.28	9.09	48.04	3.19	0.06	0.38
14.44	0.96	5.38	8.94	48.05	3.18	0.06	0.38
14.46	0.96	5.43	8.83	47.92	3.17	0.06	0.39
14.48	0.98	5.57	8.65	48.19	3.16	0.06	0.40
14.50	0.99	5.63	8.64	48.68	3.16	0.06	0.40
14.52	0.97	5.47	9.10	49.75	3.19	0.06	0.39
14.54	0.94	5.24	9.62	50.38	3.23	0.06	0.37
14.56	0.93	5.16	9.95	51.38	3.25	0.06	0.37
14.58	0.96	5.34	9.81	52.38	3.24	0.06	0.38
14.60	0.98	5.46	9.87	53.85	3.24	0.06	0.39
14.62	0.99	5.59	9.72	54.29	3.23	0.06	0.40
14.64	1.01	5.69	9.55	54.35	3.22	0.06	0.41
14.66	1.03	5.81	9.16	53.22	3.19	0.06	0.42
14.68	1.04	5.93	8.91	52.84	3.18	0.06	0.42
14.70	1.06	6.01	8.84	53.18	3.17	0.06	0.43
14.72	1.07	6.08	8.97	54.49	3.18	0.06	0.43
14.74	1.00	5.56	10.24	56.91	3.27	0.06	0.40
14.76	1.00	5.54	10.64	59.01	3.30	0.06	0.40
14.79	1.00	5.55	10.88	60.41	3.31	0.06	0.40
14.80	1.06	6.01	10.14	60.97	3.26	0.06	0.43
14.82	1.05	5.92	10.27	60.73	3.27	0.06	0.42
14.84	1.03	5.79	10.49	60.80	3.29	0.06	0.41
14.86	1.02	5.70	10.73	61.10	3.30	0.06	0.41
14.88	1.02	5.64	10.88	61.38	3.31	0.06	0.40
14.90	1.00	5.54	11.08	61.44	3.32	0.06	0.40
14.92	0.98	5.37	11.37	61.11	3.34	0.06	0.38
14.94	0.95	5.12	11.82	60.48	3.37	0.06	0.37
14.96	0.91	4.85	12.31	59.67	3.40	0.06	0.35
14.99	0.88	4.56	12.82	58.50	3.43	0.06	0.33
15.00	0.85	4.39	13.04	57.26	3.44	0.06	0.31
15.02	0.85	4.34	12.96	56.19	3.44	0.06	0.31
15.04	0.85	4.38	12.56	55.02	3.41	0.06	0.31
15.06	0.86	4.42	12.21	53.91	3.39	0.06	0.32
15.08	0.85	4.37	12.06	52.67	3.38	0.06	0.31
15.10	0.85	4.30	11.96	51.48	3.38	0.06	0.31
15.12	0.83	4.21	11.98	50.44	3.38	0.06	0.30
15.14	0.84	4.26	11.71	49.88	3.36	0.06	0.30
15.16	0.88	4.55	10.95	49.86	3.32	0.06	0.33
15.18	0.95	5.02	9.99	50.18	3.25	0.06	0.36
15.20	1.02	5.51	9.10	50.16	3.19	0.06	0.39
15.22	1.06	5.85	8.56	50.06	3.15	0.06	0.42
15.24	1.09	6.04	8.29	50.06	3.13	0.06	0.43
15.26	1.09	6.05	8.34	50.47	3.13	0.06	0.43
15.28	1.09	6.00	8.56	51.37	3.15	0.06	0.43
15.30	1.09	6.02	8.71	52.49	3.16	0.06	0.43
15.32	1.11	6.16	8.77	54.02	3.16	0.06	0.44
15.34	1.13	6.26	8.95	56.04	3.18	0.06	0.45
15.36	1.12	6.21	9.33	57.91	3.21	0.06	0.44

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	1.08	5.92	10.01	59.25	3.25	0.06	0.42
15.40	1.07	5.79	10.33	59.80	3.27	0.06	0.41
15.42	1.09	5.97	10.12	60.35	3.26	0.06	0.43
15.44	1.16	6.48	9.39	60.85	3.21	0.06	0.46
15.46	1.24	6.99	8.80	61.48	3.17	0.06	0.50
15.48	1.31	7.52	8.28	62.29	3.13	0.06	0.54
15.50	1.41	8.22	7.68	63.12	3.08	0.06	0.59
15.52	1.53	9.10	7.02	63.88	3.02	0.06	0.65
15.54	1.69	10.23	6.36	65.07	2.96	0.07	0.73
15.56	1.79	10.91	6.18	67.39	2.95	0.07	0.78
15.58	1.74	10.56	6.63	70.07	2.99	0.07	0.75
15.60	1.52	8.99	7.91	71.12	3.10	0.06	0.64
15.62	1.27	7.17	9.63	69.05	3.23	0.06	0.51
15.64	1.08	5.79	11.25	65.11	3.33	0.06	0.41
15.66	0.95	4.86	12.57	61.12	3.41	0.06	0.35
15.68	0.85	4.14	13.89	57.56	3.49	0.06	0.30
15.70	0.78	3.64	14.94	54.46	3.55	0.06	0.26
15.72	0.75	3.42	15.40	52.60	3.57	0.06	0.24
15.74	0.76	3.48	14.50	50.43	3.52	0.06	0.25

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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LIQUEFACTION ANALYSIS REPORT

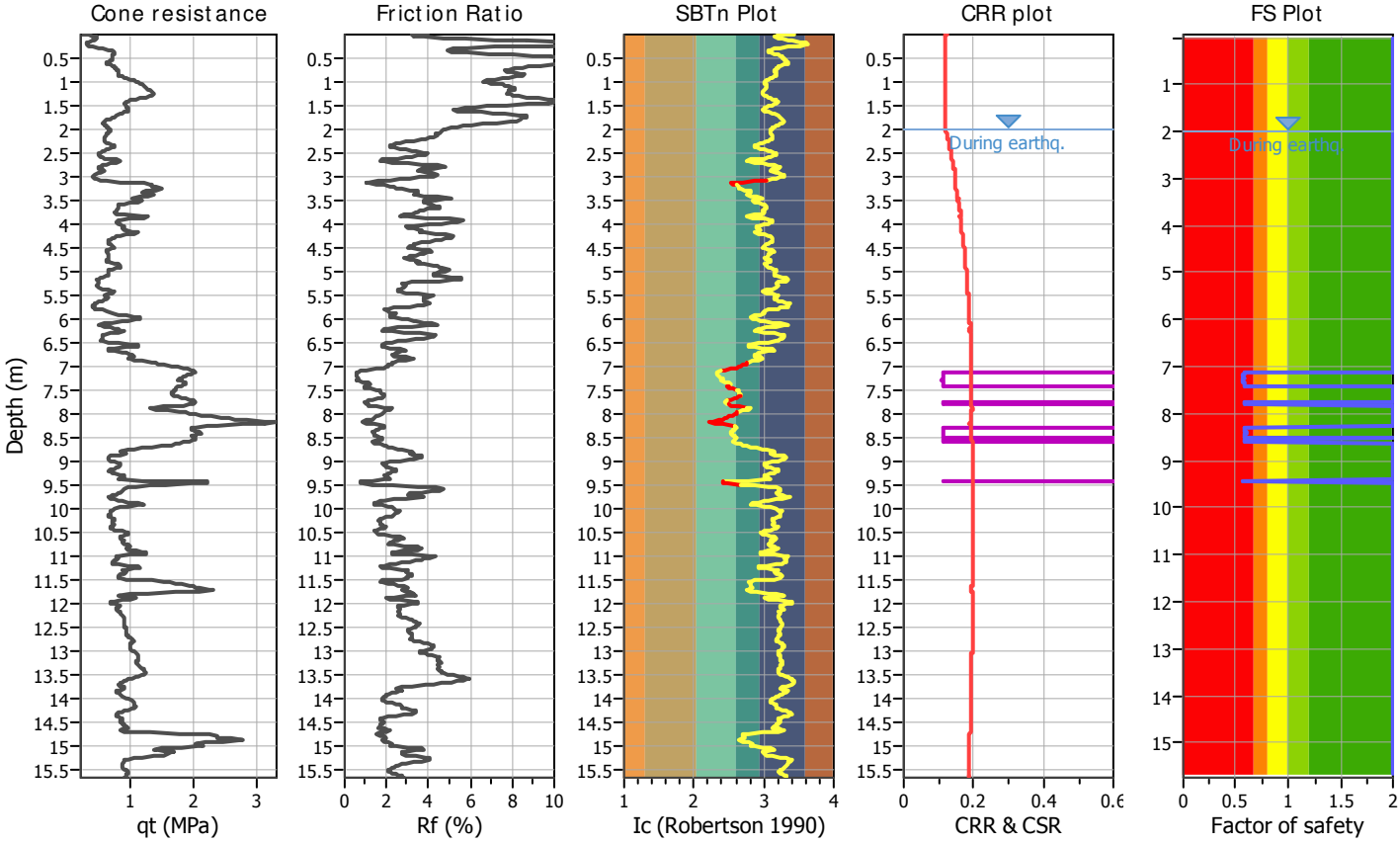
Project title :

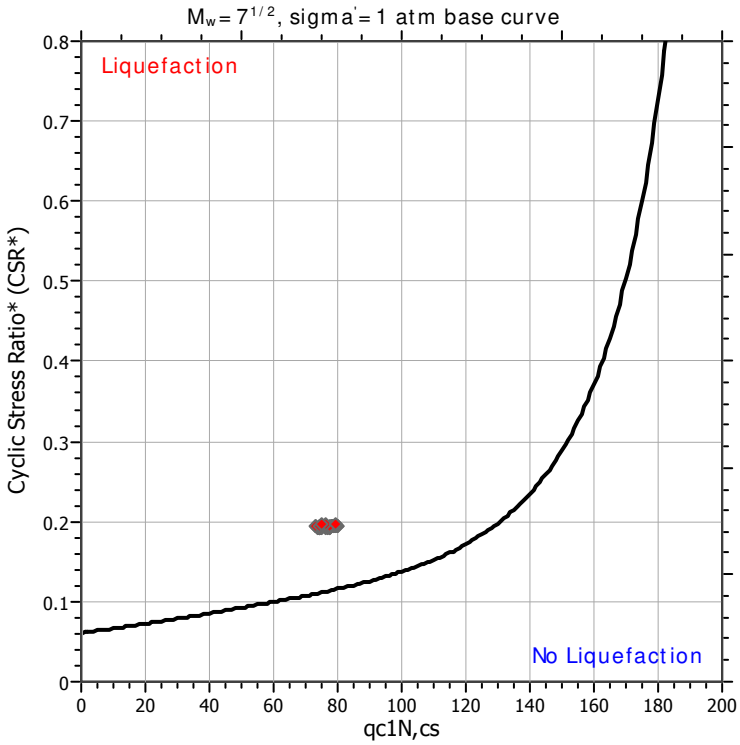
Location :

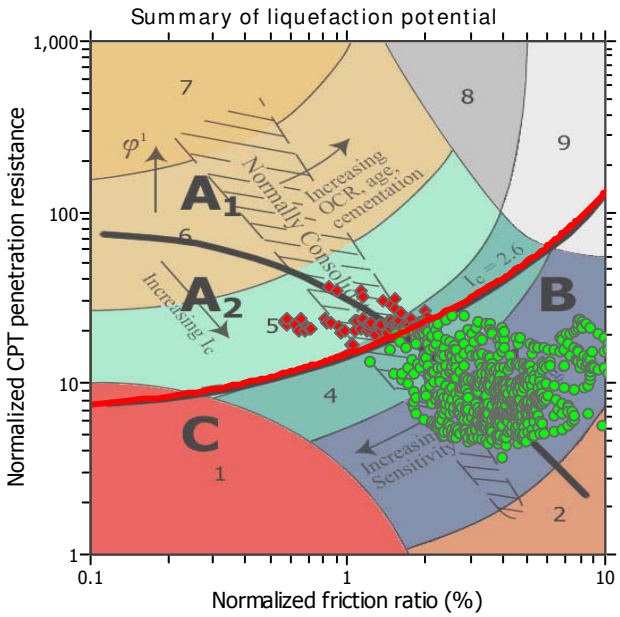
CPT file : Cptu-7

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.50 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.22	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

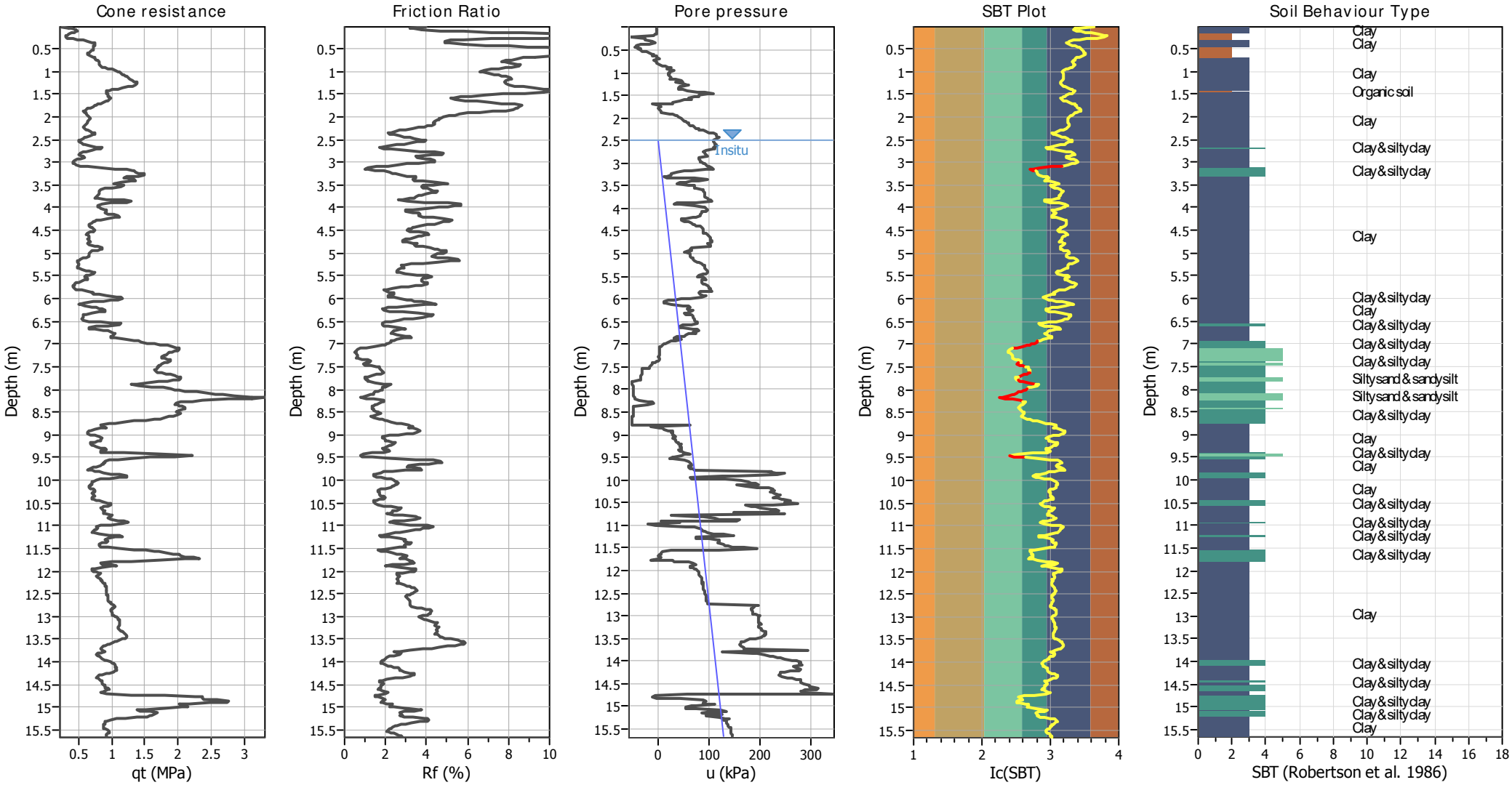






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



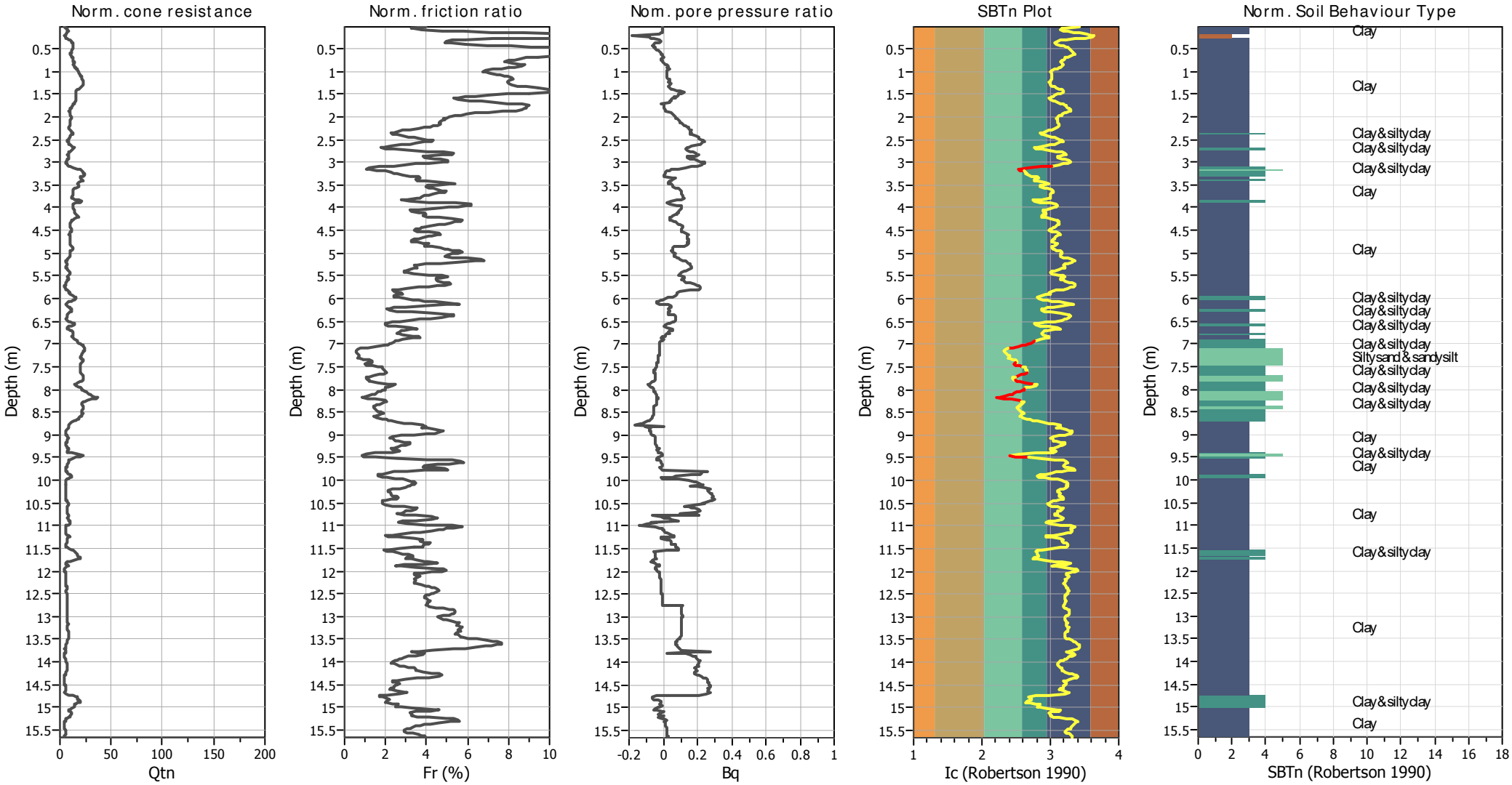
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



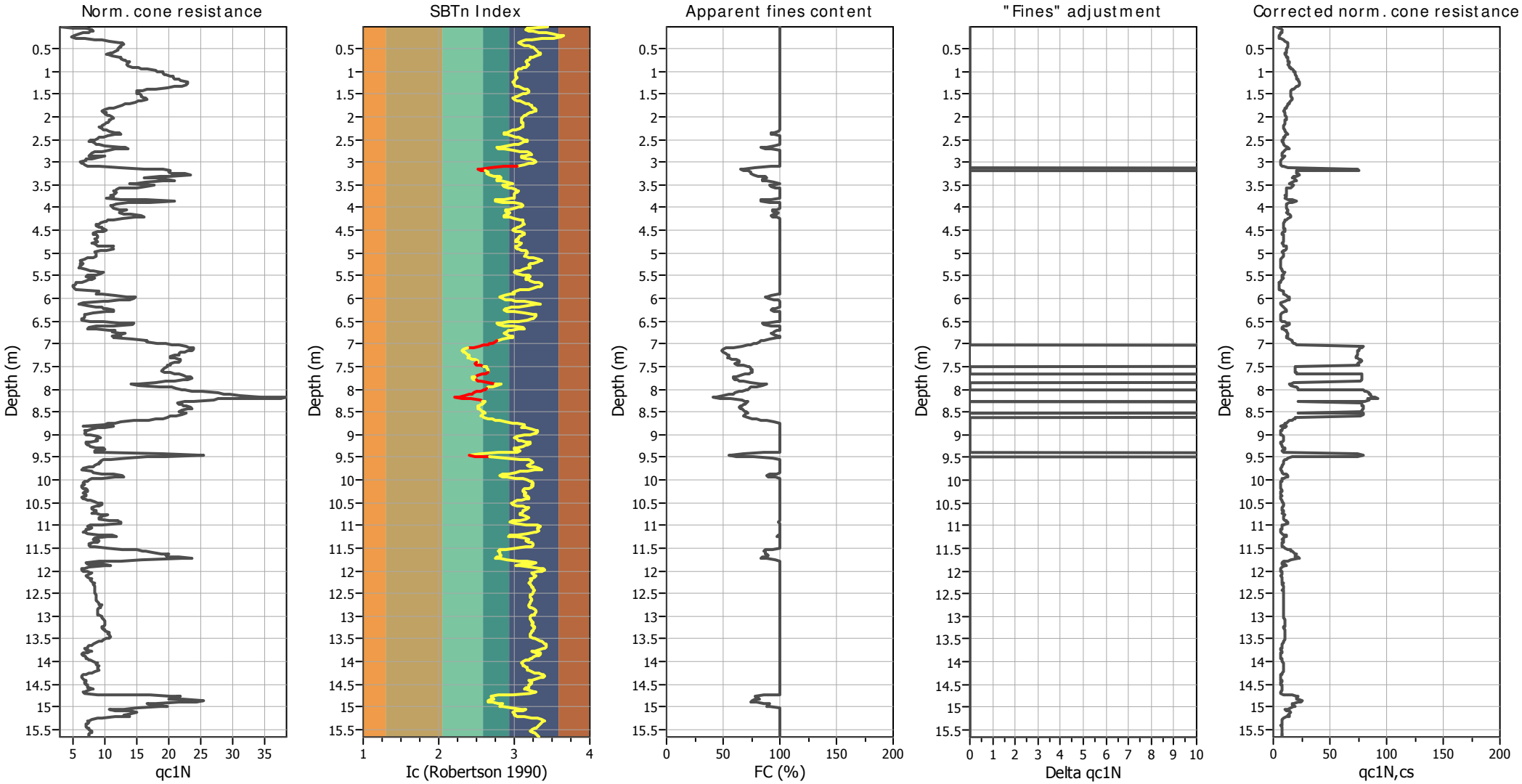
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

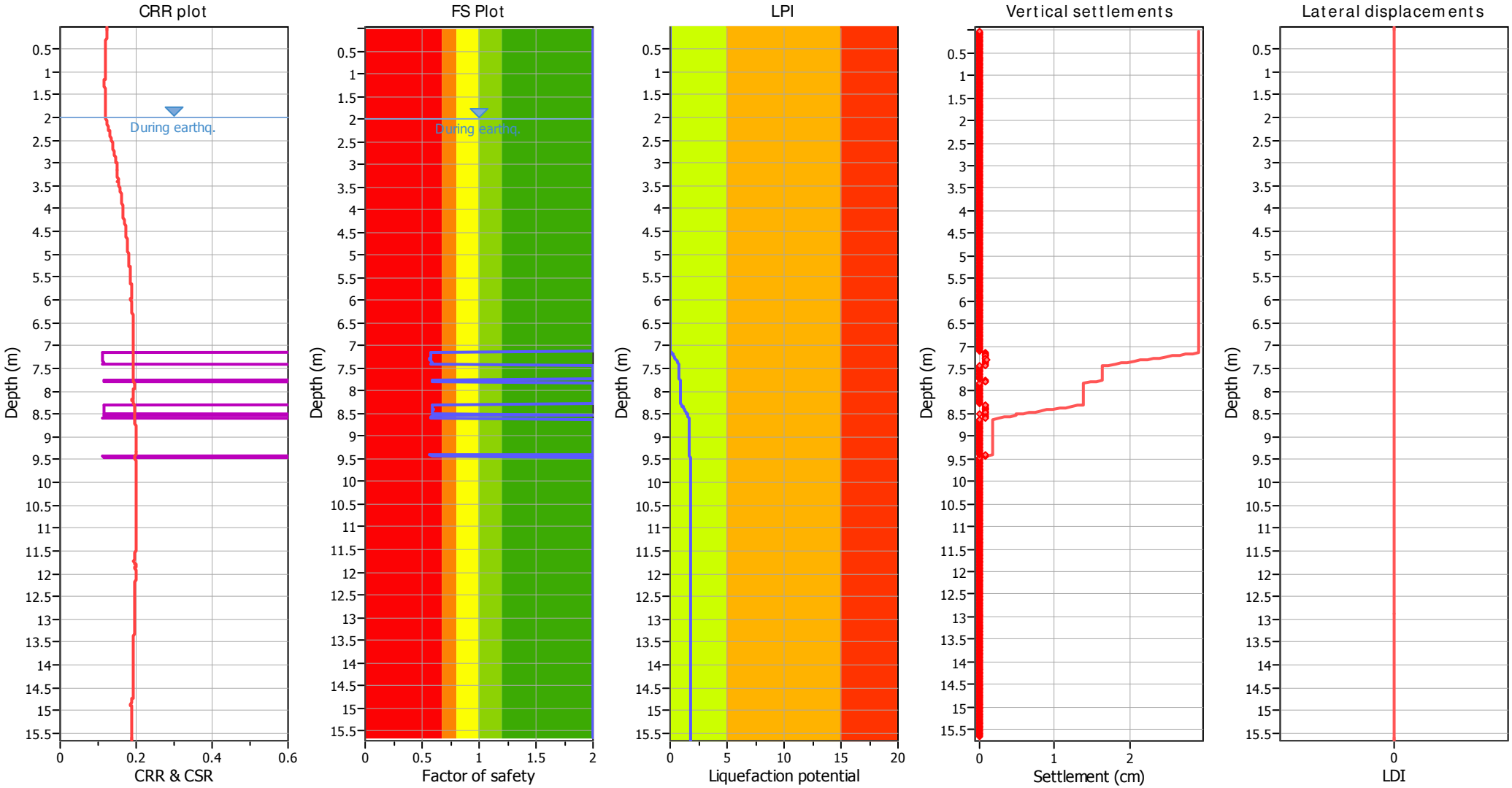
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

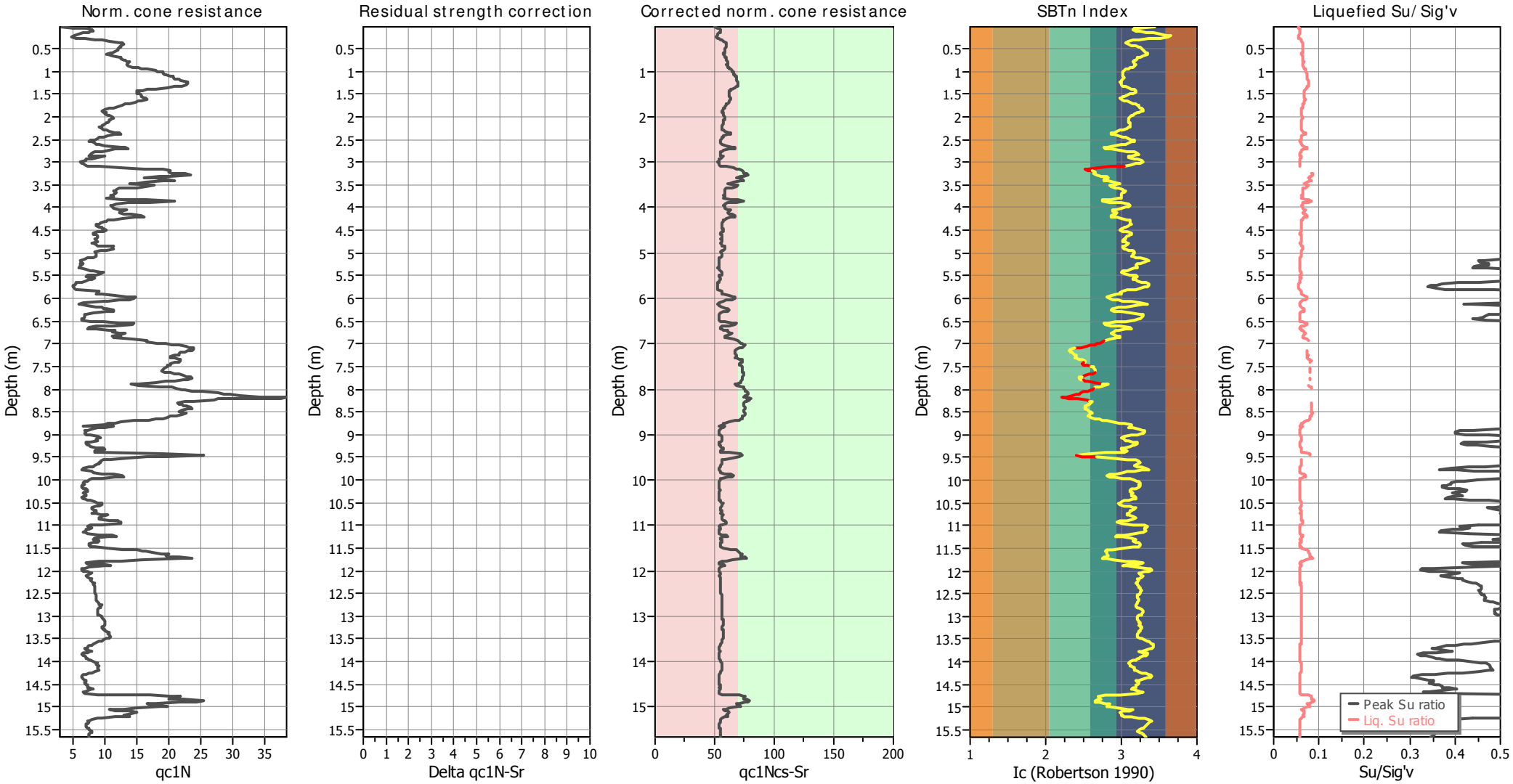
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

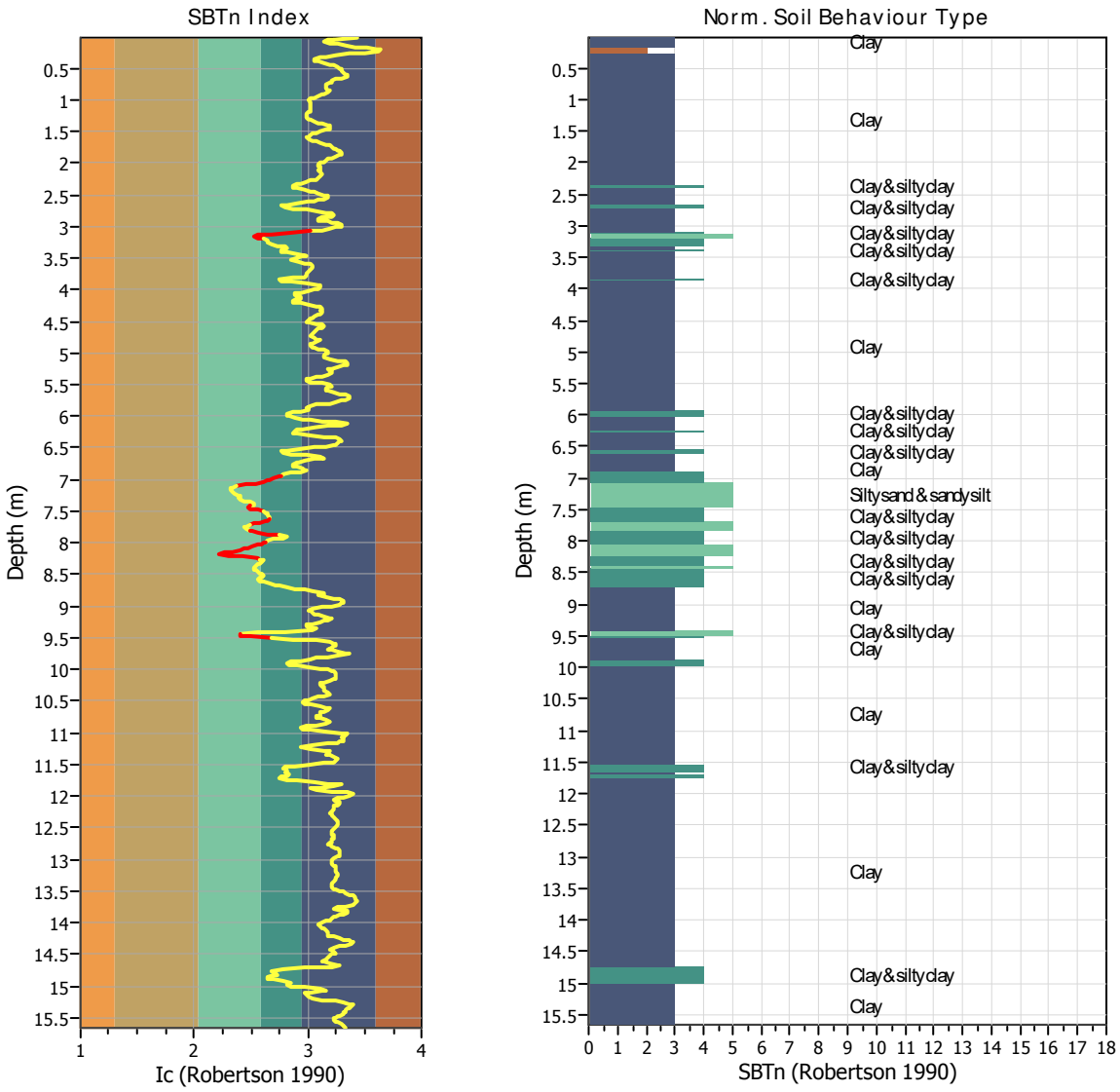
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	783
I_c maximum check value:	3.00	Total points excluded:	53
I_c change ratio value:	0.0100	Exclusion percentage:	6.77%
Minimum number of points in layer:	4	Number of layers detected:	9

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	4	Start depth: 3.10 (m)	4	Clay & silty clay
		End depth: 3.16 (m)	5	Silty sand & sandy silt
Transition layer 2	4	Start depth: 3.16 (m)	5	Silty sand & sandy silt
		End depth: 3.22 (m)	4	Clay & silty clay
Transition layer 3	9	Start depth: 6.96 (m)	4	Clay & silty clay
		End depth: 7.12 (m)	5	Silty sand & sandy silt
Transition layer 4	5	Start depth: 7.44 (m)	5	Silty sand & sandy silt
		End depth: 7.52 (m)	4	Clay & silty clay
Transition layer 5	6	Start depth: 7.64 (m)	4	Clay & silty clay
		End depth: 7.74 (m)	5	Silty sand & sandy silt
Transition layer 6	5	Start depth: 7.82 (m)	5	Silty sand & sandy silt
		End depth: 7.90 (m)	4	Clay & silty clay
Transition layer 7	10	Start depth: 8.00 (m)	4	Clay & silty clay
		End depth: 8.18 (m)	5	Silty sand & sandy silt
Transition layer 8	6	Start depth: 8.18 (m)	5	Silty sand & sandy silt
		End depth: 8.28 (m)	4	Clay & silty clay
Transition layer 9	4	Start depth: 9.46 (m)	5	Silty sand & sandy silt
		End depth: 9.52 (m)	3	Clay

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.17	8.06	-1.80	92.83	14.86
2	0.04	0.29	9.44	-1.18	74.57	15.30
3	0.06	0.41	13.48	-0.74	70.67	15.58
4	0.08	0.47	16.12	-0.37	69.04	15.95
5	0.10	0.48	21.69	-0.81	72.53	16.25
6	0.12	0.45	28.01	-1.49	77.41	16.46
7	0.14	0.44	29.74	-2.60	84.05	16.60
8	0.16	0.39	33.99	-4.28	91.28	16.68
9	0.18	0.35	38.15	-6.63	100.00	16.76
10	0.20	0.31	40.85	-49.66	100.00	16.79
11	0.22	0.30	41.73	-52.76	100.00	16.76
12	0.24	0.29	36.98	-24.05	100.00	16.67
13	0.26	0.32	31.54	-23.81	100.00	16.56
14	0.28	0.40	27.93	-23.25	86.19	16.52
15	0.30	0.50	27.70	-8.93	76.15	16.55
16	0.32	0.56	28.93	-10.17	69.72	16.65
17	0.34	0.63	31.07	-5.77	65.56	16.78
18	0.36	0.73	34.29	-16.92	62.98	16.91
19	0.38	0.76	36.93	-31.93	62.46	17.06
20	0.40	0.77	42.85	-40.17	65.02	17.22
21	0.42	0.74	50.67	-37.88	68.68	17.39
22	0.44	0.74	58.97	-43.34	72.54	17.55
23	0.46	0.73	65.71	-33.48	75.11	17.67
24	0.48	0.74	71.45	-37.76	77.52	17.77
25	0.50	0.72	75.93	-34.04	79.09	17.83
26	0.52	0.72	77.31	-28.89	80.23	17.85
27	0.54	0.71	77.16	-22.63	80.86	17.85
28	0.56	0.69	76.83	-16.18	82.19	17.83
29	0.59	0.65	75.16	-10.60	83.64	17.80
30	0.60	0.64	73.52	-8.06	85.37	17.76
31	0.62	0.61	71.93	-9.98	85.68	17.72
32	0.64	0.62	69.41	-2.79	84.48	17.70
33	0.66	0.66	68.65	-1.98	80.51	17.68
34	0.68	0.72	64.89	3.78	76.96	17.68
35	0.70	0.74	64.45	0.06	74.54	17.66
36	0.72	0.75	63.68	-6.32	73.25	17.65
37	0.74	0.77	62.21	-8.49	71.95	17.64
38	0.76	0.79	61.39	-2.54	70.55	17.63
39	0.78	0.80	60.95	-2.11	69.54	17.64
40	0.80	0.82	62.06	-3.04	69.52	17.67
41	0.82	0.81	65.77	4.22	70.31	17.71
42	0.84	0.80	68.02	10.85	71.61	17.75
43	0.86	0.80	69.66	15.19	72.05	17.78
44	0.88	0.81	70.54	21.76	71.14	17.80
45	0.90	0.85	69.83	27.96	69.22	17.82
46	0.92	0.90	70.69	17.05	67.26	17.85
47	0.94	0.93	71.60	33.60	65.20	17.87
48	0.96	0.99	71.57	33.66	62.69	17.90

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.07	71.28	24.12	60.63	17.92
50	1.00	1.08	71.28	21.76	59.14	17.95
51	1.02	1.13	75.43	23.81	59.17	18.00
52	1.04	1.13	79.59	19.96	59.50	18.08
53	1.06	1.14	84.31	20.21	60.13	18.14
54	1.08	1.17	88.20	24.55	60.24	18.20
55	1.10	1.20	91.98	27.90	60.16	18.27
56	1.12	1.23	97.51	27.09	60.22	18.32
57	1.14	1.24	100.12	24.98	60.54	18.37
58	1.16	1.24	102.93	34.10	60.43	18.40
59	1.18	1.28	103.83	46.81	59.96	18.42
60	1.20	1.29	103.30	48.48	58.70	18.44
61	1.22	1.37	104.47	36.39	58.15	18.45
62	1.25	1.35	106.78	48.17	57.75	18.48
63	1.26	1.37	109.12	56.66	57.93	18.50
64	1.28	1.37	108.58	60.94	58.06	18.50
65	1.30	1.35	108.08	47.06	58.70	18.49
66	1.32	1.31	108.57	43.34	60.19	18.48
67	1.34	1.24	109.07	39.74	62.21	18.46
68	1.36	1.17	108.01	41.97	65.05	18.43
69	1.38	1.06	106.01	49.23	67.95	18.38
70	1.40	0.99	102.99	57.97	70.58	18.32
71	1.42	0.95	98.67	76.69	72.33	18.25
72	1.44	0.89	94.63	91.57	72.80	18.18
73	1.46	0.89	88.50	108.06	72.27	18.10
74	1.48	0.89	81.31	98.02	69.81	18.00
75	1.50	0.92	71.99	81.09	66.65	17.89
76	1.52	0.94	63.61	80.60	63.64	17.76
77	1.54	0.93	58.50	73.09	61.62	17.65
78	1.56	0.93	54.22	61.07	59.84	17.57
79	1.58	0.96	50.79	65.16	58.32	17.51
80	1.60	0.97	49.47	51.21	57.29	17.50
81	1.63	0.98	51.75	42.41	58.37	17.53
82	1.64	0.94	55.99	43.52	60.70	17.60
83	1.66	0.90	60.06	30.81	63.58	17.65
84	1.68	0.88	61.41	30.56	66.56	17.68
85	1.70	0.83	63.49	-9.36	69.66	17.69
86	1.72	0.78	66.21	2.85	72.78	17.71
87	1.74	0.76	67.17	5.39	74.50	17.71
88	1.76	0.75	64.77	3.78	75.40	17.66
89	1.78	0.71	60.25	1.67	76.12	17.58
90	1.80	0.67	56.38	2.17	77.63	17.48
91	1.82	0.63	53.45	3.35	79.19	17.38
92	1.84	0.59	49.41	5.39	80.40	17.28
93	1.86	0.57	45.13	6.76	80.69	17.17
94	1.88	0.56	42.25	7.69	78.99	17.06
95	1.90	0.58	37.37	23.93	76.15	16.99
96	1.92	0.61	36.35	28.39	73.50	16.92

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	0.60	34.71	34.04	71.44	16.88
98	1.96	0.62	32.86	37.14	70.08	16.84
99	1.98	0.63	32.45	40.73	68.10	16.83
100	2.00	0.66	32.48	45.88	66.33	16.82
101	2.02	0.67	30.98	45.44	65.30	16.80
102	2.04	0.66	30.54	48.67	65.04	16.77
103	2.06	0.65	30.72	52.76	65.84	16.76
104	2.08	0.63	30.04	55.49	65.73	16.72
105	2.10	0.63	27.76	57.41	65.51	16.66
106	2.12	0.63	27.00	59.33	65.47	16.63
107	2.14	0.61	27.87	61.07	66.20	16.61
108	2.16	0.60	26.79	64.60	67.14	16.57
109	2.18	0.57	25.35	68.75	67.12	16.50
110	2.20	0.57	23.68	71.17	66.73	16.43
111	2.22	0.57	22.48	74.02	66.26	16.35
112	2.24	0.54	20.93	79.05	65.21	16.27
113	2.26	0.56	19.37	81.40	63.45	16.19
114	2.28	0.58	17.70	87.85	60.35	16.11
115	2.30	0.61	16.47	95.35	57.67	16.05
116	2.32	0.63	16.21	100.93	54.60	16.05
117	2.34	0.70	16.41	109.86	51.99	16.06
118	2.36	0.73	16.03	113.21	49.63	16.08
119	2.38	0.76	15.94	114.51	50.05	16.11
120	2.40	0.70	17.93	114.88	52.20	16.13
121	2.42	0.64	17.52	117.98	56.08	16.15
122	2.44	0.59	18.16	121.02	59.49	16.13
123	2.46	0.56	18.54	114.26	62.43	16.15
124	2.48	0.54	19.10	109.18	65.29	16.16
125	2.50	0.51	19.89	108.56	68.47	16.18
126	2.52	0.47	20.30	108.56	71.37	16.16
127	2.54	0.46	19.54	109.73	71.52	16.12
128	2.56	0.49	17.87	110.85	68.66	16.06
129	2.58	0.52	16.69	112.21	65.26	16.00
130	2.60	0.53	16.31	113.76	62.57	15.97
131	2.62	0.56	15.67	115.44	58.80	15.93
132	2.64	0.63	14.03	108.56	52.39	15.91
133	2.66	0.78	13.70	112.40	46.88	15.92
134	2.68	0.83	14.03	111.97	43.83	15.99
135	2.70	0.86	15.23	107.69	45.77	16.08
136	2.72	0.73	17.60	95.35	50.17	16.20
137	2.74	0.68	20.47	90.27	57.43	16.32
138	2.76	0.60	23.69	90.51	63.97	16.41
139	2.78	0.53	24.75	91.82	70.25	16.47
140	2.80	0.50	26.33	93.55	74.28	16.46
141	2.82	0.48	24.80	95.54	74.85	16.39
142	2.84	0.48	20.91	96.28	73.64	16.24
143	2.86	0.47	18.24	97.95	67.55	16.19
144	2.88	0.63	20.46	79.36	65.44	16.22

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	0.57	21.34	80.04	65.30	16.27
146	2.92	0.50	20.58	80.16	70.63	16.22
147	2.94	0.45	19.96	81.96	74.46	16.15
148	2.96	0.44	19.55	82.77	78.65	16.09
149	2.98	0.38	18.97	85.74	80.53	16.01
150	3.00	0.38	17.03	89.71	80.70	15.90
151	3.02	0.40	14.98	92.31	76.95	15.77
152	3.04	0.41	13.11	94.85	72.29	15.64
153	3.06	0.43	11.85	96.71	67.65	15.55
154	3.08	0.47	11.08	99.63	60.54	15.49
155	3.10	0.58	10.12	105.15	50.27	15.48
156	3.12	0.80	9.18	109.55	39.76	15.51
157	3.14	1.06	9.24	93.37	33.40	15.71
158	3.16	1.26	13.05	66.65	31.88	16.11
159	3.18	1.34	19.93	52.32	33.45	16.53
160	3.20	1.34	26.20	37.82	35.99	16.83
161	3.22	1.33	30.45	26.66	37.70	17.00
162	3.24	1.37	32.21	26.22	37.84	17.14
163	3.26	1.51	36.37	25.42	37.49	17.29
164	3.28	1.58	41.79	17.79	39.14	17.41
165	3.30	1.35	44.83	12.34	41.93	17.45
166	3.32	1.25	42.64	17.42	46.28	17.39
167	3.34	1.08	40.64	71.17	47.26	17.35
168	3.36	1.21	42.34	96.84	46.54	17.38
169	3.38	1.33	44.36	79.11	44.12	17.47
170	3.40	1.42	47.47	66.21	44.08	17.53
171	3.42	1.30	48.14	55.61	47.07	17.56
172	3.44	1.10	51.54	42.53	52.29	17.56
173	3.46	1.00	52.83	38.81	57.34	17.53
174	3.48	0.93	50.33	60.01	55.89	17.53
175	3.50	1.18	49.45	71.67	52.18	17.49
176	3.52	1.21	44.71	70.74	48.86	17.44
177	3.54	1.12	41.31	70.86	49.51	17.34
178	3.56	1.02	40.57	74.95	52.85	17.20
179	3.58	0.83	34.77	84.75	56.35	17.08
180	3.60	0.80	33.45	87.97	59.46	16.98
181	3.62	0.78	34.56	89.89	60.75	16.99
182	3.64	0.78	36.96	91.51	61.79	17.03
183	3.66	0.78	37.49	92.37	61.27	17.04
184	3.68	0.81	34.59	92.93	60.23	16.99
185	3.70	0.79	32.27	90.95	59.05	16.90
186	3.72	0.77	29.43	91.69	58.94	16.79
187	3.74	0.74	27.29	92.75	58.16	16.72
188	3.76	0.78	27.11	93.06	58.05	16.65
189	3.78	0.72	24.89	98.02	58.19	16.60
190	3.80	0.70	24.15	99.38	56.44	16.60
191	3.82	0.85	26.20	103.60	50.16	16.70
192	3.84	1.14	27.61	104.77	43.37	16.99

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	1.47	38.47	74.21	43.60	17.29
194	3.88	1.19	49.98	38.69	48.74	17.49
195	3.90	0.95	52.53	33.48	58.17	17.48
196	3.92	0.81	47.11	42.28	64.55	17.39
197	3.94	0.77	45.21	71.61	66.59	17.28
198	3.96	0.76	42.75	89.71	66.10	17.21
199	3.98	0.77	39.41	91.94	64.58	17.13
200	4.00	0.77	36.86	94.11	62.53	17.05
201	4.02	0.79	34.63	96.34	58.92	16.95
202	4.04	0.86	28.65	97.77	53.91	16.84
203	4.06	0.94	25.57	95.91	51.12	16.74
204	4.08	0.87	26.25	87.10	51.35	16.75
205	4.10	0.86	29.50	85.68	53.78	16.83
206	4.12	0.87	32.37	83.88	54.66	16.95
207	4.14	0.92	35.33	83.45	53.93	17.06
208	4.16	1.00	37.73	83.82	51.73	17.17
209	4.18	1.12	39.78	76.07	49.87	17.26
210	4.20	1.15	41.69	67.76	50.44	17.35
211	4.22	1.06	46.81	54.56	54.13	17.39
212	4.24	0.91	47.05	46.93	59.11	17.35
213	4.26	0.82	42.15	46.81	63.93	17.26
214	4.28	0.74	41.48	51.70	65.98	17.14
215	4.30	0.73	37.55	59.27	66.81	17.05
216	4.32	0.71	34.15	66.52	66.63	16.93
217	4.34	0.67	31.84	69.62	67.00	16.82
218	4.36	0.64	29.02	70.99	67.36	16.70
219	4.38	0.62	25.68	74.64	66.67	16.57
220	4.40	0.62	23.40	83.08	64.69	16.47
221	4.42	0.65	22.28	87.35	62.50	16.43
222	4.44	0.68	22.58	87.72	60.89	16.45
223	4.46	0.69	23.90	88.34	59.80	16.47
224	4.48	0.71	23.07	89.09	58.33	16.46
225	4.51	0.73	21.26	89.77	57.60	16.43
226	4.52	0.71	22.05	90.02	59.37	16.45
227	4.54	0.64	24.77	89.46	63.91	16.50
228	4.56	0.59	26.01	93.55	67.78	16.53
229	4.58	0.59	25.65	98.76	68.45	16.53
230	4.60	0.62	24.60	99.63	66.92	16.52
231	4.62	0.64	25.22	100.50	65.04	16.51
232	4.64	0.65	24.25	101.74	63.78	16.48
233	4.66	0.64	22.11	101.86	62.91	16.40
234	4.68	0.62	20.44	102.79	62.35	16.29
235	4.70	0.61	18.66	103.91	61.50	16.21
236	4.72	0.63	18.30	104.90	60.40	16.20
237	4.74	0.65	19.24	106.63	59.65	16.21
238	4.76	0.65	19.15	101.49	61.83	16.27
239	4.78	0.58	21.50	98.70	64.09	16.32
240	4.80	0.60	22.67	102.79	65.70	16.39

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	0.63	23.03	104.28	63.83	16.40
242	4.84	0.66	21.59	102.11	60.70	16.60
243	4.86	0.85	32.13	66.09	60.06	16.82
244	4.89	0.82	36.99	64.60	60.18	17.03
245	4.90	0.82	37.73	67.20	61.23	17.09
246	4.92	0.85	37.58	67.45	62.35	17.08
247	4.94	0.77	36.55	60.20	64.65	17.03
248	4.96	0.69	35.09	53.07	69.13	16.94
249	4.98	0.62	33.10	56.23	71.18	16.86
250	5.00	0.65	31.72	64.48	71.21	16.79
251	5.02	0.65	29.35	63.42	69.72	16.75
252	5.04	0.65	29.46	63.98	68.99	16.70
253	5.06	0.65	28.06	64.17	68.48	16.67
254	5.08	0.65	27.03	65.16	69.17	16.64
255	5.10	0.61	28.03	68.51	72.31	16.63
256	5.12	0.54	28.38	69.37	77.73	16.63
257	5.14	0.50	29.70	69.68	83.40	16.59
258	5.16	0.46	27.94	73.28	85.91	16.52
259	5.18	0.46	24.60	78.74	85.20	16.40
260	5.20	0.47	22.08	81.40	81.92	16.26
261	5.22	0.47	18.83	86.73	77.50	16.10
262	5.24	0.49	15.84	90.27	73.90	15.93
263	5.26	0.49	14.11	91.13	71.72	15.80
264	5.28	0.47	13.58	91.51	72.00	15.72
265	5.30	0.46	13.17	91.38	73.41	15.70
266	5.32	0.45	13.90	91.69	74.00	15.72
267	5.34	0.46	14.14	94.85	71.21	15.77
268	5.37	0.54	14.14	96.47	67.15	15.83
269	5.38	0.59	15.19	96.71	63.20	15.93
270	5.40	0.63	16.60	96.71	60.24	16.07
271	5.42	0.72	18.36	97.21	58.11	16.20
272	5.44	0.74	19.68	95.16	57.90	16.30
273	5.46	0.71	21.17	89.09	60.58	16.38
274	5.48	0.66	23.08	81.15	66.83	16.43
275	5.50	0.55	24.90	78.55	72.39	16.46
276	5.52	0.55	24.55	88.59	74.47	16.47
277	5.54	0.61	24.72	93.12	71.47	16.49
278	5.56	0.65	24.78	94.17	69.36	16.50
279	5.58	0.62	24.11	87.10	69.83	16.46
280	5.60	0.57	22.50	85.86	71.86	16.37
281	5.62	0.54	20.59	86.11	74.63	16.26
282	5.64	0.50	19.57	85.55	79.12	16.16
283	5.66	0.43	19.07	89.03	83.47	16.06
284	5.68	0.42	17.43	93.12	86.59	15.97
285	5.70	0.41	16.32	96.09	86.33	15.84
286	5.72	0.39	14.06	98.14	85.97	15.71
287	5.74	0.38	12.48	99.63	84.38	15.57
288	5.76	0.39	11.69	100.31	81.42	15.44

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	0.40	9.78	102.91	76.91	15.32
290	5.80	0.43	8.70	103.97	72.89	15.23
291	5.82	0.45	9.05	104.65	63.99	15.46
292	5.84	0.71	13.76	82.95	59.74	15.75
293	5.87	0.70	15.75	80.66	57.21	16.02
294	5.88	0.69	17.45	81.84	58.97	16.10
295	5.90	0.68	17.22	82.83	58.62	16.17
296	5.92	0.75	18.48	87.97	54.85	16.26
297	5.94	0.92	19.92	93.99	50.06	16.41
298	5.96	1.06	21.67	86.36	46.74	16.62
299	5.98	1.18	27.42	62.37	46.55	16.84
300	6.00	1.16	32.78	45.75	48.29	17.02
301	6.02	1.11	34.60	31.74	51.43	17.05
302	6.04	0.98	32.28	20.40	55.40	16.96
303	6.06	0.83	28.65	13.52	59.63	16.83
304	6.08	0.78	27.89	12.77	67.54	16.64
305	6.10	0.52	23.96	16.49	76.20	16.48
306	6.12	0.47	22.41	27.90	84.75	16.29
307	6.14	0.49	20.44	48.61	80.83	16.22
308	6.16	0.57	19.01	59.76	71.10	16.18
309	6.19	0.69	17.63	64.29	61.91	16.13
310	6.20	0.77	15.49	63.55	55.85	16.07
311	6.22	0.79	14.93	58.77	52.71	16.03
312	6.24	0.82	14.99	61.69	50.78	16.08
313	6.26	0.91	16.46	69.50	50.17	16.22
314	6.28	0.92	20.12	64.29	52.33	16.39
315	6.30	0.82	23.26	57.72	59.07	16.52
316	6.32	0.66	25.69	52.63	68.58	16.55
317	6.34	0.57	25.83	53.81	76.92	16.51
318	6.36	0.54	24.31	66.03	79.99	16.46
319	6.38	0.55	23.70	70.30	80.22	16.42
320	6.40	0.55	24.16	69.50	79.47	16.38
321	6.42	0.54	21.59	70.43	78.28	16.27
322	6.44	0.53	17.75	70.61	76.51	16.10
323	6.46	0.52	15.58	71.23	74.66	15.92
324	6.48	0.51	13.70	73.22	70.34	15.86
325	6.50	0.62	14.79	76.07	62.70	15.94
326	6.52	0.79	16.34	78.67	53.83	16.13
327	6.54	1.00	18.10	77.68	47.22	16.35
328	6.56	1.20	21.27	67.51	44.38	16.52
329	6.58	1.17	22.41	48.79	44.97	16.48
330	6.60	0.93	16.58	42.34	49.48	16.27
331	6.62	0.71	14.29	42.78	57.72	16.08
332	6.64	0.60	17.63	50.40	66.34	16.09
333	6.66	0.60	19.45	68.32	68.37	16.22
334	6.68	0.71	20.48	78.24	62.40	16.35
335	6.70	0.89	21.68	81.03	56.28	16.48
336	6.72	0.96	23.11	73.34	53.51	16.56

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	0.93	23.76	68.69	51.94	16.60
338	6.76	1.02	22.62	75.88	50.43	16.63
339	6.78	1.10	24.32	60.94	49.91	16.69
340	6.80	1.02	26.87	53.56	52.18	16.75
341	6.82	0.92	27.31	51.02	55.27	16.89
342	6.84	1.03	35.03	38.25	57.13	16.93
343	6.86	0.95	30.40	32.92	57.27	16.98
344	6.88	0.97	31.45	32.49	54.10	16.95
345	6.90	1.20	30.57	45.82	48.82	17.01
346	6.92	1.40	30.84	35.40	45.23	17.07
347	6.94	1.37	33.77	27.96	43.71	17.10
348	6.96	1.39	31.30	20.46	42.75	17.12
349	6.98	1.54	31.45	15.38	40.69	17.14
350	7.00	1.65	33.79	11.72	38.91	17.22
351	7.02	1.74	35.52	9.92	37.64	17.29
352	7.04	1.83	35.96	6.63	35.59	17.27
353	7.06	1.93	29.78	4.59	32.40	17.08
354	7.08	1.98	19.35	4.22	28.67	16.77
355	7.10	2.03	14.90	4.40	25.47	16.40
356	7.12	2.03	11.91	4.53	23.80	16.16
357	7.14	2.01	10.73	4.28	23.16	16.01
358	7.16	1.96	10.32	4.03	23.31	15.95
359	7.18	1.91	10.38	3.97	23.70	15.90
360	7.20	1.86	9.74	3.97	24.20	15.90
361	7.22	1.85	10.56	4.03	24.90	15.96
362	7.24	1.84	12.11	3.66	25.84	16.05
363	7.26	1.79	12.49	2.98	26.52	16.06
364	7.28	1.74	11.26	2.11	26.53	15.98
365	7.30	1.73	9.82	2.67	26.10	15.91
366	7.32	1.79	10.59	4.34	26.45	16.06
367	7.34	1.86	15.30	3.16	28.10	16.40
368	7.36	1.88	21.57	0.68	30.20	16.73
369	7.38	1.89	25.79	-2.23	31.50	16.87
370	7.40	1.87	23.98	-4.77	31.51	16.82
371	7.42	1.80	18.61	-11.10	30.33	16.59
372	7.44	1.75	13.72	-11.53	29.44	16.38
373	7.46	1.74	15.13	-12.52	30.62	16.46
374	7.48	1.71	22.28	-14.01	33.17	16.73
375	7.50	1.71	27.11	-15.25	35.60	16.96
376	7.52	1.71	29.60	-16.37	36.75	17.05
377	7.54	1.69	29.08	-29.94	37.33	17.07
378	7.56	1.66	28.75	-28.77	37.63	17.06
379	7.58	1.66	29.10	-29.14	38.09	17.07
380	7.60	1.65	30.54	-29.82	38.48	17.12
381	7.62	1.69	32.65	-30.38	38.50	17.19
382	7.64	1.77	34.20	-31.00	37.84	17.25
383	7.66	1.84	34.14	-31.43	36.35	17.23
384	7.68	1.90	30.04	-31.87	34.16	17.13

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	1.95	24.56	-32.36	31.98	16.99
386	7.72	2.00	23.62	-32.80	29.97	16.85
387	7.74	2.05	20.49	-33.23	28.54	16.75
388	7.76	2.08	18.29	-33.60	28.22	16.72
389	7.78	2.02	21.90	-34.10	29.16	16.78
390	7.80	1.97	24.21	-34.72	30.51	16.79
391	7.82	1.84	19.71	-47.49	31.38	16.70
392	7.84	1.73	17.80	-48.79	33.25	16.65
393	7.86	1.59	22.96	-49.78	37.75	16.75
394	7.88	1.34	27.38	-50.28	43.47	16.88
395	7.90	1.24	29.05	-50.46	47.11	16.97
396	7.92	1.35	31.49	-48.23	44.67	17.04
397	7.94	1.65	30.08	-47.37	40.72	17.14
398	7.96	1.82	32.89	-47.37	37.69	17.22
399	7.98	1.89	35.12	-47.43	36.60	17.31
400	8.00	1.97	35.94	-47.49	35.92	17.35
401	8.02	2.01	35.91	-47.61	34.72	17.36
402	8.04	2.12	34.50	-47.55	33.08	17.35
403	8.06	2.25	33.30	-47.43	31.03	17.37
404	8.08	2.48	35.56	-47.12	29.41	17.42
405	8.10	2.58	36.29	-47.06	28.22	17.47
406	8.12	2.67	36.08	-46.99	26.76	17.44
407	8.14	2.80	31.04	-46.81	24.22	17.34
408	8.16	3.10	25.54	-46.00	21.12	17.22
409	8.18	3.48	25.01	-45.01	19.70	17.23
410	8.20	3.40	29.75	-45.13	22.89	17.47
411	8.22	2.51	46.16	-43.65	27.38	17.62
412	8.24	2.44	43.79	-34.66	33.05	17.68
413	8.26	2.16	43.58	-17.48	34.41	17.59
414	8.28	2.03	38.16	-10.66	35.73	17.45
415	8.30	1.93	32.42	-7.94	35.29	17.29
416	8.32	1.96	30.45	-8.25	34.47	17.19
417	8.34	2.00	29.43	-18.60	33.49	17.13
418	8.36	2.02	27.50	-44.82	32.66	17.10
419	8.38	2.07	27.52	-46.25	31.90	17.08
420	8.40	2.12	27.82	-46.81	31.64	17.12
421	8.42	2.14	29.75	-47.06	31.76	17.15
422	8.44	2.10	29.40	-47.43	32.45	17.15
423	8.46	2.01	28.84	-47.74	33.26	17.14
424	8.48	1.97	29.34	-47.86	34.34	17.17
425	8.50	1.97	32.53	-47.99	35.20	17.28
426	8.52	2.05	37.48	-47.99	35.67	17.38
427	8.54	2.08	38.27	-48.11	35.28	17.38
428	8.56	2.03	31.39	-48.23	34.55	17.24
429	8.58	1.94	25.91	-48.42	33.60	17.00
430	8.60	1.86	21.57	-48.61	33.89	16.89
431	8.62	1.81	25.17	-48.79	35.57	16.94
432	8.64	1.75	29.95	-48.92	38.38	17.08

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	1.66	32.44	-49.23	40.87	17.12
434	8.68	1.55	29.95	-49.60	43.36	17.03
435	8.70	1.34	25.76	-49.91	46.90	16.91
436	8.72	1.15	26.49	-50.03	51.64	16.81
437	8.74	1.05	26.70	-50.03	56.85	16.77
438	8.76	0.96	26.08	-49.78	60.67	16.76
439	8.78	0.93	27.61	-49.54	68.52	16.67
440	8.80	0.60	24.82	64.85	67.93	16.75
441	8.82	1.04	30.91	-13.95	68.34	16.78
442	8.84	0.92	29.57	3.35	64.78	16.84
443	8.86	0.82	27.19	8.37	69.80	16.74
444	8.88	0.74	26.22	12.59	75.12	16.64
445	8.90	0.66	25.58	21.76	79.76	16.56
446	8.92	0.63	24.12	28.02	81.98	16.48
447	8.94	0.64	22.47	28.08	81.87	16.41
448	8.96	0.63	21.68	27.84	80.78	16.34
449	8.98	0.63	19.87	29.20	79.05	16.25
450	9.00	0.65	17.64	29.88	74.45	16.15
451	9.02	0.72	15.88	31.43	67.41	16.06
452	9.04	0.82	14.53	35.34	61.37	16.04
453	9.06	0.87	15.15	33.23	59.08	16.09
454	9.08	0.86	17.14	30.63	59.81	16.13
455	9.10	0.81	16.35	33.91	61.19	16.12
456	9.12	0.80	15.12	35.59	62.02	16.12
457	9.14	0.82	17.43	34.28	64.61	16.13
458	9.16	0.71	17.23	36.83	68.89	16.13
459	9.18	0.65	16.38	41.48	73.20	16.07
460	9.20	0.65	16.12	42.03	73.69	16.04
461	9.22	0.68	16.12	45.38	71.45	16.01
462	9.24	0.70	14.98	44.95	69.17	16.02
463	9.26	0.73	15.77	44.64	66.08	16.05
464	9.28	0.81	16.50	46.25	61.68	16.12
465	9.30	0.92	16.29	47.80	58.28	16.19
466	9.32	0.94	17.64	45.38	58.26	16.26
467	9.34	0.86	19.31	41.60	61.43	16.28
468	9.36	0.78	17.82	44.89	64.10	16.22
469	9.38	0.79	16.12	47.55	61.47	16.11
470	9.40	0.91	14.19	51.70	45.62	16.21
471	9.42	1.82	16.50	63.98	33.32	16.39
472	9.44	2.38	17.53	52.94	26.94	16.59
473	9.46	2.43	18.76	46.31	26.72	16.57
474	9.48	1.85	15.57	32.92	30.03	16.50
475	9.50	1.58	16.59	29.51	38.99	16.66
476	9.52	1.27	30.51	25.05	50.47	16.97
477	9.54	1.05	40.41	29.70	63.14	17.19
478	9.56	0.92	41.70	51.64	71.89	17.27
479	9.58	0.88	43.20	60.07	75.57	17.26
480	9.60	0.88	42.26	61.31	76.71	17.25

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	0.86	40.97	62.49	76.23	17.19
482	9.64	0.86	37.19	65.22	74.62	17.06
483	9.66	0.85	30.04	65.59	73.24	16.88
484	9.68	0.79	25.88	66.21	71.62	16.64
485	9.70	0.77	20.78	61.38	73.59	16.51
486	9.72	0.70	23.07	60.07	78.18	16.49
487	9.74	0.64	26.52	63.05	83.80	16.52
488	9.76	0.63	24.24	67.89	86.54	16.48
489	9.78	0.61	21.54	72.97	78.16	16.32
490	9.80	0.76	15.63	221.14	70.92	16.17
491	9.82	0.75	15.55	217.30	63.98	16.06
492	9.84	0.79	15.52	231.31	59.95	16.06
493	9.86	0.92	14.26	248.42	53.87	16.08
494	9.88	1.09	14.76	232.67	48.64	16.19
495	9.91	1.24	17.77	150.28	46.63	16.34
496	9.92	1.24	19.15	126.91	48.15	16.47
497	9.94	1.13	21.20	64.23	52.42	16.47
498	9.96	0.93	19.15	67.33	59.23	16.40
499	9.98	0.78	18.42	130.32	66.04	16.28
500	10.00	0.71	18.21	161.62	70.79	16.22
501	10.03	0.69	17.83	177.68	73.60	16.19
502	10.04	0.66	18.04	177.43	75.44	16.18
503	10.06	0.65	18.16	181.77	77.03	16.18
504	10.08	0.65	18.30	190.33	76.63	16.15
505	10.10	0.66	16.63	195.35	75.98	16.09
506	10.12	0.65	15.70	153.94	76.07	16.04
507	10.14	0.62	16.14	170.55	76.75	15.99
508	10.16	0.62	14.88	195.10	75.84	15.94
509	10.18	0.64	13.56	216.74	72.56	15.85
510	10.20	0.67	12.62	224.67	68.43	15.79
511	10.22	0.72	12.01	221.64	66.22	15.76
512	10.24	0.70	12.39	227.71	66.23	15.74
513	10.26	0.66	11.95	220.27	67.78	15.72
514	10.28	0.65	11.65	221.76	69.25	15.70
515	10.30	0.65	12.21	227.53	68.63	15.72
516	10.32	0.69	12.18	235.28	68.00	15.76
517	10.34	0.69	12.83	239.43	68.03	15.81
518	10.36	0.67	13.77	233.42	70.63	15.86
519	10.38	0.63	14.18	224.36	72.59	15.86
520	10.40	0.63	13.09	232.80	72.33	15.80
521	10.42	0.66	12.04	242.65	68.78	15.74
522	10.44	0.71	11.42	245.13	64.69	15.72
523	10.46	0.77	11.89	258.03	61.07	15.76
524	10.48	0.82	12.33	255.61	58.65	15.85
525	10.50	0.88	13.71	248.30	56.57	15.98
526	10.52	0.95	15.20	272.97	55.58	16.07
527	10.54	0.95	15.20	223.99	56.80	16.18
528	10.56	0.90	17.87	171.11	60.58	16.28

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	0.84	20.54	181.46	65.98	16.40
530	10.60	0.79	22.30	191.94	69.89	16.48
531	10.62	0.78	23.20	199.19	72.06	16.53
532	10.64	0.78	23.76	220.77	70.77	16.52
533	10.66	0.83	21.53	229.88	68.54	16.51
534	10.68	0.87	22.06	237.45	66.05	16.46
535	10.70	0.86	19.86	215.56	66.37	16.40
536	10.72	0.80	18.90	147.12	65.73	16.32
537	10.74	0.85	18.14	211.59	63.40	16.29
538	10.76	0.94	17.81	246.75	63.41	16.60
539	10.78	1.04	34.17	26.04	65.60	16.85
540	10.80	0.96	34.23	73.71	69.56	17.04
541	10.82	0.93	33.94	88.10	72.22	17.04
542	10.84	0.90	34.96	110.23	73.06	17.02
543	10.86	0.90	33.21	120.21	70.07	17.03
544	10.88	1.06	33.03	160.76	63.18	16.98
545	10.90	1.20	27.35	155.42	57.39	16.91
546	10.92	1.22	25.15	7.07	54.77	16.88
547	10.94	1.25	30.04	44.14	54.93	16.90
548	10.96	1.24	28.40	-8.18	60.03	16.97
549	10.98	0.95	32.79	-18.16	68.74	16.96
550	11.00	0.77	33.91	-5.64	81.11	16.94
551	11.02	0.73	33.26	54.93	85.75	16.92
552	11.04	0.77	32.62	71.61	83.52	16.87
553	11.06	0.80	29.72	80.66	81.18	16.82
554	11.08	0.77	28.37	83.38	81.64	16.73
555	11.10	0.71	26.75	85.00	82.33	16.60
556	11.12	0.71	21.63	88.28	82.63	16.43
557	11.14	0.67	18.70	91.94	80.11	16.26
558	11.16	0.69	17.35	98.45	77.75	16.17
559	11.18	0.73	17.17	108.62	70.58	16.19
560	11.20	0.91	17.87	128.08	61.41	16.28
561	11.22	1.13	18.37	146.19	54.44	16.39
562	11.24	1.21	19.66	147.49	54.03	16.51
563	11.26	1.05	22.88	73.90	60.21	16.62
564	11.28	0.86	26.84	75.51	68.59	16.68
565	11.30	0.84	26.11	100.93	72.55	16.71
566	11.32	0.90	26.52	116.31	70.83	16.72
567	11.34	0.93	26.84	121.20	70.09	16.77
568	11.36	0.90	28.51	121.45	72.32	16.80
569	11.38	0.83	29.42	118.29	75.87	16.75
570	11.40	0.76	25.37	118.54	77.35	16.65
571	11.42	0.78	22.65	129.32	77.39	16.55
572	11.44	0.77	23.50	131.25	76.64	16.55
573	11.46	0.79	24.88	136.45	75.56	16.61
574	11.48	0.86	25.81	145.63	69.23	16.68
575	11.50	1.06	25.29	168.32	59.79	16.73
576	11.52	1.31	24.11	194.30	50.71	16.76

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	1.54	23.03	119.22	45.97	16.86
578	11.56	1.65	28.63	26.91	45.13	17.06
579	11.58	1.69	36.10	9.98	46.02	17.31
580	11.60	1.81	42.31	6.82	46.50	17.54
581	11.62	1.95	49.81	7.25	46.12	17.73
582	11.64	2.06	55.87	8.00	46.72	17.89
583	11.66	2.03	63.35	5.27	47.68	18.01
584	11.68	2.04	66.92	1.61	46.87	18.04
585	11.70	2.24	59.48	2.98	44.39	18.06
586	11.72	2.44	62.35	6.88	43.06	18.07
587	11.74	2.28	66.19	1.30	46.66	18.03
588	11.76	1.62	59.09	-11.72	52.50	17.78
589	11.78	1.29	36.01	29.63	62.44	17.40
590	11.80	0.94	33.08	30.87	70.79	16.97
591	11.82	0.74	26.81	60.32	80.20	16.75
592	11.84	0.76	24.44	69.00	75.55	16.63
593	11.86	1.02	23.70	75.64	65.55	16.60
594	11.88	1.14	21.30	74.02	59.86	16.56
595	11.90	1.04	20.36	63.92	63.96	16.54
596	11.93	0.79	24.32	63.24	73.72	16.54
597	11.94	0.71	24.29	67.76	85.27	16.53
598	11.96	0.66	23.70	72.16	89.12	16.50
599	11.98	0.67	23.73	75.14	90.11	16.50
600	12.00	0.69	24.76	77.00	87.18	16.55
601	12.02	0.75	25.61	79.42	82.22	16.56
602	12.04	0.82	22.76	80.29	77.45	16.53
603	12.06	0.83	21.36	81.28	75.13	16.43
604	12.08	0.78	19.72	79.67	76.40	16.36
605	12.10	0.73	19.51	80.60	78.84	16.34
606	12.12	0.74	20.92	83.01	79.72	16.36
607	12.14	0.77	21.09	84.19	77.82	16.40
608	12.16	0.82	21.15	84.87	75.60	16.43
609	12.18	0.83	21.39	85.49	74.64	16.45
610	12.20	0.82	21.97	85.93	75.14	16.48
611	12.22	0.82	22.73	86.11	75.25	16.49
612	12.24	0.84	22.21	87.35	74.26	16.50
613	12.26	0.86	22.24	87.97	73.03	16.53
614	12.28	0.89	23.73	87.85	73.26	16.60
615	12.30	0.87	26.19	87.41	74.14	16.69
616	12.32	0.89	27.98	88.16	75.27	16.78
617	12.34	0.90	29.30	88.78	75.69	16.83
618	12.36	0.90	30.06	89.21	76.10	16.87
619	12.38	0.90	30.73	89.77	76.77	16.91
620	12.40	0.90	32.38	89.77	77.64	16.94
621	12.42	0.89	32.93	89.77	78.26	16.96
622	12.44	0.89	32.17	90.58	78.13	16.95
623	12.46	0.90	31.50	91.13	77.37	16.92
624	12.48	0.90	30.82	91.20	76.79	16.90

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
625	12.50	0.90	29.94	92.06	76.20	16.87
626	12.52	0.91	29.47	92.81	75.39	16.84
627	12.54	0.92	28.27	93.37	74.54	16.82
628	12.56	0.92	28.16	93.43	74.08	16.81
629	12.58	0.92	28.27	93.80	74.12	16.82
630	12.60	0.93	29.06	94.48	74.21	16.84
631	12.62	0.93	29.42	94.11	74.78	16.86
632	12.64	0.91	30.15	94.54	75.08	16.88
633	12.66	0.93	30.38	95.41	75.18	16.90
634	12.68	0.95	31.26	96.59	74.42	16.92
635	12.70	0.96	30.67	97.33	73.81	16.93
636	12.72	0.97	31.29	97.83	73.34	16.95
637	12.74	0.98	32.49	98.14	72.15	16.99
638	12.76	1.02	32.65	196.71	71.70	17.03
639	12.78	1.01	34.50	191.13	71.96	17.08
640	12.80	0.99	36.25	187.85	74.03	17.14
641	12.82	0.98	38.63	184.87	76.11	17.19
642	12.84	0.96	40.33	182.39	77.78	17.23
643	12.86	0.96	41.35	181.09	79.17	17.27
644	12.88	0.95	42.64	182.33	79.35	17.28
645	12.91	0.97	41.91	185.80	79.39	17.29
646	12.93	0.96	41.41	185.24	78.98	17.27
647	12.95	0.96	41.32	186.36	78.85	17.26
648	12.96	0.97	40.85	190.95	78.01	17.25
649	12.98	0.98	39.30	196.03	75.88	17.22
650	13.00	1.03	37.36	198.45	73.93	17.20
651	13.02	1.05	38.39	197.27	73.27	17.24
652	13.04	1.04	41.70	196.90	73.67	17.29
653	13.06	1.05	42.28	195.66	74.15	17.34
654	13.08	1.07	43.69	196.59	74.30	17.38
655	13.10	1.08	46.41	197.15	75.09	17.45
656	13.12	1.08	50.34	196.53	75.99	17.52
657	13.14	1.09	51.42	197.64	76.58	17.55
658	13.16	1.08	50.45	199.07	76.24	17.54
659	13.19	1.09	49.28	201.05	76.02	17.52
660	13.20	1.08	48.96	200.50	76.28	17.52
661	13.22	1.07	50.25	197.77	77.42	17.52
662	13.24	1.04	49.95	197.21	78.32	17.52
663	13.26	1.04	49.31	197.64	78.21	17.51
664	13.28	1.06	49.13	201.67	77.02	17.51
665	13.30	1.10	49.51	203.04	76.66	17.54
666	13.32	1.09	52.18	202.48	76.58	17.58
667	13.34	1.10	53.49	207.69	75.71	17.60
668	13.36	1.17	51.24	211.53	74.72	17.61
669	13.38	1.16	53.32	210.66	73.78	17.63
670	13.40	1.17	54.69	209.24	74.25	17.67
671	13.42	1.19	56.89	210.35	74.15	17.71
672	13.44	1.20	57.94	208.18	74.30	17.73

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
673	13.46	1.20	58.27	205.58	74.63	17.75
674	13.48	1.19	58.82	201.49	76.25	17.76
675	13.50	1.14	61.52	189.83	78.94	17.78
676	13.52	1.08	62.63	180.97	81.97	17.78
677	13.54	1.05	61.60	174.52	84.44	17.76
678	13.56	1.01	60.75	168.32	86.67	17.72
679	13.58	0.96	59.08	163.48	89.05	17.68
680	13.60	0.92	57.00	163.92	90.66	17.60
681	13.62	0.90	51.81	163.55	91.25	17.52
682	13.64	0.88	48.77	161.13	91.89	17.41
683	13.66	0.82	44.05	161.56	92.22	17.29
684	13.68	0.81	39.21	163.79	91.60	17.15
685	13.70	0.81	34.70	169.13	90.65	17.01
686	13.72	0.77	31.71	169.62	89.14	16.88
687	13.74	0.78	27.87	174.71	83.08	16.73
688	13.76	0.89	22.06	293.43	77.90	16.60
689	13.78	0.86	22.12	245.13	75.60	16.50
690	13.81	0.82	21.68	126.35	80.35	16.48
691	13.82	0.73	22.56	184.07	84.46	16.44
692	13.84	0.72	20.86	194.30	85.41	16.37
693	13.86	0.74	18.55	208.74	82.81	16.28
694	13.88	0.76	17.81	219.65	79.35	16.23
695	13.90	0.79	17.43	225.73	77.13	16.19
696	13.92	0.79	16.56	232.80	75.42	16.17
697	13.94	0.81	16.50	239.43	74.17	16.17
698	13.96	0.83	17.17	247.12	72.26	16.19
699	13.98	0.87	16.82	260.57	69.73	16.22
700	14.00	0.92	17.14	270.06	67.05	16.25
701	14.02	0.97	17.79	277.68	65.36	16.31
702	14.04	0.99	18.87	280.04	65.31	16.39
703	14.06	0.98	20.57	276.88	66.00	16.49
704	14.08	1.00	22.42	281.77	66.79	16.57
705	14.10	1.01	23.33	280.78	68.04	16.67
706	14.13	1.00	26.43	265.03	69.38	16.75
707	14.14	1.01	27.99	269.62	70.98	16.85
708	14.16	1.01	29.89	271.11	70.96	16.88
709	14.18	1.03	28.49	278.18	70.72	16.89
710	14.20	1.03	28.54	275.88	71.69	16.89
711	14.22	0.96	30.07	258.65	74.67	16.90
712	14.24	0.91	30.92	248.61	79.04	16.91
713	14.26	0.86	31.15	238.81	82.88	16.89
714	14.28	0.81	30.04	239.55	86.11	16.82
715	14.30	0.76	26.82	235.65	88.73	16.71
716	14.32	0.72	24.79	237.51	89.82	16.58
717	14.34	0.71	22.51	242.03	88.10	16.45
718	14.36	0.73	18.79	253.25	84.29	16.30
719	14.38	0.75	16.56	262.80	79.35	16.15
720	14.40	0.79	14.98	270.37	75.32	16.05

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
721	14.42	0.81	14.01	277.62	72.89	16.00
722	14.44	0.81	14.39	279.54	73.23	16.01
723	14.46	0.78	15.39	278.55	75.07	16.08
724	14.48	0.78	16.77	277.99	76.05	16.11
725	14.50	0.80	15.86	284.93	74.49	16.13
726	14.52	0.84	15.71	297.02	72.75	16.12
727	14.54	0.84	15.89	296.84	71.88	16.11
728	14.56	0.83	15.24	296.78	71.72	16.11
729	14.58	0.86	15.89	297.40	69.75	16.12
730	14.60	0.93	15.68	311.78	67.96	16.13
731	14.62	0.91	15.10	308.62	69.22	16.17
732	14.64	0.83	17.65	286.48	73.20	16.19
733	14.66	0.79	17.68	282.89	78.21	16.24
734	14.68	0.76	18.03	279.98	79.59	16.24
735	14.70	0.79	18.29	288.59	73.45	16.29
736	14.72	1.02	18.23	341.17	56.78	16.62
737	14.74	1.96	28.30	58.96	45.45	16.98
738	14.76	2.32	33.04	-5.08	39.84	17.37
739	14.78	2.51	42.01	-11.28	39.81	17.55
740	14.80	2.31	43.06	-9.11	41.54	17.68
741	14.82	2.29	47.52	-2.17	42.26	17.76
742	14.84	2.56	52.00	43.52	40.10	17.87
743	14.86	2.91	52.62	88.84	38.02	17.92
744	14.88	2.80	50.18	94.48	37.75	17.86
745	14.90	2.48	44.76	92.50	40.64	17.73
746	14.92	2.08	42.50	88.22	45.18	17.65
747	14.94	1.92	46.37	90.02	49.00	17.67
748	14.96	2.00	50.74	112.96	47.95	17.70
749	14.98	2.27	44.49	75.39	46.67	17.73
750	15.00	2.15	48.07	65.34	49.27	17.76
751	15.02	1.73	57.30	56.11	56.31	17.80
752	15.04	1.51	56.09	55.86	65.73	17.76
753	15.06	1.25	51.87	75.76	69.59	17.67
754	15.08	1.34	49.50	122.19	66.77	17.60
755	15.10	1.61	45.16	134.66	60.04	17.57
756	15.12	1.74	43.43	106.39	57.02	17.58
757	15.14	1.64	48.23	86.61	58.07	17.57
758	15.17	1.51	45.24	109.67	59.43	17.55
759	15.18	1.58	41.52	126.29	59.03	17.50
760	15.20	1.61	42.60	102.67	61.41	17.53
761	15.22	1.36	50.92	94.73	67.68	17.53
762	15.24	1.12	46.15	118.72	76.07	17.48
763	15.26	1.05	43.22	131.87	82.25	17.34
764	15.28	0.93	39.41	139.31	86.48	17.23
765	15.30	0.87	37.85	128.08	89.61	17.10
766	15.32	0.86	33.25	133.11	88.89	16.98
767	15.34	0.88	28.62	134.66	86.43	16.83
768	15.36	0.86	25.87	133.97	84.67	16.70

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
769	15.38	0.84	23.99	135.09	84.19	16.59
770	15.40	0.84	22.20	136.76	83.47	16.50
771	15.42	0.83	20.53	136.64	82.61	16.44
772	15.44	0.84	20.74	138.25	81.58	16.40
773	15.46	0.85	19.77	140.30	80.02	16.39
774	15.48	0.88	19.51	141.54	78.23	16.38
775	15.50	0.90	19.94	142.16	75.98	16.39
776	15.52	0.94	19.68	143.89	74.78	16.42
777	15.54	0.94	20.41	143.77	74.65	16.45
778	15.56	0.93	21.62	143.27	76.25	16.49
779	15.58	0.90	22.09	143.40	78.70	16.54
780	15.60	0.88	23.81	144.08	80.50	16.60
781	15.62	0.90	25.40	145.32	81.81	16.66
782	15.64	0.89	25.60	146.37	82.14	16.68
783	15.66	0.88	25.90	146.87	83.19	16.69

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.30	0.00	0.30	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
2	0.04	0.60	0.00	0.60	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
3	0.06	0.91	0.00	0.91	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
4	0.08	1.23	0.00	1.23	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
5	0.10	1.56	0.00	1.56	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
6	0.12	1.89	0.00	1.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
7	0.14	2.22	0.00	2.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
8	0.16	2.55	0.00	2.55	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
9	0.18	2.89	0.00	2.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
10	0.20	3.22	0.00	3.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
11	0.22	3.56	0.00	3.56	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
12	0.24	3.89	0.00	3.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
13	0.26	4.22	0.00	4.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
14	0.28	4.55	0.00	4.55	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
15	0.30	4.89	0.00	4.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
16	0.32	5.22	0.00	5.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
17	0.34	5.55	0.00	5.55	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
18	0.36	5.89	0.00	5.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
19	0.38	6.23	0.00	6.23	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
20	0.40	6.58	0.00	6.58	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
21	0.42	6.93	0.00	6.93	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
22	0.44	7.28	0.00	7.28	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
23	0.46	7.63	0.00	7.63	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
24	0.48	7.99	0.00	7.99	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
25	0.50	8.34	0.00	8.34	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
26	0.52	8.70	0.00	8.70	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
27	0.54	9.06	0.00	9.06	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
28	0.56	9.41	0.00	9.41	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
29	0.59	9.95	0.00	9.95	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
30	0.60	10.12	0.00	10.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
31	0.62	10.48	0.00	10.48	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
32	0.64	10.83	0.00	10.83	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
33	0.66	11.19	0.00	11.19	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
34	0.68	11.54	0.00	11.54	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
35	0.70	11.89	0.00	11.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
36	0.72	12.25	0.00	12.25	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
37	0.74	12.60	0.00	12.60	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
38	0.76	12.95	0.00	12.95	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
39	0.78	13.30	0.00	13.30	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
40	0.80	13.66	0.00	13.66	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
41	0.82	14.01	0.00	14.01	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
42	0.84	14.37	0.00	14.37	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
43	0.86	14.72	0.00	14.72	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
44	0.88	15.08	0.00	15.08	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
45	0.90	15.44	0.00	15.44	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
46	0.92	15.79	0.00	15.79	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
47	0.94	16.15	0.00	16.15	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
48	0.96	16.51	0.00	16.51	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	16.87	0.00	16.87	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
50	1.00	17.23	0.00	17.23	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
51	1.02	17.59	0.00	17.59	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
52	1.04	17.95	0.00	17.95	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
53	1.06	18.31	0.00	18.31	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
54	1.08	18.67	0.00	18.67	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
55	1.10	19.04	0.00	19.04	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
56	1.12	19.41	0.00	19.41	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
57	1.14	19.77	0.00	19.77	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
58	1.16	20.14	0.00	20.14	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
59	1.18	20.51	0.00	20.51	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
60	1.20	20.88	0.00	20.88	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
61	1.22	21.25	0.00	21.25	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
62	1.25	21.80	0.00	21.80	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
63	1.26	21.99	0.00	21.99	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
64	1.28	22.36	0.00	22.36	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
65	1.30	22.73	0.00	22.73	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
66	1.32	23.10	0.00	23.10	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
67	1.34	23.47	0.00	23.47	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
68	1.36	23.83	0.00	23.83	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
69	1.38	24.20	0.00	24.20	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
70	1.40	24.57	0.00	24.57	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
71	1.42	24.93	0.00	24.93	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
72	1.44	25.30	0.00	25.30	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
73	1.46	25.66	0.00	25.66	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
74	1.48	26.02	0.00	26.02	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
75	1.50	26.38	0.00	26.38	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
76	1.52	26.73	0.00	26.73	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
77	1.54	27.08	0.00	27.08	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
78	1.56	27.44	0.00	27.44	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
79	1.58	27.79	0.00	27.79	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
80	1.60	28.14	0.00	28.14	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
81	1.63	28.66	0.00	28.66	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
82	1.64	28.84	0.00	28.84	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
83	1.66	29.19	0.00	29.19	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
84	1.68	29.54	0.00	29.54	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
85	1.70	29.90	0.00	29.90	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
86	1.72	30.25	0.00	30.25	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
87	1.74	30.61	0.00	30.61	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
88	1.76	30.96	0.00	30.96	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
89	1.78	31.31	0.00	31.31	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
90	1.80	31.66	0.00	31.66	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
91	1.82	32.01	0.00	32.01	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
92	1.84	32.35	0.00	32.35	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
93	1.86	32.70	0.00	32.70	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
94	1.88	33.04	0.00	33.04	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
95	1.90	33.38	0.00	33.38	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
96	1.92	33.72	0.00	33.72	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	34.05	0.00	34.05	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
98	1.96	34.39	0.00	34.39	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
99	1.98	34.73	0.00	34.73	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
100	2.00	35.06	0.00	35.06	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
101	2.02	35.40	0.20	35.20	0.98	0.141	1.43	0.098	1.09	1.00	0.120	No
102	2.04	35.74	0.39	35.34	0.98	0.141	1.43	0.099	1.09	1.00	0.121	No
103	2.06	36.07	0.59	35.48	0.98	0.142	1.43	0.100	1.09	1.00	0.121	No
104	2.08	36.41	0.78	35.62	0.98	0.143	1.43	0.100	1.09	1.00	0.122	No
105	2.10	36.74	0.98	35.76	0.98	0.144	1.43	0.100	1.09	1.00	0.123	No
106	2.12	37.07	1.18	35.89	0.98	0.144	1.43	0.101	1.09	1.00	0.123	No
107	2.14	37.40	1.37	36.03	0.98	0.145	1.43	0.101	1.08	1.00	0.124	No
108	2.16	37.73	1.57	36.16	0.98	0.146	1.43	0.102	1.08	1.00	0.125	No
109	2.18	38.06	1.77	36.30	0.98	0.146	1.43	0.102	1.08	1.00	0.126	No
110	2.20	38.39	1.96	36.43	0.98	0.147	1.43	0.103	1.08	1.00	0.126	No
111	2.22	38.72	2.16	36.56	0.98	0.148	1.43	0.103	1.08	1.00	0.127	No
112	2.24	39.05	2.35	36.69	0.97	0.148	1.43	0.104	1.08	1.00	0.128	No
113	2.26	39.37	2.55	36.82	0.97	0.149	1.43	0.104	1.08	1.00	0.128	No
114	2.28	39.69	2.75	36.94	0.97	0.150	1.43	0.105	1.08	1.00	0.129	No
115	2.30	40.01	2.94	37.07	0.97	0.150	1.43	0.105	1.08	1.00	0.129	No
116	2.32	40.33	3.14	37.19	0.97	0.151	1.43	0.106	1.08	1.00	0.130	No
117	2.34	40.65	3.34	37.32	0.97	0.152	1.43	0.106	1.08	1.00	0.130	No
118	2.36	40.98	3.53	37.44	0.97	0.152	1.43	0.107	1.08	1.00	0.130	No
119	2.38	41.30	3.73	37.57	0.97	0.153	1.43	0.107	1.08	1.00	0.131	No
120	2.40	41.62	3.92	37.70	0.97	0.153	1.43	0.107	1.08	1.00	0.132	No
121	2.42	41.94	4.12	37.82	0.97	0.154	1.43	0.108	1.08	1.00	0.132	No
122	2.44	42.27	4.32	37.95	0.97	0.155	1.43	0.108	1.08	1.00	0.133	No
123	2.46	42.59	4.51	38.08	0.97	0.155	1.43	0.109	1.08	1.00	0.134	No
124	2.48	42.91	4.71	38.20	0.97	0.156	1.43	0.109	1.08	1.00	0.135	No
125	2.50	43.24	4.91	38.33	0.97	0.157	1.43	0.110	1.08	1.00	0.135	No
126	2.52	43.56	5.10	38.46	0.97	0.157	1.43	0.110	1.08	1.00	0.136	No
127	2.54	43.88	5.30	38.58	0.97	0.158	1.43	0.110	1.08	1.00	0.137	No
128	2.56	44.20	5.49	38.71	0.97	0.158	1.43	0.111	1.08	1.00	0.137	No
129	2.58	44.52	5.69	38.83	0.97	0.159	1.43	0.111	1.08	1.00	0.137	No
130	2.60	44.84	5.89	38.96	0.97	0.159	1.43	0.112	1.08	1.00	0.138	No
131	2.62	45.16	6.08	39.08	0.97	0.160	1.43	0.112	1.08	1.00	0.138	No
132	2.64	45.48	6.28	39.20	0.97	0.161	1.43	0.112	1.08	1.00	0.139	No
133	2.66	45.80	6.47	39.32	0.97	0.161	1.43	0.113	1.08	1.00	0.138	No
134	2.68	46.12	6.67	39.45	0.97	0.162	1.43	0.113	1.08	1.00	0.139	No
135	2.70	46.44	6.87	39.57	0.97	0.162	1.43	0.114	1.08	1.00	0.139	No
136	2.72	46.76	7.06	39.70	0.97	0.163	1.43	0.114	1.08	1.00	0.140	No
137	2.74	47.09	7.26	39.83	0.97	0.163	1.43	0.114	1.08	1.00	0.141	No
138	2.76	47.42	7.46	39.96	0.97	0.164	1.43	0.115	1.08	1.00	0.142	No
139	2.78	47.75	7.65	40.10	0.97	0.164	1.43	0.115	1.07	1.00	0.142	No
140	2.80	48.08	7.85	40.23	0.97	0.165	1.43	0.115	1.07	1.00	0.143	No
141	2.82	48.40	8.04	40.36	0.96	0.165	1.43	0.116	1.07	1.00	0.144	No
142	2.84	48.73	8.24	40.49	0.96	0.166	1.43	0.116	1.07	1.00	0.144	No
143	2.86	49.05	8.44	40.62	0.96	0.166	1.43	0.117	1.07	1.00	0.145	No
144	2.88	49.38	8.63	40.74	0.96	0.167	1.43	0.117	1.07	1.00	0.144	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	49.70	8.83	40.87	0.96	0.168	1.43	0.117	1.07	1.00	0.145	No
146	2.92	50.03	9.03	41.00	0.96	0.168	1.43	0.118	1.07	1.00	0.146	No
147	2.94	50.35	9.22	41.13	0.96	0.169	1.43	0.118	1.07	1.00	0.147	No
148	2.96	50.67	9.42	41.25	0.96	0.169	1.43	0.118	1.07	1.00	0.147	No
149	2.98	50.99	9.61	41.38	0.96	0.170	1.43	0.119	1.07	1.00	0.148	No
150	3.00	51.31	9.81	41.50	0.96	0.170	1.43	0.119	1.07	1.00	0.148	No
151	3.02	51.63	10.01	41.62	0.96	0.170	1.43	0.119	1.07	1.00	0.149	No
152	3.04	51.94	10.20	41.74	0.96	0.171	1.43	0.120	1.07	1.00	0.149	No
153	3.06	52.25	10.40	41.85	0.96	0.171	1.43	0.120	1.07	1.00	0.150	No
154	3.08	52.56	10.59	41.96	0.96	0.172	1.43	0.120	1.07	1.00	0.150	No
155	3.10	52.87	10.79	42.08	0.96	0.172	1.43	0.121	1.07	1.00	2.000	Yes
156	3.12	53.18	10.99	42.19	0.96	0.173	1.43	0.121	1.07	1.00	2.000	Yes
157	3.14	53.49	11.18	42.31	0.96	0.173	1.43	0.121	1.07	1.00	2.000	Yes
158	3.16	53.82	11.38	42.44	0.96	0.174	1.43	0.122	1.08	1.00	2.000	Yes
159	3.18	54.15	11.58	42.57	0.96	0.174	1.43	0.122	1.08	1.00	2.000	Yes
160	3.20	54.48	11.77	42.71	0.96	0.175	1.43	0.122	1.08	1.00	2.000	Yes
161	3.22	54.82	11.97	42.85	0.96	0.175	1.43	0.123	1.08	1.00	2.000	Yes
162	3.24	55.17	12.16	43.00	0.96	0.176	1.43	0.123	1.08	1.00	0.149	No
163	3.26	55.51	12.36	43.15	0.96	0.176	1.43	0.123	1.08	1.00	0.149	No
164	3.28	55.86	12.56	43.30	0.96	0.176	1.43	0.123	1.08	1.00	0.149	No
165	3.30	56.21	12.75	43.46	0.96	0.177	1.43	0.124	1.08	1.00	0.150	No
166	3.32	56.56	12.95	43.61	0.96	0.177	1.43	0.124	1.07	1.00	0.151	No
167	3.34	56.90	13.15	43.76	0.96	0.178	1.43	0.124	1.07	1.00	0.153	No
168	3.36	57.25	13.34	43.91	0.95	0.178	1.43	0.125	1.07	1.00	0.152	No
169	3.38	57.60	13.54	44.06	0.95	0.178	1.43	0.125	1.07	1.00	0.152	No
170	3.40	57.95	13.73	44.22	0.95	0.179	1.43	0.125	1.08	1.00	0.152	No
171	3.42	58.30	13.93	44.37	0.95	0.179	1.43	0.125	1.07	1.00	0.153	No
172	3.44	58.65	14.13	44.53	0.95	0.180	1.43	0.126	1.07	1.00	0.154	No
173	3.46	59.00	14.32	44.68	0.95	0.180	1.43	0.126	1.07	1.00	0.155	No
174	3.48	59.35	14.52	44.84	0.95	0.180	1.43	0.126	1.07	1.00	0.156	No
175	3.50	59.70	14.72	44.99	0.95	0.181	1.43	0.126	1.07	1.00	0.155	No
176	3.52	60.05	14.91	45.14	0.95	0.181	1.43	0.127	1.07	1.00	0.155	No
177	3.54	60.40	15.11	45.29	0.95	0.181	1.43	0.127	1.07	1.00	0.156	No
178	3.56	60.74	15.30	45.44	0.95	0.182	1.43	0.127	1.07	1.00	0.157	No
179	3.58	61.08	15.50	45.58	0.95	0.182	1.43	0.128	1.07	1.00	0.158	No
180	3.60	61.42	15.70	45.73	0.95	0.183	1.43	0.128	1.07	1.00	0.159	No
181	3.62	61.76	15.89	45.87	0.95	0.183	1.43	0.128	1.07	1.00	0.159	No
182	3.64	62.10	16.09	46.02	0.95	0.183	1.43	0.128	1.07	1.00	0.159	No
183	3.66	62.45	16.28	46.16	0.95	0.184	1.43	0.129	1.07	1.00	0.160	No
184	3.68	62.79	16.48	46.30	0.95	0.184	1.43	0.129	1.07	1.00	0.160	No
185	3.70	63.12	16.68	46.45	0.95	0.184	1.43	0.129	1.06	1.00	0.160	No
186	3.72	63.46	16.87	46.59	0.95	0.185	1.43	0.129	1.06	1.00	0.161	No
187	3.74	63.79	17.07	46.72	0.95	0.185	1.43	0.130	1.06	1.00	0.161	No
188	3.76	64.13	17.27	46.86	0.95	0.185	1.43	0.130	1.06	1.00	0.162	No
189	3.78	64.46	17.46	47.00	0.95	0.186	1.43	0.130	1.06	1.00	0.162	No
190	3.80	64.79	17.66	47.13	0.95	0.186	1.43	0.130	1.06	1.00	0.163	No
191	3.82	65.12	17.85	47.27	0.95	0.186	1.43	0.130	1.06	1.00	0.162	No
192	3.84	65.46	18.05	47.41	0.95	0.187	1.43	0.131	1.07	1.00	0.161	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	65.81	18.25	47.56	0.95	0.187	1.43	0.131	1.07	1.00	0.160	No
194	3.88	66.16	18.44	47.72	0.94	0.187	1.43	0.131	1.07	1.00	0.162	No
195	3.90	66.51	18.64	47.87	0.94	0.188	1.43	0.131	1.06	1.00	0.163	No
196	3.92	66.86	18.84	48.02	0.94	0.188	1.43	0.132	1.06	1.00	0.164	No
197	3.94	67.20	19.03	48.17	0.94	0.188	1.43	0.132	1.06	1.00	0.165	No
198	3.96	67.55	19.23	48.32	0.94	0.189	1.43	0.132	1.06	1.00	0.165	No
199	3.98	67.89	19.42	48.47	0.94	0.189	1.43	0.132	1.06	1.00	0.165	No
200	4.00	68.23	19.62	48.61	0.94	0.189	1.43	0.132	1.06	1.00	0.165	No
201	4.02	68.57	19.82	48.75	0.94	0.189	1.43	0.133	1.06	1.00	0.166	No
202	4.04	68.91	20.01	48.89	0.94	0.190	1.43	0.133	1.06	1.00	0.166	No
203	4.06	69.24	20.21	49.03	0.94	0.190	1.43	0.133	1.06	1.00	0.166	No
204	4.08	69.58	20.40	49.17	0.94	0.190	1.43	0.133	1.06	1.00	0.166	No
205	4.10	69.91	20.60	49.31	0.94	0.191	1.43	0.133	1.06	1.00	0.167	No
206	4.12	70.25	20.80	49.45	0.94	0.191	1.43	0.134	1.06	1.00	0.167	No
207	4.14	70.59	20.99	49.60	0.94	0.191	1.43	0.134	1.06	1.00	0.167	No
208	4.16	70.94	21.19	49.75	0.94	0.192	1.43	0.134	1.06	1.00	0.167	No
209	4.18	71.28	21.39	49.90	0.94	0.192	1.43	0.134	1.06	1.00	0.167	No
210	4.20	71.63	21.58	50.05	0.94	0.192	1.43	0.134	1.06	1.00	0.167	No
211	4.22	71.98	21.78	50.20	0.94	0.192	1.43	0.135	1.06	1.00	0.167	No
212	4.24	72.32	21.97	50.35	0.94	0.193	1.43	0.135	1.06	1.00	0.168	No
213	4.26	72.67	22.17	50.50	0.94	0.193	1.43	0.135	1.06	1.00	0.169	No
214	4.28	73.01	22.37	50.64	0.94	0.193	1.43	0.135	1.06	1.00	0.170	No
215	4.30	73.35	22.56	50.79	0.94	0.193	1.43	0.135	1.06	1.00	0.170	No
216	4.32	73.69	22.76	50.93	0.94	0.194	1.43	0.136	1.06	1.00	0.170	No
217	4.34	74.03	22.96	51.07	0.94	0.194	1.43	0.136	1.06	1.00	0.171	No
218	4.36	74.36	23.15	51.21	0.94	0.194	1.43	0.136	1.06	1.00	0.171	No
219	4.38	74.69	23.35	51.35	0.93	0.194	1.43	0.136	1.05	1.00	0.172	No
220	4.40	75.02	23.54	51.48	0.93	0.195	1.43	0.136	1.05	1.00	0.172	No
221	4.42	75.35	23.74	51.61	0.93	0.195	1.43	0.137	1.05	1.00	0.172	No
222	4.44	75.68	23.94	51.74	0.93	0.195	1.43	0.137	1.05	1.00	0.172	No
223	4.46	76.01	24.13	51.88	0.93	0.196	1.43	0.137	1.05	1.00	0.172	No
224	4.48	76.34	24.33	52.01	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
225	4.51	76.83	24.62	52.21	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
226	4.52	77.00	24.72	52.27	0.93	0.196	1.43	0.137	1.05	1.00	0.173	No
227	4.54	77.33	24.92	52.41	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
228	4.56	77.66	25.11	52.54	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
229	4.58	77.99	25.31	52.68	0.93	0.197	1.43	0.138	1.05	1.00	0.174	No
230	4.60	78.32	25.51	52.81	0.93	0.197	1.43	0.138	1.05	1.00	0.175	No
231	4.62	78.65	25.70	52.95	0.93	0.198	1.43	0.138	1.05	1.00	0.175	No
232	4.64	78.98	25.90	53.08	0.93	0.198	1.43	0.138	1.05	1.00	0.175	No
233	4.66	79.31	26.09	53.21	0.93	0.198	1.43	0.139	1.05	1.00	0.175	No
234	4.68	79.63	26.29	53.34	0.93	0.198	1.43	0.139	1.05	1.00	0.176	No
235	4.70	79.96	26.49	53.47	0.93	0.199	1.43	0.139	1.05	1.00	0.176	No
236	4.72	80.28	26.68	53.60	0.93	0.199	1.43	0.139	1.05	1.00	0.176	No
237	4.74	80.60	26.88	53.72	0.93	0.199	1.43	0.139	1.05	1.00	0.176	No
238	4.76	80.93	27.08	53.85	0.93	0.199	1.43	0.139	1.05	1.00	0.176	No
239	4.78	81.26	27.27	53.98	0.93	0.199	1.43	0.140	1.05	1.00	0.177	No
240	4.80	81.58	27.47	54.12	0.93	0.200	1.43	0.140	1.05	1.00	0.177	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	81.91	27.66	54.25	0.93	0.200	1.43	0.140	1.05	1.00	0.177	No
242	4.84	82.24	27.86	54.38	0.93	0.200	1.43	0.140	1.05	1.00	0.177	No
243	4.86	82.58	28.06	54.52	0.93	0.200	1.43	0.140	1.05	1.00	0.177	No
244	4.89	83.09	28.35	54.74	0.92	0.201	1.43	0.140	1.05	1.00	0.177	No
245	4.90	83.26	28.45	54.81	0.92	0.201	1.43	0.141	1.05	1.00	0.177	No
246	4.92	83.60	28.65	54.96	0.92	0.201	1.43	0.141	1.05	1.00	0.177	No
247	4.94	83.94	28.84	55.10	0.92	0.201	1.43	0.141	1.05	1.00	0.178	No
248	4.96	84.28	29.04	55.24	0.92	0.201	1.43	0.141	1.05	1.00	0.179	No
249	4.98	84.62	29.23	55.39	0.92	0.202	1.43	0.141	1.05	1.00	0.179	No
250	5.00	84.96	29.43	55.53	0.92	0.202	1.43	0.141	1.05	1.00	0.179	No
251	5.02	85.29	29.63	55.66	0.92	0.202	1.43	0.141	1.05	1.00	0.179	No
252	5.04	85.62	29.82	55.80	0.92	0.202	1.43	0.142	1.05	1.00	0.180	No
253	5.06	85.96	30.02	55.94	0.92	0.202	1.43	0.142	1.05	1.00	0.180	No
254	5.08	86.29	30.21	56.08	0.92	0.203	1.43	0.142	1.05	1.00	0.180	No
255	5.10	86.62	30.41	56.21	0.92	0.203	1.43	0.142	1.05	1.00	0.180	No
256	5.12	86.96	30.61	56.35	0.92	0.203	1.43	0.142	1.05	1.00	0.181	No
257	5.14	87.29	30.80	56.48	0.92	0.203	1.43	0.142	1.05	1.00	0.181	No
258	5.16	87.62	31.00	56.62	0.92	0.203	1.43	0.142	1.05	1.00	0.182	No
259	5.18	87.95	31.20	56.75	0.92	0.204	1.43	0.142	1.05	1.00	0.182	No
260	5.20	88.27	31.39	56.88	0.92	0.204	1.43	0.143	1.05	1.00	0.182	No
261	5.22	88.59	31.59	57.01	0.92	0.204	1.43	0.143	1.05	1.00	0.182	No
262	5.24	88.91	31.78	57.13	0.92	0.204	1.43	0.143	1.05	1.00	0.182	No
263	5.26	89.23	31.98	57.25	0.92	0.204	1.43	0.143	1.05	1.00	0.183	No
264	5.28	89.54	32.18	57.37	0.92	0.205	1.43	0.143	1.04	1.00	0.183	No
265	5.30	89.86	32.37	57.48	0.92	0.205	1.43	0.143	1.04	1.00	0.183	No
266	5.32	90.17	32.57	57.60	0.92	0.205	1.43	0.143	1.04	1.00	0.183	No
267	5.34	90.49	32.77	57.72	0.92	0.205	1.43	0.144	1.04	1.00	0.184	No
268	5.37	90.96	33.06	57.90	0.91	0.205	1.43	0.144	1.04	1.00	0.184	No
269	5.38	91.12	33.16	57.96	0.91	0.206	1.43	0.144	1.04	1.00	0.183	No
270	5.40	91.44	33.35	58.09	0.91	0.206	1.43	0.144	1.04	1.00	0.183	No
271	5.42	91.77	33.55	58.22	0.91	0.206	1.43	0.144	1.05	1.00	0.183	No
272	5.44	92.09	33.75	58.35	0.91	0.206	1.43	0.144	1.05	1.00	0.183	No
273	5.46	92.42	33.94	58.48	0.91	0.206	1.43	0.144	1.04	1.00	0.184	No
274	5.48	92.75	34.14	58.61	0.91	0.206	1.43	0.144	1.04	1.00	0.184	No
275	5.50	93.08	34.34	58.74	0.91	0.207	1.43	0.145	1.04	1.00	0.185	No
276	5.52	93.41	34.53	58.88	0.91	0.207	1.43	0.145	1.04	1.00	0.185	No
277	5.54	93.74	34.73	59.01	0.91	0.207	1.43	0.145	1.04	1.00	0.185	No
278	5.56	94.07	34.92	59.14	0.91	0.207	1.43	0.145	1.04	1.00	0.185	No
279	5.58	94.40	35.12	59.28	0.91	0.207	1.43	0.145	1.04	1.00	0.185	No
280	5.60	94.72	35.32	59.41	0.91	0.207	1.43	0.145	1.04	1.00	0.186	No
281	5.62	95.05	35.51	59.54	0.91	0.208	1.43	0.145	1.04	1.00	0.186	No
282	5.64	95.37	35.71	59.66	0.91	0.208	1.43	0.145	1.04	1.00	0.186	No
283	5.66	95.69	35.90	59.79	0.91	0.208	1.43	0.145	1.04	1.00	0.187	No
284	5.68	96.01	36.10	59.91	0.91	0.208	1.43	0.146	1.04	1.00	0.187	No
285	5.70	96.33	36.30	60.03	0.91	0.208	1.43	0.146	1.04	1.00	0.187	No
286	5.72	96.64	36.49	60.15	0.91	0.208	1.43	0.146	1.04	1.00	0.187	No
287	5.74	96.95	36.69	60.26	0.91	0.209	1.43	0.146	1.04	1.00	0.188	No
288	5.76	97.26	36.89	60.38	0.91	0.209	1.43	0.146	1.04	1.00	0.188	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	97.57	37.08	60.49	0.91	0.209	1.43	0.146	1.04	1.00	0.188	No
290	5.80	97.87	37.28	60.60	0.91	0.209	1.43	0.146	1.04	1.00	0.188	No
291	5.82	98.18	37.47	60.71	0.90	0.209	1.43	0.146	1.04	1.00	0.188	No
292	5.84	98.50	37.67	60.83	0.90	0.209	1.43	0.147	1.04	1.00	0.187	No
293	5.87	98.98	37.96	61.01	0.90	0.210	1.43	0.147	1.04	1.00	0.187	No
294	5.88	99.14	38.06	61.08	0.90	0.210	1.43	0.147	1.04	1.00	0.188	No
295	5.90	99.46	38.26	61.20	0.90	0.210	1.43	0.147	1.04	1.00	0.188	No
296	5.92	99.79	38.46	61.33	0.90	0.210	1.43	0.147	1.04	1.00	0.188	No
297	5.94	100.12	38.65	61.47	0.90	0.210	1.43	0.147	1.04	1.00	0.187	No
298	5.96	100.45	38.85	61.60	0.90	0.210	1.43	0.147	1.04	1.00	0.187	No
299	5.98	100.79	39.04	61.74	0.90	0.210	1.43	0.147	1.04	1.00	0.186	No
300	6.00	101.13	39.24	61.89	0.90	0.210	1.43	0.147	1.04	1.00	0.187	No
301	6.02	101.47	39.44	62.03	0.90	0.211	1.43	0.147	1.04	1.00	0.187	No
302	6.04	101.81	39.63	62.17	0.90	0.211	1.43	0.147	1.04	1.00	0.187	No
303	6.06	102.14	39.83	62.31	0.90	0.211	1.43	0.148	1.04	1.00	0.188	No
304	6.08	102.48	40.02	62.45	0.90	0.211	1.43	0.148	1.04	1.00	0.189	No
305	6.10	102.81	40.22	62.58	0.90	0.211	1.43	0.148	1.04	1.00	0.190	No
306	6.12	103.13	40.42	62.71	0.90	0.211	1.43	0.148	1.04	1.00	0.190	No
307	6.14	103.46	40.61	62.84	0.90	0.211	1.43	0.148	1.04	1.00	0.190	No
308	6.16	103.78	40.81	62.97	0.90	0.211	1.43	0.148	1.04	1.00	0.190	No
309	6.19	104.26	41.10	63.16	0.90	0.212	1.43	0.148	1.04	1.00	0.190	No
310	6.20	104.42	41.20	63.22	0.90	0.212	1.43	0.148	1.04	1.00	0.190	No
311	6.22	104.74	41.40	63.35	0.90	0.212	1.43	0.148	1.04	1.00	0.190	No
312	6.24	105.07	41.59	63.47	0.90	0.212	1.43	0.148	1.04	1.00	0.190	No
313	6.26	105.39	41.79	63.60	0.89	0.212	1.43	0.148	1.04	1.00	0.190	No
314	6.28	105.72	41.99	63.73	0.89	0.212	1.43	0.149	1.04	1.00	0.190	No
315	6.30	106.05	42.18	63.87	0.89	0.212	1.43	0.149	1.04	1.00	0.190	No
316	6.32	106.38	42.38	64.00	0.89	0.212	1.43	0.149	1.04	1.00	0.191	No
317	6.34	106.71	42.58	64.13	0.89	0.213	1.43	0.149	1.04	1.00	0.191	No
318	6.36	107.04	42.77	64.27	0.89	0.213	1.43	0.149	1.04	1.00	0.192	No
319	6.38	107.37	42.97	64.40	0.89	0.213	1.43	0.149	1.04	1.00	0.192	No
320	6.40	107.69	43.16	64.53	0.89	0.213	1.43	0.149	1.04	1.00	0.192	No
321	6.42	108.02	43.36	64.66	0.89	0.213	1.43	0.149	1.04	1.00	0.192	No
322	6.44	108.34	43.56	64.79	0.89	0.213	1.43	0.149	1.04	1.00	0.192	No
323	6.46	108.66	43.75	64.91	0.89	0.213	1.43	0.149	1.04	1.00	0.192	No
324	6.48	108.98	43.95	65.03	0.89	0.213	1.43	0.149	1.03	1.00	0.193	No
325	6.50	109.30	44.15	65.15	0.89	0.213	1.43	0.149	1.04	1.00	0.192	No
326	6.52	109.62	44.34	65.28	0.89	0.214	1.43	0.149	1.04	1.00	0.192	No
327	6.54	109.95	44.54	65.41	0.89	0.214	1.43	0.150	1.04	1.00	0.191	No
328	6.56	110.28	44.73	65.54	0.89	0.214	1.43	0.150	1.04	1.00	0.190	No
329	6.58	110.61	44.93	65.68	0.89	0.214	1.43	0.150	1.04	1.00	0.191	No
330	6.60	110.93	45.13	65.81	0.89	0.214	1.43	0.150	1.04	1.00	0.192	No
331	6.62	111.25	45.32	65.93	0.89	0.214	1.43	0.150	1.03	1.00	0.193	No
332	6.64	111.58	45.52	66.06	0.89	0.214	1.43	0.150	1.03	1.00	0.193	No
333	6.66	111.90	45.71	66.18	0.89	0.214	1.43	0.150	1.03	1.00	0.193	No
334	6.68	112.23	45.91	66.32	0.89	0.214	1.43	0.150	1.03	1.00	0.193	No
335	6.70	112.56	46.11	66.45	0.89	0.214	1.43	0.150	1.03	1.00	0.192	No
336	6.72	112.89	46.30	66.58	0.88	0.214	1.43	0.150	1.03	1.00	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	113.22	46.50	66.72	0.88	0.215	1.43	0.150	1.03	1.00	0.193	No
338	6.76	113.55	46.70	66.86	0.88	0.215	1.43	0.150	1.03	1.00	0.192	No
339	6.78	113.89	46.89	66.99	0.88	0.215	1.43	0.150	1.03	1.00	0.192	No
340	6.80	114.22	47.09	67.13	0.88	0.215	1.43	0.150	1.03	1.00	0.192	No
341	6.82	114.56	47.28	67.27	0.88	0.215	1.43	0.150	1.03	1.00	0.193	No
342	6.84	114.90	47.48	67.42	0.88	0.215	1.43	0.150	1.03	1.00	0.192	No
343	6.86	115.24	47.68	67.56	0.88	0.215	1.43	0.151	1.03	1.00	0.193	No
344	6.88	115.58	47.87	67.70	0.88	0.215	1.43	0.151	1.03	1.00	0.193	No
345	6.90	115.92	48.07	67.85	0.88	0.215	1.43	0.151	1.03	1.00	0.192	No
346	6.92	116.26	48.27	67.99	0.88	0.215	1.43	0.151	1.03	1.00	0.192	No
347	6.94	116.60	48.46	68.14	0.88	0.215	1.43	0.151	1.03	1.00	0.192	No
348	6.96	116.94	48.66	68.28	0.88	0.215	1.43	0.151	1.03	1.00	2.000	Yes
349	6.98	117.28	48.85	68.43	0.88	0.215	1.43	0.151	1.03	1.00	2.000	Yes
350	7.00	117.63	49.05	68.58	0.88	0.215	1.43	0.151	1.03	1.00	2.000	Yes
351	7.02	117.97	49.25	68.73	0.88	0.215	1.43	0.151	1.03	1.00	2.000	Yes
352	7.04	118.32	49.44	68.88	0.88	0.216	1.43	0.151	1.03	1.00	2.000	Yes
353	7.06	118.66	49.64	69.02	0.88	0.216	1.43	0.151	1.03	1.00	2.000	Yes
354	7.08	119.00	49.83	69.16	0.88	0.216	1.43	0.151	1.03	1.00	2.000	Yes
355	7.10	119.33	50.03	69.29	0.88	0.216	1.43	0.151	1.03	1.00	2.000	Yes
356	7.12	119.65	50.23	69.42	0.88	0.216	1.43	0.151	1.03	1.00	2.000	Yes
357	7.14	119.97	50.42	69.55	0.88	0.216	1.43	0.151	1.03	1.00	0.192	No
358	7.16	120.29	50.62	69.67	0.87	0.216	1.43	0.151	1.03	1.00	0.192	No
359	7.18	120.61	50.82	69.79	0.87	0.216	1.43	0.151	1.03	1.00	0.193	No
360	7.20	120.92	51.01	69.91	0.87	0.216	1.43	0.151	1.03	1.00	0.193	No
361	7.22	121.24	51.21	70.04	0.87	0.216	1.43	0.151	1.03	1.00	0.193	No
362	7.24	121.56	51.40	70.16	0.87	0.216	1.43	0.151	1.03	1.00	0.193	No
363	7.26	121.89	51.60	70.28	0.87	0.216	1.43	0.151	1.03	1.00	0.193	No
364	7.28	122.21	51.80	70.41	0.87	0.216	1.43	0.151	1.03	1.00	0.193	No
365	7.30	122.52	51.99	70.53	0.87	0.216	1.43	0.152	1.03	1.00	0.194	No
366	7.32	122.84	52.19	70.66	0.87	0.217	1.43	0.152	1.03	1.00	0.193	No
367	7.34	123.17	52.39	70.79	0.87	0.217	1.43	0.152	1.03	1.00	0.193	No
368	7.36	123.51	52.58	70.93	0.87	0.217	1.43	0.152	1.03	1.00	0.193	No
369	7.38	123.84	52.78	71.07	0.87	0.217	1.43	0.152	1.03	1.00	0.192	No
370	7.40	124.18	52.97	71.21	0.87	0.217	1.43	0.152	1.03	1.00	0.193	No
371	7.42	124.51	53.17	71.34	0.87	0.217	1.43	0.152	1.03	1.00	0.193	No
372	7.44	124.84	53.37	71.47	0.87	0.217	1.43	0.152	1.03	1.00	2.000	Yes
373	7.46	125.17	53.56	71.61	0.87	0.217	1.43	0.152	1.03	1.00	2.000	Yes
374	7.48	125.50	53.76	71.75	0.87	0.217	1.43	0.152	1.03	1.00	2.000	Yes
375	7.50	125.84	53.96	71.89	0.87	0.217	1.43	0.152	1.03	1.00	2.000	Yes
376	7.52	126.18	54.15	72.03	0.87	0.217	1.43	0.152	1.03	1.00	2.000	Yes
377	7.54	126.53	54.35	72.18	0.87	0.217	1.43	0.152	1.03	1.00	0.193	No
378	7.56	126.87	54.54	72.32	0.87	0.217	1.43	0.152	1.03	1.00	0.194	No
379	7.58	127.21	54.74	72.47	0.87	0.217	1.43	0.152	1.03	1.00	0.194	No
380	7.60	127.55	54.94	72.61	0.86	0.217	1.43	0.152	1.03	1.00	0.194	No
381	7.62	127.89	55.13	72.76	0.86	0.217	1.43	0.152	1.03	1.00	0.194	No
382	7.64	128.24	55.33	72.91	0.86	0.217	1.43	0.152	1.03	1.00	2.000	Yes
383	7.66	128.58	55.52	73.06	0.86	0.217	1.43	0.152	1.03	1.00	2.000	Yes
384	7.68	128.93	55.72	73.21	0.86	0.217	1.43	0.152	1.03	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	129.27	55.92	73.35	0.86	0.217	1.43	0.152	1.03	1.00	2.000	Yes
386	7.72	129.60	56.11	73.49	0.86	0.217	1.43	0.152	1.03	1.00	2.000	Yes
387	7.74	129.94	56.31	73.63	0.86	0.217	1.43	0.152	1.03	1.00	2.000	Yes
388	7.76	130.27	56.51	73.77	0.86	0.217	1.43	0.152	1.03	1.00	0.193	No
389	7.78	130.61	56.70	73.91	0.86	0.217	1.43	0.152	1.03	1.00	0.194	No
390	7.80	130.94	56.90	74.05	0.86	0.217	1.43	0.152	1.03	1.00	0.194	No
391	7.82	131.28	57.09	74.18	0.86	0.217	1.43	0.152	1.03	1.00	2.000	Yes
392	7.84	131.61	57.29	74.32	0.86	0.218	1.43	0.152	1.03	1.00	2.000	Yes
393	7.86	131.95	57.49	74.46	0.86	0.218	1.43	0.152	1.03	1.00	2.000	Yes
394	7.88	132.28	57.68	74.60	0.86	0.218	1.43	0.152	1.03	1.00	2.000	Yes
395	7.90	132.62	57.88	74.74	0.86	0.218	1.43	0.152	1.03	1.00	2.000	Yes
396	7.92	132.96	58.08	74.89	0.86	0.218	1.43	0.152	1.03	1.00	0.196	No
397	7.94	133.31	58.27	75.04	0.86	0.218	1.43	0.152	1.03	1.00	0.195	No
398	7.96	133.65	58.47	75.18	0.86	0.218	1.43	0.152	1.03	1.00	0.194	No
399	7.98	134.00	58.66	75.33	0.86	0.218	1.43	0.152	1.03	1.00	0.194	No
400	8.00	134.34	58.86	75.48	0.86	0.218	1.43	0.152	1.03	1.00	2.000	Yes
401	8.02	134.69	59.06	75.64	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
402	8.04	135.04	59.25	75.79	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
403	8.06	135.39	59.45	75.94	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
404	8.08	135.73	59.64	76.09	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
405	8.10	136.08	59.84	76.24	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
406	8.12	136.43	60.04	76.40	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
407	8.14	136.78	60.23	76.55	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
408	8.16	137.12	60.43	76.69	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
409	8.18	137.47	60.63	76.84	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
410	8.20	137.82	60.82	77.00	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
411	8.22	138.17	61.02	77.15	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
412	8.24	138.52	61.21	77.31	0.85	0.218	1.43	0.152	1.03	1.00	2.000	Yes
413	8.26	138.88	61.41	77.47	0.85	0.218	1.43	0.152	1.02	1.00	2.000	Yes
414	8.28	139.22	61.61	77.62	0.85	0.218	1.43	0.152	1.02	1.00	2.000	Yes
415	8.30	139.57	61.80	77.77	0.85	0.218	1.43	0.152	1.02	1.00	0.195	No
416	8.32	139.91	62.00	77.92	0.85	0.218	1.43	0.152	1.02	1.00	0.195	No
417	8.34	140.26	62.20	78.06	0.85	0.218	1.43	0.152	1.02	1.00	0.195	No
418	8.36	140.60	62.39	78.21	0.85	0.218	1.43	0.152	1.02	1.00	0.195	No
419	8.38	140.94	62.59	78.35	0.85	0.218	1.43	0.152	1.02	1.00	0.195	No
420	8.40	141.28	62.78	78.50	0.85	0.218	1.43	0.152	1.02	1.00	0.194	No
421	8.42	141.63	62.98	78.65	0.85	0.218	1.43	0.152	1.02	1.00	0.194	No
422	8.44	141.97	63.18	78.79	0.84	0.218	1.43	0.152	1.02	1.00	0.194	No
423	8.46	142.31	63.37	78.94	0.84	0.218	1.43	0.152	1.02	1.00	0.195	No
424	8.48	142.66	63.57	79.09	0.84	0.218	1.43	0.152	1.02	1.00	0.195	No
425	8.50	143.00	63.77	79.24	0.84	0.218	1.43	0.152	1.02	1.00	0.195	No
426	8.52	143.35	63.96	79.39	0.84	0.218	1.43	0.152	1.02	1.00	0.194	No
427	8.54	143.70	64.16	79.54	0.84	0.218	1.43	0.152	1.02	1.00	0.194	No
428	8.56	144.04	64.35	79.69	0.84	0.218	1.43	0.152	1.02	1.00	0.195	No
429	8.58	144.38	64.55	79.83	0.84	0.218	1.43	0.152	1.02	1.00	0.195	No
430	8.60	144.72	64.75	79.97	0.84	0.218	1.43	0.152	1.02	1.00	0.196	No
431	8.62	145.06	64.94	80.12	0.84	0.218	1.43	0.152	1.02	1.00	0.196	No
432	8.64	145.40	65.14	80.26	0.84	0.218	1.43	0.152	1.02	1.00	0.196	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	145.74	65.33	80.41	0.84	0.218	1.43	0.152	1.02	1.00	0.196	No
434	8.68	146.08	65.53	80.55	0.84	0.218	1.43	0.152	1.02	1.00	0.197	No
435	8.70	146.42	65.73	80.69	0.84	0.218	1.43	0.152	1.02	1.00	0.197	No
436	8.72	146.76	65.92	80.83	0.84	0.218	1.43	0.152	1.02	1.00	0.198	No
437	8.74	147.09	66.12	80.97	0.84	0.218	1.43	0.152	1.02	1.00	0.198	No
438	8.76	147.43	66.32	81.11	0.84	0.218	1.43	0.152	1.02	1.00	0.198	No
439	8.78	147.76	66.51	81.25	0.84	0.218	1.43	0.152	1.02	1.00	0.199	No
440	8.80	148.10	66.71	81.39	0.84	0.218	1.43	0.152	1.02	1.00	0.200	No
441	8.82	148.43	66.90	81.53	0.84	0.218	1.43	0.152	1.02	1.00	0.198	No
442	8.84	148.77	67.10	81.67	0.84	0.218	1.43	0.152	1.02	1.00	0.199	No
443	8.86	149.10	67.30	81.81	0.83	0.218	1.43	0.152	1.02	1.00	0.199	No
444	8.88	149.44	67.49	81.94	0.83	0.218	1.43	0.152	1.02	1.00	0.199	No
445	8.90	149.77	67.69	82.08	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
446	8.92	150.10	67.89	82.21	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
447	8.94	150.42	68.08	82.34	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
448	8.96	150.75	68.28	82.47	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
449	8.98	151.08	68.47	82.60	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
450	9.00	151.40	68.67	82.73	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
451	9.02	151.72	68.87	82.85	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
452	9.04	152.04	69.06	82.98	0.83	0.218	1.43	0.152	1.02	1.00	0.199	No
453	9.06	152.36	69.26	83.10	0.83	0.218	1.43	0.152	1.02	1.00	0.199	No
454	9.08	152.69	69.45	83.23	0.83	0.218	1.43	0.152	1.02	1.00	0.199	No
455	9.10	153.01	69.65	83.36	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
456	9.12	153.33	69.85	83.48	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
457	9.14	153.65	70.04	83.61	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
458	9.16	153.98	70.24	83.74	0.83	0.218	1.43	0.152	1.02	1.00	0.200	No
459	9.18	154.30	70.44	83.86	0.83	0.218	1.43	0.152	1.01	1.00	0.200	No
460	9.20	154.62	70.63	83.99	0.83	0.218	1.43	0.152	1.01	1.00	0.200	No
461	9.22	154.94	70.83	84.11	0.83	0.218	1.43	0.152	1.01	1.00	0.200	No
462	9.24	155.26	71.02	84.23	0.83	0.218	1.43	0.152	1.01	1.00	0.200	No
463	9.26	155.58	71.22	84.36	0.83	0.218	1.43	0.152	1.01	1.00	0.200	No
464	9.28	155.90	71.42	84.48	0.83	0.218	1.43	0.152	1.01	1.00	0.200	No
465	9.30	156.23	71.61	84.61	0.82	0.218	1.43	0.152	1.01	1.00	0.199	No
466	9.32	156.55	71.81	84.74	0.82	0.218	1.43	0.152	1.01	1.00	0.199	No
467	9.34	156.88	72.01	84.87	0.82	0.218	1.43	0.152	1.01	1.00	0.200	No
468	9.36	157.20	72.20	85.00	0.82	0.218	1.43	0.152	1.01	1.00	0.200	No
469	9.38	157.52	72.40	85.13	0.82	0.218	1.43	0.152	1.01	1.00	0.200	No
470	9.40	157.85	72.59	85.25	0.82	0.218	1.43	0.152	1.01	1.00	0.200	No
471	9.42	158.17	72.79	85.38	0.82	0.218	1.43	0.152	1.01	1.00	0.197	No
472	9.44	158.51	72.99	85.52	0.82	0.218	1.43	0.152	1.02	1.00	0.196	No
473	9.46	158.84	73.18	85.66	0.82	0.218	1.43	0.152	1.02	1.00	2.000	Yes
474	9.48	159.17	73.38	85.79	0.82	0.218	1.43	0.152	1.01	1.00	2.000	Yes
475	9.50	159.50	73.58	85.93	0.82	0.218	1.43	0.152	1.01	1.00	2.000	Yes
476	9.52	159.84	73.77	86.07	0.82	0.218	1.43	0.152	1.01	1.00	2.000	Yes
477	9.54	160.18	73.97	86.22	0.82	0.218	1.43	0.152	1.01	1.00	0.199	No
478	9.56	160.53	74.16	86.37	0.82	0.218	1.43	0.152	1.01	1.00	0.200	No
479	9.58	160.88	74.36	86.52	0.82	0.217	1.43	0.152	1.01	1.00	0.200	No
480	9.60	161.22	74.56	86.66	0.82	0.217	1.43	0.152	1.01	1.00	0.200	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	161.56	74.75	86.81	0.82	0.217	1.43	0.152	1.01	1.00	0.200	No
482	9.64	161.91	74.95	86.96	0.82	0.217	1.43	0.152	1.01	1.00	0.200	No
483	9.66	162.24	75.14	87.10	0.82	0.217	1.43	0.152	1.01	1.00	0.200	No
484	9.68	162.58	75.34	87.23	0.82	0.217	1.43	0.152	1.01	1.00	0.200	No
485	9.70	162.91	75.54	87.37	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
486	9.72	163.24	75.73	87.50	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
487	9.74	163.57	75.93	87.64	0.81	0.217	1.43	0.152	1.01	1.00	0.201	No
488	9.76	163.90	76.13	87.77	0.81	0.217	1.43	0.152	1.01	1.00	0.201	No
489	9.78	164.22	76.32	87.90	0.81	0.217	1.43	0.152	1.01	1.00	0.201	No
490	9.80	164.54	76.52	88.03	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
491	9.82	164.87	76.71	88.15	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
492	9.84	165.19	76.91	88.28	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
493	9.86	165.51	77.11	88.40	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
494	9.88	165.83	77.30	88.53	0.81	0.217	1.43	0.152	1.01	1.00	0.199	No
495	9.91	166.32	77.60	88.73	0.81	0.217	1.43	0.152	1.01	1.00	0.199	No
496	9.92	166.49	77.70	88.79	0.81	0.217	1.43	0.152	1.01	1.00	0.199	No
497	9.94	166.82	77.89	88.93	0.81	0.217	1.43	0.152	1.01	1.00	0.199	No
498	9.96	167.15	78.09	89.06	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
499	9.98	167.47	78.28	89.19	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
500	10.00	167.80	78.48	89.32	0.81	0.217	1.43	0.152	1.01	1.00	0.200	No
501	10.03	168.28	78.77	89.51	0.81	0.217	1.43	0.152	1.01	1.00	0.201	No
502	10.04	168.44	78.87	89.57	0.81	0.217	1.43	0.152	1.01	1.00	0.201	No
503	10.06	168.77	79.07	89.70	0.81	0.217	1.43	0.152	1.01	1.00	0.201	No
504	10.08	169.09	79.26	89.82	0.81	0.217	1.43	0.152	1.01	1.00	0.201	No
505	10.10	169.41	79.46	89.95	0.81	0.217	1.43	0.152	1.01	1.00	0.201	No
506	10.12	169.73	79.66	90.07	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
507	10.14	170.05	79.85	90.20	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
508	10.16	170.37	80.05	90.32	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
509	10.18	170.69	80.25	90.44	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
510	10.20	171.00	80.44	90.56	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
511	10.22	171.32	80.64	90.68	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
512	10.24	171.63	80.83	90.80	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
513	10.26	171.95	81.03	90.92	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
514	10.28	172.26	81.23	91.03	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
515	10.30	172.58	81.42	91.15	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
516	10.32	172.89	81.62	91.27	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
517	10.34	173.21	81.82	91.39	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
518	10.36	173.52	82.01	91.51	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
519	10.38	173.84	82.21	91.63	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
520	10.40	174.16	82.40	91.75	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
521	10.42	174.47	82.60	91.87	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
522	10.44	174.79	82.80	91.99	0.80	0.217	1.43	0.152	1.01	1.00	0.201	No
523	10.46	175.10	82.99	92.11	0.80	0.217	1.43	0.152	1.01	1.00	0.200	No
524	10.48	175.42	83.19	92.23	0.80	0.217	1.43	0.152	1.01	1.00	0.200	No
525	10.50	175.74	83.39	92.35	0.80	0.217	1.43	0.152	1.01	1.00	0.200	No
526	10.52	176.06	83.58	92.48	0.80	0.217	1.43	0.152	1.01	1.00	0.200	No
527	10.54	176.38	83.78	92.61	0.79	0.217	1.43	0.152	1.01	1.00	0.200	No
528	10.56	176.71	83.97	92.74	0.79	0.216	1.43	0.152	1.01	1.00	0.200	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	177.04	84.17	92.87	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
530	10.60	177.37	84.37	93.00	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
531	10.62	177.70	84.56	93.13	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
532	10.64	178.03	84.76	93.27	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
533	10.66	178.36	84.95	93.40	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
534	10.68	178.69	85.15	93.54	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
535	10.70	179.01	85.35	93.67	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
536	10.72	179.34	85.54	93.80	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
537	10.74	179.67	85.74	93.93	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
538	10.76	180.00	85.94	94.06	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
539	10.78	180.34	86.13	94.20	0.79	0.216	1.43	0.151	1.01	1.00	0.199	No
540	10.80	180.68	86.33	94.35	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
541	10.82	181.02	86.52	94.49	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
542	10.84	181.36	86.72	94.64	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
543	10.86	181.70	86.92	94.78	0.79	0.216	1.43	0.151	1.01	1.00	0.200	No
544	10.88	182.04	87.11	94.93	0.79	0.216	1.43	0.151	1.01	1.00	0.199	No
545	10.90	182.38	87.31	95.07	0.79	0.216	1.43	0.151	1.01	1.00	0.199	No
546	10.92	182.71	87.51	95.21	0.79	0.216	1.43	0.151	1.01	1.00	0.199	No
547	10.94	183.05	87.70	95.35	0.79	0.216	1.43	0.151	1.01	1.00	0.199	No
548	10.96	183.39	87.90	95.49	0.78	0.216	1.43	0.151	1.00	1.00	0.199	No
549	10.98	183.73	88.09	95.64	0.78	0.215	1.43	0.151	1.00	1.00	0.199	No
550	11.00	184.07	88.29	95.78	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
551	11.02	184.41	88.49	95.92	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
552	11.04	184.75	88.68	96.06	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
553	11.06	185.08	88.88	96.20	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
554	11.08	185.42	89.07	96.34	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
555	11.10	185.75	89.27	96.48	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
556	11.12	186.08	89.47	96.61	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
557	11.14	186.40	89.66	96.74	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
558	11.16	186.73	89.86	96.87	0.78	0.215	1.43	0.151	1.00	1.00	0.200	No
559	11.18	187.05	90.06	96.99	0.78	0.215	1.43	0.150	1.00	1.00	0.200	No
560	11.20	187.38	90.25	97.12	0.78	0.215	1.43	0.150	1.00	1.00	0.199	No
561	11.22	187.70	90.45	97.25	0.78	0.215	1.43	0.150	1.00	1.00	0.199	No
562	11.24	188.03	90.64	97.39	0.78	0.215	1.43	0.150	1.00	1.00	0.198	No
563	11.26	188.37	90.84	97.53	0.78	0.215	1.43	0.150	1.00	1.00	0.199	No
564	11.28	188.70	91.04	97.66	0.78	0.215	1.43	0.150	1.00	1.00	0.199	No
565	11.30	189.03	91.23	97.80	0.78	0.215	1.43	0.150	1.00	1.00	0.199	No
566	11.32	189.37	91.43	97.94	0.78	0.215	1.43	0.150	1.00	1.00	0.199	No
567	11.34	189.70	91.63	98.08	0.78	0.215	1.43	0.150	1.00	1.00	0.199	No
568	11.36	190.04	91.82	98.22	0.78	0.215	1.43	0.150	1.00	1.00	0.199	No
569	11.38	190.37	92.02	98.36	0.77	0.214	1.43	0.150	1.00	1.00	0.199	No
570	11.40	190.71	92.21	98.49	0.77	0.214	1.43	0.150	1.00	1.00	0.200	No
571	11.42	191.04	92.41	98.63	0.77	0.214	1.43	0.150	1.00	1.00	0.199	No
572	11.44	191.37	92.61	98.76	0.77	0.214	1.43	0.150	1.00	1.00	0.199	No
573	11.46	191.70	92.80	98.90	0.77	0.214	1.43	0.150	1.00	1.00	0.199	No
574	11.48	192.03	93.00	99.04	0.77	0.214	1.43	0.150	1.00	1.00	0.199	No
575	11.50	192.37	93.19	99.17	0.77	0.214	1.43	0.150	1.00	1.00	0.199	No
576	11.52	192.70	93.39	99.31	0.77	0.214	1.43	0.150	1.00	1.00	0.198	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	193.04	93.59	99.45	0.77	0.214	1.43	0.150	1.00	1.00	0.197	No
578	11.56	193.38	93.78	99.60	0.77	0.214	1.43	0.150	1.00	1.00	0.197	No
579	11.58	193.73	93.98	99.75	0.77	0.214	1.43	0.150	1.00	1.00	0.197	No
580	11.60	194.08	94.18	99.90	0.77	0.214	1.43	0.150	1.00	1.00	0.196	No
581	11.62	194.43	94.37	100.06	0.77	0.214	1.43	0.150	1.00	1.00	0.196	No
582	11.64	194.79	94.57	100.22	0.77	0.214	1.43	0.150	1.00	1.00	0.195	No
583	11.66	195.15	94.76	100.39	0.77	0.214	1.43	0.149	1.00	1.00	0.195	No
584	11.68	195.51	94.96	100.55	0.77	0.213	1.43	0.149	1.00	1.00	0.195	No
585	11.70	195.87	95.16	100.72	0.77	0.213	1.43	0.149	1.00	1.00	0.194	No
586	11.72	196.24	95.35	100.88	0.77	0.213	1.43	0.149	1.00	1.00	0.194	No
587	11.74	196.60	95.55	101.05	0.77	0.213	1.43	0.149	1.00	1.00	0.194	No
588	11.76	196.95	95.75	101.21	0.77	0.213	1.43	0.149	1.00	1.00	0.196	No
589	11.78	197.30	95.94	101.36	0.77	0.213	1.43	0.149	1.00	1.00	0.197	No
590	11.80	197.64	96.14	101.50	0.76	0.213	1.43	0.149	1.00	1.00	0.198	No
591	11.82	197.97	96.33	101.64	0.76	0.213	1.43	0.149	1.00	1.00	0.199	No
592	11.84	198.31	96.53	101.78	0.76	0.213	1.43	0.149	1.00	1.00	0.199	No
593	11.86	198.64	96.73	101.91	0.76	0.213	1.43	0.149	1.00	1.00	0.198	No
594	11.88	198.97	96.92	102.05	0.76	0.213	1.43	0.149	1.00	1.00	0.198	No
595	11.90	199.30	97.12	102.18	0.76	0.213	1.43	0.149	1.00	1.00	0.198	No
596	11.93	199.80	97.41	102.38	0.76	0.213	1.43	0.149	1.00	1.00	0.198	No
597	11.94	199.96	97.51	102.45	0.76	0.213	1.43	0.149	1.00	1.00	0.199	No
598	11.96	200.29	97.71	102.59	0.76	0.212	1.43	0.149	1.00	1.00	0.199	No
599	11.98	200.62	97.90	102.72	0.76	0.212	1.43	0.149	1.00	1.00	0.199	No
600	12.00	200.95	98.10	102.85	0.76	0.212	1.43	0.149	1.00	1.00	0.199	No
601	12.02	201.28	98.30	102.99	0.76	0.212	1.43	0.149	1.00	1.00	0.198	No
602	12.04	201.62	98.49	103.12	0.76	0.212	1.43	0.149	1.00	1.00	0.198	No
603	12.06	201.94	98.69	103.26	0.76	0.212	1.43	0.149	1.00	1.00	0.198	No
604	12.08	202.27	98.88	103.39	0.76	0.212	1.43	0.148	1.00	1.00	0.198	No
605	12.10	202.60	99.08	103.52	0.76	0.212	1.43	0.148	1.00	1.00	0.198	No
606	12.12	202.93	99.28	103.65	0.76	0.212	1.43	0.148	1.00	1.00	0.198	No
607	12.14	203.25	99.47	103.78	0.76	0.212	1.43	0.148	1.00	1.00	0.198	No
608	12.16	203.58	99.67	103.91	0.76	0.212	1.43	0.148	1.00	1.00	0.198	No
609	12.18	203.91	99.87	104.05	0.76	0.212	1.43	0.148	1.00	1.00	0.198	No
610	12.20	204.24	100.06	104.18	0.76	0.212	1.43	0.148	1.00	1.00	0.198	No
611	12.22	204.57	100.26	104.31	0.75	0.212	1.43	0.148	1.00	1.00	0.198	No
612	12.24	204.90	100.45	104.45	0.75	0.212	1.43	0.148	1.00	1.00	0.198	No
613	12.26	205.23	100.65	104.58	0.75	0.212	1.43	0.148	1.00	1.00	0.198	No
614	12.28	205.56	100.85	104.72	0.75	0.212	1.43	0.148	1.00	1.00	0.198	No
615	12.30	205.90	101.04	104.85	0.75	0.211	1.43	0.148	1.00	1.00	0.198	No
616	12.32	206.23	101.24	104.99	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No
617	12.34	206.57	101.44	105.13	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No
618	12.36	206.91	101.63	105.27	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No
619	12.38	207.24	101.83	105.42	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No
620	12.40	207.58	102.02	105.56	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No
621	12.42	207.92	102.22	105.70	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No
622	12.44	208.26	102.42	105.84	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No
623	12.46	208.60	102.61	105.99	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No
624	12.48	208.94	102.81	106.13	0.75	0.211	1.43	0.148	1.00	1.00	0.197	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
625	12.50	209.28	103.01	106.27	0.75	0.211	1.43	0.147	1.00	1.00	0.197	No
626	12.52	209.61	103.20	106.41	0.75	0.211	1.43	0.147	1.00	1.00	0.197	No
627	12.54	209.95	103.40	106.55	0.75	0.211	1.43	0.147	1.00	1.00	0.197	No
628	12.56	210.28	103.59	106.69	0.75	0.210	1.43	0.147	1.00	1.00	0.197	No
629	12.58	210.62	103.79	106.83	0.75	0.210	1.43	0.147	1.00	1.00	0.197	No
630	12.60	210.96	103.99	106.97	0.75	0.210	1.43	0.147	1.00	1.00	0.197	No
631	12.62	211.29	104.18	107.11	0.75	0.210	1.43	0.147	1.00	1.00	0.197	No
632	12.64	211.63	104.38	107.25	0.74	0.210	1.43	0.147	1.00	1.00	0.197	No
633	12.66	211.97	104.57	107.40	0.74	0.210	1.43	0.147	1.00	1.00	0.197	No
634	12.68	212.31	104.77	107.54	0.74	0.210	1.43	0.147	1.00	1.00	0.197	No
635	12.70	212.65	104.97	107.68	0.74	0.210	1.43	0.147	1.00	1.00	0.196	No
636	12.72	212.99	105.16	107.82	0.74	0.210	1.43	0.147	0.99	1.00	0.196	No
637	12.74	213.33	105.36	107.97	0.74	0.210	1.43	0.147	0.99	1.00	0.196	No
638	12.76	213.67	105.56	108.11	0.74	0.210	1.43	0.147	0.99	1.00	0.196	No
639	12.78	214.01	105.75	108.26	0.74	0.210	1.43	0.147	0.99	1.00	0.196	No
640	12.80	214.35	105.95	108.40	0.74	0.210	1.43	0.147	0.99	1.00	0.196	No
641	12.82	214.69	106.14	108.55	0.74	0.210	1.43	0.147	0.99	1.00	0.196	No
642	12.84	215.04	106.34	108.70	0.74	0.209	1.43	0.147	0.99	1.00	0.196	No
643	12.86	215.38	106.54	108.85	0.74	0.209	1.43	0.147	0.99	1.00	0.196	No
644	12.88	215.73	106.73	109.00	0.74	0.209	1.43	0.146	0.99	1.00	0.196	No
645	12.91	216.25	107.03	109.22	0.74	0.209	1.43	0.146	0.99	1.00	0.196	No
646	12.93	216.59	107.22	109.37	0.74	0.209	1.43	0.146	0.99	1.00	0.196	No
647	12.95	216.94	107.42	109.52	0.74	0.209	1.43	0.146	0.99	1.00	0.196	No
648	12.96	217.11	107.52	109.59	0.74	0.209	1.43	0.146	0.99	1.00	0.196	No
649	12.98	217.46	107.71	109.74	0.74	0.209	1.43	0.146	0.99	1.00	0.196	No
650	13.00	217.80	107.91	109.89	0.74	0.209	1.43	0.146	0.99	1.00	0.195	No
651	13.02	218.15	108.11	110.04	0.74	0.209	1.43	0.146	0.99	1.00	0.195	No
652	13.04	218.49	108.30	110.19	0.74	0.209	1.43	0.146	0.99	1.00	0.195	No
653	13.06	218.84	108.50	110.34	0.74	0.208	1.43	0.146	0.99	1.00	0.195	No
654	13.08	219.19	108.69	110.49	0.73	0.208	1.43	0.146	0.99	1.00	0.195	No
655	13.10	219.53	108.89	110.64	0.73	0.208	1.43	0.146	0.99	1.00	0.195	No
656	13.12	219.89	109.09	110.80	0.73	0.208	1.43	0.146	0.99	1.00	0.195	No
657	13.14	220.24	109.28	110.95	0.73	0.208	1.43	0.146	0.99	1.00	0.195	No
658	13.16	220.59	109.48	111.11	0.73	0.208	1.43	0.146	0.99	1.00	0.195	No
659	13.19	221.11	109.77	111.34	0.73	0.208	1.43	0.146	0.99	1.00	0.195	No
660	13.20	221.29	109.87	111.42	0.73	0.208	1.43	0.146	0.99	1.00	0.195	No
661	13.22	221.64	110.07	111.57	0.73	0.208	1.43	0.145	0.99	1.00	0.195	No
662	13.24	221.99	110.26	111.72	0.73	0.208	1.43	0.145	0.99	1.00	0.195	No
663	13.26	222.34	110.46	111.88	0.73	0.208	1.43	0.145	0.99	1.00	0.195	No
664	13.28	222.69	110.66	112.03	0.73	0.208	1.43	0.145	0.99	1.00	0.195	No
665	13.30	223.04	110.85	112.19	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
666	13.32	223.39	111.05	112.34	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
667	13.34	223.74	111.25	112.50	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
668	13.36	224.10	111.44	112.65	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
669	13.38	224.45	111.64	112.81	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
670	13.40	224.80	111.83	112.97	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
671	13.42	225.16	112.03	113.13	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
672	13.44	225.51	112.23	113.28	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
673	13.46	225.87	112.42	113.44	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
674	13.48	226.22	112.62	113.60	0.73	0.207	1.43	0.145	0.99	1.00	0.194	No
675	13.50	226.58	112.82	113.76	0.72	0.206	1.43	0.145	0.99	1.00	0.194	No
676	13.52	226.93	113.01	113.92	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
677	13.54	227.29	113.21	114.08	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
678	13.56	227.64	113.40	114.24	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
679	13.58	227.99	113.60	114.39	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
680	13.60	228.35	113.80	114.55	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
681	13.62	228.70	113.99	114.70	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
682	13.64	229.05	114.19	114.86	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
683	13.66	229.39	114.38	115.01	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
684	13.68	229.73	114.58	115.15	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
685	13.70	230.07	114.78	115.30	0.72	0.206	1.43	0.144	0.99	1.00	0.194	No
686	13.72	230.41	114.97	115.44	0.72	0.205	1.43	0.144	0.99	1.00	0.194	No
687	13.74	230.75	115.17	115.58	0.72	0.205	1.43	0.144	0.99	1.00	0.194	No
688	13.76	231.08	115.37	115.71	0.72	0.205	1.43	0.144	0.99	1.00	0.193	No
689	13.78	231.41	115.56	115.85	0.72	0.205	1.43	0.144	0.99	1.00	0.193	No
690	13.81	231.90	115.86	116.05	0.72	0.205	1.43	0.144	0.99	1.00	0.193	No
691	13.82	232.07	115.95	116.11	0.72	0.205	1.43	0.144	0.99	1.00	0.194	No
692	13.84	232.39	116.15	116.24	0.72	0.205	1.43	0.143	0.99	1.00	0.194	No
693	13.86	232.72	116.35	116.37	0.72	0.205	1.43	0.143	0.99	1.00	0.194	No
694	13.88	233.04	116.54	116.50	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
695	13.90	233.37	116.74	116.63	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
696	13.92	233.69	116.94	116.76	0.72	0.205	1.43	0.143	0.99	1.00	0.193	No
697	13.94	234.02	117.13	116.88	0.71	0.205	1.43	0.143	0.99	1.00	0.193	No
698	13.96	234.34	117.33	117.01	0.71	0.205	1.43	0.143	0.99	1.00	0.193	No
699	13.98	234.66	117.52	117.14	0.71	0.205	1.43	0.143	0.99	1.00	0.193	No
700	14.00	234.99	117.72	117.27	0.71	0.204	1.43	0.143	0.99	1.00	0.193	No
701	14.02	235.32	117.92	117.40	0.71	0.204	1.43	0.143	0.99	1.00	0.193	No
702	14.04	235.64	118.11	117.53	0.71	0.204	1.43	0.143	0.99	1.00	0.193	No
703	14.06	235.97	118.31	117.66	0.71	0.204	1.43	0.143	0.99	1.00	0.192	No
704	14.08	236.30	118.50	117.80	0.71	0.204	1.43	0.143	0.99	1.00	0.192	No
705	14.10	236.64	118.70	117.94	0.71	0.204	1.43	0.143	0.99	1.00	0.192	No
706	14.13	237.14	119.00	118.14	0.71	0.204	1.43	0.143	0.99	1.00	0.192	No
707	14.14	237.31	119.09	118.22	0.71	0.204	1.43	0.143	0.99	1.00	0.192	No
708	14.16	237.65	119.29	118.36	0.71	0.204	1.43	0.143	0.99	1.00	0.192	No
709	14.18	237.98	119.49	118.50	0.71	0.204	1.43	0.143	0.99	1.00	0.192	No
710	14.20	238.32	119.68	118.64	0.71	0.204	1.43	0.143	0.99	1.00	0.192	No
711	14.22	238.66	119.88	118.78	0.71	0.204	1.43	0.142	0.99	1.00	0.192	No
712	14.24	239.00	120.07	118.92	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
713	14.26	239.34	120.27	119.07	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
714	14.28	239.67	120.47	119.21	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
715	14.30	240.01	120.66	119.34	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
716	14.32	240.34	120.86	119.48	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
717	14.34	240.67	121.06	119.61	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
718	14.36	240.99	121.25	119.74	0.71	0.203	1.43	0.142	0.99	1.00	0.192	No
719	14.38	241.32	121.45	119.87	0.70	0.203	1.43	0.142	0.99	1.00	0.192	No
720	14.40	241.64	121.64	119.99	0.70	0.203	1.43	0.142	0.99	1.00	0.192	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
721	14.42	241.96	121.84	120.12	0.70	0.203	1.43	0.142	0.99	1.00	0.192	No
722	14.44	242.28	122.04	120.24	0.70	0.203	1.43	0.142	0.99	1.00	0.192	No
723	14.46	242.60	122.23	120.37	0.70	0.203	1.43	0.142	0.99	1.00	0.192	No
724	14.48	242.92	122.43	120.49	0.70	0.203	1.43	0.142	0.99	1.00	0.192	No
725	14.50	243.24	122.63	120.62	0.70	0.202	1.43	0.142	0.99	1.00	0.192	No
726	14.52	243.57	122.82	120.74	0.70	0.202	1.43	0.142	0.99	1.00	0.192	No
727	14.54	243.89	123.02	120.87	0.70	0.202	1.43	0.142	0.99	1.00	0.191	No
728	14.56	244.21	123.21	121.00	0.70	0.202	1.43	0.142	0.99	1.00	0.191	No
729	14.58	244.53	123.41	121.12	0.70	0.202	1.43	0.142	0.99	1.00	0.191	No
730	14.60	244.86	123.61	121.25	0.70	0.202	1.43	0.141	0.99	1.00	0.191	No
731	14.62	245.18	123.80	121.38	0.70	0.202	1.43	0.141	0.99	1.00	0.191	No
732	14.64	245.50	124.00	121.50	0.70	0.202	1.43	0.141	0.99	1.00	0.191	No
733	14.66	245.83	124.19	121.63	0.70	0.202	1.43	0.141	0.99	1.00	0.191	No
734	14.68	246.15	124.39	121.76	0.70	0.202	1.43	0.141	0.99	1.00	0.191	No
735	14.70	246.48	124.59	121.89	0.70	0.202	1.43	0.141	0.99	1.00	0.191	No
736	14.72	246.81	124.78	122.03	0.70	0.202	1.43	0.141	0.98	1.00	0.191	No
737	14.74	247.15	124.98	122.17	0.70	0.202	1.43	0.141	0.98	1.00	0.189	No
738	14.76	247.50	125.18	122.32	0.70	0.201	1.43	0.141	0.98	1.00	0.188	No
739	14.78	247.85	125.37	122.48	0.70	0.201	1.43	0.141	0.98	1.00	0.187	No
740	14.80	248.20	125.57	122.63	0.70	0.201	1.43	0.141	0.98	1.00	0.187	No
741	14.82	248.56	125.76	122.79	0.69	0.201	1.43	0.141	0.98	1.00	0.187	No
742	14.84	248.91	125.96	122.95	0.69	0.201	1.43	0.141	0.98	1.00	0.187	No
743	14.86	249.27	126.16	123.12	0.69	0.201	1.43	0.141	0.98	1.00	0.186	No
744	14.88	249.63	126.35	123.28	0.69	0.201	1.43	0.141	0.98	1.00	0.186	No
745	14.90	249.98	126.55	123.44	0.69	0.201	1.43	0.141	0.98	1.00	0.187	No
746	14.92	250.34	126.75	123.59	0.69	0.201	1.43	0.140	0.98	1.00	0.188	No
747	14.94	250.69	126.94	123.75	0.69	0.201	1.43	0.140	0.98	1.00	0.188	No
748	14.96	251.05	127.14	123.91	0.69	0.200	1.43	0.140	0.98	1.00	0.188	No
749	14.98	251.40	127.33	124.07	0.69	0.200	1.43	0.140	0.98	1.00	0.187	No
750	15.00	251.76	127.53	124.23	0.69	0.200	1.43	0.140	0.98	1.00	0.187	No
751	15.02	252.11	127.73	124.38	0.69	0.200	1.43	0.140	0.98	1.00	0.188	No
752	15.04	252.47	127.92	124.54	0.69	0.200	1.43	0.140	0.98	1.00	0.188	No
753	15.06	252.82	128.12	124.70	0.69	0.200	1.43	0.140	0.98	1.00	0.189	No
754	15.08	253.17	128.31	124.86	0.69	0.200	1.43	0.140	0.98	1.00	0.189	No
755	15.10	253.52	128.51	125.01	0.69	0.200	1.43	0.140	0.98	1.00	0.188	No
756	15.12	253.87	128.71	125.17	0.69	0.200	1.43	0.140	0.98	1.00	0.187	No
757	15.14	254.23	128.90	125.32	0.69	0.200	1.43	0.140	0.98	1.00	0.188	No
758	15.17	254.75	129.20	125.55	0.69	0.199	1.43	0.140	0.98	1.00	0.188	No
759	15.18	254.93	129.30	125.63	0.69	0.199	1.43	0.140	0.98	1.00	0.188	No
760	15.20	255.28	129.49	125.79	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
761	15.22	255.63	129.69	125.94	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
762	15.24	255.98	129.88	126.09	0.69	0.199	1.43	0.139	0.98	1.00	0.188	No
763	15.26	256.33	130.08	126.24	0.69	0.199	1.43	0.139	0.98	1.00	0.189	No
764	15.28	256.67	130.28	126.39	0.68	0.199	1.43	0.139	0.98	1.00	0.189	No
765	15.30	257.01	130.47	126.54	0.68	0.199	1.43	0.139	0.98	1.00	0.189	No
766	15.32	257.35	130.67	126.68	0.68	0.199	1.43	0.139	0.98	1.00	0.189	No
767	15.34	257.69	130.87	126.82	0.68	0.199	1.43	0.139	0.98	1.00	0.189	No
768	15.36	258.02	131.06	126.96	0.68	0.198	1.43	0.139	0.98	1.00	0.189	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
769	15.38	258.35	131.26	127.10	0.68	0.198	1.43	0.139	0.98	1.00	0.189	No
770	15.40	258.68	131.45	127.23	0.68	0.198	1.43	0.139	0.98	1.00	0.188	No
771	15.42	259.01	131.65	127.36	0.68	0.198	1.43	0.139	0.98	1.00	0.188	No
772	15.44	259.34	131.85	127.49	0.68	0.198	1.43	0.139	0.98	1.00	0.188	No
773	15.46	259.67	132.04	127.63	0.68	0.198	1.43	0.139	0.98	1.00	0.188	No
774	15.48	260.00	132.24	127.76	0.68	0.198	1.43	0.139	0.98	1.00	0.188	No
775	15.50	260.32	132.44	127.89	0.68	0.198	1.43	0.139	0.98	1.00	0.188	No
776	15.52	260.65	132.63	128.02	0.68	0.198	1.43	0.138	0.98	1.00	0.188	No
777	15.54	260.98	132.83	128.15	0.68	0.198	1.43	0.138	0.98	1.00	0.188	No
778	15.56	261.31	133.02	128.29	0.68	0.198	1.43	0.138	0.98	1.00	0.188	No
779	15.58	261.64	133.22	128.42	0.68	0.198	1.43	0.138	0.98	1.00	0.188	No
780	15.60	261.97	133.42	128.56	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
781	15.62	262.31	133.61	128.69	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
782	15.64	262.64	133.81	128.83	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No
783	15.66	262.97	134.00	128.97	0.68	0.197	1.43	0.138	0.98	1.00	0.188	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.21	100.00	3.43	0.61	1.70	2.90	0.00	2.90	4.000	No	Yes	2.00
2	0.04	0.33	100.00	3.22	0.60	1.70	4.94	0.00	4.94	4.000	No	Yes	2.00
3	0.06	0.39	100.00	3.17	0.59	1.70	6.95	0.00	6.95	4.000	No	Yes	2.00
4	0.08	0.45	100.00	3.15	0.59	1.70	7.82	0.00	7.82	4.000	No	Yes	2.00
5	0.10	0.47	100.00	3.19	0.59	1.70	8.05	0.00	8.05	4.000	No	Yes	2.00
6	0.12	0.46	100.00	3.26	0.59	1.70	7.63	0.00	7.63	4.000	No	Yes	2.00
7	0.14	0.43	100.00	3.34	0.59	1.70	7.37	0.00	7.37	4.000	No	Yes	2.00
8	0.16	0.39	100.00	3.42	0.60	1.70	6.58	0.00	6.58	4.000	No	Yes	2.00
9	0.18	0.35	100.00	3.52	0.60	1.70	5.86	0.00	5.86	4.000	No	Yes	2.00
10	0.20	0.31	100.00	3.60	0.60	1.70	5.26	0.00	5.26	4.000	No	Yes	2.00
11	0.22	0.29	100.00	3.65	0.60	1.70	5.08	0.00	5.08	4.000	No	Yes	2.00
12	0.24	0.30	100.00	3.61	0.60	1.70	4.81	0.00	4.81	4.000	No	Yes	2.00
13	0.26	0.33	100.00	3.51	0.60	1.70	5.39	0.00	5.39	4.000	No	Yes	2.00
14	0.28	0.40	100.00	3.36	0.60	1.70	6.68	0.00	6.68	4.000	No	Yes	2.00
15	0.30	0.49	100.00	3.24	0.59	1.70	8.47	0.00	8.47	4.000	No	Yes	2.00
16	0.32	0.56	100.00	3.16	0.58	1.70	9.42	0.00	9.42	4.000	No	Yes	2.00
17	0.34	0.64	100.00	3.10	0.58	1.70	10.59	0.00	10.59	4.000	No	Yes	2.00
18	0.36	0.70	100.00	3.07	0.57	1.70	12.23	0.00	12.23	4.000	No	Yes	2.00
19	0.38	0.75	100.00	3.06	0.57	1.70	12.68	0.00	12.68	4.000	No	Yes	2.00
20	0.40	0.75	100.00	3.09	0.57	1.70	12.92	0.00	12.92	4.000	No	Yes	2.00
21	0.42	0.74	100.00	3.14	0.57	1.70	12.39	0.00	12.39	4.000	No	Yes	2.00
22	0.44	0.73	100.00	3.19	0.57	1.70	12.39	0.00	12.39	4.000	No	Yes	2.00
23	0.46	0.73	100.00	3.23	0.57	1.70	12.28	0.00	12.28	4.000	No	Yes	2.00
24	0.48	0.72	100.00	3.26	0.57	1.70	12.39	0.00	12.39	4.000	No	Yes	2.00
25	0.50	0.72	100.00	3.28	0.57	1.70	12.05	0.00	12.05	4.000	No	Yes	2.00
26	0.52	0.71	100.00	3.29	0.57	1.70	12.08	0.00	12.08	4.000	No	Yes	2.00
27	0.54	0.70	100.00	3.30	0.57	1.70	11.99	0.00	11.99	4.000	No	Yes	2.00
28	0.56	0.68	100.00	3.31	0.58	1.70	11.64	0.00	11.64	4.000	No	Yes	2.00
29	0.59	0.66	100.00	3.33	0.58	1.70	10.99	0.00	10.99	4.000	No	Yes	2.00
30	0.60	0.63	100.00	3.35	0.58	1.70	10.78	0.00	10.78	4.000	No	Yes	2.00
31	0.62	0.62	100.00	3.35	0.58	1.70	10.23	0.00	10.23	4.000	No	Yes	2.00
32	0.64	0.63	100.00	3.34	0.58	1.70	10.40	0.00	10.40	4.000	No	Yes	2.00
33	0.66	0.67	100.00	3.29	0.58	1.70	11.14	0.00	11.14	4.000	No	Yes	2.00
34	0.68	0.71	100.00	3.25	0.57	1.70	12.14	0.00	12.14	4.000	No	Yes	2.00
35	0.70	0.74	100.00	3.22	0.57	1.70	12.42	0.00	12.42	4.000	No	Yes	2.00
36	0.72	0.75	100.00	3.20	0.57	1.70	12.51	0.00	12.51	4.000	No	Yes	2.00
37	0.74	0.77	100.00	3.19	0.57	1.70	12.94	0.00	12.94	4.000	No	Yes	2.00
38	0.76	0.78	100.00	3.17	0.57	1.70	13.18	0.00	13.18	4.000	No	Yes	2.00
39	0.78	0.80	100.00	3.15	0.57	1.70	13.38	0.00	13.38	4.000	No	Yes	2.00
40	0.80	0.81	100.00	3.15	0.57	1.70	13.77	0.00	13.77	4.000	No	Yes	2.00
41	0.82	0.81	100.00	3.17	0.57	1.70	13.63	0.00	13.63	4.000	No	Yes	2.00
42	0.84	0.80	100.00	3.18	0.57	1.70	13.38	0.00	13.38	4.000	No	Yes	2.00
43	0.86	0.81	100.00	3.19	0.57	1.70	13.35	0.00	13.35	4.000	No	Yes	2.00
44	0.88	0.82	100.00	3.18	0.57	1.70	13.67	0.00	13.67	4.000	No	Yes	2.00
45	0.90	0.86	100.00	3.15	0.57	1.70	14.28	0.00	14.28	4.000	No	Yes	2.00
46	0.92	0.90	100.00	3.12	0.56	1.70	15.17	0.00	15.17	4.000	No	Yes	2.00
47	0.94	0.95	100.00	3.10	0.56	1.70	15.62	0.00	15.62	4.000	No	Yes	2.00
48	0.96	1.00	100.00	3.06	0.56	1.70	16.56	0.00	16.56	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	1.05	100.00	3.03	0.55	1.70	17.99	0.00	17.99	4.000	No	Yes	2.00
50	1.00	1.10	100.00	3.01	0.55	1.70	18.09	0.00	18.09	4.000	No	Yes	2.00
51	1.02	1.12	100.00	3.01	0.55	1.70	18.95	0.00	18.95	4.000	No	Yes	2.00
52	1.04	1.14	100.00	3.02	0.55	1.70	18.97	0.00	18.97	4.000	No	Yes	2.00
53	1.06	1.15	100.00	3.02	0.55	1.70	19.19	0.00	19.19	4.000	No	Yes	2.00
54	1.08	1.18	100.00	3.03	0.55	1.70	19.55	0.00	19.55	4.000	No	Yes	2.00
55	1.10	1.21	100.00	3.02	0.55	1.70	20.17	0.00	20.17	4.000	No	Yes	2.00
56	1.12	1.23	100.00	3.03	0.54	1.70	20.72	0.00	20.72	4.000	No	Yes	2.00
57	1.14	1.24	100.00	3.03	0.54	1.70	20.73	0.00	20.73	4.000	No	Yes	2.00
58	1.16	1.26	100.00	3.03	0.54	1.70	20.83	0.00	20.83	4.000	No	Yes	2.00
59	1.18	1.28	100.00	3.02	0.54	1.70	21.48	0.00	21.48	4.000	No	Yes	2.00
60	1.20	1.32	100.00	3.00	0.54	1.70	21.69	0.00	21.69	4.000	No	Yes	2.00
61	1.22	1.35	100.00	2.99	0.54	1.70	22.94	0.00	22.94	4.000	No	Yes	2.00
62	1.25	1.37	100.00	2.99	0.54	1.70	22.69	0.00	22.69	4.000	No	Yes	2.00
63	1.26	1.37	100.00	2.99	0.54	1.70	22.96	0.00	22.96	4.000	No	Yes	2.00
64	1.28	1.37	100.00	2.99	0.54	1.70	23.01	0.00	23.01	4.000	No	Yes	2.00
65	1.30	1.35	100.00	3.00	0.54	1.70	22.63	0.00	22.63	4.000	No	Yes	2.00
66	1.32	1.31	100.00	3.03	0.54	1.70	21.93	0.00	21.93	4.000	No	Yes	2.00
67	1.34	1.25	100.00	3.05	0.54	1.70	20.80	0.00	20.80	4.000	No	Yes	2.00
68	1.36	1.17	100.00	3.09	0.55	1.70	19.67	0.00	19.67	4.000	No	Yes	2.00
69	1.38	1.09	100.00	3.13	0.55	1.70	17.82	0.00	17.82	4.000	No	Yes	2.00
70	1.40	1.01	100.00	3.17	0.56	1.70	16.65	0.00	16.65	4.000	No	Yes	2.00
71	1.42	0.96	100.00	3.19	0.56	1.70	15.86	0.00	15.86	4.000	No	Yes	2.00
72	1.44	0.93	100.00	3.20	0.56	1.70	15.00	0.00	15.00	4.000	No	Yes	2.00
73	1.46	0.91	100.00	3.19	0.56	1.70	14.89	0.00	14.89	4.000	No	Yes	2.00
74	1.48	0.92	100.00	3.16	0.56	1.70	14.90	0.00	14.90	4.000	No	Yes	2.00
75	1.50	0.93	100.00	3.12	0.56	1.70	15.44	0.00	15.44	4.000	No	Yes	2.00
76	1.52	0.95	100.00	3.07	0.56	1.70	15.75	0.00	15.75	4.000	No	Yes	2.00
77	1.54	0.95	100.00	3.05	0.56	1.70	15.68	0.00	15.68	4.000	No	Yes	2.00
78	1.56	0.95	100.00	3.02	0.56	1.70	15.58	0.00	15.58	4.000	No	Yes	2.00
79	1.58	0.96	100.00	3.00	0.56	1.70	16.13	0.00	16.13	4.000	No	Yes	2.00
80	1.60	0.98	100.00	2.98	0.56	1.70	16.25	0.00	16.25	4.000	No	Yes	2.00
81	1.63	0.97	100.00	3.00	0.56	1.70	16.50	0.00	16.50	4.000	No	Yes	2.00
82	1.64	0.95	100.00	3.03	0.56	1.70	15.72	0.00	15.72	4.000	No	Yes	2.00
83	1.66	0.91	100.00	3.07	0.56	1.70	15.13	0.00	15.13	4.000	No	Yes	2.00
84	1.68	0.87	100.00	3.11	0.56	1.70	14.70	0.00	14.70	4.000	No	Yes	2.00
85	1.70	0.83	100.00	3.16	0.57	1.70	13.85	0.00	13.85	4.000	No	Yes	2.00
86	1.72	0.79	100.00	3.20	0.57	1.70	13.08	0.00	13.08	4.000	No	Yes	2.00
87	1.74	0.76	100.00	3.22	0.57	1.70	12.76	0.00	12.76	4.000	No	Yes	2.00
88	1.76	0.74	100.00	3.23	0.57	1.70	12.59	0.00	12.59	4.000	No	Yes	2.00
89	1.78	0.71	100.00	3.24	0.57	1.70	11.90	0.00	11.90	4.000	No	Yes	2.00
90	1.80	0.67	100.00	3.26	0.58	1.70	11.32	0.00	11.32	4.000	No	Yes	2.00
91	1.82	0.63	100.00	3.28	0.58	1.70	10.59	0.00	10.59	4.000	No	Yes	2.00
92	1.84	0.60	100.00	3.29	0.58	1.70	9.96	0.00	9.96	4.000	No	Yes	2.00
93	1.86	0.58	100.00	3.30	0.58	1.70	9.61	0.00	9.61	4.000	No	Yes	2.00
94	1.88	0.57	100.00	3.27	0.58	1.70	9.41	0.00	9.41	4.000	No	Yes	2.00
95	1.90	0.59	100.00	3.24	0.58	1.70	9.68	0.00	9.68	4.000	No	Yes	2.00
96	1.92	0.60	100.00	3.21	0.58	1.70	10.21	0.00	10.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	0.61	100.00	3.18	0.58	1.70	10.02	0.00	10.02	4.000	No	Yes	2.00
98	1.96	0.62	100.00	3.16	0.58	1.70	10.36	0.00	10.36	4.000	No	Yes	2.00
99	1.98	0.64	100.00	3.14	0.58	1.70	10.55	0.00	10.55	4.000	No	Yes	2.00
100	2.00	0.66	100.00	3.11	0.58	1.70	11.00	0.00	11.00	4.000	No	Yes	2.00
101	2.02	0.67	100.00	3.10	0.58	1.70	11.30	0.00	11.30	4.000	No	Yes	2.00
102	2.04	0.67	100.00	3.09	0.58	1.70	11.00	0.00	11.00	4.000	No	Yes	2.00
103	2.06	0.66	100.00	3.11	0.58	1.70	10.92	0.00	10.92	4.000	No	Yes	2.00
104	2.08	0.65	100.00	3.10	0.58	1.70	10.57	0.00	10.57	4.000	No	Yes	2.00
105	2.10	0.64	100.00	3.10	0.58	1.70	10.65	0.00	10.65	4.000	No	Yes	2.00
106	2.12	0.64	100.00	3.10	0.58	1.70	10.49	0.00	10.49	4.000	No	Yes	2.00
107	2.14	0.62	100.00	3.11	0.58	1.70	10.26	0.00	10.26	4.000	No	Yes	2.00
108	2.16	0.61	100.00	3.12	0.58	1.70	9.99	0.00	9.99	4.000	No	Yes	2.00
109	2.18	0.59	100.00	3.12	0.58	1.70	9.61	0.00	9.61	4.000	No	Yes	2.00
110	2.20	0.59	100.00	3.12	0.58	1.70	9.60	0.00	9.60	4.000	No	Yes	2.00
111	2.22	0.58	100.00	3.11	0.58	1.70	9.52	0.00	9.52	4.000	No	Yes	2.00
112	2.24	0.57	100.00	3.10	0.59	1.70	9.14	0.00	9.14	4.000	No	Yes	2.00
113	2.26	0.58	100.00	3.07	0.58	1.70	9.47	0.00	9.47	4.000	No	Yes	2.00
114	2.28	0.60	100.00	3.03	0.58	1.70	9.70	0.00	9.70	4.000	No	Yes	2.00
115	2.30	0.63	100.00	2.99	0.58	1.70	10.22	0.00	10.22	4.000	No	Yes	2.00
116	2.32	0.67	98.29	2.94	0.58	1.70	10.60	0.00	10.60	4.000	No	Yes	2.00
117	2.34	0.71	94.99	2.90	0.58	1.69	11.64	0.00	11.64	4.000	No	Yes	2.00
118	2.36	0.75	91.92	2.86	0.58	1.68	12.17	0.00	12.17	4.000	No	Yes	2.00
119	2.38	0.75	92.48	2.87	0.57	1.67	12.51	0.00	12.51	4.000	No	Yes	2.00
120	2.40	0.72	95.26	2.90	0.58	1.67	11.51	0.00	11.51	4.000	No	Yes	2.00
121	2.42	0.67	100.00	2.96	0.58	1.67	10.49	0.00	10.49	4.000	No	Yes	2.00
122	2.44	0.62	100.00	3.01	0.58	1.67	9.76	0.00	9.76	4.000	No	Yes	2.00
123	2.46	0.59	100.00	3.06	0.59	1.66	9.10	0.00	9.10	4.000	No	Yes	2.00
124	2.48	0.56	100.00	3.10	0.59	1.66	8.85	0.00	8.85	4.000	No	Yes	2.00
125	2.50	0.53	100.00	3.14	0.59	1.65	8.34	0.00	8.34	4.000	No	Yes	2.00
126	2.52	0.50	100.00	3.18	0.59	1.65	7.65	0.00	7.65	4.000	No	Yes	2.00
127	2.54	0.49	100.00	3.18	0.59	1.65	7.45	0.00	7.45	4.000	No	Yes	2.00
128	2.56	0.51	100.00	3.14	0.59	1.64	7.93	0.00	7.93	4.000	No	Yes	2.00
129	2.58	0.53	100.00	3.10	0.59	1.64	8.38	0.00	8.38	4.000	No	Yes	2.00
130	2.60	0.56	100.00	3.06	0.59	1.64	8.57	0.00	8.57	4.000	No	Yes	2.00
131	2.62	0.59	100.00	3.00	0.59	1.63	8.94	0.00	8.94	4.000	No	Yes	2.00
132	2.64	0.68	95.50	2.91	0.58	1.62	10.06	0.00	10.06	4.000	No	Yes	2.00
133	2.66	0.77	88.22	2.82	0.58	1.61	12.42	0.00	12.42	4.000	No	Yes	2.00
134	2.68	0.85	83.96	2.76	0.57	1.61	13.24	0.00	13.24	4.000	No	Yes	2.00
135	2.70	0.83	86.68	2.80	0.57	1.60	13.55	0.00	13.55	4.000	No	Yes	2.00
136	2.72	0.77	92.64	2.87	0.58	1.61	11.58	0.00	11.58	4.000	No	Yes	2.00
137	2.74	0.69	100.00	2.98	0.58	1.61	10.72	0.00	10.72	4.000	No	Yes	2.00
138	2.76	0.62	100.00	3.08	0.58	1.61	9.52	0.00	9.52	4.000	No	Yes	2.00
139	2.78	0.56	100.00	3.16	0.59	1.61	8.46	0.00	8.46	4.000	No	Yes	2.00
140	2.80	0.52	100.00	3.22	0.59	1.61	8.02	0.00	8.02	4.000	No	Yes	2.00
141	2.82	0.51	100.00	3.22	0.59	1.61	7.65	0.00	7.65	4.000	No	Yes	2.00
142	2.84	0.50	100.00	3.21	0.59	1.61	7.67	0.00	7.67	4.000	No	Yes	2.00
143	2.86	0.55	100.00	3.13	0.59	1.61	7.45	0.00	7.45	4.000	No	Yes	2.00
144	2.88	0.57	100.00	3.10	0.58	1.59	9.90	0.00	9.90	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	0.58	100.00	3.10	0.59	1.59	8.89	0.00	8.89	4.000	No	Yes	2.00
146	2.92	0.52	100.00	3.17	0.59	1.60	7.94	0.00	7.94	4.000	No	Yes	2.00
147	2.94	0.48	100.00	3.22	0.59	1.60	7.06	0.00	7.06	4.000	No	Yes	2.00
148	2.96	0.44	100.00	3.27	0.59	1.60	6.91	0.00	6.91	4.000	No	Yes	2.00
149	2.98	0.42	100.00	3.29	0.60	1.60	6.07	0.00	6.07	4.000	No	Yes	2.00
150	3.00	0.40	100.00	3.30	0.60	1.60	5.99	0.00	5.99	4.000	No	Yes	2.00
151	3.02	0.41	100.00	3.25	0.60	1.59	6.22	0.00	6.22	4.000	No	Yes	2.00
152	3.04	0.43	100.00	3.19	0.60	1.59	6.45	0.00	6.45	4.000	No	Yes	2.00
153	3.06	0.46	100.00	3.13	0.60	1.58	6.78	0.00	6.78	4.000	No	Yes	2.00
154	3.08	0.51	100.00	3.03	0.59	1.58	7.29	0.00	7.29	4.000	No	Yes	2.00
155	3.10	0.64	92.76	2.87	0.59	1.57	9.03	0.00	9.03	4.000	Yes	Yes	2.00
156	3.12	0.83	77.94	2.69	0.58	1.56	12.26	0.00	12.26	4.000	Yes	Yes	2.00
157	3.14	1.06	67.73	2.56	0.57	1.55	16.14	54.90	71.04	4.000	Yes	No	2.00
158	3.16	1.23	65.11	2.53	0.56	1.53	19.04	55.22	74.25	4.000	Yes	No	2.00
159	3.18	1.32	67.82	2.56	0.56	1.52	20.15	56.08	76.23	4.000	Yes	No	2.00
160	3.20	1.35	72.04	2.61	0.55	1.52	20.12	0.00	20.12	4.000	Yes	Yes	2.00
161	3.22	1.35	74.76	2.65	0.55	1.52	19.97	0.00	19.97	4.000	Yes	Yes	2.00
162	3.24	1.41	74.98	2.65	0.55	1.51	20.45	0.00	20.45	4.000	No	Yes	2.00
163	3.26	1.49	74.43	2.64	0.55	1.50	22.42	0.00	22.42	4.000	No	Yes	2.00
164	3.28	1.49	77.00	2.67	0.54	1.49	23.34	0.00	23.34	4.000	No	Yes	2.00
165	3.30	1.40	81.20	2.73	0.55	1.50	20.09	0.00	20.09	4.000	No	Yes	2.00
166	3.32	1.23	87.39	2.80	0.55	1.50	18.56	0.00	18.56	4.000	No	Yes	2.00
167	3.34	1.19	88.75	2.82	0.56	1.51	16.08	0.00	16.08	4.000	No	Yes	2.00
168	3.36	1.22	87.75	2.81	0.56	1.50	17.95	0.00	17.95	4.000	No	Yes	2.00
169	3.38	1.34	84.37	2.77	0.55	1.49	19.61	0.00	19.61	4.000	No	Yes	2.00
170	3.40	1.36	84.31	2.77	0.55	1.49	20.83	0.00	20.83	4.000	No	Yes	2.00
171	3.42	1.29	88.49	2.82	0.55	1.49	19.11	0.00	19.11	4.000	No	Yes	2.00
172	3.44	1.14	95.37	2.90	0.56	1.49	16.25	0.00	16.25	4.000	No	Yes	2.00
173	3.46	1.02	100.00	2.98	0.56	1.50	14.74	0.00	14.74	4.000	No	Yes	2.00
174	3.48	1.05	99.87	2.96	0.57	1.50	13.74	0.00	13.74	4.000	No	Yes	2.00
175	3.50	1.12	95.23	2.90	0.56	1.48	17.33	0.00	17.33	4.000	No	Yes	2.00
176	3.52	1.18	90.90	2.85	0.56	1.48	17.62	0.00	17.62	4.000	No	Yes	2.00
177	3.54	1.13	91.76	2.86	0.56	1.48	16.41	0.00	16.41	4.000	No	Yes	2.00
178	3.56	1.01	96.09	2.91	0.56	1.48	15.01	0.00	15.01	4.000	No	Yes	2.00
179	3.58	0.90	100.00	2.97	0.57	1.49	12.16	0.00	12.16	4.000	No	Yes	2.00
180	3.60	0.82	100.00	3.01	0.58	1.49	11.75	0.00	11.75	4.000	No	Yes	2.00
181	3.62	0.80	100.00	3.03	0.58	1.49	11.47	0.00	11.47	4.000	No	Yes	2.00
182	3.64	0.80	100.00	3.05	0.58	1.49	11.41	0.00	11.41	4.000	No	Yes	2.00
183	3.66	0.81	100.00	3.04	0.58	1.48	11.45	0.00	11.45	4.000	No	Yes	2.00
184	3.68	0.81	100.00	3.03	0.58	1.48	11.81	0.00	11.81	4.000	No	Yes	2.00
185	3.70	0.81	100.00	3.01	0.58	1.48	11.53	0.00	11.53	4.000	No	Yes	2.00
186	3.72	0.78	100.00	3.01	0.58	1.48	11.19	0.00	11.19	4.000	No	Yes	2.00
187	3.74	0.78	100.00	3.00	0.58	1.48	10.79	0.00	10.79	4.000	No	Yes	2.00
188	3.76	0.76	100.00	2.99	0.58	1.47	11.28	0.00	11.28	4.000	No	Yes	2.00
189	3.78	0.75	100.00	3.00	0.58	1.47	10.50	0.00	10.50	4.000	No	Yes	2.00
190	3.80	0.78	100.00	2.97	0.58	1.47	10.13	0.00	10.13	4.000	No	Yes	2.00
191	3.82	0.92	92.62	2.87	0.58	1.46	12.35	0.00	12.35	4.000	No	Yes	2.00
192	3.84	1.17	83.30	2.75	0.56	1.45	16.30	0.00	16.30	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	1.28	83.63	2.76	0.55	1.43	20.85	0.00	20.85	4.000	No	Yes	2.00
194	3.88	1.22	90.74	2.85	0.56	1.44	17.00	0.00	17.00	4.000	No	Yes	2.00
195	3.90	0.99	100.00	3.00	0.57	1.45	13.57	0.00	13.57	4.000	No	Yes	2.00
196	3.92	0.85	100.00	3.09	0.58	1.45	11.67	0.00	11.67	4.000	No	Yes	2.00
197	3.94	0.79	100.00	3.12	0.58	1.45	10.99	0.00	10.99	4.000	No	Yes	2.00
198	3.96	0.78	100.00	3.11	0.58	1.45	10.91	0.00	10.91	4.000	No	Yes	2.00
199	3.98	0.79	100.00	3.09	0.58	1.45	11.01	0.00	11.01	4.000	No	Yes	2.00
200	4.00	0.80	100.00	3.06	0.58	1.45	10.99	0.00	10.99	4.000	No	Yes	2.00
201	4.02	0.83	100.00	3.01	0.58	1.44	11.32	0.00	11.32	4.000	No	Yes	2.00
202	4.04	0.89	97.42	2.93	0.57	1.44	12.20	0.00	12.20	4.000	No	Yes	2.00
203	4.06	0.91	93.87	2.89	0.57	1.43	13.34	0.00	13.34	4.000	No	Yes	2.00
204	4.08	0.91	94.17	2.89	0.57	1.43	12.35	0.00	12.35	4.000	No	Yes	2.00
205	4.10	0.89	97.26	2.93	0.57	1.43	12.14	0.00	12.14	4.000	No	Yes	2.00
206	4.12	0.90	98.36	2.94	0.57	1.43	12.34	0.00	12.34	4.000	No	Yes	2.00
207	4.14	0.95	97.45	2.93	0.57	1.43	13.00	0.00	13.00	4.000	No	Yes	2.00
208	4.16	1.03	94.66	2.90	0.57	1.42	14.02	0.00	14.02	4.000	No	Yes	2.00
209	4.18	1.10	92.24	2.87	0.56	1.41	15.59	0.00	15.59	4.000	No	Yes	2.00
210	4.20	1.12	92.98	2.87	0.56	1.41	15.99	0.00	15.99	4.000	No	Yes	2.00
211	4.22	1.05	97.70	2.93	0.56	1.41	14.80	0.00	14.80	4.000	No	Yes	2.00
212	4.24	0.94	100.00	3.01	0.57	1.41	12.67	0.00	12.67	4.000	No	Yes	2.00
213	4.26	0.83	100.00	3.08	0.58	1.42	11.42	0.00	11.42	4.000	No	Yes	2.00
214	4.28	0.77	100.00	3.11	0.58	1.42	10.42	0.00	10.42	4.000	No	Yes	2.00
215	4.30	0.74	100.00	3.12	0.58	1.42	10.19	0.00	10.19	4.000	No	Yes	2.00
216	4.32	0.72	100.00	3.12	0.58	1.41	9.95	0.00	9.95	4.000	No	Yes	2.00
217	4.34	0.69	100.00	3.12	0.58	1.41	9.38	0.00	9.38	4.000	No	Yes	2.00
218	4.36	0.66	100.00	3.13	0.59	1.41	8.93	0.00	8.93	4.000	No	Yes	2.00
219	4.38	0.64	100.00	3.12	0.59	1.41	8.70	0.00	8.70	4.000	No	Yes	2.00
220	4.40	0.65	100.00	3.09	0.59	1.41	8.63	0.00	8.63	4.000	No	Yes	2.00
221	4.42	0.67	100.00	3.06	0.59	1.41	9.01	0.00	9.01	4.000	No	Yes	2.00
222	4.44	0.69	100.00	3.04	0.58	1.40	9.40	0.00	9.40	4.000	No	Yes	2.00
223	4.46	0.71	100.00	3.02	0.58	1.40	9.60	0.00	9.60	4.000	No	Yes	2.00
224	4.48	0.73	100.00	3.00	0.58	1.40	9.77	0.00	9.77	4.000	No	Yes	2.00
225	4.51	0.73	100.00	2.99	0.58	1.40	10.09	0.00	10.09	4.000	No	Yes	2.00
226	4.52	0.71	100.00	3.01	0.58	1.40	9.75	0.00	9.75	4.000	No	Yes	2.00
227	4.54	0.66	100.00	3.08	0.59	1.40	8.88	0.00	8.88	4.000	No	Yes	2.00
228	4.56	0.63	100.00	3.13	0.59	1.40	8.11	0.00	8.11	4.000	No	Yes	2.00
229	4.58	0.62	100.00	3.14	0.59	1.40	8.16	0.00	8.16	4.000	No	Yes	2.00
230	4.60	0.64	100.00	3.12	0.59	1.39	8.49	0.00	8.49	4.000	No	Yes	2.00
231	4.62	0.66	100.00	3.09	0.59	1.39	8.72	0.00	8.72	4.000	No	Yes	2.00
232	4.64	0.66	100.00	3.08	0.59	1.39	8.92	0.00	8.92	4.000	No	Yes	2.00
233	4.66	0.66	100.00	3.06	0.59	1.39	8.79	0.00	8.79	4.000	No	Yes	2.00
234	4.68	0.65	100.00	3.06	0.59	1.38	8.48	0.00	8.48	4.000	No	Yes	2.00
235	4.70	0.64	100.00	3.04	0.59	1.38	8.36	0.00	8.36	4.000	No	Yes	2.00
236	4.72	0.65	100.00	3.03	0.59	1.38	8.62	0.00	8.62	4.000	No	Yes	2.00
237	4.74	0.67	100.00	3.02	0.59	1.38	8.85	0.00	8.85	4.000	No	Yes	2.00
238	4.76	0.65	100.00	3.05	0.59	1.38	8.84	0.00	8.84	4.000	No	Yes	2.00
239	4.78	0.63	100.00	3.08	0.59	1.38	7.94	0.00	7.94	4.000	No	Yes	2.00
240	4.80	0.63	100.00	3.10	0.59	1.38	8.20	0.00	8.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	0.65	100.00	3.08	0.59	1.37	8.58	0.00	8.58	4.000	No	Yes	2.00
242	4.84	0.73	100.00	3.03	0.59	1.37	8.90	0.00	8.90	4.000	No	Yes	2.00
243	4.86	0.79	100.00	3.02	0.58	1.36	11.43	0.00	11.43	4.000	No	Yes	2.00
244	4.89	0.85	100.00	3.02	0.58	1.36	11.05	0.00	11.05	4.000	No	Yes	2.00
245	4.90	0.85	100.00	3.04	0.58	1.36	11.05	0.00	11.05	4.000	No	Yes	2.00
246	4.92	0.83	100.00	3.06	0.58	1.35	11.33	0.00	11.33	4.000	No	Yes	2.00
247	4.94	0.78	100.00	3.09	0.58	1.36	10.25	0.00	10.25	4.000	No	Yes	2.00
248	4.96	0.70	100.00	3.15	0.59	1.36	9.29	0.00	9.29	4.000	No	Yes	2.00
249	4.98	0.67	100.00	3.18	0.59	1.36	8.30	0.00	8.30	4.000	No	Yes	2.00
250	5.00	0.65	100.00	3.18	0.59	1.35	8.70	0.00	8.70	4.000	No	Yes	2.00
251	5.02	0.66	100.00	3.16	0.59	1.35	8.66	0.00	8.66	4.000	No	Yes	2.00
252	5.04	0.66	100.00	3.15	0.59	1.35	8.62	0.00	8.62	4.000	No	Yes	2.00
253	5.06	0.66	100.00	3.14	0.59	1.35	8.67	0.00	8.67	4.000	No	Yes	2.00
254	5.08	0.65	100.00	3.15	0.59	1.35	8.65	0.00	8.65	4.000	No	Yes	2.00
255	5.10	0.62	100.00	3.19	0.59	1.35	8.11	0.00	8.11	4.000	No	Yes	2.00
256	5.12	0.57	100.00	3.26	0.59	1.35	7.24	0.00	7.24	4.000	No	Yes	2.00
257	5.14	0.52	100.00	3.33	0.60	1.35	6.70	0.00	6.70	4.000	No	Yes	2.00
258	5.16	0.49	100.00	3.36	0.60	1.35	6.10	0.00	6.10	4.000	No	Yes	2.00
259	5.18	0.48	100.00	3.35	0.60	1.35	6.12	0.00	6.12	4.000	No	Yes	2.00
260	5.20	0.48	100.00	3.31	0.60	1.34	6.23	0.00	6.23	4.000	No	Yes	2.00
261	5.22	0.49	100.00	3.26	0.60	1.34	6.19	0.00	6.19	4.000	No	Yes	2.00
262	5.24	0.50	100.00	3.21	0.60	1.34	6.54	0.00	6.54	4.000	No	Yes	2.00
263	5.26	0.50	100.00	3.18	0.60	1.34	6.41	0.00	6.41	4.000	No	Yes	2.00
264	5.28	0.49	100.00	3.19	0.60	1.34	6.20	0.00	6.20	4.000	No	Yes	2.00
265	5.30	0.48	100.00	3.21	0.60	1.34	6.05	0.00	6.05	4.000	No	Yes	2.00
266	5.32	0.48	100.00	3.21	0.60	1.34	5.93	0.00	5.93	4.000	No	Yes	2.00
267	5.34	0.50	100.00	3.18	0.60	1.33	6.10	0.00	6.10	4.000	No	Yes	2.00
268	5.37	0.55	100.00	3.12	0.59	1.33	7.11	0.00	7.11	4.000	No	Yes	2.00
269	5.38	0.60	100.00	3.07	0.59	1.33	7.66	0.00	7.66	4.000	No	Yes	2.00
270	5.40	0.66	100.00	3.03	0.59	1.32	8.21	0.00	8.21	4.000	No	Yes	2.00
271	5.42	0.72	100.00	2.99	0.58	1.32	9.33	0.00	9.33	4.000	No	Yes	2.00
272	5.44	0.74	100.00	2.99	0.58	1.32	9.66	0.00	9.66	4.000	No	Yes	2.00
273	5.46	0.72	100.00	3.03	0.59	1.32	9.17	0.00	9.17	4.000	No	Yes	2.00
274	5.48	0.65	100.00	3.12	0.59	1.32	8.55	0.00	8.55	4.000	No	Yes	2.00
275	5.50	0.60	100.00	3.19	0.59	1.32	7.16	0.00	7.16	4.000	No	Yes	2.00
276	5.52	0.59	100.00	3.22	0.59	1.32	7.10	0.00	7.10	4.000	No	Yes	2.00
277	5.54	0.62	100.00	3.18	0.59	1.31	7.87	0.00	7.87	4.000	No	Yes	2.00
278	5.56	0.64	100.00	3.15	0.59	1.31	8.35	0.00	8.35	4.000	No	Yes	2.00
279	5.58	0.63	100.00	3.16	0.59	1.31	8.00	0.00	8.00	4.000	No	Yes	2.00
280	5.60	0.60	100.00	3.19	0.59	1.31	7.42	0.00	7.42	4.000	No	Yes	2.00
281	5.62	0.55	100.00	3.22	0.59	1.31	7.01	0.00	7.01	4.000	No	Yes	2.00
282	5.64	0.51	100.00	3.28	0.60	1.31	6.40	0.00	6.40	4.000	No	Yes	2.00
283	5.66	0.46	100.00	3.33	0.60	1.31	5.50	0.00	5.50	4.000	No	Yes	2.00
284	5.68	0.43	100.00	3.36	0.60	1.31	5.38	0.00	5.38	4.000	No	Yes	2.00
285	5.70	0.42	100.00	3.36	0.60	1.31	5.23	0.00	5.23	4.000	No	Yes	2.00
286	5.72	0.41	100.00	3.36	0.60	1.31	5.03	0.00	5.03	4.000	No	Yes	2.00
287	5.74	0.41	100.00	3.34	0.60	1.30	4.91	0.00	4.91	4.000	No	Yes	2.00
288	5.76	0.41	100.00	3.30	0.60	1.30	5.05	0.00	5.05	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	0.43	100.00	3.25	0.60	1.30	5.16	0.00	5.16	4.000	No	Yes	2.00
290	5.80	0.45	100.00	3.20	0.60	1.30	5.48	0.00	5.48	4.000	No	Yes	2.00
291	5.82	0.55	100.00	3.08	0.60	1.30	5.70	0.00	5.70	4.000	No	Yes	2.00
292	5.84	0.63	100.00	3.02	0.59	1.29	8.97	0.00	8.97	4.000	No	Yes	2.00
293	5.87	0.72	100.00	2.98	0.59	1.29	8.85	0.00	8.85	4.000	No	Yes	2.00
294	5.88	0.71	100.00	3.01	0.59	1.29	8.82	0.00	8.82	4.000	No	Yes	2.00
295	5.90	0.73	100.00	3.00	0.59	1.29	8.61	0.00	8.61	4.000	No	Yes	2.00
296	5.92	0.80	98.59	2.94	0.58	1.28	9.53	0.00	9.53	4.000	No	Yes	2.00
297	5.94	0.93	92.49	2.87	0.58	1.28	11.60	0.00	11.60	4.000	No	Yes	2.00
298	5.96	1.07	88.03	2.81	0.57	1.27	13.26	0.00	13.26	4.000	No	Yes	2.00
299	5.98	1.14	87.78	2.81	0.57	1.27	14.71	0.00	14.71	4.000	No	Yes	2.00
300	6.00	1.16	90.13	2.84	0.57	1.27	14.55	0.00	14.55	4.000	No	Yes	2.00
301	6.02	1.09	94.27	2.89	0.57	1.27	13.81	0.00	13.81	4.000	No	Yes	2.00
302	6.04	0.98	99.27	2.95	0.57	1.27	12.24	0.00	12.24	4.000	No	Yes	2.00
303	6.06	0.87	100.00	3.02	0.58	1.27	10.37	0.00	10.37	4.000	No	Yes	2.00
304	6.08	0.71	100.00	3.13	0.58	1.27	9.78	0.00	9.78	4.000	No	Yes	2.00
305	6.10	0.59	100.00	3.24	0.60	1.27	6.55	0.00	6.55	4.000	No	Yes	2.00
306	6.12	0.50	100.00	3.34	0.60	1.27	5.87	0.00	5.87	4.000	No	Yes	2.00
307	6.14	0.52	100.00	3.30	0.60	1.27	6.17	0.00	6.17	4.000	No	Yes	2.00
308	6.16	0.59	100.00	3.18	0.59	1.27	7.12	0.00	7.12	4.000	No	Yes	2.00
309	6.19	0.69	100.00	3.05	0.59	1.26	8.61	0.00	8.61	4.000	No	Yes	2.00
310	6.20	0.76	99.83	2.96	0.58	1.26	9.57	0.00	9.57	4.000	No	Yes	2.00
311	6.22	0.80	95.91	2.91	0.58	1.26	9.78	0.00	9.78	4.000	No	Yes	2.00
312	6.24	0.85	93.43	2.88	0.58	1.26	10.16	0.00	10.16	4.000	No	Yes	2.00
313	6.26	0.90	92.63	2.87	0.58	1.25	11.22	0.00	11.22	4.000	No	Yes	2.00
314	6.28	0.90	95.42	2.91	0.58	1.25	11.43	0.00	11.43	4.000	No	Yes	2.00
315	6.30	0.81	100.00	3.01	0.58	1.25	10.12	0.00	10.12	4.000	No	Yes	2.00
316	6.32	0.69	100.00	3.14	0.59	1.26	8.13	0.00	8.13	4.000	No	Yes	2.00
317	6.34	0.60	100.00	3.25	0.59	1.26	7.05	0.00	7.05	4.000	No	Yes	2.00
318	6.36	0.57	100.00	3.29	0.60	1.26	6.74	0.00	6.74	4.000	No	Yes	2.00
319	6.38	0.56	100.00	3.29	0.60	1.25	6.81	0.00	6.81	4.000	No	Yes	2.00
320	6.40	0.56	100.00	3.28	0.60	1.25	6.78	0.00	6.78	4.000	No	Yes	2.00
321	6.42	0.56	100.00	3.27	0.60	1.25	6.71	0.00	6.71	4.000	No	Yes	2.00
322	6.44	0.55	100.00	3.24	0.60	1.25	6.59	0.00	6.59	4.000	No	Yes	2.00
323	6.46	0.54	100.00	3.22	0.60	1.25	6.39	0.00	6.39	4.000	No	Yes	2.00
324	6.48	0.57	100.00	3.17	0.60	1.25	6.33	0.00	6.33	4.000	No	Yes	2.00
325	6.50	0.66	100.00	3.06	0.59	1.24	7.67	0.00	7.67	4.000	No	Yes	2.00
326	6.52	0.82	97.32	2.93	0.58	1.24	9.68	0.00	9.68	4.000	No	Yes	2.00
327	6.54	1.01	88.69	2.82	0.58	1.23	12.18	0.00	12.18	4.000	No	Yes	2.00
328	6.56	1.14	84.73	2.77	0.57	1.23	14.57	0.00	14.57	4.000	No	Yes	2.00
329	6.58	1.11	85.57	2.78	0.57	1.23	14.18	0.00	14.18	4.000	No	Yes	2.00
330	6.60	0.94	91.72	2.86	0.58	1.23	11.25	0.00	11.25	4.000	No	Yes	2.00
331	6.62	0.75	100.00	2.99	0.59	1.23	8.64	0.00	8.64	4.000	No	Yes	2.00
332	6.64	0.65	100.00	3.11	0.59	1.24	7.35	0.00	7.35	4.000	No	Yes	2.00
333	6.66	0.65	100.00	3.14	0.59	1.23	7.32	0.00	7.32	4.000	No	Yes	2.00
334	6.68	0.75	100.00	3.06	0.59	1.23	8.56	0.00	8.56	4.000	No	Yes	2.00
335	6.70	0.87	100.00	2.97	0.58	1.23	10.74	0.00	10.74	4.000	No	Yes	2.00
336	6.72	0.94	96.92	2.92	0.58	1.22	11.62	0.00	11.62	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	0.98	94.93	2.90	0.58	1.22	11.18	0.00	11.18	4.000	No	Yes	2.00
338	6.76	1.03	92.98	2.87	0.58	1.22	12.24	0.00	12.24	4.000	No	Yes	2.00
339	6.78	1.06	92.29	2.87	0.57	1.22	13.22	0.00	13.22	4.000	No	Yes	2.00
340	6.80	1.03	95.23	2.90	0.57	1.22	12.29	0.00	12.29	4.000	No	Yes	2.00
341	6.82	1.00	99.11	2.95	0.58	1.22	11.05	0.00	11.05	4.000	No	Yes	2.00
342	6.84	0.98	100.00	2.98	0.57	1.21	12.38	0.00	12.38	4.000	No	Yes	2.00
343	6.86	0.99	100.00	2.98	0.58	1.21	11.40	0.00	11.40	4.000	No	Yes	2.00
344	6.88	1.05	97.67	2.93	0.58	1.21	11.58	0.00	11.58	4.000	No	Yes	2.00
345	6.90	1.20	90.85	2.85	0.57	1.21	14.28	0.00	14.28	4.000	No	Yes	2.00
346	6.92	1.33	85.94	2.79	0.56	1.20	16.64	0.00	16.64	4.000	No	Yes	2.00
347	6.94	1.39	83.77	2.76	0.56	1.20	16.28	0.00	16.28	4.000	No	Yes	2.00
348	6.96	1.44	82.39	2.74	0.56	1.20	16.53	0.00	16.53	4.000	Yes	Yes	2.00
349	6.98	1.53	79.35	2.70	0.56	1.20	18.16	0.00	18.16	4.000	Yes	Yes	2.00
350	7.00	1.64	76.65	2.67	0.55	1.20	19.45	0.00	19.45	4.000	Yes	Yes	2.00
351	7.02	1.74	74.67	2.65	0.55	1.19	20.44	0.00	20.44	4.000	Yes	Yes	2.00
352	7.04	1.83	71.38	2.60	0.55	1.19	21.52	0.00	21.52	4.000	Yes	Yes	2.00
353	7.06	1.91	66.03	2.54	0.55	1.19	22.62	56.43	79.06	4.000	Yes	No	2.00
354	7.08	1.98	59.32	2.45	0.55	1.19	23.17	55.04	78.21	4.000	Yes	No	2.00
355	7.10	2.01	53.13	2.38	0.55	1.19	23.75	53.39	77.14	4.000	Yes	No	2.00
356	7.12	2.02	49.71	2.33	0.56	1.19	23.78	52.20	75.97	4.000	Yes	No	2.00
357	7.14	2.00	48.37	2.32	0.56	1.19	23.61	51.64	75.25	0.112	No	No	0.58
358	7.16	1.96	48.68	2.32	0.56	1.19	22.99	51.60	74.59	0.111	No	No	0.58
359	7.18	1.91	49.51	2.33	0.56	1.19	22.37	51.75	74.12	0.111	No	No	0.57
360	7.20	1.88	50.55	2.34	0.56	1.19	21.80	51.98	73.79	0.111	No	No	0.57
361	7.22	1.85	51.99	2.36	0.56	1.18	21.67	52.45	74.12	0.111	No	No	0.57
362	7.24	1.83	53.87	2.39	0.56	1.18	21.46	53.01	74.47	0.111	No	No	0.58
363	7.26	1.79	55.21	2.40	0.56	1.18	20.87	53.26	74.12	0.111	No	No	0.57
364	7.28	1.75	55.22	2.40	0.56	1.18	20.30	53.11	73.41	0.110	No	No	0.57
365	7.30	1.76	54.38	2.39	0.56	1.18	20.21	52.83	73.04	0.110	No	No	0.57
366	7.32	1.80	55.07	2.40	0.56	1.18	20.86	53.21	74.07	0.111	No	No	0.57
367	7.34	1.85	58.25	2.44	0.56	1.18	21.65	54.33	75.97	0.112	No	No	0.58
368	7.36	1.88	62.13	2.49	0.55	1.17	21.79	55.34	77.13	0.113	No	No	0.59
369	7.38	1.88	64.45	2.52	0.55	1.17	21.86	55.88	77.74	0.114	No	No	0.59
370	7.40	1.85	64.47	2.52	0.55	1.17	21.61	55.81	77.42	0.114	No	No	0.59
371	7.42	1.81	62.37	2.49	0.56	1.17	20.83	55.12	75.95	0.112	No	No	0.58
372	7.44	1.76	60.74	2.47	0.56	1.17	20.28	54.58	74.86	4.000	Yes	No	2.00
373	7.46	1.73	62.89	2.50	0.56	1.17	20.12	55.04	75.17	4.000	Yes	No	2.00
374	7.48	1.72	67.34	2.55	0.56	1.17	19.71	55.86	75.57	4.000	Yes	No	2.00
375	7.50	1.71	71.40	2.60	0.56	1.17	19.73	0.00	19.73	4.000	Yes	Yes	2.00
376	7.52	1.70	73.25	2.63	0.56	1.17	19.65	0.00	19.65	4.000	Yes	Yes	2.00
377	7.54	1.68	74.18	2.64	0.56	1.16	19.38	0.00	19.38	4.000	No	Yes	2.00
378	7.56	1.66	74.66	2.65	0.56	1.16	19.10	0.00	19.10	4.000	No	Yes	2.00
379	7.58	1.65	75.38	2.65	0.56	1.16	19.03	0.00	19.03	4.000	No	Yes	2.00
380	7.60	1.66	75.99	2.66	0.56	1.16	18.93	0.00	18.93	4.000	No	Yes	2.00
381	7.62	1.70	76.02	2.66	0.56	1.16	19.34	0.00	19.34	4.000	No	Yes	2.00
382	7.64	1.76	74.98	2.65	0.55	1.16	20.16	0.00	20.16	4.000	Yes	Yes	2.00
383	7.66	1.83	72.61	2.62	0.55	1.16	20.95	0.00	20.95	4.000	Yes	Yes	2.00
384	7.68	1.89	69.01	2.58	0.55	1.15	21.59	56.72	78.32	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	1.94	65.29	2.53	0.55	1.15	22.21	56.16	78.38	4.000	Yes	No	2.00
386	7.72	1.99	61.71	2.48	0.55	1.15	22.76	55.52	78.27	4.000	Yes	No	2.00
387	7.74	2.04	59.08	2.45	0.55	1.15	23.27	55.00	78.27	4.000	Yes	No	2.00
388	7.76	2.04	58.47	2.44	0.55	1.15	23.55	54.92	78.47	0.115	No	No	0.59
389	7.78	2.01	60.23	2.47	0.55	1.15	22.94	55.20	78.15	0.114	No	No	0.59
390	7.80	1.93	62.69	2.50	0.55	1.15	22.26	55.60	77.86	0.114	No	No	0.59
391	7.82	1.83	64.24	2.52	0.56	1.15	20.79	55.53	76.32	4.000	Yes	No	2.00
392	7.84	1.71	67.49	2.56	0.56	1.15	19.58	55.85	75.43	4.000	Yes	No	2.00
393	7.86	1.54	74.83	2.65	0.56	1.15	17.99	0.00	17.99	4.000	Yes	Yes	2.00
394	7.88	1.38	83.43	2.76	0.57	1.15	15.14	0.00	15.14	4.000	Yes	Yes	2.00
395	7.90	1.30	88.53	2.82	0.57	1.15	14.07	0.00	14.07	4.000	Yes	Yes	2.00
396	7.92	1.41	85.14	2.78	0.57	1.14	15.26	0.00	15.26	4.000	No	Yes	2.00
397	7.94	1.60	79.40	2.71	0.56	1.14	18.59	0.00	18.59	4.000	No	Yes	2.00
398	7.96	1.78	74.75	2.65	0.55	1.14	20.43	0.00	20.43	4.000	No	Yes	2.00
399	7.98	1.88	73.01	2.63	0.55	1.14	21.21	0.00	21.21	4.000	No	Yes	2.00
400	8.00	1.95	71.92	2.61	0.55	1.14	22.03	0.00	22.03	4.000	Yes	Yes	2.00
401	8.02	2.02	69.95	2.59	0.55	1.13	22.51	57.16	79.67	4.000	Yes	No	2.00
402	8.04	2.12	67.19	2.55	0.54	1.13	23.63	56.96	80.59	4.000	Yes	No	2.00
403	8.06	2.27	63.61	2.51	0.54	1.13	25.13	56.63	81.76	4.000	Yes	No	2.00
404	8.08	2.43	60.69	2.47	0.54	1.13	27.59	56.63	84.22	4.000	Yes	No	2.00
405	8.10	2.57	58.47	2.44	0.53	1.13	28.69	56.35	85.04	4.000	Yes	No	2.00
406	8.12	2.68	55.68	2.41	0.53	1.12	29.63	55.80	85.43	4.000	Yes	No	2.00
407	8.14	2.85	50.58	2.34	0.53	1.12	31.06	54.45	85.51	4.000	Yes	No	2.00
408	8.16	3.12	43.92	2.26	0.53	1.12	34.33	52.39	86.72	4.000	Yes	No	2.00
409	8.18	3.32	40.67	2.22	0.52	1.12	38.40	51.60	89.99	4.000	Yes	No	2.00
410	8.20	3.12	47.80	2.31	0.52	1.12	37.47	55.02	92.49	4.000	Yes	No	2.00
411	8.22	2.78	56.88	2.42	0.54	1.12	27.77	55.64	83.42	4.000	Yes	No	2.00
412	8.24	2.36	67.14	2.55	0.53	1.12	26.95	57.91	84.86	4.000	Yes	No	2.00
413	8.26	2.21	69.43	2.58	0.54	1.12	23.84	57.46	81.30	4.000	Yes	No	2.00
414	8.28	2.04	71.61	2.61	0.55	1.12	22.43	0.00	22.43	4.000	Yes	Yes	2.00
415	8.30	1.97	70.90	2.60	0.55	1.12	21.33	56.99	78.32	0.114	No	No	0.59
416	8.32	1.96	69.54	2.58	0.55	1.12	21.66	56.84	78.51	0.115	No	No	0.59
417	8.34	1.99	67.88	2.56	0.55	1.12	21.99	56.62	78.61	0.115	No	No	0.59
418	8.36	2.02	66.47	2.54	0.55	1.12	22.22	56.41	78.63	0.115	No	No	0.59
419	8.38	2.06	65.15	2.53	0.55	1.11	22.76	56.29	79.05	0.115	No	No	0.59
420	8.40	2.10	64.70	2.52	0.55	1.11	23.33	56.36	79.68	0.116	No	No	0.59
421	8.42	2.11	64.91	2.52	0.55	1.11	23.51	56.45	79.96	0.116	No	No	0.60
422	8.44	2.07	66.12	2.54	0.55	1.11	23.02	56.57	79.59	0.116	No	No	0.59
423	8.46	2.02	67.49	2.56	0.55	1.11	22.00	56.55	78.55	0.115	No	No	0.59
424	8.48	1.97	69.32	2.58	0.55	1.11	21.58	56.78	78.36	0.114	No	No	0.59
425	8.50	1.99	70.74	2.60	0.55	1.11	21.53	57.02	78.56	0.115	No	No	0.59
426	8.52	2.03	71.52	2.61	0.55	1.11	22.38	0.00	22.38	4.000	No	Yes	2.00
427	8.54	2.04	70.88	2.60	0.55	1.10	22.73	57.39	80.12	0.116	No	No	0.60
428	8.56	2.01	69.67	2.58	0.55	1.10	22.10	56.99	79.09	0.115	No	No	0.59
429	8.58	1.93	68.08	2.56	0.55	1.10	21.11	56.41	77.52	0.114	No	No	0.58
430	8.60	1.86	68.57	2.57	0.56	1.10	20.22	56.24	76.46	0.113	No	No	0.58
431	8.62	1.80	71.35	2.60	0.56	1.10	19.71	0.00	19.71	4.000	No	Yes	2.00
432	8.64	1.73	75.83	2.66	0.56	1.10	19.03	0.00	19.03	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	1.64	79.62	2.71	0.56	1.10	17.99	0.00	17.99	4.000	No	Yes	2.00
434	8.68	1.51	83.27	2.75	0.56	1.10	16.78	0.00	16.78	4.000	No	Yes	2.00
435	8.70	1.34	88.25	2.82	0.57	1.10	14.60	0.00	14.60	4.000	No	Yes	2.00
436	8.72	1.17	94.54	2.89	0.57	1.10	12.50	0.00	12.50	4.000	No	Yes	2.00
437	8.74	1.05	100.00	2.98	0.58	1.10	11.44	0.00	11.44	4.000	No	Yes	2.00
438	8.76	0.97	100.00	3.03	0.58	1.10	10.46	0.00	10.46	4.000	No	Yes	2.00
439	8.78	0.83	100.00	3.14	0.58	1.10	10.06	0.00	10.06	4.000	No	Yes	2.00
440	8.80	0.86	100.00	3.13	0.60	1.10	6.57	0.00	6.57	4.000	No	Yes	2.00
441	8.82	0.86	100.00	3.14	0.58	1.10	11.23	0.00	11.23	4.000	No	Yes	2.00
442	8.84	0.93	100.00	3.09	0.58	1.10	9.96	0.00	9.96	4.000	No	Yes	2.00
443	8.86	0.83	100.00	3.16	0.59	1.10	8.91	0.00	8.91	4.000	No	Yes	2.00
444	8.88	0.75	100.00	3.23	0.59	1.10	8.00	0.00	8.00	4.000	No	Yes	2.00
445	8.90	0.68	100.00	3.28	0.59	1.09	7.17	0.00	7.17	4.000	No	Yes	2.00
446	8.92	0.65	100.00	3.31	0.59	1.09	6.85	0.00	6.85	4.000	No	Yes	2.00
447	8.94	0.64	100.00	3.31	0.59	1.09	6.89	0.00	6.89	4.000	No	Yes	2.00
448	8.96	0.64	100.00	3.30	0.59	1.09	6.84	0.00	6.84	4.000	No	Yes	2.00
449	8.98	0.64	100.00	3.28	0.60	1.09	6.78	0.00	6.78	4.000	No	Yes	2.00
450	9.00	0.67	100.00	3.22	0.59	1.09	6.94	0.00	6.94	4.000	No	Yes	2.00
451	9.02	0.73	100.00	3.13	0.59	1.09	7.71	0.00	7.71	4.000	No	Yes	2.00
452	9.04	0.81	100.00	3.04	0.59	1.09	8.76	0.00	8.76	4.000	No	Yes	2.00
453	9.06	0.85	100.00	3.01	0.58	1.09	9.33	0.00	9.33	4.000	No	Yes	2.00
454	9.08	0.85	100.00	3.02	0.59	1.09	9.16	0.00	9.16	4.000	No	Yes	2.00
455	9.10	0.83	100.00	3.04	0.59	1.08	8.69	0.00	8.69	4.000	No	Yes	2.00
456	9.12	0.82	100.00	3.05	0.59	1.08	8.59	0.00	8.59	4.000	No	Yes	2.00
457	9.14	0.78	100.00	3.09	0.59	1.08	8.78	0.00	8.78	4.000	No	Yes	2.00
458	9.16	0.73	100.00	3.15	0.59	1.08	7.57	0.00	7.57	4.000	No	Yes	2.00
459	9.18	0.68	100.00	3.20	0.59	1.08	6.90	0.00	6.90	4.000	No	Yes	2.00
460	9.20	0.67	100.00	3.21	0.59	1.08	6.94	0.00	6.94	4.000	No	Yes	2.00
461	9.22	0.69	100.00	3.18	0.59	1.08	7.25	0.00	7.25	4.000	No	Yes	2.00
462	9.24	0.71	100.00	3.15	0.59	1.08	7.50	0.00	7.50	4.000	No	Yes	2.00
463	9.26	0.76	100.00	3.11	0.59	1.08	7.76	0.00	7.76	4.000	No	Yes	2.00
464	9.28	0.83	100.00	3.05	0.59	1.08	8.59	0.00	8.59	4.000	No	Yes	2.00
465	9.30	0.90	100.00	3.00	0.58	1.07	9.80	0.00	9.80	4.000	No	Yes	2.00
466	9.32	0.92	100.00	3.00	0.58	1.07	9.96	0.00	9.96	4.000	No	Yes	2.00
467	9.34	0.87	100.00	3.04	0.59	1.07	9.12	0.00	9.12	4.000	No	Yes	2.00
468	9.36	0.82	100.00	3.08	0.59	1.07	8.26	0.00	8.26	4.000	No	Yes	2.00
469	9.38	0.84	100.00	3.04	0.59	1.07	8.35	0.00	8.35	4.000	No	Yes	2.00
470	9.40	1.18	86.48	2.79	0.59	1.07	9.61	0.00	9.61	4.000	No	Yes	2.00
471	9.42	1.71	67.60	2.56	0.56	1.07	19.14	55.74	74.88	0.111	No	No	0.56
472	9.44	2.22	56.04	2.41	0.55	1.06	24.97	54.63	79.60	0.116	No	No	0.59
473	9.46	2.23	55.61	2.41	0.55	1.06	25.48	54.64	80.12	4.000	Yes	No	2.00
474	9.48	1.96	61.82	2.49	0.56	1.06	19.41	54.59	74.00	4.000	Yes	No	2.00
475	9.50	1.57	76.77	2.67	0.56	1.06	16.56	0.00	16.56	4.000	Yes	Yes	2.00
476	9.52	1.30	93.02	2.88	0.57	1.06	13.34	0.00	13.34	4.000	Yes	Yes	2.00
477	9.54	1.09	100.00	3.07	0.58	1.06	10.97	0.00	10.97	4.000	No	Yes	2.00
478	9.56	0.96	100.00	3.19	0.58	1.06	9.65	0.00	9.65	4.000	No	Yes	2.00
479	9.58	0.91	100.00	3.23	0.59	1.06	9.26	0.00	9.26	4.000	No	Yes	2.00
480	9.60	0.89	100.00	3.25	0.59	1.06	9.21	0.00	9.21	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	0.88	100.00	3.24	0.59	1.06	9.03	0.00	9.03	4.000	No	Yes	2.00
482	9.64	0.87	100.00	3.22	0.59	1.06	9.00	0.00	9.00	4.000	No	Yes	2.00
483	9.66	0.85	100.00	3.20	0.59	1.06	8.92	0.00	8.92	4.000	No	Yes	2.00
484	9.68	0.82	100.00	3.18	0.59	1.06	8.27	0.00	8.27	4.000	No	Yes	2.00
485	9.70	0.77	100.00	3.21	0.59	1.06	8.06	0.00	8.06	4.000	No	Yes	2.00
486	9.72	0.72	100.00	3.27	0.59	1.06	7.34	0.00	7.34	4.000	No	Yes	2.00
487	9.74	0.67	100.00	3.33	0.60	1.06	6.63	0.00	6.63	4.000	No	Yes	2.00
488	9.76	0.64	100.00	3.36	0.60	1.05	6.53	0.00	6.53	4.000	No	Yes	2.00
489	9.78	0.69	100.00	3.26	0.60	1.05	6.39	0.00	6.39	4.000	No	Yes	2.00
490	9.80	0.74	100.00	3.17	0.59	1.05	7.85	0.00	7.85	4.000	No	Yes	2.00
491	9.82	0.81	100.00	3.08	0.59	1.05	7.82	0.00	7.82	4.000	No	Yes	2.00
492	9.84	0.87	100.00	3.02	0.59	1.05	8.16	0.00	8.16	4.000	No	Yes	2.00
493	9.86	0.98	97.38	2.93	0.58	1.05	9.58	0.00	9.58	4.000	No	Yes	2.00
494	9.88	1.13	90.60	2.85	0.58	1.05	11.27	0.00	11.27	4.000	No	Yes	2.00
495	9.91	1.22	87.87	2.81	0.57	1.05	12.76	0.00	12.76	4.000	No	Yes	2.00
496	9.92	1.22	89.95	2.84	0.57	1.05	12.81	0.00	12.81	4.000	No	Yes	2.00
497	9.94	1.12	95.53	2.91	0.58	1.05	11.61	0.00	11.61	4.000	No	Yes	2.00
498	9.96	0.96	100.00	3.01	0.58	1.05	9.59	0.00	9.59	4.000	No	Yes	2.00
499	9.98	0.83	100.00	3.11	0.59	1.04	8.00	0.00	8.00	4.000	No	Yes	2.00
500	10.00	0.76	100.00	3.17	0.59	1.04	7.35	0.00	7.35	4.000	No	Yes	2.00
501	10.03	0.72	100.00	3.21	0.59	1.04	7.13	0.00	7.13	4.000	No	Yes	2.00
502	10.04	0.70	100.00	3.23	0.60	1.04	6.81	0.00	6.81	4.000	No	Yes	2.00
503	10.06	0.69	100.00	3.25	0.60	1.04	6.64	0.00	6.64	4.000	No	Yes	2.00
504	10.08	0.69	100.00	3.25	0.60	1.04	6.64	0.00	6.64	4.000	No	Yes	2.00
505	10.10	0.69	100.00	3.24	0.60	1.04	6.75	0.00	6.75	4.000	No	Yes	2.00
506	10.12	0.68	100.00	3.24	0.60	1.04	6.63	0.00	6.63	4.000	No	Yes	2.00
507	10.14	0.66	100.00	3.25	0.60	1.04	6.39	0.00	6.39	4.000	No	Yes	2.00
508	10.16	0.66	100.00	3.24	0.60	1.04	6.32	0.00	6.32	4.000	No	Yes	2.00
509	10.18	0.68	100.00	3.19	0.60	1.04	6.52	0.00	6.52	4.000	No	Yes	2.00
510	10.20	0.72	100.00	3.14	0.59	1.04	6.88	0.00	6.88	4.000	No	Yes	2.00
511	10.22	0.74	100.00	3.11	0.59	1.04	7.32	0.00	7.32	4.000	No	Yes	2.00
512	10.24	0.74	100.00	3.11	0.59	1.03	7.17	0.00	7.17	4.000	No	Yes	2.00
513	10.26	0.72	100.00	3.13	0.60	1.03	6.78	0.00	6.78	4.000	No	Yes	2.00
514	10.28	0.70	100.00	3.15	0.60	1.03	6.66	0.00	6.66	4.000	No	Yes	2.00
515	10.30	0.71	100.00	3.14	0.60	1.03	6.61	0.00	6.61	4.000	No	Yes	2.00
516	10.32	0.72	100.00	3.13	0.59	1.03	7.02	0.00	7.02	4.000	No	Yes	2.00
517	10.34	0.73	100.00	3.13	0.59	1.03	7.06	0.00	7.06	4.000	No	Yes	2.00
518	10.36	0.71	100.00	3.17	0.59	1.03	6.85	0.00	6.85	4.000	No	Yes	2.00
519	10.38	0.69	100.00	3.19	0.60	1.03	6.39	0.00	6.39	4.000	No	Yes	2.00
520	10.40	0.69	100.00	3.19	0.60	1.03	6.43	0.00	6.43	4.000	No	Yes	2.00
521	10.42	0.71	100.00	3.14	0.60	1.03	6.68	0.00	6.68	4.000	No	Yes	2.00
522	10.44	0.76	100.00	3.09	0.59	1.03	7.18	0.00	7.18	4.000	No	Yes	2.00
523	10.46	0.82	100.00	3.04	0.59	1.03	7.79	0.00	7.79	4.000	No	Yes	2.00
524	10.48	0.87	100.00	3.00	0.59	1.03	8.33	0.00	8.33	4.000	No	Yes	2.00
525	10.50	0.93	100.00	2.97	0.59	1.02	8.85	0.00	8.85	4.000	No	Yes	2.00
526	10.52	0.97	99.49	2.96	0.58	1.02	9.60	0.00	9.60	4.000	No	Yes	2.00
527	10.54	0.98	100.00	2.97	0.58	1.02	9.59	0.00	9.59	4.000	No	Yes	2.00
528	10.56	0.94	100.00	3.03	0.59	1.02	9.06	0.00	9.06	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	0.88	100.00	3.11	0.59	1.02	8.51	0.00	8.51	4.000	No	Yes	2.00
530	10.60	0.84	100.00	3.16	0.59	1.02	7.92	0.00	7.92	4.000	No	Yes	2.00
531	10.62	0.83	100.00	3.19	0.59	1.02	7.89	0.00	7.89	4.000	No	Yes	2.00
532	10.64	0.84	100.00	3.17	0.59	1.02	7.88	0.00	7.88	4.000	No	Yes	2.00
533	10.66	0.87	100.00	3.14	0.59	1.02	8.31	0.00	8.31	4.000	No	Yes	2.00
534	10.68	0.89	100.00	3.11	0.59	1.02	8.69	0.00	8.69	4.000	No	Yes	2.00
535	10.70	0.88	100.00	3.11	0.59	1.02	8.59	0.00	8.59	4.000	No	Yes	2.00
536	10.72	0.87	100.00	3.10	0.59	1.02	7.97	0.00	7.97	4.000	No	Yes	2.00
537	10.74	0.90	100.00	3.07	0.59	1.01	8.51	0.00	8.51	4.000	No	Yes	2.00
538	10.76	0.97	100.00	3.07	0.58	1.01	9.38	0.00	9.38	4.000	No	Yes	2.00
539	10.78	1.00	100.00	3.10	0.58	1.01	10.40	0.00	10.40	4.000	No	Yes	2.00
540	10.80	0.99	100.00	3.16	0.58	1.01	9.58	0.00	9.58	4.000	No	Yes	2.00
541	10.82	0.95	100.00	3.19	0.59	1.01	9.28	0.00	9.28	4.000	No	Yes	2.00
542	10.84	0.93	100.00	3.20	0.59	1.01	8.96	0.00	8.96	4.000	No	Yes	2.00
543	10.86	0.98	100.00	3.16	0.59	1.01	9.00	0.00	9.00	4.000	No	Yes	2.00
544	10.88	1.08	100.00	3.07	0.58	1.01	10.54	0.00	10.54	4.000	No	Yes	2.00
545	10.90	1.18	100.00	2.98	0.57	1.01	11.98	0.00	11.98	4.000	No	Yes	2.00
546	10.92	1.24	98.50	2.94	0.57	1.01	12.15	0.00	12.15	4.000	No	Yes	2.00
547	10.94	1.24	98.69	2.95	0.57	1.01	12.36	0.00	12.36	4.000	No	Yes	2.00
548	10.96	1.15	100.00	3.02	0.57	1.01	12.35	0.00	12.35	4.000	No	Yes	2.00
549	10.98	0.99	100.00	3.14	0.58	1.00	9.46	0.00	9.46	4.000	No	Yes	2.00
550	11.00	0.82	100.00	3.30	0.59	1.00	7.64	0.00	7.64	4.000	No	Yes	2.00
551	11.02	0.76	100.00	3.36	0.59	1.00	7.19	0.00	7.19	4.000	No	Yes	2.00
552	11.04	0.78	100.00	3.33	0.59	1.00	7.65	0.00	7.65	4.000	No	Yes	2.00
553	11.06	0.80	100.00	3.30	0.59	1.00	7.90	0.00	7.90	4.000	No	Yes	2.00
554	11.08	0.77	100.00	3.31	0.59	1.00	7.56	0.00	7.56	4.000	No	Yes	2.00
555	11.10	0.74	100.00	3.32	0.59	1.00	6.97	0.00	6.97	4.000	No	Yes	2.00
556	11.12	0.71	100.00	3.32	0.59	1.00	6.97	0.00	6.97	4.000	No	Yes	2.00
557	11.14	0.71	100.00	3.29	0.60	1.00	6.58	0.00	6.58	4.000	No	Yes	2.00
558	11.16	0.72	100.00	3.26	0.60	1.00	6.80	0.00	6.80	4.000	No	Yes	2.00
559	11.18	0.80	100.00	3.17	0.59	1.00	7.19	0.00	7.19	4.000	No	Yes	2.00
560	11.20	0.95	100.00	3.04	0.59	1.00	8.98	0.00	8.98	4.000	No	Yes	2.00
561	11.22	1.11	98.09	2.94	0.58	1.00	11.12	0.00	11.12	4.000	No	Yes	2.00
562	11.24	1.16	97.57	2.93	0.58	0.99	11.89	0.00	11.89	4.000	No	Yes	2.00
563	11.26	1.06	100.00	3.03	0.58	0.99	10.31	0.00	10.31	4.000	No	Yes	2.00
564	11.28	0.93	100.00	3.14	0.59	0.99	8.42	0.00	8.42	4.000	No	Yes	2.00
565	11.30	0.89	100.00	3.19	0.59	0.99	8.21	0.00	8.21	4.000	No	Yes	2.00
566	11.32	0.91	100.00	3.17	0.59	0.99	8.80	0.00	8.80	4.000	No	Yes	2.00
567	11.34	0.93	100.00	3.16	0.59	0.99	9.11	0.00	9.11	4.000	No	Yes	2.00
568	11.36	0.91	100.00	3.19	0.59	0.99	8.79	0.00	8.79	4.000	No	Yes	2.00
569	11.38	0.85	100.00	3.24	0.59	0.99	8.08	0.00	8.08	4.000	No	Yes	2.00
570	11.40	0.82	100.00	3.25	0.59	0.99	7.45	0.00	7.45	4.000	No	Yes	2.00
571	11.42	0.80	100.00	3.26	0.59	0.99	7.64	0.00	7.64	4.000	No	Yes	2.00
572	11.44	0.81	100.00	3.25	0.59	0.99	7.46	0.00	7.46	4.000	No	Yes	2.00
573	11.46	0.83	100.00	3.23	0.59	0.99	7.65	0.00	7.65	4.000	No	Yes	2.00
574	11.48	0.93	100.00	3.15	0.59	0.99	8.35	0.00	8.35	4.000	No	Yes	2.00
575	11.50	1.11	100.00	3.02	0.58	0.98	10.32	0.00	10.32	4.000	No	Yes	2.00
576	11.52	1.34	93.34	2.88	0.57	0.98	12.72	0.00	12.72	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	1.52	86.97	2.80	0.57	0.98	14.94	0.00	14.94	4.000	No	Yes	2.00
578	11.56	1.64	85.80	2.78	0.56	0.98	15.98	0.00	15.98	4.000	No	Yes	2.00
579	11.58	1.72	87.04	2.80	0.56	0.98	16.39	0.00	16.39	4.000	No	Yes	2.00
580	11.60	1.82	87.70	2.81	0.56	0.98	17.51	0.00	17.51	4.000	No	Yes	2.00
581	11.62	1.94	87.18	2.80	0.55	0.98	18.83	0.00	18.83	4.000	No	Yes	2.00
582	11.64	2.01	88.01	2.81	0.55	0.98	19.88	0.00	19.88	4.000	No	Yes	2.00
583	11.66	2.04	89.31	2.83	0.55	0.98	19.61	0.00	19.61	4.000	No	Yes	2.00
584	11.68	2.10	88.20	2.82	0.55	0.98	19.67	0.00	19.67	4.000	No	Yes	2.00
585	11.70	2.24	84.75	2.77	0.54	0.98	21.59	0.00	21.59	4.000	No	Yes	2.00
586	11.72	2.32	82.85	2.75	0.54	0.98	23.51	0.00	23.51	4.000	No	Yes	2.00
587	11.74	2.11	87.91	2.81	0.54	0.98	21.92	0.00	21.92	4.000	No	Yes	2.00
588	11.76	1.73	95.65	2.91	0.56	0.97	15.56	0.00	15.56	4.000	No	Yes	2.00
589	11.78	1.28	100.00	3.06	0.57	0.97	12.36	0.00	12.36	4.000	No	Yes	2.00
590	11.80	1.00	100.00	3.17	0.59	0.97	8.97	0.00	8.97	4.000	No	Yes	2.00
591	11.82	0.82	100.00	3.29	0.59	0.97	7.08	0.00	7.08	4.000	No	Yes	2.00
592	11.84	0.85	100.00	3.23	0.59	0.97	7.23	0.00	7.23	4.000	No	Yes	2.00
593	11.86	0.99	100.00	3.10	0.58	0.97	9.75	0.00	9.75	4.000	No	Yes	2.00
594	11.88	1.08	100.00	3.02	0.58	0.97	10.95	0.00	10.95	4.000	No	Yes	2.00
595	11.90	1.00	100.00	3.08	0.58	0.97	9.91	0.00	9.91	4.000	No	Yes	2.00
596	11.93	0.86	100.00	3.21	0.59	0.97	7.50	0.00	7.50	4.000	No	Yes	2.00
597	11.94	0.73	100.00	3.35	0.60	0.97	6.81	0.00	6.81	4.000	No	Yes	2.00
598	11.96	0.69	100.00	3.39	0.60	0.97	6.24	0.00	6.24	4.000	No	Yes	2.00
599	11.98	0.69	100.00	3.40	0.60	0.96	6.37	0.00	6.37	4.000	No	Yes	2.00
600	12.00	0.72	100.00	3.37	0.60	0.96	6.58	0.00	6.58	4.000	No	Yes	2.00
601	12.02	0.77	100.00	3.31	0.59	0.96	7.17	0.00	7.17	4.000	No	Yes	2.00
602	12.04	0.82	100.00	3.26	0.59	0.96	7.77	0.00	7.77	4.000	No	Yes	2.00
603	12.06	0.83	100.00	3.23	0.59	0.96	7.87	0.00	7.87	4.000	No	Yes	2.00
604	12.08	0.80	100.00	3.24	0.59	0.96	7.41	0.00	7.41	4.000	No	Yes	2.00
605	12.10	0.77	100.00	3.27	0.59	0.96	6.96	0.00	6.96	4.000	No	Yes	2.00
606	12.12	0.76	100.00	3.28	0.59	0.96	7.00	0.00	7.00	4.000	No	Yes	2.00
607	12.14	0.79	100.00	3.26	0.59	0.96	7.27	0.00	7.27	4.000	No	Yes	2.00
608	12.16	0.82	100.00	3.23	0.59	0.96	7.76	0.00	7.76	4.000	No	Yes	2.00
609	12.18	0.84	100.00	3.22	0.59	0.96	7.84	0.00	7.84	4.000	No	Yes	2.00
610	12.20	0.84	100.00	3.23	0.59	0.96	7.72	0.00	7.72	4.000	No	Yes	2.00
611	12.22	0.84	100.00	3.23	0.59	0.96	7.74	0.00	7.74	4.000	No	Yes	2.00
612	12.24	0.86	100.00	3.22	0.59	0.96	7.88	0.00	7.88	4.000	No	Yes	2.00
613	12.26	0.88	100.00	3.20	0.59	0.96	8.14	0.00	8.14	4.000	No	Yes	2.00
614	12.28	0.89	100.00	3.20	0.59	0.95	8.34	0.00	8.34	4.000	No	Yes	2.00
615	12.30	0.90	100.00	3.21	0.59	0.95	8.23	0.00	8.23	4.000	No	Yes	2.00
616	12.32	0.90	100.00	3.23	0.59	0.95	8.37	0.00	8.37	4.000	No	Yes	2.00
617	12.34	0.91	100.00	3.23	0.59	0.95	8.43	0.00	8.43	4.000	No	Yes	2.00
618	12.36	0.92	100.00	3.24	0.59	0.95	8.43	0.00	8.43	4.000	No	Yes	2.00
619	12.38	0.92	100.00	3.25	0.59	0.95	8.46	0.00	8.46	4.000	No	Yes	2.00
620	12.40	0.91	100.00	3.26	0.59	0.95	8.44	0.00	8.44	4.000	No	Yes	2.00
621	12.42	0.91	100.00	3.27	0.59	0.95	8.32	0.00	8.32	4.000	No	Yes	2.00
622	12.44	0.91	100.00	3.26	0.59	0.95	8.34	0.00	8.34	4.000	No	Yes	2.00
623	12.46	0.92	100.00	3.26	0.59	0.95	8.42	0.00	8.42	4.000	No	Yes	2.00
624	12.48	0.92	100.00	3.25	0.59	0.95	8.45	0.00	8.45	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
625	12.50	0.92	100.00	3.24	0.59	0.95	8.38	0.00	8.38	4.000	No	Yes	2.00
626	12.52	0.93	100.00	3.23	0.59	0.95	8.48	0.00	8.48	4.000	No	Yes	2.00
627	12.54	0.93	100.00	3.22	0.59	0.95	8.56	0.00	8.56	4.000	No	Yes	2.00
628	12.56	0.94	100.00	3.21	0.59	0.94	8.57	0.00	8.57	4.000	No	Yes	2.00
629	12.58	0.94	100.00	3.21	0.59	0.94	8.57	0.00	8.57	4.000	No	Yes	2.00
630	12.60	0.94	100.00	3.22	0.59	0.94	8.62	0.00	8.62	4.000	No	Yes	2.00
631	12.62	0.94	100.00	3.22	0.59	0.94	8.66	0.00	8.66	4.000	No	Yes	2.00
632	12.64	0.94	100.00	3.23	0.59	0.94	8.50	0.00	8.50	4.000	No	Yes	2.00
633	12.66	0.95	100.00	3.23	0.59	0.94	8.62	0.00	8.62	4.000	No	Yes	2.00
634	12.68	0.96	100.00	3.22	0.59	0.94	8.78	0.00	8.78	4.000	No	Yes	2.00
635	12.70	0.98	100.00	3.21	0.59	0.94	8.88	0.00	8.88	4.000	No	Yes	2.00
636	12.72	0.99	100.00	3.20	0.59	0.94	8.98	0.00	8.98	4.000	No	Yes	2.00
637	12.74	1.02	100.00	3.19	0.59	0.94	9.12	0.00	9.12	4.000	No	Yes	2.00
638	12.76	1.04	100.00	3.18	0.58	0.94	9.45	0.00	9.45	4.000	No	Yes	2.00
639	12.78	1.05	100.00	3.19	0.58	0.94	9.33	0.00	9.33	4.000	No	Yes	2.00
640	12.80	1.03	100.00	3.21	0.59	0.94	9.18	0.00	9.18	4.000	No	Yes	2.00
641	12.82	1.01	100.00	3.24	0.59	0.94	9.01	0.00	9.01	4.000	No	Yes	2.00
642	12.84	1.00	100.00	3.26	0.59	0.94	8.87	0.00	8.87	4.000	No	Yes	2.00
643	12.86	0.99	100.00	3.28	0.59	0.93	8.85	0.00	8.85	4.000	No	Yes	2.00
644	12.88	0.99	100.00	3.28	0.59	0.93	8.71	0.00	8.71	4.000	No	Yes	2.00
645	12.91	1.00	100.00	3.28	0.59	0.93	8.91	0.00	8.91	4.000	No	Yes	2.00
646	12.93	1.00	100.00	3.27	0.59	0.93	8.84	0.00	8.84	4.000	No	Yes	2.00
647	12.95	1.00	100.00	3.27	0.59	0.93	8.79	0.00	8.79	4.000	No	Yes	2.00
648	12.96	1.01	100.00	3.26	0.59	0.93	8.89	0.00	8.89	4.000	No	Yes	2.00
649	12.98	1.03	100.00	3.24	0.59	0.93	9.02	0.00	9.02	4.000	No	Yes	2.00
650	13.00	1.06	100.00	3.21	0.58	0.93	9.43	0.00	9.43	4.000	No	Yes	2.00
651	13.02	1.08	100.00	3.20	0.58	0.93	9.61	0.00	9.61	4.000	No	Yes	2.00
652	13.04	1.09	100.00	3.21	0.58	0.93	9.56	0.00	9.56	4.000	No	Yes	2.00
653	13.06	1.10	100.00	3.21	0.58	0.93	9.65	0.00	9.65	4.000	No	Yes	2.00
654	13.08	1.11	100.00	3.22	0.58	0.93	9.81	0.00	9.81	4.000	No	Yes	2.00
655	13.10	1.12	100.00	3.23	0.58	0.93	9.86	0.00	9.86	4.000	No	Yes	2.00
656	13.12	1.12	100.00	3.24	0.58	0.93	9.87	0.00	9.87	4.000	No	Yes	2.00
657	13.14	1.12	100.00	3.25	0.58	0.92	9.92	0.00	9.92	4.000	No	Yes	2.00
658	13.16	1.13	100.00	3.24	0.58	0.92	9.85	0.00	9.85	4.000	No	Yes	2.00
659	13.19	1.13	100.00	3.24	0.58	0.92	9.96	0.00	9.96	4.000	No	Yes	2.00
660	13.20	1.12	100.00	3.24	0.58	0.92	9.87	0.00	9.87	4.000	No	Yes	2.00
661	13.22	1.10	100.00	3.26	0.58	0.92	9.70	0.00	9.70	4.000	No	Yes	2.00
662	13.24	1.09	100.00	3.27	0.58	0.92	9.46	0.00	9.46	4.000	No	Yes	2.00
663	13.26	1.09	100.00	3.27	0.58	0.92	9.47	0.00	9.47	4.000	No	Yes	2.00
664	13.28	1.11	100.00	3.25	0.58	0.92	9.67	0.00	9.67	4.000	No	Yes	2.00
665	13.30	1.13	100.00	3.25	0.58	0.92	10.00	0.00	10.00	4.000	No	Yes	2.00
666	13.32	1.14	100.00	3.25	0.58	0.92	9.85	0.00	9.85	4.000	No	Yes	2.00
667	13.34	1.16	100.00	3.23	0.58	0.92	10.00	0.00	10.00	4.000	No	Yes	2.00
668	13.36	1.18	100.00	3.22	0.58	0.92	10.57	0.00	10.57	4.000	No	Yes	2.00
669	13.38	1.21	100.00	3.21	0.58	0.92	10.46	0.00	10.46	4.000	No	Yes	2.00
670	13.40	1.21	100.00	3.22	0.58	0.92	10.61	0.00	10.61	4.000	No	Yes	2.00
671	13.42	1.23	100.00	3.21	0.58	0.92	10.72	0.00	10.72	4.000	No	Yes	2.00
672	13.44	1.24	100.00	3.22	0.58	0.91	10.85	0.00	10.85	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
673	13.46	1.24	100.00	3.22	0.58	0.91	10.78	0.00	10.78	4.000	No	Yes	2.00
674	13.48	1.21	100.00	3.24	0.58	0.91	10.69	0.00	10.69	4.000	No	Yes	2.00
675	13.50	1.17	100.00	3.27	0.58	0.91	10.23	0.00	10.23	4.000	No	Yes	2.00
676	13.52	1.12	100.00	3.31	0.58	0.91	9.69	0.00	9.69	4.000	No	Yes	2.00
677	13.54	1.08	100.00	3.34	0.58	0.91	9.41	0.00	9.41	4.000	No	Yes	2.00
678	13.56	1.04	100.00	3.37	0.59	0.91	9.10	0.00	9.10	4.000	No	Yes	2.00
679	13.58	1.00	100.00	3.39	0.59	0.91	8.58	0.00	8.58	4.000	No	Yes	2.00
680	13.60	0.96	100.00	3.41	0.59	0.91	8.24	0.00	8.24	4.000	No	Yes	2.00
681	13.62	0.93	100.00	3.42	0.59	0.91	8.05	0.00	8.05	4.000	No	Yes	2.00
682	13.64	0.90	100.00	3.42	0.59	0.91	7.84	0.00	7.84	4.000	No	Yes	2.00
683	13.66	0.87	100.00	3.43	0.59	0.90	7.35	0.00	7.35	4.000	No	Yes	2.00
684	13.68	0.85	100.00	3.42	0.59	0.90	7.26	0.00	7.26	4.000	No	Yes	2.00
685	13.70	0.83	100.00	3.41	0.59	0.90	7.21	0.00	7.21	4.000	No	Yes	2.00
686	13.72	0.82	100.00	3.39	0.59	0.90	6.86	0.00	6.86	4.000	No	Yes	2.00
687	13.74	0.86	100.00	3.32	0.59	0.90	6.93	0.00	6.93	4.000	No	Yes	2.00
688	13.76	0.89	100.00	3.26	0.59	0.90	7.92	0.00	7.92	4.000	No	Yes	2.00
689	13.78	0.90	100.00	3.23	0.59	0.90	7.66	0.00	7.66	4.000	No	Yes	2.00
690	13.81	0.84	100.00	3.29	0.59	0.90	7.25	0.00	7.25	4.000	No	Yes	2.00
691	13.82	0.79	100.00	3.34	0.60	0.90	6.52	0.00	6.52	4.000	No	Yes	2.00
692	13.84	0.77	100.00	3.35	0.60	0.90	6.36	0.00	6.36	4.000	No	Yes	2.00
693	13.86	0.78	100.00	3.32	0.60	0.90	6.55	0.00	6.55	4.000	No	Yes	2.00
694	13.88	0.81	100.00	3.28	0.60	0.90	6.75	0.00	6.75	4.000	No	Yes	2.00
695	13.90	0.83	100.00	3.25	0.59	0.90	6.99	0.00	6.99	4.000	No	Yes	2.00
696	13.92	0.84	100.00	3.23	0.59	0.90	7.01	0.00	7.01	4.000	No	Yes	2.00
697	13.94	0.86	100.00	3.21	0.59	0.90	7.14	0.00	7.14	4.000	No	Yes	2.00
698	13.96	0.89	100.00	3.19	0.59	0.90	7.36	0.00	7.36	4.000	No	Yes	2.00
699	13.98	0.93	100.00	3.16	0.59	0.90	7.70	0.00	7.70	4.000	No	Yes	2.00
700	14.00	0.98	100.00	3.12	0.59	0.90	8.18	0.00	8.18	4.000	No	Yes	2.00
701	14.02	1.02	100.00	3.10	0.59	0.90	8.55	0.00	8.55	4.000	No	Yes	2.00
702	14.04	1.04	100.00	3.10	0.59	0.89	8.75	0.00	8.75	4.000	No	Yes	2.00
703	14.06	1.05	100.00	3.11	0.59	0.89	8.69	0.00	8.69	4.000	No	Yes	2.00
704	14.08	1.06	100.00	3.12	0.59	0.89	8.84	0.00	8.84	4.000	No	Yes	2.00
705	14.10	1.06	100.00	3.13	0.59	0.89	8.94	0.00	8.94	4.000	No	Yes	2.00
706	14.13	1.06	100.00	3.15	0.59	0.89	8.81	0.00	8.81	4.000	No	Yes	2.00
707	14.14	1.06	100.00	3.17	0.59	0.89	8.87	0.00	8.87	4.000	No	Yes	2.00
708	14.16	1.07	100.00	3.17	0.59	0.89	8.88	0.00	8.88	4.000	No	Yes	2.00
709	14.18	1.08	100.00	3.17	0.59	0.89	9.02	0.00	9.02	4.000	No	Yes	2.00
710	14.20	1.06	100.00	3.18	0.59	0.89	9.03	0.00	9.03	4.000	No	Yes	2.00
711	14.22	1.02	100.00	3.22	0.59	0.89	8.47	0.00	8.47	4.000	No	Yes	2.00
712	14.24	0.96	100.00	3.28	0.59	0.89	7.97	0.00	7.97	4.000	No	Yes	2.00
713	14.26	0.91	100.00	3.32	0.59	0.89	7.54	0.00	7.54	4.000	No	Yes	2.00
714	14.28	0.86	100.00	3.36	0.59	0.89	7.10	0.00	7.10	4.000	No	Yes	2.00
715	14.30	0.81	100.00	3.39	0.60	0.89	6.62	0.00	6.62	4.000	No	Yes	2.00
716	14.32	0.78	100.00	3.40	0.60	0.88	6.30	0.00	6.30	4.000	No	Yes	2.00
717	14.34	0.77	100.00	3.38	0.60	0.88	6.24	0.00	6.24	4.000	No	Yes	2.00
718	14.36	0.78	100.00	3.34	0.60	0.88	6.41	0.00	6.41	4.000	No	Yes	2.00
719	14.38	0.81	100.00	3.28	0.60	0.88	6.56	0.00	6.56	4.000	No	Yes	2.00
720	14.40	0.84	100.00	3.23	0.59	0.88	6.86	0.00	6.86	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
721	14.42	0.86	100.00	3.20	0.59	0.88	7.09	0.00	7.09	4.000	No	Yes	2.00
722	14.44	0.86	100.00	3.20	0.59	0.88	7.09	0.00	7.09	4.000	No	Yes	2.00
723	14.46	0.85	100.00	3.23	0.60	0.88	6.79	0.00	6.79	4.000	No	Yes	2.00
724	14.48	0.84	100.00	3.24	0.59	0.88	6.82	0.00	6.82	4.000	No	Yes	2.00
725	14.50	0.87	100.00	3.22	0.59	0.88	6.94	0.00	6.94	4.000	No	Yes	2.00
726	14.52	0.89	100.00	3.20	0.59	0.88	7.33	0.00	7.33	4.000	No	Yes	2.00
727	14.54	0.90	100.00	3.19	0.59	0.88	7.30	0.00	7.30	4.000	No	Yes	2.00
728	14.56	0.90	100.00	3.18	0.59	0.88	7.16	0.00	7.16	4.000	No	Yes	2.00
729	14.58	0.93	100.00	3.16	0.59	0.88	7.42	0.00	7.42	4.000	No	Yes	2.00
730	14.60	0.96	100.00	3.13	0.59	0.88	8.02	0.00	8.02	4.000	No	Yes	2.00
731	14.62	0.95	100.00	3.15	0.59	0.88	7.86	0.00	7.86	4.000	No	Yes	2.00
732	14.64	0.90	100.00	3.20	0.59	0.88	7.17	0.00	7.17	4.000	No	Yes	2.00
733	14.66	0.85	100.00	3.27	0.60	0.88	6.79	0.00	6.79	4.000	No	Yes	2.00
734	14.68	0.83	100.00	3.28	0.60	0.88	6.54	0.00	6.54	4.000	No	Yes	2.00
735	14.70	0.92	100.00	3.21	0.60	0.88	6.81	0.00	6.81	4.000	No	Yes	2.00
736	14.72	1.30	100.00	2.97	0.59	0.88	8.86	0.00	8.86	4.000	No	Yes	2.00
737	14.74	1.79	86.25	2.79	0.56	0.88	17.01	0.00	17.01	4.000	No	Yes	2.00
738	14.76	2.27	78.08	2.69	0.55	0.88	20.24	0.00	20.24	4.000	No	Yes	2.00
739	14.78	2.38	78.02	2.69	0.55	0.88	21.89	0.00	21.89	4.000	No	Yes	2.00
740	14.80	2.37	80.62	2.72	0.55	0.88	20.09	0.00	20.09	4.000	No	Yes	2.00
741	14.82	2.39	81.68	2.73	0.55	0.88	19.93	0.00	19.93	4.000	No	Yes	2.00
742	14.84	2.60	78.47	2.69	0.54	0.88	22.29	0.00	22.29	4.000	No	Yes	2.00
743	14.86	2.77	75.27	2.65	0.54	0.88	25.33	0.00	25.33	4.000	No	Yes	2.00
744	14.88	2.75	74.83	2.65	0.54	0.88	24.34	0.00	24.34	4.000	No	Yes	2.00
745	14.90	2.47	79.28	2.70	0.55	0.88	21.48	0.00	21.48	4.000	No	Yes	2.00
746	14.92	2.18	85.87	2.79	0.56	0.88	18.00	0.00	18.00	4.000	No	Yes	2.00
747	14.94	2.02	91.09	2.85	0.56	0.87	16.55	0.00	16.55	4.000	No	Yes	2.00
748	14.96	2.08	89.68	2.83	0.56	0.87	17.26	0.00	17.26	4.000	No	Yes	2.00
749	14.98	2.16	87.94	2.81	0.55	0.88	19.64	0.00	19.64	4.000	No	Yes	2.00
750	15.00	2.06	91.45	2.86	0.55	0.87	18.54	0.00	18.54	4.000	No	Yes	2.00
751	15.02	1.81	100.00	2.97	0.56	0.87	14.86	0.00	14.86	4.000	No	Yes	2.00
752	15.04	1.51	100.00	3.10	0.57	0.87	12.96	0.00	12.96	4.000	No	Yes	2.00
753	15.06	1.38	100.00	3.16	0.58	0.87	10.70	0.00	10.70	4.000	No	Yes	2.00
754	15.08	1.42	100.00	3.12	0.58	0.87	11.45	0.00	11.45	4.000	No	Yes	2.00
755	15.10	1.59	100.00	3.02	0.57	0.87	13.78	0.00	13.78	4.000	No	Yes	2.00
756	15.12	1.68	100.00	2.98	0.56	0.87	14.92	0.00	14.92	4.000	No	Yes	2.00
757	15.14	1.65	100.00	2.99	0.57	0.87	14.03	0.00	14.03	4.000	No	Yes	2.00
758	15.17	1.60	100.00	3.01	0.57	0.87	12.88	0.00	12.88	4.000	No	Yes	2.00
759	15.18	1.59	100.00	3.01	0.57	0.87	13.52	0.00	13.52	4.000	No	Yes	2.00
760	15.20	1.54	100.00	3.04	0.57	0.87	13.72	0.00	13.72	4.000	No	Yes	2.00
761	15.22	1.38	100.00	3.13	0.58	0.86	11.58	0.00	11.58	4.000	No	Yes	2.00
762	15.24	1.20	100.00	3.24	0.58	0.86	9.50	0.00	9.50	4.000	No	Yes	2.00
763	15.26	1.06	100.00	3.31	0.59	0.86	8.93	0.00	8.93	4.000	No	Yes	2.00
764	15.28	0.98	100.00	3.36	0.59	0.86	7.92	0.00	7.92	4.000	No	Yes	2.00
765	15.30	0.91	100.00	3.40	0.59	0.86	7.35	0.00	7.35	4.000	No	Yes	2.00
766	15.32	0.90	100.00	3.39	0.59	0.86	7.26	0.00	7.26	4.000	No	Yes	2.00
767	15.34	0.89	100.00	3.36	0.59	0.86	7.45	0.00	7.45	4.000	No	Yes	2.00
768	15.36	0.89	100.00	3.34	0.59	0.86	7.25	0.00	7.25	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
769	15.38	0.87	100.00	3.34	0.59	0.85	7.09	0.00	7.09	4.000	No	Yes	2.00
770	15.40	0.86	100.00	3.33	0.59	0.85	7.06	0.00	7.06	4.000	No	Yes	2.00
771	15.42	0.86	100.00	3.32	0.59	0.85	7.00	0.00	7.00	4.000	No	Yes	2.00
772	15.44	0.87	100.00	3.31	0.59	0.85	7.05	0.00	7.05	4.000	No	Yes	2.00
773	15.46	0.88	100.00	3.29	0.59	0.85	7.14	0.00	7.14	4.000	No	Yes	2.00
774	15.48	0.90	100.00	3.27	0.59	0.85	7.39	0.00	7.39	4.000	No	Yes	2.00
775	15.50	0.93	100.00	3.24	0.59	0.85	7.56	0.00	7.56	4.000	No	Yes	2.00
776	15.52	0.96	100.00	3.22	0.59	0.85	7.92	0.00	7.92	4.000	No	Yes	2.00
777	15.54	0.97	100.00	3.22	0.59	0.85	7.93	0.00	7.93	4.000	No	Yes	2.00
778	15.56	0.95	100.00	3.24	0.59	0.85	7.79	0.00	7.79	4.000	No	Yes	2.00
779	15.58	0.93	100.00	3.27	0.59	0.85	7.58	0.00	7.58	4.000	No	Yes	2.00
780	15.60	0.92	100.00	3.29	0.59	0.85	7.41	0.00	7.41	4.000	No	Yes	2.00
781	15.62	0.92	100.00	3.31	0.59	0.85	7.54	0.00	7.54	4.000	No	Yes	2.00
782	15.64	0.92	100.00	3.31	0.59	0.85	7.46	0.00	7.46	4.000	No	Yes	2.00
783	15.66	0.91	100.00	3.33	0.59	0.85	7.36	0.00	7.36	4.000	No	Yes	2.00

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.44	2.00	0.00	9.78	0.02	0.00
0.46	2.00	0.00	9.77	0.02	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.59	2.00	0.00	9.71	0.03	0.00	0.60	2.00	0.00	9.70	0.01	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.04	2.00	0.00	9.48	0.02	0.00
1.06	2.00	0.00	9.47	0.02	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.10	2.00	0.00	9.45	0.02	0.00	1.12	2.00	0.00	9.44	0.02	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.16	2.00	0.00	9.42	0.02	0.00
1.18	2.00	0.00	9.41	0.02	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.25	2.00	0.00	9.38	0.03	0.00
1.26	2.00	0.00	9.37	0.01	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.63	2.00	0.00	9.19	0.03	0.00	1.64	2.00	0.00	9.18	0.01	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.14	2.00	0.00	8.93	0.02	0.00	2.16	2.00	0.00	8.92	0.02	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.08	2.00	0.00	8.46	0.02	0.00
3.10	2.00	0.00	8.45	0.02	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.14	2.00	0.00	8.43	0.02	0.00	3.16	2.00	0.00	8.42	0.02	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.04	2.00	0.00	7.98	0.02	0.00
4.06	2.00	0.00	7.97	0.02	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	2.00	0.00	7.87	0.02	0.00	4.28	2.00	0.00	7.86	0.02	0.00
4.30	2.00	0.00	7.85	0.02	0.00	4.32	2.00	0.00	7.84	0.02	0.00
4.34	2.00	0.00	7.83	0.02	0.00	4.36	2.00	0.00	7.82	0.02	0.00
4.38	2.00	0.00	7.81	0.02	0.00	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.48	2.00	0.00	7.76	0.02	0.00
4.51	2.00	0.00	7.75	0.03	0.00	4.52	2.00	0.00	7.74	0.01	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.89	2.00	0.00	7.56	0.03	0.00
4.90	2.00	0.00	7.55	0.01	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.37	2.00	0.00	7.32	0.03	0.00
5.38	2.00	0.00	7.31	0.01	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.87	2.00	0.00	7.07	0.03	0.00	5.88	2.00	0.00	7.06	0.01	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.98	2.00	0.00	7.01	0.02	0.00	6.00	2.00	0.00	7.00	0.02	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.19	2.00	0.00	6.91	0.03	0.00	6.20	2.00	0.00	6.90	0.01	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	2.00	0.00	6.80	0.02	0.00
6.42	2.00	0.00	6.79	0.02	0.00	6.44	2.00	0.00	6.78	0.02	0.00
6.46	2.00	0.00	6.77	0.02	0.00	6.48	2.00	0.00	6.76	0.02	0.00
6.50	2.00	0.00	6.75	0.02	0.00	6.52	2.00	0.00	6.74	0.02	0.00
6.54	2.00	0.00	6.73	0.02	0.00	6.56	2.00	0.00	6.72	0.02	0.00
6.58	2.00	0.00	6.71	0.02	0.00	6.60	2.00	0.00	6.70	0.02	0.00
6.62	2.00	0.00	6.69	0.02	0.00	6.64	2.00	0.00	6.68	0.02	0.00
6.66	2.00	0.00	6.67	0.02	0.00	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.84	2.00	0.00	6.58	0.02	0.00
6.86	2.00	0.00	6.57	0.02	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	0.58	0.42	6.43	0.02	0.05	7.16	0.58	0.42	6.42	0.02	0.05
7.18	0.57	0.43	6.41	0.02	0.05	7.20	0.57	0.43	6.40	0.02	0.05
7.22	0.57	0.43	6.39	0.02	0.05	7.24	0.58	0.42	6.38	0.02	0.05
7.26	0.57	0.43	6.37	0.02	0.05	7.28	0.57	0.43	6.36	0.02	0.05
7.30	0.57	0.43	6.35	0.02	0.05	7.32	0.57	0.43	6.34	0.02	0.05
7.34	0.58	0.42	6.33	0.02	0.05	7.36	0.59	0.41	6.32	0.02	0.05
7.38	0.59	0.41	6.31	0.02	0.05	7.40	0.59	0.41	6.30	0.02	0.05
7.42	0.58	0.42	6.29	0.02	0.05	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	0.59	0.41	6.12	0.02	0.05
7.78	0.59	0.41	6.11	0.02	0.05	7.80	0.59	0.41	6.10	0.02	0.05
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.98	2.00	0.00	6.01	0.02	0.00	8.00	2.00	0.00	6.00	0.02	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.16	2.00	0.00	5.92	0.02	0.00
8.18	2.00	0.00	5.91	0.02	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	0.59	0.41	5.85	0.02	0.05	8.32	0.59	0.41	5.84	0.02	0.05
8.34	0.59	0.41	5.83	0.02	0.05	8.36	0.59	0.41	5.82	0.02	0.05
8.38	0.59	0.41	5.81	0.02	0.05	8.40	0.59	0.41	5.80	0.02	0.05
8.42	0.60	0.40	5.79	0.02	0.05	8.44	0.59	0.41	5.78	0.02	0.05
8.46	0.59	0.41	5.77	0.02	0.05	8.48	0.59	0.41	5.76	0.02	0.05
8.50	0.59	0.41	5.75	0.02	0.05	8.52	2.00	0.00	5.74	0.02	0.00
8.54	0.60	0.40	5.73	0.02	0.05	8.56	0.59	0.41	5.72	0.02	0.05
8.58	0.58	0.42	5.71	0.02	0.05	8.60	0.58	0.42	5.70	0.02	0.05
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	2.00	0.00	5.66	0.02	0.00
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.80	2.00	0.00	5.60	0.02	0.00
8.82	2.00	0.00	5.59	0.02	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.00	2.00	0.00	5.50	0.02	0.00
9.02	2.00	0.00	5.49	0.02	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	0.56	0.44	5.29	0.02	0.05	9.44	0.59	0.41	5.28	0.02	0.04
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.91	2.00	0.00	5.05	0.03	0.00	9.92	2.00	0.00	5.04	0.01	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.03	2.00	0.00	4.99	0.03	0.00	10.04	2.00	0.00	4.98	0.01	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	2.00	0.00	4.96	0.02	0.00
10.10	2.00	0.00	4.95	0.02	0.00	10.12	2.00	0.00	4.94	0.02	0.00
10.14	2.00	0.00	4.93	0.02	0.00	10.16	2.00	0.00	4.92	0.02	0.00
10.18	2.00	0.00	4.91	0.02	0.00	10.20	2.00	0.00	4.90	0.02	0.00
10.22	2.00	0.00	4.89	0.02	0.00	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	2.00	0.00	4.72	0.02	0.00
10.58	2.00	0.00	4.71	0.02	0.00	10.60	2.00	0.00	4.70	0.02	0.00
10.62	2.00	0.00	4.69	0.02	0.00	10.64	2.00	0.00	4.68	0.02	0.00
10.66	2.00	0.00	4.67	0.02	0.00	10.68	2.00	0.00	4.66	0.02	0.00
10.70	2.00	0.00	4.65	0.02	0.00	10.72	2.00	0.00	4.64	0.02	0.00
10.74	2.00	0.00	4.63	0.02	0.00	10.76	2.00	0.00	4.62	0.02	0.00
10.78	2.00	0.00	4.61	0.02	0.00	10.80	2.00	0.00	4.60	0.02	0.00
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.90	2.00	0.00	4.55	0.02	0.00	10.92	2.00	0.00	4.54	0.02	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	2.00	0.00	4.42	0.02	0.00
11.18	2.00	0.00	4.41	0.02	0.00	11.20	2.00	0.00	4.40	0.02	0.00
11.22	2.00	0.00	4.39	0.02	0.00	11.24	2.00	0.00	4.38	0.02	0.00
11.26	2.00	0.00	4.37	0.02	0.00	11.28	2.00	0.00	4.36	0.02	0.00
11.30	2.00	0.00	4.35	0.02	0.00	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	2.00	0.00	4.19	0.02	0.00	11.64	2.00	0.00	4.18	0.02	0.00
11.66	2.00	0.00	4.17	0.02	0.00	11.68	2.00	0.00	4.16	0.02	0.00
11.70	2.00	0.00	4.15	0.02	0.00	11.72	2.00	0.00	4.14	0.02	0.00
11.74	2.00	0.00	4.13	0.02	0.00	11.76	2.00	0.00	4.12	0.02	0.00
11.78	2.00	0.00	4.11	0.02	0.00	11.80	2.00	0.00	4.10	0.02	0.00
11.82	2.00	0.00	4.09	0.02	0.00	11.84	2.00	0.00	4.08	0.02	0.00
11.86	2.00	0.00	4.07	0.02	0.00	11.88	2.00	0.00	4.06	0.02	0.00
11.90	2.00	0.00	4.05	0.02	0.00	11.93	2.00	0.00	4.04	0.03	0.00
11.94	2.00	0.00	4.03	0.01	0.00	11.96	2.00	0.00	4.02	0.02	0.00
11.98	2.00	0.00	4.01	0.02	0.00	12.00	2.00	0.00	4.00	0.02	0.00
12.02	2.00	0.00	3.99	0.02	0.00	12.04	2.00	0.00	3.98	0.02	0.00
12.06	2.00	0.00	3.97	0.02	0.00	12.08	2.00	0.00	3.96	0.02	0.00
12.10	2.00	0.00	3.95	0.02	0.00	12.12	2.00	0.00	3.94	0.02	0.00
12.14	2.00	0.00	3.93	0.02	0.00	12.16	2.00	0.00	3.92	0.02	0.00
12.18	2.00	0.00	3.91	0.02	0.00	12.20	2.00	0.00	3.90	0.02	0.00
12.22	2.00	0.00	3.89	0.02	0.00	12.24	2.00	0.00	3.88	0.02	0.00
12.26	2.00	0.00	3.87	0.02	0.00	12.28	2.00	0.00	3.86	0.02	0.00
12.30	2.00	0.00	3.85	0.02	0.00	12.32	2.00	0.00	3.84	0.02	0.00
12.34	2.00	0.00	3.83	0.02	0.00	12.36	2.00	0.00	3.82	0.02	0.00
12.38	2.00	0.00	3.81	0.02	0.00	12.40	2.00	0.00	3.80	0.02	0.00
12.42	2.00	0.00	3.79	0.02	0.00	12.44	2.00	0.00	3.78	0.02	0.00
12.46	2.00	0.00	3.77	0.02	0.00	12.48	2.00	0.00	3.76	0.02	0.00
12.50	2.00	0.00	3.75	0.02	0.00	12.52	2.00	0.00	3.74	0.02	0.00
12.54	2.00	0.00	3.73	0.02	0.00	12.56	2.00	0.00	3.72	0.02	0.00
12.58	2.00	0.00	3.71	0.02	0.00	12.60	2.00	0.00	3.70	0.02	0.00
12.62	2.00	0.00	3.69	0.02	0.00	12.64	2.00	0.00	3.68	0.02	0.00
12.66	2.00	0.00	3.67	0.02	0.00	12.68	2.00	0.00	3.66	0.02	0.00
12.70	2.00	0.00	3.65	0.02	0.00	12.72	2.00	0.00	3.64	0.02	0.00
12.74	2.00	0.00	3.63	0.02	0.00	12.76	2.00	0.00	3.62	0.02	0.00
12.78	2.00	0.00	3.61	0.02	0.00	12.80	2.00	0.00	3.60	0.02	0.00
12.82	2.00	0.00	3.59	0.02	0.00	12.84	2.00	0.00	3.58	0.02	0.00
12.86	2.00	0.00	3.57	0.02	0.00	12.88	2.00	0.00	3.56	0.02	0.00
12.91	2.00	0.00	3.55	0.03	0.00	12.93	2.00	0.00	3.54	0.02	0.00
12.95	2.00	0.00	3.53	0.02	0.00	12.96	2.00	0.00	3.52	0.01	0.00
12.98	2.00	0.00	3.51	0.02	0.00	13.00	2.00	0.00	3.50	0.02	0.00
13.02	2.00	0.00	3.49	0.02	0.00	13.04	2.00	0.00	3.48	0.02	0.00
13.06	2.00	0.00	3.47	0.02	0.00	13.08	2.00	0.00	3.46	0.02	0.00
13.10	2.00	0.00	3.45	0.02	0.00	13.12	2.00	0.00	3.44	0.02	0.00
13.14	2.00	0.00	3.43	0.02	0.00	13.16	2.00	0.00	3.42	0.02	0.00
13.19	2.00	0.00	3.41	0.03	0.00	13.20	2.00	0.00	3.40	0.01	0.00
13.22	2.00	0.00	3.39	0.02	0.00	13.24	2.00	0.00	3.38	0.02	0.00
13.26	2.00	0.00	3.37	0.02	0.00	13.28	2.00	0.00	3.36	0.02	0.00
13.30	2.00	0.00	3.35	0.02	0.00	13.32	2.00	0.00	3.34	0.02	0.00
13.34	2.00	0.00	3.33	0.02	0.00	13.36	2.00	0.00	3.32	0.02	0.00
13.38	2.00	0.00	3.31	0.02	0.00	13.40	2.00	0.00	3.30	0.02	0.00
13.42	2.00	0.00	3.29	0.02	0.00	13.44	2.00	0.00	3.28	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
13.46	2.00	0.00	3.27	0.02	0.00	13.48	2.00	0.00	3.26	0.02	0.00
13.50	2.00	0.00	3.25	0.02	0.00	13.52	2.00	0.00	3.24	0.02	0.00
13.54	2.00	0.00	3.23	0.02	0.00	13.56	2.00	0.00	3.22	0.02	0.00
13.58	2.00	0.00	3.21	0.02	0.00	13.60	2.00	0.00	3.20	0.02	0.00
13.62	2.00	0.00	3.19	0.02	0.00	13.64	2.00	0.00	3.18	0.02	0.00
13.66	2.00	0.00	3.17	0.02	0.00	13.68	2.00	0.00	3.16	0.02	0.00
13.70	2.00	0.00	3.15	0.02	0.00	13.72	2.00	0.00	3.14	0.02	0.00
13.74	2.00	0.00	3.13	0.02	0.00	13.76	2.00	0.00	3.12	0.02	0.00
13.78	2.00	0.00	3.11	0.02	0.00	13.81	2.00	0.00	3.10	0.03	0.00
13.82	2.00	0.00	3.09	0.01	0.00	13.84	2.00	0.00	3.08	0.02	0.00
13.86	2.00	0.00	3.07	0.02	0.00	13.88	2.00	0.00	3.06	0.02	0.00
13.90	2.00	0.00	3.05	0.02	0.00	13.92	2.00	0.00	3.04	0.02	0.00
13.94	2.00	0.00	3.03	0.02	0.00	13.96	2.00	0.00	3.02	0.02	0.00
13.98	2.00	0.00	3.01	0.02	0.00	14.00	2.00	0.00	3.00	0.02	0.00
14.02	2.00	0.00	2.99	0.02	0.00	14.04	2.00	0.00	2.98	0.02	0.00
14.06	2.00	0.00	2.97	0.02	0.00	14.08	2.00	0.00	2.96	0.02	0.00
14.10	2.00	0.00	2.95	0.02	0.00	14.13	2.00	0.00	2.94	0.03	0.00
14.14	2.00	0.00	2.93	0.01	0.00	14.16	2.00	0.00	2.92	0.02	0.00
14.18	2.00	0.00	2.91	0.02	0.00	14.20	2.00	0.00	2.90	0.02	0.00
14.22	2.00	0.00	2.89	0.02	0.00	14.24	2.00	0.00	2.88	0.02	0.00
14.26	2.00	0.00	2.87	0.02	0.00	14.28	2.00	0.00	2.86	0.02	0.00
14.30	2.00	0.00	2.85	0.02	0.00	14.32	2.00	0.00	2.84	0.02	0.00
14.34	2.00	0.00	2.83	0.02	0.00	14.36	2.00	0.00	2.82	0.02	0.00
14.38	2.00	0.00	2.81	0.02	0.00	14.40	2.00	0.00	2.80	0.02	0.00
14.42	2.00	0.00	2.79	0.02	0.00	14.44	2.00	0.00	2.78	0.02	0.00
14.46	2.00	0.00	2.77	0.02	0.00	14.48	2.00	0.00	2.76	0.02	0.00
14.50	2.00	0.00	2.75	0.02	0.00	14.52	2.00	0.00	2.74	0.02	0.00
14.54	2.00	0.00	2.73	0.02	0.00	14.56	2.00	0.00	2.72	0.02	0.00
14.58	2.00	0.00	2.71	0.02	0.00	14.60	2.00	0.00	2.70	0.02	0.00
14.62	2.00	0.00	2.69	0.02	0.00	14.64	2.00	0.00	2.68	0.02	0.00
14.66	2.00	0.00	2.67	0.02	0.00	14.68	2.00	0.00	2.66	0.02	0.00
14.70	2.00	0.00	2.65	0.02	0.00	14.72	2.00	0.00	2.64	0.02	0.00
14.74	2.00	0.00	2.63	0.02	0.00	14.76	2.00	0.00	2.62	0.02	0.00
14.78	2.00	0.00	2.61	0.02	0.00	14.80	2.00	0.00	2.60	0.02	0.00
14.82	2.00	0.00	2.59	0.02	0.00	14.84	2.00	0.00	2.58	0.02	0.00
14.86	2.00	0.00	2.57	0.02	0.00	14.88	2.00	0.00	2.56	0.02	0.00
14.90	2.00	0.00	2.55	0.02	0.00	14.92	2.00	0.00	2.54	0.02	0.00
14.94	2.00	0.00	2.53	0.02	0.00	14.96	2.00	0.00	2.52	0.02	0.00
14.98	2.00	0.00	2.51	0.02	0.00	15.00	2.00	0.00	2.50	0.02	0.00
15.02	2.00	0.00	2.49	0.02	0.00	15.04	2.00	0.00	2.48	0.02	0.00
15.06	2.00	0.00	2.47	0.02	0.00	15.08	2.00	0.00	2.46	0.02	0.00
15.10	2.00	0.00	2.45	0.02	0.00	15.12	2.00	0.00	2.44	0.02	0.00
15.14	2.00	0.00	2.43	0.02	0.00	15.17	2.00	0.00	2.42	0.03	0.00
15.18	2.00	0.00	2.41	0.01	0.00	15.20	2.00	0.00	2.40	0.02	0.00
15.22	2.00	0.00	2.39	0.02	0.00	15.24	2.00	0.00	2.38	0.02	0.00
15.26	2.00	0.00	2.37	0.02	0.00	15.28	2.00	0.00	2.36	0.02	0.00
15.30	2.00	0.00	2.35	0.02	0.00	15.32	2.00	0.00	2.34	0.02	0.00
15.34	2.00	0.00	2.33	0.02	0.00	15.36	2.00	0.00	2.32	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
15.38	2.00	0.00	2.31	0.02	0.00	15.40	2.00	0.00	2.30	0.02	0.00
15.42	2.00	0.00	2.29	0.02	0.00	15.44	2.00	0.00	2.28	0.02	0.00
15.46	2.00	0.00	2.27	0.02	0.00	15.48	2.00	0.00	2.26	0.02	0.00
15.50	2.00	0.00	2.25	0.02	0.00	15.52	2.00	0.00	2.24	0.02	0.00
15.54	2.00	0.00	2.23	0.02	0.00	15.56	2.00	0.00	2.22	0.02	0.00
15.58	2.00	0.00	2.21	0.02	0.00	15.60	2.00	0.00	2.20	0.02	0.00
15.62	2.00	0.00	2.19	0.02	0.00	15.64	2.00	0.00	2.18	0.02	0.00
15.66	2.00	0.00	2.17	0.02	0.00						

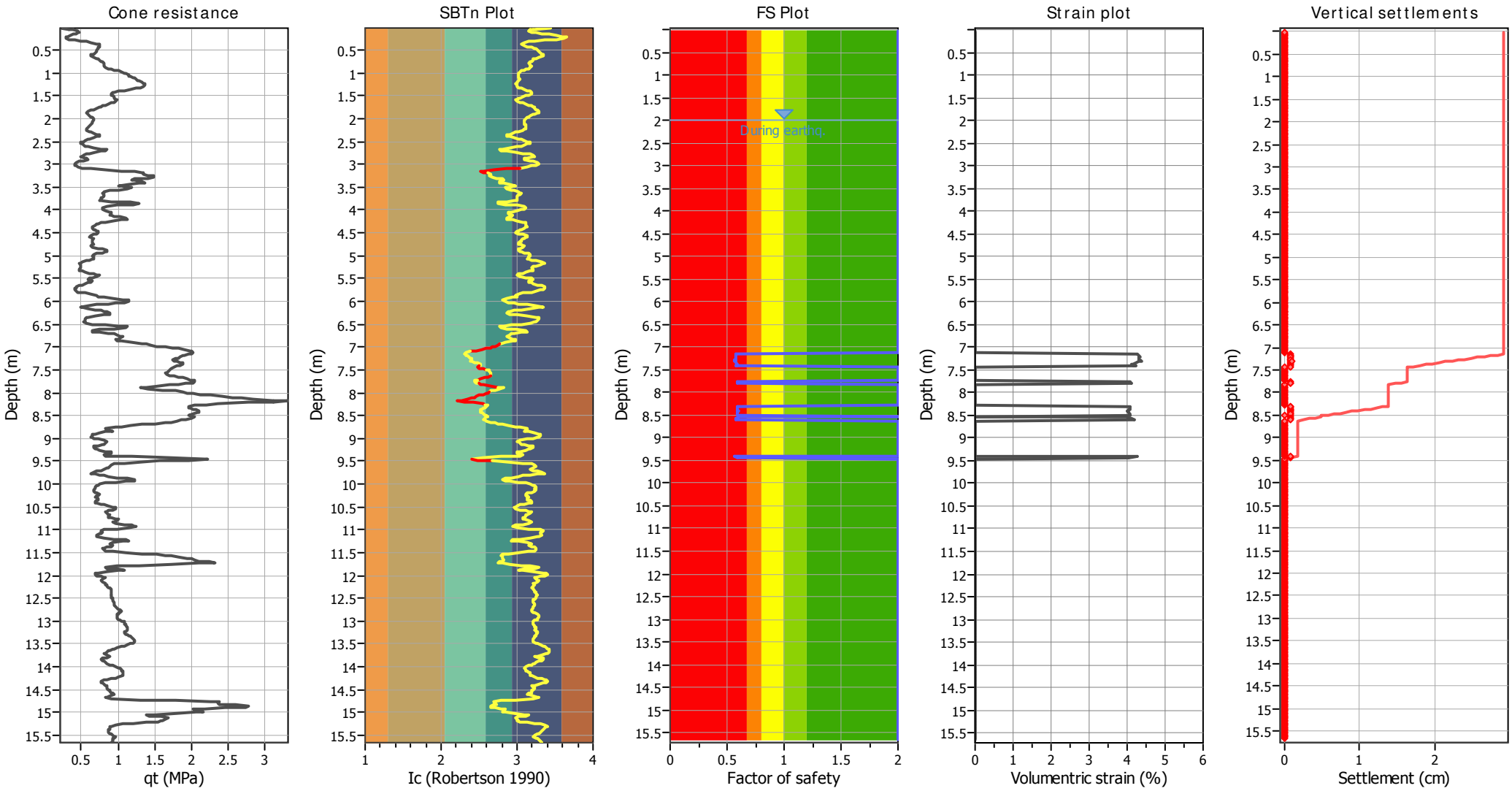
Overall liquefaction potential: 1.76

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.00	11.00	2.00	0.00	1.00	0.00	2.02	11.30	2.00	0.00	1.00	0.00
2.04	11.00	2.00	0.00	1.00	0.00	2.06	10.92	2.00	0.00	1.00	0.00
2.08	10.57	2.00	0.00	1.00	0.00	2.10	10.65	2.00	0.00	1.00	0.00
2.12	10.49	2.00	0.00	1.00	0.00	2.14	10.26	2.00	0.00	1.00	0.00
2.16	9.99	2.00	0.00	1.00	0.00	2.18	9.61	2.00	0.00	1.00	0.00
2.20	9.60	2.00	0.00	1.00	0.00	2.22	9.52	2.00	0.00	1.00	0.00
2.24	9.14	2.00	0.00	1.00	0.00	2.26	9.47	2.00	0.00	1.00	0.00
2.28	9.70	2.00	0.00	1.00	0.00	2.30	10.22	2.00	0.00	1.00	0.00
2.32	10.60	2.00	0.00	1.00	0.00	2.34	11.64	2.00	0.00	1.00	0.00
2.36	12.17	2.00	0.00	1.00	0.00	2.38	12.51	2.00	0.00	1.00	0.00
2.40	11.51	2.00	0.00	1.00	0.00	2.42	10.49	2.00	0.00	1.00	0.00
2.44	9.76	2.00	0.00	1.00	0.00	2.46	9.10	2.00	0.00	1.00	0.00
2.48	8.85	2.00	0.00	1.00	0.00	2.50	8.34	2.00	0.00	1.00	0.00
2.52	7.65	2.00	0.00	1.00	0.00	2.54	7.45	2.00	0.00	1.00	0.00
2.56	7.93	2.00	0.00	1.00	0.00	2.58	8.38	2.00	0.00	1.00	0.00
2.60	8.57	2.00	0.00	1.00	0.00	2.62	8.94	2.00	0.00	1.00	0.00
2.64	10.06	2.00	0.00	1.00	0.00	2.66	12.42	2.00	0.00	1.00	0.00
2.68	13.24	2.00	0.00	1.00	0.00	2.70	13.55	2.00	0.00	1.00	0.00
2.72	11.58	2.00	0.00	1.00	0.00	2.74	10.72	2.00	0.00	1.00	0.00
2.76	9.52	2.00	0.00	1.00	0.00	2.78	8.46	2.00	0.00	1.00	0.00
2.80	8.02	2.00	0.00	1.00	0.00	2.82	7.65	2.00	0.00	1.00	0.00
2.84	7.67	2.00	0.00	1.00	0.00	2.86	7.45	2.00	0.00	1.00	0.00
2.88	9.90	2.00	0.00	1.00	0.00	2.90	8.89	2.00	0.00	1.00	0.00
2.92	7.94	2.00	0.00	1.00	0.00	2.94	7.06	2.00	0.00	1.00	0.00
2.96	6.91	2.00	0.00	1.00	0.00	2.98	6.07	2.00	0.00	1.00	0.00
3.00	5.99	2.00	0.00	1.00	0.00	3.02	6.22	2.00	0.00	1.00	0.00
3.04	6.45	2.00	0.00	1.00	0.00	3.06	6.78	2.00	0.00	1.00	0.00
3.08	7.29	2.00	0.00	1.00	0.00	3.10	9.03	2.00	0.00	1.00	0.00
3.12	12.26	2.00	0.00	1.00	0.00	3.14	71.04	2.00	0.00	1.00	0.00
3.16	74.25	2.00	0.00	1.00	0.00	3.18	76.23	2.00	0.00	1.00	0.00
3.20	20.12	2.00	0.00	1.00	0.00	3.22	19.97	2.00	0.00	1.00	0.00
3.24	20.45	2.00	0.00	1.00	0.00	3.26	22.42	2.00	0.00	1.00	0.00
3.28	23.34	2.00	0.00	1.00	0.00	3.30	20.09	2.00	0.00	1.00	0.00
3.32	18.56	2.00	0.00	1.00	0.00	3.34	16.08	2.00	0.00	1.00	0.00
3.36	17.95	2.00	0.00	1.00	0.00	3.38	19.61	2.00	0.00	1.00	0.00
3.40	20.83	2.00	0.00	1.00	0.00	3.42	19.11	2.00	0.00	1.00	0.00
3.44	16.25	2.00	0.00	1.00	0.00	3.46	14.74	2.00	0.00	1.00	0.00
3.48	13.74	2.00	0.00	1.00	0.00	3.50	17.33	2.00	0.00	1.00	0.00
3.52	17.62	2.00	0.00	1.00	0.00	3.54	16.41	2.00	0.00	1.00	0.00
3.56	15.01	2.00	0.00	1.00	0.00	3.58	12.16	2.00	0.00	1.00	0.00
3.60	11.75	2.00	0.00	1.00	0.00	3.62	11.47	2.00	0.00	1.00	0.00
3.64	11.41	2.00	0.00	1.00	0.00	3.66	11.45	2.00	0.00	1.00	0.00
3.68	11.81	2.00	0.00	1.00	0.00	3.70	11.53	2.00	0.00	1.00	0.00
3.72	11.19	2.00	0.00	1.00	0.00	3.74	10.79	2.00	0.00	1.00	0.00
3.76	11.28	2.00	0.00	1.00	0.00	3.78	10.50	2.00	0.00	1.00	0.00
3.80	10.13	2.00	0.00	1.00	0.00	3.82	12.35	2.00	0.00	1.00	0.00
3.84	16.30	2.00	0.00	1.00	0.00	3.86	20.85	2.00	0.00	1.00	0.00
3.88	17.00	2.00	0.00	1.00	0.00	3.90	13.57	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.92	11.67	2.00	0.00	1.00	0.00	3.94	10.99	2.00	0.00	1.00	0.00
3.96	10.91	2.00	0.00	1.00	0.00	3.98	11.01	2.00	0.00	1.00	0.00
4.00	10.99	2.00	0.00	1.00	0.00	4.02	11.32	2.00	0.00	1.00	0.00
4.04	12.20	2.00	0.00	1.00	0.00	4.06	13.34	2.00	0.00	1.00	0.00
4.08	12.35	2.00	0.00	1.00	0.00	4.10	12.14	2.00	0.00	1.00	0.00
4.12	12.34	2.00	0.00	1.00	0.00	4.14	13.00	2.00	0.00	1.00	0.00
4.16	14.02	2.00	0.00	1.00	0.00	4.18	15.59	2.00	0.00	1.00	0.00
4.20	15.99	2.00	0.00	1.00	0.00	4.22	14.80	2.00	0.00	1.00	0.00
4.24	12.67	2.00	0.00	1.00	0.00	4.26	11.42	2.00	0.00	1.00	0.00
4.28	10.42	2.00	0.00	1.00	0.00	4.30	10.19	2.00	0.00	1.00	0.00
4.32	9.95	2.00	0.00	1.00	0.00	4.34	9.38	2.00	0.00	1.00	0.00
4.36	8.93	2.00	0.00	1.00	0.00	4.38	8.70	2.00	0.00	1.00	0.00
4.40	8.63	2.00	0.00	1.00	0.00	4.42	9.01	2.00	0.00	1.00	0.00
4.44	9.40	2.00	0.00	1.00	0.00	4.46	9.60	2.00	0.00	1.00	0.00
4.48	9.77	2.00	0.00	1.00	0.00	4.51	10.09	2.00	0.00	1.00	0.00
4.52	9.75	2.00	0.00	1.00	0.00	4.54	8.88	2.00	0.00	1.00	0.00
4.56	8.11	2.00	0.00	1.00	0.00	4.58	8.16	2.00	0.00	1.00	0.00
4.60	8.49	2.00	0.00	1.00	0.00	4.62	8.72	2.00	0.00	1.00	0.00
4.64	8.92	2.00	0.00	1.00	0.00	4.66	8.79	2.00	0.00	1.00	0.00
4.68	8.48	2.00	0.00	1.00	0.00	4.70	8.36	2.00	0.00	1.00	0.00
4.72	8.62	2.00	0.00	1.00	0.00	4.74	8.85	2.00	0.00	1.00	0.00
4.76	8.84	2.00	0.00	1.00	0.00	4.78	7.94	2.00	0.00	1.00	0.00
4.80	8.20	2.00	0.00	1.00	0.00	4.82	8.58	2.00	0.00	1.00	0.00
4.84	8.90	2.00	0.00	1.00	0.00	4.86	11.43	2.00	0.00	1.00	0.00
4.89	11.05	2.00	0.00	1.00	0.00	4.90	11.05	2.00	0.00	1.00	0.00
4.92	11.33	2.00	0.00	1.00	0.00	4.94	10.25	2.00	0.00	1.00	0.00
4.96	9.29	2.00	0.00	1.00	0.00	4.98	8.30	2.00	0.00	1.00	0.00
5.00	8.70	2.00	0.00	1.00	0.00	5.02	8.66	2.00	0.00	1.00	0.00
5.04	8.62	2.00	0.00	1.00	0.00	5.06	8.67	2.00	0.00	1.00	0.00
5.08	8.65	2.00	0.00	1.00	0.00	5.10	8.11	2.00	0.00	1.00	0.00
5.12	7.24	2.00	0.00	1.00	0.00	5.14	6.70	2.00	0.00	1.00	0.00
5.16	6.10	2.00	0.00	1.00	0.00	5.18	6.12	2.00	0.00	1.00	0.00
5.20	6.23	2.00	0.00	1.00	0.00	5.22	6.19	2.00	0.00	1.00	0.00
5.24	6.54	2.00	0.00	1.00	0.00	5.26	6.41	2.00	0.00	1.00	0.00
5.28	6.20	2.00	0.00	1.00	0.00	5.30	6.05	2.00	0.00	1.00	0.00
5.32	5.93	2.00	0.00	1.00	0.00	5.34	6.10	2.00	0.00	1.00	0.00
5.37	7.11	2.00	0.00	1.00	0.00	5.38	7.66	2.00	0.00	1.00	0.00
5.40	8.21	2.00	0.00	1.00	0.00	5.42	9.33	2.00	0.00	1.00	0.00
5.44	9.66	2.00	0.00	1.00	0.00	5.46	9.17	2.00	0.00	1.00	0.00
5.48	8.55	2.00	0.00	1.00	0.00	5.50	7.16	2.00	0.00	1.00	0.00
5.52	7.10	2.00	0.00	1.00	0.00	5.54	7.87	2.00	0.00	1.00	0.00
5.56	8.35	2.00	0.00	1.00	0.00	5.58	8.00	2.00	0.00	1.00	0.00
5.60	7.42	2.00	0.00	1.00	0.00	5.62	7.01	2.00	0.00	1.00	0.00
5.64	6.40	2.00	0.00	1.00	0.00	5.66	5.50	2.00	0.00	1.00	0.00
5.68	5.38	2.00	0.00	1.00	0.00	5.70	5.23	2.00	0.00	1.00	0.00
5.72	5.03	2.00	0.00	1.00	0.00	5.74	4.91	2.00	0.00	1.00	0.00
5.76	5.05	2.00	0.00	1.00	0.00	5.78	5.16	2.00	0.00	1.00	0.00
5.80	5.48	2.00	0.00	1.00	0.00	5.82	5.70	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.84	8.97	2.00	0.00	1.00	0.00	5.87	8.85	2.00	0.00	1.00	0.00
5.88	8.82	2.00	0.00	1.00	0.00	5.90	8.61	2.00	0.00	1.00	0.00
5.92	9.53	2.00	0.00	1.00	0.00	5.94	11.60	2.00	0.00	1.00	0.00
5.96	13.26	2.00	0.00	1.00	0.00	5.98	14.71	2.00	0.00	1.00	0.00
6.00	14.55	2.00	0.00	1.00	0.00	6.02	13.81	2.00	0.00	1.00	0.00
6.04	12.24	2.00	0.00	1.00	0.00	6.06	10.37	2.00	0.00	1.00	0.00
6.08	9.78	2.00	0.00	1.00	0.00	6.10	6.55	2.00	0.00	1.00	0.00
6.12	5.87	2.00	0.00	1.00	0.00	6.14	6.17	2.00	0.00	1.00	0.00
6.16	7.12	2.00	0.00	1.00	0.00	6.19	8.61	2.00	0.00	1.00	0.00
6.20	9.57	2.00	0.00	1.00	0.00	6.22	9.78	2.00	0.00	1.00	0.00
6.24	10.16	2.00	0.00	1.00	0.00	6.26	11.22	2.00	0.00	1.00	0.00
6.28	11.43	2.00	0.00	1.00	0.00	6.30	10.12	2.00	0.00	1.00	0.00
6.32	8.13	2.00	0.00	1.00	0.00	6.34	7.05	2.00	0.00	1.00	0.00
6.36	6.74	2.00	0.00	1.00	0.00	6.38	6.81	2.00	0.00	1.00	0.00
6.40	6.78	2.00	0.00	1.00	0.00	6.42	6.71	2.00	0.00	1.00	0.00
6.44	6.59	2.00	0.00	1.00	0.00	6.46	6.39	2.00	0.00	1.00	0.00
6.48	6.33	2.00	0.00	1.00	0.00	6.50	7.67	2.00	0.00	1.00	0.00
6.52	9.68	2.00	0.00	1.00	0.00	6.54	12.18	2.00	0.00	1.00	0.00
6.56	14.57	2.00	0.00	1.00	0.00	6.58	14.18	2.00	0.00	1.00	0.00
6.60	11.25	2.00	0.00	1.00	0.00	6.62	8.64	2.00	0.00	1.00	0.00
6.64	7.35	2.00	0.00	1.00	0.00	6.66	7.32	2.00	0.00	1.00	0.00
6.68	8.56	2.00	0.00	1.00	0.00	6.70	10.74	2.00	0.00	1.00	0.00
6.72	11.62	2.00	0.00	1.00	0.00	6.74	11.18	2.00	0.00	1.00	0.00
6.76	12.24	2.00	0.00	1.00	0.00	6.78	13.22	2.00	0.00	1.00	0.00
6.80	12.29	2.00	0.00	1.00	0.00	6.82	11.05	2.00	0.00	1.00	0.00
6.84	12.38	2.00	0.00	1.00	0.00	6.86	11.40	2.00	0.00	1.00	0.00
6.88	11.58	2.00	0.00	1.00	0.00	6.90	14.28	2.00	0.00	1.00	0.00
6.92	16.64	2.00	0.00	1.00	0.00	6.94	16.28	2.00	0.00	1.00	0.00
6.96	16.53	2.00	0.00	1.00	0.00	6.98	18.16	2.00	0.00	1.00	0.00
7.00	19.45	2.00	0.00	1.00	0.00	7.02	20.44	2.00	0.00	1.00	0.00
7.04	21.52	2.00	0.00	1.00	0.00	7.06	79.06	2.00	0.00	1.00	0.00
7.08	78.21	2.00	0.00	1.00	0.00	7.10	77.14	2.00	0.00	1.00	0.00
7.12	75.97	2.00	0.00	1.00	0.00	7.14	75.25	0.58	4.25	1.00	0.09
7.16	74.59	0.58	4.29	1.00	0.09	7.18	74.12	0.57	4.31	1.00	0.09
7.20	73.79	0.57	4.33	1.00	0.09	7.22	74.12	0.57	4.31	1.00	0.09
7.24	74.47	0.58	4.29	1.00	0.09	7.26	74.12	0.57	4.31	1.00	0.09
7.28	73.41	0.57	4.35	1.00	0.09	7.30	73.04	0.57	4.37	1.00	0.09
7.32	74.07	0.57	4.31	1.00	0.09	7.34	75.97	0.58	4.21	1.00	0.08
7.36	77.13	0.59	4.15	1.00	0.08	7.38	77.74	0.59	4.12	1.00	0.08
7.40	77.42	0.59	4.14	1.00	0.08	7.42	75.95	0.58	4.21	1.00	0.08
7.44	74.86	2.00	0.00	1.00	0.00	7.46	75.17	2.00	0.00	1.00	0.00
7.48	75.57	2.00	0.00	1.00	0.00	7.50	19.73	2.00	0.00	1.00	0.00
7.52	19.65	2.00	0.00	1.00	0.00	7.54	19.38	2.00	0.00	1.00	0.00
7.56	19.10	2.00	0.00	1.00	0.00	7.58	19.03	2.00	0.00	1.00	0.00
7.60	18.93	2.00	0.00	1.00	0.00	7.62	19.34	2.00	0.00	1.00	0.00
7.64	20.16	2.00	0.00	1.00	0.00	7.66	20.95	2.00	0.00	1.00	0.00
7.68	78.32	2.00	0.00	1.00	0.00	7.70	78.38	2.00	0.00	1.00	0.00
7.72	78.27	2.00	0.00	1.00	0.00	7.74	78.27	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.76	78.47	0.59	4.08	1.00	0.08	7.78	78.15	0.59	4.10	1.00	0.08
7.80	77.86	0.59	4.11	1.00	0.08	7.82	76.32	2.00	0.00	1.00	0.00
7.84	75.43	2.00	0.00	1.00	0.00	7.86	17.99	2.00	0.00	1.00	0.00
7.88	15.14	2.00	0.00	1.00	0.00	7.90	14.07	2.00	0.00	1.00	0.00
7.92	15.26	2.00	0.00	1.00	0.00	7.94	18.59	2.00	0.00	1.00	0.00
7.96	20.43	2.00	0.00	1.00	0.00	7.98	21.21	2.00	0.00	1.00	0.00
8.00	22.03	2.00	0.00	1.00	0.00	8.02	79.67	2.00	0.00	1.00	0.00
8.04	80.59	2.00	0.00	1.00	0.00	8.06	81.76	2.00	0.00	1.00	0.00
8.08	84.22	2.00	0.00	1.00	0.00	8.10	85.04	2.00	0.00	1.00	0.00
8.12	85.43	2.00	0.00	1.00	0.00	8.14	85.51	2.00	0.00	1.00	0.00
8.16	86.72	2.00	0.00	1.00	0.00	8.18	89.99	2.00	0.00	1.00	0.00
8.20	92.49	2.00	0.00	1.00	0.00	8.22	83.42	2.00	0.00	1.00	0.00
8.24	84.86	2.00	0.00	1.00	0.00	8.26	81.30	2.00	0.00	1.00	0.00
8.28	22.43	2.00	0.00	1.00	0.00	8.30	78.32	0.59	4.09	1.00	0.08
8.32	78.51	0.59	4.08	1.00	0.08	8.34	78.61	0.59	4.08	1.00	0.08
8.36	78.63	0.59	4.08	1.00	0.08	8.38	79.05	0.59	4.06	1.00	0.08
8.40	79.68	0.59	4.02	1.00	0.08	8.42	79.96	0.60	4.01	1.00	0.08
8.44	79.59	0.59	4.03	1.00	0.08	8.46	78.55	0.59	4.08	1.00	0.08
8.48	78.36	0.59	4.09	1.00	0.08	8.50	78.56	0.59	4.08	1.00	0.08
8.52	22.38	2.00	0.00	1.00	0.00	8.54	80.12	0.60	4.00	1.00	0.08
8.56	79.09	0.59	4.05	1.00	0.08	8.58	77.52	0.58	4.13	1.00	0.08
8.60	76.46	0.58	4.19	1.00	0.08	8.62	19.71	2.00	0.00	1.00	0.00
8.64	19.03	2.00	0.00	1.00	0.00	8.66	17.99	2.00	0.00	1.00	0.00
8.68	16.78	2.00	0.00	1.00	0.00	8.70	14.60	2.00	0.00	1.00	0.00
8.72	12.50	2.00	0.00	1.00	0.00	8.74	11.44	2.00	0.00	1.00	0.00
8.76	10.46	2.00	0.00	1.00	0.00	8.78	10.06	2.00	0.00	1.00	0.00
8.80	6.57	2.00	0.00	1.00	0.00	8.82	11.23	2.00	0.00	1.00	0.00
8.84	9.96	2.00	0.00	1.00	0.00	8.86	8.91	2.00	0.00	1.00	0.00
8.88	8.00	2.00	0.00	1.00	0.00	8.90	7.17	2.00	0.00	1.00	0.00
8.92	6.85	2.00	0.00	1.00	0.00	8.94	6.89	2.00	0.00	1.00	0.00
8.96	6.84	2.00	0.00	1.00	0.00	8.98	6.78	2.00	0.00	1.00	0.00
9.00	6.94	2.00	0.00	1.00	0.00	9.02	7.71	2.00	0.00	1.00	0.00
9.04	8.76	2.00	0.00	1.00	0.00	9.06	9.33	2.00	0.00	1.00	0.00
9.08	9.16	2.00	0.00	1.00	0.00	9.10	8.69	2.00	0.00	1.00	0.00
9.12	8.59	2.00	0.00	1.00	0.00	9.14	8.78	2.00	0.00	1.00	0.00
9.16	7.57	2.00	0.00	1.00	0.00	9.18	6.90	2.00	0.00	1.00	0.00
9.20	6.94	2.00	0.00	1.00	0.00	9.22	7.25	2.00	0.00	1.00	0.00
9.24	7.50	2.00	0.00	1.00	0.00	9.26	7.76	2.00	0.00	1.00	0.00
9.28	8.59	2.00	0.00	1.00	0.00	9.30	9.80	2.00	0.00	1.00	0.00
9.32	9.96	2.00	0.00	1.00	0.00	9.34	9.12	2.00	0.00	1.00	0.00
9.36	8.26	2.00	0.00	1.00	0.00	9.38	8.35	2.00	0.00	1.00	0.00
9.40	9.61	2.00	0.00	1.00	0.00	9.42	74.88	0.56	4.27	1.00	0.09
9.44	79.60	0.59	4.03	1.00	0.08	9.46	80.12	2.00	0.00	1.00	0.00
9.48	74.00	2.00	0.00	1.00	0.00	9.50	16.56	2.00	0.00	1.00	0.00
9.52	13.34	2.00	0.00	1.00	0.00	9.54	10.97	2.00	0.00	1.00	0.00
9.56	9.65	2.00	0.00	1.00	0.00	9.58	9.26	2.00	0.00	1.00	0.00
9.60	9.21	2.00	0.00	1.00	0.00	9.62	9.03	2.00	0.00	1.00	0.00
9.64	9.00	2.00	0.00	1.00	0.00	9.66	8.92	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.68	8.27	2.00	0.00	1.00	0.00	9.70	8.06	2.00	0.00	1.00	0.00
9.72	7.34	2.00	0.00	1.00	0.00	9.74	6.63	2.00	0.00	1.00	0.00
9.76	6.53	2.00	0.00	1.00	0.00	9.78	6.39	2.00	0.00	1.00	0.00
9.80	7.85	2.00	0.00	1.00	0.00	9.82	7.82	2.00	0.00	1.00	0.00
9.84	8.16	2.00	0.00	1.00	0.00	9.86	9.58	2.00	0.00	1.00	0.00
9.88	11.27	2.00	0.00	1.00	0.00	9.91	12.76	2.00	0.00	1.00	0.00
9.92	12.81	2.00	0.00	1.00	0.00	9.94	11.61	2.00	0.00	1.00	0.00
9.96	9.59	2.00	0.00	1.00	0.00	9.98	8.00	2.00	0.00	1.00	0.00
10.00	7.35	2.00	0.00	1.00	0.00	10.03	7.13	2.00	0.00	1.00	0.00
10.04	6.81	2.00	0.00	1.00	0.00	10.06	6.64	2.00	0.00	1.00	0.00
10.08	6.64	2.00	0.00	1.00	0.00	10.10	6.75	2.00	0.00	1.00	0.00
10.12	6.63	2.00	0.00	1.00	0.00	10.14	6.39	2.00	0.00	1.00	0.00
10.16	6.32	2.00	0.00	1.00	0.00	10.18	6.52	2.00	0.00	1.00	0.00
10.20	6.88	2.00	0.00	1.00	0.00	10.22	7.32	2.00	0.00	1.00	0.00
10.24	7.17	2.00	0.00	1.00	0.00	10.26	6.78	2.00	0.00	1.00	0.00
10.28	6.66	2.00	0.00	1.00	0.00	10.30	6.61	2.00	0.00	1.00	0.00
10.32	7.02	2.00	0.00	1.00	0.00	10.34	7.06	2.00	0.00	1.00	0.00
10.36	6.85	2.00	0.00	1.00	0.00	10.38	6.39	2.00	0.00	1.00	0.00
10.40	6.43	2.00	0.00	1.00	0.00	10.42	6.68	2.00	0.00	1.00	0.00
10.44	7.18	2.00	0.00	1.00	0.00	10.46	7.79	2.00	0.00	1.00	0.00
10.48	8.33	2.00	0.00	1.00	0.00	10.50	8.85	2.00	0.00	1.00	0.00
10.52	9.60	2.00	0.00	1.00	0.00	10.54	9.59	2.00	0.00	1.00	0.00
10.56	9.06	2.00	0.00	1.00	0.00	10.58	8.51	2.00	0.00	1.00	0.00
10.60	7.92	2.00	0.00	1.00	0.00	10.62	7.89	2.00	0.00	1.00	0.00
10.64	7.88	2.00	0.00	1.00	0.00	10.66	8.31	2.00	0.00	1.00	0.00
10.68	8.69	2.00	0.00	1.00	0.00	10.70	8.59	2.00	0.00	1.00	0.00
10.72	7.97	2.00	0.00	1.00	0.00	10.74	8.51	2.00	0.00	1.00	0.00
10.76	9.38	2.00	0.00	1.00	0.00	10.78	10.40	2.00	0.00	1.00	0.00
10.80	9.58	2.00	0.00	1.00	0.00	10.82	9.28	2.00	0.00	1.00	0.00
10.84	8.96	2.00	0.00	1.00	0.00	10.86	9.00	2.00	0.00	1.00	0.00
10.88	10.54	2.00	0.00	1.00	0.00	10.90	11.98	2.00	0.00	1.00	0.00
10.92	12.15	2.00	0.00	1.00	0.00	10.94	12.36	2.00	0.00	1.00	0.00
10.96	12.35	2.00	0.00	1.00	0.00	10.98	9.46	2.00	0.00	1.00	0.00
11.00	7.64	2.00	0.00	1.00	0.00	11.02	7.19	2.00	0.00	1.00	0.00
11.04	7.65	2.00	0.00	1.00	0.00	11.06	7.90	2.00	0.00	1.00	0.00
11.08	7.56	2.00	0.00	1.00	0.00	11.10	6.97	2.00	0.00	1.00	0.00
11.12	6.97	2.00	0.00	1.00	0.00	11.14	6.58	2.00	0.00	1.00	0.00
11.16	6.80	2.00	0.00	1.00	0.00	11.18	7.19	2.00	0.00	1.00	0.00
11.20	8.98	2.00	0.00	1.00	0.00	11.22	11.12	2.00	0.00	1.00	0.00
11.24	11.89	2.00	0.00	1.00	0.00	11.26	10.31	2.00	0.00	1.00	0.00
11.28	8.42	2.00	0.00	1.00	0.00	11.30	8.21	2.00	0.00	1.00	0.00
11.32	8.80	2.00	0.00	1.00	0.00	11.34	9.11	2.00	0.00	1.00	0.00
11.36	8.79	2.00	0.00	1.00	0.00	11.38	8.08	2.00	0.00	1.00	0.00
11.40	7.45	2.00	0.00	1.00	0.00	11.42	7.64	2.00	0.00	1.00	0.00
11.44	7.46	2.00	0.00	1.00	0.00	11.46	7.65	2.00	0.00	1.00	0.00
11.48	8.35	2.00	0.00	1.00	0.00	11.50	10.32	2.00	0.00	1.00	0.00
11.52	12.72	2.00	0.00	1.00	0.00	11.54	14.94	2.00	0.00	1.00	0.00
11.56	15.98	2.00	0.00	1.00	0.00	11.58	16.39	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.60	17.51	2.00	0.00	1.00	0.00	11.62	18.83	2.00	0.00	1.00	0.00
11.64	19.88	2.00	0.00	1.00	0.00	11.66	19.61	2.00	0.00	1.00	0.00
11.68	19.67	2.00	0.00	1.00	0.00	11.70	21.59	2.00	0.00	1.00	0.00
11.72	23.51	2.00	0.00	1.00	0.00	11.74	21.92	2.00	0.00	1.00	0.00
11.76	15.56	2.00	0.00	1.00	0.00	11.78	12.36	2.00	0.00	1.00	0.00
11.80	8.97	2.00	0.00	1.00	0.00	11.82	7.08	2.00	0.00	1.00	0.00
11.84	7.23	2.00	0.00	1.00	0.00	11.86	9.75	2.00	0.00	1.00	0.00
11.88	10.95	2.00	0.00	1.00	0.00	11.90	9.91	2.00	0.00	1.00	0.00
11.93	7.50	2.00	0.00	1.00	0.00	11.94	6.81	2.00	0.00	1.00	0.00
11.96	6.24	2.00	0.00	1.00	0.00	11.98	6.37	2.00	0.00	1.00	0.00
12.00	6.58	2.00	0.00	1.00	0.00	12.02	7.17	2.00	0.00	1.00	0.00
12.04	7.77	2.00	0.00	1.00	0.00	12.06	7.87	2.00	0.00	1.00	0.00
12.08	7.41	2.00	0.00	1.00	0.00	12.10	6.96	2.00	0.00	1.00	0.00
12.12	7.00	2.00	0.00	1.00	0.00	12.14	7.27	2.00	0.00	1.00	0.00
12.16	7.76	2.00	0.00	1.00	0.00	12.18	7.84	2.00	0.00	1.00	0.00
12.20	7.72	2.00	0.00	1.00	0.00	12.22	7.74	2.00	0.00	1.00	0.00
12.24	7.88	2.00	0.00	1.00	0.00	12.26	8.14	2.00	0.00	1.00	0.00
12.28	8.34	2.00	0.00	1.00	0.00	12.30	8.23	2.00	0.00	1.00	0.00
12.32	8.37	2.00	0.00	1.00	0.00	12.34	8.43	2.00	0.00	1.00	0.00
12.36	8.43	2.00	0.00	1.00	0.00	12.38	8.46	2.00	0.00	1.00	0.00
12.40	8.44	2.00	0.00	1.00	0.00	12.42	8.32	2.00	0.00	1.00	0.00
12.44	8.34	2.00	0.00	1.00	0.00	12.46	8.42	2.00	0.00	1.00	0.00
12.48	8.45	2.00	0.00	1.00	0.00	12.50	8.38	2.00	0.00	1.00	0.00
12.52	8.48	2.00	0.00	1.00	0.00	12.54	8.56	2.00	0.00	1.00	0.00
12.56	8.57	2.00	0.00	1.00	0.00	12.58	8.57	2.00	0.00	1.00	0.00
12.60	8.62	2.00	0.00	1.00	0.00	12.62	8.66	2.00	0.00	1.00	0.00
12.64	8.50	2.00	0.00	1.00	0.00	12.66	8.62	2.00	0.00	1.00	0.00
12.68	8.78	2.00	0.00	1.00	0.00	12.70	8.88	2.00	0.00	1.00	0.00
12.72	8.98	2.00	0.00	1.00	0.00	12.74	9.12	2.00	0.00	1.00	0.00
12.76	9.45	2.00	0.00	1.00	0.00	12.78	9.33	2.00	0.00	1.00	0.00
12.80	9.18	2.00	0.00	1.00	0.00	12.82	9.01	2.00	0.00	1.00	0.00
12.84	8.87	2.00	0.00	1.00	0.00	12.86	8.85	2.00	0.00	1.00	0.00
12.88	8.71	2.00	0.00	1.00	0.00	12.91	8.91	2.00	0.00	1.00	0.00
12.93	8.84	2.00	0.00	1.00	0.00	12.95	8.79	2.00	0.00	1.00	0.00
12.96	8.89	2.00	0.00	1.00	0.00	12.98	9.02	2.00	0.00	1.00	0.00
13.00	9.43	2.00	0.00	1.00	0.00	13.02	9.61	2.00	0.00	1.00	0.00
13.04	9.56	2.00	0.00	1.00	0.00	13.06	9.65	2.00	0.00	1.00	0.00
13.08	9.81	2.00	0.00	1.00	0.00	13.10	9.86	2.00	0.00	1.00	0.00
13.12	9.87	2.00	0.00	1.00	0.00	13.14	9.92	2.00	0.00	1.00	0.00
13.16	9.85	2.00	0.00	1.00	0.00	13.19	9.96	2.00	0.00	1.00	0.00
13.20	9.87	2.00	0.00	1.00	0.00	13.22	9.70	2.00	0.00	1.00	0.00
13.24	9.46	2.00	0.00	1.00	0.00	13.26	9.47	2.00	0.00	1.00	0.00
13.28	9.67	2.00	0.00	1.00	0.00	13.30	10.00	2.00	0.00	1.00	0.00
13.32	9.85	2.00	0.00	1.00	0.00	13.34	10.00	2.00	0.00	1.00	0.00
13.36	10.57	2.00	0.00	1.00	0.00	13.38	10.46	2.00	0.00	1.00	0.00
13.40	10.61	2.00	0.00	1.00	0.00	13.42	10.72	2.00	0.00	1.00	0.00
13.44	10.85	2.00	0.00	1.00	0.00	13.46	10.78	2.00	0.00	1.00	0.00
13.48	10.69	2.00	0.00	1.00	0.00	13.50	10.23	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
13.52	9.69	2.00	0.00	1.00	0.00	13.54	9.41	2.00	0.00	1.00	0.00
13.56	9.10	2.00	0.00	1.00	0.00	13.58	8.58	2.00	0.00	1.00	0.00
13.60	8.24	2.00	0.00	1.00	0.00	13.62	8.05	2.00	0.00	1.00	0.00
13.64	7.84	2.00	0.00	1.00	0.00	13.66	7.35	2.00	0.00	1.00	0.00
13.68	7.26	2.00	0.00	1.00	0.00	13.70	7.21	2.00	0.00	1.00	0.00
13.72	6.86	2.00	0.00	1.00	0.00	13.74	6.93	2.00	0.00	1.00	0.00
13.76	7.92	2.00	0.00	1.00	0.00	13.78	7.66	2.00	0.00	1.00	0.00
13.81	7.25	2.00	0.00	1.00	0.00	13.82	6.52	2.00	0.00	1.00	0.00
13.84	6.36	2.00	0.00	1.00	0.00	13.86	6.55	2.00	0.00	1.00	0.00
13.88	6.75	2.00	0.00	1.00	0.00	13.90	6.99	2.00	0.00	1.00	0.00
13.92	7.01	2.00	0.00	1.00	0.00	13.94	7.14	2.00	0.00	1.00	0.00
13.96	7.36	2.00	0.00	1.00	0.00	13.98	7.70	2.00	0.00	1.00	0.00
14.00	8.18	2.00	0.00	1.00	0.00	14.02	8.55	2.00	0.00	1.00	0.00
14.04	8.75	2.00	0.00	1.00	0.00	14.06	8.69	2.00	0.00	1.00	0.00
14.08	8.84	2.00	0.00	1.00	0.00	14.10	8.94	2.00	0.00	1.00	0.00
14.13	8.81	2.00	0.00	1.00	0.00	14.14	8.87	2.00	0.00	1.00	0.00
14.16	8.88	2.00	0.00	1.00	0.00	14.18	9.02	2.00	0.00	1.00	0.00
14.20	9.03	2.00	0.00	1.00	0.00	14.22	8.47	2.00	0.00	1.00	0.00
14.24	7.97	2.00	0.00	1.00	0.00	14.26	7.54	2.00	0.00	1.00	0.00
14.28	7.10	2.00	0.00	1.00	0.00	14.30	6.62	2.00	0.00	1.00	0.00
14.32	6.30	2.00	0.00	1.00	0.00	14.34	6.24	2.00	0.00	1.00	0.00
14.36	6.41	2.00	0.00	1.00	0.00	14.38	6.56	2.00	0.00	1.00	0.00
14.40	6.86	2.00	0.00	1.00	0.00	14.42	7.09	2.00	0.00	1.00	0.00
14.44	7.09	2.00	0.00	1.00	0.00	14.46	6.79	2.00	0.00	1.00	0.00
14.48	6.82	2.00	0.00	1.00	0.00	14.50	6.94	2.00	0.00	1.00	0.00
14.52	7.33	2.00	0.00	1.00	0.00	14.54	7.30	2.00	0.00	1.00	0.00
14.56	7.16	2.00	0.00	1.00	0.00	14.58	7.42	2.00	0.00	1.00	0.00
14.60	8.02	2.00	0.00	1.00	0.00	14.62	7.86	2.00	0.00	1.00	0.00
14.64	7.17	2.00	0.00	1.00	0.00	14.66	6.79	2.00	0.00	1.00	0.00
14.68	6.54	2.00	0.00	1.00	0.00	14.70	6.81	2.00	0.00	1.00	0.00
14.72	8.86	2.00	0.00	1.00	0.00	14.74	17.01	2.00	0.00	1.00	0.00
14.76	20.24	2.00	0.00	1.00	0.00	14.78	21.89	2.00	0.00	1.00	0.00
14.80	20.09	2.00	0.00	1.00	0.00	14.82	19.93	2.00	0.00	1.00	0.00
14.84	22.29	2.00	0.00	1.00	0.00	14.86	25.33	2.00	0.00	1.00	0.00
14.88	24.34	2.00	0.00	1.00	0.00	14.90	21.48	2.00	0.00	1.00	0.00
14.92	18.00	2.00	0.00	1.00	0.00	14.94	16.55	2.00	0.00	1.00	0.00
14.96	17.26	2.00	0.00	1.00	0.00	14.98	19.64	2.00	0.00	1.00	0.00
15.00	18.54	2.00	0.00	1.00	0.00	15.02	14.86	2.00	0.00	1.00	0.00
15.04	12.96	2.00	0.00	1.00	0.00	15.06	10.70	2.00	0.00	1.00	0.00
15.08	11.45	2.00	0.00	1.00	0.00	15.10	13.78	2.00	0.00	1.00	0.00
15.12	14.92	2.00	0.00	1.00	0.00	15.14	14.03	2.00	0.00	1.00	0.00
15.17	12.88	2.00	0.00	1.00	0.00	15.18	13.52	2.00	0.00	1.00	0.00
15.20	13.72	2.00	0.00	1.00	0.00	15.22	11.58	2.00	0.00	1.00	0.00
15.24	9.50	2.00	0.00	1.00	0.00	15.26	8.93	2.00	0.00	1.00	0.00
15.28	7.92	2.00	0.00	1.00	0.00	15.30	7.35	2.00	0.00	1.00	0.00
15.32	7.26	2.00	0.00	1.00	0.00	15.34	7.45	2.00	0.00	1.00	0.00
15.36	7.25	2.00	0.00	1.00	0.00	15.38	7.09	2.00	0.00	1.00	0.00
15.40	7.06	2.00	0.00	1.00	0.00	15.42	7.00	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
15.44	7.05	2.00	0.00	1.00	0.00	15.46	7.14	2.00	0.00	1.00	0.00
15.48	7.39	2.00	0.00	1.00	0.00	15.50	7.56	2.00	0.00	1.00	0.00
15.52	7.92	2.00	0.00	1.00	0.00	15.54	7.93	2.00	0.00	1.00	0.00
15.56	7.79	2.00	0.00	1.00	0.00	15.58	7.58	2.00	0.00	1.00	0.00
15.60	7.41	2.00	0.00	1.00	0.00	15.62	7.54	2.00	0.00	1.00	0.00
15.64	7.46	2.00	0.00	1.00	0.00	15.66	7.36	2.00	0.00	1.00	0.00

Total estimated settlement: 2.91

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.21	3.62	12.92	46.77	3.43	0.05	51.17
0.04	0.33	5.67	9.53	54.08	3.22	0.06	39.52
0.06	0.39	6.64	8.83	58.67	3.17	0.06	30.50
0.08	0.45	7.68	8.55	65.67	3.15	0.06	26.16
0.10	0.47	7.91	9.17	72.47	3.19	0.06	21.31
0.12	0.46	7.75	10.05	77.82	3.26	0.06	17.24
0.14	0.43	7.24	11.27	81.58	3.34	0.06	13.70
0.16	0.39	6.63	12.63	83.72	3.42	0.06	10.91
0.18	0.35	5.86	14.49	84.90	3.52	0.06	8.52
0.20	0.31	5.29	16.05	84.91	3.60	0.06	6.89
0.22	0.29	4.91	16.91	83.06	3.65	0.06	5.80
0.24	0.30	4.98	16.28	81.07	3.61	0.06	5.37
0.26	0.33	5.55	14.29	79.33	3.51	0.06	5.52
0.28	0.40	6.80	11.67	79.29	3.36	0.06	6.27
0.30	0.49	8.17	9.82	80.18	3.24	0.06	7.02
0.32	0.56	9.50	8.67	82.36	3.16	0.06	7.65
0.34	0.64	10.76	7.94	85.41	3.10	0.06	8.14
0.36	0.70	11.83	7.50	88.69	3.07	0.06	8.44
0.38	0.75	12.57	7.41	93.13	3.06	0.06	8.47
0.40	0.75	12.59	7.85	98.83	3.09	0.06	8.04
0.42	0.74	12.48	8.48	105.84	3.14	0.06	7.57
0.44	0.73	12.26	9.17	112.42	3.19	0.06	7.08
0.46	0.73	12.26	9.63	118.05	3.23	0.06	6.75
0.48	0.72	12.15	10.07	122.28	3.26	0.06	6.39
0.50	0.72	12.08	10.35	125.05	3.28	0.06	6.08
0.52	0.71	11.95	10.56	126.26	3.29	0.06	5.77
0.54	0.70	11.83	10.68	126.32	3.30	0.06	5.49
0.56	0.68	11.48	10.92	125.36	3.31	0.06	5.12
0.59	0.66	11.07	11.19	123.95	3.33	0.06	4.68
0.60	0.63	10.60	11.52	122.09	3.35	0.06	4.40
0.62	0.62	10.41	11.57	120.44	3.35	0.06	4.17
0.64	0.63	10.53	11.35	119.49	3.34	0.06	4.08
0.66	0.67	11.18	10.61	118.69	3.29	0.06	4.20
0.68	0.71	11.86	9.96	118.17	3.25	0.06	4.32
0.70	0.74	12.31	9.53	117.27	3.22	0.06	4.35
0.72	0.75	12.56	9.29	116.75	3.20	0.06	4.31
0.74	0.77	12.81	9.06	116.08	3.19	0.06	4.27
0.76	0.78	13.10	8.81	115.50	3.17	0.07	4.25
0.78	0.80	13.39	8.64	115.60	3.15	0.07	4.23
0.80	0.81	13.54	8.63	116.89	3.15	0.07	4.17
0.82	0.81	13.55	8.77	118.84	3.17	0.07	4.06
0.84	0.80	13.42	9.00	120.82	3.18	0.07	3.92
0.86	0.81	13.45	9.08	122.09	3.19	0.07	3.84
0.88	0.82	13.77	8.92	122.75	3.18	0.07	3.84
0.90	0.86	14.38	8.58	123.34	3.15	0.07	3.91
0.92	0.90	15.04	8.24	123.89	3.12	0.07	4.00
0.94	0.95	15.81	7.88	124.58	3.10	0.07	4.11
0.96	1.00	16.77	7.45	124.89	3.06	0.07	4.27

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	1.05	17.58	7.10	124.84	3.03	0.07	4.38
1.00	1.10	18.37	6.85	125.90	3.01	0.07	4.48
1.02	1.12	18.70	6.86	128.20	3.01	0.07	4.47
1.04	1.14	19.06	6.91	131.73	3.02	0.07	4.46
1.06	1.15	19.25	7.02	135.12	3.02	0.07	4.42
1.08	1.18	19.66	7.04	138.34	3.03	0.07	4.42
1.10	1.21	20.18	7.02	141.70	3.02	0.07	4.45
1.12	1.23	20.57	7.03	144.67	3.03	0.07	4.45
1.14	1.24	20.80	7.09	147.37	3.03	0.07	4.42
1.16	1.26	21.07	7.07	148.90	3.03	0.07	4.40
1.18	1.28	21.41	6.99	149.67	3.02	0.08	4.39
1.20	1.32	22.13	6.78	150.00	3.00	0.08	4.45
1.22	1.35	22.53	6.69	150.68	2.99	0.08	4.46
1.25	1.37	22.96	6.62	152.04	2.99	0.08	4.42
1.26	1.37	23.00	6.65	153.03	2.99	0.08	4.40
1.28	1.37	22.98	6.67	153.35	2.99	0.08	4.32
1.30	1.35	22.61	6.78	153.25	3.00	0.08	4.18
1.32	1.31	21.83	7.03	153.41	3.03	0.08	3.97
1.34	1.25	20.82	7.37	153.37	3.05	0.07	3.73
1.36	1.17	19.43	7.85	152.58	3.09	0.07	3.43
1.38	1.09	18.05	8.36	150.78	3.13	0.07	3.13
1.40	1.01	16.79	8.82	148.10	3.17	0.07	2.87
1.42	0.96	15.88	9.13	145.00	3.19	0.07	2.68
1.44	0.93	15.34	9.21	141.34	3.20	0.07	2.55
1.46	0.91	15.03	9.12	137.08	3.19	0.07	2.46
1.48	0.92	15.16	8.68	131.64	3.16	0.07	2.45
1.50	0.93	15.41	8.13	125.29	3.12	0.07	2.45
1.52	0.95	15.64	7.61	119.03	3.07	0.07	2.46
1.54	0.95	15.66	7.27	113.81	3.05	0.07	2.43
1.56	0.95	15.76	6.97	109.87	3.02	0.07	2.41
1.58	0.96	15.92	6.72	106.97	3.00	0.07	2.41
1.60	0.98	16.21	6.55	106.13	2.98	0.07	2.42
1.63	0.97	16.04	6.72	107.85	3.00	0.07	2.35
1.64	0.95	15.64	7.11	111.21	3.03	0.07	2.28
1.66	0.91	15.01	7.60	114.09	3.07	0.07	2.16
1.68	0.87	14.31	8.11	116.12	3.11	0.07	2.04
1.70	0.83	13.58	8.66	117.56	3.16	0.07	1.91
1.72	0.79	12.89	9.21	118.72	3.20	0.06	1.79
1.74	0.76	12.47	9.52	118.76	3.22	0.06	1.71
1.76	0.74	12.07	9.68	116.85	3.23	0.06	1.64
1.78	0.71	11.57	9.81	113.54	3.24	0.06	1.55
1.80	0.67	10.89	10.09	109.81	3.26	0.06	1.44
1.82	0.63	10.23	10.37	106.11	3.28	0.06	1.34
1.84	0.60	9.65	10.59	102.27	3.29	0.06	1.25
1.86	0.58	9.25	10.65	98.54	3.30	0.06	1.19
1.88	0.57	9.18	10.34	94.83	3.27	0.06	1.17
1.90	0.59	9.40	9.82	92.28	3.24	0.06	1.18
1.92	0.60	9.63	9.34	89.96	3.21	0.06	1.20

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	0.61	9.87	8.97	88.55	3.18	0.06	1.22
1.96	0.62	9.99	8.73	87.23	3.16	0.06	1.22
1.98	0.64	10.33	8.38	86.58	3.14	0.06	1.25
2.00	0.66	10.65	8.07	86.00	3.11	0.06	1.28
2.02	0.67	10.80	7.90	85.32	3.10	0.06	1.28
2.04	0.67	10.78	7.85	84.63	3.09	0.06	1.27
2.06	0.66	10.54	7.99	84.19	3.11	0.06	1.23
2.08	0.65	10.42	7.97	83.07	3.10	0.06	1.20
2.10	0.64	10.28	7.93	81.54	3.10	0.06	1.18
2.12	0.64	10.18	7.92	80.63	3.10	0.06	1.15
2.14	0.62	9.96	8.05	80.17	3.11	0.06	1.12
2.16	0.61	9.66	8.22	79.39	3.12	0.06	1.08
2.18	0.59	9.45	8.21	77.57	3.12	0.06	1.04
2.20	0.59	9.29	8.14	75.69	3.12	0.06	1.02
2.22	0.58	9.14	8.06	73.70	3.11	0.06	0.99
2.24	0.57	9.10	7.88	71.74	3.10	0.06	0.98
2.26	0.58	9.17	7.58	69.51	3.07	0.06	0.98
2.28	0.60	9.55	7.05	67.37	3.03	0.06	1.01
2.30	0.63	9.95	6.61	65.75	2.99	0.06	1.04
2.32	0.67	10.64	6.11	65.02	2.94	0.06	1.11
2.34	0.71	11.35	5.70	64.66	2.90	0.07	1.17
2.36	0.75	12.07	5.33	64.35	2.86	0.07	1.24
2.38	0.75	12.08	5.40	65.19	2.87	0.07	1.23
2.40	0.72	11.54	5.73	66.12	2.90	0.07	1.16
2.42	0.67	10.62	6.35	67.42	2.96	0.06	1.06
2.44	0.62	9.80	6.91	67.74	3.01	0.06	0.97
2.46	0.59	9.25	7.40	68.46	3.06	0.06	0.91
2.48	0.56	8.76	7.89	69.17	3.10	0.06	0.86
2.50	0.53	8.26	8.45	69.79	3.14	0.06	0.80
2.52	0.50	7.78	8.96	69.70	3.18	0.06	0.75
2.54	0.49	7.64	8.99	68.68	3.18	0.06	0.74
2.56	0.51	7.92	8.48	67.16	3.14	0.06	0.76
2.58	0.53	8.34	7.89	65.76	3.10	0.06	0.80
2.60	0.56	8.71	7.43	64.74	3.06	0.06	0.83
2.62	0.59	9.33	6.80	63.39	3.00	0.06	0.89
2.64	0.68	10.73	5.76	61.83	2.91	0.06	1.02
2.66	0.77	12.31	4.92	60.49	2.82	0.07	1.17
2.68	0.85	13.60	4.47	60.79	2.76	0.07	1.29
2.70	0.83	13.29	4.75	63.14	2.80	0.07	1.26
2.72	0.77	12.36	5.41	66.94	2.87	0.07	1.16
2.74	0.69	10.88	6.57	71.48	2.98	0.06	1.02
2.76	0.62	9.74	7.67	74.69	3.08	0.06	0.91
2.78	0.56	8.77	8.76	76.80	3.16	0.06	0.82
2.80	0.52	8.10	9.48	76.77	3.22	0.06	0.75
2.82	0.51	7.83	9.58	74.99	3.22	0.06	0.73
2.84	0.50	7.63	9.36	71.44	3.21	0.06	0.71
2.86	0.55	8.45	8.29	70.02	3.13	0.06	0.78
2.88	0.57	8.89	7.92	70.40	3.10	0.06	0.82

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	0.58	9.06	7.90	71.54	3.10	0.06	0.83
2.92	0.52	8.02	8.83	70.83	3.17	0.06	0.73
2.94	0.48	7.30	9.51	69.49	3.22	0.06	0.67
2.96	0.44	6.63	10.27	68.08	3.27	0.06	0.60
2.98	0.42	6.25	10.62	66.33	3.29	0.06	0.57
3.00	0.40	6.01	10.65	63.97	3.30	0.06	0.54
3.02	0.41	6.16	9.96	61.40	3.25	0.06	0.56
3.04	0.43	6.47	9.12	59.02	3.19	0.06	0.58
3.06	0.46	6.88	8.30	57.12	3.13	0.06	0.62
3.08	0.51	7.85	7.09	55.65	3.03	0.06	0.70
3.10	0.64	9.92	5.43	53.85	2.87	0.06	0.89
3.12	0.83	13.25	3.90	51.69	2.69	0.07	1.18
3.14	1.06	17.03	3.09	52.55	2.56	0.08	0.60
3.16	1.23	20.04	2.91	58.22	2.53	0.08	0.62
3.18	1.32	21.58	3.09	66.71	2.56	0.08	0.63
3.20	1.35	21.96	3.41	74.82	2.61	0.08	1.94
3.22	1.35	22.10	3.63	80.17	2.65	0.08	1.94
3.24	1.41	23.05	3.65	84.03	2.65	0.08	2.02
3.26	1.49	24.44	3.60	87.98	2.64	0.09	2.14
3.28	1.49	24.33	3.82	92.87	2.67	0.09	2.12
3.30	1.40	22.83	4.20	95.88	2.73	0.08	1.98
3.32	1.23	20.03	4.83	96.66	2.80	0.08	1.73
3.34	1.19	19.31	4.97	96.03	2.82	0.08	1.67
3.36	1.22	19.83	4.86	96.46	2.81	0.08	1.71
3.38	1.34	21.75	4.51	98.15	2.77	0.08	1.87
3.40	1.36	22.21	4.51	100.04	2.77	0.08	1.90
3.42	1.29	20.86	4.94	103.14	2.82	0.08	1.78
3.44	1.14	18.42	5.74	105.83	2.90	0.07	1.57
3.46	1.02	16.32	6.56	107.00	2.98	0.07	1.38
3.48	1.05	16.81	6.32	106.24	2.96	0.07	1.42
3.50	1.12	18.02	5.73	103.22	2.90	0.07	1.52
3.52	1.18	19.12	5.21	99.69	2.85	0.08	1.61
3.54	1.13	18.22	5.31	96.79	2.86	0.07	1.52
3.56	1.01	16.07	5.83	93.75	2.91	0.07	1.34
3.58	0.90	14.25	6.39	91.15	2.97	0.06	1.19
3.60	0.82	12.88	6.91	88.95	3.01	0.06	1.07
3.62	0.80	12.61	7.12	89.78	3.03	0.06	1.04
3.64	0.80	12.51	7.30	91.28	3.05	0.06	1.03
3.66	0.81	12.67	7.21	91.30	3.04	0.06	1.04
3.68	0.81	12.73	7.03	89.55	3.03	0.06	1.04
3.70	0.81	12.64	6.84	86.43	3.01	0.06	1.03
3.72	0.78	12.25	6.82	83.50	3.01	0.06	1.00
3.74	0.78	12.16	6.69	81.36	3.00	0.06	0.99
3.76	0.76	11.90	6.67	79.43	2.99	0.06	0.97
3.78	0.75	11.66	6.69	78.07	3.00	0.06	0.94
3.80	0.78	12.11	6.41	77.64	2.97	0.06	0.98
3.82	0.92	14.48	5.41	78.37	2.87	0.07	1.17
3.84	1.17	18.85	4.40	83.01	2.75	0.08	1.51

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	1.28	20.70	4.44	91.84	2.76	0.08	1.66
3.88	1.22	19.54	5.20	101.49	2.85	0.08	1.56
3.90	0.99	15.75	6.69	105.40	3.00	0.07	1.25
3.92	0.85	13.35	7.77	103.72	3.09	0.06	1.06
3.94	0.79	12.35	8.12	100.29	3.12	0.06	0.98
3.96	0.78	12.16	8.03	97.67	3.11	0.06	0.96
3.98	0.79	12.20	7.77	94.82	3.09	0.06	0.96
4.00	0.80	12.39	7.42	91.96	3.06	0.06	0.97
4.02	0.83	12.90	6.82	87.93	3.01	0.06	1.01
4.04	0.89	13.87	6.00	83.25	2.93	0.07	1.08
4.06	0.91	14.30	5.56	79.54	2.89	0.07	1.11
4.08	0.91	14.28	5.60	79.92	2.89	0.07	1.11
4.10	0.89	13.87	5.98	82.94	2.93	0.07	1.07
4.12	0.90	14.15	6.12	86.63	2.94	0.07	1.09
4.14	0.95	14.95	6.00	89.73	2.93	0.07	1.15
4.16	1.03	16.31	5.66	92.25	2.90	0.07	1.25
4.18	1.10	17.56	5.37	94.27	2.87	0.07	1.35
4.20	1.12	17.88	5.46	97.52	2.87	0.07	1.37
4.22	1.05	16.65	6.04	100.47	2.93	0.07	1.27
4.24	0.94	14.74	6.85	100.90	3.01	0.06	1.12
4.26	0.83	12.92	7.66	98.97	3.08	0.06	0.98
4.28	0.77	11.92	8.01	95.50	3.11	0.06	0.90
4.30	0.74	11.34	8.16	92.54	3.12	0.06	0.86
4.32	0.72	10.95	8.13	88.94	3.12	0.06	0.82
4.34	0.69	10.45	8.19	85.59	3.12	0.06	0.78
4.36	0.66	9.95	8.25	82.12	3.13	0.06	0.75
4.38	0.64	9.66	8.13	78.61	3.12	0.06	0.72
4.40	0.65	9.73	7.79	75.76	3.09	0.06	0.72
4.42	0.67	10.04	7.42	74.46	3.06	0.06	0.75
4.44	0.69	10.46	7.14	74.74	3.04	0.06	0.78
4.46	0.71	10.79	6.96	75.12	3.02	0.06	0.80
4.48	0.73	11.09	6.72	74.52	3.00	0.06	0.82
4.51	0.73	11.16	6.60	73.66	2.99	0.06	0.82
4.52	0.71	10.81	6.89	74.45	3.01	0.06	0.79
4.54	0.66	9.99	7.66	76.47	3.08	0.06	0.73
4.56	0.63	9.34	8.33	77.78	3.13	0.06	0.68
4.58	0.62	9.20	8.44	77.64	3.14	0.06	0.67
4.60	0.64	9.47	8.18	77.43	3.12	0.06	0.69
4.62	0.66	9.80	7.85	76.95	3.09	0.06	0.71
4.64	0.66	9.94	7.64	75.91	3.08	0.06	0.72
4.66	0.66	9.85	7.49	73.77	3.06	0.06	0.71
4.68	0.65	9.62	7.39	71.13	3.06	0.06	0.69
4.70	0.64	9.56	7.25	69.29	3.04	0.06	0.69
4.72	0.65	9.73	7.06	68.72	3.03	0.06	0.70
4.74	0.67	9.94	6.94	68.99	3.02	0.06	0.71
4.76	0.65	9.66	7.30	70.52	3.05	0.06	0.69
4.78	0.63	9.37	7.69	72.04	3.08	0.06	0.67
4.80	0.63	9.25	7.96	73.68	3.10	0.06	0.66

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	0.65	9.65	7.64	73.77	3.08	0.06	0.69
4.84	0.73	10.97	7.11	78.06	3.03	0.06	0.78
4.86	0.79	11.97	7.01	83.82	3.02	0.06	0.85
4.89	0.85	12.80	7.03	89.94	3.02	0.06	0.91
4.90	0.85	12.76	7.20	91.89	3.04	0.06	0.91
4.92	0.83	12.39	7.39	91.60	3.06	0.06	0.89
4.94	0.78	11.62	7.78	90.42	3.09	0.06	0.83
4.96	0.70	10.31	8.56	88.27	3.15	0.06	0.74
4.98	0.67	9.65	8.92	86.10	3.18	0.06	0.69
5.00	0.65	9.38	8.93	83.79	3.18	0.06	0.67
5.02	0.66	9.51	8.67	82.45	3.16	0.06	0.68
5.04	0.66	9.48	8.54	80.98	3.15	0.06	0.68
5.06	0.66	9.47	8.45	80.00	3.14	0.06	0.68
5.08	0.65	9.25	8.57	79.27	3.15	0.06	0.66
5.10	0.62	8.65	9.13	78.95	3.19	0.06	0.62
5.12	0.57	7.83	10.10	79.13	3.26	0.06	0.56
5.14	0.52	6.99	11.15	77.95	3.33	0.06	0.50
5.16	0.49	6.53	11.62	75.84	3.36	0.06	0.47
5.18	0.48	6.34	11.48	72.78	3.35	0.06	0.45
5.20	0.48	6.38	10.87	69.39	3.31	0.06	0.46
5.22	0.49	6.56	10.06	65.98	3.26	0.06	0.47
5.24	0.50	6.63	9.41	62.42	3.21	0.06	0.47
5.26	0.50	6.63	9.02	59.83	3.18	0.06	0.47
5.28	0.49	6.42	9.07	58.26	3.19	0.06	0.46
5.30	0.48	6.21	9.32	57.94	3.21	0.06	0.44
5.32	0.48	6.17	9.43	58.14	3.21	0.06	0.44
5.34	0.50	6.60	8.93	58.96	3.18	0.06	0.47
5.37	0.55	7.30	8.22	59.98	3.12	0.06	0.52
5.38	0.60	8.17	7.54	61.55	3.07	0.06	0.58
5.40	0.66	9.07	7.04	63.82	3.03	0.06	0.65
5.42	0.72	9.88	6.68	66.04	2.99	0.06	0.71
5.44	0.74	10.26	6.65	68.18	2.99	0.06	0.73
5.46	0.72	9.91	7.09	70.28	3.03	0.06	0.71
5.48	0.65	8.85	8.16	72.22	3.12	0.06	0.63
5.50	0.60	7.99	9.14	73.04	3.19	0.06	0.57
5.52	0.59	7.71	9.51	73.40	3.22	0.06	0.55
5.54	0.62	8.21	8.98	73.67	3.18	0.06	0.59
5.56	0.64	8.56	8.60	73.66	3.15	0.06	0.61
5.58	0.63	8.36	8.69	72.59	3.16	0.06	0.60
5.60	0.60	7.79	9.05	70.48	3.19	0.06	0.56
5.62	0.55	7.13	9.54	68.04	3.22	0.06	0.51
5.64	0.51	6.35	10.36	65.75	3.28	0.06	0.45
5.66	0.46	5.69	11.16	63.50	3.33	0.06	0.41
5.68	0.43	5.22	11.74	61.34	3.36	0.06	0.37
5.70	0.42	5.04	11.69	58.89	3.36	0.06	0.36
5.72	0.41	4.85	11.63	56.35	3.36	0.06	0.35
5.74	0.41	4.77	11.33	54.06	3.34	0.06	0.34
5.76	0.41	4.82	10.78	52.00	3.30	0.06	0.34

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	0.43	5.05	9.96	50.26	3.25	0.06	0.36
5.80	0.45	5.31	9.23	48.98	3.20	0.06	0.38
5.82	0.55	6.82	7.67	52.28	3.08	0.06	0.49
5.84	0.63	8.14	6.95	56.61	3.02	0.06	0.58
5.87	0.72	9.35	6.54	61.10	2.98	0.06	0.67
5.88	0.71	9.20	6.83	62.81	3.01	0.06	0.66
5.90	0.73	9.47	6.77	64.10	3.00	0.06	0.68
5.92	0.80	10.60	6.15	65.19	2.94	0.06	0.76
5.94	0.93	12.35	5.40	66.65	2.87	0.07	0.89
5.96	1.07	14.26	4.89	69.82	2.81	0.07	1.04
5.98	1.14	15.37	4.87	74.82	2.81	0.07	1.12
6.00	1.16	15.60	5.13	79.95	2.84	0.07	1.13
6.02	1.09	14.67	5.61	82.30	2.89	0.07	1.05
6.04	0.98	13.02	6.24	81.25	2.95	0.06	0.93
6.06	0.87	11.36	6.93	78.76	3.02	0.06	0.81
6.08	0.71	9.06	8.28	75.07	3.13	0.06	0.65
6.10	0.59	7.27	9.83	71.44	3.24	0.06	0.52
6.12	0.50	5.86	11.40	66.84	3.34	0.06	0.42
6.14	0.52	6.12	10.67	65.35	3.30	0.06	0.44
6.16	0.59	7.24	8.91	64.49	3.18	0.06	0.52
6.19	0.69	8.58	7.32	62.78	3.05	0.06	0.61
6.20	0.76	9.64	6.31	60.85	2.96	0.06	0.69
6.22	0.80	10.21	5.81	59.34	2.91	0.06	0.73
6.24	0.85	10.82	5.51	59.59	2.88	0.07	0.78
6.26	0.90	11.45	5.41	61.98	2.87	0.07	0.82
6.28	0.90	11.47	5.75	65.97	2.91	0.07	0.82
6.30	0.81	10.26	6.84	70.17	3.01	0.06	0.73
6.32	0.69	8.50	8.47	71.97	3.14	0.06	0.61
6.34	0.60	7.16	9.96	71.29	3.25	0.06	0.51
6.36	0.57	6.65	10.52	69.93	3.29	0.06	0.47
6.38	0.56	6.55	10.56	69.16	3.29	0.06	0.47
6.40	0.56	6.54	10.42	68.12	3.28	0.06	0.47
6.42	0.56	6.44	10.21	65.75	3.27	0.06	0.46
6.44	0.55	6.29	9.88	62.13	3.24	0.06	0.45
6.46	0.54	6.13	9.55	58.56	3.22	0.06	0.44
6.48	0.57	6.55	8.78	57.51	3.17	0.06	0.47
6.50	0.66	7.84	7.45	58.44	3.06	0.06	0.56
6.52	0.82	10.13	5.99	60.67	2.93	0.06	0.72
6.54	1.01	12.65	4.97	62.83	2.82	0.07	0.92
6.56	1.14	14.26	4.55	64.86	2.77	0.07	1.04
6.58	1.11	13.88	4.63	64.30	2.78	0.07	1.01
6.60	0.94	11.67	5.31	61.94	2.86	0.07	0.84
6.62	0.75	9.09	6.62	60.15	2.99	0.06	0.65
6.64	0.65	7.57	8.08	61.13	3.11	0.06	0.54
6.66	0.65	7.57	8.43	63.78	3.14	0.06	0.54
6.68	0.75	8.91	7.40	65.92	3.06	0.06	0.64
6.70	0.87	10.58	6.38	67.52	2.97	0.06	0.76
6.72	0.94	11.58	5.94	68.73	2.92	0.07	0.83

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	0.98	12.11	5.69	68.88	2.90	0.07	0.87
6.76	1.03	12.67	5.45	69.10	2.87	0.07	0.91
6.78	1.06	13.06	5.37	70.20	2.87	0.07	0.94
6.80	1.03	12.62	5.73	72.28	2.90	0.07	0.90
6.82	1.00	12.30	6.22	76.47	2.95	0.06	0.88
6.84	0.98	11.92	6.52	77.73	2.98	0.06	0.85
6.86	0.99	12.09	6.54	79.14	2.98	0.06	0.86
6.88	1.05	12.83	6.03	77.37	2.93	0.06	0.92
6.90	1.20	14.72	5.21	76.67	2.85	0.07	1.06
6.92	1.33	16.39	4.67	76.60	2.79	0.08	1.19
6.94	1.39	17.16	4.45	76.39	2.76	0.08	1.25
6.96	1.44	17.67	4.32	76.27	2.74	0.08	1.29
6.98	1.53	18.77	4.03	75.61	2.70	0.08	1.38
7.00	1.64	20.16	3.79	76.34	2.67	0.08	1.48
7.02	1.74	21.34	3.62	77.25	2.65	0.08	1.57
7.04	1.83	22.41	3.36	75.21	2.60	0.08	1.66
7.06	1.91	23.22	2.97	68.90	2.54	0.08	0.64
7.08	1.98	23.78	2.55	60.57	2.45	0.08	0.64
7.10	2.01	23.96	2.22	53.17	2.38	0.08	0.64
7.12	2.02	23.96	2.06	49.42	2.33	0.08	0.64
7.14	2.00	23.62	2.01	47.36	2.32	0.07	0.64
7.16	1.96	23.10	2.02	46.62	2.32	0.07	0.64
7.18	1.91	22.46	2.05	46.13	2.33	0.07	0.64
7.20	1.88	22.01	2.10	46.22	2.34	0.07	0.63
7.22	1.85	21.72	2.17	47.04	2.36	0.07	0.63
7.24	1.83	21.43	2.26	48.35	2.39	0.08	0.63
7.26	1.79	20.97	2.32	48.71	2.40	0.08	0.63
7.28	1.75	20.50	2.32	47.64	2.40	0.07	0.63
7.30	1.76	20.47	2.28	46.68	2.39	0.07	0.63
7.32	1.80	20.97	2.32	48.57	2.40	0.08	0.63
7.34	1.85	21.64	2.49	53.79	2.44	0.08	0.63
7.36	1.88	22.11	2.71	60.03	2.49	0.08	0.63
7.38	1.88	22.16	2.86	63.41	2.52	0.08	0.63
7.40	1.85	21.78	2.86	62.34	2.52	0.08	0.63
7.42	1.81	21.11	2.73	57.60	2.49	0.08	0.63
7.44	1.76	20.50	2.63	53.90	2.47	0.08	0.63
7.46	1.73	20.13	2.76	55.59	2.50	0.08	0.62
7.48	1.72	20.04	3.06	61.27	2.55	0.08	0.62
7.50	1.71	19.96	3.36	67.01	2.60	0.08	1.47
7.52	1.70	19.86	3.50	69.58	2.63	0.08	1.46
7.54	1.68	19.63	3.58	70.25	2.64	0.08	1.44
7.56	1.66	19.38	3.62	70.13	2.65	0.08	1.42
7.58	1.65	19.22	3.68	70.70	2.65	0.08	1.41
7.60	1.66	19.31	3.73	72.03	2.66	0.08	1.41
7.62	1.70	19.71	3.73	73.60	2.66	0.08	1.44
7.64	1.76	20.42	3.65	74.45	2.65	0.08	1.50
7.66	1.83	21.18	3.45	73.11	2.62	0.08	1.56
7.68	1.89	21.82	3.18	69.34	2.58	0.08	0.63

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	1.94	22.36	2.92	65.24	2.53	0.08	0.64
7.72	1.99	22.86	2.69	61.45	2.48	0.08	0.64
7.74	2.04	23.25	2.53	58.90	2.45	0.08	0.64
7.76	2.04	23.29	2.50	58.18	2.44	0.08	0.64
7.78	2.01	22.96	2.60	59.67	2.47	0.08	0.64
7.80	1.93	21.99	2.75	60.46	2.50	0.08	0.63
7.82	1.83	20.78	2.85	59.19	2.52	0.08	0.63
7.84	1.71	19.28	3.07	59.16	2.56	0.08	0.62
7.86	1.54	17.36	3.63	63.06	2.65	0.08	1.27
7.88	1.38	15.48	4.42	68.36	2.76	0.08	1.12
7.90	1.30	14.54	4.95	71.96	2.82	0.07	1.05
7.92	1.41	15.76	4.59	72.32	2.78	0.08	1.14
7.94	1.60	17.99	4.03	72.54	2.71	0.08	1.31
7.96	1.78	20.06	3.63	72.73	2.65	0.08	1.47
7.98	1.88	21.26	3.48	74.09	2.63	0.08	1.56
8.00	1.95	21.98	3.40	74.70	2.61	0.08	1.61
8.02	2.02	22.81	3.25	74.06	2.59	0.08	0.64
8.04	2.12	23.85	3.05	72.69	2.55	0.09	0.64
8.06	2.27	25.59	2.81	71.85	2.51	0.09	0.65
8.08	2.43	27.33	2.63	71.78	2.47	0.09	0.66
8.10	2.57	28.87	2.50	72.14	2.44	0.09	0.67
8.12	2.68	30.01	2.35	70.46	2.41	0.09	0.67
8.14	2.85	31.85	2.10	66.92	2.34	0.09	0.68
8.16	3.12	34.74	1.83	63.61	2.26	0.08	0.69
8.18	3.32	36.91	1.72	63.45	2.22	0.09	0.70
8.20	3.12	34.81	1.98	68.97	2.31	0.09	0.69
8.22	2.78	31.01	2.41	74.75	2.42	0.09	0.67
8.24	2.36	26.36	3.04	80.25	2.55	0.09	0.66
8.26	2.21	24.50	3.21	78.63	2.58	0.09	0.65
8.28	2.04	22.51	3.37	75.96	2.61	0.08	1.64
8.30	1.97	21.70	3.32	72.02	2.60	0.08	0.63
8.32	1.96	21.49	3.22	69.12	2.58	0.08	0.63
8.34	1.99	21.73	3.10	67.29	2.56	0.08	0.63
8.36	2.02	22.05	3.00	66.10	2.54	0.08	0.63
8.38	2.06	22.47	2.91	65.34	2.53	0.08	0.64
8.40	2.10	22.91	2.88	65.93	2.52	0.08	0.64
8.42	2.11	22.99	2.89	66.49	2.52	0.08	0.64
8.44	2.07	22.52	2.97	66.97	2.54	0.08	0.64
8.46	2.02	21.85	3.07	67.04	2.56	0.08	0.63
8.48	1.97	21.33	3.20	68.27	2.58	0.08	0.63
8.50	1.99	21.48	3.31	71.05	2.60	0.08	0.63
8.52	2.03	21.90	3.37	73.72	2.61	0.08	1.59
8.54	2.04	22.07	3.32	73.22	2.60	0.09	0.63
8.56	2.01	21.58	3.23	69.61	2.58	0.08	0.63
8.58	1.93	20.64	3.11	64.18	2.56	0.08	0.63
8.60	1.86	19.78	3.15	62.21	2.57	0.08	0.62
8.62	1.80	19.06	3.35	63.93	2.60	0.08	1.39
8.64	1.73	18.32	3.72	68.10	2.66	0.08	1.33

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	1.64	17.31	4.05	70.18	2.71	0.08	1.25
8.68	1.51	15.76	4.40	69.38	2.75	0.08	1.14
8.70	1.34	13.83	4.92	68.04	2.82	0.07	0.99
8.72	1.17	11.96	5.64	67.48	2.89	0.07	0.85
8.74	1.05	10.47	6.48	67.78	2.98	0.06	0.75
8.76	0.97	9.58	7.11	68.10	3.03	0.06	0.68
8.78	0.83	7.91	8.46	66.92	3.14	0.06	0.57
8.80	0.86	8.21	8.35	68.60	3.13	0.06	0.59
8.82	0.86	8.21	8.42	69.18	3.14	0.06	0.59
8.84	0.93	8.99	7.81	70.21	3.09	0.06	0.64
8.86	0.83	7.85	8.68	68.17	3.16	0.06	0.56
8.88	0.75	6.86	9.63	66.11	3.23	0.06	0.49
8.90	0.68	6.14	10.48	64.31	3.28	0.06	0.44
8.92	0.65	5.75	10.89	62.58	3.31	0.06	0.41
8.94	0.64	5.63	10.87	61.15	3.31	0.06	0.40
8.96	0.64	5.60	10.66	59.70	3.30	0.06	0.40
8.98	0.64	5.61	10.35	58.06	3.28	0.06	0.40
9.00	0.67	5.92	9.51	56.30	3.22	0.06	0.42
9.02	0.73	6.62	8.26	54.70	3.13	0.06	0.47
9.04	0.81	7.47	7.22	53.94	3.04	0.06	0.53
9.06	0.85	7.97	6.84	54.55	3.01	0.06	0.57
9.08	0.85	7.94	6.96	55.30	3.02	0.06	0.57
9.10	0.83	7.67	7.20	55.21	3.04	0.06	0.55
9.12	0.82	7.53	7.34	55.27	3.05	0.06	0.54
9.14	0.78	7.13	7.78	55.48	3.09	0.06	0.51
9.16	0.73	6.53	8.52	55.65	3.15	0.06	0.47
9.18	0.68	5.88	9.29	54.62	3.20	0.06	0.42
9.20	0.67	5.77	9.37	54.06	3.21	0.06	0.41
9.22	0.69	5.98	8.97	53.66	3.18	0.06	0.43
9.24	0.71	6.27	8.57	53.70	3.15	0.06	0.45
9.26	0.76	6.74	8.03	54.09	3.11	0.06	0.48
9.28	0.83	7.54	7.28	54.90	3.05	0.06	0.54
9.30	0.90	8.31	6.71	55.77	3.00	0.06	0.59
9.32	0.92	8.49	6.71	56.91	3.00	0.06	0.61
9.34	0.87	7.93	7.24	57.42	3.04	0.06	0.57
9.36	0.82	7.36	7.69	56.63	3.08	0.06	0.53
9.38	0.84	7.53	7.24	54.57	3.04	0.06	0.54
9.40	1.18	11.32	4.73	53.56	2.79	0.07	0.81
9.42	1.71	16.99	3.08	52.26	2.56	0.08	0.60
9.44	2.22	22.36	2.37	52.91	2.41	0.08	0.64
9.46	2.23	22.41	2.34	52.53	2.41	0.08	0.64
9.48	1.96	19.53	2.69	52.64	2.49	0.08	0.62
9.50	1.57	15.41	3.80	58.54	2.67	0.08	1.11
9.52	1.30	12.56	5.46	68.59	2.88	0.07	0.90
9.54	1.09	10.16	7.53	76.45	3.07	0.06	0.73
9.56	0.96	8.75	9.05	79.20	3.19	0.06	0.62
9.58	0.91	8.15	9.71	79.12	3.23	0.06	0.58
9.60	0.89	7.93	9.92	78.69	3.25	0.06	0.57

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	0.88	7.84	9.83	77.06	3.24	0.06	0.56
9.64	0.87	7.73	9.54	73.78	3.22	0.06	0.55
9.66	0.85	7.47	9.29	69.37	3.20	0.06	0.53
9.68	0.82	7.13	9.00	64.17	3.18	0.06	0.51
9.70	0.77	6.57	9.36	61.47	3.21	0.06	0.47
9.72	0.72	5.99	10.19	61.04	3.27	0.06	0.43
9.74	0.67	5.46	11.22	61.31	3.33	0.06	0.39
9.76	0.64	5.14	11.73	60.27	3.36	0.06	0.37
9.78	0.69	5.66	10.18	57.68	3.26	0.06	0.40
9.80	0.74	6.21	8.88	55.14	3.17	0.06	0.44
9.82	0.81	6.93	7.67	53.15	3.08	0.06	0.50
9.84	0.87	7.54	6.99	52.71	3.02	0.06	0.54
9.86	0.98	8.74	6.00	52.41	2.93	0.06	0.62
9.88	1.13	10.26	5.18	53.13	2.85	0.07	0.73
9.91	1.22	11.26	4.88	54.91	2.81	0.07	0.81
9.92	1.22	11.26	5.11	57.52	2.84	0.07	0.81
9.94	1.12	10.11	5.76	58.30	2.91	0.07	0.72
9.96	0.96	8.45	6.87	58.04	3.01	0.06	0.60
9.98	0.83	7.04	8.02	56.52	3.11	0.06	0.50
10.00	0.76	6.27	8.86	55.55	3.17	0.06	0.45
10.03	0.72	5.88	9.36	55.05	3.21	0.06	0.42
10.04	0.70	5.65	9.69	54.80	3.23	0.06	0.40
10.06	0.69	5.49	9.98	54.75	3.25	0.06	0.39
10.08	0.69	5.47	9.91	54.21	3.25	0.06	0.39
10.10	0.69	5.44	9.79	53.28	3.24	0.06	0.39
10.12	0.68	5.34	9.80	52.34	3.24	0.06	0.38
10.14	0.66	5.19	9.93	51.49	3.25	0.06	0.37
10.16	0.66	5.19	9.76	50.67	3.24	0.06	0.37
10.18	0.68	5.39	9.17	49.46	3.19	0.06	0.39
10.20	0.72	5.75	8.44	48.51	3.14	0.06	0.41
10.22	0.74	5.97	8.05	48.11	3.11	0.06	0.43
10.24	0.74	5.93	8.06	47.77	3.11	0.06	0.42
10.26	0.72	5.70	8.33	47.46	3.13	0.06	0.41
10.28	0.70	5.50	8.58	47.22	3.15	0.06	0.39
10.30	0.71	5.59	8.48	47.37	3.14	0.06	0.40
10.32	0.72	5.73	8.37	47.96	3.13	0.06	0.41
10.34	0.73	5.81	8.37	48.67	3.13	0.06	0.42
10.36	0.71	5.59	8.83	49.32	3.17	0.06	0.40
10.38	0.69	5.36	9.18	49.22	3.19	0.06	0.38
10.40	0.69	5.31	9.13	48.44	3.19	0.06	0.38
10.42	0.71	5.58	8.50	47.47	3.14	0.06	0.40
10.44	0.76	6.06	7.79	47.19	3.09	0.06	0.43
10.46	0.82	6.62	7.17	47.51	3.04	0.06	0.47
10.48	0.87	7.19	6.77	48.66	3.00	0.06	0.51
10.50	0.93	7.80	6.43	50.18	2.97	0.06	0.56
10.52	0.97	8.20	6.27	51.42	2.96	0.06	0.59
10.54	0.98	8.21	6.47	53.13	2.97	0.06	0.59
10.56	0.94	7.78	7.09	55.16	3.03	0.06	0.56

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	0.88	7.18	8.01	57.55	3.11	0.06	0.51
10.60	0.84	6.80	8.70	59.12	3.16	0.06	0.49
10.62	0.83	6.61	9.08	60.00	3.19	0.06	0.47
10.64	0.84	6.76	8.85	59.84	3.17	0.06	0.48
10.66	0.87	7.05	8.46	59.62	3.14	0.06	0.50
10.68	0.89	7.28	8.03	58.40	3.11	0.06	0.52
10.70	0.88	7.10	8.08	57.38	3.11	0.06	0.51
10.72	0.87	7.02	7.97	55.93	3.10	0.06	0.50
10.74	0.90	7.30	7.57	55.26	3.07	0.06	0.52
10.76	0.97	8.03	7.57	60.79	3.07	0.06	0.57
10.78	1.00	8.29	7.95	65.89	3.10	0.06	0.59
10.80	0.99	8.14	8.64	70.34	3.16	0.06	0.58
10.82	0.95	7.71	9.11	70.23	3.19	0.06	0.55
10.84	0.93	7.54	9.26	69.79	3.20	0.06	0.54
10.86	0.98	8.00	8.73	69.83	3.16	0.06	0.57
10.88	1.08	9.04	7.53	68.09	3.07	0.06	0.65
10.90	1.18	10.01	6.56	65.72	2.98	0.06	0.72
10.92	1.24	10.54	6.14	64.71	2.94	0.07	0.75
10.94	1.24	10.55	6.16	65.01	2.95	0.07	0.75
10.96	1.15	9.62	7.00	67.33	3.02	0.06	0.69
10.98	0.99	8.00	8.50	67.94	3.14	0.06	0.57
11.00	0.82	6.31	10.72	67.63	3.30	0.06	0.45
11.02	0.76	5.76	11.59	66.69	3.36	0.06	0.41
11.04	0.78	5.90	11.17	65.87	3.33	0.06	0.42
11.06	0.80	6.04	10.74	64.81	3.30	0.06	0.43
11.08	0.77	5.82	10.82	62.93	3.31	0.06	0.42
11.10	0.74	5.50	10.95	60.25	3.32	0.06	0.39
11.12	0.71	5.18	11.01	56.98	3.32	0.06	0.37
11.14	0.71	5.12	10.54	54.00	3.29	0.06	0.37
11.16	0.72	5.21	10.11	52.62	3.26	0.06	0.37
11.18	0.80	6.02	8.82	53.11	3.17	0.06	0.43
11.20	0.95	7.49	7.23	54.14	3.04	0.06	0.53
11.22	1.11	9.06	6.09	55.16	2.94	0.06	0.65
11.24	1.16	9.46	6.02	56.96	2.93	0.07	0.68
11.26	1.06	8.51	7.03	59.85	3.03	0.06	0.61
11.28	0.93	7.26	8.47	61.46	3.14	0.06	0.52
11.30	0.89	6.78	9.17	62.18	3.19	0.06	0.48
11.32	0.91	7.03	8.86	62.34	3.17	0.06	0.50
11.34	0.93	7.23	8.73	63.14	3.16	0.06	0.52
11.36	0.91	6.99	9.13	63.76	3.19	0.06	0.50
11.38	0.85	6.43	9.77	62.82	3.24	0.06	0.46
11.40	0.82	6.05	10.03	60.75	3.25	0.06	0.43
11.42	0.80	5.85	10.04	58.79	3.26	0.06	0.42
11.44	0.81	5.93	9.91	58.70	3.25	0.06	0.42
11.46	0.83	6.16	9.71	59.85	3.23	0.06	0.44
11.48	0.93	7.12	8.58	61.12	3.15	0.06	0.51
11.50	1.11	8.82	6.96	61.41	3.02	0.06	0.63
11.52	1.34	10.97	5.50	60.31	2.88	0.07	0.78

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	1.52	12.75	4.78	60.95	2.80	0.07	0.91
11.56	1.64	13.83	4.66	64.43	2.78	0.08	0.99
11.58	1.72	14.59	4.79	69.87	2.80	0.08	1.04
11.60	1.82	15.50	4.86	75.31	2.81	0.08	1.11
11.62	1.94	16.63	4.80	79.90	2.80	0.08	1.19
11.64	2.01	17.30	4.89	84.65	2.81	0.08	1.23
11.66	2.04	17.56	5.04	88.40	2.83	0.08	1.25
11.68	2.10	18.10	4.91	88.95	2.82	0.08	1.29
11.70	2.24	19.38	4.55	88.18	2.77	0.08	1.38
11.72	2.32	20.11	4.36	87.67	2.75	0.09	1.43
11.74	2.11	18.08	4.88	88.29	2.81	0.08	1.29
11.76	1.73	14.43	5.78	83.36	2.91	0.07	1.03
11.78	1.28	10.22	7.41	75.69	3.06	0.06	0.73
11.80	1.00	7.50	8.86	66.39	3.17	0.06	0.54
11.82	0.82	5.84	10.56	61.70	3.29	0.06	0.42
11.84	0.85	6.12	9.71	59.44	3.23	0.06	0.44
11.86	0.99	7.39	7.94	58.63	3.10	0.06	0.53
11.88	1.08	8.25	6.97	57.51	3.02	0.06	0.59
11.90	1.00	7.50	7.67	57.51	3.08	0.06	0.54
11.93	0.86	6.14	9.38	57.59	3.21	0.06	0.44
11.94	0.73	4.96	11.50	56.98	3.35	0.06	0.35
11.96	0.69	4.59	12.22	56.09	3.39	0.06	0.33
11.98	0.69	4.52	12.41	56.03	3.40	0.06	0.32
12.00	0.72	4.82	11.85	57.13	3.37	0.06	0.34
12.02	0.77	5.27	10.93	57.63	3.31	0.06	0.38
12.04	0.82	5.69	10.05	57.21	3.26	0.06	0.41
12.06	0.83	5.76	9.63	55.52	3.23	0.06	0.41
12.08	0.80	5.50	9.86	54.21	3.24	0.06	0.39
12.10	0.77	5.21	10.31	53.70	3.27	0.06	0.37
12.12	0.76	5.16	10.47	54.03	3.28	0.06	0.37
12.14	0.79	5.42	10.12	54.83	3.26	0.06	0.39
12.16	0.82	5.69	9.72	55.26	3.23	0.06	0.41
12.18	0.84	5.83	9.54	55.65	3.22	0.06	0.42
12.20	0.84	5.82	9.64	56.09	3.23	0.06	0.42
12.22	0.84	5.83	9.66	56.32	3.23	0.06	0.42
12.24	0.86	5.96	9.48	56.51	3.22	0.06	0.43
12.26	0.88	6.15	9.26	56.95	3.20	0.06	0.44
12.28	0.89	6.26	9.30	58.19	3.20	0.06	0.45
12.30	0.90	6.33	9.46	59.86	3.21	0.06	0.45
12.32	0.90	6.36	9.66	61.38	3.23	0.06	0.45
12.34	0.91	6.41	9.73	62.43	3.23	0.06	0.46
12.36	0.92	6.44	9.81	63.14	3.24	0.06	0.46
12.38	0.92	6.43	9.93	63.89	3.25	0.06	0.46
12.40	0.91	6.40	10.09	64.53	3.26	0.06	0.46
12.42	0.91	6.35	10.20	64.80	3.27	0.06	0.45
12.44	0.91	6.34	10.18	64.54	3.26	0.06	0.45
12.46	0.92	6.38	10.04	64.04	3.26	0.06	0.46
12.48	0.92	6.39	9.93	63.46	3.25	0.06	0.46

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
12.50	0.92	6.40	9.83	62.94	3.24	0.06	0.46
12.52	0.93	6.43	9.68	62.28	3.23	0.06	0.46
12.54	0.93	6.49	9.53	61.84	3.22	0.06	0.46
12.56	0.94	6.51	9.44	61.51	3.21	0.06	0.47
12.58	0.94	6.53	9.45	61.71	3.21	0.06	0.47
12.60	0.94	6.55	9.47	62.03	3.22	0.06	0.47
12.62	0.94	6.53	9.57	62.47	3.22	0.06	0.47
12.64	0.94	6.52	9.62	62.78	3.23	0.06	0.47
12.66	0.95	6.56	9.64	63.25	3.23	0.06	0.47
12.68	0.96	6.68	9.51	63.47	3.22	0.06	0.48
12.70	0.98	6.79	9.40	63.77	3.21	0.06	0.48
12.72	0.99	6.89	9.31	64.14	3.20	0.06	0.49
12.74	1.02	7.12	9.10	64.79	3.19	0.06	0.51
12.76	1.04	7.28	9.02	65.69	3.18	0.06	0.52
12.78	1.05	7.35	9.07	66.64	3.19	0.06	0.53
12.80	1.03	7.20	9.43	67.91	3.21	0.06	0.51
12.82	1.01	7.04	9.81	69.08	3.24	0.06	0.50
12.84	1.00	6.93	10.11	70.05	3.26	0.06	0.49
12.86	0.99	6.83	10.37	70.77	3.28	0.06	0.49
12.88	0.99	6.83	10.40	71.08	3.28	0.06	0.49
12.91	1.00	6.82	10.41	71.03	3.28	0.06	0.49
12.93	1.00	6.85	10.33	70.74	3.27	0.06	0.49
12.95	1.00	6.84	10.31	70.47	3.27	0.06	0.49
12.96	1.01	6.90	10.16	70.07	3.26	0.06	0.49
12.98	1.03	7.10	9.77	69.38	3.24	0.06	0.51
13.00	1.06	7.33	9.42	69.00	3.21	0.06	0.52
13.02	1.08	7.49	9.30	69.65	3.20	0.06	0.54
13.04	1.09	7.55	9.37	70.77	3.21	0.06	0.54
13.06	1.10	7.61	9.46	71.95	3.21	0.06	0.54
13.08	1.11	7.70	9.48	73.00	3.22	0.06	0.55
13.10	1.12	7.76	9.63	74.71	3.23	0.06	0.55
13.12	1.12	7.79	9.79	76.27	3.24	0.06	0.56
13.14	1.12	7.78	9.90	77.03	3.25	0.06	0.56
13.16	1.13	7.81	9.83	76.81	3.24	0.06	0.56
13.19	1.13	7.78	9.79	76.23	3.24	0.06	0.56
13.20	1.12	7.73	9.84	76.12	3.24	0.06	0.55
13.22	1.10	7.57	10.05	76.05	3.26	0.06	0.54
13.24	1.09	7.44	10.21	75.93	3.27	0.06	0.53
13.26	1.09	7.42	10.19	75.66	3.27	0.06	0.53
13.28	1.11	7.59	9.98	75.71	3.25	0.06	0.54
13.30	1.13	7.71	9.91	76.36	3.25	0.06	0.55
13.32	1.14	7.81	9.90	77.28	3.25	0.06	0.56
13.34	1.16	7.98	9.74	77.74	3.23	0.06	0.57
13.36	1.18	8.17	9.56	78.09	3.22	0.06	0.58
13.38	1.21	8.35	9.39	78.44	3.21	0.06	0.60
13.40	1.21	8.39	9.47	79.52	3.22	0.06	0.60
13.42	1.23	8.51	9.46	80.46	3.21	0.06	0.61
13.44	1.24	8.55	9.48	81.12	3.22	0.06	0.61

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
13.46	1.24	8.53	9.54	81.42	3.22	0.06	0.61
13.48	1.21	8.32	9.84	81.84	3.24	0.06	0.59
13.50	1.17	7.96	10.33	82.19	3.27	0.06	0.57
13.52	1.12	7.54	10.88	82.10	3.31	0.06	0.54
13.54	1.08	7.17	11.34	81.38	3.34	0.06	0.51
13.56	1.04	6.82	11.76	80.14	3.37	0.06	0.49
13.58	1.00	6.44	12.21	78.64	3.39	0.06	0.46
13.60	0.96	6.11	12.51	76.44	3.41	0.06	0.44
13.62	0.93	5.88	12.62	74.17	3.42	0.06	0.42
13.64	0.90	5.59	12.74	71.27	3.42	0.06	0.40
13.66	0.87	5.34	12.81	68.41	3.43	0.06	0.38
13.68	0.85	5.15	12.69	65.31	3.42	0.06	0.37
13.70	0.83	5.00	12.51	62.50	3.41	0.06	0.36
13.72	0.82	4.90	12.22	59.89	3.39	0.06	0.35
13.74	0.86	5.18	11.09	57.48	3.32	0.06	0.37
13.76	0.89	5.47	10.14	55.42	3.26	0.06	0.39
13.78	0.90	5.53	9.72	53.77	3.23	0.06	0.40
13.81	0.84	5.03	10.58	53.26	3.29	0.06	0.36
13.82	0.79	4.60	11.35	52.23	3.34	0.06	0.33
13.84	0.77	4.43	11.52	51.06	3.35	0.06	0.32
13.86	0.78	4.52	11.04	49.88	3.32	0.06	0.32
13.88	0.81	4.73	10.40	49.18	3.28	0.06	0.34
13.90	0.83	4.88	10.00	48.74	3.25	0.06	0.35
13.92	0.84	5.00	9.68	48.46	3.23	0.06	0.36
13.94	0.86	5.13	9.46	48.49	3.21	0.06	0.37
13.96	0.89	5.35	9.12	48.77	3.19	0.06	0.38
13.98	0.93	5.68	8.67	49.24	3.16	0.06	0.41
14.00	0.98	6.06	8.20	49.67	3.12	0.06	0.43
14.02	1.02	6.39	7.91	50.50	3.10	0.06	0.46
14.04	1.04	6.54	7.90	51.66	3.10	0.06	0.47
14.06	1.05	6.63	8.02	53.13	3.11	0.06	0.47
14.08	1.06	6.68	8.15	54.48	3.12	0.06	0.48
14.10	1.06	6.71	8.37	56.16	3.13	0.06	0.48
14.13	1.06	6.70	8.61	57.66	3.15	0.06	0.48
14.14	1.06	6.68	8.89	59.37	3.17	0.06	0.48
14.16	1.07	6.74	8.89	59.92	3.17	0.06	0.48
14.18	1.08	6.79	8.84	60.07	3.17	0.06	0.49
14.20	1.06	6.65	9.02	59.99	3.18	0.06	0.48
14.22	1.02	6.31	9.55	60.27	3.22	0.06	0.45
14.24	0.96	5.83	10.34	60.34	3.28	0.06	0.42
14.26	0.91	5.40	11.05	59.70	3.32	0.06	0.39
14.28	0.86	4.98	11.65	58.03	3.36	0.06	0.36
14.30	0.81	4.60	12.15	55.82	3.39	0.06	0.33
14.32	0.78	4.33	12.35	53.48	3.40	0.06	0.31
14.34	0.77	4.27	12.03	51.37	3.38	0.06	0.31
14.36	0.78	4.36	11.31	49.35	3.34	0.06	0.31
14.38	0.81	4.56	10.40	47.46	3.28	0.06	0.33
14.40	0.84	4.78	9.67	46.20	3.23	0.06	0.34

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
14.42	0.86	4.94	9.23	45.63	3.20	0.06	0.35
14.44	0.86	4.92	9.29	45.74	3.20	0.06	0.35
14.46	0.85	4.84	9.62	46.55	3.23	0.06	0.35
14.48	0.84	4.79	9.80	46.96	3.24	0.06	0.34
14.50	0.87	4.96	9.52	47.23	3.22	0.06	0.35
14.52	0.89	5.12	9.21	47.09	3.20	0.06	0.37
14.54	0.90	5.19	9.05	46.93	3.19	0.06	0.37
14.56	0.90	5.21	9.02	47.00	3.18	0.06	0.37
14.58	0.93	5.43	8.67	47.10	3.16	0.06	0.39
14.60	0.96	5.64	8.36	47.18	3.13	0.06	0.40
14.62	0.95	5.56	8.58	47.70	3.15	0.06	0.40
14.64	0.90	5.17	9.29	48.00	3.20	0.06	0.37
14.66	0.85	4.75	10.19	48.41	3.27	0.06	0.34
14.68	0.83	4.64	10.44	48.43	3.28	0.06	0.33
14.70	0.92	5.29	9.33	49.35	3.21	0.06	0.38
14.72	1.30	8.32	6.46	53.75	2.97	0.06	0.59
14.74	1.79	12.25	4.71	57.63	2.79	0.08	0.87
14.76	2.27	16.12	3.91	63.06	2.69	0.08	1.13
14.78	2.38	17.00	3.91	66.44	2.69	0.08	1.20
14.80	2.37	16.85	4.15	69.85	2.72	0.08	1.19
14.82	2.39	16.96	4.25	72.04	2.73	0.08	1.20
14.84	2.60	18.64	3.95	73.58	2.69	0.09	1.31
14.86	2.77	20.08	3.67	73.67	2.65	0.09	1.41
14.88	2.75	19.86	3.63	72.14	2.65	0.09	1.39
14.90	2.47	17.55	4.02	70.57	2.70	0.08	1.24
14.92	2.18	15.08	4.67	70.35	2.79	0.08	1.07
14.94	2.02	13.74	5.24	71.94	2.85	0.07	0.98
14.96	2.08	14.23	5.08	72.24	2.83	0.08	1.02
14.98	2.16	14.83	4.89	72.45	2.81	0.08	1.06
15.00	2.06	14.03	5.28	74.00	2.86	0.08	1.00
15.02	1.81	12.03	6.39	76.85	2.97	0.07	0.86
15.04	1.51	9.71	7.97	77.36	3.10	0.06	0.69
15.06	1.38	8.72	8.64	75.40	3.16	0.06	0.62
15.08	1.42	9.00	8.15	73.35	3.12	0.06	0.64
15.10	1.59	10.26	7.00	71.83	3.02	0.07	0.73
15.12	1.68	11.00	6.50	71.53	2.98	0.07	0.79
15.14	1.65	10.71	6.68	71.52	2.99	0.07	0.77
15.17	1.60	10.29	6.90	71.05	3.01	0.06	0.74
15.18	1.59	10.21	6.83	69.79	3.01	0.07	0.73
15.20	1.54	9.81	7.23	70.96	3.04	0.07	0.70
15.22	1.38	8.61	8.31	71.56	3.13	0.06	0.62
15.24	1.20	7.21	9.80	70.65	3.24	0.06	0.51
15.26	1.06	6.14	10.94	67.12	3.31	0.06	0.44
15.28	0.98	5.50	11.72	64.47	3.36	0.06	0.39
15.30	0.91	5.00	12.31	61.57	3.40	0.06	0.36
15.32	0.90	4.86	12.18	59.12	3.39	0.06	0.35
15.34	0.89	4.83	11.71	56.53	3.36	0.06	0.34
15.36	0.89	4.77	11.39	54.32	3.34	0.06	0.34

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
15.38	0.87	4.65	11.30	52.58	3.34	0.06	0.33
15.40	0.86	4.58	11.16	51.11	3.33	0.06	0.33
15.42	0.86	4.57	11.00	50.24	3.32	0.06	0.33
15.44	0.87	4.59	10.81	49.62	3.31	0.06	0.33
15.46	0.88	4.70	10.52	49.49	3.29	0.06	0.34
15.48	0.90	4.85	10.20	49.46	3.27	0.06	0.35
15.50	0.93	5.08	9.79	49.70	3.24	0.06	0.36
15.52	0.96	5.24	9.57	50.11	3.22	0.06	0.37
15.54	0.97	5.30	9.55	50.63	3.22	0.06	0.38
15.56	0.95	5.20	9.84	51.16	3.24	0.06	0.37
15.58	0.93	5.04	10.28	51.85	3.27	0.06	0.36
15.60	0.92	4.96	10.61	52.69	3.29	0.06	0.35
15.62	0.92	4.93	10.85	53.47	3.31	0.06	0.35
15.64	0.92	4.94	10.91	53.90	3.31	0.06	0.35
15.66	0.91	4.85	11.11	53.94	3.33	0.06	0.35

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

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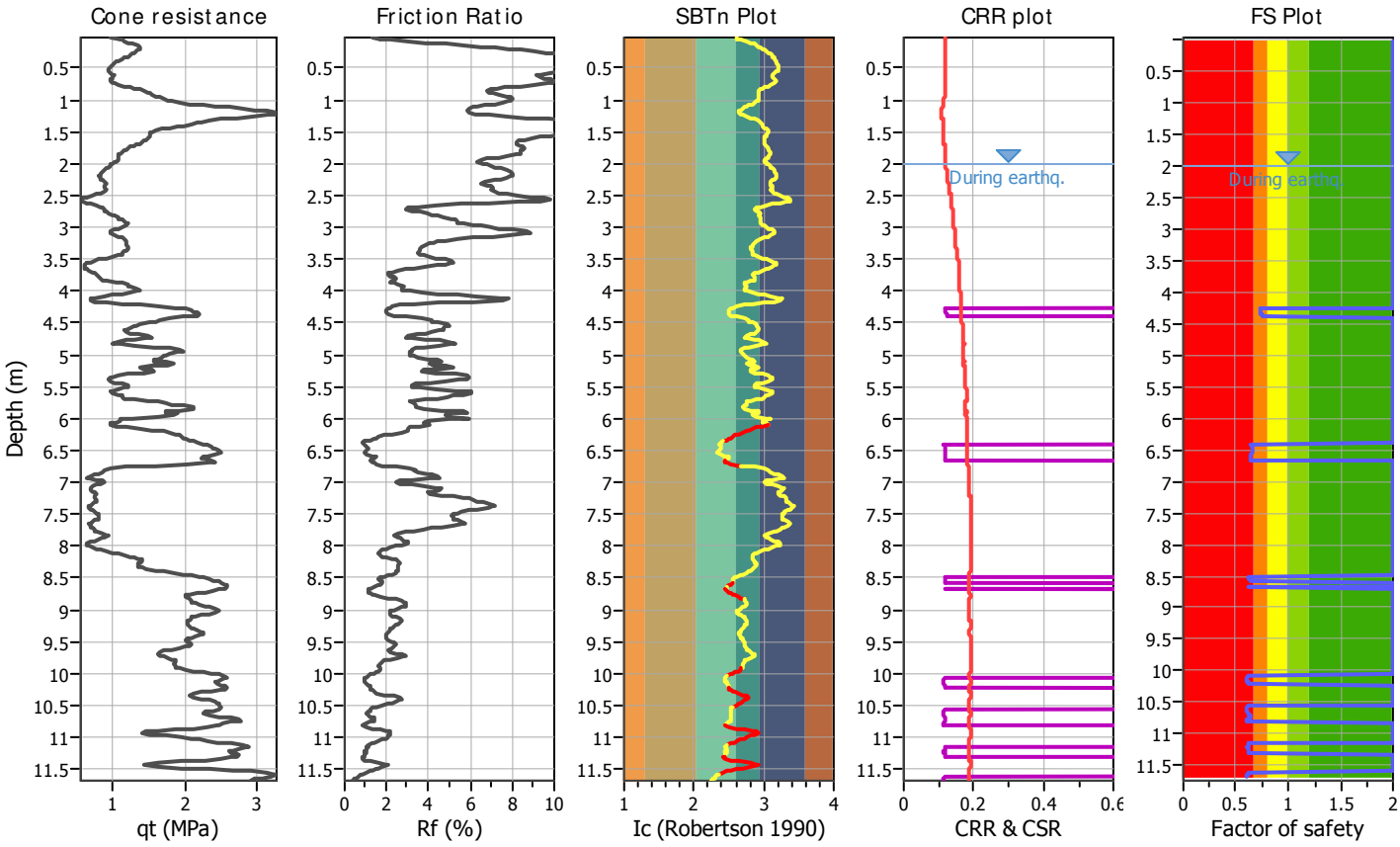
LIQUEFACTION ANALYSIS REPORT

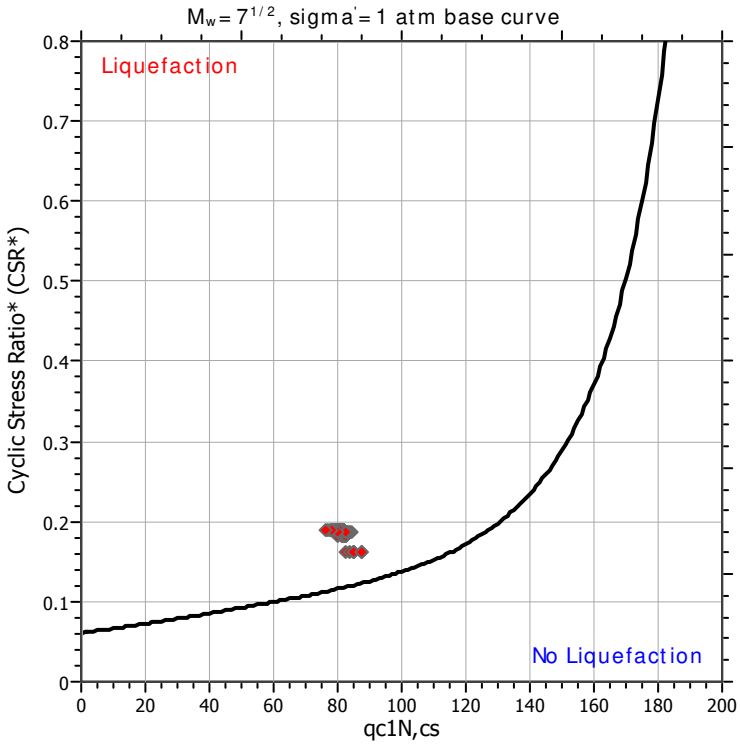
Project title : Location :

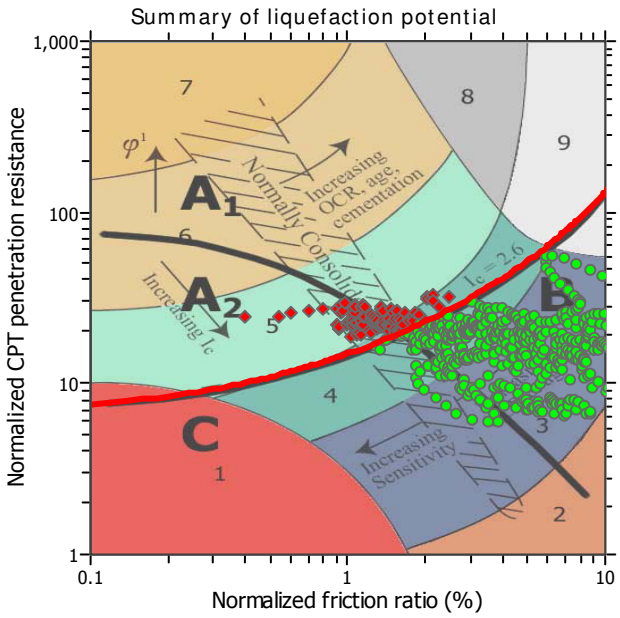
CPT file : Cptu-8

Input parameters and analysis data

Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.50 m	Use fill:	No	Clay like behavior applied:	Sands only
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	Limit depth applied:	No
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth:	N/A
Earthquake magnitude M_w:	6.14	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	MSF method:	Method based
Peak ground acceleration:	0.22	Unit weight calculation:	Based on SBT	K_σ applied:	Yes		

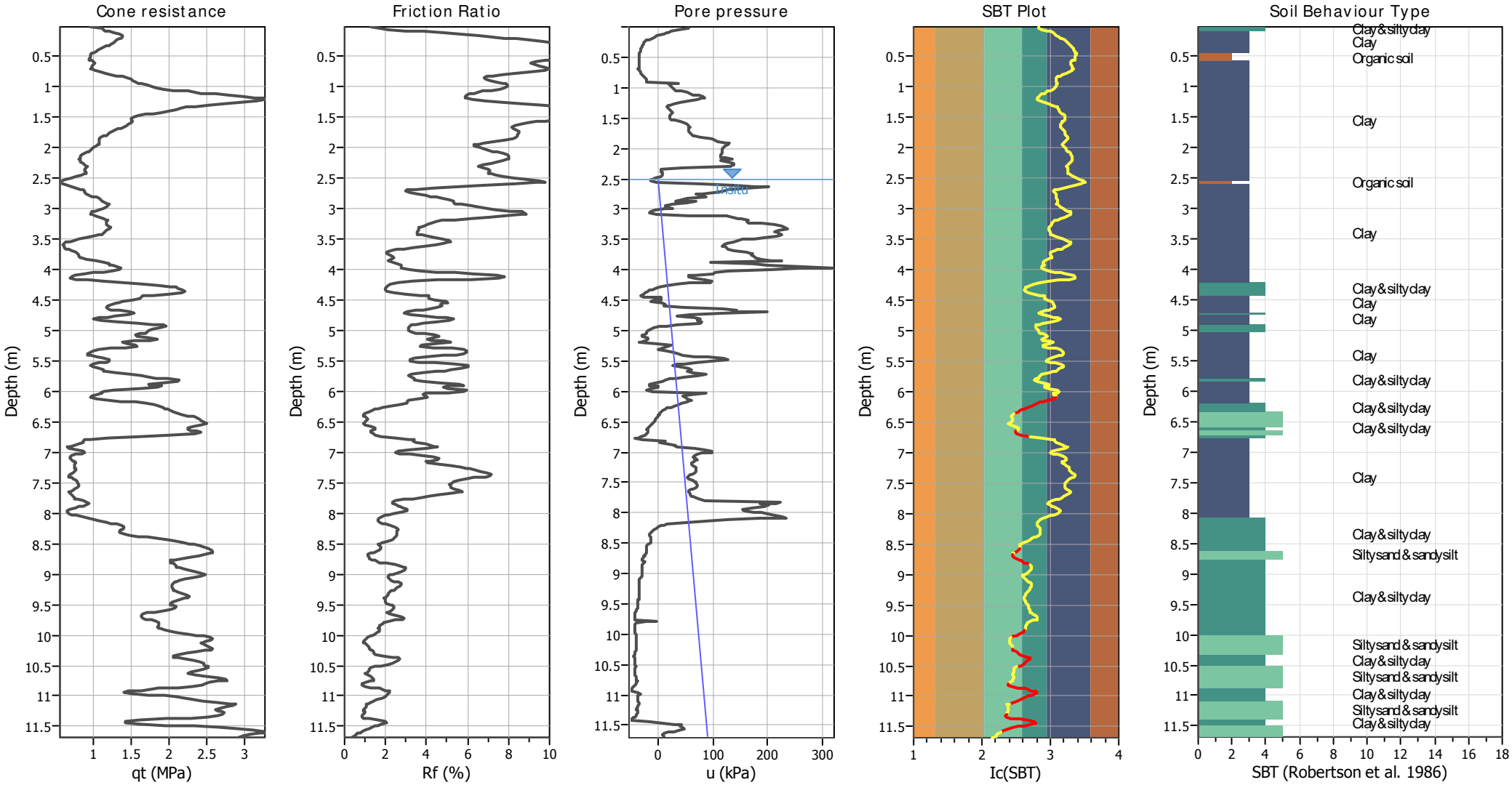






Zone A_1: Cyclic liquefaction likely depending on size and duration of cyclic loading
Zone A_2: Cyclic liquefaction and strength loss likely depending on loading and ground geometry
Zone B: Liquefaction and post-earthquake strength loss unlikely, check cyclic softening
Zone C: Cyclic liquefaction and strength loss possible depending on soil plasticity, brittleness/sensitivity, strain to peak undrained strength and ground geometry

CPT basic interpretation plots



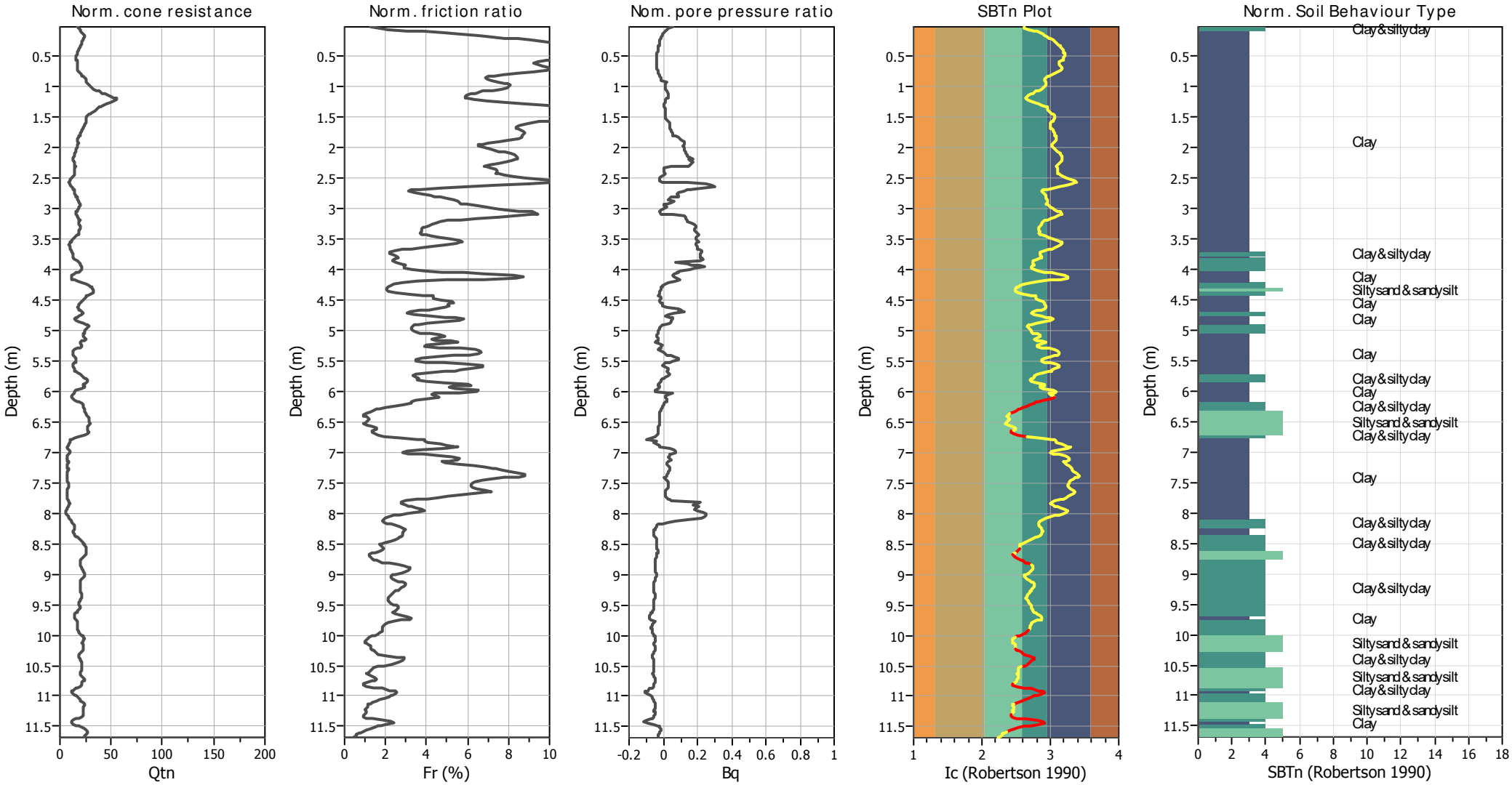
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBT legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

CPT basic interpretation plots (normalized)



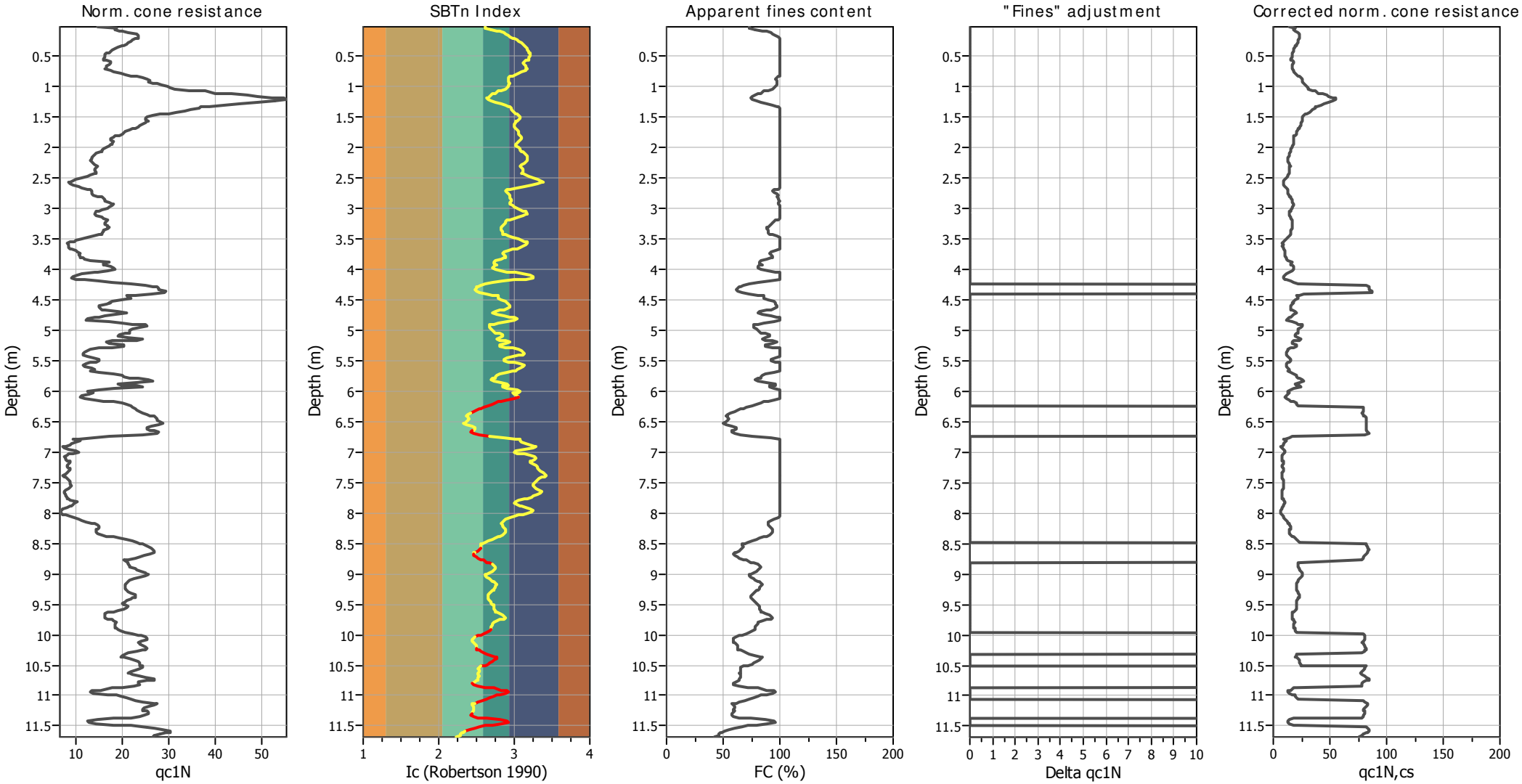
Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

SBTn legend

1. Sensitive fine grained
2. Organic material
3. Clay to silty clay
4. Clayey silt to silty
5. Silty sand to sandy silt
6. Clean sand to silty sand
7. Gravely sand to sand
8. Very stiff sand to
9. Very stiff fine grained

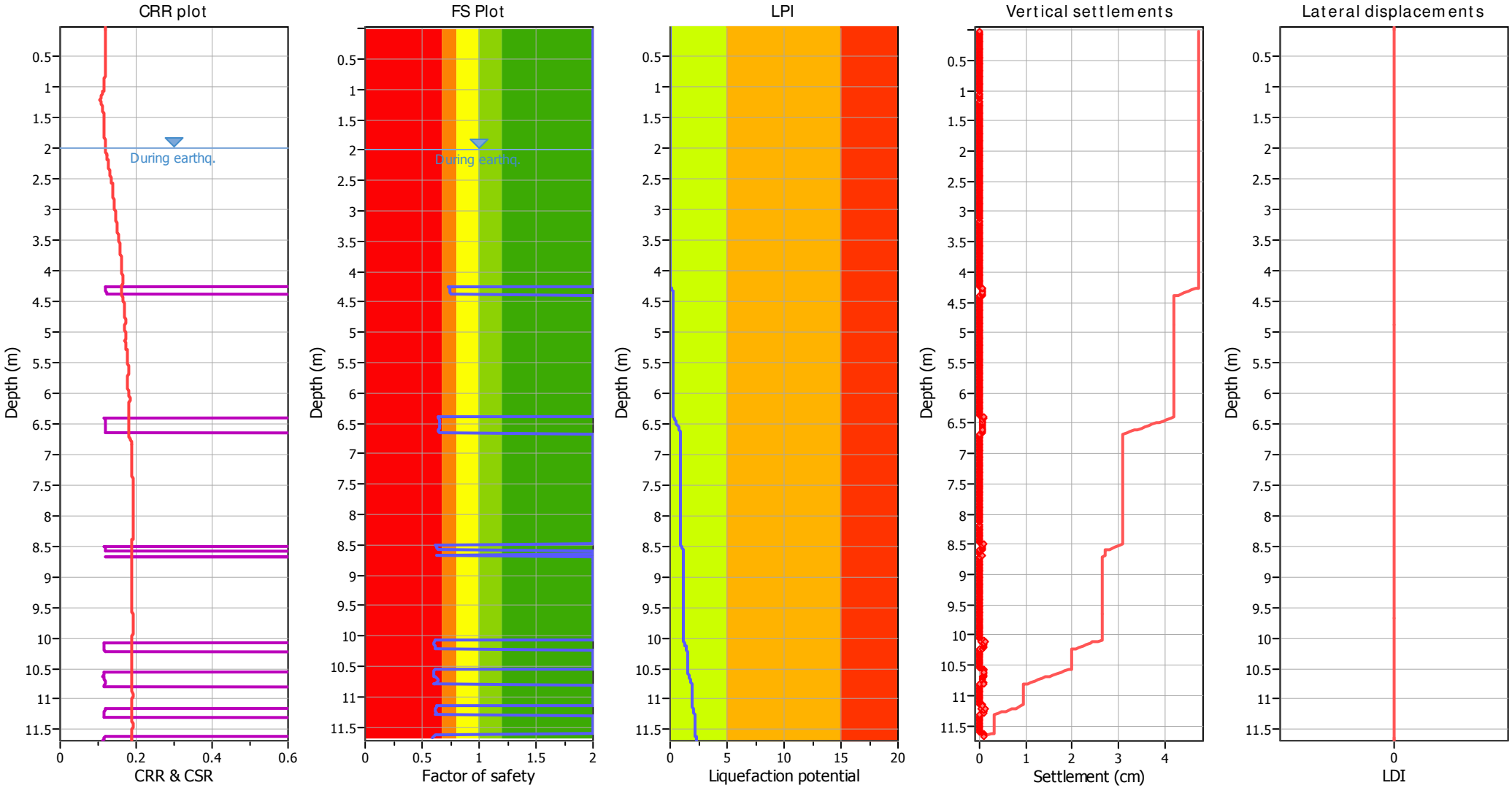
Liquefaction analysis overall plots (intermediate results)



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

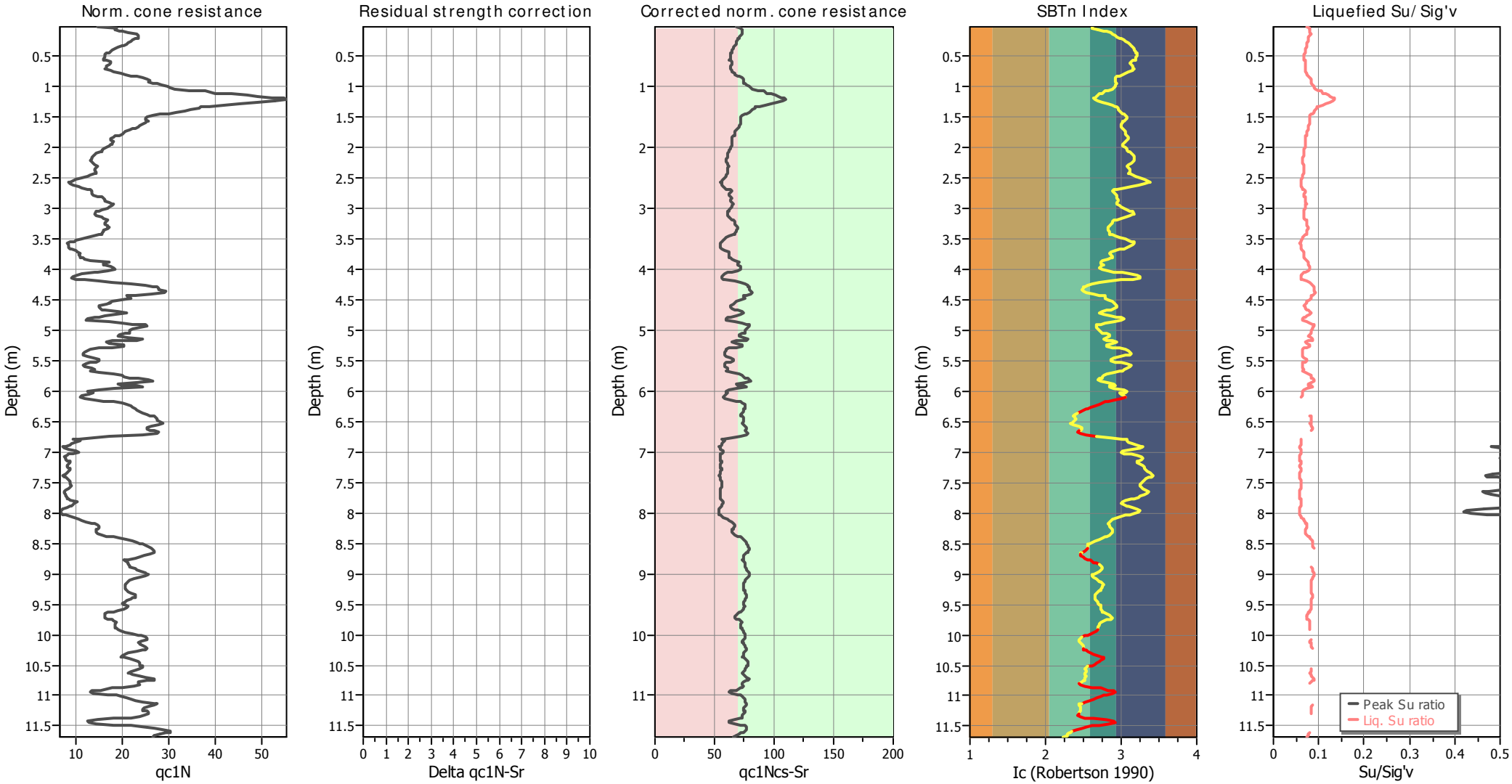
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Check for strength loss plots (Idriss & Boulanger (2008))



Input parameters and analysis data

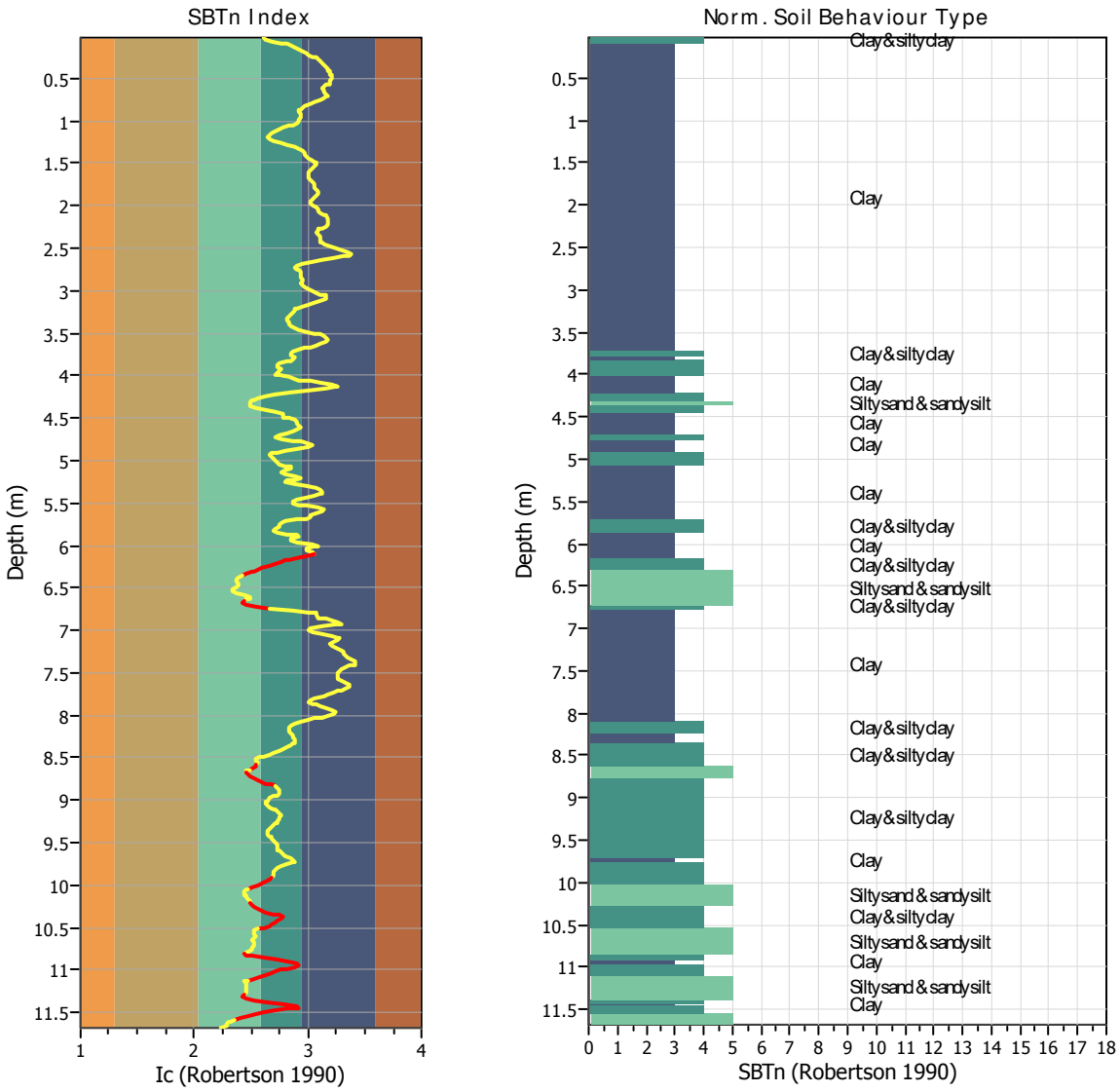
Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	Yes
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_σ applied:	Yes
Earthquake magnitude M_w:	6.14	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.22	Use fill:	No	Limit depth applied:	No
Depth to water table (insitu):	2.50 m	Fill height:	N/A	Limit depth:	N/A

TRANSITION LAYER DETECTION ALGORITHM REPORT
Summary Details & Plots

Short description

The software will delete data when the cone is in transition from either clay to sand or vise-versa. To do this the software requires a range of I_c values over which the transition will be defined (typically somewhere between $1.80 < I_c < 3.0$) and a rate of change of I_c. Transitions typically occur when the rate of change of I_c is fast (i.e. delta I_c is small).

The SBT_n plot below, displays in red the detected transition layers based on the parameters listed below the graphs.



Transition layer algorithm properties		General statistics	
I_c minimum check value:	1.70	Total points in CPT file:	584
I_c maximum check value:	3.00	Total points excluded:	88
I_c change ratio value:	0.0100	Exclusion percentage:	15.07%
Minimum number of points in layer:	4	Number of layers detected:	11

Transition layer No	Number of points	Depth	SBT_n number	SBT_n description
Transition layer 1	14	Start depth: 6.12 (m)	3	Clay
		End depth: 6.38 (m)	5	Silty sand & sandy silt
Transition layer 2	5	Start depth: 6.68 (m)	5	Silty sand & sandy silt
		End depth: 6.76 (m)	3	Clay
Transition layer 3	4	Start depth: 8.60 (m)	4	Clay & silty clay
		End depth: 8.66 (m)	5	Silty sand & sandy silt
Transition layer 4	9	Start depth: 8.70 (m)	5	Silty sand & sandy silt
		End depth: 8.86 (m)	4	Clay & silty clay
Transition layer 5	7	Start depth: 9.94 (m)	4	Clay & silty clay
		End depth: 10.06 (m)	5	Silty sand & sandy silt
Transition layer 6	8	Start depth: 10.24 (m)	5	Silty sand & sandy silt
		End depth: 10.38 (m)	4	Clay & silty clay
Transition layer 7	8	Start depth: 10.40 (m)	4	Clay & silty clay
		End depth: 10.54 (m)	5	Silty sand & sandy silt
Transition layer 8	7	Start depth: 10.82 (m)	5	Silty sand & sandy silt
		End depth: 10.94 (m)	3	Clay
Transition layer 9	11	Start depth: 10.94 (m)	3	Clay
		End depth: 11.14 (m)	5	Silty sand & sandy silt
Transition layer 10	6	Start depth: 11.32 (m)	5	Silty sand & sandy silt
		End depth: 11.42 (m)	3	Clay
Transition layer 11	9	Start depth: 11.44 (m)	3	Clay
		End depth: 11.60 (m)	5	Silty sand & sandy silt

Start depth: Depth where the transition layer begins
End depth: Depth where the transition layer ends

:: Field input data ::

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
1	0.02	0.88	10.70	55.36	36.31	15.89
2	0.04	1.12	16.38	35.90	36.54	16.40
3	0.06	1.10	23.47	24.55	39.54	16.71
4	0.08	1.16	33.38	18.85	43.90	17.12
5	0.10	1.18	47.21	15.81	46.80	17.47
6	0.12	1.27	58.40	8.87	49.50	17.82
7	0.14	1.38	79.47	-2.60	51.23	18.08
8	0.16	1.40	89.66	-6.76	53.39	18.29
9	0.18	1.39	101.03	-12.03	55.25	18.41
10	0.20	1.39	107.68	-16.92	57.20	18.49
11	0.22	1.36	113.22	-22.19	59.10	18.55
12	0.24	1.32	119.38	-24.74	61.14	18.59
13	0.26	1.29	123.89	-26.78	63.08	18.63
14	0.28	1.27	128.44	-28.33	64.64	18.66
15	0.30	1.24	130.86	-29.20	66.15	18.67
16	0.32	1.21	131.44	-30.19	67.32	18.67
17	0.34	1.18	130.53	-30.94	68.62	18.65
18	0.36	1.13	128.42	-32.05	69.60	18.62
19	0.38	1.10	124.29	-32.86	70.80	18.57
20	0.40	1.06	121.07	-33.54	71.65	18.53
21	0.42	1.04	118.75	-34.72	72.31	18.50
22	0.45	1.03	116.47	-34.78	73.01	18.46
23	0.46	0.98	114.33	-35.34	73.66	18.44
24	0.48	0.97	113.31	-35.52	74.10	18.41
25	0.50	0.97	109.12	-35.34	73.57	18.37
26	0.52	0.97	104.29	-35.34	73.05	18.32
27	0.54	0.95	100.98	-35.77	72.73	18.28
28	0.56	0.94	97.88	-35.65	71.95	18.24
29	0.58	0.98	95.10	-35.34	69.95	18.22
30	0.60	1.03	92.93	-35.34	68.07	18.22
31	0.62	1.04	93.49	-35.34	67.21	18.22
32	0.64	1.03	93.84	-35.65	68.02	18.22
33	0.66	0.99	94.69	-36.14	69.07	18.22
34	0.68	0.98	95.31	-36.58	69.99	18.23
35	0.70	0.99	96.83	-36.33	70.60	18.24
36	0.72	0.97	99.18	-35.96	70.09	18.27
37	0.74	1.04	99.94	-33.73	68.89	18.30
38	0.76	1.09	100.97	-32.05	65.80	18.31
39	0.78	1.18	97.01	-30.13	62.67	18.30
40	0.80	1.23	92.35	-28.52	59.48	18.30
41	0.82	1.31	94.32	-26.41	57.10	18.32
42	0.84	1.38	95.61	-24.67	55.20	18.36
43	0.86	1.46	98.54	-22.44	53.86	18.41
44	0.88	1.51	101.70	-21.70	53.21	18.47
45	0.90	1.55	107.97	-20.89	53.56	18.54
46	0.92	1.53	115.25	35.96	53.90	18.61
47	0.94	1.59	120.67	18.41	54.42	18.70
48	0.96	1.63	131.40	20.21	54.22	18.77

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
49	0.98	1.69	136.05	24.24	53.75	18.84
50	1.00	1.77	140.44	27.34	52.95	18.88
51	1.02	1.80	141.63	29.82	52.14	18.92
52	1.05	1.86	145.03	31.99	50.56	18.96
53	1.06	2.06	148.69	41.79	48.03	19.01
54	1.08	2.25	148.63	53.13	45.43	19.07
55	1.11	2.40	155.10	62.86	43.05	19.12
56	1.12	2.60	157.14	74.52	41.27	19.19
57	1.14	2.80	166.49	81.59	39.74	19.26
58	1.17	2.94	174.25	84.81	38.61	19.34
59	1.18	3.13	182.55	79.60	37.77	19.42
60	1.20	3.28	192.76	71.48	37.46	19.49
61	1.22	3.31	204.33	54.93	38.33	19.56
62	1.24	3.17	216.39	39.49	40.53	19.61
63	1.26	2.93	229.25	28.02	43.68	19.64
64	1.28	2.70	236.89	21.26	47.23	19.66
65	1.30	2.50	244.46	17.85	50.72	19.66
66	1.32	2.31	249.43	16.24	53.62	19.65
67	1.34	2.21	246.25	17.42	55.29	19.62
68	1.36	2.18	237.78	19.84	56.00	19.57
69	1.38	2.08	225.52	23.74	56.31	19.50
70	1.40	2.00	212.74	25.79	57.05	19.42
71	1.42	1.89	201.00	24.86	57.94	19.34
72	1.44	1.79	192.04	23.50	59.28	19.26
73	1.46	1.68	183.39	21.70	60.79	19.18
74	1.48	1.58	174.61	20.52	62.37	19.12
75	1.50	1.51	171.15	21.33	63.18	19.06
76	1.52	1.50	163.45	23.31	63.15	19.01
77	1.54	1.49	155.56	28.27	62.00	18.95
78	1.56	1.52	148.95	38.19	60.80	18.90
79	1.58	1.51	141.16	48.23	59.77	18.84
80	1.60	1.48	134.12	53.07	59.15	18.77
81	1.62	1.46	125.64	55.49	58.69	18.70
82	1.64	1.42	118.08	56.17	58.42	18.63
83	1.66	1.40	114.62	56.73	58.49	18.58
84	1.68	1.37	112.09	55.24	59.15	18.54
85	1.70	1.32	110.98	54.25	59.79	18.51
86	1.72	1.29	106.87	54.87	60.96	18.47
87	1.74	1.23	106.96	57.28	61.85	18.44
88	1.76	1.21	105.64	60.94	62.61	18.41
89	1.78	1.20	101.03	63.05	62.83	18.37
90	1.80	1.16	98.28	65.10	63.35	18.33
91	1.82	1.11	95.55	76.07	64.12	18.27
92	1.84	1.08	91.48	97.46	64.82	18.22
93	1.86	1.05	88.46	104.53	64.88	18.17
94	1.88	1.03	84.71	107.44	63.72	18.10
95	1.90	1.07	77.32	124.67	62.39	18.04
96	1.92	1.05	74.39	130.38	60.72	17.97

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
97	1.94	1.06	70.11	127.96	59.97	17.90
98	1.96	1.04	65.02	122.63	59.66	17.85
99	1.98	1.01	65.54	119.34	60.27	17.82
100	2.00	0.99	66.51	116.80	61.82	17.82
101	2.02	0.95	66.83	117.42	63.27	17.81
102	2.04	0.93	67.27	116.00	64.39	17.81
103	2.06	0.93	67.89	116.18	65.32	17.82
104	2.08	0.91	69.35	116.12	66.69	17.83
105	2.10	0.86	69.41	114.51	68.53	17.81
106	2.12	0.83	68.18	113.02	69.86	17.78
107	2.15	0.82	66.48	113.58	70.74	17.76
108	2.16	0.80	66.31	121.33	71.13	17.74
109	2.18	0.79	66.45	136.02	71.42	17.73
110	2.20	0.80	65.60	113.27	71.39	17.72
111	2.22	0.79	63.99	126.10	70.61	17.70
112	2.24	0.81	62.26	137.69	69.43	17.68
113	2.26	0.84	61.65	136.58	67.67	17.67
114	2.28	0.86	60.68	134.84	65.46	17.67
115	2.30	0.91	59.16	132.30	64.27	17.66
116	2.32	0.91	59.48	44.45	64.14	17.67
117	2.34	0.90	61.73	4.09	65.44	17.68
118	2.36	0.88	62.20	4.96	66.48	17.70
119	2.38	0.89	64.02	3.66	66.54	17.72
120	2.40	0.92	64.19	6.08	66.17	17.74
121	2.42	0.92	64.40	8.25	65.86	17.74
122	2.44	0.90	63.26	7.32	67.14	17.72
123	2.46	0.84	63.02	3.53	69.10	17.67
124	2.48	0.79	60.35	-6.70	72.42	17.61
125	2.50	0.72	58.39	-11.59	76.28	17.54
126	2.52	0.64	57.13	-13.14	81.18	17.48
127	2.54	0.59	56.49	-12.90	85.76	17.43
128	2.56	0.55	55.55	-3.04	88.10	17.38
129	2.58	0.54	53.56	74.09	86.87	17.34
130	2.60	0.57	49.98	138.56	82.16	17.28
131	2.62	0.61	45.12	174.02	75.07	17.20
132	2.64	0.68	39.23	201.74	67.96	17.08
133	2.66	0.74	33.31	162.37	60.97	16.94
134	2.68	0.81	28.74	126.35	55.29	16.79
135	2.70	0.86	25.28	120.21	51.72	16.72
136	2.72	0.88	26.16	103.22	50.65	16.72
137	2.74	0.88	28.04	79.36	51.88	16.81
138	2.76	0.88	31.85	69.93	53.43	16.94
139	2.78	0.91	36.68	80.53	54.51	17.12
140	2.80	0.97	42.60	88.34	54.30	17.27
141	2.82	1.04	45.21	51.33	54.16	17.41
142	2.84	1.07	50.72	42.28	54.52	17.53
143	2.86	1.09	56.40	32.55	55.46	17.65
144	2.88	1.09	59.80	69.31	55.62	17.73

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
145	2.90	1.16	62.20	51.83	55.03	17.80
146	2.92	1.21	64.37	26.60	54.48	17.86
147	2.94	1.23	68.59	12.34	55.21	17.94
148	2.96	1.21	74.63	11.66	56.99	18.01
149	2.98	1.16	78.49	26.22	58.71	18.05
150	3.00	1.15	77.82	13.95	60.93	18.05
151	3.02	1.07	79.37	-6.57	63.34	18.05
152	3.04	1.02	81.95	-14.07	66.67	18.07
153	3.06	0.98	84.88	-17.61	69.28	18.08
154	3.09	0.95	86.78	-3.97	70.29	18.09
155	3.10	0.96	85.17	55.92	69.41	18.08
156	3.12	0.98	81.39	125.17	66.04	18.05
157	3.15	1.07	76.32	145.07	62.70	18.01
158	3.16	1.09	72.34	151.77	58.35	17.93
159	3.18	1.17	61.99	163.73	55.23	17.83
160	3.20	1.17	56.42	162.31	52.48	17.71
161	3.22	1.15	52.38	164.41	51.45	17.61
162	3.24	1.13	49.27	188.96	50.70	17.54
163	3.26	1.13	47.54	213.21	49.74	17.50
164	3.28	1.16	46.16	224.74	48.83	17.48
165	3.30	1.17	45.96	231.06	47.75	17.46
166	3.32	1.20	44.55	237.07	47.26	17.44
167	3.34	1.18	43.64	220.64	47.40	17.40
168	3.36	1.12	42.30	213.39	47.94	17.36
169	3.38	1.11	40.98	213.83	48.42	17.32
170	3.40	1.10	39.89	220.77	48.35	17.29
171	3.42	1.09	39.83	226.97	49.06	17.28
172	3.44	1.05	40.92	218.66	50.83	17.27
173	3.46	0.96	40.45	193.92	53.71	17.24
174	3.48	0.88	39.13	174.40	57.60	17.19
175	3.50	0.79	39.57	153.50	61.99	17.13
176	3.52	0.71	39.10	146.06	65.81	17.07
177	3.54	0.67	36.38	138.19	68.71	16.96
178	3.56	0.61	32.25	124.92	70.48	16.84
179	3.58	0.57	30.14	117.92	70.86	16.71
180	3.60	0.59	27.30	116.62	69.61	16.59
181	3.62	0.58	23.55	120.64	66.63	16.44
182	3.64	0.59	20.29	123.87	63.48	16.29
183	3.66	0.61	18.04	126.66	60.49	16.19
184	3.68	0.63	17.92	137.94	56.65	16.12
185	3.70	0.69	16.14	161.25	52.97	16.08
186	3.72	0.74	14.97	170.43	49.64	16.04
187	3.74	0.77	15.61	171.85	48.99	16.10
188	3.76	0.76	17.78	169.75	49.52	16.19
189	3.78	0.78	19.04	175.20	50.62	16.30
190	3.80	0.78	20.45	178.24	50.46	16.36
191	3.82	0.81	20.71	187.54	49.45	16.40
192	3.84	0.86	20.33	207.63	47.02	16.42

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
193	3.86	0.93	20.22	226.72	43.30	16.59
194	3.88	1.24	27.22	94.23	42.38	16.82
195	3.90	1.16	32.64	173.09	42.35	17.01
196	3.92	1.16	32.85	198.95	43.86	17.10
197	3.94	1.17	35.22	260.82	42.92	17.15
198	3.96	1.29	35.78	318.97	42.02	17.22
199	3.98	1.32	37.45	257.41	41.36	17.29
200	4.00	1.35	40.29	209.36	43.47	17.39
201	4.02	1.23	47.06	127.96	47.58	17.48
202	4.05	1.08	51.45	104.22	52.78	17.55
203	4.06	1.04	53.09	99.44	59.69	17.57
204	4.08	0.81	56.11	65.65	66.08	17.55
205	4.10	0.75	56.61	54.68	74.01	17.52
206	4.12	0.69	56.82	56.04	77.35	17.48
207	4.14	0.66	53.06	64.66	76.87	17.42
208	4.16	0.72	48.70	83.51	69.76	17.32
209	4.18	0.87	40.08	99.26	58.57	17.25
210	4.20	1.12	36.71	94.67	48.62	17.20
211	4.22	1.34	35.75	59.21	41.28	17.25
212	4.24	1.65	37.47	33.97	36.42	17.35
213	4.26	1.90	40.05	15.62	33.49	17.47
214	4.28	2.02	42.98	2.79	31.86	17.55
215	4.30	2.11	42.31	-5.15	31.06	17.58
216	4.32	2.13	41.49	-12.21	30.54	17.57
217	4.34	2.12	41.28	-17.23	30.15	17.60
218	4.36	2.27	44.62	-20.33	30.62	17.69
219	4.38	2.22	51.13	-24.12	32.56	17.82
220	4.40	2.02	59.53	-27.96	36.65	17.94
221	4.42	1.75	66.60	-32.05	41.51	18.02
222	4.44	1.61	69.97	-26.22	44.79	18.05
223	4.46	1.64	70.17	5.64	45.02	18.03
224	4.49	1.69	63.75	5.89	45.45	18.00
225	4.50	1.51	66.10	-7.87	47.70	17.99
226	4.52	1.36	71.46	-13.33	51.40	17.99
227	4.54	1.31	69.52	6.20	52.58	17.93
228	4.56	1.33	59.47	12.71	52.54	17.85
229	4.58	1.26	59.56	13.64	52.99	17.75
230	4.60	1.15	56.42	11.22	54.42	17.70
231	4.62	1.15	53.99	45.20	54.15	17.62
232	4.64	1.17	49.33	118.60	52.31	17.56
233	4.66	1.20	46.63	143.27	50.11	17.51
234	4.68	1.26	46.28	134.53	46.72	17.52
235	4.70	1.49	46.75	199.81	42.88	17.52
236	4.72	1.63	42.27	119.28	41.58	17.52
237	4.74	1.43	44.32	59.08	44.10	17.55
238	4.76	1.27	52.49	35.09	49.68	17.61
239	4.78	1.16	55.54	66.21	54.11	17.63
240	4.80	1.09	52.67	77.81	58.08	17.60

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
241	4.82	0.96	53.08	70.86	61.27	17.57
242	4.84	0.94	55.25	70.86	58.61	17.66
243	4.86	1.35	60.86	77.99	52.19	17.78
244	4.88	1.58	60.40	76.26	45.57	17.87
245	4.90	1.76	58.87	32.98	41.71	17.95
246	4.92	1.99	65.23	14.57	39.50	18.00
247	4.94	2.02	63.65	2.11	38.86	18.00
248	4.96	1.89	58.26	-8.56	39.39	17.92
249	4.98	1.76	54.30	-15.00	40.43	17.82
250	5.00	1.71	53.16	-19.47	41.22	17.79
251	5.02	1.72	54.62	-21.70	42.12	17.82
252	5.04	1.71	60.37	-22.63	43.37	17.88
253	5.06	1.64	61.83	-26.10	45.93	17.96
254	5.08	1.54	69.60	-28.77	48.57	18.02
255	5.10	1.52	74.72	-28.70	49.18	18.11
256	5.12	1.71	76.25	-19.84	46.27	18.15
257	5.14	1.97	72.20	-19.90	44.05	18.19
258	5.16	1.88	75.92	-23.37	45.91	18.17
259	5.18	1.44	76.45	-31.49	50.71	18.12
260	5.20	1.33	71.73	-35.03	54.40	18.02
261	5.22	1.38	65.78	-3.78	50.74	17.92
262	5.24	1.63	55.68	22.13	46.50	17.84
263	5.26	1.65	53.95	14.26	46.00	17.83
264	5.28	1.42	63.41	6.63	50.65	17.86
265	5.30	1.20	66.69	-0.87	57.74	17.86
266	5.32	1.06	62.85	-1.05	63.10	17.79
267	5.34	1.00	60.68	16.24	65.89	17.70
268	5.36	0.94	56.52	29.20	67.28	17.64
269	5.38	0.93	55.64	36.02	67.66	17.57
270	5.40	0.92	51.95	43.96	66.42	17.49
271	5.42	0.94	46.41	66.77	62.89	17.39
272	5.44	1.01	40.81	90.64	57.77	17.30
273	5.46	1.12	39.08	118.97	52.62	17.25
274	5.48	1.22	36.95	126.53	50.01	17.25
275	5.50	1.22	38.53	95.78	49.91	17.28
276	5.52	1.18	41.78	67.95	53.04	17.36
277	5.54	1.07	46.88	46.37	58.26	17.46
278	5.56	0.99	54.20	35.03	64.32	17.56
279	5.58	0.93	58.72	27.34	68.08	17.65
280	5.60	0.96	61.29	41.54	67.13	17.72
281	5.62	1.10	62.56	56.48	63.58	17.75
282	5.64	1.16	60.24	61.69	60.56	17.73
283	5.66	1.12	54.82	56.29	59.68	17.67
284	5.68	1.09	52.65	53.13	57.36	17.59
285	5.70	1.24	48.73	64.10	52.24	17.58
286	5.72	1.49	47.44	87.29	46.40	17.59
287	5.74	1.67	47.79	72.23	44.04	17.71
288	5.76	1.70	59.04	48.42	43.51	17.84

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
289	5.78	1.79	63.11	32.67	43.13	17.98
290	5.80	1.97	65.40	20.40	41.50	18.09
291	5.82	2.16	72.84	12.46	40.10	18.20
292	5.84	2.25	77.44	7.87	42.07	18.32
293	5.87	1.92	90.37	-7.13	47.09	18.41
294	5.88	1.61	100.33	-16.37	52.67	18.47
295	5.90	1.68	101.88	-16.92	53.15	18.51
296	5.92	1.95	101.65	-1.92	49.01	18.49
297	5.94	2.07	86.00	0.31	48.72	18.39
298	5.96	1.53	80.64	-13.64	52.22	18.23
299	5.99	1.27	77.03	-21.39	61.50	18.06
300	6.00	1.03	69.79	-11.04	64.27	17.86
301	6.02	1.10	51.77	69.87	62.19	17.64
302	6.04	1.14	44.39	86.55	57.35	17.39
303	6.06	1.07	36.48	61.07	58.08	17.27
304	6.08	0.94	40.29	45.38	61.01	17.19
305	6.10	0.91	39.58	49.16	62.21	17.19
306	6.12	1.01	37.30	53.01	57.87	17.18
307	6.14	1.18	36.42	59.33	52.07	17.22
308	6.16	1.35	38.53	57.47	48.12	17.39
309	6.18	1.56	49.34	53.38	45.63	17.59
310	6.20	1.72	54.23	41.10	43.70	17.73
311	6.22	1.80	51.42	37.45	41.04	17.70
312	6.24	1.87	42.01	28.64	38.11	17.56
313	6.26	1.92	35.77	22.75	35.12	17.36
314	6.28	1.95	30.17	16.12	33.23	17.23
315	6.30	1.97	29.59	11.66	32.07	17.15
316	6.32	2.00	29.09	7.25	30.88	17.07
317	6.34	2.05	23.91	4.15	29.12	16.94
318	6.36	2.10	20.07	3.35	27.01	16.77
319	6.38	2.18	18.66	2.29	25.67	16.70
320	6.40	2.25	19.72	0.62	25.22	16.77
321	6.42	2.34	22.71	-1.18	25.54	16.91
322	6.44	2.37	26.16	-3.53	25.95	17.03
323	6.46	2.39	26.93	-4.96	26.22	17.10
324	6.48	2.41	26.93	-7.19	25.85	17.09
325	6.50	2.46	25.23	-9.18	25.05	17.04
326	6.52	2.51	23.09	-9.92	24.02	16.95
327	6.54	2.53	21.16	-10.97	23.87	16.92
328	6.56	2.43	23.12	-13.45	25.36	17.01
329	6.58	2.31	29.78	-16.86	28.14	17.21
330	6.60	2.23	35.93	-19.22	30.09	17.32
331	6.62	2.23	33.38	-20.58	30.12	17.31
332	6.64	2.28	28.66	-20.27	28.70	17.21
333	6.66	2.36	27.43	-20.33	27.88	17.23
334	6.68	2.46	33.85	-20.40	27.70	17.28
335	6.70	2.43	31.80	-21.64	29.01	17.32
336	6.72	2.14	32.10	-24.74	32.38	17.19

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
337	6.74	1.52	27.85	-32.05	38.60	17.03
338	6.76	1.20	25.83	-36.95	49.75	16.96
339	6.78	0.91	35.58	-41.97	59.28	16.89
340	6.80	0.82	28.99	-30.01	63.41	16.87
341	6.82	0.96	26.34	13.89	63.73	16.83
342	6.85	0.86	32.67	2.29	65.07	16.86
343	6.86	0.78	32.38	18.72	70.03	16.89
344	6.88	0.76	30.53	31.68	73.76	16.83
345	6.90	0.68	30.74	28.70	77.87	16.78
346	6.92	0.61	30.30	32.86	80.45	16.73
347	6.94	0.65	27.90	65.78	76.90	16.66
348	6.96	0.75	24.82	83.57	67.69	16.60
349	6.98	0.89	22.65	98.02	60.23	16.52
350	7.00	0.92	20.48	99.01	58.50	16.51
351	7.02	0.82	23.15	80.16	61.54	16.51
352	7.04	0.75	24.06	71.92	67.99	16.57
353	7.06	0.70	26.73	64.91	73.89	16.65
354	7.08	0.66	29.98	63.73	77.86	16.76
355	7.10	0.69	32.94	68.57	79.52	16.83
356	7.12	0.69	32.97	70.68	78.28	16.86
357	7.14	0.72	31.45	65.65	75.38	16.83
358	7.16	0.76	28.87	65.59	73.16	16.81
359	7.18	0.77	30.74	60.94	73.24	16.86
360	7.20	0.75	34.76	61.44	76.28	16.96
361	7.22	0.73	38.77	64.60	79.77	17.08
362	7.24	0.73	42.93	68.20	81.74	17.19
363	7.26	0.75	45.69	69.56	82.36	17.27
364	7.28	0.76	47.85	69.81	82.08	17.34
365	7.30	0.78	49.61	69.19	83.01	17.38
366	7.32	0.75	51.08	68.01	84.88	17.39
367	7.34	0.72	50.61	65.53	87.82	17.38
368	7.36	0.68	49.70	60.01	90.82	17.34
369	7.38	0.64	48.33	57.90	91.83	17.29
370	7.40	0.67	45.92	54.49	90.81	17.26
371	7.42	0.70	45.28	51.77	87.25	17.23
372	7.44	0.73	43.61	56.23	84.06	17.22
373	7.46	0.75	42.49	62.12	81.37	17.20
374	7.48	0.77	42.08	66.09	79.42	17.19
375	7.50	0.79	40.88	69.62	78.43	17.19
376	7.52	0.79	41.59	69.50	77.72	17.19
377	7.54	0.80	41.88	70.18	77.45	17.21
378	7.56	0.81	42.41	70.49	77.64	17.20
379	7.58	0.78	41.32	67.76	78.44	17.19
380	7.60	0.76	40.53	64.60	80.89	17.15
381	7.62	0.71	40.42	60.20	84.04	17.13
382	7.64	0.67	41.18	56.54	86.58	17.10
383	7.66	0.68	39.10	55.36	86.95	17.05
384	7.68	0.67	35.96	57.28	84.31	16.97

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
385	7.70	0.70	32.53	58.90	81.05	16.87
386	7.72	0.72	30.13	60.76	77.45	16.79
387	7.74	0.74	28.05	63.98	74.84	16.70
388	7.76	0.74	25.50	68.20	71.64	16.60
389	7.78	0.77	22.57	76.88	68.36	16.51
390	7.80	0.80	21.31	83.38	62.36	16.47
391	7.82	0.94	21.07	222.26	59.57	16.49
392	7.84	0.90	22.39	215.38	58.70	16.53
393	7.86	0.86	22.92	186.42	61.48	16.55
394	7.88	0.82	23.30	200.56	63.56	16.53
395	7.90	0.79	22.13	193.99	65.84	16.49
396	7.92	0.74	21.78	171.92	69.35	16.44
397	7.94	0.66	21.84	155.18	73.58	16.37
398	7.96	0.62	20.11	157.78	76.76	16.28
399	7.99	0.60	18.62	174.71	75.32	16.16
400	8.00	0.64	15.77	188.90	71.57	16.06
401	8.02	0.67	14.93	198.76	67.02	16.00
402	8.04	0.72	15.42	211.35	62.88	16.03
403	8.06	0.81	15.63	225.79	58.74	16.08
404	8.08	0.88	15.69	232.42	54.56	16.13
405	8.10	0.98	15.95	184.50	51.55	16.20
406	8.12	1.06	17.24	127.03	49.51	16.31
407	8.14	1.14	19.32	88.34	48.24	16.48
408	8.17	1.25	22.84	52.39	47.76	16.66
409	8.18	1.30	25.98	16.31	47.76	16.86
410	8.20	1.37	30.69	9.73	48.29	17.03
411	8.22	1.41	34.53	5.08	48.95	17.17
412	8.24	1.41	36.82	-0.43	49.74	17.24
413	8.26	1.39	37.08	-4.28	50.49	17.25
414	8.28	1.36	35.85	-8.93	50.90	17.22
415	8.30	1.34	34.01	-12.40	50.97	17.18
416	8.32	1.35	34.30	-14.07	50.77	17.18
417	8.34	1.37	35.21	-15.19	49.90	17.23
418	8.36	1.48	37.55	-16.00	48.58	17.31
419	8.38	1.58	40.04	-15.50	46.64	17.41
420	8.40	1.72	42.53	-14.82	44.82	17.51
421	8.42	1.85	45.70	-13.64	42.68	17.59
422	8.44	1.99	45.49	-13.02	40.67	17.65
423	8.46	2.10	45.81	-12.77	38.27	17.62
424	8.48	2.20	40.54	-13.45	35.99	17.56
425	8.50	2.26	36.26	-13.83	34.02	17.48
426	8.52	2.34	36.73	-19.03	33.01	17.48
427	8.54	2.41	39.45	-21.08	33.00	17.57
428	8.56	2.47	44.52	-20.89	33.17	17.67
429	8.58	2.51	45.99	-21.02	32.99	17.71
430	8.60	2.56	43.85	-21.33	32.24	17.68
431	8.62	2.58	40.39	-21.57	31.17	17.61
432	8.64	2.60	37.31	-21.82	29.94	17.49

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
433	8.66	2.58	31.39	-22.38	29.01	17.34
434	8.68	2.49	27.97	-23.62	28.68	17.20
435	8.70	2.39	27.23	-24.98	29.24	17.13
436	8.72	2.31	27.14	-26.04	30.28	17.10
437	8.74	2.20	26.70	-27.15	31.65	17.07
438	8.76	2.06	26.44	-28.64	33.65	17.09
439	8.78	1.97	30.13	-29.82	35.07	17.15
440	8.81	2.05	31.72	-25.11	37.14	17.35
441	8.82	2.06	43.20	-27.34	38.99	17.57
442	8.84	2.08	52.26	-28.27	41.24	17.79
443	8.86	2.10	57.38	-28.83	42.62	17.92
444	8.88	2.10	60.64	-29.88	43.35	17.99
445	8.90	2.11	63.01	-30.50	43.39	18.05
446	8.92	2.22	65.44	-30.38	42.95	18.09
447	8.94	2.26	66.47	-30.38	42.02	18.13
448	8.96	2.34	66.79	-30.13	40.60	18.12
449	8.98	2.45	61.95	-29.45	38.95	18.08
450	9.01	2.49	58.35	-29.32	37.23	18.00
451	9.02	2.50	52.64	-29.82	36.43	17.93
452	9.04	2.46	51.84	-30.69	36.54	17.87
453	9.06	2.34	50.88	-31.87	37.40	17.81
454	9.08	2.22	47.33	-33.11	38.71	17.76
455	9.10	2.11	47.24	-34.28	40.04	17.74
456	9.12	2.09	51.08	-34.84	41.43	17.79
457	9.14	2.09	54.48	-35.09	42.61	17.86
458	9.16	2.07	57.35	-35.28	43.55	17.91
459	9.18	2.04	57.96	-35.15	43.86	17.89
460	9.20	2.03	52.83	-35.28	43.52	17.85
461	9.22	2.05	51.81	-35.34	42.79	17.80
462	9.24	2.05	50.25	-35.40	42.29	17.78
463	9.26	2.07	49.78	-35.46	41.72	17.74
464	9.28	2.08	47.17	-35.59	40.97	17.71
465	9.30	2.11	45.83	-35.52	40.12	17.69
466	9.32	2.17	46.56	-35.21	39.19	17.70
467	9.34	2.26	47.29	-34.72	38.52	17.72
468	9.36	2.27	47.00	-34.90	37.80	17.71
469	9.38	2.28	44.36	-35.28	37.56	17.67
470	9.40	2.22	42.42	-35.96	37.68	17.62
471	9.42	2.17	42.77	-36.39	38.34	17.59
472	9.44	2.10	41.19	-37.07	39.01	17.55
473	9.46	2.05	39.79	-37.69	39.76	17.52
474	9.48	2.00	40.84	-37.94	40.54	17.55
475	9.50	2.03	44.38	-38.00	41.57	17.64
476	9.52	2.07	50.63	-37.82	41.91	17.73
477	9.54	2.12	50.45	-37.69	42.09	17.78
478	9.56	2.09	49.95	-38.00	42.09	17.75
479	9.58	2.03	47.75	-38.81	42.53	17.68
480	9.60	1.93	43.09	-39.99	43.01	17.56

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
481	9.62	1.82	37.88	-41.10	43.65	17.41
482	9.64	1.70	34.01	-41.97	44.70	17.31
483	9.66	1.64	35.15	-42.72	46.36	17.31
484	9.68	1.64	39.96	-42.90	48.54	17.43
485	9.70	1.63	46.43	-43.03	50.19	17.55
486	9.72	1.64	48.10	-43.03	50.74	17.63
487	9.74	1.70	48.75	-42.72	49.74	17.65
488	9.76	1.78	48.31	-42.16	46.86	17.57
489	9.78	1.84	35.99	-4.46	44.14	17.47
490	9.80	1.88	36.43	-22.63	41.89	17.33
491	9.82	1.87	34.11	-41.60	41.26	17.29
492	9.84	1.87	31.89	-42.34	40.68	17.21
493	9.86	1.86	30.28	-42.78	40.25	17.17
494	9.88	1.87	30.60	-43.34	40.05	17.17
495	9.90	1.89	31.24	-43.58	40.04	17.20
496	9.92	1.92	32.86	-43.65	39.57	17.25
497	9.94	2.02	33.79	-43.21	38.64	17.30
498	9.96	2.11	34.03	-42.59	36.91	17.32
499	9.98	2.25	32.94	-41.91	34.99	17.33
500	10.00	2.39	32.91	-40.92	33.10	17.32
501	10.02	2.47	31.27	-40.42	31.38	17.29
502	10.04	2.57	29.22	-40.05	29.86	17.22
503	10.06	2.60	26.65	-39.74	28.65	17.14
504	10.08	2.60	24.83	-39.93	28.17	17.03
505	10.11	2.47	22.37	-40.79	28.31	16.95
506	10.12	2.41	22.19	-41.17	28.61	16.91
507	10.14	2.44	22.66	-41.04	29.16	16.96
508	10.16	2.44	25.44	-41.04	29.90	17.08
509	10.18	2.50	30.10	-40.73	30.46	17.20
510	10.20	2.56	30.87	-40.55	30.50	17.28
511	10.22	2.59	30.54	-40.42	30.39	17.30
512	10.24	2.58	31.89	-40.55	30.93	17.34
513	10.26	2.51	33.94	-41.17	32.18	17.37
514	10.28	2.38	34.21	-42.16	33.68	17.34
515	10.30	2.21	30.84	-43.27	34.91	17.27
516	10.32	2.14	29.61	-43.83	36.71	17.27
517	10.34	2.06	35.67	-44.45	40.07	17.47
518	10.36	2.02	50.38	-44.82	43.19	17.71
519	10.38	2.11	56.91	-44.08	44.59	17.90
520	10.40	2.22	59.96	-43.46	43.78	18.00
521	10.42	2.34	62.13	-42.72	42.25	18.03
522	10.44	2.44	59.81	-42.16	40.92	18.04
523	10.46	2.46	58.29	-42.10	39.48	17.97
524	10.48	2.47	51.67	-42.10	38.09	17.87
525	10.50	2.48	45.16	-41.97	35.86	17.70
526	10.52	2.53	36.19	-41.72	33.66	17.52
527	10.54	2.54	31.89	-41.72	32.08	17.36
528	10.56	2.49	30.48	-42.03	31.81	17.26

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
529	10.58	2.39	28.87	-42.72	32.20	17.17
530	10.60	2.28	25.94	-43.52	32.36	17.05
531	10.62	2.23	22.63	-43.83	31.89	16.91
532	10.64	2.25	20.78	-43.71	31.46	16.88
533	10.66	2.32	24.18	-43.34	31.71	17.06
534	10.68	2.50	32.59	-42.41	32.12	17.29
535	10.70	2.63	36.72	-41.48	31.90	17.50
536	10.72	2.82	40.17	-40.42	31.57	17.60
537	10.74	2.81	40.76	-40.42	31.44	17.60
538	10.76	2.67	36.66	-41.29	31.05	17.41
539	10.78	2.48	23.52	-38.00	29.84	17.11
540	10.80	2.48	19.21	-39.93	28.37	16.84
541	10.82	2.49	20.38	-40.92	28.64	16.81
542	10.84	2.36	22.11	-42.78	31.30	16.93
543	10.86	2.11	27.21	-45.32	35.89	17.07
544	10.88	1.87	32.04	-47.24	41.89	17.18
545	10.91	1.63	34.09	-49.10	47.48	17.16
546	10.92	1.42	30.02	-51.21	51.79	17.11
547	10.94	1.38	31.08	-49.78	53.33	17.06
548	10.96	1.44	31.60	-39.00	50.66	17.16
549	10.98	1.78	35.47	-32.55	46.82	17.32
550	11.00	1.99	40.57	-37.32	43.83	17.49
551	11.02	2.10	44.41	-38.00	41.68	17.56
552	11.04	2.21	39.72	-37.76	39.31	17.53
553	11.06	2.32	35.53	-37.88	36.62	17.46
554	11.08	2.43	35.06	-37.69	34.40	17.43
555	11.10	2.60	35.15	-37.01	31.62	17.40
556	11.12	2.88	30.34	-35.46	29.53	17.39
557	11.14	2.94	32.30	-35.59	28.13	17.34
558	11.16	2.87	30.22	-36.52	28.54	17.33
559	11.18	2.75	30.08	-37.76	28.86	17.24
560	11.21	2.65	26.30	-38.44	28.96	17.13
561	11.22	2.60	22.90	-39.37	28.77	17.05
562	11.24	2.62	24.95	-39.49	28.73	17.07
563	11.26	2.73	27.91	-38.93	28.86	17.16
564	11.28	2.76	28.29	-38.75	28.30	17.15
565	11.30	2.74	23.45	-39.12	27.87	17.06
566	11.32	2.66	22.34	-39.68	27.56	16.92
567	11.34	2.56	20.52	-40.42	28.61	16.85
568	11.36	2.34	20.58	-42.34	31.62	16.84
569	11.38	1.96	23.54	-46.25	37.54	16.88
570	11.40	1.58	26.35	-49.78	46.02	16.94
571	11.42	1.34	29.43	-50.96	52.22	16.97
572	11.44	1.39	28.90	-17.67	52.98	17.02
573	11.46	1.56	30.13	6.76	47.28	17.07
574	11.48	1.94	29.40	29.82	41.06	17.21
575	11.50	2.36	34.47	41.29	36.18	17.37
576	11.52	2.65	38.34	40.61	32.53	17.47

:: Field input data :: (continued)

Point ID	Depth (m)	q_c (MPa)	f_s (kPa)	u (kPa)	Fines content (%)	Unit weight (kN/m^3)
577	11.54	2.92	34.26	44.76	29.42	17.46
578	11.56	3.11	30.07	46.00	26.49	17.37
579	11.58	3.28	28.26	37.26	24.52	17.26
580	11.60	3.29	24.71	27.59	23.25	17.11
581	11.62	3.19	19.91	16.99	22.70	16.93
582	11.64	3.05	18.27	9.98	22.14	16.68
583	11.66	2.93	13.08	8.62	21.86	16.51
584	11.68	2.90	9.56	9.55	5.00	16.13

Abbreviations

Depth:	Depth from free surface, at which CPT was performed (m)
q_c:	Measured cone resistance (MPa)
f_s:	Sleeve friction resistance (kPa)
u:	Pore pressure (kPa)
Fines content:	Percentage of fines in soil (%)
Unit weight:	Bulk soil unit weight (kN/m^3)

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data ::

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
1	0.02	0.32	0.00	0.32	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
2	0.04	0.65	0.00	0.65	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
3	0.06	0.98	0.00	0.98	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
4	0.08	1.32	0.00	1.32	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
5	0.10	1.67	0.00	1.67	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
6	0.12	2.03	0.00	2.03	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
7	0.14	2.39	0.00	2.39	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
8	0.16	2.76	0.00	2.76	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
9	0.18	3.12	0.00	3.12	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
10	0.20	3.49	0.00	3.49	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
11	0.22	3.86	0.00	3.86	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
12	0.24	4.24	0.00	4.24	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
13	0.26	4.61	0.00	4.61	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
14	0.28	4.98	0.00	4.98	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
15	0.30	5.36	0.00	5.36	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
16	0.32	5.73	0.00	5.73	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
17	0.34	6.10	0.00	6.10	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
18	0.36	6.47	0.00	6.47	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
19	0.38	6.85	0.00	6.85	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
20	0.40	7.22	0.00	7.22	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
21	0.42	7.59	0.00	7.59	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
22	0.45	8.14	0.00	8.14	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
23	0.46	8.32	0.00	8.32	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
24	0.48	8.69	0.00	8.69	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
25	0.50	9.06	0.00	9.06	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
26	0.52	9.43	0.00	9.43	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
27	0.54	9.79	0.00	9.79	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
28	0.56	10.16	0.00	10.16	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
29	0.58	10.52	0.00	10.52	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
30	0.60	10.89	0.00	10.89	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
31	0.62	11.25	0.00	11.25	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
32	0.64	11.61	0.00	11.61	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
33	0.66	11.98	0.00	11.98	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
34	0.68	12.34	0.00	12.34	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
35	0.70	12.71	0.00	12.71	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
36	0.72	13.07	0.00	13.07	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
37	0.74	13.44	0.00	13.44	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
38	0.76	13.81	0.00	13.81	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
39	0.78	14.17	0.00	14.17	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
40	0.80	14.54	0.00	14.54	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
41	0.82	14.90	0.00	14.90	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
42	0.84	15.27	0.00	15.27	1.00	0.143	1.43	0.100	1.10	1.00	2.000	No
43	0.86	15.64	0.00	15.64	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
44	0.88	16.01	0.00	16.01	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
45	0.90	16.38	0.00	16.38	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
46	0.92	16.75	0.00	16.75	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
47	0.94	17.13	0.00	17.13	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No
48	0.96	17.50	0.00	17.50	1.00	0.142	1.43	0.100	1.10	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
49	0.98	17.88	0.00	17.88	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
50	1.00	18.26	0.00	18.26	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
51	1.02	18.63	0.00	18.63	0.99	0.142	1.43	0.100	1.10	1.00	2.000	No
52	1.05	19.20	0.00	19.20	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
53	1.06	19.39	0.00	19.39	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
54	1.08	19.77	0.00	19.77	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
55	1.11	20.35	0.00	20.35	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
56	1.12	20.54	0.00	20.54	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
57	1.14	20.93	0.00	20.93	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
58	1.17	21.51	0.00	21.51	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
59	1.18	21.70	0.00	21.70	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
60	1.20	22.09	0.00	22.09	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
61	1.22	22.48	0.00	22.48	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
62	1.24	22.87	0.00	22.87	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
63	1.26	23.27	0.00	23.27	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
64	1.28	23.66	0.00	23.66	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
65	1.30	24.05	0.00	24.05	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
66	1.32	24.45	0.00	24.45	0.99	0.142	1.43	0.099	1.10	1.00	2.000	No
67	1.34	24.84	0.00	24.84	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
68	1.36	25.23	0.00	25.23	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
69	1.38	25.62	0.00	25.62	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
70	1.40	26.01	0.00	26.01	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
71	1.42	26.39	0.00	26.39	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
72	1.44	26.78	0.00	26.78	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
73	1.46	27.16	0.00	27.16	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
74	1.48	27.55	0.00	27.55	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
75	1.50	27.93	0.00	27.93	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
76	1.52	28.31	0.00	28.31	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
77	1.54	28.69	0.00	28.69	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
78	1.56	29.06	0.00	29.06	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
79	1.58	29.44	0.00	29.44	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
80	1.60	29.82	0.00	29.82	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
81	1.62	30.19	0.00	30.19	0.99	0.141	1.43	0.099	1.10	1.00	2.000	No
82	1.64	30.56	0.00	30.56	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
83	1.66	30.93	0.00	30.93	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
84	1.68	31.31	0.00	31.31	0.98	0.141	1.43	0.099	1.10	1.00	2.000	No
85	1.70	31.68	0.00	31.68	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
86	1.72	32.04	0.00	32.04	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
87	1.74	32.41	0.00	32.41	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
88	1.76	32.78	0.00	32.78	0.98	0.141	1.43	0.098	1.10	1.00	2.000	No
89	1.78	33.15	0.00	33.15	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
90	1.80	33.52	0.00	33.52	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
91	1.82	33.88	0.00	33.88	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
92	1.84	34.25	0.00	34.25	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
93	1.86	34.61	0.00	34.61	0.98	0.140	1.43	0.098	1.10	1.00	2.000	No
94	1.88	34.97	0.00	34.97	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
95	1.90	35.33	0.00	35.33	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
96	1.92	35.69	0.00	35.69	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
97	1.94	36.05	0.00	36.05	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
98	1.96	36.41	0.00	36.41	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
99	1.98	36.76	0.00	36.76	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
100	2.00	37.12	0.00	37.12	0.98	0.140	1.43	0.098	1.09	1.00	2.000	No
101	2.02	37.48	0.20	37.28	0.98	0.141	1.43	0.098	1.09	1.00	0.119	No
102	2.04	37.83	0.39	37.44	0.98	0.141	1.43	0.099	1.09	1.00	0.120	No
103	2.06	38.19	0.59	37.60	0.98	0.142	1.43	0.099	1.09	1.00	0.120	No
104	2.08	38.54	0.78	37.76	0.98	0.143	1.43	0.100	1.09	1.00	0.121	No
105	2.10	38.90	0.98	37.92	0.98	0.143	1.43	0.100	1.08	1.00	0.122	No
106	2.12	39.26	1.18	38.08	0.98	0.144	1.43	0.101	1.08	1.00	0.123	No
107	2.15	39.79	1.47	38.32	0.98	0.145	1.43	0.101	1.08	1.00	0.124	No
108	2.16	39.97	1.57	38.40	0.98	0.145	1.43	0.102	1.08	1.00	0.124	No
109	2.18	40.32	1.77	38.56	0.98	0.146	1.43	0.102	1.08	1.00	0.125	No
110	2.20	40.68	1.96	38.71	0.98	0.147	1.43	0.103	1.08	1.00	0.125	No
111	2.22	41.03	2.16	38.87	0.98	0.147	1.43	0.103	1.08	1.00	0.126	No
112	2.24	41.38	2.35	39.03	0.97	0.148	1.43	0.103	1.08	1.00	0.126	No
113	2.26	41.74	2.55	39.19	0.97	0.148	1.43	0.104	1.08	1.00	0.127	No
114	2.28	42.09	2.75	39.34	0.97	0.149	1.43	0.104	1.08	1.00	0.127	No
115	2.30	42.44	2.94	39.50	0.97	0.150	1.43	0.105	1.08	1.00	0.128	No
116	2.32	42.80	3.14	39.66	0.97	0.150	1.43	0.105	1.08	1.00	0.128	No
117	2.34	43.15	3.34	39.81	0.97	0.151	1.43	0.106	1.08	1.00	0.129	No
118	2.36	43.50	3.53	39.97	0.97	0.151	1.43	0.106	1.08	1.00	0.129	No
119	2.38	43.86	3.73	40.13	0.97	0.152	1.43	0.106	1.08	1.00	0.130	No
120	2.40	44.21	3.92	40.29	0.97	0.153	1.43	0.107	1.08	1.00	0.130	No
121	2.42	44.57	4.12	40.45	0.97	0.153	1.43	0.107	1.08	1.00	0.131	No
122	2.44	44.92	4.32	40.61	0.97	0.154	1.43	0.108	1.08	1.00	0.132	No
123	2.46	45.28	4.51	40.76	0.97	0.154	1.43	0.108	1.08	1.00	0.132	No
124	2.48	45.63	4.71	40.92	0.97	0.155	1.43	0.108	1.08	1.00	0.133	No
125	2.50	45.98	4.91	41.07	0.97	0.155	1.43	0.109	1.07	1.00	0.134	No
126	2.52	46.33	5.10	41.23	0.97	0.156	1.43	0.109	1.07	1.00	0.135	No
127	2.54	46.68	5.30	41.38	0.97	0.156	1.43	0.109	1.07	1.00	0.136	No
128	2.56	47.02	5.49	41.53	0.97	0.157	1.43	0.110	1.07	1.00	0.136	No
129	2.58	47.37	5.69	41.68	0.97	0.157	1.43	0.110	1.07	1.00	0.137	No
130	2.60	47.72	5.89	41.83	0.97	0.158	1.43	0.111	1.07	1.00	0.137	No
131	2.62	48.06	6.08	41.98	0.97	0.159	1.43	0.111	1.07	1.00	0.138	No
132	2.64	48.40	6.28	42.12	0.97	0.159	1.43	0.111	1.07	1.00	0.138	No
133	2.66	48.74	6.47	42.27	0.97	0.160	1.43	0.112	1.07	1.00	0.138	No
134	2.68	49.08	6.67	42.41	0.97	0.160	1.43	0.112	1.07	1.00	0.138	No
135	2.70	49.41	6.87	42.54	0.97	0.161	1.43	0.112	1.07	1.00	0.138	No
136	2.72	49.75	7.06	42.68	0.97	0.161	1.43	0.113	1.07	1.00	0.139	No
137	2.74	50.08	7.26	42.82	0.97	0.162	1.43	0.113	1.07	1.00	0.139	No
138	2.76	50.42	7.46	42.97	0.97	0.162	1.43	0.113	1.07	1.00	0.140	No
139	2.78	50.76	7.65	43.11	0.97	0.163	1.43	0.114	1.07	1.00	0.140	No
140	2.80	51.11	7.85	43.26	0.97	0.163	1.43	0.114	1.07	1.00	0.140	No
141	2.82	51.46	8.04	43.41	0.96	0.164	1.43	0.114	1.07	1.00	0.140	No
142	2.84	51.81	8.24	43.57	0.96	0.164	1.43	0.115	1.07	1.00	0.141	No
143	2.86	52.16	8.44	43.72	0.96	0.164	1.43	0.115	1.07	1.00	0.141	No
144	2.88	52.52	8.63	43.88	0.96	0.165	1.43	0.115	1.07	1.00	0.141	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
145	2.90	52.87	8.83	44.04	0.96	0.165	1.43	0.116	1.07	1.00	0.141	No
146	2.92	53.23	9.03	44.20	0.96	0.166	1.43	0.116	1.07	1.00	0.142	No
147	2.94	53.59	9.22	44.37	0.96	0.166	1.43	0.116	1.07	1.00	0.142	No
148	2.96	53.95	9.42	44.53	0.96	0.167	1.43	0.117	1.07	1.00	0.142	No
149	2.98	54.31	9.61	44.69	0.96	0.167	1.43	0.117	1.07	1.00	0.143	No
150	3.00	54.67	9.81	44.86	0.96	0.168	1.43	0.117	1.07	1.00	0.144	No
151	3.02	55.03	10.01	45.02	0.96	0.168	1.43	0.118	1.07	1.00	0.144	No
152	3.04	55.39	10.20	45.19	0.96	0.168	1.43	0.118	1.07	1.00	0.145	No
153	3.06	55.75	10.40	45.35	0.96	0.169	1.43	0.118	1.07	1.00	0.146	No
154	3.09	56.30	10.69	45.60	0.96	0.169	1.43	0.119	1.07	1.00	0.147	No
155	3.10	56.48	10.79	45.69	0.96	0.170	1.43	0.119	1.07	1.00	0.147	No
156	3.12	56.84	10.99	45.85	0.96	0.170	1.43	0.119	1.07	1.00	0.147	No
157	3.15	57.38	11.28	46.10	0.96	0.171	1.43	0.119	1.07	1.00	0.147	No
158	3.16	57.56	11.38	46.18	0.96	0.171	1.43	0.120	1.07	1.00	0.147	No
159	3.18	57.91	11.58	46.34	0.96	0.171	1.43	0.120	1.07	1.00	0.147	No
160	3.20	58.27	11.77	46.50	0.96	0.172	1.43	0.120	1.07	1.00	0.148	No
161	3.22	58.62	11.97	46.65	0.96	0.172	1.43	0.120	1.07	1.00	0.148	No
162	3.24	58.97	12.16	46.81	0.96	0.172	1.43	0.121	1.07	1.00	0.149	No
163	3.26	59.32	12.36	46.96	0.96	0.173	1.43	0.121	1.07	1.00	0.149	No
164	3.28	59.67	12.56	47.11	0.96	0.173	1.43	0.121	1.07	1.00	0.149	No
165	3.30	60.02	12.75	47.27	0.96	0.174	1.43	0.122	1.07	1.00	0.150	No
166	3.32	60.37	12.95	47.42	0.96	0.174	1.43	0.122	1.07	1.00	0.150	No
167	3.34	60.72	13.15	47.57	0.96	0.174	1.43	0.122	1.07	1.00	0.150	No
168	3.36	61.06	13.34	47.72	0.95	0.175	1.43	0.122	1.07	1.00	0.151	No
169	3.38	61.41	13.54	47.87	0.95	0.175	1.43	0.123	1.06	1.00	0.152	No
170	3.40	61.76	13.73	48.02	0.95	0.175	1.43	0.123	1.06	1.00	0.152	No
171	3.42	62.10	13.93	48.17	0.95	0.176	1.43	0.123	1.06	1.00	0.152	No
172	3.44	62.45	14.13	48.32	0.95	0.176	1.43	0.123	1.06	1.00	0.153	No
173	3.46	62.79	14.32	48.47	0.95	0.177	1.43	0.124	1.06	1.00	0.154	No
174	3.48	63.14	14.52	48.62	0.95	0.177	1.43	0.124	1.06	1.00	0.154	No
175	3.50	63.48	14.72	48.76	0.95	0.177	1.43	0.124	1.06	1.00	0.155	No
176	3.52	63.82	14.91	48.91	0.95	0.178	1.43	0.124	1.06	1.00	0.156	No
177	3.54	64.16	15.11	49.05	0.95	0.178	1.43	0.125	1.06	1.00	0.156	No
178	3.56	64.50	15.30	49.19	0.95	0.178	1.43	0.125	1.06	1.00	0.157	No
179	3.58	64.83	15.50	49.33	0.95	0.179	1.43	0.125	1.06	1.00	0.157	No
180	3.60	65.16	15.70	49.47	0.95	0.179	1.43	0.125	1.06	1.00	0.158	No
181	3.62	65.49	15.89	49.60	0.95	0.179	1.43	0.126	1.06	1.00	0.158	No
182	3.64	65.82	16.09	49.73	0.95	0.180	1.43	0.126	1.06	1.00	0.158	No
183	3.66	66.14	16.28	49.86	0.95	0.180	1.43	0.126	1.06	1.00	0.159	No
184	3.68	66.46	16.48	49.98	0.95	0.180	1.43	0.126	1.06	1.00	0.159	No
185	3.70	66.78	16.68	50.11	0.95	0.181	1.43	0.127	1.06	1.00	0.159	No
186	3.72	67.10	16.87	50.23	0.95	0.181	1.43	0.127	1.06	1.00	0.159	No
187	3.74	67.43	17.07	50.36	0.95	0.181	1.43	0.127	1.06	1.00	0.159	No
188	3.76	67.75	17.27	50.49	0.95	0.182	1.43	0.127	1.06	1.00	0.160	No
189	3.78	68.08	17.46	50.61	0.95	0.182	1.43	0.127	1.06	1.00	0.160	No
190	3.80	68.40	17.66	50.75	0.95	0.182	1.43	0.128	1.06	1.00	0.160	No
191	3.82	68.73	17.85	50.88	0.95	0.183	1.43	0.128	1.06	1.00	0.161	No
192	3.84	69.06	18.05	51.01	0.95	0.183	1.43	0.128	1.06	1.00	0.161	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
193	3.86	69.39	18.25	51.15	0.95	0.183	1.43	0.128	1.06	1.00	0.161	No
194	3.88	69.73	18.44	51.29	0.94	0.184	1.43	0.129	1.06	1.00	0.160	No
195	3.90	70.07	18.64	51.43	0.94	0.184	1.43	0.129	1.06	1.00	0.160	No
196	3.92	70.41	18.84	51.58	0.94	0.184	1.43	0.129	1.06	1.00	0.161	No
197	3.94	70.75	19.03	51.72	0.94	0.185	1.43	0.129	1.06	1.00	0.161	No
198	3.96	71.10	19.23	51.87	0.94	0.185	1.43	0.129	1.06	1.00	0.161	No
199	3.98	71.44	19.42	52.02	0.94	0.185	1.43	0.130	1.06	1.00	0.161	No
200	4.00	71.79	19.62	52.17	0.94	0.185	1.43	0.130	1.06	1.00	0.161	No
201	4.02	72.14	19.82	52.33	0.94	0.186	1.43	0.130	1.06	1.00	0.162	No
202	4.05	72.67	20.11	52.56	0.94	0.186	1.43	0.130	1.06	1.00	0.163	No
203	4.06	72.84	20.21	52.64	0.94	0.186	1.43	0.130	1.06	1.00	0.163	No
204	4.08	73.19	20.40	52.79	0.94	0.187	1.43	0.131	1.05	1.00	0.164	No
205	4.10	73.55	20.60	52.94	0.94	0.187	1.43	0.131	1.05	1.00	0.165	No
206	4.12	73.89	20.80	53.10	0.94	0.187	1.43	0.131	1.05	1.00	0.165	No
207	4.14	74.24	20.99	53.25	0.94	0.187	1.43	0.131	1.05	1.00	0.166	No
208	4.16	74.59	21.19	53.40	0.94	0.188	1.43	0.131	1.05	1.00	0.166	No
209	4.18	74.93	21.39	53.55	0.94	0.188	1.43	0.132	1.05	1.00	0.165	No
210	4.20	75.28	21.58	53.70	0.94	0.188	1.43	0.132	1.05	1.00	0.165	No
211	4.22	75.62	21.78	53.85	0.94	0.188	1.43	0.132	1.06	1.00	0.164	No
212	4.24	75.97	21.97	54.00	0.94	0.189	1.43	0.132	1.06	1.00	0.163	No
213	4.26	76.32	22.17	54.15	0.94	0.189	1.43	0.132	1.06	1.00	0.162	No
214	4.28	76.67	22.37	54.30	0.94	0.189	1.43	0.132	1.06	1.00	0.162	No
215	4.30	77.02	22.56	54.46	0.94	0.189	1.43	0.133	1.06	1.00	0.162	No
216	4.32	77.37	22.76	54.62	0.94	0.190	1.43	0.133	1.06	1.00	0.162	No
217	4.34	77.73	22.96	54.77	0.94	0.190	1.43	0.133	1.06	1.00	0.163	No
218	4.36	78.08	23.15	54.93	0.94	0.190	1.43	0.133	1.06	1.00	0.162	No
219	4.38	78.44	23.35	55.09	0.93	0.190	1.43	0.133	1.06	1.00	0.162	No
220	4.40	78.80	23.54	55.25	0.93	0.191	1.43	0.133	1.06	1.00	0.163	No
221	4.42	79.16	23.74	55.42	0.93	0.191	1.43	0.134	1.06	1.00	0.165	No
222	4.44	79.52	23.94	55.58	0.93	0.191	1.43	0.134	1.05	1.00	0.165	No
223	4.46	79.88	24.13	55.74	0.93	0.191	1.43	0.134	1.05	1.00	0.165	No
224	4.49	80.42	24.43	55.99	0.93	0.192	1.43	0.134	1.05	1.00	0.165	No
225	4.50	80.60	24.53	56.07	0.93	0.192	1.43	0.134	1.05	1.00	0.166	No
226	4.52	80.96	24.72	56.24	0.93	0.192	1.43	0.134	1.05	1.00	0.167	No
227	4.54	81.32	24.92	56.40	0.93	0.192	1.43	0.134	1.05	1.00	0.168	No
228	4.56	81.67	25.11	56.56	0.93	0.192	1.43	0.135	1.05	1.00	0.168	No
229	4.58	82.03	25.31	56.72	0.93	0.193	1.43	0.135	1.05	1.00	0.169	No
230	4.60	82.38	25.51	56.88	0.93	0.193	1.43	0.135	1.05	1.00	0.169	No
231	4.62	82.73	25.70	57.03	0.93	0.193	1.43	0.135	1.05	1.00	0.170	No
232	4.64	83.09	25.90	57.19	0.93	0.193	1.43	0.135	1.05	1.00	0.170	No
233	4.66	83.44	26.09	57.34	0.93	0.193	1.43	0.135	1.05	1.00	0.170	No
234	4.68	83.79	26.29	57.49	0.93	0.194	1.43	0.135	1.05	1.00	0.170	No
235	4.70	84.14	26.49	57.65	0.93	0.194	1.43	0.136	1.05	1.00	0.169	No
236	4.72	84.49	26.68	57.80	0.93	0.194	1.43	0.136	1.05	1.00	0.169	No
237	4.74	84.84	26.88	57.96	0.93	0.194	1.43	0.136	1.05	1.00	0.170	No
238	4.76	85.19	27.08	58.11	0.93	0.194	1.43	0.136	1.05	1.00	0.171	No
239	4.78	85.54	27.27	58.27	0.93	0.195	1.43	0.136	1.05	1.00	0.171	No
240	4.80	85.89	27.47	58.43	0.93	0.195	1.43	0.136	1.05	1.00	0.172	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
241	4.82	86.25	27.66	58.58	0.93	0.195	1.43	0.136	1.05	1.00	0.173	No
242	4.84	86.60	27.86	58.74	0.93	0.195	1.43	0.137	1.05	1.00	0.173	No
243	4.86	86.95	28.06	58.90	0.93	0.195	1.43	0.137	1.05	1.00	0.171	No
244	4.88	87.31	28.25	59.06	0.92	0.195	1.43	0.137	1.05	1.00	0.171	No
245	4.90	87.67	28.45	59.22	0.92	0.196	1.43	0.137	1.05	1.00	0.170	No
246	4.92	88.03	28.65	59.39	0.92	0.196	1.43	0.137	1.05	1.00	0.169	No
247	4.94	88.39	28.84	59.55	0.92	0.196	1.43	0.137	1.05	1.00	0.169	No
248	4.96	88.75	29.04	59.71	0.92	0.196	1.43	0.137	1.05	1.00	0.170	No
249	4.98	89.11	29.23	59.87	0.92	0.196	1.43	0.137	1.05	1.00	0.171	No
250	5.00	89.46	29.43	60.03	0.92	0.197	1.43	0.138	1.05	1.00	0.171	No
251	5.02	89.82	29.63	60.19	0.92	0.197	1.43	0.138	1.05	1.00	0.171	No
252	5.04	90.18	29.82	60.35	0.92	0.197	1.43	0.138	1.05	1.00	0.172	No
253	5.06	90.53	30.02	60.52	0.92	0.197	1.43	0.138	1.05	1.00	0.172	No
254	5.08	90.90	30.21	60.68	0.92	0.197	1.43	0.138	1.05	1.00	0.173	No
255	5.10	91.26	30.41	60.85	0.92	0.197	1.43	0.138	1.05	1.00	0.173	No
256	5.12	91.62	30.61	61.01	0.92	0.197	1.43	0.138	1.05	1.00	0.172	No
257	5.14	91.98	30.80	61.18	0.92	0.198	1.43	0.138	1.05	1.00	0.171	No
258	5.16	92.35	31.00	61.35	0.92	0.198	1.43	0.138	1.05	1.00	0.172	No
259	5.18	92.71	31.20	61.51	0.92	0.198	1.43	0.139	1.04	1.00	0.174	No
260	5.20	93.07	31.39	61.68	0.92	0.198	1.43	0.139	1.04	1.00	0.174	No
261	5.22	93.43	31.59	61.84	0.92	0.198	1.43	0.139	1.04	1.00	0.175	No
262	5.24	93.79	31.78	62.00	0.92	0.198	1.43	0.139	1.04	1.00	0.174	No
263	5.26	94.14	31.98	62.16	0.92	0.199	1.43	0.139	1.04	1.00	0.174	No
264	5.28	94.50	32.18	62.32	0.92	0.199	1.43	0.139	1.04	1.00	0.175	No
265	5.30	94.86	32.37	62.48	0.92	0.199	1.43	0.139	1.04	1.00	0.176	No
266	5.32	95.21	32.57	62.64	0.92	0.199	1.43	0.139	1.04	1.00	0.177	No
267	5.34	95.57	32.77	62.80	0.92	0.199	1.43	0.139	1.04	1.00	0.177	No
268	5.36	95.92	32.96	62.96	0.91	0.199	1.43	0.139	1.04	1.00	0.178	No
269	5.38	96.27	33.16	63.11	0.91	0.199	1.43	0.140	1.04	1.00	0.178	No
270	5.40	96.62	33.35	63.27	0.91	0.200	1.43	0.140	1.04	1.00	0.178	No
271	5.42	96.97	33.55	63.42	0.91	0.200	1.43	0.140	1.04	1.00	0.178	No
272	5.44	97.31	33.75	63.57	0.91	0.200	1.43	0.140	1.04	1.00	0.178	No
273	5.46	97.66	33.94	63.72	0.91	0.200	1.43	0.140	1.04	1.00	0.178	No
274	5.48	98.00	34.14	63.87	0.91	0.200	1.43	0.140	1.04	1.00	0.178	No
275	5.50	98.35	34.34	64.01	0.91	0.200	1.43	0.140	1.04	1.00	0.178	No
276	5.52	98.70	34.53	64.17	0.91	0.200	1.43	0.140	1.04	1.00	0.178	No
277	5.54	99.05	34.73	64.32	0.91	0.201	1.43	0.140	1.04	1.00	0.179	No
278	5.56	99.40	34.92	64.47	0.91	0.201	1.43	0.140	1.04	1.00	0.179	No
279	5.58	99.75	35.12	64.63	0.91	0.201	1.43	0.141	1.04	1.00	0.180	No
280	5.60	100.10	35.32	64.79	0.91	0.201	1.43	0.141	1.04	1.00	0.180	No
281	5.62	100.46	35.51	64.95	0.91	0.201	1.43	0.141	1.04	1.00	0.179	No
282	5.64	100.81	35.71	65.11	0.91	0.201	1.43	0.141	1.04	1.00	0.179	No
283	5.66	101.17	35.90	65.26	0.91	0.201	1.43	0.141	1.04	1.00	0.179	No
284	5.68	101.52	36.10	65.42	0.91	0.201	1.43	0.141	1.04	1.00	0.180	No
285	5.70	101.87	36.30	65.57	0.91	0.202	1.43	0.141	1.04	1.00	0.179	No
286	5.72	102.22	36.49	65.73	0.91	0.202	1.43	0.141	1.04	1.00	0.178	No
287	5.74	102.58	36.69	65.89	0.91	0.202	1.43	0.141	1.04	1.00	0.178	No
288	5.76	102.93	36.89	66.05	0.91	0.202	1.43	0.141	1.04	1.00	0.178	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
289	5.78	103.29	37.08	66.21	0.91	0.202	1.43	0.141	1.04	1.00	0.177	No
290	5.80	103.66	37.28	66.38	0.91	0.202	1.43	0.141	1.04	1.00	0.177	No
291	5.82	104.02	37.47	66.54	0.90	0.202	1.43	0.142	1.04	1.00	0.176	No
292	5.84	104.39	37.67	66.71	0.90	0.202	1.43	0.142	1.04	1.00	0.175	No
293	5.87	104.94	37.96	66.97	0.90	0.202	1.43	0.142	1.04	1.00	0.177	No
294	5.88	105.12	38.06	67.06	0.90	0.203	1.43	0.142	1.04	1.00	0.179	No
295	5.90	105.49	38.26	67.23	0.90	0.203	1.43	0.142	1.04	1.00	0.178	No
296	5.92	105.86	38.46	67.41	0.90	0.203	1.43	0.142	1.04	1.00	0.177	No
297	5.94	106.23	38.65	67.58	0.90	0.203	1.43	0.142	1.04	1.00	0.177	No
298	5.96	106.59	38.85	67.75	0.90	0.203	1.43	0.142	1.04	1.00	0.180	No
299	5.99	107.14	39.14	67.99	0.90	0.203	1.43	0.142	1.03	1.00	0.181	No
300	6.00	107.32	39.24	68.08	0.90	0.203	1.43	0.142	1.03	1.00	0.182	No
301	6.02	107.67	39.44	68.23	0.90	0.203	1.43	0.142	1.03	1.00	0.182	No
302	6.04	108.02	39.63	68.38	0.90	0.203	1.43	0.142	1.03	1.00	0.182	No
303	6.06	108.36	39.83	68.53	0.90	0.203	1.43	0.142	1.03	1.00	0.182	No
304	6.08	108.70	40.02	68.68	0.90	0.203	1.43	0.142	1.03	1.00	0.183	No
305	6.10	109.05	40.22	68.83	0.90	0.204	1.43	0.142	1.03	1.00	0.183	No
306	6.12	109.39	40.42	68.98	0.90	0.204	1.43	0.143	1.03	1.00	2.000	Yes
307	6.14	109.74	40.61	69.12	0.90	0.204	1.43	0.143	1.03	1.00	2.000	Yes
308	6.16	110.08	40.81	69.27	0.90	0.204	1.43	0.143	1.03	1.00	2.000	Yes
309	6.18	110.44	41.01	69.43	0.90	0.204	1.43	0.143	1.03	1.00	2.000	Yes
310	6.20	110.79	41.20	69.59	0.90	0.204	1.43	0.143	1.03	1.00	2.000	Yes
311	6.22	111.14	41.40	69.75	0.90	0.204	1.43	0.143	1.03	1.00	2.000	Yes
312	6.24	111.50	41.59	69.90	0.90	0.204	1.43	0.143	1.03	1.00	2.000	Yes
313	6.26	111.84	41.79	70.05	0.89	0.204	1.43	0.143	1.03	1.00	2.000	Yes
314	6.28	112.19	41.99	70.20	0.89	0.204	1.43	0.143	1.03	1.00	2.000	Yes
315	6.30	112.53	42.18	70.35	0.89	0.205	1.43	0.143	1.03	1.00	2.000	Yes
316	6.32	112.87	42.38	70.49	0.89	0.205	1.43	0.143	1.03	1.00	2.000	Yes
317	6.34	113.21	42.58	70.64	0.89	0.205	1.43	0.143	1.03	1.00	2.000	Yes
318	6.36	113.55	42.77	70.77	0.89	0.205	1.43	0.143	1.03	1.00	2.000	Yes
319	6.38	113.88	42.97	70.91	0.89	0.205	1.43	0.143	1.03	1.00	2.000	Yes
320	6.40	114.22	43.16	71.05	0.89	0.205	1.43	0.144	1.03	1.00	0.181	No
321	6.42	114.55	43.36	71.19	0.89	0.205	1.43	0.144	1.03	1.00	0.181	No
322	6.44	114.89	43.56	71.34	0.89	0.205	1.43	0.144	1.03	1.00	0.181	No
323	6.46	115.24	43.75	71.48	0.89	0.205	1.43	0.144	1.03	1.00	0.181	No
324	6.48	115.58	43.95	71.63	0.89	0.205	1.43	0.144	1.03	1.00	0.181	No
325	6.50	115.92	44.15	71.77	0.89	0.205	1.43	0.144	1.03	1.00	0.181	No
326	6.52	116.26	44.34	71.92	0.89	0.206	1.43	0.144	1.03	1.00	0.181	No
327	6.54	116.60	44.54	72.06	0.89	0.206	1.43	0.144	1.03	1.00	0.181	No
328	6.56	116.94	44.73	72.20	0.89	0.206	1.43	0.144	1.03	1.00	0.181	No
329	6.58	117.28	44.93	72.35	0.89	0.206	1.43	0.144	1.03	1.00	0.182	No
330	6.60	117.63	45.13	72.50	0.89	0.206	1.43	0.144	1.03	1.00	0.182	No
331	6.62	117.97	45.32	72.65	0.89	0.206	1.43	0.144	1.03	1.00	0.182	No
332	6.64	118.32	45.52	72.80	0.89	0.206	1.43	0.144	1.03	1.00	0.182	No
333	6.66	118.66	45.71	72.95	0.89	0.206	1.43	0.144	1.03	1.00	0.182	No
334	6.68	119.01	45.91	73.10	0.89	0.206	1.43	0.144	1.03	1.00	2.000	Yes
335	6.70	119.35	46.11	73.25	0.89	0.206	1.43	0.144	1.03	1.00	2.000	Yes
336	6.72	119.70	46.30	73.39	0.88	0.206	1.43	0.144	1.03	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
337	6.74	120.04	46.50	73.54	0.88	0.206	1.43	0.144	1.03	1.00	2.000	Yes
338	6.76	120.38	46.70	73.68	0.88	0.206	1.43	0.145	1.03	1.00	2.000	Yes
339	6.78	120.72	46.89	73.82	0.88	0.207	1.43	0.145	1.03	1.00	0.187	No
340	6.80	121.05	47.09	73.97	0.88	0.207	1.43	0.145	1.03	1.00	0.187	No
341	6.82	121.39	47.28	74.11	0.88	0.207	1.43	0.145	1.03	1.00	0.187	No
342	6.85	121.90	47.58	74.32	0.88	0.207	1.43	0.145	1.03	1.00	0.188	No
343	6.86	122.06	47.68	74.39	0.88	0.207	1.43	0.145	1.03	1.00	0.188	No
344	6.88	122.40	47.87	74.53	0.88	0.207	1.43	0.145	1.02	1.00	0.188	No
345	6.90	122.74	48.07	74.67	0.88	0.207	1.43	0.145	1.02	1.00	0.188	No
346	6.92	123.07	48.27	74.81	0.88	0.207	1.43	0.145	1.02	1.00	0.189	No
347	6.94	123.40	48.46	74.94	0.88	0.207	1.43	0.145	1.02	1.00	0.189	No
348	6.96	123.74	48.66	75.08	0.88	0.207	1.43	0.145	1.02	1.00	0.188	No
349	6.98	124.07	48.85	75.21	0.88	0.207	1.43	0.145	1.02	1.00	0.188	No
350	7.00	124.40	49.05	75.35	0.88	0.207	1.43	0.145	1.02	1.00	0.188	No
351	7.02	124.73	49.25	75.48	0.88	0.207	1.43	0.145	1.02	1.00	0.188	No
352	7.04	125.06	49.44	75.62	0.88	0.208	1.43	0.145	1.02	1.00	0.189	No
353	7.06	125.39	49.64	75.75	0.88	0.208	1.43	0.145	1.02	1.00	0.189	No
354	7.08	125.73	49.83	75.89	0.88	0.208	1.43	0.145	1.02	1.00	0.189	No
355	7.10	126.06	50.03	76.03	0.88	0.208	1.43	0.145	1.02	1.00	0.189	No
356	7.12	126.40	50.23	76.17	0.88	0.208	1.43	0.145	1.02	1.00	0.189	No
357	7.14	126.74	50.42	76.31	0.88	0.208	1.43	0.145	1.02	1.00	0.189	No
358	7.16	127.07	50.62	76.45	0.87	0.208	1.43	0.146	1.02	1.00	0.189	No
359	7.18	127.41	50.82	76.59	0.87	0.208	1.43	0.146	1.02	1.00	0.189	No
360	7.20	127.75	51.01	76.74	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
361	7.22	128.09	51.21	76.88	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
362	7.24	128.44	51.40	77.03	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
363	7.26	128.78	51.60	77.18	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
364	7.28	129.13	51.80	77.33	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
365	7.30	129.48	51.99	77.48	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
366	7.32	129.82	52.19	77.63	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
367	7.34	130.17	52.39	77.79	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
368	7.36	130.52	52.58	77.94	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
369	7.38	130.86	52.78	78.09	0.87	0.208	1.43	0.146	1.02	1.00	0.191	No
370	7.40	131.21	52.97	78.23	0.87	0.208	1.43	0.146	1.02	1.00	0.191	No
371	7.42	131.55	53.17	78.38	0.87	0.208	1.43	0.146	1.02	1.00	0.190	No
372	7.44	131.90	53.37	78.53	0.87	0.209	1.43	0.146	1.02	1.00	0.190	No
373	7.46	132.24	53.56	78.68	0.87	0.209	1.43	0.146	1.02	1.00	0.190	No
374	7.48	132.59	53.76	78.83	0.87	0.209	1.43	0.146	1.02	1.00	0.190	No
375	7.50	132.93	53.96	78.97	0.87	0.209	1.43	0.146	1.02	1.00	0.190	No
376	7.52	133.27	54.15	79.12	0.87	0.209	1.43	0.146	1.02	1.00	0.191	No
377	7.54	133.62	54.35	79.27	0.87	0.209	1.43	0.146	1.02	1.00	0.191	No
378	7.56	133.96	54.54	79.42	0.87	0.209	1.43	0.146	1.02	1.00	0.191	No
379	7.58	134.30	54.74	79.56	0.87	0.209	1.43	0.146	1.02	1.00	0.191	No
380	7.60	134.65	54.94	79.71	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
381	7.62	134.99	55.13	79.86	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
382	7.64	135.33	55.33	80.00	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
383	7.66	135.67	55.52	80.15	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
384	7.68	136.01	55.72	80.29	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
385	7.70	136.35	55.92	80.43	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
386	7.72	136.69	56.11	80.57	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
387	7.74	137.02	56.31	80.71	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
388	7.76	137.35	56.51	80.85	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
389	7.78	137.68	56.70	80.98	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
390	7.80	138.01	56.90	81.11	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
391	7.82	138.34	57.09	81.25	0.86	0.209	1.43	0.146	1.02	1.00	0.191	No
392	7.84	138.67	57.29	81.38	0.86	0.209	1.43	0.147	1.02	1.00	0.191	No
393	7.86	139.00	57.49	81.52	0.86	0.209	1.43	0.147	1.02	1.00	0.191	No
394	7.88	139.33	57.68	81.65	0.86	0.209	1.43	0.147	1.02	1.00	0.192	No
395	7.90	139.66	57.88	81.78	0.86	0.209	1.43	0.147	1.02	1.00	0.192	No
396	7.92	139.99	58.08	81.92	0.86	0.209	1.43	0.147	1.02	1.00	0.192	No
397	7.94	140.32	58.27	82.05	0.86	0.210	1.43	0.147	1.02	1.00	0.192	No
398	7.96	140.64	58.47	82.18	0.86	0.210	1.43	0.147	1.02	1.00	0.192	No
399	7.99	141.13	58.76	82.37	0.86	0.210	1.43	0.147	1.02	1.00	0.193	No
400	8.00	141.29	58.86	82.43	0.86	0.210	1.43	0.147	1.02	1.00	0.193	No
401	8.02	141.61	59.06	82.55	0.85	0.210	1.43	0.147	1.02	1.00	0.192	No
402	8.04	141.93	59.25	82.68	0.85	0.210	1.43	0.147	1.02	1.00	0.192	No
403	8.06	142.25	59.45	82.80	0.85	0.210	1.43	0.147	1.02	1.00	0.192	No
404	8.08	142.58	59.64	82.93	0.85	0.210	1.43	0.147	1.02	1.00	0.192	No
405	8.10	142.90	59.84	83.06	0.85	0.210	1.43	0.147	1.02	1.00	0.192	No
406	8.12	143.23	60.04	83.19	0.85	0.210	1.43	0.147	1.02	1.00	0.192	No
407	8.14	143.56	60.23	83.32	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
408	8.17	144.06	60.53	83.53	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
409	8.18	144.22	60.63	83.60	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
410	8.20	144.56	60.82	83.74	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
411	8.22	144.91	61.02	83.89	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
412	8.24	145.25	61.21	84.04	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
413	8.26	145.60	61.41	84.19	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
414	8.28	145.94	61.61	84.34	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
415	8.30	146.29	61.80	84.48	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
416	8.32	146.63	62.00	84.63	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
417	8.34	146.97	62.20	84.78	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
418	8.36	147.32	62.39	84.93	0.85	0.210	1.43	0.147	1.02	1.00	0.191	No
419	8.38	147.67	62.59	85.08	0.85	0.210	1.43	0.147	1.02	1.00	0.190	No
420	8.40	148.02	62.78	85.23	0.85	0.210	1.43	0.147	1.02	1.00	0.190	No
421	8.42	148.37	62.98	85.39	0.85	0.210	1.43	0.147	1.02	1.00	0.190	No
422	8.44	148.72	63.18	85.55	0.84	0.210	1.43	0.147	1.02	1.00	0.189	No
423	8.46	149.08	63.37	85.70	0.84	0.210	1.43	0.147	1.02	1.00	0.189	No
424	8.48	149.43	63.57	85.86	0.84	0.210	1.43	0.147	1.02	1.00	0.189	No
425	8.50	149.78	63.77	86.01	0.84	0.210	1.43	0.147	1.02	1.00	0.189	No
426	8.52	150.13	63.96	86.17	0.84	0.210	1.43	0.147	1.01	1.00	0.188	No
427	8.54	150.48	64.16	86.32	0.84	0.210	1.43	0.147	1.01	1.00	0.188	No
428	8.56	150.83	64.35	86.48	0.84	0.210	1.43	0.147	1.01	1.00	0.188	No
429	8.58	151.19	64.55	86.64	0.84	0.210	1.43	0.147	1.01	1.00	0.188	No
430	8.60	151.54	64.75	86.79	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
431	8.62	151.89	64.94	86.95	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
432	8.64	152.24	65.14	87.10	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
433	8.66	152.59	65.33	87.25	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
434	8.68	152.93	65.53	87.40	0.84	0.210	1.43	0.147	1.01	1.00	0.189	No
435	8.70	153.27	65.73	87.55	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
436	8.72	153.62	65.92	87.69	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
437	8.74	153.96	66.12	87.84	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
438	8.76	154.30	66.32	87.98	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
439	8.78	154.64	66.51	88.13	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
440	8.81	155.16	66.81	88.36	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
441	8.82	155.34	66.90	88.43	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
442	8.84	155.69	67.10	88.59	0.84	0.210	1.43	0.147	1.01	1.00	2.000	Yes
443	8.86	156.05	67.30	88.76	0.83	0.210	1.43	0.147	1.01	1.00	2.000	Yes
444	8.88	156.41	67.49	88.92	0.83	0.210	1.43	0.147	1.01	1.00	0.189	No
445	8.90	156.77	67.69	89.08	0.83	0.210	1.43	0.147	1.01	1.00	0.189	No
446	8.92	157.14	67.89	89.25	0.83	0.210	1.43	0.147	1.01	1.00	0.189	No
447	8.94	157.50	68.08	89.42	0.83	0.210	1.43	0.147	1.01	1.00	0.189	No
448	8.96	157.86	68.28	89.58	0.83	0.210	1.43	0.147	1.01	1.00	0.188	No
449	8.98	158.22	68.47	89.75	0.83	0.210	1.43	0.147	1.01	1.00	0.188	No
450	9.01	158.76	68.77	89.99	0.83	0.210	1.43	0.147	1.01	1.00	0.188	No
451	9.02	158.94	68.87	90.07	0.83	0.210	1.43	0.147	1.01	1.00	0.188	No
452	9.04	159.30	69.06	90.24	0.83	0.210	1.43	0.147	1.01	1.00	0.188	No
453	9.06	159.65	69.26	90.40	0.83	0.210	1.43	0.147	1.01	1.00	0.189	No
454	9.08	160.01	69.45	90.56	0.83	0.210	1.43	0.147	1.01	1.00	0.189	No
455	9.10	160.36	69.65	90.71	0.83	0.210	1.43	0.147	1.01	1.00	0.190	No
456	9.12	160.72	69.85	90.87	0.83	0.210	1.43	0.147	1.01	1.00	0.190	No
457	9.14	161.08	70.04	91.03	0.83	0.210	1.43	0.147	1.01	1.00	0.190	No
458	9.16	161.44	70.24	91.20	0.83	0.210	1.43	0.147	1.01	1.00	0.190	No
459	9.18	161.79	70.44	91.36	0.83	0.210	1.43	0.147	1.01	1.00	0.190	No
460	9.20	162.15	70.63	91.52	0.83	0.210	1.43	0.147	1.01	1.00	0.190	No
461	9.22	162.51	70.83	91.68	0.83	0.209	1.43	0.147	1.01	1.00	0.190	No
462	9.24	162.86	71.02	91.84	0.83	0.209	1.43	0.147	1.01	1.00	0.190	No
463	9.26	163.22	71.22	92.00	0.83	0.209	1.43	0.147	1.01	1.00	0.190	No
464	9.28	163.57	71.42	92.15	0.83	0.209	1.43	0.147	1.01	1.00	0.190	No
465	9.30	163.93	71.61	92.31	0.82	0.209	1.43	0.147	1.01	1.00	0.190	No
466	9.32	164.28	71.81	92.47	0.82	0.209	1.43	0.147	1.01	1.00	0.190	No
467	9.34	164.63	72.01	92.63	0.82	0.209	1.43	0.147	1.01	1.00	0.189	No
468	9.36	164.99	72.20	92.79	0.82	0.209	1.43	0.146	1.01	1.00	0.189	No
469	9.38	165.34	72.40	92.94	0.82	0.209	1.43	0.146	1.01	1.00	0.189	No
470	9.40	165.69	72.59	93.10	0.82	0.209	1.43	0.146	1.01	1.00	0.189	No
471	9.42	166.05	72.79	93.26	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
472	9.44	166.40	72.99	93.41	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
473	9.46	166.75	73.18	93.56	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
474	9.48	167.10	73.38	93.72	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
475	9.50	167.45	73.58	93.88	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
476	9.52	167.81	73.77	94.03	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
477	9.54	168.16	73.97	94.19	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
478	9.56	168.52	74.16	94.35	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
479	9.58	168.87	74.36	94.51	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No
480	9.60	169.22	74.56	94.66	0.82	0.209	1.43	0.146	1.01	1.00	0.190	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
481	9.62	169.57	74.75	94.82	0.82	0.209	1.43	0.146	1.01	1.00	0.191	No
482	9.64	169.92	74.95	94.97	0.82	0.209	1.43	0.146	1.01	1.00	0.191	No
483	9.66	170.26	75.14	95.12	0.82	0.209	1.43	0.146	1.01	1.00	0.191	No
484	9.68	170.61	75.34	95.27	0.82	0.209	1.43	0.146	1.01	1.00	0.191	No
485	9.70	170.96	75.54	95.42	0.81	0.209	1.43	0.146	1.01	1.00	0.191	No
486	9.72	171.31	75.73	95.58	0.81	0.209	1.43	0.146	1.01	1.00	0.191	No
487	9.74	171.67	75.93	95.74	0.81	0.209	1.43	0.146	1.00	1.00	0.191	No
488	9.76	172.02	76.13	95.89	0.81	0.209	1.43	0.146	1.00	1.00	0.191	No
489	9.78	172.37	76.32	96.05	0.81	0.209	1.43	0.146	1.00	1.00	0.191	No
490	9.80	172.71	76.52	96.20	0.81	0.209	1.43	0.146	1.00	1.00	0.191	No
491	9.82	173.06	76.71	96.35	0.81	0.209	1.43	0.146	1.00	1.00	0.191	No
492	9.84	173.40	76.91	96.49	0.81	0.209	1.43	0.146	1.00	1.00	0.191	No
493	9.86	173.75	77.11	96.64	0.81	0.209	1.43	0.146	1.00	1.00	0.191	No
494	9.88	174.09	77.30	96.79	0.81	0.209	1.43	0.146	1.00	1.00	0.191	No
495	9.90	174.44	77.50	96.94	0.81	0.208	1.43	0.146	1.00	1.00	0.191	No
496	9.92	174.78	77.70	97.08	0.81	0.208	1.43	0.146	1.00	1.00	0.191	No
497	9.94	175.13	77.89	97.23	0.81	0.208	1.43	0.146	1.00	1.00	2.000	Yes
498	9.96	175.47	78.09	97.38	0.81	0.208	1.43	0.146	1.00	1.00	2.000	Yes
499	9.98	175.82	78.28	97.54	0.81	0.208	1.43	0.146	1.00	1.00	2.000	Yes
500	10.00	176.17	78.48	97.69	0.81	0.208	1.43	0.146	1.00	1.00	2.000	Yes
501	10.02	176.51	78.68	97.83	0.81	0.208	1.43	0.146	1.00	1.00	2.000	Yes
502	10.04	176.86	78.87	97.98	0.81	0.208	1.43	0.146	1.00	1.00	2.000	Yes
503	10.06	177.20	79.07	98.13	0.81	0.208	1.43	0.146	1.00	1.00	2.000	Yes
504	10.08	177.54	79.26	98.27	0.81	0.208	1.43	0.146	1.00	1.00	0.189	No
505	10.11	178.05	79.56	98.49	0.81	0.208	1.43	0.146	1.00	1.00	0.190	No
506	10.12	178.22	79.66	98.56	0.80	0.208	1.43	0.146	1.00	1.00	0.190	No
507	10.14	178.56	79.85	98.70	0.80	0.208	1.43	0.146	1.00	1.00	0.190	No
508	10.16	178.90	80.05	98.85	0.80	0.208	1.43	0.146	1.00	1.00	0.190	No
509	10.18	179.24	80.25	99.00	0.80	0.208	1.43	0.146	1.00	1.00	0.189	No
510	10.20	179.59	80.44	99.14	0.80	0.208	1.43	0.146	1.00	1.00	0.189	No
511	10.22	179.93	80.64	99.29	0.80	0.208	1.43	0.146	1.00	1.00	0.189	No
512	10.24	180.28	80.83	99.45	0.80	0.208	1.43	0.146	1.00	1.00	2.000	Yes
513	10.26	180.63	81.03	99.60	0.80	0.208	1.43	0.146	1.00	1.00	2.000	Yes
514	10.28	180.97	81.23	99.75	0.80	0.208	1.43	0.145	1.00	1.00	2.000	Yes
515	10.30	181.32	81.42	99.90	0.80	0.208	1.43	0.145	1.00	1.00	2.000	Yes
516	10.32	181.66	81.62	100.05	0.80	0.208	1.43	0.145	1.00	1.00	2.000	Yes
517	10.34	182.01	81.82	100.20	0.80	0.208	1.43	0.145	1.00	1.00	2.000	Yes
518	10.36	182.37	82.01	100.36	0.80	0.208	1.43	0.145	1.00	1.00	2.000	Yes
519	10.38	182.73	82.21	100.52	0.80	0.208	1.43	0.145	1.00	1.00	2.000	Yes
520	10.40	183.09	82.40	100.68	0.80	0.208	1.43	0.145	1.00	1.00	2.000	Yes
521	10.42	183.45	82.60	100.85	0.80	0.208	1.43	0.145	1.00	1.00	2.000	Yes
522	10.44	183.81	82.80	101.01	0.80	0.207	1.43	0.145	1.00	1.00	2.000	Yes
523	10.46	184.17	82.99	101.17	0.80	0.207	1.43	0.145	1.00	1.00	2.000	Yes
524	10.48	184.52	83.19	101.34	0.80	0.207	1.43	0.145	1.00	1.00	2.000	Yes
525	10.50	184.88	83.39	101.49	0.80	0.207	1.43	0.145	1.00	1.00	2.000	Yes
526	10.52	185.23	83.58	101.65	0.80	0.207	1.43	0.145	1.00	1.00	2.000	Yes
527	10.54	185.58	83.78	101.80	0.79	0.207	1.43	0.145	1.00	1.00	2.000	Yes
528	10.56	185.92	83.97	101.95	0.79	0.207	1.43	0.145	1.00	1.00	0.189	No

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
529	10.58	186.26	84.17	102.09	0.79	0.207	1.43	0.145	1.00	1.00	0.189	No
530	10.60	186.61	84.37	102.24	0.79	0.207	1.43	0.145	1.00	1.00	0.190	No
531	10.62	186.94	84.56	102.38	0.79	0.207	1.43	0.145	1.00	1.00	0.190	No
532	10.64	187.28	84.76	102.52	0.79	0.207	1.43	0.145	1.00	1.00	0.190	No
533	10.66	187.62	84.95	102.67	0.79	0.207	1.43	0.145	1.00	1.00	0.190	No
534	10.68	187.97	85.15	102.82	0.79	0.207	1.43	0.145	1.00	1.00	0.189	No
535	10.70	188.32	85.35	102.97	0.79	0.207	1.43	0.145	1.00	1.00	0.189	No
536	10.72	188.67	85.54	103.13	0.79	0.207	1.43	0.145	1.00	1.00	0.188	No
537	10.74	189.02	85.74	103.28	0.79	0.207	1.43	0.145	1.00	1.00	0.188	No
538	10.76	189.37	85.94	103.43	0.79	0.207	1.43	0.145	1.00	1.00	0.188	No
539	10.78	189.71	86.13	103.58	0.79	0.207	1.43	0.145	1.00	1.00	0.189	No
540	10.80	190.05	86.33	103.72	0.79	0.207	1.43	0.145	1.00	1.00	0.189	No
541	10.82	190.39	86.52	103.86	0.79	0.207	1.43	0.145	1.00	1.00	2.000	Yes
542	10.84	190.72	86.72	104.00	0.79	0.207	1.43	0.145	1.00	1.00	2.000	Yes
543	10.86	191.07	86.92	104.15	0.79	0.207	1.43	0.145	1.00	1.00	2.000	Yes
544	10.88	191.41	87.11	104.30	0.79	0.206	1.43	0.145	1.00	1.00	2.000	Yes
545	10.91	191.92	87.41	104.52	0.79	0.206	1.43	0.144	1.00	1.00	2.000	Yes
546	10.92	192.09	87.51	104.59	0.79	0.206	1.43	0.144	1.00	1.00	2.000	Yes
547	10.94	192.44	87.70	104.73	0.79	0.206	1.43	0.144	1.00	1.00	2.000	Yes
548	10.96	192.78	87.90	104.88	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
549	10.98	193.13	88.09	105.03	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
550	11.00	193.48	88.29	105.19	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
551	11.02	193.83	88.49	105.34	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
552	11.04	194.18	88.68	105.49	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
553	11.06	194.53	88.88	105.65	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
554	11.08	194.87	89.07	105.80	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
555	11.10	195.22	89.27	105.95	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
556	11.12	195.57	89.47	106.10	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
557	11.14	195.92	89.66	106.25	0.78	0.206	1.43	0.144	1.00	1.00	2.000	Yes
558	11.16	196.26	89.86	106.40	0.78	0.206	1.43	0.144	1.00	1.00	0.188	No
559	11.18	196.61	90.06	106.55	0.78	0.206	1.43	0.144	1.00	1.00	0.188	No
560	11.21	197.12	90.35	106.77	0.78	0.206	1.43	0.144	1.00	1.00	0.188	No
561	11.22	197.29	90.45	106.85	0.78	0.206	1.43	0.144	1.00	1.00	0.189	No
562	11.24	197.63	90.64	106.99	0.78	0.206	1.43	0.144	1.00	1.00	0.189	No
563	11.26	197.98	90.84	107.14	0.78	0.205	1.43	0.144	0.99	1.00	0.188	No
564	11.28	198.32	91.04	107.28	0.78	0.205	1.43	0.144	0.99	1.00	0.188	No
565	11.30	198.66	91.23	107.43	0.78	0.205	1.43	0.144	0.99	1.00	0.188	No
566	11.32	199.00	91.43	107.57	0.78	0.205	1.43	0.144	0.99	1.00	2.000	Yes
567	11.34	199.34	91.63	107.71	0.78	0.205	1.43	0.144	0.99	1.00	2.000	Yes
568	11.36	199.67	91.82	107.85	0.78	0.205	1.43	0.144	0.99	1.00	2.000	Yes
569	11.38	200.01	92.02	107.99	0.77	0.205	1.43	0.144	0.99	1.00	2.000	Yes
570	11.40	200.35	92.21	108.14	0.77	0.205	1.43	0.144	0.99	1.00	2.000	Yes
571	11.42	200.69	92.41	108.28	0.77	0.205	1.43	0.144	0.99	1.00	2.000	Yes
572	11.44	201.03	92.61	108.42	0.77	0.205	1.43	0.144	0.99	1.00	2.000	Yes
573	11.46	201.37	92.80	108.57	0.77	0.205	1.43	0.143	0.99	1.00	2.000	Yes
574	11.48	201.72	93.00	108.72	0.77	0.205	1.43	0.143	0.99	1.00	2.000	Yes
575	11.50	202.06	93.19	108.87	0.77	0.205	1.43	0.143	0.99	1.00	2.000	Yes
576	11.52	202.41	93.39	109.02	0.77	0.205	1.43	0.143	0.99	1.00	2.000	Yes

:: Cyclic Stress Ratio fully adjusted (CSR*) calculation data :: (continued)

Point ID	Depth (m)	σ_v (kPa)	u_0 (kPa)	σ_v' (kPa)	r_d	CSR	MSF	CSR_{eq}	K_σ	User FS	CSR^*	Belongs to transition
577	11.54	202.76	93.59	109.17	0.77	0.205	1.43	0.143	0.99	1.00	2.000	Yes
578	11.56	203.11	93.78	109.33	0.77	0.205	1.43	0.143	0.99	1.00	2.000	Yes
579	11.58	203.45	93.98	109.47	0.77	0.205	1.43	0.143	0.99	1.00	2.000	Yes
580	11.60	203.80	94.18	109.62	0.77	0.205	1.43	0.143	0.99	1.00	2.000	Yes
581	11.62	204.14	94.37	109.76	0.77	0.205	1.43	0.143	0.99	1.00	0.187	No
582	11.64	204.47	94.57	109.90	0.77	0.204	1.43	0.143	0.99	1.00	0.188	No
583	11.66	204.80	94.76	110.03	0.77	0.204	1.43	0.143	0.99	1.00	0.189	No
584	11.68	205.12	94.96	110.16	0.77	0.204	1.43	0.143	0.99	1.00	0.189	No

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
σ_v: Total overburden pressure at test point (kPa)
u_0: Water pressure at test point (kPa)
σ_v': Effective overburden pressure based on GWT during earthquake (kPa)
r_d: Nonlinear shear mass factor
CSR: Cyclic Stress Ratio
MSF: Magnitude Scaling Factor
CSR_{eq}: CSR adjusted for M=7.5
K_σ: Effective overburden stress factor
CSR^*: CSR fully adjusted

:: Cyclic Resistance Ratio (CRR) calculation data ::

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
1	0.02	0.97	72.54	2.62	0.57	1.70	14.74	0.00	14.74	4.000	No	Yes	2.00
2	0.04	1.12	72.92	2.62	0.56	1.70	18.75	0.00	18.75	4.000	No	Yes	2.00
3	0.06	1.13	77.62	2.68	0.56	1.70	18.52	0.00	18.52	4.000	No	Yes	2.00
4	0.08	1.15	84.05	2.76	0.55	1.70	19.39	0.00	19.39	4.000	No	Yes	2.00
5	0.10	1.21	88.11	2.81	0.55	1.70	19.85	0.00	19.85	4.000	No	Yes	2.00
6	0.12	1.28	91.75	2.86	0.54	1.70	21.32	0.00	21.32	4.000	No	Yes	2.00
7	0.14	1.35	94.01	2.89	0.54	1.70	23.14	0.00	23.14	4.000	No	Yes	2.00
8	0.16	1.39	96.77	2.92	0.54	1.70	23.41	0.00	23.41	4.000	No	Yes	2.00
9	0.18	1.39	99.09	2.95	0.53	1.70	23.30	0.00	23.30	4.000	No	Yes	2.00
10	0.20	1.38	100.00	2.98	0.53	1.70	23.35	0.00	23.35	4.000	No	Yes	2.00
11	0.22	1.35	100.00	3.01	0.54	1.70	22.75	0.00	22.75	4.000	No	Yes	2.00
12	0.24	1.32	100.00	3.04	0.54	1.70	22.12	0.00	22.12	4.000	No	Yes	2.00
13	0.26	1.29	100.00	3.07	0.54	1.70	21.72	0.00	21.72	4.000	No	Yes	2.00
14	0.28	1.26	100.00	3.09	0.54	1.70	21.24	0.00	21.24	4.000	No	Yes	2.00
15	0.30	1.23	100.00	3.11	0.54	1.70	20.87	0.00	20.87	4.000	No	Yes	2.00
16	0.32	1.21	100.00	3.13	0.54	1.70	20.25	0.00	20.25	4.000	No	Yes	2.00
17	0.34	1.17	100.00	3.14	0.55	1.70	19.84	0.00	19.84	4.000	No	Yes	2.00
18	0.36	1.13	100.00	3.16	0.55	1.70	19.03	0.00	19.03	4.000	No	Yes	2.00
19	0.38	1.09	100.00	3.17	0.55	1.70	18.51	0.00	18.51	4.000	No	Yes	2.00
20	0.40	1.06	100.00	3.18	0.55	1.70	17.73	0.00	17.73	4.000	No	Yes	2.00
21	0.42	1.03	100.00	3.19	0.55	1.70	17.37	0.00	17.37	4.000	No	Yes	2.00
22	0.45	1.01	100.00	3.20	0.56	1.70	17.23	0.00	17.23	4.000	No	Yes	2.00
23	0.46	0.99	100.00	3.21	0.56	1.70	16.52	0.00	16.52	4.000	No	Yes	2.00
24	0.48	0.97	100.00	3.21	0.56	1.70	16.31	0.00	16.31	4.000	No	Yes	2.00
25	0.50	0.96	100.00	3.21	0.56	1.70	16.28	0.00	16.28	4.000	No	Yes	2.00
26	0.52	0.96	100.00	3.20	0.56	1.70	16.33	0.00	16.33	4.000	No	Yes	2.00
27	0.54	0.95	100.00	3.20	0.56	1.70	15.93	0.00	15.93	4.000	No	Yes	2.00
28	0.56	0.95	100.00	3.19	0.56	1.70	15.75	0.00	15.75	4.000	No	Yes	2.00
29	0.58	0.98	100.00	3.16	0.56	1.70	16.40	0.00	16.40	4.000	No	Yes	2.00
30	0.60	1.01	100.00	3.14	0.56	1.70	17.32	0.00	17.32	4.000	No	Yes	2.00
31	0.62	1.03	100.00	3.12	0.55	1.70	17.41	0.00	17.41	4.000	No	Yes	2.00
32	0.64	1.01	100.00	3.13	0.56	1.70	17.27	0.00	17.27	4.000	No	Yes	2.00
33	0.66	0.99	100.00	3.15	0.56	1.70	16.59	0.00	16.59	4.000	No	Yes	2.00
34	0.68	0.98	100.00	3.16	0.56	1.70	16.45	0.00	16.45	4.000	No	Yes	2.00
35	0.70	0.97	100.00	3.17	0.56	1.70	16.57	0.00	16.57	4.000	No	Yes	2.00
36	0.72	0.99	100.00	3.16	0.56	1.70	16.35	0.00	16.35	4.000	No	Yes	2.00
37	0.74	1.03	100.00	3.15	0.55	1.70	17.38	0.00	17.38	4.000	No	Yes	2.00
38	0.76	1.09	100.00	3.10	0.55	1.70	18.22	0.00	18.22	4.000	No	Yes	2.00
39	0.78	1.16	100.00	3.06	0.55	1.70	19.74	0.00	19.74	4.000	No	Yes	2.00
40	0.80	1.23	100.00	3.01	0.54	1.70	20.64	0.00	20.64	4.000	No	Yes	2.00
41	0.82	1.30	100.00	2.98	0.54	1.70	22.00	0.00	22.00	4.000	No	Yes	2.00
42	0.84	1.38	99.02	2.95	0.54	1.70	23.22	0.00	23.22	4.000	No	Yes	2.00
43	0.86	1.45	97.36	2.93	0.53	1.70	24.51	0.00	24.51	4.000	No	Yes	2.00
44	0.88	1.50	96.54	2.92	0.53	1.70	25.27	0.00	25.27	4.000	No	Yes	2.00
45	0.90	1.53	96.98	2.92	0.53	1.70	25.95	0.00	25.95	4.000	No	Yes	2.00
46	0.92	1.56	97.41	2.93	0.53	1.70	25.64	0.00	25.64	4.000	No	Yes	2.00
47	0.94	1.59	98.06	2.94	0.52	1.70	26.66	0.00	26.66	4.000	No	Yes	2.00
48	0.96	1.64	97.81	2.94	0.52	1.70	27.42	0.00	27.42	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
49	0.98	1.70	97.23	2.93	0.52	1.70	28.36	0.00	28.36	4.000	No	Yes	2.00
50	1.00	1.76	96.22	2.92	0.52	1.70	29.76	0.00	29.76	4.000	No	Yes	2.00
51	1.02	1.82	95.18	2.90	0.51	1.70	30.28	0.00	30.28	4.000	No	Yes	2.00
52	1.05	1.91	93.14	2.88	0.51	1.70	31.22	0.00	31.22	4.000	No	Yes	2.00
53	1.06	2.07	89.79	2.83	0.50	1.70	34.53	0.00	34.53	4.000	No	Yes	2.00
54	1.08	2.25	86.21	2.79	0.49	1.70	37.80	0.00	37.80	4.000	No	Yes	2.00
55	1.11	2.43	82.83	2.75	0.49	1.70	40.22	0.00	40.22	4.000	No	Yes	2.00
56	1.12	2.61	80.22	2.72	0.48	1.70	43.60	0.00	43.60	4.000	No	Yes	2.00
57	1.14	2.79	77.92	2.69	0.47	1.70	46.90	0.00	46.90	4.000	No	Yes	2.00
58	1.17	2.97	76.18	2.66	0.47	1.70	49.25	0.00	49.25	4.000	No	Yes	2.00
59	1.18	3.13	74.88	2.65	0.46	1.70	52.50	0.00	52.50	4.000	No	Yes	2.00
60	1.20	3.25	74.39	2.64	0.45	1.70	54.96	0.00	54.96	4.000	No	Yes	2.00
61	1.22	3.26	75.75	2.66	0.45	1.70	55.49	0.00	55.49	4.000	No	Yes	2.00
62	1.24	3.14	79.12	2.70	0.46	1.70	53.11	0.00	53.11	4.000	No	Yes	2.00
63	1.26	2.94	83.74	2.76	0.46	1.70	49.11	0.00	49.11	4.000	No	Yes	2.00
64	1.28	2.72	88.70	2.82	0.47	1.70	45.33	0.00	45.33	4.000	No	Yes	2.00
65	1.30	2.51	93.35	2.88	0.48	1.70	42.01	0.00	42.01	4.000	No	Yes	2.00
66	1.32	2.34	97.05	2.93	0.49	1.70	38.77	0.00	38.77	4.000	No	Yes	2.00
67	1.34	2.24	99.13	2.95	0.49	1.70	37.06	0.00	37.06	4.000	No	Yes	2.00
68	1.36	2.16	100.00	2.96	0.49	1.70	36.62	0.00	36.62	4.000	No	Yes	2.00
69	1.38	2.09	100.00	2.97	0.50	1.70	34.85	0.00	34.85	4.000	No	Yes	2.00
70	1.40	1.99	100.00	2.98	0.50	1.70	33.47	0.00	33.47	4.000	No	Yes	2.00
71	1.42	1.90	100.00	2.99	0.51	1.70	31.69	0.00	31.69	4.000	No	Yes	2.00
72	1.44	1.79	100.00	3.01	0.51	1.70	29.98	0.00	29.98	4.000	No	Yes	2.00
73	1.46	1.69	100.00	3.03	0.52	1.70	28.13	0.00	28.13	4.000	No	Yes	2.00
74	1.48	1.59	100.00	3.06	0.52	1.70	26.49	0.00	26.49	4.000	No	Yes	2.00
75	1.50	1.53	100.00	3.07	0.53	1.70	25.36	0.00	25.36	4.000	No	Yes	2.00
76	1.52	1.51	100.00	3.07	0.53	1.70	25.13	0.00	25.13	4.000	No	Yes	2.00
77	1.54	1.51	100.00	3.05	0.53	1.70	25.05	0.00	25.05	4.000	No	Yes	2.00
78	1.56	1.51	100.00	3.03	0.53	1.70	25.50	0.00	25.50	4.000	No	Yes	2.00
79	1.58	1.51	100.00	3.02	0.53	1.70	25.28	0.00	25.28	4.000	No	Yes	2.00
80	1.60	1.49	100.00	3.01	0.53	1.70	24.90	0.00	24.90	4.000	No	Yes	2.00
81	1.62	1.47	100.00	3.00	0.53	1.70	24.42	0.00	24.42	4.000	No	Yes	2.00
82	1.64	1.44	100.00	3.00	0.53	1.70	23.86	0.00	23.86	4.000	No	Yes	2.00
83	1.66	1.41	100.00	3.00	0.53	1.70	23.46	0.00	23.46	4.000	No	Yes	2.00
84	1.68	1.37	100.00	3.01	0.54	1.70	22.94	0.00	22.94	4.000	No	Yes	2.00
85	1.70	1.34	100.00	3.02	0.54	1.70	22.09	0.00	22.09	4.000	No	Yes	2.00
86	1.72	1.29	100.00	3.04	0.54	1.70	21.69	0.00	21.69	4.000	No	Yes	2.00
87	1.74	1.26	100.00	3.05	0.54	1.70	20.65	0.00	20.65	4.000	No	Yes	2.00
88	1.76	1.22	100.00	3.06	0.54	1.70	20.26	0.00	20.26	4.000	No	Yes	2.00
89	1.78	1.20	100.00	3.06	0.55	1.70	20.05	0.00	20.05	4.000	No	Yes	2.00
90	1.80	1.17	100.00	3.07	0.55	1.70	19.51	0.00	19.51	4.000	No	Yes	2.00
91	1.82	1.13	100.00	3.08	0.55	1.70	18.56	0.00	18.56	4.000	No	Yes	2.00
92	1.84	1.10	100.00	3.09	0.55	1.70	18.05	0.00	18.05	4.000	No	Yes	2.00
93	1.86	1.07	100.00	3.09	0.55	1.70	17.59	0.00	17.59	4.000	No	Yes	2.00
94	1.88	1.07	100.00	3.08	0.56	1.70	17.36	0.00	17.36	4.000	No	Yes	2.00
95	1.90	1.08	100.00	3.06	0.55	1.70	17.95	0.00	17.95	4.000	No	Yes	2.00
96	1.92	1.09	100.00	3.03	0.55	1.70	17.65	0.00	17.65	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
97	1.94	1.08	100.00	3.02	0.55	1.70	17.73	0.00	17.73	4.000	No	Yes	2.00
98	1.96	1.06	100.00	3.02	0.55	1.70	17.47	0.00	17.47	4.000	No	Yes	2.00
99	1.98	1.04	100.00	3.03	0.56	1.70	17.02	0.00	17.02	4.000	No	Yes	2.00
100	2.00	1.01	100.00	3.05	0.56	1.70	16.60	0.00	16.60	4.000	No	Yes	2.00
101	2.02	0.98	100.00	3.07	0.56	1.70	15.92	0.00	15.92	4.000	No	Yes	2.00
102	2.04	0.96	100.00	3.08	0.56	1.70	15.62	0.00	15.62	4.000	No	Yes	2.00
103	2.06	0.95	100.00	3.10	0.56	1.70	15.58	0.00	15.58	4.000	No	Yes	2.00
104	2.08	0.92	100.00	3.12	0.56	1.70	15.24	0.00	15.24	4.000	No	Yes	2.00
105	2.10	0.89	100.00	3.14	0.57	1.70	14.49	0.00	14.49	4.000	No	Yes	2.00
106	2.12	0.86	100.00	3.16	0.57	1.70	13.88	0.00	13.88	4.000	No	Yes	2.00
107	2.15	0.84	100.00	3.17	0.57	1.70	13.77	0.00	13.77	4.000	No	Yes	2.00
108	2.16	0.83	100.00	3.18	0.57	1.70	13.41	0.00	13.41	4.000	No	Yes	2.00
109	2.18	0.82	100.00	3.18	0.57	1.69	13.24	0.00	13.24	4.000	No	Yes	2.00
110	2.20	0.82	100.00	3.18	0.57	1.68	13.32	0.00	13.32	4.000	No	Yes	2.00
111	2.22	0.83	100.00	3.17	0.57	1.67	13.04	0.00	13.04	4.000	No	Yes	2.00
112	2.24	0.84	100.00	3.15	0.57	1.67	13.30	0.00	13.30	4.000	No	Yes	2.00
113	2.26	0.86	100.00	3.13	0.57	1.66	13.66	0.00	13.66	4.000	No	Yes	2.00
114	2.28	0.90	100.00	3.10	0.57	1.65	13.98	0.00	13.98	4.000	No	Yes	2.00
115	2.30	0.92	100.00	3.08	0.56	1.63	14.75	0.00	14.75	4.000	No	Yes	2.00
116	2.32	0.92	100.00	3.08	0.56	1.63	14.61	0.00	14.61	4.000	No	Yes	2.00
117	2.34	0.90	100.00	3.10	0.57	1.62	14.44	0.00	14.44	4.000	No	Yes	2.00
118	2.36	0.89	100.00	3.11	0.57	1.61	14.10	0.00	14.10	4.000	No	Yes	2.00
119	2.38	0.90	100.00	3.11	0.57	1.61	14.10	0.00	14.10	4.000	No	Yes	2.00
120	2.40	0.91	100.00	3.11	0.57	1.60	14.45	0.00	14.45	4.000	No	Yes	2.00
121	2.42	0.91	100.00	3.11	0.57	1.59	14.46	0.00	14.46	4.000	No	Yes	2.00
122	2.44	0.89	100.00	3.12	0.57	1.59	14.12	0.00	14.12	4.000	No	Yes	2.00
123	2.46	0.84	100.00	3.15	0.57	1.58	13.08	0.00	13.08	4.000	No	Yes	2.00
124	2.48	0.78	100.00	3.19	0.57	1.58	12.38	0.00	12.38	4.000	No	Yes	2.00
125	2.50	0.71	100.00	3.24	0.58	1.58	11.14	0.00	11.14	4.000	No	Yes	2.00
126	2.52	0.65	100.00	3.30	0.58	1.58	10.00	0.00	10.00	4.000	No	Yes	2.00
127	2.54	0.59	100.00	3.36	0.59	1.58	9.23	0.00	9.23	4.000	No	Yes	2.00
128	2.56	0.56	100.00	3.38	0.59	1.58	8.59	0.00	8.59	4.000	No	Yes	2.00
129	2.58	0.57	100.00	3.37	0.59	1.58	8.40	0.00	8.40	4.000	No	Yes	2.00
130	2.60	0.60	100.00	3.31	0.59	1.57	8.83	0.00	8.83	4.000	No	Yes	2.00
131	2.62	0.65	100.00	3.23	0.58	1.57	9.42	0.00	9.42	4.000	No	Yes	2.00
132	2.64	0.71	100.00	3.13	0.58	1.56	10.45	0.00	10.45	4.000	No	Yes	2.00
133	2.66	0.77	100.00	3.04	0.58	1.55	11.31	0.00	11.31	4.000	No	Yes	2.00
134	2.68	0.83	99.13	2.95	0.57	1.55	12.39	0.00	12.39	4.000	No	Yes	2.00
135	2.70	0.88	94.65	2.90	0.57	1.54	13.14	0.00	13.14	4.000	No	Yes	2.00
136	2.72	0.90	93.26	2.88	0.57	1.54	13.43	0.00	13.43	4.000	No	Yes	2.00
137	2.74	0.90	94.85	2.90	0.57	1.54	13.40	0.00	13.40	4.000	No	Yes	2.00
138	2.76	0.91	96.82	2.92	0.57	1.53	13.28	0.00	13.28	4.000	No	Yes	2.00
139	2.78	0.94	98.18	2.94	0.57	1.53	13.79	0.00	13.79	4.000	No	Yes	2.00
140	2.80	0.99	97.91	2.94	0.57	1.52	14.62	0.00	14.62	4.000	No	Yes	2.00
141	2.82	1.04	97.74	2.93	0.56	1.52	15.51	0.00	15.51	4.000	No	Yes	2.00
142	2.84	1.07	98.19	2.94	0.56	1.51	16.00	0.00	16.00	4.000	No	Yes	2.00
143	2.86	1.09	99.34	2.95	0.56	1.51	16.20	0.00	16.20	4.000	No	Yes	2.00
144	2.88	1.12	99.55	2.96	0.56	1.50	16.22	0.00	16.22	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
145	2.90	1.16	98.82	2.95	0.56	1.50	17.12	0.00	17.12	4.000	No	Yes	2.00
146	2.92	1.20	98.14	2.94	0.55	1.49	17.80	0.00	17.80	4.000	No	Yes	2.00
147	2.94	1.22	99.04	2.95	0.55	1.49	18.02	0.00	18.02	4.000	No	Yes	2.00
148	2.96	1.20	100.00	2.98	0.55	1.49	17.70	0.00	17.70	4.000	No	Yes	2.00
149	2.98	1.18	100.00	3.00	0.56	1.49	17.10	0.00	17.10	4.000	No	Yes	2.00
150	3.00	1.13	100.00	3.04	0.56	1.49	16.88	0.00	16.88	4.000	No	Yes	2.00
151	3.02	1.08	100.00	3.07	0.56	1.49	15.67	0.00	15.67	4.000	No	Yes	2.00
152	3.04	1.02	100.00	3.12	0.56	1.49	14.97	0.00	14.97	4.000	No	Yes	2.00
153	3.06	0.98	100.00	3.15	0.57	1.49	14.34	0.00	14.34	4.000	No	Yes	2.00
154	3.09	0.97	100.00	3.16	0.57	1.48	13.88	0.00	13.88	4.000	No	Yes	2.00
155	3.10	0.98	100.00	3.15	0.57	1.48	14.11	0.00	14.11	4.000	No	Yes	2.00
156	3.12	1.03	100.00	3.11	0.57	1.48	14.34	0.00	14.34	4.000	No	Yes	2.00
157	3.15	1.08	100.00	3.06	0.56	1.47	15.53	0.00	15.53	4.000	No	Yes	2.00
158	3.16	1.14	100.00	3.00	0.56	1.47	15.86	0.00	15.86	4.000	No	Yes	2.00
159	3.18	1.17	99.06	2.95	0.56	1.46	16.83	0.00	16.83	4.000	No	Yes	2.00
160	3.20	1.19	95.62	2.91	0.56	1.46	16.80	0.00	16.80	4.000	No	Yes	2.00
161	3.22	1.18	94.30	2.89	0.56	1.46	16.62	0.00	16.62	4.000	No	Yes	2.00
162	3.24	1.18	93.33	2.88	0.56	1.46	16.28	0.00	16.28	4.000	No	Yes	2.00
163	3.26	1.18	92.06	2.86	0.56	1.46	16.28	0.00	16.28	4.000	No	Yes	2.00
164	3.28	1.20	90.86	2.85	0.56	1.45	16.69	0.00	16.69	4.000	No	Yes	2.00
165	3.30	1.22	89.41	2.83	0.56	1.45	16.76	0.00	16.76	4.000	No	Yes	2.00
166	3.32	1.23	88.74	2.82	0.56	1.45	17.11	0.00	17.11	4.000	No	Yes	2.00
167	3.34	1.21	88.93	2.82	0.56	1.44	16.89	0.00	16.89	4.000	No	Yes	2.00
168	3.36	1.18	89.66	2.83	0.56	1.45	15.97	0.00	15.97	4.000	No	Yes	2.00
169	3.38	1.15	90.32	2.84	0.56	1.44	15.81	0.00	15.81	4.000	No	Yes	2.00
170	3.40	1.14	90.22	2.84	0.56	1.44	15.60	0.00	15.60	4.000	No	Yes	2.00
171	3.42	1.12	91.17	2.85	0.56	1.44	15.55	0.00	15.55	4.000	No	Yes	2.00
172	3.44	1.08	93.49	2.88	0.57	1.44	14.87	0.00	14.87	4.000	No	Yes	2.00
173	3.46	1.00	97.17	2.93	0.57	1.44	13.66	0.00	13.66	4.000	No	Yes	2.00
174	3.48	0.91	100.00	2.99	0.57	1.44	12.49	0.00	12.49	4.000	No	Yes	2.00
175	3.50	0.82	100.00	3.05	0.58	1.44	11.19	0.00	11.19	4.000	No	Yes	2.00
176	3.52	0.75	100.00	3.10	0.58	1.45	10.08	0.00	10.08	4.000	No	Yes	2.00
177	3.54	0.69	100.00	3.14	0.58	1.44	9.60	0.00	9.60	4.000	No	Yes	2.00
178	3.56	0.64	100.00	3.17	0.59	1.45	8.68	0.00	8.68	4.000	No	Yes	2.00
179	3.58	0.62	100.00	3.17	0.59	1.45	8.19	0.00	8.19	4.000	No	Yes	2.00
180	3.60	0.61	100.00	3.16	0.59	1.44	8.43	0.00	8.43	4.000	No	Yes	2.00
181	3.62	0.61	100.00	3.12	0.59	1.44	8.27	0.00	8.27	4.000	No	Yes	2.00
182	3.64	0.62	100.00	3.07	0.59	1.44	8.38	0.00	8.38	4.000	No	Yes	2.00
183	3.66	0.64	100.00	3.03	0.59	1.44	8.69	0.00	8.69	4.000	No	Yes	2.00
184	3.68	0.67	100.00	2.97	0.59	1.43	8.93	0.00	8.93	4.000	No	Yes	2.00
185	3.70	0.72	96.23	2.92	0.58	1.43	9.80	0.00	9.80	4.000	No	Yes	2.00
186	3.72	0.77	91.93	2.86	0.58	1.43	10.39	0.00	10.39	4.000	No	Yes	2.00
187	3.74	0.79	91.08	2.85	0.58	1.42	10.78	0.00	10.78	4.000	No	Yes	2.00
188	3.76	0.80	91.77	2.86	0.58	1.42	10.68	0.00	10.68	4.000	No	Yes	2.00
189	3.78	0.81	93.22	2.88	0.58	1.42	10.88	0.00	10.88	4.000	No	Yes	2.00
190	3.80	0.83	93.01	2.88	0.58	1.42	10.90	0.00	10.90	4.000	No	Yes	2.00
191	3.82	0.85	91.68	2.86	0.58	1.41	11.36	0.00	11.36	4.000	No	Yes	2.00
192	3.84	0.91	88.41	2.82	0.58	1.41	11.91	0.00	11.91	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
193	3.86	1.04	83.19	2.75	0.58	1.41	12.95	0.00	12.95	4.000	No	Yes	2.00
194	3.88	1.14	81.86	2.74	0.56	1.39	17.04	0.00	17.04	4.000	No	Yes	2.00
195	3.90	1.22	81.82	2.74	0.57	1.39	15.98	0.00	15.98	4.000	No	Yes	2.00
196	3.92	1.21	83.99	2.76	0.56	1.39	15.86	0.00	15.86	4.000	No	Yes	2.00
197	3.94	1.26	82.64	2.75	0.56	1.39	16.08	0.00	16.08	4.000	No	Yes	2.00
198	3.96	1.32	81.32	2.73	0.56	1.38	17.55	0.00	17.55	4.000	No	Yes	2.00
199	3.98	1.37	80.36	2.72	0.56	1.38	18.04	0.00	18.04	4.000	No	Yes	2.00
200	4.00	1.34	83.44	2.76	0.56	1.38	18.30	0.00	18.30	4.000	No	Yes	2.00
201	4.02	1.25	89.18	2.83	0.56	1.38	16.75	0.00	16.75	4.000	No	Yes	2.00
202	4.05	1.14	96.00	2.91	0.57	1.38	14.71	0.00	14.71	4.000	No	Yes	2.00
203	4.06	1.00	100.00	3.02	0.57	1.38	14.13	0.00	14.13	4.000	No	Yes	2.00
204	4.08	0.88	100.00	3.11	0.58	1.38	11.11	0.00	11.11	4.000	No	Yes	2.00
205	4.10	0.76	100.00	3.21	0.58	1.39	10.23	0.00	10.23	4.000	No	Yes	2.00
206	4.12	0.71	100.00	3.25	0.58	1.39	9.43	0.00	9.43	4.000	No	Yes	2.00
207	4.14	0.70	100.00	3.25	0.59	1.38	9.05	0.00	9.05	4.000	No	Yes	2.00
208	4.16	0.77	100.00	3.16	0.58	1.38	9.79	0.00	9.79	4.000	No	Yes	2.00
209	4.18	0.92	100.00	3.00	0.58	1.37	11.83	0.00	11.83	4.000	No	Yes	2.00
210	4.20	1.13	90.57	2.84	0.57	1.36	15.02	0.00	15.02	4.000	No	Yes	2.00
211	4.22	1.38	80.24	2.72	0.56	1.36	17.90	0.00	17.90	4.000	No	Yes	2.00
212	4.24	1.64	72.72	2.62	0.55	1.35	21.96	0.00	21.96	4.000	No	Yes	2.00
213	4.26	1.86	67.89	2.56	0.54	1.34	25.13	57.53	82.66	0.118	No	No	0.73
214	4.28	2.01	65.08	2.53	0.54	1.33	26.65	57.39	84.04	0.120	No	No	0.74
215	4.30	2.09	63.67	2.51	0.53	1.33	27.67	57.37	85.03	0.121	No	No	0.75
216	4.32	2.12	62.74	2.50	0.53	1.33	27.91	57.22	85.12	0.121	No	No	0.74
217	4.34	2.17	62.03	2.49	0.53	1.33	27.82	57.02	84.84	0.120	No	No	0.74
218	4.36	2.20	62.89	2.50	0.53	1.32	29.52	57.71	87.23	0.123	No	No	0.76
219	4.38	2.17	66.29	2.54	0.53	1.32	28.95	58.31	87.26	0.123	No	No	0.76
220	4.40	1.99	73.09	2.63	0.53	1.32	26.32	0.00	26.32	4.000	No	Yes	2.00
221	4.42	1.79	80.58	2.72	0.54	1.32	22.89	0.00	22.89	4.000	No	Yes	2.00
222	4.44	1.66	85.32	2.78	0.55	1.33	21.02	0.00	21.02	4.000	No	Yes	2.00
223	4.46	1.64	85.64	2.78	0.54	1.32	21.36	0.00	21.36	4.000	No	Yes	2.00
224	4.49	1.61	86.24	2.79	0.54	1.32	21.96	0.00	21.96	4.000	No	Yes	2.00
225	4.50	1.52	89.34	2.83	0.55	1.32	19.73	0.00	19.73	4.000	No	Yes	2.00
226	4.52	1.39	94.24	2.89	0.55	1.32	17.75	0.00	17.75	4.000	No	Yes	2.00
227	4.54	1.33	95.75	2.91	0.56	1.32	17.15	0.00	17.15	4.000	No	Yes	2.00
228	4.56	1.30	95.70	2.91	0.56	1.32	17.32	0.00	17.32	4.000	No	Yes	2.00
229	4.58	1.25	96.26	2.92	0.56	1.32	16.38	0.00	16.38	4.000	No	Yes	2.00
230	4.60	1.19	98.05	2.94	0.56	1.32	15.06	0.00	15.06	4.000	No	Yes	2.00
231	4.62	1.17	97.72	2.93	0.56	1.32	14.92	0.00	14.92	4.000	No	Yes	2.00
232	4.64	1.19	95.41	2.91	0.56	1.32	15.21	0.00	15.21	4.000	No	Yes	2.00
233	4.66	1.24	92.55	2.87	0.56	1.32	15.62	0.00	15.62	4.000	No	Yes	2.00
234	4.68	1.35	88.00	2.81	0.56	1.31	16.34	0.00	16.34	4.000	No	Yes	2.00
235	4.70	1.49	82.59	2.74	0.55	1.31	19.16	0.00	19.16	4.000	No	Yes	2.00
236	4.72	1.54	80.68	2.72	0.55	1.30	20.88	0.00	20.88	4.000	No	Yes	2.00
237	4.74	1.46	84.34	2.77	0.56	1.30	18.42	0.00	18.42	4.000	No	Yes	2.00
238	4.76	1.30	91.99	2.86	0.56	1.30	16.35	0.00	16.35	4.000	No	Yes	2.00
239	4.78	1.19	97.67	2.93	0.56	1.31	14.96	0.00	14.96	4.000	No	Yes	2.00
240	4.80	1.09	100.00	2.99	0.57	1.31	14.09	0.00	14.09	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
241	4.82	1.01	100.00	3.04	0.57	1.31	12.39	0.00	12.39	4.000	No	Yes	2.00
242	4.84	1.10	100.00	3.00	0.57	1.31	12.15	0.00	12.15	4.000	No	Yes	2.00
243	4.86	1.31	95.24	2.90	0.56	1.29	17.23	0.00	17.23	4.000	No	Yes	2.00
244	4.88	1.58	86.41	2.79	0.55	1.29	20.05	0.00	20.05	4.000	No	Yes	2.00
245	4.90	1.79	80.87	2.72	0.54	1.28	22.33	0.00	22.33	4.000	No	Yes	2.00
246	4.92	1.93	77.55	2.68	0.54	1.28	25.09	0.00	25.09	4.000	No	Yes	2.00
247	4.94	1.97	76.56	2.67	0.53	1.27	25.42	0.00	25.42	4.000	No	Yes	2.00
248	4.96	1.89	77.38	2.68	0.54	1.27	23.80	0.00	23.80	4.000	No	Yes	2.00
249	4.98	1.78	78.96	2.70	0.54	1.28	22.11	0.00	22.11	4.000	No	Yes	2.00
250	5.00	1.73	80.15	2.71	0.55	1.28	21.50	0.00	21.50	4.000	No	Yes	2.00
251	5.02	1.71	81.48	2.73	0.55	1.27	21.64	0.00	21.64	4.000	No	Yes	2.00
252	5.04	1.69	83.29	2.75	0.55	1.27	21.41	0.00	21.41	4.000	No	Yes	2.00
253	5.06	1.62	86.91	2.80	0.55	1.27	20.58	0.00	20.58	4.000	No	Yes	2.00
254	5.08	1.56	90.51	2.84	0.55	1.27	19.33	0.00	19.33	4.000	No	Yes	2.00
255	5.10	1.59	91.32	2.85	0.55	1.27	19.03	0.00	19.03	4.000	No	Yes	2.00
256	5.12	1.73	87.38	2.80	0.54	1.26	21.34	0.00	21.34	4.000	No	Yes	2.00
257	5.14	1.85	84.27	2.77	0.54	1.26	24.44	0.00	24.44	4.000	No	Yes	2.00
258	5.16	1.76	86.89	2.80	0.54	1.26	23.29	0.00	23.29	4.000	No	Yes	2.00
259	5.18	1.54	93.34	2.88	0.55	1.26	17.90	0.00	17.90	4.000	No	Yes	2.00
260	5.20	1.38	98.03	2.94	0.56	1.26	16.61	0.00	16.61	4.000	No	Yes	2.00
261	5.22	1.45	93.38	2.88	0.56	1.26	17.19	0.00	17.19	4.000	No	Yes	2.00
262	5.24	1.56	87.70	2.81	0.55	1.26	20.23	0.00	20.23	4.000	No	Yes	2.00
263	5.26	1.57	87.01	2.80	0.55	1.25	20.45	0.00	20.45	4.000	No	Yes	2.00
264	5.28	1.43	93.26	2.88	0.56	1.26	17.63	0.00	17.63	4.000	No	Yes	2.00
265	5.30	1.23	100.00	2.99	0.56	1.26	14.89	0.00	14.89	4.000	No	Yes	2.00
266	5.32	1.09	100.00	3.07	0.57	1.26	13.20	0.00	13.20	4.000	No	Yes	2.00
267	5.34	1.00	100.00	3.11	0.57	1.26	12.44	0.00	12.44	4.000	No	Yes	2.00
268	5.36	0.96	100.00	3.12	0.58	1.26	11.73	0.00	11.73	4.000	No	Yes	2.00
269	5.38	0.94	100.00	3.13	0.58	1.26	11.49	0.00	11.49	4.000	No	Yes	2.00
270	5.40	0.94	100.00	3.11	0.58	1.26	11.36	0.00	11.36	4.000	No	Yes	2.00
271	5.42	0.97	100.00	3.06	0.58	1.25	11.59	0.00	11.59	4.000	No	Yes	2.00
272	5.44	1.04	100.00	2.99	0.57	1.25	12.43	0.00	12.43	4.000	No	Yes	2.00
273	5.46	1.14	95.79	2.91	0.57	1.25	13.78	0.00	13.78	4.000	No	Yes	2.00
274	5.48	1.21	92.42	2.87	0.57	1.25	14.96	0.00	14.96	4.000	No	Yes	2.00
275	5.50	1.22	92.29	2.87	0.57	1.24	14.92	0.00	14.92	4.000	No	Yes	2.00
276	5.52	1.17	96.33	2.92	0.57	1.24	14.43	0.00	14.43	4.000	No	Yes	2.00
277	5.54	1.09	100.00	3.00	0.57	1.24	13.14	0.00	13.14	4.000	No	Yes	2.00
278	5.56	1.00	100.00	3.08	0.57	1.24	12.09	0.00	12.09	4.000	No	Yes	2.00
279	5.58	0.96	100.00	3.14	0.58	1.24	11.40	0.00	11.40	4.000	No	Yes	2.00
280	5.60	1.00	100.00	3.12	0.58	1.24	11.74	0.00	11.74	4.000	No	Yes	2.00
281	5.62	1.08	100.00	3.07	0.57	1.24	13.40	0.00	13.40	4.000	No	Yes	2.00
282	5.64	1.14	100.00	3.03	0.57	1.23	14.17	0.00	14.17	4.000	No	Yes	2.00
283	5.66	1.14	100.00	3.02	0.57	1.23	13.67	0.00	13.67	4.000	No	Yes	2.00
284	5.68	1.16	100.00	2.98	0.57	1.23	13.22	0.00	13.22	4.000	No	Yes	2.00
285	5.70	1.29	95.30	2.90	0.56	1.23	15.06	0.00	15.06	4.000	No	Yes	2.00
286	5.72	1.48	87.57	2.81	0.56	1.22	17.99	0.00	17.99	4.000	No	Yes	2.00
287	5.74	1.63	84.25	2.77	0.55	1.22	20.04	0.00	20.04	4.000	No	Yes	2.00
288	5.76	1.73	83.50	2.76	0.55	1.22	20.37	0.00	20.37	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
289	5.78	1.83	82.94	2.75	0.55	1.21	21.45	0.00	21.45	4.000	No	Yes	2.00
290	5.80	1.98	80.57	2.72	0.54	1.21	23.51	0.00	23.51	4.000	No	Yes	2.00
291	5.82	2.13	78.47	2.69	0.53	1.20	25.69	0.00	25.69	4.000	No	Yes	2.00
292	5.84	2.11	81.40	2.73	0.53	1.20	26.71	0.00	26.71	4.000	No	Yes	2.00
293	5.87	1.93	88.52	2.82	0.54	1.20	22.79	0.00	22.79	4.000	No	Yes	2.00
294	5.88	1.73	95.86	2.91	0.55	1.21	19.15	0.00	19.15	4.000	No	Yes	2.00
295	5.90	1.74	96.46	2.92	0.55	1.20	19.91	0.00	19.91	4.000	No	Yes	2.00
296	5.92	1.90	91.10	2.85	0.54	1.20	23.10	0.00	23.10	4.000	No	Yes	2.00
297	5.94	1.85	90.71	2.85	0.53	1.20	24.47	0.00	24.47	4.000	No	Yes	2.00
298	5.96	1.62	95.29	2.90	0.55	1.20	18.16	0.00	18.16	4.000	No	Yes	2.00
299	5.99	1.27	100.00	3.04	0.56	1.20	15.05	0.00	15.05	4.000	No	Yes	2.00
300	6.00	1.13	100.00	3.08	0.57	1.21	12.31	0.00	12.31	4.000	No	Yes	2.00
301	6.02	1.10	100.00	3.05	0.57	1.20	13.03	0.00	13.03	4.000	No	Yes	2.00
302	6.04	1.12	100.00	2.98	0.57	1.20	13.57	0.00	13.57	4.000	No	Yes	2.00
303	6.06	1.06	100.00	2.99	0.57	1.20	12.68	0.00	12.68	4.000	No	Yes	2.00
304	6.08	0.98	100.00	3.04	0.58	1.20	11.11	0.00	11.11	4.000	No	Yes	2.00
305	6.10	0.96	100.00	3.05	0.58	1.20	10.83	0.00	10.83	4.000	No	Yes	2.00
306	6.12	1.04	100.00	2.99	0.57	1.20	11.94	0.00	11.94	4.000	Yes	Yes	2.00
307	6.14	1.19	95.09	2.90	0.57	1.20	13.88	0.00	13.88	4.000	Yes	Yes	2.00
308	6.16	1.37	89.91	2.84	0.56	1.19	15.90	0.00	15.90	4.000	Yes	Yes	2.00
309	6.18	1.55	86.49	2.79	0.56	1.19	18.25	0.00	18.25	4.000	Yes	Yes	2.00
310	6.20	1.70	83.77	2.76	0.55	1.18	20.09	0.00	20.09	4.000	Yes	Yes	2.00
311	6.22	1.80	79.87	2.71	0.55	1.18	21.00	0.00	21.00	4.000	Yes	Yes	2.00
312	6.24	1.87	75.40	2.66	0.55	1.18	21.79	0.00	21.79	4.000	Yes	Yes	2.00
313	6.26	1.92	70.61	2.60	0.55	1.18	22.34	57.23	79.58	4.000	Yes	No	2.00
314	6.28	1.95	67.44	2.56	0.55	1.18	22.66	56.73	79.39	4.000	Yes	No	2.00
315	6.30	1.98	65.45	2.53	0.55	1.18	22.93	56.40	79.33	4.000	Yes	No	2.00
316	6.32	2.01	63.36	2.50	0.55	1.18	23.24	56.04	79.28	4.000	Yes	No	2.00
317	6.34	2.05	60.17	2.46	0.55	1.17	23.73	55.41	79.14	4.000	Yes	No	2.00
318	6.36	2.11	56.17	2.41	0.55	1.17	24.35	54.50	78.85	4.000	Yes	No	2.00
319	6.38	2.18	53.53	2.38	0.55	1.17	25.18	53.91	79.08	4.000	Yes	No	2.00
320	6.40	2.25	52.63	2.37	0.55	1.17	26.00	53.83	79.82	0.116	No	No	0.64
321	6.42	2.32	53.27	2.38	0.54	1.17	26.94	54.30	81.23	0.117	No	No	0.65
322	6.44	2.37	54.09	2.39	0.54	1.17	27.34	54.67	82.01	0.118	No	No	0.65
323	6.46	2.39	54.63	2.40	0.54	1.16	27.52	54.90	82.42	0.118	No	No	0.65
324	6.48	2.42	53.89	2.39	0.54	1.16	27.66	54.70	82.36	0.118	No	No	0.65
325	6.50	2.46	52.28	2.37	0.54	1.16	28.24	54.31	82.55	0.118	No	No	0.65
326	6.52	2.50	50.17	2.34	0.54	1.16	28.79	53.70	82.49	0.118	No	No	0.65
327	6.54	2.49	49.87	2.34	0.54	1.16	28.93	53.62	82.55	0.118	No	No	0.65
328	6.56	2.42	52.91	2.37	0.54	1.16	27.84	54.42	82.27	0.118	No	No	0.65
329	6.58	2.32	58.32	2.44	0.54	1.16	26.38	55.66	82.04	0.118	No	No	0.65
330	6.60	2.25	61.93	2.49	0.54	1.16	25.43	56.32	81.76	0.118	No	No	0.65
331	6.62	2.24	61.99	2.49	0.54	1.16	25.38	56.32	81.71	0.117	No	No	0.65
332	6.64	2.28	59.38	2.45	0.54	1.15	25.96	55.83	81.79	0.118	No	No	0.65
333	6.66	2.36	57.84	2.44	0.54	1.15	26.84	55.66	82.51	0.118	No	No	0.65
334	6.68	2.41	57.48	2.43	0.54	1.15	27.99	55.88	83.87	4.000	Yes	No	2.00
335	6.70	2.34	59.95	2.46	0.54	1.15	27.58	56.43	84.01	4.000	Yes	No	2.00
336	6.72	2.02	65.99	2.54	0.54	1.15	24.33	56.92	81.25	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
337	6.74	1.61	76.17	2.66	0.56	1.15	17.27	0.00	17.27	4.000	Yes	Yes	2.00
338	6.76	1.20	92.08	2.86	0.57	1.16	13.66	0.00	13.66	4.000	Yes	Yes	2.00
339	6.78	0.97	100.00	3.01	0.58	1.16	10.44	0.00	10.44	4.000	No	Yes	2.00
340	6.80	0.89	100.00	3.07	0.58	1.16	9.39	0.00	9.39	4.000	No	Yes	2.00
341	6.82	0.88	100.00	3.08	0.58	1.15	10.93	0.00	10.93	4.000	No	Yes	2.00
342	6.85	0.87	100.00	3.09	0.58	1.15	9.79	0.00	9.79	4.000	No	Yes	2.00
343	6.86	0.80	100.00	3.16	0.59	1.15	8.93	0.00	8.93	4.000	No	Yes	2.00
344	6.88	0.75	100.00	3.21	0.59	1.15	8.66	0.00	8.66	4.000	No	Yes	2.00
345	6.90	0.69	100.00	3.26	0.59	1.15	7.79	0.00	7.79	4.000	No	Yes	2.00
346	6.92	0.66	100.00	3.29	0.59	1.15	6.99	0.00	6.99	4.000	No	Yes	2.00
347	6.94	0.68	100.00	3.25	0.59	1.15	7.39	0.00	7.39	4.000	No	Yes	2.00
348	6.96	0.78	100.00	3.13	0.59	1.15	8.45	0.00	8.45	4.000	No	Yes	2.00
349	6.98	0.87	100.00	3.03	0.58	1.15	10.04	0.00	10.04	4.000	No	Yes	2.00
350	7.00	0.90	100.00	3.00	0.58	1.14	10.41	0.00	10.41	4.000	No	Yes	2.00
351	7.02	0.85	100.00	3.04	0.59	1.15	9.29	0.00	9.29	4.000	No	Yes	2.00
352	7.04	0.77	100.00	3.13	0.59	1.14	8.47	0.00	8.47	4.000	No	Yes	2.00
353	7.06	0.72	100.00	3.21	0.59	1.14	7.91	0.00	7.91	4.000	No	Yes	2.00
354	7.08	0.70	100.00	3.26	0.59	1.14	7.45	0.00	7.45	4.000	No	Yes	2.00
355	7.10	0.69	100.00	3.28	0.59	1.14	7.75	0.00	7.75	4.000	No	Yes	2.00
356	7.12	0.71	100.00	3.27	0.59	1.14	7.81	0.00	7.81	4.000	No	Yes	2.00
357	7.14	0.74	100.00	3.23	0.59	1.14	8.06	0.00	8.06	4.000	No	Yes	2.00
358	7.16	0.76	100.00	3.20	0.59	1.14	8.58	0.00	8.58	4.000	No	Yes	2.00
359	7.18	0.77	100.00	3.20	0.59	1.14	8.60	0.00	8.60	4.000	No	Yes	2.00
360	7.20	0.76	100.00	3.24	0.59	1.14	8.36	0.00	8.36	4.000	No	Yes	2.00
361	7.22	0.75	100.00	3.28	0.59	1.13	8.15	0.00	8.15	4.000	No	Yes	2.00
362	7.24	0.75	100.00	3.31	0.59	1.13	8.12	0.00	8.12	4.000	No	Yes	2.00
363	7.26	0.76	100.00	3.32	0.59	1.13	8.36	0.00	8.36	4.000	No	Yes	2.00
364	7.28	0.78	100.00	3.31	0.59	1.13	8.53	0.00	8.53	4.000	No	Yes	2.00
365	7.30	0.78	100.00	3.32	0.59	1.13	8.70	0.00	8.70	4.000	No	Yes	2.00
366	7.32	0.76	100.00	3.35	0.59	1.13	8.34	0.00	8.34	4.000	No	Yes	2.00
367	7.34	0.73	100.00	3.38	0.59	1.13	7.96	0.00	7.96	4.000	No	Yes	2.00
368	7.36	0.69	100.00	3.41	0.59	1.13	7.60	0.00	7.60	4.000	No	Yes	2.00
369	7.38	0.68	100.00	3.42	0.59	1.13	7.15	0.00	7.15	4.000	No	Yes	2.00
370	7.40	0.68	100.00	3.41	0.59	1.12	7.39	0.00	7.39	4.000	No	Yes	2.00
371	7.42	0.71	100.00	3.37	0.59	1.12	7.71	0.00	7.71	4.000	No	Yes	2.00
372	7.44	0.74	100.00	3.34	0.59	1.12	8.10	0.00	8.10	4.000	No	Yes	2.00
373	7.46	0.76	100.00	3.30	0.59	1.12	8.34	0.00	8.34	4.000	No	Yes	2.00
374	7.48	0.78	100.00	3.28	0.59	1.12	8.52	0.00	8.52	4.000	No	Yes	2.00
375	7.50	0.80	100.00	3.27	0.59	1.12	8.69	0.00	8.69	4.000	No	Yes	2.00
376	7.52	0.81	100.00	3.26	0.59	1.12	8.68	0.00	8.68	4.000	No	Yes	2.00
377	7.54	0.81	100.00	3.26	0.59	1.11	8.82	0.00	8.82	4.000	No	Yes	2.00
378	7.56	0.81	100.00	3.26	0.59	1.11	8.94	0.00	8.94	4.000	No	Yes	2.00
379	7.58	0.80	100.00	3.27	0.59	1.11	8.58	0.00	8.58	4.000	No	Yes	2.00
380	7.60	0.76	100.00	3.30	0.59	1.11	8.38	0.00	8.38	4.000	No	Yes	2.00
381	7.62	0.73	100.00	3.34	0.59	1.11	7.78	0.00	7.78	4.000	No	Yes	2.00
382	7.64	0.70	100.00	3.36	0.59	1.11	7.38	0.00	7.38	4.000	No	Yes	2.00
383	7.66	0.69	100.00	3.37	0.59	1.11	7.40	0.00	7.40	4.000	No	Yes	2.00
384	7.68	0.70	100.00	3.34	0.59	1.11	7.37	0.00	7.37	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
385	7.70	0.71	100.00	3.30	0.59	1.11	7.68	0.00	7.68	4.000	No	Yes	2.00
386	7.72	0.73	100.00	3.26	0.59	1.11	7.87	0.00	7.87	4.000	No	Yes	2.00
387	7.74	0.75	100.00	3.22	0.59	1.10	8.06	0.00	8.06	4.000	No	Yes	2.00
388	7.76	0.76	100.00	3.18	0.59	1.10	8.05	0.00	8.05	4.000	No	Yes	2.00
389	7.78	0.79	100.00	3.14	0.59	1.10	8.41	0.00	8.41	4.000	No	Yes	2.00
390	7.80	0.86	100.00	3.06	0.59	1.10	8.72	0.00	8.72	4.000	No	Yes	2.00
391	7.82	0.91	100.00	3.02	0.58	1.10	10.19	0.00	10.19	4.000	No	Yes	2.00
392	7.84	0.94	100.00	3.00	0.58	1.10	9.72	0.00	9.72	4.000	No	Yes	2.00
393	7.86	0.90	100.00	3.04	0.59	1.10	9.30	0.00	9.30	4.000	No	Yes	2.00
394	7.88	0.86	100.00	3.07	0.59	1.10	8.88	0.00	8.88	4.000	No	Yes	2.00
395	7.90	0.82	100.00	3.11	0.59	1.10	8.56	0.00	8.56	4.000	No	Yes	2.00
396	7.92	0.77	100.00	3.15	0.59	1.10	8.00	0.00	8.00	4.000	No	Yes	2.00
397	7.94	0.70	100.00	3.21	0.59	1.10	7.14	0.00	7.14	4.000	No	Yes	2.00
398	7.96	0.66	100.00	3.25	0.60	1.09	6.66	0.00	6.66	4.000	No	Yes	2.00
399	7.99	0.65	100.00	3.23	0.60	1.09	6.48	0.00	6.48	4.000	No	Yes	2.00
400	8.00	0.68	100.00	3.18	0.59	1.09	6.89	0.00	6.89	4.000	No	Yes	2.00
401	8.02	0.72	100.00	3.12	0.59	1.09	7.25	0.00	7.25	4.000	No	Yes	2.00
402	8.04	0.78	100.00	3.06	0.59	1.09	7.75	0.00	7.75	4.000	No	Yes	2.00
403	8.06	0.85	100.00	3.00	0.59	1.09	8.66	0.00	8.66	4.000	No	Yes	2.00
404	8.08	0.93	98.24	2.94	0.58	1.09	9.48	0.00	9.48	4.000	No	Yes	2.00
405	8.10	1.01	94.43	2.89	0.58	1.09	10.46	0.00	10.46	4.000	No	Yes	2.00
406	8.12	1.09	91.77	2.86	0.58	1.08	11.34	0.00	11.34	4.000	No	Yes	2.00
407	8.14	1.17	90.07	2.84	0.58	1.08	12.22	0.00	12.22	4.000	No	Yes	2.00
408	8.17	1.24	89.42	2.83	0.57	1.08	13.35	0.00	13.35	4.000	No	Yes	2.00
409	8.18	1.31	89.41	2.83	0.57	1.08	13.87	0.00	13.87	4.000	No	Yes	2.00
410	8.20	1.36	90.14	2.84	0.57	1.08	14.58	0.00	14.58	4.000	No	Yes	2.00
411	8.22	1.40	91.02	2.85	0.57	1.08	14.99	0.00	14.99	4.000	No	Yes	2.00
412	8.24	1.40	92.06	2.86	0.57	1.08	15.00	0.00	15.00	4.000	No	Yes	2.00
413	8.26	1.39	93.06	2.88	0.57	1.08	14.75	0.00	14.75	4.000	No	Yes	2.00
414	8.28	1.36	93.59	2.88	0.57	1.07	14.41	0.00	14.41	4.000	No	Yes	2.00
415	8.30	1.35	93.67	2.88	0.57	1.07	14.18	0.00	14.18	4.000	No	Yes	2.00
416	8.32	1.35	93.41	2.88	0.57	1.07	14.29	0.00	14.29	4.000	No	Yes	2.00
417	8.34	1.40	92.28	2.87	0.57	1.07	14.53	0.00	14.53	4.000	No	Yes	2.00
418	8.36	1.48	90.52	2.84	0.56	1.07	15.66	0.00	15.66	4.000	No	Yes	2.00
419	8.38	1.59	87.90	2.81	0.56	1.07	16.69	0.00	16.69	4.000	No	Yes	2.00
420	8.40	1.71	85.36	2.78	0.56	1.07	18.09	0.00	18.09	4.000	No	Yes	2.00
421	8.42	1.85	82.29	2.74	0.55	1.07	19.48	0.00	19.48	4.000	No	Yes	2.00
422	8.44	1.98	79.32	2.70	0.55	1.06	20.88	0.00	20.88	4.000	No	Yes	2.00
423	8.46	2.09	75.66	2.66	0.55	1.06	22.08	0.00	22.08	4.000	No	Yes	2.00
424	8.48	2.19	72.03	2.61	0.54	1.06	23.03	0.00	23.03	4.000	No	Yes	2.00
425	8.50	2.26	68.78	2.57	0.54	1.06	23.70	57.29	81.00	0.117	No	No	0.62
426	8.52	2.33	67.08	2.55	0.54	1.06	24.45	57.18	81.62	0.117	No	No	0.62
427	8.54	2.40	67.05	2.55	0.54	1.06	25.17	57.38	82.54	0.118	No	No	0.63
428	8.56	2.46	67.34	2.55	0.54	1.06	25.78	57.61	83.39	0.119	No	No	0.63
429	8.58	2.51	67.03	2.55	0.54	1.06	26.20	57.67	83.87	0.120	No	No	0.64
430	8.60	2.55	65.75	2.53	0.54	1.05	26.65	57.53	84.18	4.000	Yes	No	2.00
431	8.62	2.57	63.88	2.51	0.54	1.05	26.80	57.16	83.96	4.000	Yes	No	2.00
432	8.64	2.58	61.66	2.48	0.54	1.05	27.00	56.70	83.70	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
433	8.66	2.55	59.96	2.46	0.54	1.05	26.83	56.22	83.05	4.000	Yes	No	2.00
434	8.68	2.48	59.33	2.45	0.54	1.05	25.87	55.79	81.66	0.117	No	No	0.62
435	8.70	2.39	60.38	2.47	0.54	1.05	24.81	55.77	80.58	4.000	Yes	No	2.00
436	8.72	2.29	62.28	2.49	0.55	1.05	23.90	55.97	79.88	4.000	Yes	No	2.00
437	8.74	2.18	64.71	2.52	0.55	1.05	22.75	56.19	78.94	4.000	Yes	No	2.00
438	8.76	2.07	68.15	2.56	0.55	1.05	21.28	56.47	77.75	4.000	Yes	No	2.00
439	8.78	2.02	70.52	2.59	0.55	1.05	20.35	56.64	76.99	4.000	Yes	No	2.00
440	8.81	2.02	73.87	2.64	0.55	1.05	21.17	0.00	21.17	4.000	Yes	Yes	2.00
441	8.82	2.06	76.77	2.67	0.55	1.05	21.28	0.00	21.28	4.000	Yes	Yes	2.00
442	8.84	2.07	80.17	2.71	0.55	1.04	21.40	0.00	21.40	4.000	Yes	Yes	2.00
443	8.86	2.09	82.20	2.74	0.55	1.04	21.65	0.00	21.65	4.000	Yes	Yes	2.00
444	8.88	2.10	83.26	2.75	0.54	1.04	21.58	0.00	21.58	4.000	No	Yes	2.00
445	8.90	2.14	83.31	2.75	0.54	1.04	21.71	0.00	21.71	4.000	No	Yes	2.00
446	8.92	2.19	82.68	2.75	0.54	1.04	22.76	0.00	22.76	4.000	No	Yes	2.00
447	8.94	2.27	81.33	2.73	0.54	1.04	23.22	0.00	23.22	4.000	No	Yes	2.00
448	8.96	2.35	79.22	2.70	0.54	1.04	24.03	0.00	24.03	4.000	No	Yes	2.00
449	8.98	2.42	76.70	2.67	0.54	1.04	25.10	0.00	25.10	4.000	No	Yes	2.00
450	9.01	2.47	74.02	2.64	0.54	1.04	25.47	0.00	25.47	4.000	No	Yes	2.00
451	9.02	2.48	72.75	2.62	0.54	1.04	25.53	0.00	25.53	4.000	No	Yes	2.00
452	9.04	2.42	72.92	2.62	0.54	1.03	25.07	0.00	25.07	4.000	No	Yes	2.00
453	9.06	2.33	74.28	2.64	0.54	1.03	23.83	0.00	23.83	4.000	No	Yes	2.00
454	9.08	2.21	76.34	2.67	0.54	1.03	22.62	0.00	22.62	4.000	No	Yes	2.00
455	9.10	2.13	78.38	2.69	0.55	1.03	21.48	0.00	21.48	4.000	No	Yes	2.00
456	9.12	2.09	80.46	2.72	0.55	1.03	21.29	0.00	21.29	4.000	No	Yes	2.00
457	9.14	2.08	82.19	2.74	0.55	1.03	21.29	0.00	21.29	4.000	No	Yes	2.00
458	9.16	2.06	83.56	2.76	0.55	1.03	21.03	0.00	21.03	4.000	No	Yes	2.00
459	9.18	2.04	83.99	2.76	0.55	1.03	20.70	0.00	20.70	4.000	No	Yes	2.00
460	9.20	2.03	83.50	2.76	0.55	1.03	20.54	0.00	20.54	4.000	No	Yes	2.00
461	9.22	2.03	82.45	2.74	0.55	1.03	20.77	0.00	20.77	4.000	No	Yes	2.00
462	9.24	2.05	81.72	2.73	0.55	1.03	20.75	0.00	20.75	4.000	No	Yes	2.00
463	9.26	2.06	80.89	2.72	0.55	1.02	20.92	0.00	20.92	4.000	No	Yes	2.00
464	9.28	2.08	79.78	2.71	0.55	1.02	20.99	0.00	20.99	4.000	No	Yes	2.00
465	9.30	2.11	78.49	2.69	0.55	1.02	21.33	0.00	21.33	4.000	No	Yes	2.00
466	9.32	2.17	77.08	2.68	0.55	1.02	21.91	0.00	21.91	4.000	No	Yes	2.00
467	9.34	2.23	76.04	2.66	0.54	1.02	22.75	0.00	22.75	4.000	No	Yes	2.00
468	9.36	2.26	74.93	2.65	0.54	1.02	22.87	0.00	22.87	4.000	No	Yes	2.00
469	9.38	2.25	74.55	2.64	0.54	1.02	22.95	0.00	22.95	4.000	No	Yes	2.00
470	9.40	2.22	74.74	2.65	0.55	1.02	22.30	0.00	22.30	4.000	No	Yes	2.00
471	9.42	2.16	75.76	2.66	0.55	1.02	21.80	0.00	21.80	4.000	No	Yes	2.00
472	9.44	2.10	76.80	2.67	0.55	1.02	21.04	0.00	21.04	4.000	No	Yes	2.00
473	9.46	2.04	77.95	2.69	0.55	1.02	20.53	0.00	20.53	4.000	No	Yes	2.00
474	9.48	2.02	79.13	2.70	0.55	1.02	20.08	0.00	20.08	4.000	No	Yes	2.00
475	9.50	2.03	80.67	2.72	0.55	1.01	20.28	0.00	20.28	4.000	No	Yes	2.00
476	9.52	2.06	81.17	2.73	0.55	1.01	20.70	0.00	20.70	4.000	No	Yes	2.00
477	9.54	2.09	81.43	2.73	0.55	1.01	21.13	0.00	21.13	4.000	No	Yes	2.00
478	9.56	2.07	81.44	2.73	0.55	1.01	20.90	0.00	20.90	4.000	No	Yes	2.00
479	9.58	2.01	82.07	2.74	0.55	1.01	20.23	0.00	20.23	4.000	No	Yes	2.00
480	9.60	1.92	82.77	2.75	0.55	1.01	19.20	0.00	19.20	4.000	No	Yes	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
481	9.62	1.81	83.69	2.76	0.56	1.01	18.11	0.00	18.11	4.000	No	Yes	2.00
482	9.64	1.71	85.19	2.78	0.56	1.01	16.91	0.00	16.91	4.000	No	Yes	2.00
483	9.66	1.65	87.50	2.81	0.56	1.01	16.35	0.00	16.35	4.000	No	Yes	2.00
484	9.68	1.63	90.47	2.84	0.56	1.01	16.32	0.00	16.32	4.000	No	Yes	2.00
485	9.70	1.63	92.65	2.87	0.56	1.01	16.19	0.00	16.19	4.000	No	Yes	2.00
486	9.72	1.65	93.38	2.88	0.56	1.00	16.26	0.00	16.26	4.000	No	Yes	2.00
487	9.74	1.70	92.07	2.86	0.56	1.00	16.85	0.00	16.85	4.000	No	Yes	2.00
488	9.76	1.77	88.19	2.81	0.56	1.00	17.64	0.00	17.64	4.000	No	Yes	2.00
489	9.78	1.83	84.40	2.77	0.56	1.00	18.17	0.00	18.17	4.000	No	Yes	2.00
490	9.80	1.86	81.14	2.73	0.56	1.00	18.62	0.00	18.62	4.000	No	Yes	2.00
491	9.82	1.87	80.20	2.72	0.56	1.00	18.43	0.00	18.43	4.000	No	Yes	2.00
492	9.84	1.86	79.34	2.70	0.56	1.00	18.42	0.00	18.42	4.000	No	Yes	2.00
493	9.86	1.85	78.70	2.70	0.56	1.00	18.32	0.00	18.32	4.000	No	Yes	2.00
494	9.88	1.86	78.39	2.69	0.56	1.00	18.37	0.00	18.37	4.000	No	Yes	2.00
495	9.90	1.88	78.37	2.69	0.56	1.00	18.60	0.00	18.60	4.000	No	Yes	2.00
496	9.92	1.93	77.66	2.68	0.56	1.00	18.90	0.00	18.90	4.000	No	Yes	2.00
497	9.94	2.01	76.24	2.67	0.55	1.00	19.81	0.00	19.81	4.000	Yes	Yes	2.00
498	9.96	2.12	73.51	2.63	0.55	0.99	20.76	0.00	20.76	4.000	Yes	Yes	2.00
499	9.98	2.24	70.40	2.59	0.55	0.99	22.05	57.11	79.16	4.000	Yes	No	2.00
500	10.00	2.36	67.23	2.55	0.55	0.99	23.41	56.91	80.32	4.000	Yes	No	2.00
501	10.02	2.47	64.24	2.52	0.54	0.99	24.17	56.49	80.66	4.000	Yes	No	2.00
502	10.04	2.54	61.51	2.48	0.54	0.99	25.13	56.14	81.26	4.000	Yes	No	2.00
503	10.06	2.58	59.28	2.45	0.54	0.99	25.46	55.67	81.13	4.000	Yes	No	2.00
504	10.08	2.55	58.38	2.44	0.54	0.99	25.37	55.40	80.77	0.117	No	No	0.62
505	10.11	2.49	58.65	2.45	0.55	0.99	24.13	55.13	79.26	0.115	No	No	0.61
506	10.12	2.43	59.21	2.45	0.55	0.99	23.54	55.11	78.65	0.115	No	No	0.60
507	10.14	2.42	60.24	2.47	0.55	0.99	23.78	55.44	79.22	0.115	No	No	0.61
508	10.16	2.45	61.58	2.48	0.55	0.99	23.81	55.78	79.59	0.116	No	No	0.61
509	10.18	2.49	62.59	2.49	0.54	0.99	24.30	56.16	80.46	0.116	No	No	0.61
510	10.20	2.54	62.67	2.50	0.54	0.99	24.91	56.35	81.26	0.117	No	No	0.62
511	10.22	2.57	62.47	2.49	0.54	0.98	25.22	56.39	81.61	0.117	No	No	0.62
512	10.24	2.56	63.45	2.51	0.54	0.98	25.10	56.58	81.69	4.000	Yes	No	2.00
513	10.26	2.49	65.65	2.53	0.54	0.98	24.39	56.86	81.25	4.000	Yes	No	2.00
514	10.28	2.36	68.20	2.57	0.55	0.98	23.12	57.01	80.13	4.000	Yes	No	2.00
515	10.30	2.23	70.27	2.59	0.55	0.98	21.39	56.90	78.28	4.000	Yes	No	2.00
516	10.32	2.13	73.19	2.63	0.55	0.98	20.68	0.00	20.68	4.000	Yes	Yes	2.00
517	10.34	2.07	78.43	2.69	0.55	0.98	19.97	0.00	19.97	4.000	Yes	Yes	2.00
518	10.36	2.06	83.03	2.75	0.55	0.98	19.54	0.00	19.54	4.000	Yes	Yes	2.00
519	10.38	2.11	85.03	2.78	0.55	0.98	20.35	0.00	20.35	4.000	Yes	Yes	2.00
520	10.40	2.21	83.88	2.76	0.55	0.98	21.42	0.00	21.42	4.000	Yes	Yes	2.00
521	10.42	2.32	81.67	2.73	0.54	0.98	22.57	0.00	22.57	4.000	Yes	Yes	2.00
522	10.44	2.41	79.70	2.71	0.54	0.98	23.50	0.00	23.50	4.000	Yes	Yes	2.00
523	10.46	2.45	77.52	2.68	0.54	0.98	23.71	0.00	23.71	4.000	Yes	Yes	2.00
524	10.48	2.46	75.37	2.65	0.54	0.97	23.78	0.00	23.78	4.000	Yes	Yes	2.00
525	10.50	2.48	71.81	2.61	0.54	0.97	23.85	0.00	23.85	4.000	Yes	Yes	2.00
526	10.52	2.51	68.17	2.56	0.54	0.97	24.26	57.34	81.60	4.000	Yes	No	2.00
527	10.54	2.51	65.46	2.53	0.54	0.97	24.38	56.82	81.20	4.000	Yes	No	2.00
528	10.56	2.47	64.99	2.52	0.54	0.97	23.90	56.58	80.48	0.116	No	No	0.62

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
529	10.58	2.38	65.68	2.53	0.55	0.97	22.91	56.45	79.36	0.115	No	No	0.61
530	10.60	2.29	65.95	2.54	0.55	0.97	21.79	56.18	77.97	0.114	No	No	0.60
531	10.62	2.24	65.13	2.53	0.55	0.97	21.29	55.87	77.16	0.113	No	No	0.60
532	10.64	2.26	64.37	2.52	0.55	0.97	21.48	55.76	77.24	0.113	No	No	0.60
533	10.66	2.35	64.82	2.52	0.55	0.97	22.17	56.05	78.22	0.114	No	No	0.60
534	10.68	2.47	65.54	2.53	0.54	0.97	23.82	56.68	80.50	0.116	No	No	0.62
535	10.70	2.64	65.16	2.53	0.54	0.97	25.09	56.96	82.04	0.118	No	No	0.62
536	10.72	2.75	64.57	2.52	0.54	0.97	26.94	57.36	84.30	0.120	No	No	0.64
537	10.74	2.76	64.35	2.52	0.54	0.97	26.78	57.26	84.04	0.120	No	No	0.64
538	10.76	2.65	63.65	2.51	0.54	0.96	25.41	56.72	82.13	0.118	No	No	0.63
539	10.78	2.53	61.49	2.48	0.55	0.96	23.59	55.70	79.29	0.115	No	No	0.61
540	10.80	2.47	58.77	2.45	0.55	0.96	23.53	54.99	78.52	0.115	No	No	0.60
541	10.82	2.43	59.27	2.45	0.55	0.96	23.60	55.14	78.75	4.000	Yes	No	2.00
542	10.84	2.31	64.10	2.51	0.55	0.96	22.41	55.96	78.37	4.000	Yes	No	2.00
543	10.86	2.11	71.87	2.61	0.55	0.96	20.01	0.00	20.01	4.000	Yes	Yes	2.00
544	10.88	1.86	81.13	2.73	0.56	0.96	17.68	0.00	17.68	4.000	Yes	Yes	2.00
545	10.91	1.63	89.05	2.83	0.56	0.96	15.42	0.00	15.42	4.000	Yes	Yes	2.00
546	10.92	1.47	94.73	2.90	0.57	0.96	13.41	0.00	13.41	4.000	Yes	Yes	2.00
547	10.94	1.40	96.69	2.92	0.57	0.96	13.01	0.00	13.01	4.000	Yes	Yes	2.00
548	10.96	1.53	93.27	2.88	0.57	0.96	13.60	0.00	13.60	4.000	Yes	Yes	2.00
549	10.98	1.73	88.14	2.81	0.56	0.96	16.77	0.00	16.77	4.000	Yes	Yes	2.00
550	11.00	1.95	83.95	2.76	0.55	0.96	18.78	0.00	18.78	4.000	Yes	Yes	2.00
551	11.02	2.09	80.82	2.72	0.55	0.95	19.74	0.00	19.74	4.000	Yes	Yes	2.00
552	11.04	2.20	77.27	2.68	0.55	0.95	20.83	0.00	20.83	4.000	Yes	Yes	2.00
553	11.06	2.32	73.05	2.63	0.55	0.95	21.87	0.00	21.87	4.000	Yes	Yes	2.00
554	11.08	2.44	69.42	2.58	0.55	0.95	22.86	57.17	80.03	4.000	Yes	No	2.00
555	11.10	2.63	64.66	2.52	0.54	0.95	24.40	56.65	81.05	4.000	Yes	No	2.00
556	11.12	2.80	60.90	2.47	0.54	0.95	27.03	56.52	83.55	4.000	Yes	No	2.00
557	11.14	2.89	58.31	2.44	0.54	0.95	27.59	56.00	83.59	4.000	Yes	No	2.00
558	11.16	2.84	59.08	2.45	0.54	0.95	26.92	56.02	82.94	0.119	No	No	0.63
559	11.18	2.75	59.67	2.46	0.54	0.95	25.75	55.85	81.60	0.117	No	No	0.62
560	11.21	2.66	59.86	2.46	0.55	0.95	24.82	55.64	80.46	0.116	No	No	0.62
561	11.22	2.62	59.51	2.46	0.55	0.95	24.34	55.41	79.75	0.116	No	No	0.61
562	11.24	2.64	59.44	2.46	0.55	0.95	24.52	55.44	79.97	0.116	No	No	0.61
563	11.26	2.70	59.67	2.46	0.54	0.95	25.47	55.77	81.24	0.117	No	No	0.62
564	11.28	2.73	58.62	2.45	0.54	0.95	25.79	55.58	81.37	0.117	No	No	0.62
565	11.30	2.71	57.82	2.44	0.54	0.95	25.57	55.30	80.87	0.117	No	No	0.62
566	11.32	2.64	57.23	2.43	0.55	0.94	24.76	54.91	79.68	4.000	Yes	No	2.00
567	11.34	2.51	59.20	2.45	0.55	0.94	23.85	55.20	79.05	4.000	Yes	No	2.00
568	11.36	2.28	64.65	2.52	0.55	0.94	21.79	55.91	77.69	4.000	Yes	No	2.00
569	11.38	1.95	74.50	2.64	0.56	0.94	18.22	0.00	18.22	4.000	Yes	Yes	2.00
570	11.40	1.62	87.04	2.80	0.57	0.94	14.66	0.00	14.66	4.000	Yes	Yes	2.00
571	11.42	1.43	95.28	2.90	0.57	0.94	12.40	0.00	12.40	4.000	Yes	Yes	2.00
572	11.44	1.43	96.25	2.92	0.57	0.94	12.85	0.00	12.85	4.000	Yes	Yes	2.00
573	11.46	1.63	88.77	2.82	0.57	0.94	14.46	0.00	14.46	4.000	Yes	Yes	2.00
574	11.48	1.96	79.91	2.71	0.56	0.94	17.95	0.00	17.95	4.000	Yes	Yes	2.00
575	11.50	2.32	72.34	2.62	0.55	0.94	21.84	0.00	21.84	4.000	Yes	Yes	2.00
576	11.52	2.65	66.24	2.54	0.54	0.94	24.54	57.03	81.57	4.000	Yes	No	2.00

:: Cyclic Resistance Ratio (CRR) calculation data :: (continued)

Point ID	Depth (m)	q_t (MPa)	FC (%)	Ic	m	C_N	q_{c1N}	Δq_{c1N}	$q_{c1N,cs}$	$CRR_{7.5}$	Belongs to trans. layer	Clay-like behaviour	FS
577	11.54	2.90	60.71	2.47	0.54	0.94	27.03	56.47	83.50	4.000	Yes	No	2.00
578	11.56	3.11	55.16	2.40	0.54	0.94	28.80	55.41	84.21	4.000	Yes	No	2.00
579	11.58	3.24	51.21	2.35	0.53	0.94	30.35	54.50	84.85	4.000	Yes	No	2.00
580	11.60	3.26	48.56	2.32	0.54	0.94	30.43	53.50	83.93	4.000	Yes	No	2.00
581	11.62	3.18	47.39	2.30	0.54	0.94	29.49	52.77	82.26	0.118	No	No	0.63
582	11.64	3.06	46.18	2.29	0.55	0.93	28.09	51.88	79.96	0.116	No	No	0.62
583	11.66	2.97	45.56	2.28	0.55	0.93	26.96	51.31	78.26	0.114	No	No	0.61
584	11.68	2.91	42.08	2.24	0.56	0.93	26.70	49.53	76.23	0.113	No	No	0.60

Abbreviations

Depth: Depth from free surface, at which CPT was performed (m)
q_t: Total cone resistance
FC: Fines content (%)
I_c: Soil behavior type index
m: Stress exponent
C_N: Overburden correction factor
q_{c1N}: Normalized and adjusted cone resistance
Δq_{c1N}: Cone resistance correction factor due to fines
$q_{c1N,cs}$: Normalized and adjusted cone resistance
$CRR_{7.5}$: Cyclic resistance ratio for M_w=7.5
FS: Factor of safety against soil liquefaction

:: Liquefaction Potential Index calculation data ::

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
0.02	2.00	0.00	9.99	0.02	0.00	0.04	2.00	0.00	9.98	0.02	0.00
0.06	2.00	0.00	9.97	0.02	0.00	0.08	2.00	0.00	9.96	0.02	0.00
0.10	2.00	0.00	9.95	0.02	0.00	0.12	2.00	0.00	9.94	0.02	0.00
0.14	2.00	0.00	9.93	0.02	0.00	0.16	2.00	0.00	9.92	0.02	0.00
0.18	2.00	0.00	9.91	0.02	0.00	0.20	2.00	0.00	9.90	0.02	0.00
0.22	2.00	0.00	9.89	0.02	0.00	0.24	2.00	0.00	9.88	0.02	0.00
0.26	2.00	0.00	9.87	0.02	0.00	0.28	2.00	0.00	9.86	0.02	0.00
0.30	2.00	0.00	9.85	0.02	0.00	0.32	2.00	0.00	9.84	0.02	0.00
0.34	2.00	0.00	9.83	0.02	0.00	0.36	2.00	0.00	9.82	0.02	0.00
0.38	2.00	0.00	9.81	0.02	0.00	0.40	2.00	0.00	9.80	0.02	0.00
0.42	2.00	0.00	9.79	0.02	0.00	0.45	2.00	0.00	9.78	0.03	0.00
0.46	2.00	0.00	9.77	0.01	0.00	0.48	2.00	0.00	9.76	0.02	0.00
0.50	2.00	0.00	9.75	0.02	0.00	0.52	2.00	0.00	9.74	0.02	0.00
0.54	2.00	0.00	9.73	0.02	0.00	0.56	2.00	0.00	9.72	0.02	0.00
0.58	2.00	0.00	9.71	0.02	0.00	0.60	2.00	0.00	9.70	0.02	0.00
0.62	2.00	0.00	9.69	0.02	0.00	0.64	2.00	0.00	9.68	0.02	0.00
0.66	2.00	0.00	9.67	0.02	0.00	0.68	2.00	0.00	9.66	0.02	0.00
0.70	2.00	0.00	9.65	0.02	0.00	0.72	2.00	0.00	9.64	0.02	0.00
0.74	2.00	0.00	9.63	0.02	0.00	0.76	2.00	0.00	9.62	0.02	0.00
0.78	2.00	0.00	9.61	0.02	0.00	0.80	2.00	0.00	9.60	0.02	0.00
0.82	2.00	0.00	9.59	0.02	0.00	0.84	2.00	0.00	9.58	0.02	0.00
0.86	2.00	0.00	9.57	0.02	0.00	0.88	2.00	0.00	9.56	0.02	0.00
0.90	2.00	0.00	9.55	0.02	0.00	0.92	2.00	0.00	9.54	0.02	0.00
0.94	2.00	0.00	9.53	0.02	0.00	0.96	2.00	0.00	9.52	0.02	0.00
0.98	2.00	0.00	9.51	0.02	0.00	1.00	2.00	0.00	9.50	0.02	0.00
1.02	2.00	0.00	9.49	0.02	0.00	1.05	2.00	0.00	9.48	0.03	0.00
1.06	2.00	0.00	9.47	0.01	0.00	1.08	2.00	0.00	9.46	0.02	0.00
1.11	2.00	0.00	9.45	0.03	0.00	1.12	2.00	0.00	9.44	0.01	0.00
1.14	2.00	0.00	9.43	0.02	0.00	1.17	2.00	0.00	9.41	0.03	0.00
1.18	2.00	0.00	9.41	0.01	0.00	1.20	2.00	0.00	9.40	0.02	0.00
1.22	2.00	0.00	9.39	0.02	0.00	1.24	2.00	0.00	9.38	0.02	0.00
1.26	2.00	0.00	9.37	0.02	0.00	1.28	2.00	0.00	9.36	0.02	0.00
1.30	2.00	0.00	9.35	0.02	0.00	1.32	2.00	0.00	9.34	0.02	0.00
1.34	2.00	0.00	9.33	0.02	0.00	1.36	2.00	0.00	9.32	0.02	0.00
1.38	2.00	0.00	9.31	0.02	0.00	1.40	2.00	0.00	9.30	0.02	0.00
1.42	2.00	0.00	9.29	0.02	0.00	1.44	2.00	0.00	9.28	0.02	0.00
1.46	2.00	0.00	9.27	0.02	0.00	1.48	2.00	0.00	9.26	0.02	0.00
1.50	2.00	0.00	9.25	0.02	0.00	1.52	2.00	0.00	9.24	0.02	0.00
1.54	2.00	0.00	9.23	0.02	0.00	1.56	2.00	0.00	9.22	0.02	0.00
1.58	2.00	0.00	9.21	0.02	0.00	1.60	2.00	0.00	9.20	0.02	0.00
1.62	2.00	0.00	9.19	0.02	0.00	1.64	2.00	0.00	9.18	0.02	0.00
1.66	2.00	0.00	9.17	0.02	0.00	1.68	2.00	0.00	9.16	0.02	0.00
1.70	2.00	0.00	9.15	0.02	0.00	1.72	2.00	0.00	9.14	0.02	0.00
1.74	2.00	0.00	9.13	0.02	0.00	1.76	2.00	0.00	9.12	0.02	0.00
1.78	2.00	0.00	9.11	0.02	0.00	1.80	2.00	0.00	9.10	0.02	0.00
1.82	2.00	0.00	9.09	0.02	0.00	1.84	2.00	0.00	9.08	0.02	0.00
1.86	2.00	0.00	9.07	0.02	0.00	1.88	2.00	0.00	9.06	0.02	0.00
1.90	2.00	0.00	9.05	0.02	0.00	1.92	2.00	0.00	9.04	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
1.94	2.00	0.00	9.03	0.02	0.00	1.96	2.00	0.00	9.02	0.02	0.00
1.98	2.00	0.00	9.01	0.02	0.00	2.00	2.00	0.00	9.00	0.02	0.00
2.02	2.00	0.00	8.99	0.02	0.00	2.04	2.00	0.00	8.98	0.02	0.00
2.06	2.00	0.00	8.97	0.02	0.00	2.08	2.00	0.00	8.96	0.02	0.00
2.10	2.00	0.00	8.95	0.02	0.00	2.12	2.00	0.00	8.94	0.02	0.00
2.15	2.00	0.00	8.93	0.03	0.00	2.16	2.00	0.00	8.92	0.01	0.00
2.18	2.00	0.00	8.91	0.02	0.00	2.20	2.00	0.00	8.90	0.02	0.00
2.22	2.00	0.00	8.89	0.02	0.00	2.24	2.00	0.00	8.88	0.02	0.00
2.26	2.00	0.00	8.87	0.02	0.00	2.28	2.00	0.00	8.86	0.02	0.00
2.30	2.00	0.00	8.85	0.02	0.00	2.32	2.00	0.00	8.84	0.02	0.00
2.34	2.00	0.00	8.83	0.02	0.00	2.36	2.00	0.00	8.82	0.02	0.00
2.38	2.00	0.00	8.81	0.02	0.00	2.40	2.00	0.00	8.80	0.02	0.00
2.42	2.00	0.00	8.79	0.02	0.00	2.44	2.00	0.00	8.78	0.02	0.00
2.46	2.00	0.00	8.77	0.02	0.00	2.48	2.00	0.00	8.76	0.02	0.00
2.50	2.00	0.00	8.75	0.02	0.00	2.52	2.00	0.00	8.74	0.02	0.00
2.54	2.00	0.00	8.73	0.02	0.00	2.56	2.00	0.00	8.72	0.02	0.00
2.58	2.00	0.00	8.71	0.02	0.00	2.60	2.00	0.00	8.70	0.02	0.00
2.62	2.00	0.00	8.69	0.02	0.00	2.64	2.00	0.00	8.68	0.02	0.00
2.66	2.00	0.00	8.67	0.02	0.00	2.68	2.00	0.00	8.66	0.02	0.00
2.70	2.00	0.00	8.65	0.02	0.00	2.72	2.00	0.00	8.64	0.02	0.00
2.74	2.00	0.00	8.63	0.02	0.00	2.76	2.00	0.00	8.62	0.02	0.00
2.78	2.00	0.00	8.61	0.02	0.00	2.80	2.00	0.00	8.60	0.02	0.00
2.82	2.00	0.00	8.59	0.02	0.00	2.84	2.00	0.00	8.58	0.02	0.00
2.86	2.00	0.00	8.57	0.02	0.00	2.88	2.00	0.00	8.56	0.02	0.00
2.90	2.00	0.00	8.55	0.02	0.00	2.92	2.00	0.00	8.54	0.02	0.00
2.94	2.00	0.00	8.53	0.02	0.00	2.96	2.00	0.00	8.52	0.02	0.00
2.98	2.00	0.00	8.51	0.02	0.00	3.00	2.00	0.00	8.50	0.02	0.00
3.02	2.00	0.00	8.49	0.02	0.00	3.04	2.00	0.00	8.48	0.02	0.00
3.06	2.00	0.00	8.47	0.02	0.00	3.09	2.00	0.00	8.46	0.03	0.00
3.10	2.00	0.00	8.45	0.01	0.00	3.12	2.00	0.00	8.44	0.02	0.00
3.15	2.00	0.00	8.43	0.03	0.00	3.16	2.00	0.00	8.42	0.01	0.00
3.18	2.00	0.00	8.41	0.02	0.00	3.20	2.00	0.00	8.40	0.02	0.00
3.22	2.00	0.00	8.39	0.02	0.00	3.24	2.00	0.00	8.38	0.02	0.00
3.26	2.00	0.00	8.37	0.02	0.00	3.28	2.00	0.00	8.36	0.02	0.00
3.30	2.00	0.00	8.35	0.02	0.00	3.32	2.00	0.00	8.34	0.02	0.00
3.34	2.00	0.00	8.33	0.02	0.00	3.36	2.00	0.00	8.32	0.02	0.00
3.38	2.00	0.00	8.31	0.02	0.00	3.40	2.00	0.00	8.30	0.02	0.00
3.42	2.00	0.00	8.29	0.02	0.00	3.44	2.00	0.00	8.28	0.02	0.00
3.46	2.00	0.00	8.27	0.02	0.00	3.48	2.00	0.00	8.26	0.02	0.00
3.50	2.00	0.00	8.25	0.02	0.00	3.52	2.00	0.00	8.24	0.02	0.00
3.54	2.00	0.00	8.23	0.02	0.00	3.56	2.00	0.00	8.22	0.02	0.00
3.58	2.00	0.00	8.21	0.02	0.00	3.60	2.00	0.00	8.20	0.02	0.00
3.62	2.00	0.00	8.19	0.02	0.00	3.64	2.00	0.00	8.18	0.02	0.00
3.66	2.00	0.00	8.17	0.02	0.00	3.68	2.00	0.00	8.16	0.02	0.00
3.70	2.00	0.00	8.15	0.02	0.00	3.72	2.00	0.00	8.14	0.02	0.00
3.74	2.00	0.00	8.13	0.02	0.00	3.76	2.00	0.00	8.12	0.02	0.00
3.78	2.00	0.00	8.11	0.02	0.00	3.80	2.00	0.00	8.10	0.02	0.00
3.82	2.00	0.00	8.09	0.02	0.00	3.84	2.00	0.00	8.08	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
3.86	2.00	0.00	8.07	0.02	0.00	3.88	2.00	0.00	8.06	0.02	0.00
3.90	2.00	0.00	8.05	0.02	0.00	3.92	2.00	0.00	8.04	0.02	0.00
3.94	2.00	0.00	8.03	0.02	0.00	3.96	2.00	0.00	8.02	0.02	0.00
3.98	2.00	0.00	8.01	0.02	0.00	4.00	2.00	0.00	8.00	0.02	0.00
4.02	2.00	0.00	7.99	0.02	0.00	4.05	2.00	0.00	7.98	0.03	0.00
4.06	2.00	0.00	7.97	0.01	0.00	4.08	2.00	0.00	7.96	0.02	0.00
4.10	2.00	0.00	7.95	0.02	0.00	4.12	2.00	0.00	7.94	0.02	0.00
4.14	2.00	0.00	7.93	0.02	0.00	4.16	2.00	0.00	7.92	0.02	0.00
4.18	2.00	0.00	7.91	0.02	0.00	4.20	2.00	0.00	7.90	0.02	0.00
4.22	2.00	0.00	7.89	0.02	0.00	4.24	2.00	0.00	7.88	0.02	0.00
4.26	0.73	0.27	7.87	0.02	0.04	4.28	0.74	0.26	7.86	0.02	0.04
4.30	0.75	0.25	7.85	0.02	0.04	4.32	0.74	0.26	7.84	0.02	0.04
4.34	0.74	0.26	7.83	0.02	0.04	4.36	0.76	0.24	7.82	0.02	0.04
4.38	0.76	0.24	7.81	0.02	0.04	4.40	2.00	0.00	7.80	0.02	0.00
4.42	2.00	0.00	7.79	0.02	0.00	4.44	2.00	0.00	7.78	0.02	0.00
4.46	2.00	0.00	7.77	0.02	0.00	4.49	2.00	0.00	7.76	0.03	0.00
4.50	2.00	0.00	7.75	0.01	0.00	4.52	2.00	0.00	7.74	0.02	0.00
4.54	2.00	0.00	7.73	0.02	0.00	4.56	2.00	0.00	7.72	0.02	0.00
4.58	2.00	0.00	7.71	0.02	0.00	4.60	2.00	0.00	7.70	0.02	0.00
4.62	2.00	0.00	7.69	0.02	0.00	4.64	2.00	0.00	7.68	0.02	0.00
4.66	2.00	0.00	7.67	0.02	0.00	4.68	2.00	0.00	7.66	0.02	0.00
4.70	2.00	0.00	7.65	0.02	0.00	4.72	2.00	0.00	7.64	0.02	0.00
4.74	2.00	0.00	7.63	0.02	0.00	4.76	2.00	0.00	7.62	0.02	0.00
4.78	2.00	0.00	7.61	0.02	0.00	4.80	2.00	0.00	7.60	0.02	0.00
4.82	2.00	0.00	7.59	0.02	0.00	4.84	2.00	0.00	7.58	0.02	0.00
4.86	2.00	0.00	7.57	0.02	0.00	4.88	2.00	0.00	7.56	0.02	0.00
4.90	2.00	0.00	7.55	0.02	0.00	4.92	2.00	0.00	7.54	0.02	0.00
4.94	2.00	0.00	7.53	0.02	0.00	4.96	2.00	0.00	7.52	0.02	0.00
4.98	2.00	0.00	7.51	0.02	0.00	5.00	2.00	0.00	7.50	0.02	0.00
5.02	2.00	0.00	7.49	0.02	0.00	5.04	2.00	0.00	7.48	0.02	0.00
5.06	2.00	0.00	7.47	0.02	0.00	5.08	2.00	0.00	7.46	0.02	0.00
5.10	2.00	0.00	7.45	0.02	0.00	5.12	2.00	0.00	7.44	0.02	0.00
5.14	2.00	0.00	7.43	0.02	0.00	5.16	2.00	0.00	7.42	0.02	0.00
5.18	2.00	0.00	7.41	0.02	0.00	5.20	2.00	0.00	7.40	0.02	0.00
5.22	2.00	0.00	7.39	0.02	0.00	5.24	2.00	0.00	7.38	0.02	0.00
5.26	2.00	0.00	7.37	0.02	0.00	5.28	2.00	0.00	7.36	0.02	0.00
5.30	2.00	0.00	7.35	0.02	0.00	5.32	2.00	0.00	7.34	0.02	0.00
5.34	2.00	0.00	7.33	0.02	0.00	5.36	2.00	0.00	7.32	0.02	0.00
5.38	2.00	0.00	7.31	0.02	0.00	5.40	2.00	0.00	7.30	0.02	0.00
5.42	2.00	0.00	7.29	0.02	0.00	5.44	2.00	0.00	7.28	0.02	0.00
5.46	2.00	0.00	7.27	0.02	0.00	5.48	2.00	0.00	7.26	0.02	0.00
5.50	2.00	0.00	7.25	0.02	0.00	5.52	2.00	0.00	7.24	0.02	0.00
5.54	2.00	0.00	7.23	0.02	0.00	5.56	2.00	0.00	7.22	0.02	0.00
5.58	2.00	0.00	7.21	0.02	0.00	5.60	2.00	0.00	7.20	0.02	0.00
5.62	2.00	0.00	7.19	0.02	0.00	5.64	2.00	0.00	7.18	0.02	0.00
5.66	2.00	0.00	7.17	0.02	0.00	5.68	2.00	0.00	7.16	0.02	0.00
5.70	2.00	0.00	7.15	0.02	0.00	5.72	2.00	0.00	7.14	0.02	0.00
5.74	2.00	0.00	7.13	0.02	0.00	5.76	2.00	0.00	7.12	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
5.78	2.00	0.00	7.11	0.02	0.00	5.80	2.00	0.00	7.10	0.02	0.00
5.82	2.00	0.00	7.09	0.02	0.00	5.84	2.00	0.00	7.08	0.02	0.00
5.87	2.00	0.00	7.07	0.03	0.00	5.88	2.00	0.00	7.06	0.01	0.00
5.90	2.00	0.00	7.05	0.02	0.00	5.92	2.00	0.00	7.04	0.02	0.00
5.94	2.00	0.00	7.03	0.02	0.00	5.96	2.00	0.00	7.02	0.02	0.00
5.99	2.00	0.00	7.01	0.03	0.00	6.00	2.00	0.00	7.00	0.01	0.00
6.02	2.00	0.00	6.99	0.02	0.00	6.04	2.00	0.00	6.98	0.02	0.00
6.06	2.00	0.00	6.97	0.02	0.00	6.08	2.00	0.00	6.96	0.02	0.00
6.10	2.00	0.00	6.95	0.02	0.00	6.12	2.00	0.00	6.94	0.02	0.00
6.14	2.00	0.00	6.93	0.02	0.00	6.16	2.00	0.00	6.92	0.02	0.00
6.18	2.00	0.00	6.91	0.02	0.00	6.20	2.00	0.00	6.90	0.02	0.00
6.22	2.00	0.00	6.89	0.02	0.00	6.24	2.00	0.00	6.88	0.02	0.00
6.26	2.00	0.00	6.87	0.02	0.00	6.28	2.00	0.00	6.86	0.02	0.00
6.30	2.00	0.00	6.85	0.02	0.00	6.32	2.00	0.00	6.84	0.02	0.00
6.34	2.00	0.00	6.83	0.02	0.00	6.36	2.00	0.00	6.82	0.02	0.00
6.38	2.00	0.00	6.81	0.02	0.00	6.40	0.64	0.36	6.80	0.02	0.05
6.42	0.65	0.35	6.79	0.02	0.05	6.44	0.65	0.35	6.78	0.02	0.05
6.46	0.65	0.35	6.77	0.02	0.05	6.48	0.65	0.35	6.76	0.02	0.05
6.50	0.65	0.35	6.75	0.02	0.05	6.52	0.65	0.35	6.74	0.02	0.05
6.54	0.65	0.35	6.73	0.02	0.05	6.56	0.65	0.35	6.72	0.02	0.05
6.58	0.65	0.35	6.71	0.02	0.05	6.60	0.65	0.35	6.70	0.02	0.05
6.62	0.65	0.35	6.69	0.02	0.05	6.64	0.65	0.35	6.68	0.02	0.05
6.66	0.65	0.35	6.67	0.02	0.05	6.68	2.00	0.00	6.66	0.02	0.00
6.70	2.00	0.00	6.65	0.02	0.00	6.72	2.00	0.00	6.64	0.02	0.00
6.74	2.00	0.00	6.63	0.02	0.00	6.76	2.00	0.00	6.62	0.02	0.00
6.78	2.00	0.00	6.61	0.02	0.00	6.80	2.00	0.00	6.60	0.02	0.00
6.82	2.00	0.00	6.59	0.02	0.00	6.85	2.00	0.00	6.58	0.03	0.00
6.86	2.00	0.00	6.57	0.01	0.00	6.88	2.00	0.00	6.56	0.02	0.00
6.90	2.00	0.00	6.55	0.02	0.00	6.92	2.00	0.00	6.54	0.02	0.00
6.94	2.00	0.00	6.53	0.02	0.00	6.96	2.00	0.00	6.52	0.02	0.00
6.98	2.00	0.00	6.51	0.02	0.00	7.00	2.00	0.00	6.50	0.02	0.00
7.02	2.00	0.00	6.49	0.02	0.00	7.04	2.00	0.00	6.48	0.02	0.00
7.06	2.00	0.00	6.47	0.02	0.00	7.08	2.00	0.00	6.46	0.02	0.00
7.10	2.00	0.00	6.45	0.02	0.00	7.12	2.00	0.00	6.44	0.02	0.00
7.14	2.00	0.00	6.43	0.02	0.00	7.16	2.00	0.00	6.42	0.02	0.00
7.18	2.00	0.00	6.41	0.02	0.00	7.20	2.00	0.00	6.40	0.02	0.00
7.22	2.00	0.00	6.39	0.02	0.00	7.24	2.00	0.00	6.38	0.02	0.00
7.26	2.00	0.00	6.37	0.02	0.00	7.28	2.00	0.00	6.36	0.02	0.00
7.30	2.00	0.00	6.35	0.02	0.00	7.32	2.00	0.00	6.34	0.02	0.00
7.34	2.00	0.00	6.33	0.02	0.00	7.36	2.00	0.00	6.32	0.02	0.00
7.38	2.00	0.00	6.31	0.02	0.00	7.40	2.00	0.00	6.30	0.02	0.00
7.42	2.00	0.00	6.29	0.02	0.00	7.44	2.00	0.00	6.28	0.02	0.00
7.46	2.00	0.00	6.27	0.02	0.00	7.48	2.00	0.00	6.26	0.02	0.00
7.50	2.00	0.00	6.25	0.02	0.00	7.52	2.00	0.00	6.24	0.02	0.00
7.54	2.00	0.00	6.23	0.02	0.00	7.56	2.00	0.00	6.22	0.02	0.00
7.58	2.00	0.00	6.21	0.02	0.00	7.60	2.00	0.00	6.20	0.02	0.00
7.62	2.00	0.00	6.19	0.02	0.00	7.64	2.00	0.00	6.18	0.02	0.00
7.66	2.00	0.00	6.17	0.02	0.00	7.68	2.00	0.00	6.16	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
7.70	2.00	0.00	6.15	0.02	0.00	7.72	2.00	0.00	6.14	0.02	0.00
7.74	2.00	0.00	6.13	0.02	0.00	7.76	2.00	0.00	6.12	0.02	0.00
7.78	2.00	0.00	6.11	0.02	0.00	7.80	2.00	0.00	6.10	0.02	0.00
7.82	2.00	0.00	6.09	0.02	0.00	7.84	2.00	0.00	6.08	0.02	0.00
7.86	2.00	0.00	6.07	0.02	0.00	7.88	2.00	0.00	6.06	0.02	0.00
7.90	2.00	0.00	6.05	0.02	0.00	7.92	2.00	0.00	6.04	0.02	0.00
7.94	2.00	0.00	6.03	0.02	0.00	7.96	2.00	0.00	6.02	0.02	0.00
7.99	2.00	0.00	6.01	0.03	0.00	8.00	2.00	0.00	6.00	0.01	0.00
8.02	2.00	0.00	5.99	0.02	0.00	8.04	2.00	0.00	5.98	0.02	0.00
8.06	2.00	0.00	5.97	0.02	0.00	8.08	2.00	0.00	5.96	0.02	0.00
8.10	2.00	0.00	5.95	0.02	0.00	8.12	2.00	0.00	5.94	0.02	0.00
8.14	2.00	0.00	5.93	0.02	0.00	8.17	2.00	0.00	5.92	0.03	0.00
8.18	2.00	0.00	5.91	0.01	0.00	8.20	2.00	0.00	5.90	0.02	0.00
8.22	2.00	0.00	5.89	0.02	0.00	8.24	2.00	0.00	5.88	0.02	0.00
8.26	2.00	0.00	5.87	0.02	0.00	8.28	2.00	0.00	5.86	0.02	0.00
8.30	2.00	0.00	5.85	0.02	0.00	8.32	2.00	0.00	5.84	0.02	0.00
8.34	2.00	0.00	5.83	0.02	0.00	8.36	2.00	0.00	5.82	0.02	0.00
8.38	2.00	0.00	5.81	0.02	0.00	8.40	2.00	0.00	5.80	0.02	0.00
8.42	2.00	0.00	5.79	0.02	0.00	8.44	2.00	0.00	5.78	0.02	0.00
8.46	2.00	0.00	5.77	0.02	0.00	8.48	2.00	0.00	5.76	0.02	0.00
8.50	0.62	0.38	5.75	0.02	0.04	8.52	0.62	0.38	5.74	0.02	0.04
8.54	0.63	0.37	5.73	0.02	0.04	8.56	0.63	0.37	5.72	0.02	0.04
8.58	0.64	0.36	5.71	0.02	0.04	8.60	2.00	0.00	5.70	0.02	0.00
8.62	2.00	0.00	5.69	0.02	0.00	8.64	2.00	0.00	5.68	0.02	0.00
8.66	2.00	0.00	5.67	0.02	0.00	8.68	0.62	0.38	5.66	0.02	0.04
8.70	2.00	0.00	5.65	0.02	0.00	8.72	2.00	0.00	5.64	0.02	0.00
8.74	2.00	0.00	5.63	0.02	0.00	8.76	2.00	0.00	5.62	0.02	0.00
8.78	2.00	0.00	5.61	0.02	0.00	8.81	2.00	0.00	5.60	0.03	0.00
8.82	2.00	0.00	5.59	0.01	0.00	8.84	2.00	0.00	5.58	0.02	0.00
8.86	2.00	0.00	5.57	0.02	0.00	8.88	2.00	0.00	5.56	0.02	0.00
8.90	2.00	0.00	5.55	0.02	0.00	8.92	2.00	0.00	5.54	0.02	0.00
8.94	2.00	0.00	5.53	0.02	0.00	8.96	2.00	0.00	5.52	0.02	0.00
8.98	2.00	0.00	5.51	0.02	0.00	9.01	2.00	0.00	5.50	0.03	0.00
9.02	2.00	0.00	5.49	0.01	0.00	9.04	2.00	0.00	5.48	0.02	0.00
9.06	2.00	0.00	5.47	0.02	0.00	9.08	2.00	0.00	5.46	0.02	0.00
9.10	2.00	0.00	5.45	0.02	0.00	9.12	2.00	0.00	5.44	0.02	0.00
9.14	2.00	0.00	5.43	0.02	0.00	9.16	2.00	0.00	5.42	0.02	0.00
9.18	2.00	0.00	5.41	0.02	0.00	9.20	2.00	0.00	5.40	0.02	0.00
9.22	2.00	0.00	5.39	0.02	0.00	9.24	2.00	0.00	5.38	0.02	0.00
9.26	2.00	0.00	5.37	0.02	0.00	9.28	2.00	0.00	5.36	0.02	0.00
9.30	2.00	0.00	5.35	0.02	0.00	9.32	2.00	0.00	5.34	0.02	0.00
9.34	2.00	0.00	5.33	0.02	0.00	9.36	2.00	0.00	5.32	0.02	0.00
9.38	2.00	0.00	5.31	0.02	0.00	9.40	2.00	0.00	5.30	0.02	0.00
9.42	2.00	0.00	5.29	0.02	0.00	9.44	2.00	0.00	5.28	0.02	0.00
9.46	2.00	0.00	5.27	0.02	0.00	9.48	2.00	0.00	5.26	0.02	0.00
9.50	2.00	0.00	5.25	0.02	0.00	9.52	2.00	0.00	5.24	0.02	0.00
9.54	2.00	0.00	5.23	0.02	0.00	9.56	2.00	0.00	5.22	0.02	0.00
9.58	2.00	0.00	5.21	0.02	0.00	9.60	2.00	0.00	5.20	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
9.62	2.00	0.00	5.19	0.02	0.00	9.64	2.00	0.00	5.18	0.02	0.00
9.66	2.00	0.00	5.17	0.02	0.00	9.68	2.00	0.00	5.16	0.02	0.00
9.70	2.00	0.00	5.15	0.02	0.00	9.72	2.00	0.00	5.14	0.02	0.00
9.74	2.00	0.00	5.13	0.02	0.00	9.76	2.00	0.00	5.12	0.02	0.00
9.78	2.00	0.00	5.11	0.02	0.00	9.80	2.00	0.00	5.10	0.02	0.00
9.82	2.00	0.00	5.09	0.02	0.00	9.84	2.00	0.00	5.08	0.02	0.00
9.86	2.00	0.00	5.07	0.02	0.00	9.88	2.00	0.00	5.06	0.02	0.00
9.90	2.00	0.00	5.05	0.02	0.00	9.92	2.00	0.00	5.04	0.02	0.00
9.94	2.00	0.00	5.03	0.02	0.00	9.96	2.00	0.00	5.02	0.02	0.00
9.98	2.00	0.00	5.01	0.02	0.00	10.00	2.00	0.00	5.00	0.02	0.00
10.02	2.00	0.00	4.99	0.02	0.00	10.04	2.00	0.00	4.98	0.02	0.00
10.06	2.00	0.00	4.97	0.02	0.00	10.08	0.62	0.38	4.96	0.02	0.04
10.11	0.61	0.39	4.95	0.03	0.06	10.12	0.60	0.40	4.94	0.01	0.02
10.14	0.61	0.39	4.93	0.02	0.04	10.16	0.61	0.39	4.92	0.02	0.04
10.18	0.61	0.39	4.91	0.02	0.04	10.20	0.62	0.38	4.90	0.02	0.04
10.22	0.62	0.38	4.89	0.02	0.04	10.24	2.00	0.00	4.88	0.02	0.00
10.26	2.00	0.00	4.87	0.02	0.00	10.28	2.00	0.00	4.86	0.02	0.00
10.30	2.00	0.00	4.85	0.02	0.00	10.32	2.00	0.00	4.84	0.02	0.00
10.34	2.00	0.00	4.83	0.02	0.00	10.36	2.00	0.00	4.82	0.02	0.00
10.38	2.00	0.00	4.81	0.02	0.00	10.40	2.00	0.00	4.80	0.02	0.00
10.42	2.00	0.00	4.79	0.02	0.00	10.44	2.00	0.00	4.78	0.02	0.00
10.46	2.00	0.00	4.77	0.02	0.00	10.48	2.00	0.00	4.76	0.02	0.00
10.50	2.00	0.00	4.75	0.02	0.00	10.52	2.00	0.00	4.74	0.02	0.00
10.54	2.00	0.00	4.73	0.02	0.00	10.56	0.62	0.38	4.72	0.02	0.04
10.58	0.61	0.39	4.71	0.02	0.04	10.60	0.60	0.40	4.70	0.02	0.04
10.62	0.60	0.40	4.69	0.02	0.04	10.64	0.60	0.40	4.68	0.02	0.04
10.66	0.60	0.40	4.67	0.02	0.04	10.68	0.62	0.38	4.66	0.02	0.04
10.70	0.62	0.38	4.65	0.02	0.03	10.72	0.64	0.36	4.64	0.02	0.03
10.74	0.64	0.36	4.63	0.02	0.03	10.76	0.63	0.37	4.62	0.02	0.03
10.78	0.61	0.39	4.61	0.02	0.04	10.80	0.60	0.40	4.60	0.02	0.04
10.82	2.00	0.00	4.59	0.02	0.00	10.84	2.00	0.00	4.58	0.02	0.00
10.86	2.00	0.00	4.57	0.02	0.00	10.88	2.00	0.00	4.56	0.02	0.00
10.91	2.00	0.00	4.55	0.03	0.00	10.92	2.00	0.00	4.54	0.01	0.00
10.94	2.00	0.00	4.53	0.02	0.00	10.96	2.00	0.00	4.52	0.02	0.00
10.98	2.00	0.00	4.51	0.02	0.00	11.00	2.00	0.00	4.50	0.02	0.00
11.02	2.00	0.00	4.49	0.02	0.00	11.04	2.00	0.00	4.48	0.02	0.00
11.06	2.00	0.00	4.47	0.02	0.00	11.08	2.00	0.00	4.46	0.02	0.00
11.10	2.00	0.00	4.45	0.02	0.00	11.12	2.00	0.00	4.44	0.02	0.00
11.14	2.00	0.00	4.43	0.02	0.00	11.16	0.63	0.37	4.42	0.02	0.03
11.18	0.62	0.38	4.41	0.02	0.03	11.21	0.62	0.38	4.39	0.03	0.05
11.22	0.61	0.39	4.39	0.01	0.02	11.24	0.61	0.39	4.38	0.02	0.03
11.26	0.62	0.38	4.37	0.02	0.03	11.28	0.62	0.38	4.36	0.02	0.03
11.30	0.62	0.38	4.35	0.02	0.03	11.32	2.00	0.00	4.34	0.02	0.00
11.34	2.00	0.00	4.33	0.02	0.00	11.36	2.00	0.00	4.32	0.02	0.00
11.38	2.00	0.00	4.31	0.02	0.00	11.40	2.00	0.00	4.30	0.02	0.00
11.42	2.00	0.00	4.29	0.02	0.00	11.44	2.00	0.00	4.28	0.02	0.00
11.46	2.00	0.00	4.27	0.02	0.00	11.48	2.00	0.00	4.26	0.02	0.00
11.50	2.00	0.00	4.25	0.02	0.00	11.52	2.00	0.00	4.24	0.02	0.00

:: Liquefaction Potential Index calculation data :: (continued)

Depth (m)	FS	F_L	w_z	d_z	LPI	Depth (m)	FS	F_L	w_z	d_z	LPI
11.54	2.00	0.00	4.23	0.02	0.00	11.56	2.00	0.00	4.22	0.02	0.00
11.58	2.00	0.00	4.21	0.02	0.00	11.60	2.00	0.00	4.20	0.02	0.00
11.62	0.63	0.37	4.19	0.02	0.03	11.64	0.62	0.38	4.18	0.02	0.03
11.66	0.61	0.39	4.17	0.02	0.03	11.68	0.60	0.40	4.16	0.02	0.03

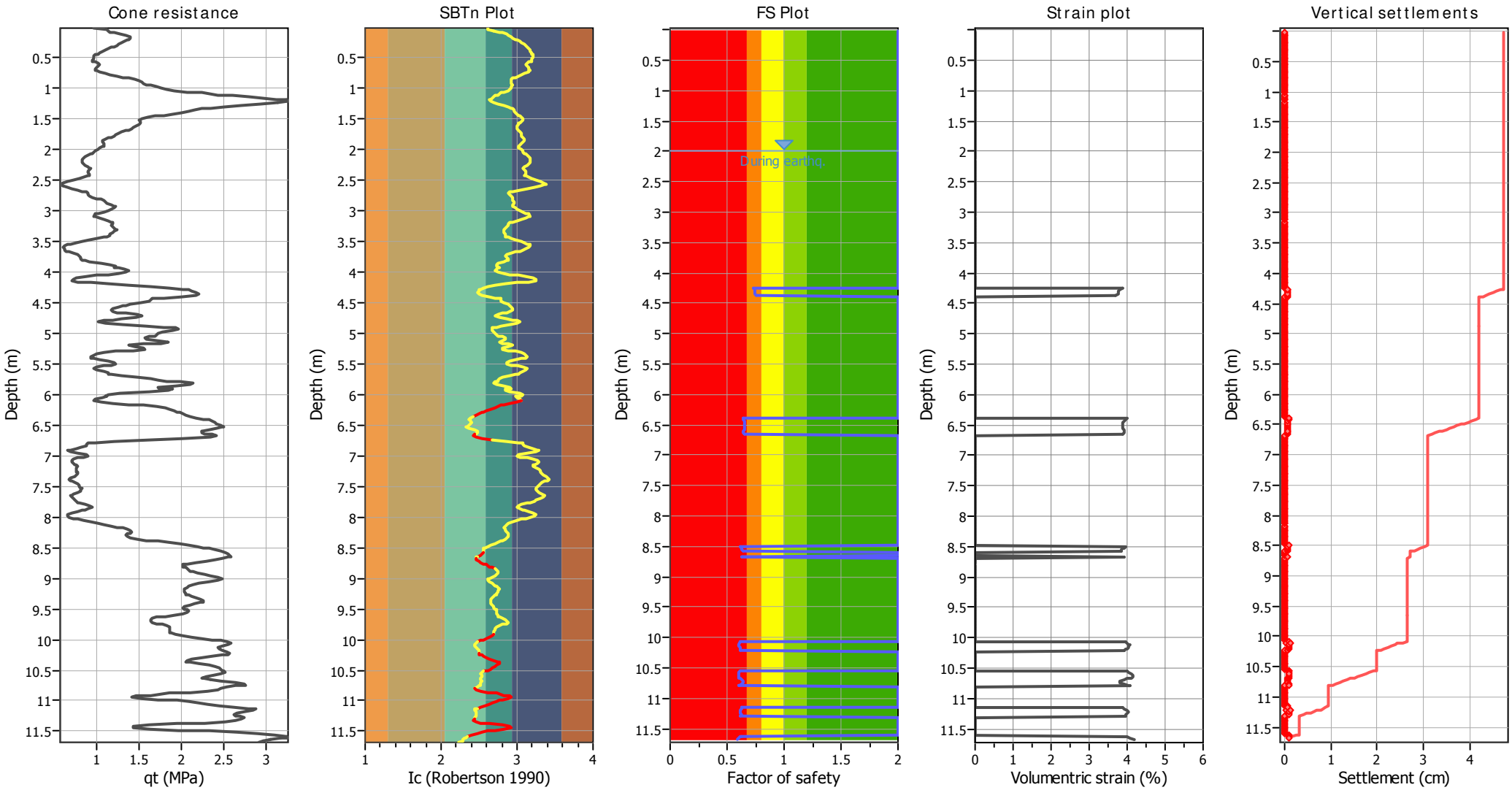
Overall liquefaction potential: 2.37

LPI = 0.00 - Liquefaction risk very low
LPI between 0.00 and 5.00 - Liquefaction risk low
LPI between 5.00 and 15.00 - Liquefaction risk high
LPI > 15.00 - Liquefaction risk very high

Abbreviations

FS: Calculated factor of safety for test point
F_L: 1 - FS
w_z: Function value of the extend of soil liquefaction according to depth
d_z: Layer thickness (m)
LPI: Liquefaction potential index value for test point

Estimation of post-earthquake settlements



Abbreviations

q_t:	Total cone resistance (cone resistance q_c corrected for pore water effects)
I_c:	Soil Behaviour Type Index
FS:	Calculated Factor of Safety against liquefaction
Volumentric strain:	Post-liquefaction volumentric strain

:: Post-earthquake settlement due to soil liquefaction ::

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
2.00	16.60	2.00	0.00	1.00	0.00	2.02	15.92	2.00	0.00	1.00	0.00
2.04	15.62	2.00	0.00	1.00	0.00	2.06	15.58	2.00	0.00	1.00	0.00
2.08	15.24	2.00	0.00	1.00	0.00	2.10	14.49	2.00	0.00	1.00	0.00
2.12	13.88	2.00	0.00	1.00	0.00	2.15	13.77	2.00	0.00	1.00	0.00
2.16	13.41	2.00	0.00	1.00	0.00	2.18	13.24	2.00	0.00	1.00	0.00
2.20	13.32	2.00	0.00	1.00	0.00	2.22	13.04	2.00	0.00	1.00	0.00
2.24	13.30	2.00	0.00	1.00	0.00	2.26	13.66	2.00	0.00	1.00	0.00
2.28	13.98	2.00	0.00	1.00	0.00	2.30	14.75	2.00	0.00	1.00	0.00
2.32	14.61	2.00	0.00	1.00	0.00	2.34	14.44	2.00	0.00	1.00	0.00
2.36	14.10	2.00	0.00	1.00	0.00	2.38	14.10	2.00	0.00	1.00	0.00
2.40	14.45	2.00	0.00	1.00	0.00	2.42	14.46	2.00	0.00	1.00	0.00
2.44	14.12	2.00	0.00	1.00	0.00	2.46	13.08	2.00	0.00	1.00	0.00
2.48	12.38	2.00	0.00	1.00	0.00	2.50	11.14	2.00	0.00	1.00	0.00
2.52	10.00	2.00	0.00	1.00	0.00	2.54	9.23	2.00	0.00	1.00	0.00
2.56	8.59	2.00	0.00	1.00	0.00	2.58	8.40	2.00	0.00	1.00	0.00
2.60	8.83	2.00	0.00	1.00	0.00	2.62	9.42	2.00	0.00	1.00	0.00
2.64	10.45	2.00	0.00	1.00	0.00	2.66	11.31	2.00	0.00	1.00	0.00
2.68	12.39	2.00	0.00	1.00	0.00	2.70	13.14	2.00	0.00	1.00	0.00
2.72	13.43	2.00	0.00	1.00	0.00	2.74	13.40	2.00	0.00	1.00	0.00
2.76	13.28	2.00	0.00	1.00	0.00	2.78	13.79	2.00	0.00	1.00	0.00
2.80	14.62	2.00	0.00	1.00	0.00	2.82	15.51	2.00	0.00	1.00	0.00
2.84	16.00	2.00	0.00	1.00	0.00	2.86	16.20	2.00	0.00	1.00	0.00
2.88	16.22	2.00	0.00	1.00	0.00	2.90	17.12	2.00	0.00	1.00	0.00
2.92	17.80	2.00	0.00	1.00	0.00	2.94	18.02	2.00	0.00	1.00	0.00
2.96	17.70	2.00	0.00	1.00	0.00	2.98	17.10	2.00	0.00	1.00	0.00
3.00	16.88	2.00	0.00	1.00	0.00	3.02	15.67	2.00	0.00	1.00	0.00
3.04	14.97	2.00	0.00	1.00	0.00	3.06	14.34	2.00	0.00	1.00	0.00
3.09	13.88	2.00	0.00	1.00	0.00	3.10	14.11	2.00	0.00	1.00	0.00
3.12	14.34	2.00	0.00	1.00	0.00	3.15	15.53	2.00	0.00	1.00	0.00
3.16	15.86	2.00	0.00	1.00	0.00	3.18	16.83	2.00	0.00	1.00	0.00
3.20	16.80	2.00	0.00	1.00	0.00	3.22	16.62	2.00	0.00	1.00	0.00
3.24	16.28	2.00	0.00	1.00	0.00	3.26	16.28	2.00	0.00	1.00	0.00
3.28	16.69	2.00	0.00	1.00	0.00	3.30	16.76	2.00	0.00	1.00	0.00
3.32	17.11	2.00	0.00	1.00	0.00	3.34	16.89	2.00	0.00	1.00	0.00
3.36	15.97	2.00	0.00	1.00	0.00	3.38	15.81	2.00	0.00	1.00	0.00
3.40	15.60	2.00	0.00	1.00	0.00	3.42	15.55	2.00	0.00	1.00	0.00
3.44	14.87	2.00	0.00	1.00	0.00	3.46	13.66	2.00	0.00	1.00	0.00
3.48	12.49	2.00	0.00	1.00	0.00	3.50	11.19	2.00	0.00	1.00	0.00
3.52	10.08	2.00	0.00	1.00	0.00	3.54	9.60	2.00	0.00	1.00	0.00
3.56	8.68	2.00	0.00	1.00	0.00	3.58	8.19	2.00	0.00	1.00	0.00
3.60	8.43	2.00	0.00	1.00	0.00	3.62	8.27	2.00	0.00	1.00	0.00
3.64	8.38	2.00	0.00	1.00	0.00	3.66	8.69	2.00	0.00	1.00	0.00
3.68	8.93	2.00	0.00	1.00	0.00	3.70	9.80	2.00	0.00	1.00	0.00
3.72	10.39	2.00	0.00	1.00	0.00	3.74	10.78	2.00	0.00	1.00	0.00
3.76	10.68	2.00	0.00	1.00	0.00	3.78	10.88	2.00	0.00	1.00	0.00
3.80	10.90	2.00	0.00	1.00	0.00	3.82	11.36	2.00	0.00	1.00	0.00
3.84	11.91	2.00	0.00	1.00	0.00	3.86	12.95	2.00	0.00	1.00	0.00
3.88	17.04	2.00	0.00	1.00	0.00	3.90	15.98	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
3.92	15.86	2.00	0.00	1.00	0.00	3.94	16.08	2.00	0.00	1.00	0.00
3.96	17.55	2.00	0.00	1.00	0.00	3.98	18.04	2.00	0.00	1.00	0.00
4.00	18.30	2.00	0.00	1.00	0.00	4.02	16.75	2.00	0.00	1.00	0.00
4.05	14.71	2.00	0.00	1.00	0.00	4.06	14.13	2.00	0.00	1.00	0.00
4.08	11.11	2.00	0.00	1.00	0.00	4.10	10.23	2.00	0.00	1.00	0.00
4.12	9.43	2.00	0.00	1.00	0.00	4.14	9.05	2.00	0.00	1.00	0.00
4.16	9.79	2.00	0.00	1.00	0.00	4.18	11.83	2.00	0.00	1.00	0.00
4.20	15.02	2.00	0.00	1.00	0.00	4.22	17.90	2.00	0.00	1.00	0.00
4.24	21.96	2.00	0.00	1.00	0.00	4.26	82.66	0.73	3.88	1.00	0.08
4.28	84.04	0.74	3.82	1.00	0.08	4.30	85.03	0.75	3.78	1.00	0.08
4.32	85.12	0.74	3.77	1.00	0.08	4.34	84.84	0.74	3.79	1.00	0.08
4.36	87.23	0.76	3.68	1.00	0.07	4.38	87.26	0.76	3.68	1.00	0.07
4.40	26.32	2.00	0.00	1.00	0.00	4.42	22.89	2.00	0.00	1.00	0.00
4.44	21.02	2.00	0.00	1.00	0.00	4.46	21.36	2.00	0.00	1.00	0.00
4.49	21.96	2.00	0.00	1.00	0.00	4.50	19.73	2.00	0.00	1.00	0.00
4.52	17.75	2.00	0.00	1.00	0.00	4.54	17.15	2.00	0.00	1.00	0.00
4.56	17.32	2.00	0.00	1.00	0.00	4.58	16.38	2.00	0.00	1.00	0.00
4.60	15.06	2.00	0.00	1.00	0.00	4.62	14.92	2.00	0.00	1.00	0.00
4.64	15.21	2.00	0.00	1.00	0.00	4.66	15.62	2.00	0.00	1.00	0.00
4.68	16.34	2.00	0.00	1.00	0.00	4.70	19.16	2.00	0.00	1.00	0.00
4.72	20.88	2.00	0.00	1.00	0.00	4.74	18.42	2.00	0.00	1.00	0.00
4.76	16.35	2.00	0.00	1.00	0.00	4.78	14.96	2.00	0.00	1.00	0.00
4.80	14.09	2.00	0.00	1.00	0.00	4.82	12.39	2.00	0.00	1.00	0.00
4.84	12.15	2.00	0.00	1.00	0.00	4.86	17.23	2.00	0.00	1.00	0.00
4.88	20.05	2.00	0.00	1.00	0.00	4.90	22.33	2.00	0.00	1.00	0.00
4.92	25.09	2.00	0.00	1.00	0.00	4.94	25.42	2.00	0.00	1.00	0.00
4.96	23.80	2.00	0.00	1.00	0.00	4.98	22.11	2.00	0.00	1.00	0.00
5.00	21.50	2.00	0.00	1.00	0.00	5.02	21.64	2.00	0.00	1.00	0.00
5.04	21.41	2.00	0.00	1.00	0.00	5.06	20.58	2.00	0.00	1.00	0.00
5.08	19.33	2.00	0.00	1.00	0.00	5.10	19.03	2.00	0.00	1.00	0.00
5.12	21.34	2.00	0.00	1.00	0.00	5.14	24.44	2.00	0.00	1.00	0.00
5.16	23.29	2.00	0.00	1.00	0.00	5.18	17.90	2.00	0.00	1.00	0.00
5.20	16.61	2.00	0.00	1.00	0.00	5.22	17.19	2.00	0.00	1.00	0.00
5.24	20.23	2.00	0.00	1.00	0.00	5.26	20.45	2.00	0.00	1.00	0.00
5.28	17.63	2.00	0.00	1.00	0.00	5.30	14.89	2.00	0.00	1.00	0.00
5.32	13.20	2.00	0.00	1.00	0.00	5.34	12.44	2.00	0.00	1.00	0.00
5.36	11.73	2.00	0.00	1.00	0.00	5.38	11.49	2.00	0.00	1.00	0.00
5.40	11.36	2.00	0.00	1.00	0.00	5.42	11.59	2.00	0.00	1.00	0.00
5.44	12.43	2.00	0.00	1.00	0.00	5.46	13.78	2.00	0.00	1.00	0.00
5.48	14.96	2.00	0.00	1.00	0.00	5.50	14.92	2.00	0.00	1.00	0.00
5.52	14.43	2.00	0.00	1.00	0.00	5.54	13.14	2.00	0.00	1.00	0.00
5.56	12.09	2.00	0.00	1.00	0.00	5.58	11.40	2.00	0.00	1.00	0.00
5.60	11.74	2.00	0.00	1.00	0.00	5.62	13.40	2.00	0.00	1.00	0.00
5.64	14.17	2.00	0.00	1.00	0.00	5.66	13.67	2.00	0.00	1.00	0.00
5.68	13.22	2.00	0.00	1.00	0.00	5.70	15.06	2.00	0.00	1.00	0.00
5.72	17.99	2.00	0.00	1.00	0.00	5.74	20.04	2.00	0.00	1.00	0.00
5.76	20.37	2.00	0.00	1.00	0.00	5.78	21.45	2.00	0.00	1.00	0.00
5.80	23.51	2.00	0.00	1.00	0.00	5.82	25.69	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
5.84	26.71	2.00	0.00	1.00	0.00	5.87	22.79	2.00	0.00	1.00	0.00
5.88	19.15	2.00	0.00	1.00	0.00	5.90	19.91	2.00	0.00	1.00	0.00
5.92	23.10	2.00	0.00	1.00	0.00	5.94	24.47	2.00	0.00	1.00	0.00
5.96	18.16	2.00	0.00	1.00	0.00	5.99	15.05	2.00	0.00	1.00	0.00
6.00	12.31	2.00	0.00	1.00	0.00	6.02	13.03	2.00	0.00	1.00	0.00
6.04	13.57	2.00	0.00	1.00	0.00	6.06	12.68	2.00	0.00	1.00	0.00
6.08	11.11	2.00	0.00	1.00	0.00	6.10	10.83	2.00	0.00	1.00	0.00
6.12	11.94	2.00	0.00	1.00	0.00	6.14	13.88	2.00	0.00	1.00	0.00
6.16	15.90	2.00	0.00	1.00	0.00	6.18	18.25	2.00	0.00	1.00	0.00
6.20	20.09	2.00	0.00	1.00	0.00	6.22	21.00	2.00	0.00	1.00	0.00
6.24	21.79	2.00	0.00	1.00	0.00	6.26	79.58	2.00	0.00	1.00	0.00
6.28	79.39	2.00	0.00	1.00	0.00	6.30	79.33	2.00	0.00	1.00	0.00
6.32	79.28	2.00	0.00	1.00	0.00	6.34	79.14	2.00	0.00	1.00	0.00
6.36	78.85	2.00	0.00	1.00	0.00	6.38	79.08	2.00	0.00	1.00	0.00
6.40	79.82	0.64	4.02	1.00	0.08	6.42	81.23	0.65	3.95	1.00	0.08
6.44	82.01	0.65	3.91	1.00	0.08	6.46	82.42	0.65	3.90	1.00	0.08
6.48	82.36	0.65	3.90	1.00	0.08	6.50	82.55	0.65	3.89	1.00	0.08
6.52	82.49	0.65	3.89	1.00	0.08	6.54	82.55	0.65	3.89	1.00	0.08
6.56	82.27	0.65	3.90	1.00	0.08	6.58	82.04	0.65	3.91	1.00	0.08
6.60	81.76	0.65	3.93	1.00	0.08	6.62	81.71	0.65	3.93	1.00	0.08
6.64	81.79	0.65	3.92	1.00	0.08	6.66	82.51	0.65	3.89	1.00	0.08
6.68	83.87	2.00	0.00	1.00	0.00	6.70	84.01	2.00	0.00	1.00	0.00
6.72	81.25	2.00	0.00	1.00	0.00	6.74	17.27	2.00	0.00	1.00	0.00
6.76	13.66	2.00	0.00	1.00	0.00	6.78	10.44	2.00	0.00	1.00	0.00
6.80	9.39	2.00	0.00	1.00	0.00	6.82	10.93	2.00	0.00	1.00	0.00
6.85	9.79	2.00	0.00	1.00	0.00	6.86	8.93	2.00	0.00	1.00	0.00
6.88	8.66	2.00	0.00	1.00	0.00	6.90	7.79	2.00	0.00	1.00	0.00
6.92	6.99	2.00	0.00	1.00	0.00	6.94	7.39	2.00	0.00	1.00	0.00
6.96	8.45	2.00	0.00	1.00	0.00	6.98	10.04	2.00	0.00	1.00	0.00
7.00	10.41	2.00	0.00	1.00	0.00	7.02	9.29	2.00	0.00	1.00	0.00
7.04	8.47	2.00	0.00	1.00	0.00	7.06	7.91	2.00	0.00	1.00	0.00
7.08	7.45	2.00	0.00	1.00	0.00	7.10	7.75	2.00	0.00	1.00	0.00
7.12	7.81	2.00	0.00	1.00	0.00	7.14	8.06	2.00	0.00	1.00	0.00
7.16	8.58	2.00	0.00	1.00	0.00	7.18	8.60	2.00	0.00	1.00	0.00
7.20	8.36	2.00	0.00	1.00	0.00	7.22	8.15	2.00	0.00	1.00	0.00
7.24	8.12	2.00	0.00	1.00	0.00	7.26	8.36	2.00	0.00	1.00	0.00
7.28	8.53	2.00	0.00	1.00	0.00	7.30	8.70	2.00	0.00	1.00	0.00
7.32	8.34	2.00	0.00	1.00	0.00	7.34	7.96	2.00	0.00	1.00	0.00
7.36	7.60	2.00	0.00	1.00	0.00	7.38	7.15	2.00	0.00	1.00	0.00
7.40	7.39	2.00	0.00	1.00	0.00	7.42	7.71	2.00	0.00	1.00	0.00
7.44	8.10	2.00	0.00	1.00	0.00	7.46	8.34	2.00	0.00	1.00	0.00
7.48	8.52	2.00	0.00	1.00	0.00	7.50	8.69	2.00	0.00	1.00	0.00
7.52	8.68	2.00	0.00	1.00	0.00	7.54	8.82	2.00	0.00	1.00	0.00
7.56	8.94	2.00	0.00	1.00	0.00	7.58	8.58	2.00	0.00	1.00	0.00
7.60	8.38	2.00	0.00	1.00	0.00	7.62	7.78	2.00	0.00	1.00	0.00
7.64	7.38	2.00	0.00	1.00	0.00	7.66	7.40	2.00	0.00	1.00	0.00
7.68	7.37	2.00	0.00	1.00	0.00	7.70	7.68	2.00	0.00	1.00	0.00
7.72	7.87	2.00	0.00	1.00	0.00	7.74	8.06	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
7.76	8.05	2.00	0.00	1.00	0.00	7.78	8.41	2.00	0.00	1.00	0.00
7.80	8.72	2.00	0.00	1.00	0.00	7.82	10.19	2.00	0.00	1.00	0.00
7.84	9.72	2.00	0.00	1.00	0.00	7.86	9.30	2.00	0.00	1.00	0.00
7.88	8.88	2.00	0.00	1.00	0.00	7.90	8.56	2.00	0.00	1.00	0.00
7.92	8.00	2.00	0.00	1.00	0.00	7.94	7.14	2.00	0.00	1.00	0.00
7.96	6.66	2.00	0.00	1.00	0.00	7.99	6.48	2.00	0.00	1.00	0.00
8.00	6.89	2.00	0.00	1.00	0.00	8.02	7.25	2.00	0.00	1.00	0.00
8.04	7.75	2.00	0.00	1.00	0.00	8.06	8.66	2.00	0.00	1.00	0.00
8.08	9.48	2.00	0.00	1.00	0.00	8.10	10.46	2.00	0.00	1.00	0.00
8.12	11.34	2.00	0.00	1.00	0.00	8.14	12.22	2.00	0.00	1.00	0.00
8.17	13.35	2.00	0.00	1.00	0.00	8.18	13.87	2.00	0.00	1.00	0.00
8.20	14.58	2.00	0.00	1.00	0.00	8.22	14.99	2.00	0.00	1.00	0.00
8.24	15.00	2.00	0.00	1.00	0.00	8.26	14.75	2.00	0.00	1.00	0.00
8.28	14.41	2.00	0.00	1.00	0.00	8.30	14.18	2.00	0.00	1.00	0.00
8.32	14.29	2.00	0.00	1.00	0.00	8.34	14.53	2.00	0.00	1.00	0.00
8.36	15.66	2.00	0.00	1.00	0.00	8.38	16.69	2.00	0.00	1.00	0.00
8.40	18.09	2.00	0.00	1.00	0.00	8.42	19.48	2.00	0.00	1.00	0.00
8.44	20.88	2.00	0.00	1.00	0.00	8.46	22.08	2.00	0.00	1.00	0.00
8.48	23.03	2.00	0.00	1.00	0.00	8.50	81.00	0.62	3.96	1.00	0.08
8.52	81.62	0.62	3.93	1.00	0.08	8.54	82.54	0.63	3.89	1.00	0.08
8.56	83.39	0.63	3.85	1.00	0.08	8.58	83.87	0.64	3.83	1.00	0.08
8.60	84.18	2.00	0.00	1.00	0.00	8.62	83.96	2.00	0.00	1.00	0.00
8.64	83.70	2.00	0.00	1.00	0.00	8.66	83.05	2.00	0.00	1.00	0.00
8.68	81.66	0.62	3.93	1.00	0.08	8.70	80.58	2.00	0.00	1.00	0.00
8.72	79.88	2.00	0.00	1.00	0.00	8.74	78.94	2.00	0.00	1.00	0.00
8.76	77.75	2.00	0.00	1.00	0.00	8.78	76.99	2.00	0.00	1.00	0.00
8.81	21.17	2.00	0.00	1.00	0.00	8.82	21.28	2.00	0.00	1.00	0.00
8.84	21.40	2.00	0.00	1.00	0.00	8.86	21.65	2.00	0.00	1.00	0.00
8.88	21.58	2.00	0.00	1.00	0.00	8.90	21.71	2.00	0.00	1.00	0.00
8.92	22.76	2.00	0.00	1.00	0.00	8.94	23.22	2.00	0.00	1.00	0.00
8.96	24.03	2.00	0.00	1.00	0.00	8.98	25.10	2.00	0.00	1.00	0.00
9.01	25.47	2.00	0.00	1.00	0.00	9.02	25.53	2.00	0.00	1.00	0.00
9.04	25.07	2.00	0.00	1.00	0.00	9.06	23.83	2.00	0.00	1.00	0.00
9.08	22.62	2.00	0.00	1.00	0.00	9.10	21.48	2.00	0.00	1.00	0.00
9.12	21.29	2.00	0.00	1.00	0.00	9.14	21.29	2.00	0.00	1.00	0.00
9.16	21.03	2.00	0.00	1.00	0.00	9.18	20.70	2.00	0.00	1.00	0.00
9.20	20.54	2.00	0.00	1.00	0.00	9.22	20.77	2.00	0.00	1.00	0.00
9.24	20.75	2.00	0.00	1.00	0.00	9.26	20.92	2.00	0.00	1.00	0.00
9.28	20.99	2.00	0.00	1.00	0.00	9.30	21.33	2.00	0.00	1.00	0.00
9.32	21.91	2.00	0.00	1.00	0.00	9.34	22.75	2.00	0.00	1.00	0.00
9.36	22.87	2.00	0.00	1.00	0.00	9.38	22.95	2.00	0.00	1.00	0.00
9.40	22.30	2.00	0.00	1.00	0.00	9.42	21.80	2.00	0.00	1.00	0.00
9.44	21.04	2.00	0.00	1.00	0.00	9.46	20.53	2.00	0.00	1.00	0.00
9.48	20.08	2.00	0.00	1.00	0.00	9.50	20.28	2.00	0.00	1.00	0.00
9.52	20.70	2.00	0.00	1.00	0.00	9.54	21.13	2.00	0.00	1.00	0.00
9.56	20.90	2.00	0.00	1.00	0.00	9.58	20.23	2.00	0.00	1.00	0.00
9.60	19.20	2.00	0.00	1.00	0.00	9.62	18.11	2.00	0.00	1.00	0.00
9.64	16.91	2.00	0.00	1.00	0.00	9.66	16.35	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
9.68	16.32	2.00	0.00	1.00	0.00	9.70	16.19	2.00	0.00	1.00	0.00
9.72	16.26	2.00	0.00	1.00	0.00	9.74	16.85	2.00	0.00	1.00	0.00
9.76	17.64	2.00	0.00	1.00	0.00	9.78	18.17	2.00	0.00	1.00	0.00
9.80	18.62	2.00	0.00	1.00	0.00	9.82	18.43	2.00	0.00	1.00	0.00
9.84	18.42	2.00	0.00	1.00	0.00	9.86	18.32	2.00	0.00	1.00	0.00
9.88	18.37	2.00	0.00	1.00	0.00	9.90	18.60	2.00	0.00	1.00	0.00
9.92	18.90	2.00	0.00	1.00	0.00	9.94	19.81	2.00	0.00	1.00	0.00
9.96	20.76	2.00	0.00	1.00	0.00	9.98	79.16	2.00	0.00	1.00	0.00
10.00	80.32	2.00	0.00	1.00	0.00	10.02	80.66	2.00	0.00	1.00	0.00
10.04	81.26	2.00	0.00	1.00	0.00	10.06	81.13	2.00	0.00	1.00	0.00
10.08	80.77	0.62	3.97	1.00	0.08	10.11	79.26	0.61	4.05	1.00	0.12
10.12	78.65	0.60	4.08	1.00	0.04	10.14	79.22	0.61	4.05	1.00	0.08
10.16	79.59	0.61	4.03	1.00	0.08	10.18	80.46	0.61	3.99	1.00	0.08
10.20	81.26	0.62	3.95	1.00	0.08	10.22	81.61	0.62	3.93	1.00	0.08
10.24	81.69	2.00	0.00	1.00	0.00	10.26	81.25	2.00	0.00	1.00	0.00
10.28	80.13	2.00	0.00	1.00	0.00	10.30	78.28	2.00	0.00	1.00	0.00
10.32	20.68	2.00	0.00	1.00	0.00	10.34	19.97	2.00	0.00	1.00	0.00
10.36	19.54	2.00	0.00	1.00	0.00	10.38	20.35	2.00	0.00	1.00	0.00
10.40	21.42	2.00	0.00	1.00	0.00	10.42	22.57	2.00	0.00	1.00	0.00
10.44	23.50	2.00	0.00	1.00	0.00	10.46	23.71	2.00	0.00	1.00	0.00
10.48	23.78	2.00	0.00	1.00	0.00	10.50	23.85	2.00	0.00	1.00	0.00
10.52	81.60	2.00	0.00	1.00	0.00	10.54	81.20	2.00	0.00	1.00	0.00
10.56	80.48	0.62	3.99	1.00	0.08	10.58	79.36	0.61	4.04	1.00	0.08
10.60	77.97	0.60	4.11	1.00	0.08	10.62	77.16	0.60	4.15	1.00	0.08
10.64	77.24	0.60	4.15	1.00	0.08	10.66	78.22	0.60	4.10	1.00	0.08
10.68	80.50	0.62	3.98	1.00	0.08	10.70	82.04	0.62	3.91	1.00	0.08
10.72	84.30	0.64	3.81	1.00	0.08	10.74	84.04	0.64	3.82	1.00	0.08
10.76	82.13	0.63	3.91	1.00	0.08	10.78	79.29	0.61	4.04	1.00	0.08
10.80	78.52	0.60	4.08	1.00	0.08	10.82	78.75	2.00	0.00	1.00	0.00
10.84	78.37	2.00	0.00	1.00	0.00	10.86	20.01	2.00	0.00	1.00	0.00
10.88	17.68	2.00	0.00	1.00	0.00	10.91	15.42	2.00	0.00	1.00	0.00
10.92	13.41	2.00	0.00	1.00	0.00	10.94	13.01	2.00	0.00	1.00	0.00
10.96	13.60	2.00	0.00	1.00	0.00	10.98	16.77	2.00	0.00	1.00	0.00
11.00	18.78	2.00	0.00	1.00	0.00	11.02	19.74	2.00	0.00	1.00	0.00
11.04	20.83	2.00	0.00	1.00	0.00	11.06	21.87	2.00	0.00	1.00	0.00
11.08	80.03	2.00	0.00	1.00	0.00	11.10	81.05	2.00	0.00	1.00	0.00
11.12	83.55	2.00	0.00	1.00	0.00	11.14	83.59	2.00	0.00	1.00	0.00
11.16	82.94	0.63	3.87	1.00	0.08	11.18	81.60	0.62	3.93	1.00	0.08
11.21	80.46	0.62	3.99	1.00	0.12	11.22	79.75	0.61	4.02	1.00	0.04
11.24	79.97	0.61	4.01	1.00	0.08	11.26	81.24	0.62	3.95	1.00	0.08
11.28	81.37	0.62	3.94	1.00	0.08	11.30	80.87	0.62	3.97	1.00	0.08
11.32	79.68	2.00	0.00	1.00	0.00	11.34	79.05	2.00	0.00	1.00	0.00
11.36	77.69	2.00	0.00	1.00	0.00	11.38	18.22	2.00	0.00	1.00	0.00
11.40	14.66	2.00	0.00	1.00	0.00	11.42	12.40	2.00	0.00	1.00	0.00
11.44	12.85	2.00	0.00	1.00	0.00	11.46	14.46	2.00	0.00	1.00	0.00
11.48	17.95	2.00	0.00	1.00	0.00	11.50	21.84	2.00	0.00	1.00	0.00
11.52	81.57	2.00	0.00	1.00	0.00	11.54	83.50	2.00	0.00	1.00	0.00
11.56	84.21	2.00	0.00	1.00	0.00	11.58	84.85	2.00	0.00	1.00	0.00

:: Post-earthquake settlement due to soil liquefaction :: (continued)

Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)	Depth (m)	$q_{c1N,cs}$	FS	e_v (%)	DF	Settlement (cm)
11.60	83.93	2.00	0.00	1.00	0.00	11.62	82.26	0.63	3.90	1.00	0.08
11.64	79.96	0.62	4.01	1.00	0.08	11.66	78.26	0.61	4.09	1.00	0.08
11.68	76.23	0.60	4.20	1.00	0.08						

Total estimated settlement: 4.73

Abbreviations

$Q_{tn,cs}$:	Equivalent clean sand normalized cone resistance
FS:	Factor of safety against liquefaction
e_v (%):	Post-liquefaction volumentric strain
DF:	e_v depth weighting factor
Settlement:	Calculated settlement

:: Strength loss calculation Idriss & Boulanger (2008) ::

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.02	0.97	16.45	3.45	56.70	2.62	0.08	217.47
0.04	1.12	19.02	3.48	66.13	2.62	0.08	123.73
0.06	1.13	19.21	3.87	74.39	2.68	0.08	82.36
0.08	1.15	19.55	4.48	87.59	2.76	0.08	62.13
0.10	1.21	20.48	4.90	100.42	2.81	0.08	51.46
0.12	1.28	21.71	5.31	115.32	2.86	0.08	44.98
0.14	1.35	22.88	5.58	127.64	2.89	0.08	40.23
0.16	1.39	23.52	5.92	139.21	2.92	0.08	35.86
0.18	1.39	23.57	6.22	146.50	2.95	0.08	31.70
0.20	1.38	23.32	6.53	152.37	2.98	0.08	28.05
0.22	1.35	22.91	6.85	156.79	3.01	0.08	24.90
0.24	1.32	22.34	7.19	160.55	3.04	0.08	22.15
0.26	1.29	21.81	7.52	163.93	3.07	0.08	19.89
0.28	1.26	21.38	7.78	166.37	3.09	0.07	18.03
0.30	1.23	20.87	8.04	167.86	3.11	0.07	16.38
0.32	1.21	20.39	8.25	168.16	3.13	0.07	14.96
0.34	1.17	19.76	8.47	167.41	3.14	0.07	13.60
0.36	1.13	19.16	8.65	165.65	3.16	0.07	12.44
0.38	1.09	18.44	8.86	163.31	3.17	0.07	11.32
0.40	1.06	17.87	9.01	160.97	3.18	0.07	10.40
0.42	1.03	17.43	9.13	159.06	3.19	0.07	9.65
0.45	1.01	17.01	9.25	157.36	3.20	0.07	8.78
0.46	0.99	16.65	9.37	155.96	3.21	0.07	8.40
0.48	0.97	16.32	9.45	154.16	3.21	0.07	7.89
0.50	0.96	16.25	9.35	151.97	3.21	0.07	7.54
0.52	0.96	16.11	9.26	149.19	3.20	0.07	7.18
0.54	0.95	15.93	9.20	146.57	3.20	0.07	6.84
0.56	0.95	15.95	9.06	144.51	3.19	0.07	6.60
0.58	0.98	16.41	8.71	142.91	3.16	0.07	6.55
0.60	1.01	16.97	8.38	142.12	3.14	0.07	6.55
0.62	1.03	17.25	8.23	141.92	3.12	0.07	6.44
0.64	1.01	17.00	8.37	142.25	3.13	0.07	6.15
0.66	0.99	16.67	8.55	142.55	3.15	0.07	5.85
0.68	0.98	16.42	8.71	143.13	3.16	0.07	5.59
0.70	0.97	16.34	8.82	144.13	3.17	0.07	5.40
0.72	0.99	16.65	8.73	145.36	3.16	0.07	5.35
0.74	1.03	17.20	8.52	146.57	3.15	0.07	5.38
0.76	1.09	18.35	7.98	146.45	3.10	0.07	5.58
0.78	1.16	19.45	7.45	144.81	3.06	0.07	5.77
0.80	1.23	20.73	6.91	143.19	3.01	0.07	5.99
0.82	1.30	21.90	6.52	142.71	2.98	0.08	6.17
0.84	1.38	23.21	6.21	144.05	2.95	0.08	6.39
0.86	1.45	24.31	5.99	145.68	2.93	0.08	6.53
0.88	1.50	25.23	5.89	148.57	2.92	0.08	6.62
0.90	1.53	25.67	5.94	152.61	2.92	0.08	6.59
0.92	1.56	26.18	6.00	157.09	2.93	0.08	6.57
0.94	1.59	26.72	6.08	162.51	2.94	0.08	6.56
0.96	1.64	27.62	6.05	167.11	2.94	0.08	6.63

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
0.98	1.70	28.67	5.98	171.33	2.93	0.09	6.74
1.00	1.76	29.64	5.85	173.36	2.92	0.09	6.82
1.02	1.82	30.61	5.72	175.08	2.90	0.09	6.90
1.05	1.91	32.22	5.47	176.39	2.88	0.09	7.05
1.06	2.07	34.79	5.09	176.99	2.83	0.10	7.54
1.08	2.25	37.85	4.70	177.95	2.79	0.11	8.04
1.11	2.43	40.95	4.36	178.44	2.75	0.11	8.46
1.12	2.61	44.05	4.11	180.97	2.72	0.12	9.01
1.14	2.79	47.12	3.90	183.73	2.69	0.12	9.46
1.17	2.97	50.12	3.75	187.81	2.66	0.12	9.79
1.18	3.13	52.83	3.64	192.13	2.65	0.13	10.23
1.20	3.25	54.90	3.60	197.43	2.64	0.13	10.44
1.22	3.26	55.05	3.71	204.24	2.66	0.14	10.29
1.24	3.14	53.02	4.01	212.44	2.70	0.13	9.74
1.26	2.94	49.54	4.45	220.36	2.76	0.12	8.95
1.28	2.72	45.76	4.97	227.31	2.82	0.12	8.13
1.30	2.51	42.25	5.50	232.34	2.88	0.11	7.38
1.32	2.34	39.44	5.95	234.84	2.93	0.10	6.78
1.34	2.24	37.62	6.22	234.03	2.95	0.10	6.36
1.36	2.16	36.29	6.34	229.97	2.96	0.10	6.04
1.38	2.09	35.08	6.39	224.07	2.97	0.09	5.75
1.40	1.99	33.42	6.51	217.52	2.98	0.09	5.40
1.42	1.90	31.77	6.65	211.43	2.99	0.09	5.06
1.44	1.79	29.95	6.88	205.98	3.01	0.09	4.70
1.46	1.69	28.19	7.13	200.95	3.03	0.08	4.36
1.48	1.59	26.62	7.40	196.83	3.06	0.08	4.06
1.50	1.53	25.60	7.53	192.85	3.07	0.08	3.85
1.52	1.51	25.12	7.53	189.04	3.07	0.08	3.73
1.54	1.51	25.18	7.33	184.59	3.05	0.08	3.69
1.56	1.51	25.25	7.13	180.00	3.03	0.08	3.65
1.58	1.51	25.22	6.96	175.47	3.02	0.08	3.60
1.60	1.49	24.87	6.85	170.43	3.01	0.08	3.50
1.62	1.47	24.39	6.78	165.32	3.00	0.08	3.39
1.64	1.44	23.90	6.73	160.91	3.00	0.08	3.29
1.66	1.41	23.40	6.75	157.81	3.00	0.08	3.18
1.68	1.37	22.79	6.85	156.19	3.01	0.08	3.06
1.70	1.34	22.18	6.96	154.40	3.02	0.08	2.94
1.72	1.29	21.41	7.16	153.19	3.04	0.08	2.81
1.74	1.26	20.79	7.31	151.91	3.05	0.07	2.69
1.76	1.22	20.24	7.44	150.49	3.06	0.07	2.59
1.78	1.20	19.86	7.47	148.39	3.06	0.07	2.52
1.80	1.17	19.29	7.56	145.90	3.07	0.07	2.42
1.82	1.13	18.65	7.69	143.48	3.08	0.07	2.31
1.84	1.10	18.04	7.81	140.97	3.09	0.07	2.21
1.86	1.07	17.67	7.82	138.20	3.09	0.07	2.14
1.88	1.07	17.66	7.62	134.61	3.08	0.07	2.12
1.90	1.08	17.70	7.40	130.93	3.06	0.07	2.10
1.92	1.09	17.84	7.12	126.98	3.03	0.07	2.10

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
1.94	1.08	17.67	6.99	123.54	3.02	0.07	2.06
1.96	1.06	17.44	6.94	121.02	3.02	0.07	2.01
1.98	1.04	17.04	7.04	119.98	3.03	0.07	1.95
2.00	1.01	16.50	7.30	120.49	3.05	0.07	1.87
2.02	0.98	16.02	7.55	120.94	3.07	0.07	1.80
2.04	0.96	15.67	7.74	121.27	3.08	0.07	1.74
2.06	0.95	15.43	7.90	121.92	3.10	0.07	1.70
2.08	0.92	15.04	8.14	122.41	3.12	0.07	1.64
2.10	0.89	14.46	8.46	122.28	3.14	0.07	1.56
2.12	0.86	13.95	8.69	121.27	3.16	0.07	1.49
2.15	0.84	13.59	8.85	120.25	3.17	0.07	1.44
2.16	0.83	13.42	8.92	119.69	3.18	0.07	1.41
2.18	0.82	13.31	8.97	119.39	3.18	0.07	1.39
2.20	0.82	13.25	8.96	118.73	3.18	0.07	1.37
2.22	0.83	13.33	8.82	117.64	3.17	0.06	1.37
2.24	0.84	13.54	8.62	116.65	3.15	0.07	1.37
2.26	0.86	13.95	8.31	115.89	3.13	0.07	1.40
2.28	0.90	14.54	7.92	115.17	3.10	0.07	1.45
2.30	0.92	14.85	7.72	114.61	3.08	0.07	1.47
2.32	0.92	14.93	7.70	114.93	3.08	0.07	1.47
2.34	0.90	14.62	7.92	115.75	3.10	0.07	1.42
2.36	0.89	14.45	8.10	117.01	3.11	0.07	1.40
2.38	0.90	14.52	8.11	117.73	3.11	0.07	1.39
2.40	0.91	14.72	8.05	118.41	3.11	0.07	1.40
2.42	0.91	14.79	7.99	118.21	3.11	0.07	1.39
2.44	0.89	14.33	8.22	117.75	3.12	0.07	1.34
2.46	0.84	13.59	8.56	116.32	3.15	0.06	1.26
2.48	0.78	12.50	9.15	114.36	3.19	0.06	1.15
2.50	0.71	11.37	9.84	111.85	3.24	0.06	1.04
2.52	0.65	10.20	10.74	109.54	3.30	0.06	0.93
2.54	0.59	9.27	11.59	107.43	3.36	0.06	0.84
2.56	0.56	8.79	12.03	105.67	3.38	0.06	0.79
2.58	0.57	8.82	11.80	104.06	3.37	0.06	0.80
2.60	0.60	9.35	10.92	102.06	3.31	0.06	0.84
2.62	0.65	10.28	9.62	98.87	3.23	0.06	0.92
2.64	0.71	11.25	8.36	94.05	3.13	0.06	1.01
2.66	0.77	12.34	7.16	88.36	3.04	0.06	1.10
2.68	0.83	13.29	6.22	82.71	2.95	0.06	1.18
2.70	0.88	14.05	5.66	79.47	2.90	0.07	1.24
2.72	0.90	14.41	5.49	79.06	2.88	0.07	1.27
2.74	0.90	14.42	5.68	81.93	2.90	0.07	1.27
2.76	0.91	14.56	5.92	86.28	2.92	0.07	1.28
2.78	0.94	15.07	6.10	91.90	2.94	0.07	1.32
2.80	0.99	15.95	6.06	96.68	2.94	0.07	1.39
2.82	1.04	16.80	6.04	101.47	2.93	0.07	1.46
2.84	1.07	17.39	6.10	106.04	2.94	0.07	1.51
2.86	1.09	17.72	6.25	110.73	2.95	0.07	1.53
2.88	1.12	18.20	6.28	114.25	2.96	0.07	1.57

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
2.90	1.16	18.86	6.18	116.57	2.95	0.07	1.62
2.92	1.20	19.55	6.09	119.09	2.94	0.07	1.67
2.94	1.22	19.77	6.21	122.73	2.95	0.07	1.69
2.96	1.20	19.52	6.50	126.83	2.98	0.07	1.66
2.98	1.18	19.09	6.78	129.45	3.00	0.07	1.62
3.00	1.13	18.28	7.15	130.76	3.04	0.07	1.54
3.02	1.08	17.41	7.56	131.62	3.07	0.07	1.47
3.04	1.02	16.38	8.13	133.23	3.12	0.07	1.37
3.06	0.98	15.70	8.59	134.83	3.15	0.07	1.31
3.09	0.97	15.45	8.77	135.50	3.16	0.07	1.29
3.10	0.98	15.64	8.61	134.74	3.15	0.07	1.30
3.12	1.03	16.50	8.02	132.42	3.11	0.07	1.37
3.15	1.08	17.34	7.45	129.20	3.06	0.07	1.43
3.16	1.14	18.42	6.72	123.82	3.00	0.07	1.52
3.18	1.17	18.98	6.21	117.88	2.95	0.07	1.56
3.20	1.19	19.32	5.77	111.58	2.91	0.07	1.58
3.22	1.18	19.15	5.61	107.47	2.89	0.07	1.56
3.24	1.18	19.02	5.50	104.52	2.88	0.07	1.55
3.26	1.18	19.14	5.35	102.34	2.86	0.07	1.55
3.28	1.20	19.40	5.21	101.08	2.85	0.08	1.57
3.30	1.22	19.79	5.05	99.87	2.83	0.08	1.59
3.32	1.23	19.89	4.97	98.92	2.82	0.08	1.60
3.34	1.21	19.57	4.99	97.72	2.82	0.08	1.57
3.36	1.18	19.04	5.07	96.61	2.83	0.07	1.52
3.38	1.15	18.54	5.15	95.41	2.84	0.07	1.48
3.40	1.14	18.40	5.14	94.54	2.84	0.07	1.46
3.42	1.12	18.05	5.24	94.64	2.85	0.07	1.43
3.44	1.08	17.24	5.52	95.12	2.88	0.07	1.36
3.46	1.00	15.95	5.97	95.22	2.93	0.07	1.26
3.48	0.91	14.39	6.60	94.98	2.99	0.06	1.13
3.50	0.82	12.89	7.33	94.51	3.05	0.06	1.01
3.52	0.75	11.69	7.98	93.30	3.10	0.06	0.91
3.54	0.69	10.64	8.49	90.32	3.14	0.06	0.83
3.56	0.64	9.85	8.80	86.70	3.17	0.06	0.77
3.58	0.62	9.36	8.87	83.04	3.17	0.06	0.73
3.60	0.61	9.20	8.65	79.56	3.16	0.06	0.71
3.62	0.61	9.29	8.13	75.52	3.12	0.06	0.72
3.64	0.62	9.42	7.58	71.41	3.07	0.06	0.72
3.66	0.64	9.71	7.08	68.75	3.03	0.06	0.75
3.68	0.67	10.34	6.44	66.65	2.97	0.06	0.79
3.70	0.72	11.10	5.85	64.92	2.92	0.06	0.85
3.72	0.77	11.90	5.33	63.47	2.86	0.07	0.91
3.74	0.79	12.28	5.23	64.29	2.85	0.07	0.93
3.76	0.80	12.50	5.31	66.45	2.86	0.07	0.95
3.78	0.81	12.58	5.48	68.96	2.88	0.07	0.95
3.80	0.83	12.89	5.46	70.37	2.88	0.07	0.97
3.82	0.85	13.37	5.30	70.89	2.86	0.07	1.01
3.84	0.91	14.28	4.94	70.49	2.82	0.07	1.07

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
3.86	1.04	16.58	4.39	72.85	2.75	0.07	1.24
3.88	1.14	18.27	4.26	77.91	2.74	0.08	1.37
3.90	1.22	19.45	4.26	82.84	2.74	0.08	1.45
3.92	1.21	19.30	4.47	86.33	2.76	0.08	1.44
3.94	1.26	20.06	4.34	87.08	2.75	0.08	1.50
3.96	1.32	20.96	4.21	88.28	2.73	0.08	1.57
3.98	1.37	21.76	4.12	89.69	2.72	0.08	1.63
4.00	1.34	21.37	4.42	94.40	2.76	0.08	1.59
4.02	1.25	20.02	5.02	100.53	2.83	0.08	1.47
4.05	1.14	18.14	5.82	105.61	2.91	0.07	1.33
4.06	1.00	15.69	6.94	108.97	3.02	0.07	1.15
4.08	0.88	13.74	8.03	110.33	3.11	0.06	1.00
4.10	0.76	11.70	9.43	110.38	3.21	0.06	0.85
4.12	0.71	10.84	10.03	108.77	3.25	0.06	0.79
4.14	0.70	10.70	9.95	106.42	3.25	0.06	0.77
4.16	0.77	11.79	8.67	102.22	3.16	0.06	0.85
4.18	0.92	14.39	6.76	97.26	3.00	0.06	1.03
4.20	1.13	17.58	5.18	91.03	2.84	0.07	1.28
4.22	1.38	21.24	4.11	87.31	2.72	0.08	1.59
4.24	1.64	24.88	3.46	86.11	2.62	0.08	1.89
4.26	1.86	28.05	3.10	86.85	2.56	0.09	0.66
4.28	2.01	30.10	2.90	87.40	2.53	0.09	0.67
4.30	2.09	31.06	2.81	87.32	2.51	0.09	0.67
4.32	2.12	31.41	2.75	86.45	2.50	0.09	0.68
4.34	2.17	32.07	2.71	86.86	2.49	0.09	0.68
4.36	2.20	32.54	2.76	89.87	2.50	0.09	0.68
4.38	2.17	32.18	2.99	96.08	2.54	0.09	0.68
4.40	1.99	29.96	3.49	104.56	2.63	0.09	2.27
4.42	1.79	27.15	4.14	112.43	2.72	0.09	2.02
4.44	1.66	25.37	4.61	116.93	2.78	0.08	1.87
4.46	1.64	25.02	4.64	116.14	2.78	0.08	1.84
4.49	1.61	24.47	4.70	115.10	2.79	0.08	1.80
4.50	1.52	23.11	5.04	116.41	2.83	0.08	1.68
4.52	1.39	21.28	5.61	119.30	2.89	0.07	1.53
4.54	1.33	20.33	5.79	117.72	2.91	0.07	1.46
4.56	1.30	19.75	5.78	114.22	2.91	0.07	1.42
4.58	1.25	18.86	5.85	110.41	2.92	0.07	1.35
4.60	1.19	17.93	6.08	109.05	2.94	0.07	1.28
4.62	1.17	17.51	6.04	105.77	2.93	0.07	1.25
4.64	1.19	17.77	5.75	102.17	2.91	0.07	1.28
4.66	1.24	18.32	5.40	99.01	2.87	0.07	1.32
4.68	1.35	19.83	4.89	96.99	2.81	0.08	1.45
4.70	1.49	21.69	4.33	94.03	2.74	0.08	1.60
4.72	1.54	22.34	4.15	92.77	2.72	0.08	1.66
4.74	1.46	21.18	4.51	95.51	2.77	0.08	1.56
4.76	1.30	19.00	5.34	101.48	2.86	0.07	1.38
4.78	1.19	17.42	6.03	105.10	2.93	0.07	1.25
4.80	1.09	15.79	6.68	105.45	2.99	0.07	1.13

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
4.82	1.01	14.60	7.21	105.27	3.04	0.06	1.04
4.84	1.10	15.91	6.76	107.59	3.00	0.06	1.14
4.86	1.31	18.99	5.73	108.77	2.90	0.07	1.36
4.88	1.58	22.73	4.72	107.33	2.79	0.08	1.66
4.90	1.79	25.57	4.17	106.60	2.72	0.09	1.89
4.92	1.93	27.46	3.87	106.18	2.68	0.09	2.05
4.94	1.97	27.93	3.78	105.55	2.67	0.09	2.08
4.96	1.89	26.71	3.85	102.85	2.68	0.09	1.99
4.98	1.78	25.16	3.99	100.43	2.70	0.09	1.87
5.00	1.73	24.31	4.10	99.70	2.71	0.08	1.80
5.02	1.71	24.06	4.23	101.71	2.73	0.08	1.78
5.04	1.69	23.74	4.40	104.55	2.75	0.08	1.75
5.06	1.62	22.95	4.77	109.59	2.80	0.08	1.67
5.08	1.56	22.11	5.17	114.30	2.84	0.08	1.60
5.10	1.59	22.44	5.26	118.10	2.85	0.08	1.62
5.12	1.73	24.34	4.82	117.43	2.80	0.08	1.77
5.14	1.85	25.89	4.50	116.56	2.77	0.09	1.90
5.16	1.76	24.59	4.77	117.36	2.80	0.09	1.79
5.18	1.54	21.64	5.50	119.00	2.88	0.08	1.56
5.20	1.38	19.29	6.08	117.29	2.94	0.07	1.38
5.22	1.45	20.12	5.50	110.73	2.88	0.07	1.45
5.24	1.56	21.48	4.86	104.35	2.81	0.08	1.56
5.26	1.57	21.61	4.79	103.40	2.80	0.08	1.57
5.28	1.43	19.65	5.49	107.88	2.88	0.08	1.41
5.30	1.23	16.81	6.62	111.34	2.99	0.07	1.20
5.32	1.09	14.69	7.52	110.48	3.07	0.07	1.05
5.34	1.00	13.43	8.00	107.39	3.11	0.06	0.96
5.36	0.96	12.76	8.24	105.13	3.12	0.06	0.91
5.38	0.94	12.34	8.31	102.49	3.13	0.06	0.88
5.40	0.94	12.31	8.09	99.56	3.11	0.06	0.88
5.42	0.97	12.72	7.48	95.20	3.06	0.06	0.91
5.44	1.04	13.75	6.63	91.09	2.99	0.06	0.98
5.46	1.14	15.10	5.80	87.50	2.91	0.07	1.08
5.48	1.21	15.98	5.39	86.13	2.87	0.07	1.15
5.50	1.22	16.17	5.37	86.91	2.87	0.07	1.17
5.52	1.17	15.46	5.86	90.66	2.92	0.07	1.11
5.54	1.09	14.29	6.71	95.81	3.00	0.07	1.02
5.56	1.00	13.02	7.73	100.60	3.08	0.06	0.93
5.58	0.96	12.44	8.38	104.25	3.14	0.06	0.89
5.60	1.00	12.97	8.21	106.52	3.12	0.06	0.93
5.62	1.08	14.09	7.60	107.09	3.07	0.07	1.01
5.64	1.14	14.85	7.09	105.30	3.03	0.07	1.06
5.66	1.14	14.76	6.94	102.45	3.02	0.07	1.05
5.68	1.16	15.10	6.56	99.02	2.98	0.07	1.08
5.70	1.29	16.78	5.74	96.23	2.90	0.07	1.20
5.72	1.48	19.24	4.84	93.20	2.81	0.08	1.40
5.74	1.63	21.16	4.50	95.22	2.77	0.08	1.54
5.76	1.73	22.42	4.42	99.18	2.76	0.08	1.64

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
5.78	1.83	23.68	4.37	103.48	2.75	0.08	1.73
5.80	1.98	25.62	4.14	106.08	2.72	0.09	1.88
5.82	2.13	27.54	3.95	108.71	2.69	0.09	2.03
5.84	2.11	27.34	4.22	115.35	2.73	0.09	2.00
5.87	1.93	24.99	4.95	123.65	2.82	0.08	1.81
5.88	1.73	22.55	5.80	130.93	2.91	0.08	1.61
5.90	1.74	22.68	5.88	133.35	2.92	0.08	1.62
5.92	1.90	24.58	5.24	128.73	2.85	0.08	1.77
5.94	1.85	23.85	5.19	123.84	2.85	0.09	1.72
5.96	1.62	20.80	5.73	119.25	2.90	0.07	1.49
5.99	1.27	16.00	7.25	115.99	3.04	0.07	1.14
6.00	1.13	14.08	7.72	108.66	3.08	0.06	1.01
6.02	1.10	13.58	7.36	100.01	3.05	0.06	0.97
6.04	1.12	13.77	6.56	90.31	2.98	0.07	0.98
6.06	1.06	12.99	6.68	86.71	2.99	0.06	0.93
6.08	0.98	11.88	7.17	85.11	3.04	0.06	0.85
6.10	0.96	11.57	7.37	85.26	3.05	0.06	0.83
6.12	1.04	12.64	6.64	83.98	2.99	0.06	0.90
6.14	1.19	14.56	5.71	83.14	2.90	0.07	1.04
6.16	1.37	16.86	5.10	86.02	2.84	0.07	1.22
6.18	1.55	19.12	4.73	90.47	2.79	0.08	1.39
6.20	1.70	20.96	4.45	93.30	2.76	0.08	1.52
6.22	1.80	22.15	4.08	90.27	2.71	0.08	1.62
6.24	1.87	22.82	3.68	83.98	2.66	0.08	1.68
6.26	1.92	23.24	3.30	76.63	2.60	0.08	0.64
6.28	1.95	23.53	3.07	72.12	2.56	0.08	0.64
6.30	1.98	23.76	2.93	69.58	2.53	0.08	0.64
6.32	2.01	24.06	2.79	67.15	2.50	0.08	0.64
6.34	2.05	24.44	2.60	63.45	2.46	0.08	0.65
6.36	2.11	24.99	2.37	59.32	2.41	0.08	0.65
6.38	2.18	25.71	2.24	57.55	2.38	0.08	0.65
6.40	2.25	26.60	2.20	58.40	2.37	0.08	0.66
6.42	2.32	27.40	2.23	61.00	2.38	0.08	0.66
6.44	2.37	27.98	2.27	63.42	2.39	0.08	0.66
6.46	2.39	28.25	2.29	64.78	2.40	0.08	0.66
6.48	2.42	28.53	2.26	64.37	2.39	0.08	0.66
6.50	2.46	28.90	2.18	62.97	2.37	0.08	0.67
6.52	2.50	29.26	2.08	60.93	2.34	0.08	0.67
6.54	2.49	29.09	2.07	60.18	2.34	0.08	0.67
6.56	2.42	28.31	2.21	62.53	2.37	0.08	0.66
6.58	2.32	27.21	2.49	67.74	2.44	0.08	0.66
6.60	2.25	26.41	2.70	71.36	2.49	0.09	0.66
6.62	2.24	26.24	2.71	71.00	2.49	0.09	0.65
6.64	2.28	26.66	2.55	67.98	2.45	0.08	0.66
6.66	2.36	27.54	2.46	67.85	2.44	0.08	0.66
6.68	2.41	28.11	2.44	68.69	2.43	0.09	0.66
6.70	2.34	27.25	2.58	70.40	2.46	0.09	0.66
6.72	2.02	23.49	2.96	69.64	2.54	0.09	0.64

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
6.74	1.61	18.59	3.75	69.64	2.66	0.08	1.36
6.76	1.20	13.69	5.35	73.25	2.86	0.07	0.98
6.78	0.97	10.79	6.88	74.21	3.01	0.06	0.77
6.80	0.89	9.80	7.57	74.21	3.07	0.06	0.70
6.82	0.88	9.59	7.63	73.13	3.08	0.06	0.68
6.85	0.87	9.44	7.86	74.14	3.09	0.06	0.67
6.86	0.80	8.61	8.72	75.10	3.16	0.06	0.61
6.88	0.75	7.88	9.39	73.93	3.21	0.06	0.56
6.90	0.69	7.16	10.13	72.56	3.26	0.06	0.51
6.92	0.66	6.71	10.60	71.18	3.29	0.06	0.48
6.94	0.68	7.00	9.95	69.65	3.25	0.06	0.50
6.96	0.78	8.17	8.31	67.93	3.13	0.06	0.58
6.98	0.87	9.31	7.03	65.47	3.03	0.06	0.66
7.00	0.90	9.60	6.75	64.80	3.00	0.06	0.69
7.02	0.85	8.99	7.25	65.24	3.04	0.06	0.64
7.04	0.77	8.03	8.36	67.18	3.13	0.06	0.57
7.06	0.72	7.33	9.41	68.98	3.21	0.06	0.52
7.08	0.70	7.05	10.13	71.44	3.26	0.06	0.50
7.10	0.69	7.02	10.43	73.19	3.28	0.06	0.50
7.12	0.71	7.23	10.20	73.82	3.27	0.06	0.52
7.14	0.74	7.53	9.68	72.88	3.23	0.06	0.54
7.16	0.76	7.80	9.28	72.39	3.20	0.06	0.56
7.18	0.77	7.90	9.29	73.43	3.20	0.06	0.56
7.20	0.76	7.74	9.84	76.14	3.24	0.06	0.55
7.22	0.75	7.56	10.48	79.22	3.28	0.06	0.54
7.24	0.75	7.56	10.84	81.95	3.31	0.06	0.54
7.26	0.76	7.69	10.96	84.29	3.32	0.06	0.55
7.28	0.78	7.90	10.90	86.10	3.31	0.06	0.56
7.30	0.78	7.88	11.08	87.27	3.32	0.06	0.56
7.32	0.76	7.66	11.42	87.49	3.35	0.06	0.55
7.34	0.73	7.24	11.97	86.73	3.38	0.06	0.52
7.36	0.69	6.79	12.54	85.18	3.41	0.06	0.49
7.38	0.68	6.57	12.73	83.63	3.42	0.06	0.47
7.40	0.68	6.59	12.54	82.66	3.41	0.06	0.47
7.42	0.71	6.93	11.87	82.20	3.37	0.06	0.49
7.44	0.74	7.27	11.27	81.92	3.34	0.06	0.52
7.46	0.76	7.57	10.77	81.53	3.30	0.06	0.54
7.48	0.78	7.79	10.41	81.07	3.28	0.06	0.56
7.50	0.80	7.91	10.23	80.93	3.27	0.06	0.56
7.52	0.81	8.01	10.10	80.94	3.26	0.06	0.57
7.54	0.81	8.09	10.05	81.36	3.26	0.06	0.58
7.56	0.81	8.05	10.09	81.19	3.26	0.06	0.57
7.58	0.80	7.88	10.23	80.60	3.27	0.06	0.56
7.60	0.76	7.44	10.68	79.51	3.30	0.06	0.53
7.62	0.73	6.99	11.27	78.78	3.34	0.06	0.50
7.64	0.70	6.62	11.74	77.76	3.36	0.06	0.47
7.66	0.69	6.46	11.81	76.35	3.37	0.06	0.46
7.68	0.70	6.57	11.32	74.32	3.34	0.06	0.47

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
7.70	0.71	6.73	10.71	72.15	3.30	0.06	0.48
7.72	0.73	6.98	10.05	70.17	3.26	0.06	0.50
7.74	0.75	7.11	9.58	68.16	3.22	0.06	0.51
7.76	0.76	7.31	9.01	65.88	3.18	0.06	0.52
7.78	0.79	7.56	8.43	63.72	3.14	0.06	0.54
7.80	0.86	8.44	7.39	62.41	3.06	0.06	0.60
7.82	0.91	9.01	6.92	62.39	3.02	0.06	0.64
7.84	0.94	9.29	6.78	62.98	3.00	0.06	0.66
7.86	0.90	8.80	7.24	63.71	3.04	0.06	0.63
7.88	0.86	8.35	7.60	63.48	3.07	0.06	0.60
7.90	0.82	7.87	7.99	62.87	3.11	0.06	0.56
7.92	0.77	7.21	8.60	61.98	3.15	0.06	0.51
7.94	0.70	6.49	9.35	60.71	3.21	0.06	0.46
7.96	0.66	5.95	9.93	59.04	3.25	0.06	0.42
7.99	0.65	5.87	9.67	56.74	3.23	0.06	0.42
8.00	0.68	6.11	8.99	54.97	3.18	0.06	0.44
8.02	0.72	6.58	8.19	53.95	3.12	0.06	0.47
8.04	0.78	7.24	7.48	54.13	3.06	0.06	0.52
8.06	0.85	8.05	6.79	54.59	3.00	0.06	0.57
8.08	0.93	8.98	6.11	54.82	2.94	0.06	0.64
8.10	1.01	9.84	5.63	55.40	2.89	0.07	0.70
8.12	1.09	10.68	5.31	56.74	2.86	0.07	0.76
8.14	1.17	11.59	5.12	59.32	2.84	0.07	0.83
8.17	1.24	12.38	5.05	62.46	2.83	0.07	0.89
8.18	1.31	13.15	5.05	66.39	2.83	0.07	0.94
8.20	1.36	13.69	5.13	70.21	2.84	0.07	0.98
8.22	1.40	14.08	5.23	73.59	2.85	0.07	1.01
8.24	1.40	14.13	5.35	75.54	2.86	0.07	1.01
8.26	1.39	13.90	5.46	75.98	2.88	0.07	0.99
8.28	1.36	13.60	5.53	75.15	2.88	0.07	0.97
8.30	1.35	13.41	5.54	74.28	2.88	0.07	0.96
8.32	1.35	13.44	5.51	74.02	2.88	0.07	0.96
8.34	1.40	13.94	5.37	74.91	2.87	0.07	1.00
8.36	1.48	14.76	5.17	76.32	2.84	0.07	1.06
8.38	1.59	15.98	4.88	77.99	2.81	0.08	1.15
8.40	1.71	17.29	4.61	79.76	2.78	0.08	1.24
8.42	1.85	18.72	4.31	80.61	2.74	0.08	1.35
8.44	1.98	20.08	4.03	80.84	2.70	0.08	1.45
8.46	2.09	21.27	3.70	78.77	2.66	0.09	1.53
8.48	2.19	22.21	3.41	75.65	2.61	0.09	1.60
8.50	2.26	22.98	3.16	72.62	2.57	0.09	0.64
8.52	2.33	23.68	3.04	71.98	2.55	0.09	0.64
8.54	2.40	24.38	3.04	74.07	2.55	0.09	0.65
8.56	2.46	24.98	3.06	76.39	2.55	0.09	0.65
8.58	2.51	25.48	3.04	77.36	2.55	0.09	0.65
8.60	2.55	25.80	2.95	76.05	2.53	0.09	0.65
8.62	2.57	26.03	2.82	73.53	2.51	0.09	0.65
8.64	2.58	26.05	2.69	69.95	2.48	0.09	0.65

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
8.66	2.55	25.69	2.58	66.38	2.46	0.09	0.65
8.68	2.48	24.92	2.55	63.47	2.45	0.08	0.65
8.70	2.39	23.90	2.61	62.34	2.47	0.08	0.64
8.72	2.29	22.83	2.72	62.17	2.49	0.08	0.64
8.74	2.18	21.61	2.88	62.22	2.52	0.08	0.63
8.76	2.07	20.40	3.12	63.57	2.56	0.08	0.63
8.78	2.02	19.87	3.29	65.37	2.59	0.08	0.62
8.81	2.02	19.86	3.55	70.59	2.64	0.08	1.43
8.82	2.06	20.25	3.80	76.91	2.67	0.08	1.45
8.84	2.07	20.42	4.10	83.79	2.71	0.08	1.47
8.86	2.09	20.52	4.30	88.17	2.74	0.08	1.47
8.88	2.10	20.61	4.40	90.73	2.75	0.08	1.48
8.90	2.14	20.98	4.41	92.44	2.75	0.08	1.50
8.92	2.19	21.53	4.34	93.50	2.75	0.09	1.54
8.94	2.27	22.30	4.21	93.95	2.73	0.09	1.60
8.96	2.35	23.08	4.02	92.69	2.70	0.09	1.66
8.98	2.42	23.82	3.79	90.33	2.67	0.09	1.71
9.01	2.47	24.28	3.57	86.58	2.64	0.09	1.74
9.02	2.48	24.27	3.46	84.04	2.62	0.09	1.74
9.04	2.42	23.68	3.48	82.34	2.62	0.09	1.70
9.06	2.33	22.67	3.59	81.35	2.64	0.09	1.63
9.08	2.21	21.44	3.76	80.62	2.67	0.09	1.54
9.10	2.13	20.56	3.94	81.01	2.69	0.08	1.47
9.12	2.09	20.10	4.13	83.03	2.72	0.08	1.44
9.14	2.08	19.93	4.30	85.63	2.74	0.08	1.43
9.16	2.06	19.72	4.43	87.38	2.76	0.08	1.41
9.18	2.04	19.45	4.47	87.02	2.76	0.08	1.39
9.20	2.03	19.35	4.42	85.62	2.76	0.08	1.38
9.22	2.03	19.35	4.32	83.59	2.74	0.08	1.38
9.24	2.05	19.46	4.25	82.70	2.73	0.08	1.39
9.26	2.06	19.51	4.17	81.41	2.72	0.08	1.40
9.28	2.08	19.69	4.07	80.10	2.71	0.08	1.41
9.30	2.11	20.01	3.95	79.05	2.69	0.08	1.43
9.32	2.17	20.59	3.83	78.78	2.68	0.08	1.47
9.34	2.23	21.10	3.74	78.81	2.66	0.09	1.51
9.36	2.26	21.43	3.64	78.03	2.65	0.09	1.53
9.38	2.25	21.26	3.61	76.75	2.64	0.09	1.52
9.40	2.22	20.89	3.63	75.72	2.65	0.09	1.49
9.42	2.16	20.23	3.71	75.07	2.66	0.08	1.45
9.44	2.10	19.62	3.80	74.55	2.67	0.08	1.40
9.46	2.04	19.02	3.90	74.21	2.69	0.08	1.36
9.48	2.02	18.75	4.01	75.16	2.70	0.08	1.34
9.50	2.03	18.80	4.15	78.04	2.72	0.08	1.34
9.52	2.06	19.14	4.20	80.37	2.73	0.08	1.37
9.54	2.09	19.34	4.22	81.66	2.73	0.08	1.38
9.56	2.07	19.17	4.22	80.94	2.73	0.08	1.37
9.58	2.01	18.50	4.28	79.25	2.74	0.08	1.32
9.60	1.92	17.55	4.35	76.37	2.75	0.08	1.25

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
9.62	1.81	16.42	4.44	72.94	2.76	0.08	1.17
9.64	1.71	15.44	4.59	70.97	2.78	0.08	1.10
9.66	1.65	14.83	4.84	71.75	2.81	0.08	1.06
9.68	1.63	14.58	5.17	75.30	2.84	0.07	1.04
9.70	1.63	14.54	5.42	78.75	2.87	0.07	1.04
9.72	1.65	14.71	5.50	80.92	2.88	0.07	1.05
9.74	1.70	15.18	5.35	81.19	2.86	0.07	1.08
9.76	1.77	15.83	4.91	77.78	2.81	0.08	1.13
9.78	1.83	16.43	4.51	74.16	2.77	0.08	1.17
9.80	1.86	16.68	4.19	69.98	2.73	0.08	1.19
9.82	1.87	16.73	4.11	68.71	2.72	0.08	1.19
9.84	1.86	16.61	4.03	66.87	2.70	0.08	1.18
9.86	1.85	16.57	3.97	65.77	2.70	0.08	1.18
9.88	1.86	16.62	3.94	65.51	2.69	0.08	1.19
9.90	1.88	16.80	3.94	66.20	2.69	0.08	1.20
9.92	1.93	17.27	3.88	66.95	2.68	0.08	1.23
9.94	2.01	17.98	3.75	67.47	2.67	0.08	1.28
9.96	2.12	19.03	3.52	67.07	2.63	0.08	1.36
9.98	2.24	20.22	3.28	66.34	2.59	0.08	0.62
10.00	2.36	21.35	3.05	65.13	2.55	0.08	0.63
10.02	2.47	22.37	2.85	63.71	2.52	0.08	0.64
10.04	2.54	23.05	2.68	61.67	2.48	0.08	0.64
10.06	2.58	23.44	2.54	59.65	2.45	0.08	0.64
10.08	2.55	23.11	2.49	57.60	2.44	0.08	0.64
10.11	2.49	22.44	2.51	56.29	2.45	0.08	0.64
10.12	2.43	21.92	2.54	55.67	2.45	0.08	0.63
10.14	2.42	21.79	2.60	56.65	2.47	0.08	0.63
10.16	2.45	22.03	2.68	59.04	2.48	0.08	0.63
10.18	2.49	22.39	2.74	61.40	2.49	0.08	0.64
10.20	2.54	22.84	2.75	62.75	2.50	0.08	0.64
10.22	2.57	23.09	2.74	63.17	2.49	0.09	0.64
10.24	2.56	22.90	2.80	64.06	2.51	0.09	0.64
10.26	2.49	22.19	2.94	65.26	2.53	0.09	0.63
10.28	2.36	20.93	3.12	65.30	2.57	0.08	0.63
10.30	2.23	19.69	3.27	64.41	2.59	0.08	0.62
10.32	2.13	18.63	3.50	65.17	2.63	0.08	1.32
10.34	2.07	17.98	3.94	70.92	2.69	0.08	1.28
10.36	2.06	17.84	4.38	78.10	2.75	0.08	1.27
10.38	2.11	18.29	4.58	83.76	2.78	0.08	1.30
10.40	2.21	19.28	4.46	86.04	2.76	0.08	1.37
10.42	2.32	20.31	4.25	86.23	2.73	0.09	1.45
10.44	2.41	21.06	4.06	85.48	2.71	0.09	1.50
10.46	2.45	21.45	3.86	82.86	2.68	0.09	1.53
10.48	2.46	21.56	3.68	79.31	2.65	0.09	1.53
10.50	2.48	21.75	3.39	73.73	2.61	0.09	1.54
10.52	2.51	21.96	3.12	68.46	2.56	0.09	0.63
10.54	2.51	21.98	2.93	64.39	2.53	0.09	0.63
10.56	2.47	21.53	2.90	62.40	2.52	0.08	0.63

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
10.58	2.38	20.67	2.94	60.86	2.53	0.08	0.63
10.60	2.29	19.81	2.96	58.67	2.54	0.08	0.62
10.62	2.24	19.34	2.91	56.20	2.53	0.08	0.62
10.64	2.26	19.46	2.86	55.58	2.52	0.08	0.62
10.66	2.35	20.27	2.89	58.50	2.52	0.08	0.62
10.68	2.47	21.43	2.93	62.88	2.53	0.08	0.63
10.70	2.64	22.97	2.91	66.83	2.53	0.09	0.64
10.72	2.75	23.93	2.87	68.66	2.52	0.09	0.64
10.74	2.76	24.02	2.85	68.58	2.52	0.09	0.64
10.76	2.65	22.93	2.81	64.43	2.51	0.09	0.64
10.78	2.53	21.88	2.67	58.52	2.48	0.08	0.63
10.80	2.47	21.31	2.52	53.59	2.45	0.08	0.63
10.82	2.43	20.91	2.54	53.18	2.45	0.08	0.63
10.84	2.31	19.71	2.84	55.94	2.51	0.08	0.62
10.86	2.11	17.71	3.39	60.11	2.61	0.08	1.25
10.88	1.86	15.37	4.19	64.46	2.73	0.08	1.09
10.91	1.63	13.17	5.01	65.91	2.83	0.07	0.94
10.92	1.47	11.64	5.67	65.96	2.90	0.07	0.83
10.94	1.40	11.05	5.91	65.31	2.92	0.07	0.79
10.96	1.53	12.14	5.49	66.63	2.88	0.07	0.87
10.98	1.73	14.01	4.91	68.77	2.81	0.08	1.00
11.00	1.95	16.01	4.47	71.54	2.76	0.08	1.14
11.02	2.09	17.32	4.16	72.14	2.72	0.08	1.23
11.04	2.20	18.33	3.84	70.42	2.68	0.08	1.30
11.06	2.32	19.37	3.49	67.54	2.63	0.08	1.37
11.08	2.44	20.54	3.21	65.88	2.58	0.08	0.63
11.10	2.63	22.24	2.88	63.96	2.52	0.09	0.64
11.12	2.80	23.80	2.64	62.82	2.47	0.09	0.64
11.14	2.89	24.64	2.49	61.32	2.44	0.09	0.65
11.16	2.84	24.20	2.53	61.30	2.45	0.09	0.65
11.18	2.75	23.29	2.57	59.78	2.46	0.08	0.64
11.21	2.66	22.43	2.58	57.82	2.46	0.08	0.64
11.22	2.62	22.04	2.56	56.37	2.46	0.08	0.63
11.24	2.64	22.24	2.55	56.79	2.46	0.08	0.64
11.26	2.70	22.69	2.57	58.24	2.46	0.08	0.64
11.28	2.73	23.03	2.51	57.74	2.45	0.08	0.64
11.30	2.71	22.81	2.46	56.15	2.44	0.08	0.64
11.32	2.64	22.18	2.43	53.90	2.43	0.08	0.63
11.34	2.51	20.93	2.54	53.15	2.45	0.08	0.63
11.36	2.28	18.74	2.88	53.89	2.52	0.08	0.62
11.38	1.95	15.68	3.61	56.54	2.64	0.08	1.11
11.40	1.62	12.57	4.79	60.21	2.80	0.07	0.90
11.42	1.43	10.84	5.73	62.16	2.90	0.07	0.77
11.44	1.43	10.81	5.85	63.25	2.92	0.07	0.77
11.46	1.63	12.63	4.98	62.83	2.82	0.07	0.90
11.48	1.96	15.58	4.08	63.56	2.71	0.08	1.10
11.50	2.32	18.87	3.43	64.75	2.62	0.08	1.33
11.52	2.65	21.84	2.98	65.14	2.54	0.09	0.63

:: Strength loss calculation (Idriss & Boulanger (2008) :: (continued)

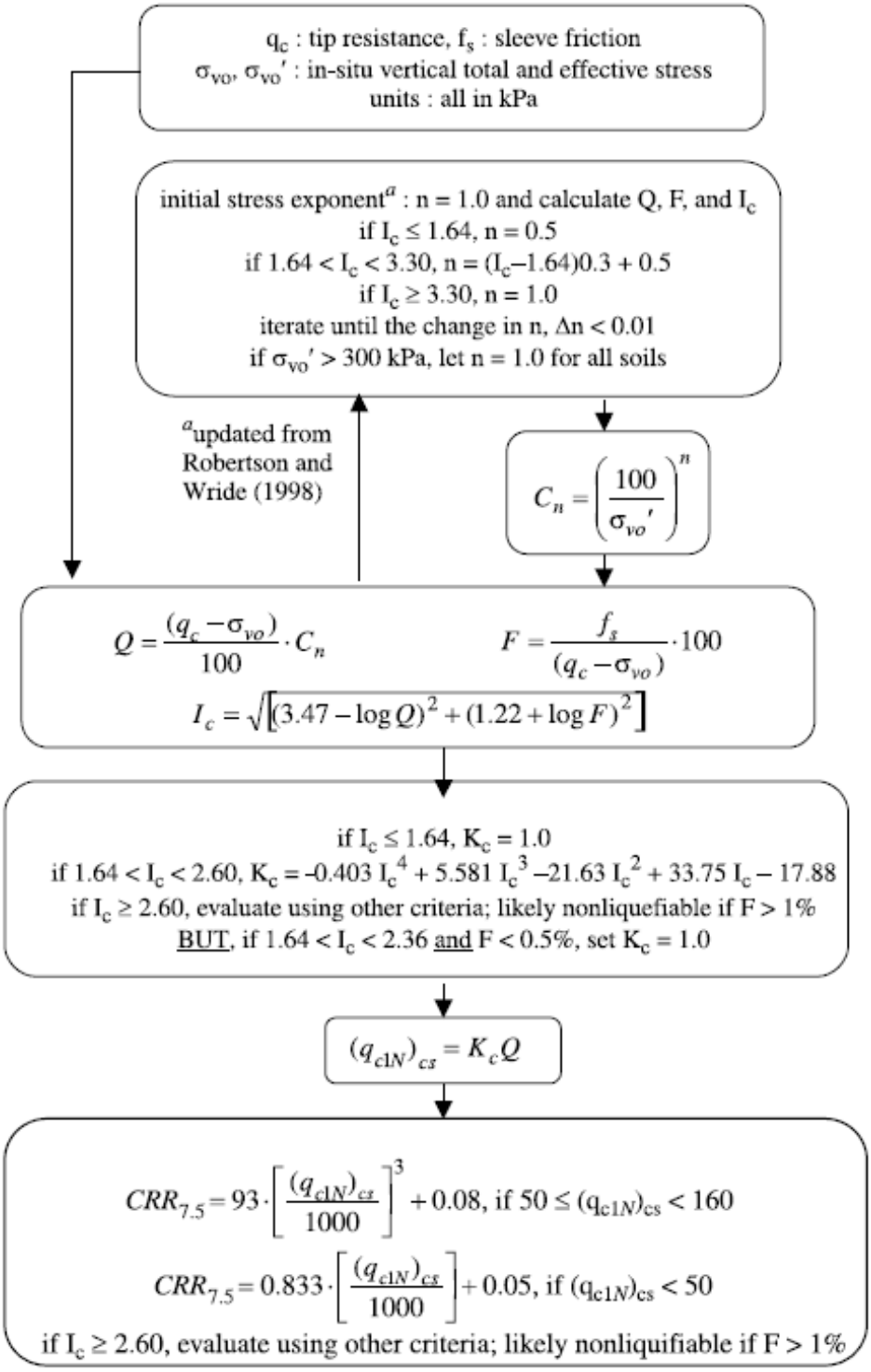
Depth (m)	q_t (MPa)	Q_{tn}	K_c	$Q_{tn,cs}$	I_c	$S_{u(liq)}/\sigma'_v$	$S_{u(peak)}/\sigma'_v$
11.54	2.90	24.14	2.63	63.42	2.47	0.09	0.64
11.56	3.11	26.08	2.32	60.51	2.40	0.09	0.65
11.58	3.24	27.22	2.13	57.96	2.35	0.08	0.66
11.60	3.26	27.47	2.01	55.29	2.32	0.08	0.66
11.62	3.18	26.74	1.96	52.54	2.30	0.08	0.66
11.64	3.06	25.63	1.92	49.11	2.29	0.08	0.65
11.66	2.97	24.81	1.89	46.95	2.28	0.08	0.65
11.68	2.91	24.34	1.00	24.34	2.24	0.07	0.65

Abbreviations

q_t:	Total cone resistance
K_c:	Cone resistance correction factor due to fines
$Q_{tn,cs}$:	Adjusted and corrected cone resistance due to fines
I_c:	Soil behavior type index
$S_{u(liq)}/\sigma'_v$:	Calculated liquefied undrained strength ratio
$S_{u(peak)}/\sigma'_v$:	Calculated peak undrained strength ratio

Procedure for the evaluation of soil liquefaction resistance, NCEER (1998)

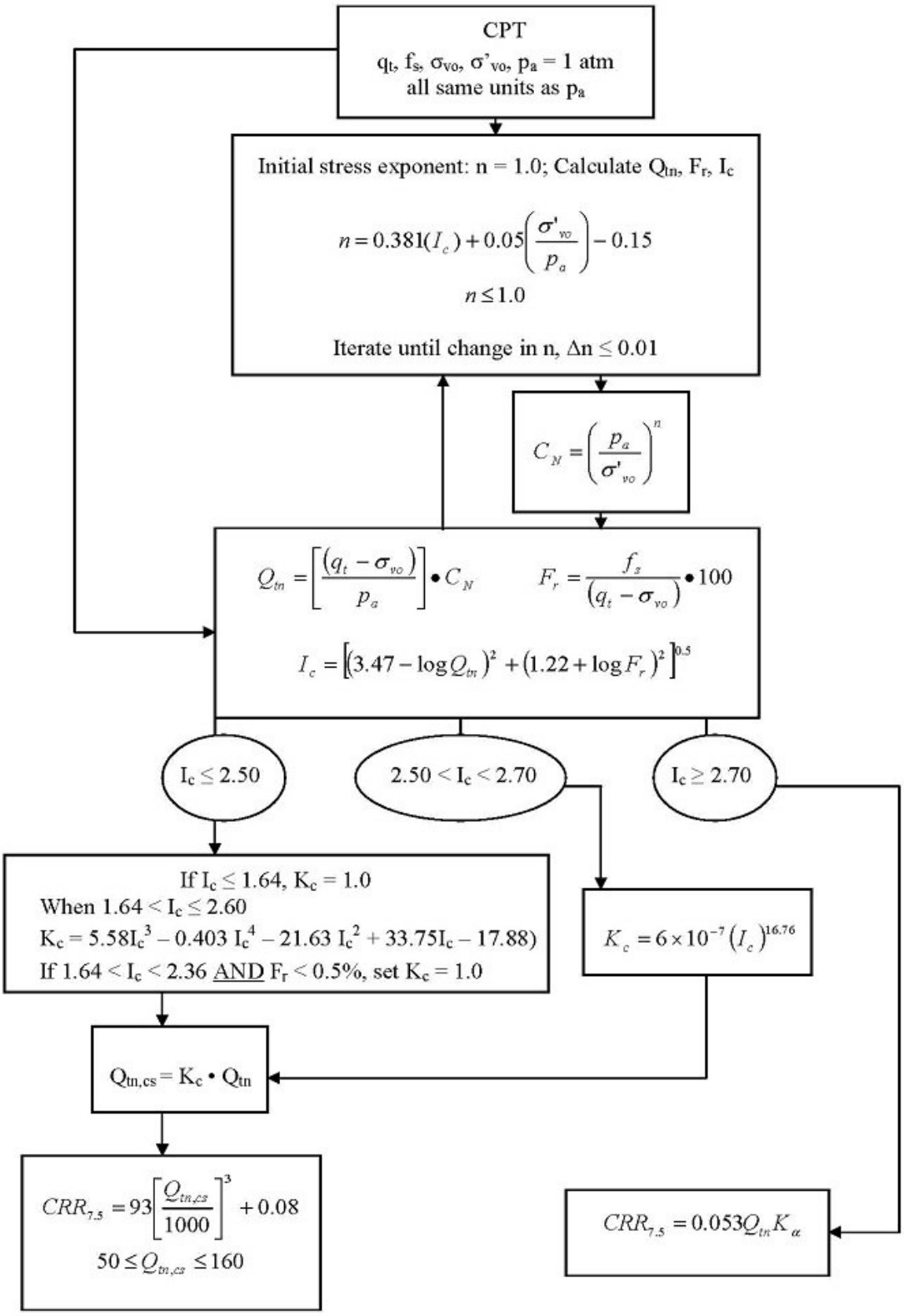
Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. The procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:



[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

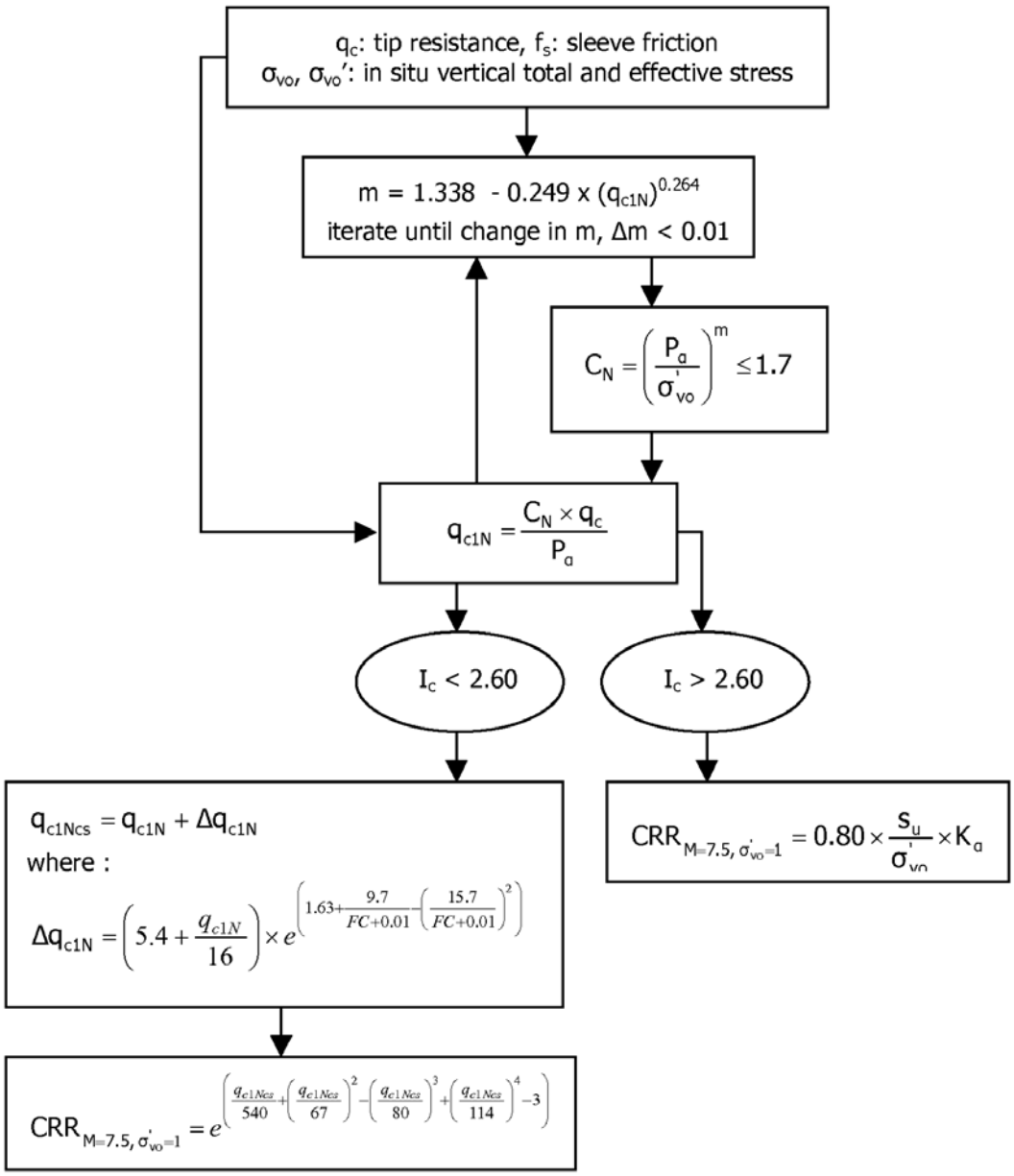
Procedure for the evaluation of soil liquefaction resistance (all soils), Robertson (2010)

Calculation of soil resistance against liquefaction is performed according to the Robertson & Wride (1998) procedure. This procedure used in the software, slightly differs from the one originally published in NCEER-97-0022 (Proceedings of the NCEER Workshop on Evaluation of Liquefaction Resistance of Soils). The revised procedure is presented below in the form of a flowchart[1]:

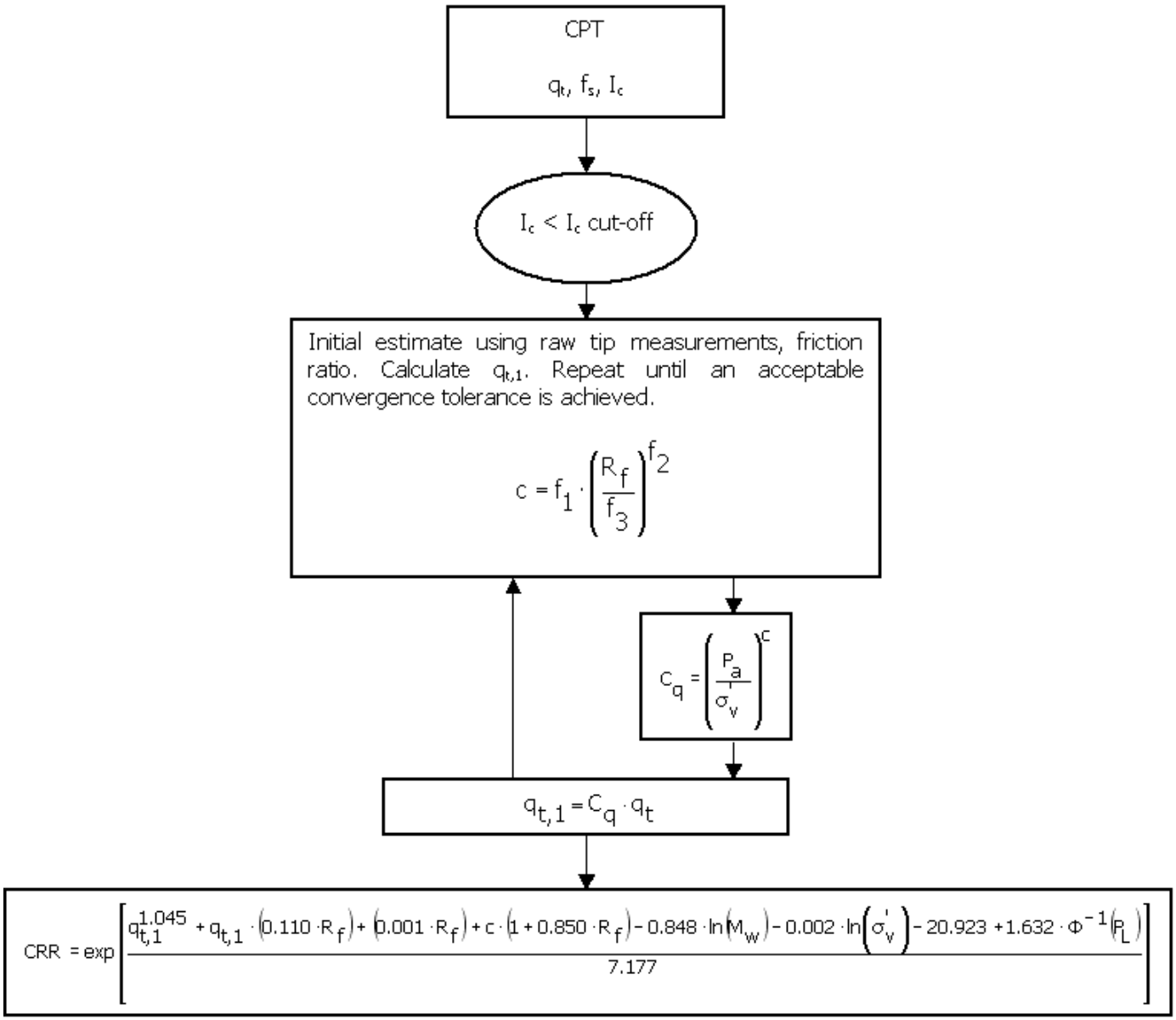


[1] P.K. Robertson, 2009. "Performance based earthquake design using the CPT", Keynote Lecture, International Conference on Performance-based Design in Earthquake Geotechnical Engineering – from case history to practice, IS-Tokyo, June 2009

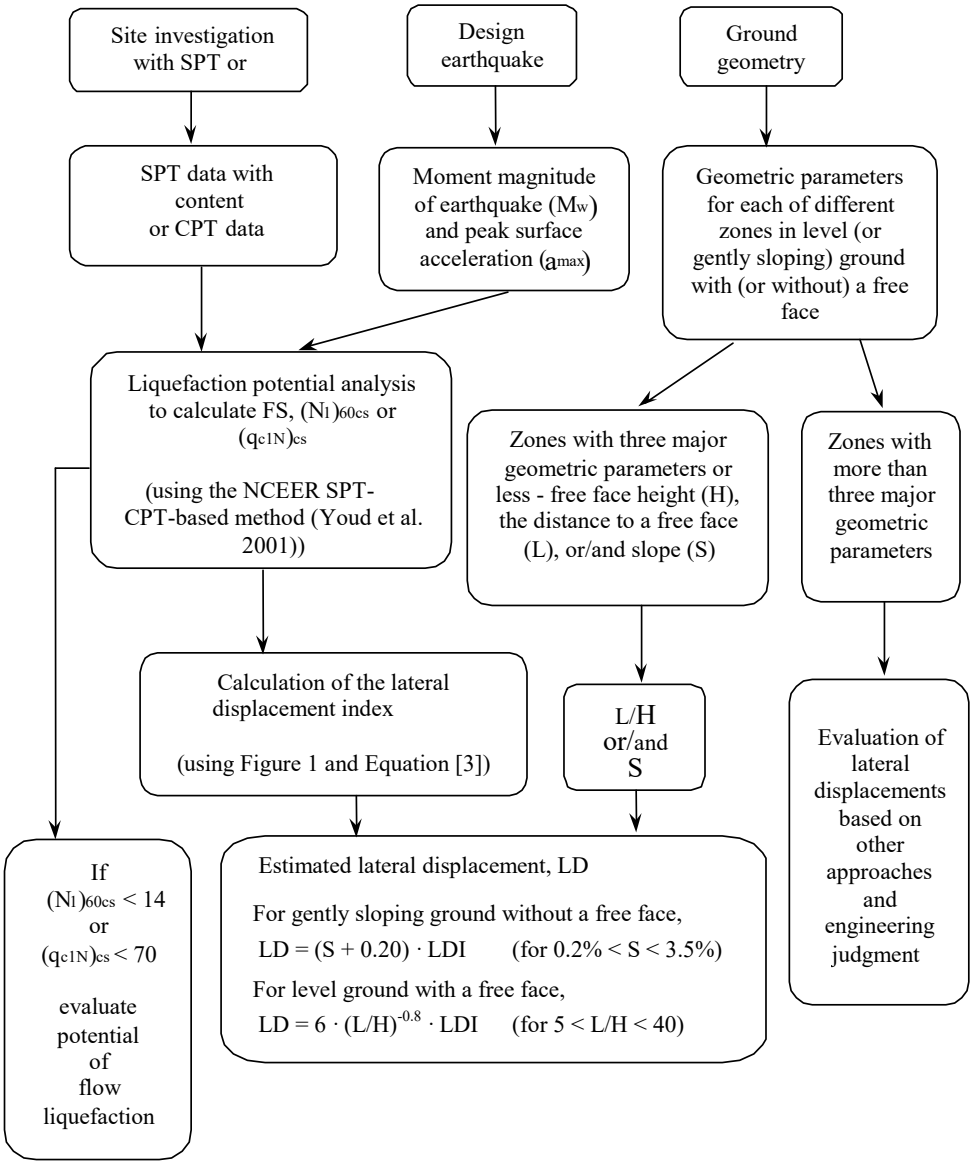
Procedure for the evaluation of soil liquefaction resistance, Idriss & Boulanger (2008)



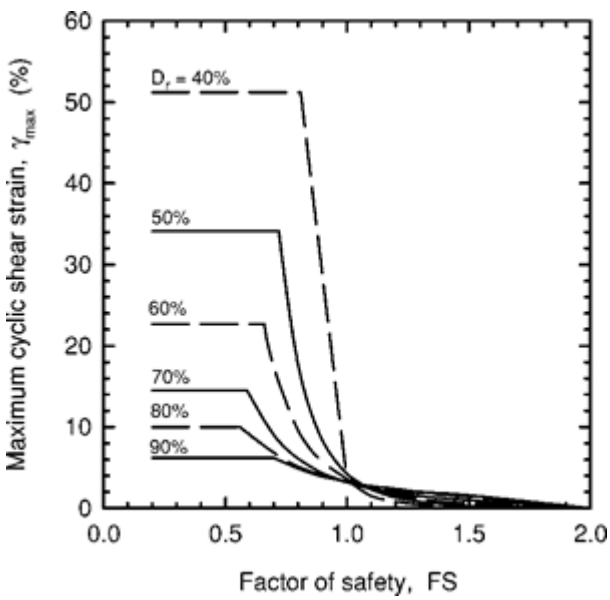
Procedure for the evaluation of soil liquefaction resistance (sandy soils), Moss et al. (2006)



Procedure for the evaluation of liquefaction-induced lateral spreading displacements



[1] Flow chart illustrating major steps in estimating liquefaction-induced lateral spreading displacements using the proposed approach



[1] Figure 1

$$LDI = \int_0^{z_{max}} \gamma_{max} dz$$

[1] Equation [3]

[1] "Estimating liquefaction-induced ground settlements from CPT for level ground", G. Zhang, P.K. Robertson, and R.W.I. Brachman

Procedure for the estimation of seismic induced settlements in dry sands

Average shear stress, τ_{av}

$$\tau_{av} = CSR^{*} \cdot \sigma_{v0}' = 0.65 \cdot \frac{a_{max}}{g} \cdot \sigma_{v0} \cdot r_a$$

Estimate small shear strain modulus, G_0

$$G_0 = 0.0188 \cdot \left[10^{(0.55 I_c + 1.68)}\right] \cdot (q_t - \sigma_v)$$

Estimate shear strain amplitude, γ

(based on Pradel (1998))

$$\gamma = \left[\frac{1 + \alpha \cdot e^{bR}}{1 + \alpha}\right] \cdot R \cdot 100 \ (\%)$$

$$R = \frac{\tau_{av}}{G_0} \text{ (Note } \tau_{av} \text{ and } G_0 \text{ same units)}$$

$$\alpha = 0.0389 \cdot \left(\frac{\sigma_v}{p_a}\right) + 0.124$$

$$b = 6400 \cdot \left(\frac{\sigma_v}{p_a}\right)$$

Estimate volumetric strain in 15 cycles

$$\varepsilon_{vol(15)} = \gamma \cdot \left[\frac{(N_1)_{60,cs}}{20}\right]^{-1.20}$$

$$(N_1)_{60,cs} = \frac{Q_{tn,cs}}{8.5 \cdot \left[1 - \frac{I_c}{4.6}\right]}$$

Volumetric strain in design earthquake

$$\Sigma_{vol} = \varepsilon_{vol(15)} \cdot \left[\frac{N_c}{15}\right]^{0.45}$$

$$N_c = (M - 4)^{2.17}$$

Seismic settlement, s

$$s = 2 \cdot \int_0^{GWT} \Sigma_{vol} \cdot dz$$

Robertson, P.K. and Lisheng, S., 2010, "Estimation of seismic compression in dry soils using the CPT" FIFTH INTERNATIONAL CONFERENCE ON RECENT ADVANCES IN GEOTECHNICAL EARTHQUAKE ENGINEERING AND SOIL DYNAMICS, Symposium in honor of professor I. M. Idriss, San Diego, CA

Liquefaction Potential Index (LPI) calculation procedure

Calculation of the Liquefaction Potential Index (LPI) is used to interpret the liquefaction assessment calculations in terms of severity over depth. The calculation procedure is based on the methology developed by Iwasaki (1982) and is adopted by AFPS.

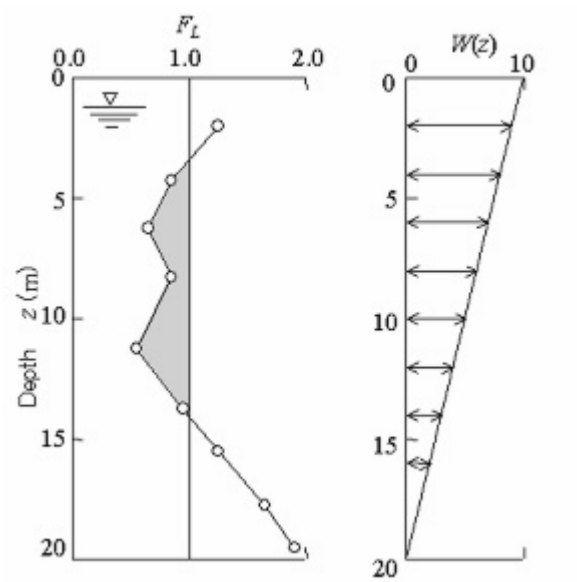
To estimate the severity of liquefaction extent at a given site, LPI is calculated based on the following equation:

$$\text{LPI} = \int_0^{20} (10 - 0{,}5_Z) \times F_L \times d_z$$

where:
F_L = 1 - F.S. when F.S. less than 1
F_L = 0 when F.S. greater than 1
z depth of measurment in meters

Values of LPI range between zero (0) when no test point is characterized as liquefiable and 100 when all points are characterized as susceptible to liquefaction. Iwasaki proposed four (4) discrete categories based on the numeric value of LPI:

- LPI = 0 : Liquefaction risk is very low
- 0 < LPI <= 5 : Liquefaction risk is low
- 5 < LPI <= 15 : Liquefaction risk is high
- LPI > 15 : Liquefaction risk is very high



Graphical presentation of the LPI calculation procedure

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